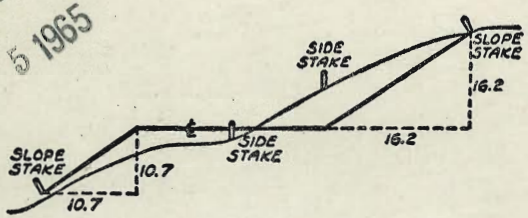
2270

SEWER



Distances from Side Stakes for Cross-Sectioning

Slope 1 to 1. Roadway of Any Width

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

Table XIII—Corrections for Tangents and Externals

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

For Tangents Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	03	.06	09	13	16	19	.22	.25	.28	.31	34	38	42	.46
15°	04	10	14	19	24	.29	.34	.39	45	.51	.53	58	.63	.68
20°	06	.13	19	.26	.32	.39	.45	.51	.58	.65	.72	79	.84	.90
25°	.08	16	24	.33	40	49	.58	67	.75	.83	90	.99	1.06	1.14
30°	10	19	.29	39	49	.59	.69	79	.89	.99	1.09	1.20	1.29	1.39
35°	11	22	.34	47	.58	.69	.70	.81	.92	1.04	1.29	1.42	1.54	1.66
40°	13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94
45°	15	.30	44	60	76	91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21
50°	17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48
55°	19	38	.57	76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77
60°	.21	42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07
65°	23	46	.69	.93	1.16	1 40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39
70°	25	.51	76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09
80°	30	.61	.91	1.22	1.53	1.84	2.15	2.46	2 78	3.10	3.44	3.78	4.12	4.46
85°	33	66	1.00	1.33	1.68	2.02	2.36	2 70	3.05	3.40	3.77	4.14	4.55	4 89
90°	36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32
95°	39	79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34
110°	51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4 76	5.31	5 86	6.43	7 01	7 60
120°	62	1.25	1 93	2.52	3.16	3.81	4 45	5.11	5.77	6 44	7 12	7.80	8.50	9 22

For Externals Add

Central Angle	Degree of Curve													
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083
25°	.009	.018	.027	036	.046	.056	.065	.074	.083	.093	.106	120	127	135
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.711	.845	.922	1.01
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20
95°	.174	.350	.522	.706	.985	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32

INDEX Pg

Proposed Sewer - Lot 53 Ex-Mission Lands) 48
S'wly Euclid + Churchwood

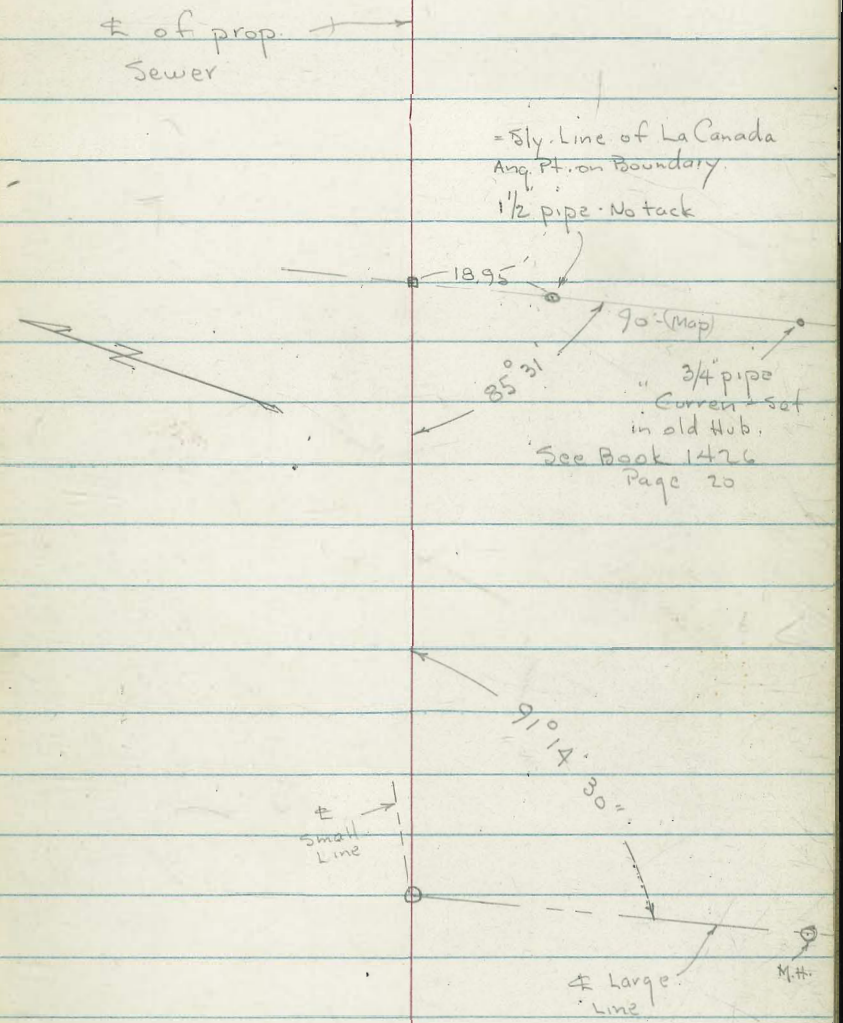
Survey for Prop. Sewer in
La Canada Canyon -

6927

W.O. 21075 5-19-53 7.0.

1+87.39 = Set Hub. on Ely. Line of La Jolla Hermosa - Prod. from S.

0+00 = ℄ Exist. Sewer M.H. Folsom Drive & La Canada



16+09.70 = Ang. 4° 36' Rt. = Hub.

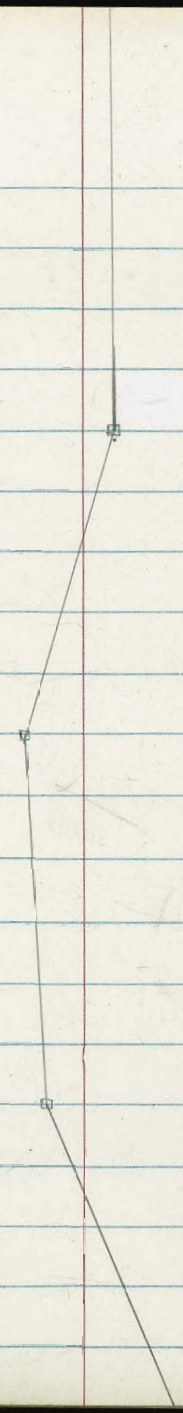
13+49.74 = Ang. 12° 48' Lt. = Hub.

3+71.84 = Ang. 9° 06' Lt. = Hub.

25+75.22 = Ang. 21° 24' Lt. = Hub.

21+37.68 = Ang. 11° 11' Rt. = Hub.

19+58.72 = Ang. 20° 28' Rt. = Hub.



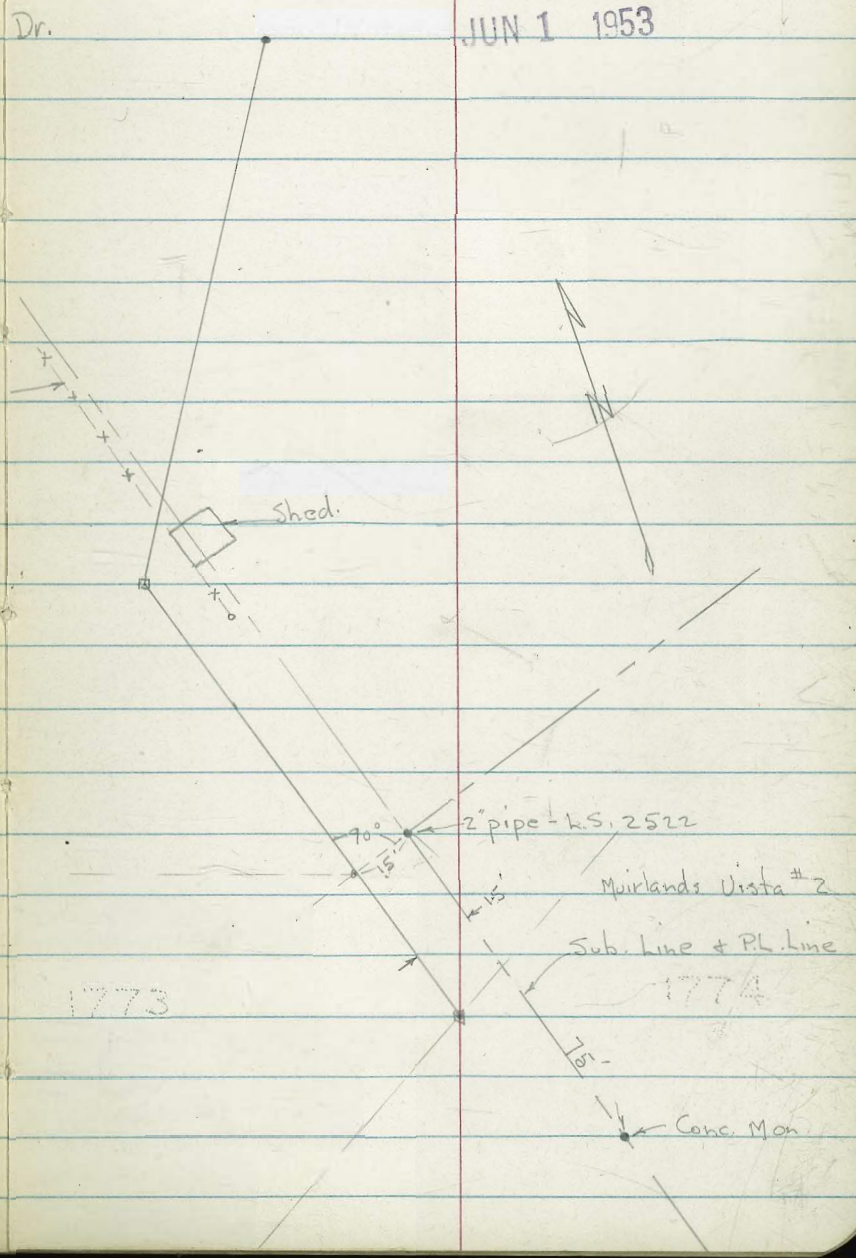
34+40 = P.K. about ℄ of Paue – La Jolla Mesa Dr.

6' Cyclone fence

31+46.95' = Ang. 45° 11' Rt. = Hub.

29+13.32 = Nail – 90° to Sub. Cor.

28+87.55' = Ang. 76° 56' Lt. – 15' from Sub. line = Hub.



Begin Levels along ℄ of Prop. Sewer in La Canada Canyon - See Sketch - P. 1

See Note Below before Reducing.

				Lt.		℄	Rt.		
1+40				8.95 23.5 in gut. Dr	8.69 10	8.82	9.10 6.5 gut.	8.45 Top	8.23 11.5 walk
T.P.	13.18	207.29	-0.28	194.11		207.29			
1+00				0.96 Top	1.56 22.8 gut.	12.3 10	1.29	1.54 7 gut.	0.91 Top	0.91 12 walk
0+70				3.93 Top	4.61 23.1 gut.	4.20 10	4.25	4.42 6.7 gut.	3.84 Top	3.70 11.7 walk
0+47.7 = opp. P.C. of Ret. on Rt				4.98 Top	5.61 24.8 gut.	5.31 10	5.38	5.59 5.7 gut.	4.88 Top = P.C.	4.76 10.7 = walk
0+30				5.60 Top cb.	6.26 33 gut.	5.99 15	5.99		6.27 9.6 gut.	5.59 Top	5.58 15.3 edge walk
0+15						6.47 10	6.52 conc. pave			7.21 24.8 gut.	6.66 Top cb.
0+00 = ℄ Exist. MH.				7.30 25	7.04 Rim		194.39 = π		19.12 I.E.	7.29 25 Conc. Pave

Note: All H.I.s are 8.66 too High

B.M.	+430	194.39 π	181.43 = Corr. ~~190.09~~ = Top of N.W. Hyd. - Folsom Dr. & La Canada Book 142 - P. 20	

					Lt.	℄	Rt.
T.P.	7.53	238.99	0.28	231.46 = Stub -3+20 25' Rt			
3+21 = Wire Dam on Lt. - 7.4' To S. end.					8.1 12.3 7.3 6.2 2.7 20 20 22.5 14.8 8 7.4 15 Top ℄ wash ℄ Rail ℄ Rail in Conc. Bottom		
2+95					13.5 14.4 13.2 9.3 4.4 30 12 5 20 ℄ wash		
T.P.	12.94	231.74	0.65	218.80 = Top Rail - 6.3 Rt. 2+68		231.74	
2+69 = Top					2.5 2.3 1.1 +1.0 20 11 20		
2+68 = Wire Dam					5.5 4.7 4.9 1.1 +1.0 30 16 8.7 0.4 6.3 6 11 20 ℄ Rail ℄ Rail		
Wire Dams = R.R. Iron posts - Heavy wire mesh + ½" Cables							
2+23 = Top of Dam					5.8 6.1 4.0 30 30		
2+22 = Wire Dam					8.7 8.3 8.1 4.0 30 16.3 9 1.6 4.3 12.1 15 30 ℄ Rail ℄ Rail		
check 2" pipe		116.1		207.84 = Brook 1426			
1+80 = Top of Dam					10.4 10.1 10.5 8.4 20 20 50		
T.P.	12.19	219.45 See B. 1426	0.03	207.26		219.45	
end of cb. + Pave is Covered							
1+79 = face of Vert. Dirt Dam - Wire + R.R. Iron Support					3.19 3.94 3.54 3.69 3.83 3.04 29.5 0.5 Top 25.7 15 12 3.8 4 = 4.3 9.3 15 g.t. ℄ Rail ℄ Rail Set in Conc. g.t. Top walk		
1+76.5 - 4.5 Rt. = cb. face at ℄ of 5.7 opening							
.40 High = outlet for abandoned Drain						207.29	- .866 Too High

Lt. ℄ Rt.

5+50.5 = Wire Dam - Mostly buried

10.6 9.5
23.5 15.5 7.5 Bot. Top 0.7 9.3 17.2
℄ Rail ℄ Rail

5+30

11.4 10.7 11.2 11.8
45 20 26
Toe Toe

Set B.M. = Top of end Rail - Wly. 6.68 245.45
Left of Dam

5+19 = Wire Dam - no bank - wire 4' High

17 9.3 1.4 7 14.8
℄ Rail ℄ pipe 252.13 ℄ Rail
4

T.P. 13.19 252.13 0.05 238.94

4+92 = Wire Dam

5.3 0.8 4.0 0.3 0.0 2.1 4.0
Bot. 30 18 9.1 1.5 Bot. Top 7.4 1.5 23 25 28 Bot.
Top ℄ Rail ℄ Rail Top Top
℄ wash ℄ wash

4+50

6.5 6.2 6.3 7.1
40 15 30
Toe ℄ wash Toe

℄

4+09 = Wire dam

Cor Sect.
Ang as shown

9.1 7.5 11.0 7.4 11.7 7.7 6.7 0.8
40 Bot. 15 11.7 3.9 4.5 11 12 20
Bot. Top Top ℄ Rail Bot. Top ℄ Rail
~~℄ wash~~

3+90 = ℄ at Bot. of Bank

11.9

3+71.84 = Ang. Pt. - Sect. 90° to Back Tang. 15.2 Bot.

13.8 12.7 7.5 5.32 +0.4
20 18.5 10.5 10 6 on Hub. 15
℄ wash ℄ Rail
Top

238.99

					Lt.	℄	Rt.
8+40					8.2 40 Toe	7.2	8.5 21 ℄ wash + Toe
8+13 = Wire Dam Mostly Covered.							1.8 ℄ Rail 9.6 17.3
8+00							
T.P.	12.97	277.48	0.25	264.51 - Top Rail	11.9 43 ℄ wash 9.6 15	10.3 277.48	13.1 15 ℄ wash 10.2 26
7+52 = ℄ Wire Dam					12.8 Rt. 7+52		
7+00					2.4 23 ℄ wash 19.5 11.2 3.2 ℄ Rail	3.1 Bot.	1.6 Top 5.1 ℄ Rail 2.2 10 Top ℄ wash 5.7 Bot. 12.8 Rail 0.7 29 Bank
6+47 = Wire Dam					5.7 35 Toe	6.0	7.9 20 ℄ wash 7.1 28 Toe
T.P.	13.21	264.76	0.58	251.85 - Top Rail 20.3 Lt.	13.0 9.1 Bot. 35 20 12.4 4.2 at Toe Top ℄ rail 5+28	13.7 Bot. 264.76	9.2 Top 3.8 12.1 14.0 10.0 9.4 ℄ Rail 15 Top 26 Bot. Toe ℄ wash
5+28 = Wire Dam					5.6 2.1 Bot. 21 ℄ wash Top 20.3 11.3 ℄ Rail	2.9	3.4 4 ℄ wash 5.5 ℄ Rail 14.2 2.6 15 ℄ wash
5+24 - 2.3 Lt. - ℄ Rail pushed downstrem from Dam.							
5+83 = Wire Dam - 3' above to Top.					7.4 38 5.5 Toe 16.5 Top 8.5 ℄ Rail 12 ℄ wash 8.9 Bot. ℄ pipe	7.2 Bot. 252.13	5.9 Top 0.4 8.2 16.2 7.5 2.9 ℄ Rail 23 25.8 ℄ wash end no bank Rail

— 8.66 Too High

					Lt.		℄		Rt.		
11+10					10.8 50 ℄ Main wash	12.3 28 ℄ wash - small	11.4		10.5 13 = Bank		5.2 15 = Top
T.P.	13.25	302.32	0.10	289.07			302.32				
10+65						1.4 30 ℄ wash	2.1		2.8 12 = Bank		
10+35						4.1 24 ℄ wash	4.7		4.6 14 = Bank - 8'		
10+14 = ℄ wash						5.4 20	7.6 ℄ wash		5.3 14 Toe Bank		
9+80 = Wire Dam - Mostly covered					9.0 40	15.6 7.3 ℄ rail	10.4 Bot.	7.8 Top	1 9 ℄ Rail	8.7 12.4 10 Top Bot. ℄ wash	8.4 16 Toe
9+30					12.3 40	12.6 20	13.5	14.4 8 ℄ wash	13.6 19 = Toe of Bank		
T.P.	13.03	289.17	1.34	276.14			289.17				
~~9+30~~											
8+75 = Wire dam				4.0 38 Toe	6.6 4.9 Bot. 20 Top ℄ wash	19.6. 10.8 2.2 ℄ rail	4.8	5.5 6.8 4 Top Bot. ℄ wash	5.8 1.4 ℄ Rail		4.2 25 Toe
							277.48				

						Lt.		℄		Rt.	
								19.6			
						14.1 17 Side wash	14.3 7 in wash	7.3	2.5 4	3.2 20	1.3 37 Toe
								9.2	4.1 2		
								4.3			
						17.0 20 10' wide	7.5 18 Bot. edge	10.5 8 ℄ gulley	6.88 on Hub.	6.9 20	5.4 32 = Toe
13+85 = opp side wash on Lt.											
13+72											
13+70											
13+49.74 = Avg. Pt. - Sect. on split											
T.P.	13.23	326.92	0.98	313.69 = Rock 10' Rt - 12+95				326.92			
13+00						9.4 12 in wash 10' wide	1.1 8	1.1		0.5 34 Toe	
12+50						13.4 20 ℄ wash	7.1 8	7.1	6.5 32	Toe	
12+00						16.8 25 ℄ wash	13.2 19	13.0		12.3 32 Toe	
T.P.	12.53	314.67	0.18	302.14				314.67			
11+55						8.2 45 ℄ wash	6.8 20	5.8	5.3 18 Bank - 7' High		
								302.32			

						Lt.	℄	Rt.		
T.P	12.65	350.51	1.68	337.86 =	Stub. 14+80					
14+65							34.8 / 4.7			
						0.3 / 28 / 20' Bank	4.3 / 15		4.7 / 10	17.2 / 15 / Bot. - 5' wide
14+40							31.2 / 8.3			
						0.6 / 20 / Beg. Bank	7.6 / 7		8.1 / 23 / Top	19.1 / Bot. - 6' wide
14+23 = ℄ on Edge of Bank							29.2 / 10.3			23.0 / 7 = Bot. - 6' wide
14+17 = ℄ in Wash							23.3 / 16.2 = on Edge			
14+10 = 1' Rt. to top of Vert. Bank as wash							21.3 / 12.2		12.2 / 1	24.6 = Bot. / 1
T.P.	1.68	339.54	1.04	337.86			339.54			
14+04 = Top of Nly. Bank							26.4			
						11.9 / 21 / Toe	12.5 / Top	24.5 / 2 / in Bottom 6' wide	14.8 / 8	12.0 / 18	9.9 / 38 / Toe
T.P.	12.54	338.90	0.56	326.36 = Rock Lt.	14+00		338.90			
13+97 = ℄ Wash							13.7 / 13.2 / Bot. wash			
							326.92			

					Lt.		℄	Rt.	
16+09.70 = Ang. Pt. Sect. on split					0.6 20 30' Bank	6.0 9	5.76 on tub.	6.9 19 Top	18.4 Bot. -4' wide
15+90						4.5 20 30' Bank	9.0 Top	20.0 2	23.0 5 = Bot. -6' wide
15+80							24.4 = in Bot. -7' wide		
15+73 = ℄ + Top of Deep wash							11.7 Top	24.7 Bot. - 6' wide	
15+65 - Loose Sect. of Bank on Lt. May Come down						11.3 9 Toe	11.9		
T.P.	12.64	362.58	0.57	349.94			362.58		
15+40						+6.9 13 20' Bank	0.1	2.2 6	4.5 22 Top 20.0 Bot. -4' wide
15+05						9.3 27 =30' Bank Vert.	8.9 350.51	9.1 29 Top	23.1 Bot. -4' wide

							40 46 64 73	Lt.		℄	Rt.		
T.P.	13.12	387.93	0.53	374.81 - stob 25' Rt.	17+50								
17+50								+6.2 20	0.0 10	1.7	0.7 27 Top	33 Bot.	
17+28 = ℄ in Wash									2.8 3 Top	5.8	3.0 3 Top	3.4 15 Top	20.9 28 - Bot. - 5' wide
17+10					2.4 22 15' Bank	5.1 9	9.1 5 ℄ wash	5.8 2	5.8		6.9 25 Top	22.0 bot.	
16+73 = Top Bank					9.7 22 Toe	10.2 8 Top	18.7 4 ℄ wash		11.2 375.34		11.3 10 Top	26.4 20 Bot. - 6' wide	
T.P.	13.12	375.34	0.36	362.22									
16+64 = ℄ in wash								+0.2 5 Top		9.7 Bot. N. Branch	0.0 3 Top	+1.0 10 Top	13.0 14 Bot. of S. Branch
16+46 = ℄ in wash									0.4 6 Top	12.7 Bot.		13.5 20 Bot. on S. Bank	
16+40 = ℄ = Top of Bank								+1.8 21		1.9	15.5 6 Bot - 7' wide		
										362.58			

					Lt.		℄	Rt.	
									+90 14 +20 +40
19+90					11.7 10 20' Vert Bank		13.8	15.7 14 Top	35 = Bot.
T.P.	12.91	426.46	0.06	413.55			426.46		
19+58.72 = Ang. Pt. = Sect. on split					+2.5 18 Bank	3.6 8	4.97 on Hob.	6.2 15 Top	25.9 32 = Bot. 5' wide
19+15					8.9 20 20' Bank		12.5 413.61	13.1 15 Top	31.0 30 Bot. - 4' wide
T.P.	12.87	413.61	0.25	400.74					
18+75					0.5 20	4.7 10	6.7	7.9 25 Top	23.0 32 Bot. - 6' wide
18+40					10.0 20 Toe	13.1 5	11.8 400.99	13.0 19 Top	27.0 23 Bot. - 6' wide
T.P.	13.23	400.99	0.17	387.76					
18+00					5.0 15		6.2 387.93	6.9 25 Top	18.0 30 Bot. - 4' wide

					Lt.	℄	Rt.			
22+05					9.1 10 6' Bank	12.1	13.2 10	12.8 20	12.7 30	
T.P.	13.21	452.34	0.41	439.13 = Rock Pt. 22+10		452.34				
21+68					0.0 9 7' Bank	4.6	8.7 4	5.4 12	4.1 30	
21+37.68 = Ang. Pt - Sect. on split					6.4 6 15' Bank	7.9 1 on Hub	9.8 11	11.4 12 ℄ 3 Ditch	8.0 50 = Toe	
T.P.	13.08	439.54	0.00	426.46 21+10		439.54				
20+80					0.0 11 20' Bank	3.2	6.3 11	3.7 13	3.4 40	
20+60					1.9 11 - 20' Bank	5.4	7.0 6	9.5 8 3' Ditch	7.1 9	6.4 18 Top	26.3 30 Bot.
20+40					4.6 9 30' Vert. Bank.	7.4	7.8 1 Top	17.1 2 Bot of Bank	28.3 15 Bot. of wash	30.0 25 Bot Branch
20+20 - ℄ = Top of Bank					7.3 8 20' Bank (Hard)	9.0			32.5 25 Bot 5' wide	
						426.46				

					Lt.			℄	Rt.		
24+55					10.6	18.5	18.5	10.0	10.0	10.2	11.7
					20	11	6	1.5		15	30
T.P. 12.89	475.78	1.66	462.89 =	Mon 24+35 -16.3' Rt.				475.78			
24+30						8.7	1.6	1.5			
						13	12			30 Toe	
						9' wide Bot	Top				
23+80					6.4	11.8	9.0	8.8		7.8	
					23	10	7			30	
					Bank						
T.P. 12.63	464.55	0.42	451.92	= stub 6' Lt. 23+60				464.55			
23+30					0.7	2.9		1.7		0.5	
					20	10				30	
					Bank						
22+90					3.3	3.7		6.9	5.2	4.4	
					25	15			15	30	
22+45						6.2		8.8	10.3	8.8	8.1
					Side Draw	30			7	15	40
								452.34			

					Lt.		℄	Rt.	
27+25					17.8 33 Bot.	12.3 23 Top	11.2	9.3 30	6.6 37 Bank
T.P	13.15	500.58	0.34	487.43			500.58		
26+75					10.1 37 Lwash	3.0 25 Top	1.5	1.1 16	+2.9 23 = Bank
26+25					8' Deep 3' wide	6.6 30 = Top - bank of wash	5.8	6.1 10	2.6 18 = Bank
25+75 .22 = Ang. Pt. Sect. on split						10.8 20	10.39 on Hub.	10.3 7	7.3 15 = Bank
T.P	13.21	487.77	1.22	474.56			487.77		
25+35					6' wide 10.5' Deep	1.5 32 Top of wash	2.7		1.1 26 = Toe
24+90					16.3 18 Bot. 4' wide	7.0 12	6.9 475.78		6.3 15

					Lt.	℄	Rt.			
29+25					14.0 30	12.0	9.3 40 = Bank			
T.P.	12.09	512.25	8.57	500.16		512.25				
90° to foward Tang.						6.4 30	3.0 = 95 edge			
28+87.55' = Ang. Pt. – outs 90° to Back Tang.						8.57 on Hub.	8.6 30	2.9 100 = Bank 20'		
Set B.M. on Conc. Mon. on P.L. Line			7.33	501.40						
T.P.	8.57	508.73	0.42	500.16		508.73				
28+25					5.7 30	5.7	4.7 33 = Toe			
27+75					8.9 25	12.2 14 ℄ wash	9.0 9	8.7	11.2 7 ℄ wash	7.9 12	6.7 30 Toe
27+70 = ℄ wash						11.7				
27+53						9.8 500.58				

				Lt.	℄	Rt.	
31+43.5 - 12.3' Rt. = S.W. Cor. of shed. - 12.3' N&S of Bank (Conc. found. 8.3' E&W)						2.8 Dirt. 12.3 = floor	
31+33.3 - 12' Rt. = Beg. 6' Cyclone fence - also top							
31+25 = Top of Bank				4.6 20	3.5	3.8 6 Top	
T.P.	10.89	535.65	0.22		535.65		524.76
T.P.	12.86	524.98	0.13				512.12
31+15 = Toe of Bank				+6.0 15 on Bank	1.7	1.4 20	
30+75				7.4 40	6.8	1.3 45	
30+25				11.6 40	9.0	6.7 30	2.9 55 Toe
29+75				13.3 40	11.3	6.8 50	1.6 90 = Bank
					512.25		

	Lt.	℄	Rt.	
34 +00	5.6 30	5.6	4.9 15	3.4 25.1 = along cyclone fence
33 + 50		6.5		
33+48 - 37 Lt. = ℄ sprinkler				
33 +00	7.8 30	7.5		7.2 30
32 +65		8.0		
32 +42 - 9.6 Lt. = ℄ 1½" pipe - overhead sprinkler				
32 +30 - Thru field - Level - was orchard.	8.9 30	8.8		8.4 30
32 +04 - 8.8' Rt. = ℄ 4" Lemon Tree				
31 +85	9.4 20	9.2	8.8 20	
31 +84.5 - 6' Rt. = ℄ 4" Lemon Tree				
31 +79 - 6' Lt. = ℄ Holly Tree				
T.P. 8.70 541.60 2.75 532.90		541.60		
31 +65 = Cross Cyclone fence (Gate Locked)				
31 +62.2 - 27' Rt. = N.W. Cor. Shed + Beg. wire fence				
31 +46.95 = Hng. Pt. - Sect. 90° to Back Tang.	7.5 40 Low pt.	5.2 20	4.00	3.3 12.3 = By shed
		535.65		

				536.43 - 8.66
	+ La Jolla Mesa Dr.			
check B.M.	SE. Cor Bescano Dr.		7.93	536.43
	0.57	544.36	12.68	543.79
	9.24	556.47	0.84	547.23
T.P.	6.75	548.07	0.28	541.32

34 + 40 = P.K. in ℄ = end.

34 + 25 = edge of A.C. Pave

34 + 16.5 = Cross wire fence

34 + 10

Lt.	℄	Rt.

See B. 1426 - P. 20 Starting B.M. is 8.66 High = 527.77 = o.k.

527.51 = Book 527.86 = Water Dept. — (wow!)

4.13	3.83	3.40
40		40
along ℄		along ℄ of Road
	3.83	
	3.5	
	4.8	

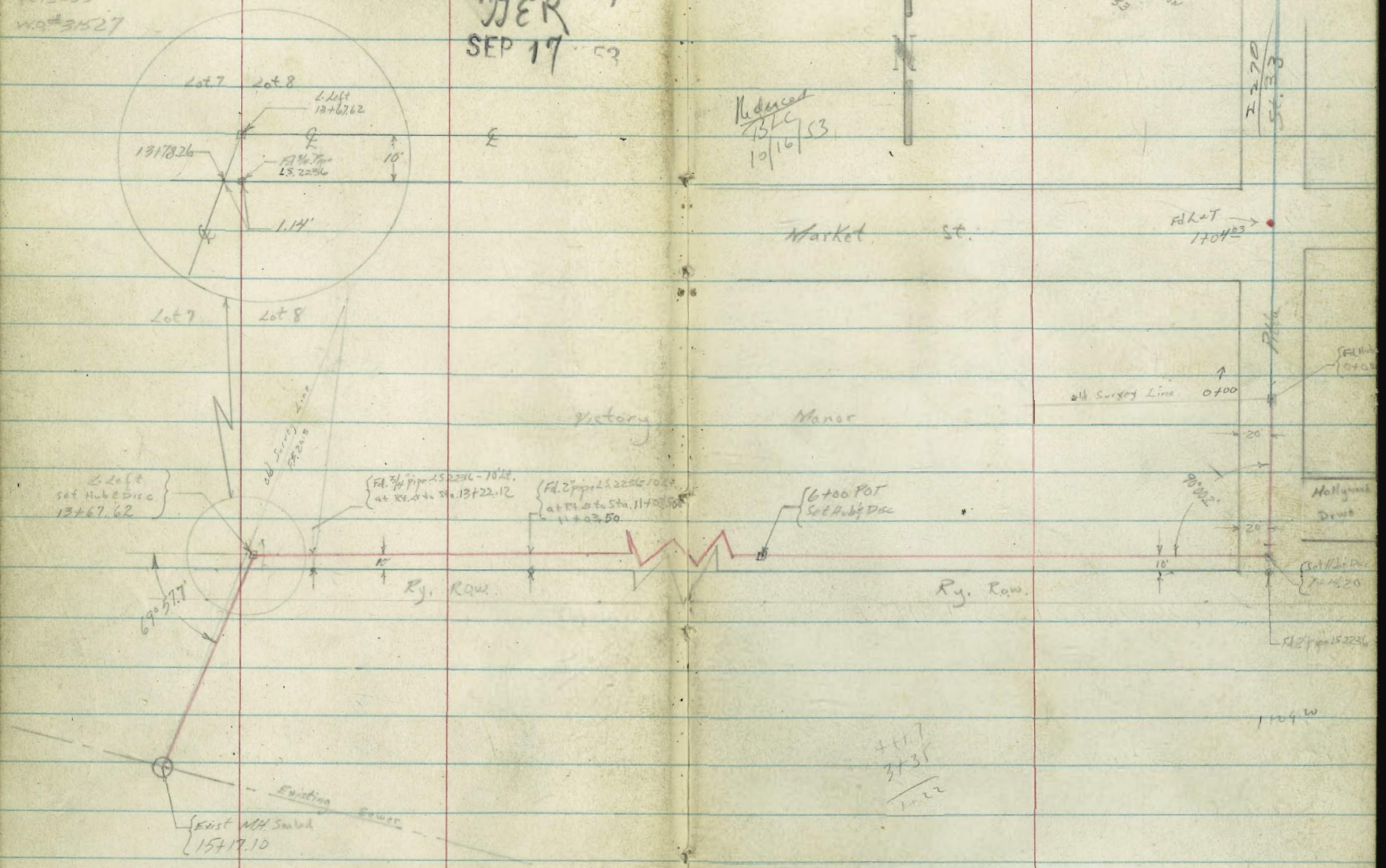
541.60 - 8.66 Too High

Roberts
Cota
Monre
Moralez
9-15-53
WO #31527

Survey For Proposed Sewer
in Victory Manor.

added blue line extension
JDB. 11-10-53

Reduced
JSC
10/16/53



2+1
3+3
1+22

Cont'd from Page 22

					Lt	℄	Rt
1+14.20					157.1 / 12.5 (9 Rt. ∠s to forward Tangent)	162.3 / 7.3 (5 Tan)	16.45 / 5.1
1+07						163.6 / 6.0	
0+92						164.7 / 4.9	
0+50						166.3 / 2.9	
T.P.	0.50	169.62 ⊼	13.21	169.12		169.62 ⊼	
0+00		℄ Pitta & So. of Market S. in Pitta St				170.9 / 11.4	
B.M.	0.47	182.33 ⊼		181.86 SE BT Market & Pitta		182.33 ⊼	

1+09 = 163.9

Cont'd From Page 23

					Lt	℄	Rt
T.P.	-1.84	163.58 ⊼	7.88	161.74			
3+50					154.8 14.8 10 Toe	158.2 11.4 5	161.7 7.9	162.2 7.4 10
3+00					155.4 14.2 11 Toe	159.5 10.1 5	162.7 6.9	163.4 6.2 10
2+50					156.1 13.5 10 Toe	159.8 9.8 5	162.9 6.7	163.6 6.0 10
2+00					156.7 12.9 11 Toe	160.6 9.0 5	163.3 6.3	163.7 5.9 10
1+78					157.2 12.4 10 Toe	160.4 9.2 5	162.7 6.9	163.4 6.2 10
1+50					157.0 12.6 10 Toe	161.1 8.5 5	164.1 5.5	163.9 5.7 10
		169.62 ⊼					169.62 ⊼

Contd from Page 24

		Lt	℄		Rt
6+70		149.0 14.6 10 Toe	151.2 11.4 5	154.9 8.7	155.7 7.9 10
6+50		148.7 14.9 10 Toe	152.2 11.4 5	155.6 8.0	156.2 7.4 10
6+00	P.O.T.	149.9 13.7 10 Toe	152.1 10.5 5	154.98 8.60 ON HUB	155.9 7.7 10
5+50		150.7 12.9 10 Toe	155.2 8.4 5	155.9 7.7	157.0 6.6 10
5+00		151.8 11.8 10 Toe	155.0 8.6 5	157.3 6.3	157.8 5.8 10
4+50		152.8 10.8 10 Toe	156.4 7.2 5	159.0 4.6	159.0 4.6 10
4+00		153.5 10.1 10 Toe	157.8 5.8 5	160.5 3.1	160.6 3.0 10
	163.58 ⊼			163.58 ⊼	

Contd From Page 25

					Lt.		℄		Rt
8+10					145.9 7.9 10	146.1 7.7 5 Toe	149.2 4.6	150.1 3.7 10	
8+06	10° Rt begin wire chicken coop								
8+00					146.2 7.6 10	146.5 7.3 5	146.8 7.0	149.6 4.2 8	149.7 4.1 10
7+95					146.3 7.5 10	146.6 7.2 5	145.9 6.9	147.8 6.0 10	
7+84					146.5 7.3 10	146.7 7.1 5	147.0 6.8	147.7 6.1 10	
7+50					146.9 6.9 10	147.4 6.4 5 Toe	148.3 5.5	148.4 5.4 2	149.5 4.3 5	150.1 3.7 10
T.P.	173	153.75 ⊼	11.56	152.02			153.75 ⊼		
7+00					146.1 15.5 10 Toe	150.8 12.8 5	151.6 12.0	152.5 11.1 10	
		163.58 ⊼					163.58 ⊼		

3' R.
8 × 2.8
24
1.05
147.9

Cont'd From Page 26

T.P.	-0.63	142.40 ⊼	11.98	141.77
10+00	9' Rt to wire fence			
9+50				
9+00				
8+70				
8+50				
8+25	10' Rt begin wire fence			
8+22	10' Rt End wire chicken coop			
		153.75 ⊼		

Lt	℄	Rt
141.7 12.1 10	141.3 12.5 5	141.5 12.3	141.9 11.9 10
142.1 10.7 10	142.9 11.1 5	143.4 10.4	144.2 9.6 10
143.9 10.1 10	143.7 10.1 5 Toe	145.2 8.6	147.0 6.8 10
144.6 9.2 10	147.5 9.3 5 Toe	147.7 6.1	148.9 5.1 10
145.4 9.0 10	146.0 8.8 5 Toe.	148.7 5.1	149.4 4.4 10
		153.75 ⊼	

Cont'd From Page 27

		Lt.	℄	Rt.
12+50		136.4 6.0 12 / 133.7 8.7 5 / 132.9 9.5 4 / 132.9 9.5	133.2 9.2 4 / 135.2 7.2 9 / 135.2 7.2 10	
12+40.5	8.8' Rt begin wire fence 8.8' Rt End conc. Ret. wall with fence on top.			
12+00		136.9 5.5 10 / 134.6 7.8 5 / 134.6 7.8	135.9 7.1 8.9	
11+98.5	8.9' Rt begin conc. Retaining wall with fence			
11+53		138.4 4.1 10 / 136.5 5.9 5 / 136.6 5.8	138.0 4.4 10	
11+50	9.0' Rt End wire fence	138.3 4.1 10 / 136.7 5.7 5 / 136.7 5.7	137.7 4.7 3 / 139.6 2.8 10	
11+00		139.5 2.9 10 / 138.4 4.0 5 / 138.3 4.1	139.6 2.8 5 / 139.8 2.6 10	
10+50		140.8 1.6 10 / 139.8 2.6 5 / 141.9 2.5	140.8 1.6 10	

142.40 ⊼

142.40 ⊼

Cont'd From Page 28

		Lt	℄	Rt
13+86.42	Inside edge of North rail. (Gauge)		134.77 7.63 Top Rail	
13+80.			133.9 8.5	
13+75			132.0 10.4	
13+67.62 L.	LEFT Section at Rt. ∠ to back Tangent.	134.1 8.3 12	131.8 10.6 6	131.6 10.6 5	131.7 10.7	132.5 9.9 10
		134.7 7.7 15	133.4 9.0 5	132.3 10.1 2	132.3 10.1	132.6 9.6 10
133	11° Rt End wire fence					
13+00		135.4 7.0 12	133.0 9.4 5	131.9 10.5 3	131.9 10.5	132.1 10.3 5	133.1 9.3 10

142.40 ⊼

142.40 ⊼

Cont'd From Page 29

		Lt	℄	Rt
14+45			129.5 12.9	
14+35.5	11.0' Lt to center P.Pole # 70139			
14+22			129.2 13.2	
14+19			128.4 14.0	
14+09			128.6 13.8	
13+98			133.4 9.0	
13+91.44	Inside edge of South rail. (Gauge)		133.75 7.65 Top Rail	
	142.40 ⅄		142.40 ⅄	

Cont'd From Page 30

		Lt	℄	Rt
15+17.10	Exist M.H.			
				124.1
		13.32 Rim		18.3 GRD
14+98				
			125.1	
			17.3	
14+88				
			128.0	
			14.4	
14+60				
			128.7	
			13.7	
	142.40 ⊼			142.40 ⊼

128.08 = 129.09 FR 1960

D. Smith
J. Rorer
R. Taylor
Rtish

Extend Sewer Victory Manor
Nly along Fifth St

WO # 31527
11-10-53

	Lt-Wly	℄	Rt-Ely			℄	Rt-Ely
1+22 1.8 Rt end con pav			182.24 / 3.62 / 1.8 con	TP3	8.45	216.12	0.68 / 207.67
1+19.5 Nly par AC, ℄ crosses			182.28 / 3.58	3+50			205.4 / 3.0; 204.2 / 4.2 (25); 200.3 / 8.1 (50); 196.0 / 12.2 (75)
1+04.03			182.50 / 3.36 / on Lt	3+00			200.9 / 7.5; 200.0 / 8.4 (25); 197.4 / 11.0 (50); 193.5 / 14.9 (75)
0+82.5 ℄ crosses AC par Sly edge			182.42 / 3.44	2+50			197.6 / 10.8; 196.9 / 11.5 (25); 194.5 / 13.9 (50); 191.8 / 16.6 (75)
0+84 1.8 Rt Begin con pav edge			182.09 / 3.27 / 1.8 con	TP2	11.63	208.35	0.65 / 196.22
0+80			181.6 / 4.3	2+00			192.7 / 4.7; 192.1 / 5.3 (25); 190.1 / 7.3 (50); 188.8 / 8.6 (75)
0+40			175.4 / 10.0	1+50			186.8 / 10.8
0+24 34' Lt ℄ House	176.9 / 9.00 / 34' Floor			TP1	11.76	197.37	0.25 / 185.61
0+00 = 0+00 Bang 23.			170.8 / 5.1	1+46 189 Rt SW cor House			184.71 / 1.15 / 109 Floor; 189.60
				1+46 40.3 Rt SW cor House			+3.74 / 40.3 Floor
B.M.	4.00	185.86	181.86 SE cor Rod & Market St			185.86	

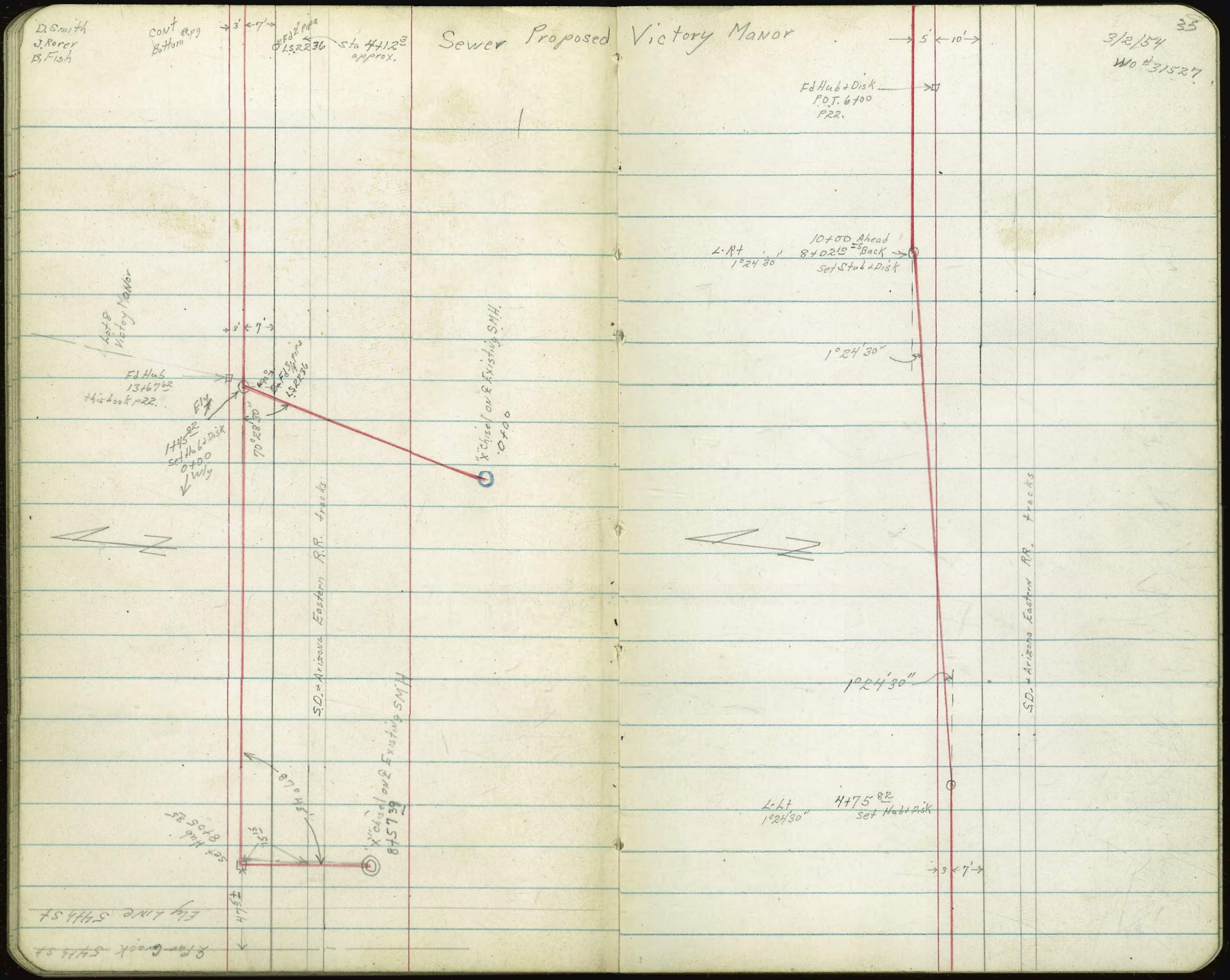
	Lt=Wly	℄	Rt=Ely	℄
			181.85	
BM. starting		9.20	181.85	
TP5	0.75 191.05	12.97	190.30	
TP4	0.68 203.27	12.93	203.19	
5+50			215.8 / 0.3	211.9 / 4.2 (25)
			207.2 / 8.0 (50)	203.1 / 13.0 (75)
5+24.32 Mon Sly Kenwood			214.43 / 0.9 on Mon	215.1 / 1.0 dirt
5+00			213.4 / 2.2	210.5 / 5.6 (25)
			205.0 / 11.1 (50)	198.1 / 18.0 (75)
4+50			210.9 / 5.2	208.9 / 7.2 (25)
			202.7 / 13.4 (50)	195.1 / 21.0 (75)
4+00			208.6 / 7.5	205.8 / 10.3 (25)
			201.8 / 14.3 (50)	195.8 / 20.3 (75)
			216.12	

D. Smith
J. Rorer
B. Fish

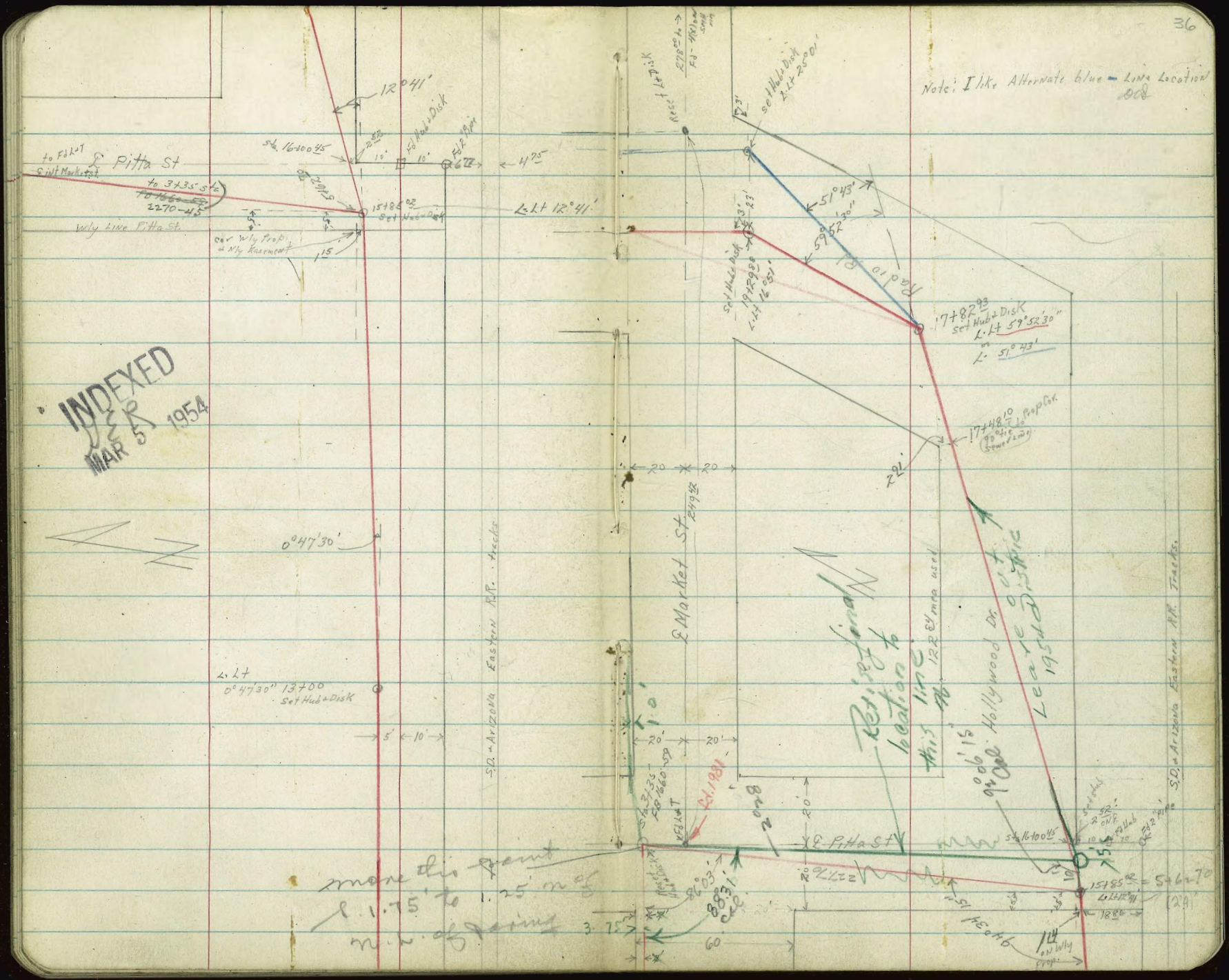
Cont R.pg Bottom

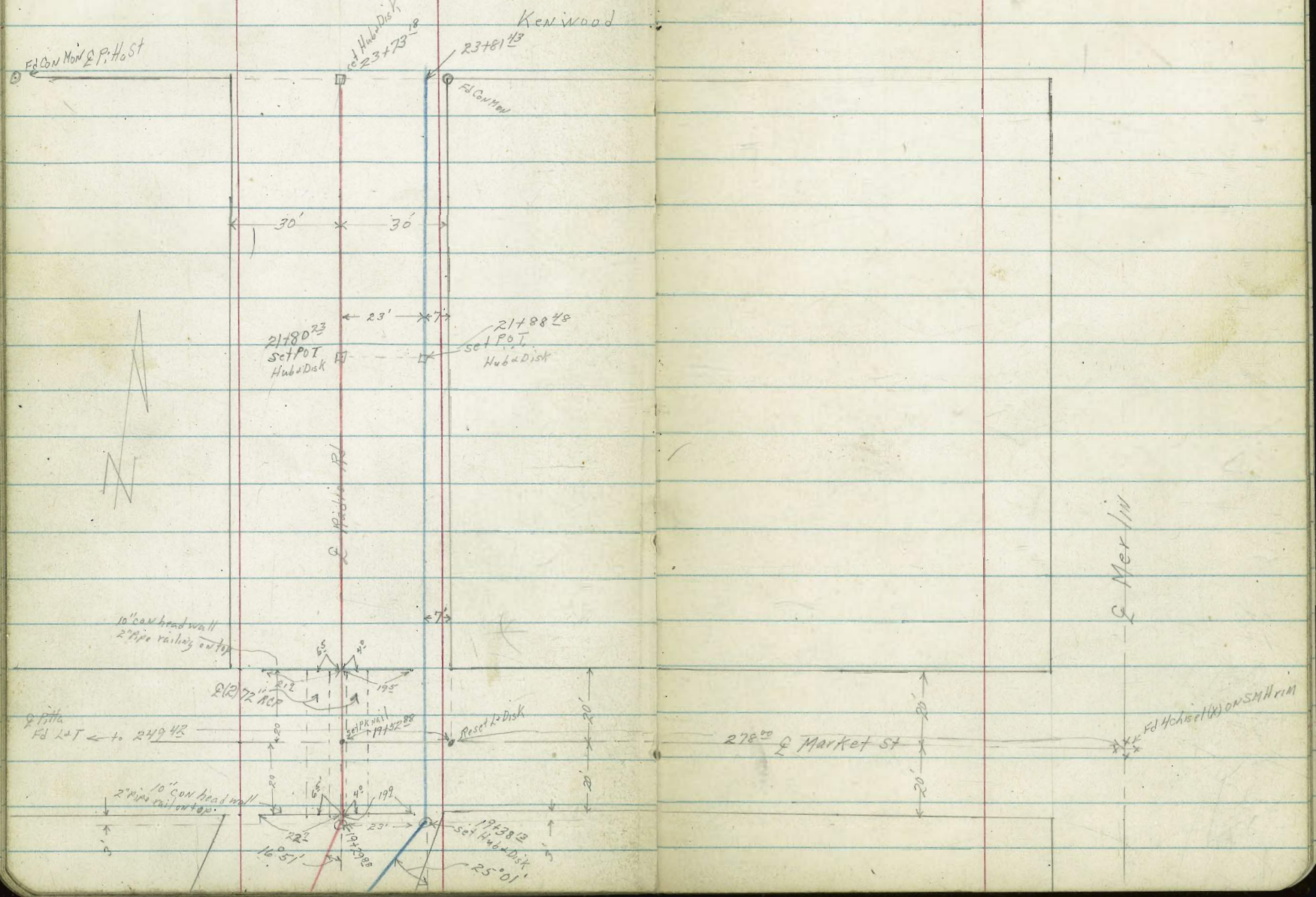
Sewer Proposed Victory Manor

3/2/54
W.O. #31527



Note: I like Alternate blue — Line Location




Kenwood
Fd Con Mon & P. Ho St
set Hub & Disk
23+73.18
23+81.43
Fd Con Mon
30'
30'
23'
7'
21+80.23
set POT
Hub & Disk
21+88.48
set POT
Hub & Disk
℄ Middle Rd
7'
10" con head wall
2" pipe railing on top
5°
4°
21.2
19.5
℄(2) 72" RCP
℄ Pitts
Fd ⊥ T ← to 24+9.42
20'
set PK nail
19+52.88
Reset to Disk
20'
20'
20'
2" pipe
10" con head wall
railing on top
6.5'
4°
19.9
22.1
23'
19+38.13
set Hub & Disk
16°57'
19+29.88
25°01'
℄ Merlin
278.00 ℄ Market St
20'
20'
Fd Hchisel (X) on SM Trim

	Lt	℄	Rt
1+35	131.3 / 10 9 / 15	133.9 / 8 3	134.3 / 7 9 / 10
1+18	133.8 / 8 4 / 10	133.3 / 8 9	132.1 / 10 1 / 10
1+08	129.8 / 12 4 / 10	128.8 / 13 4	128.5 / 13 2 / 10
0+97	128.2 / 14 0 / 7	129.0 / 13 2	129.1 / 13 1 / 10
0+81 11 8 Rt ℄ 12" P Pole # 70139			
0+75	129.0 / 13 2 / 10	129.4 / 12 8	129.9 / 12 3 / 10
0+30	124.8 / 17 4 / 13	128.7 / 13 5	128.5 / 13 7 / 10
0+20	124.3 / 17 9 / 10	124.6 / 17 6	127.8 / 14 4 / 10
15+17 0 P31 =S 0+00 Existing SMH		129.08 / 12 16 / RIM	124.5 / 17 7 / 9d
BM	13 16 ⟨142 24⟩	⟨129 08⟩	15+17 0 RIM SMH p31

	Lt	℄	Rt
TP,	11 52 ⟨151 54⟩		2 22 ⟨140 02⟩ on Hub 4+75 82
4+75 82 L. Lt 1°24'30"	141.2 / 1 0 / 10	140.4 / 1 8 / 5	140.0 / 2 22 on Hub
	140.0 / 2 2 / 5	140.7 / 1 5 / 7	141.0 / 1 2 / 10
4+35	140.4 / 1 8 / 10	139.4 / 2 5 / 6	139.0 / 3 2
	139.1 / 3 1 / 4	140.1 / 2 1 / 6	140.1 / 2 1 / 10
4+00	139.7 / 2 5 / 10	139.9 / 4 3 / 3	137.8 / 4 4
	138.0 / 4 2 / 4	139.2 / 3 0 / 7	139.4 / 2 8 / 10
3+50	137.3 / 4 9 / 10	136.1 / 6 1 / 4	135.8 / 6 4
	135.9 / 6 3 / 3	137.9 / 4 3 / 8	
3+00	135.3 / 6 9 / 10	134.6 / 7 6 / 8	134.1 / 8 1
	137.1 / 5 1 / 10		
2+50	134.2 / 8 0 / 10	132.7 / 9 5 / 7	132.4 / 9 8
	133.1 / 9 1 / 3	135.9 / 6 3 / 10	
2+00	132.7 / 9 5 / 10	132.0 / 10 2	133.0 / 9 2 / 5
	135.0 / 7 2 / 10		
1+80	132.7 / 9 5 / 10	132.4 / 10 0 / 4	133.5 / 8 7
	134.2 / 8 0 / 10		
1+45 82 Ely 70°28'30" L. Rt	131.80 / 10 44 on Hub		131.7 1660/62 ~~45 131.7 Page 46.~~ 2370/29 = 131.7
1+42	131.5 / 10 7 / 10	131.6 / 10 6	134.3 / 7 9 / 13
	⟨142 24⟩		

	Lt	℄	Rt
10+00 Ahead = 8+02 1° BK L·Rt 1°24'30"	151.6 / +0.1 / 10	150.8 / 0.23 / on stub 46	150.6 / 0.9 / 3 / 12 — 147.7
7+50	150.2 / 1.3 / 10	148.9 / 2.6	149.0 / 2.5 / 3 — 146.6 / 4.9 / 9 — 146.3 / 5.2 / 15
7+28	146.9 / 4.6 / 10	147.0 / 4.5	146.8 / 4.7 / 10
7+08	150.0 / 1.5 / 10	149.2 / 2.3	146.4 / 5.1 / 8 — 146.4 / 5.1 / 10
7+00	149.9 / 1.6 / 10	149.3 / 2.2	146.2 / 5.3 / 10
6+50	148.9 / 2.6 / 10	148.0 / 3.5	144.5 / 7.0 / 9
6+25	147.3 / 4.2 / 10	146.5 / 5.0	143.9 / 7.6 / 6 — 144.0 / 7.5 / 10
6+00	145.8 / 5.7 / 10	144.4 / 7.1	143.3 / 8.2 / 10
5+75	144.4 / 7.1 / 10	143.8 / 7.7	142.8 / 8.7 / 10
5+25	142.4 / 9.1 / 10 — 142.4 / 9.1 / 3	141.8 / 9.7	141.9 / 9.6 / 10
	⟨π 151.5 4⟩		

	Lt	℄	Rt
14+50	163.9 / 4.2 / 10	163.2 / 4.7	163.0 / 5.1 / 6 — 156.0 / 12.1 / 16
14+00	163.0 / 5.1 / 10	162.5 / 5.6	162.5 / 5.6 / 6 — 155.1 / 13.0 / 21
TP3	6.10	π⟨168.12⟩	0.83 [162.02]
13+50	161.9 / 1.0 / 10	161.7 / 1.2	161.6 / 1.3 / 6 — 154.3 / 8.6 / 19
13+00 L·Lt 0°47'30"	160.3 / 2.6	159.98 / 2.97 on stub 46	160.2 / 2.7 / 6 — 153.3 / 9.6 / 19
12+50	158.7 / 4.2 / 10	158.7 / 4.2	158.5 / 4.4 / 8 — 152.6 / 10.1 / 18
12+00	157.7 / 5.2 / 10	157.6 / 5.3	157.1 / 5.8 / 8 — 151.3 / 11.6 / 16
11+50	156.6 / 6.3 / 10	155.9 / 7.0	154.9 / 8.0 / 7 — 150.9 / 12.0 / 15
11+00	156.2 / 6.7 / 10	155.6 / 7.3	154.9 / 8.0 / 8 — 149.5 / 13.4 / 16
10+45	156.1 / 6.8 / 10	155.3 / 7.6	155.0 / 7.9 / 7 — 148.2 / 14.7 / 16
TP2	12.14	π⟨162.95⟩	0.73 ⟨150.81⟩ on stub 8+02.10

	Lt	℄	Rt
17+82.93 L. Lt — 51°43' / — 59°52'30"	157.6 / 10.5 / 10	157.39 / 10.73 / on H46	157.5 / 10.6 / 10
17+40	158.2 / 9.2 / 10	158.0 / 10.1	157.7 / 10.4 / 10
16+90	158.2 / 9.2 / 10	158.3 / 9.8	158.8 / 9.3 / 10
16+50	162.6 / 5.5 / 10	161.6 / 6.5	160.9 / 7.2 / 10
16+00	164.7 / 3.4 / 10	163.7 / 4.4	164.0 / 4.1 / 10
5+62.70 Pitts st = 5 / 15+85.02 L. Lt 12°41'	164.3 / 3.8 / 10	163.72 / 4.20 / on H46	164.5 / 3.6 / 9.2	164.2 / 3.9 / 10
15+40	164.1 / 4.0 / 10	163.3 / 4.8	163.0 / 5.1 / 9
15+00	163.8 / 4.3 / 10	163.5 / 4.6	163.1 / 5.0 / 7	156.8 / 11.3 / 18

⟨T 168.12⟩

Lt ℄ Rt

Red

TP 4 — 8 77 ⟨π 175.11⟩ — 178 ⟨166 34⟩

	168.0	160.3	157.3	157.3
18+96	0 1 / 14	7 8 / 3	10 8	10 8 / 10
	167.4	162.9	157.5	157.5
18+88	0 7 / 10	5 2	10 6 / 3	10 6 / 10
	166.3	166.6	163.5	163.4	157.5
18+80	1 8 / 10	1 5 / 6	4 6	4 2 / 4	10 6 / 6
	163.6	165.5	162.5	157.1
18+68	4 5 / 10	3 6	5 6 / 7	11 0 / 9
	160.7	160.9	162.7
18+54	7 4 / 10	7 2	5 4 / 8
	159.2	158.9	157.0	156.7
18+30	8 9 / 10	9 2	11 1 / 8	11 4 / 10
	156.7	156.3	156.6
18+06	11 4 / 10	11 8	11 5 / 10
	158.1	157.6	157.5
18+04	10 0 / 10	10 5	10 6 / 10
	158.0	157.4	157.2
18+00	10 1 / 10	10 7	10 9 / 10

⟨π 168 12⟩

Lt ℄ Rt

Blue

19+38 13 ∠ Lt 25°01′ — 166.5 / 16 / 6 — 178 166.3 / ON HUG — 166.7 / 14 / 10

	157.7	157.7	166.8	167.5
19+11	10 4 / 10	10 4 / 7	1 3	0 6 / 10
	157.5	157.4	164.2	167.0
19+04	10 6 / 10	10 7 / 3	3 2	1 1 / 10
	157.4	157.5	164.6	165.4
19+00	10 7 / 10	10 6 / 1	3 5 / 4	2 7 / 10
	165.5	162.2	162.8	157.3	157.0
18+70	2 6 / 18	5 9 / 6	5 3 / 3	10 8	11 1 / 10
	163.7	161.8	161.8	156.9	157.1
18+63	4 4 / 8	6 3 / 6	6 3	11 2 / 2	11 0 / 10
	160.4	160.3	160.2	157.7
18+52	7 7 / 10	7 8	7 9 / 4	10 4 / 10
	159.1	157.0	156.8
18+34	9 0 / 10	11 1	11 3 / 10
	156.5	156.6	156.4
18+07	11 6 / 10	11 5	11 7 / 10
	157.9	157.1	157.0
18+00	10 2 / 10	11 0	11 1 / 10

⟨168 12⟩

Lt ℄ Rt

Red

20+56 — 166.9 164.4 163.7 166.5 169.3
8.2 10.7 11.4 8.6 5.8
12 8 9 14

20+45 — 165.6 168.8 170.1 168.5
9.5 6.3 5.0 6.6
10 5 10

20+35 — 168.0 169.6 170.4 163.4
7.1 5.5 4.7 11.7
12 10 10

20+00 — 167.1 159.0 158.0
8.0 16.1 17.1
15 10

19+72.1 — 156.98 159.2 156.89
18.13 15.9 18.22
6.5 4.0
1¢ 1¢
G'RCP G'RCP

19+72.1 top abut — 166.07 167.24 167.25 166.41 167.16 166.11
9.04 7.87 7.86 8.70 7.95 9.00
gut top top gut 19.5 19.0
21.9 21.9 top gut

19+52.88 ℄ — 166.20
8.91

12+32.1 top bridge abut — 165.09 166.06 166.14 165.22 166.19 165.32
10.02 9.05 8.97 9.89 8.92 9.79
22.7 22.7 gut 19.9 19.2
gut to top gut

19+32.1 — 158.77 158.2 155.7
19.34 16.9 19.40
6.5 4.0
1¢ 1¢
G'RCP G'RCP

19+29.88 L.L+16° 51' — 158.2
16.2

⟨π 175.11⟩

Lt ℄ Rt

Blue

175.9 175.7 176.0 177.3
9.1 9.3 9.0 7.7
10 7 10

21+50

TP 10.20 ⟨8497⟩ 0.34 ⟨17477⟩

21+00 — 168.9 171.4 171.5 171.6 173.4
6.3 3.7 3.6 3.5 1.7
15 10 7 12

20+50 — 169.0 168.9
6.1 6.2
10

20+00 — 166.8 167.0
8.3 8.1
10

19+81.3 edge pav. — 166.25 166.51
8.86 8.60
10

19+76.3 No cb — 166.28 166.53
8.83 8.58
gut 10 gut

19+61.3 ℄ Market — 166.46
8.63

Market st.

19+46.3 sly cb line — 165.96 165.42 166.30 165.72
9.15 9.67 8.81 9.39
cb gut 10 10
cb gut

19+41.3 ℄ K's sidewalk — 166.03
9.08

TP 8.77 ⟨175.11⟩ 1.78 ⟨166.34⟩

on Hub pkg 19+38.13

Lt ℄ Rt

Red

	Lt	℄	Rt
23+10	170.7	170.3	169.7
	14 3/10	14 2	15 3/10
23+00	166.9	166.0	166.1
	18 4/10	19 0	18 9/10
22+61	165.5	166.2	167.9
	19 5/10	18 8	17 1/10
22+35	174.4	176.0	178.2
	10 6/10	9 0	6 8/10
22+00	176.0	177.6	179.7
	9 0/10	7 4	5 3/10
21+80 23 POT		177.03	
		7 94 on Hub	
21+56 10° Lt ℄ deadman	173.6	174.8	176.2
21+50	11 4/10	10 2	8 8/10
TP5 10 20	⟨π 184 97⟩	034	⟨174 77⟩
21+36 10° Lt 28" PPL #P370899			
21+00	166.7	168.3	169.6
	8 4/10	6 8	5 5/10
		⟨π 175 41⟩	

Lt ℄ Rt

Blue

	Lt	℄	Rt
23+45	172.1	170.9	169.9
	12 2/10	14 1	15 1/10
23+15	168.6	166.7	166.2
	16 4/12	18 3	18 8/10
22+79	166.1	166.2	170.8
	18 9/6	18 8	14 2/10
22+44	178.4	180.3	181.7
	6 6/10	4 7	3 3/10
~~22+32~~ 21+32	180.0	181.5	181.9
	5 0/10	3 5	3 1/10
22+00	179.7	179.5	179.9 181.1
	5 3/10	5 5	5 1/7 3 9/10
21+88 48 POT		178.71	
		6 26 on Hub	
		⟨π 184 97⟩	

Lt ℄ Rt
Red

Lt ℄ Rt
Blue

181 86
Step
Pillar
Market

140 ⟨181 84⟩

TP6 595 ⟨183 84⟩ 768 ⟨177 79⟩

179.0 177.3 175.8
6 0 / 0 765 / 0 on Hub 9 2 / 10

23+73 18 end

175.7 174.8 173.4
9 3 / 10 10 2 / 10 11 6 / 10

23+42

173.2
11 8

23+81 43 end

⟨π 184 97⟩

184 97

Line S.W. in Pitta St from N. Side Market

45

Along N. Side Market St W. of Pitta FB 1660 "A" Line

15+85.0 on Page 40.

	Lt	℄	Rt			
3+00		183.8 / 6.3	184.14 / 6.34 (3' par edge)	5+62.20	164.3 / 12.8 (9d)	163.95 / 13.16 (Hub) — 163.92 / 40
2+50		183.2 / 5.2	183.22 / 5.89 (3' par edge)	5+30	165.3 / 11.8	
2+00		183.9 / 5.2	183.74 / 5.37 (3' par edge)	5+00	167.1 / 10.0	
1+50		184.3 / 4.8	184.36 / 4.75 (3' par edge)	4+50	171.9 / 5.2	
1+00		184.1 / 4.4	184.85 / 4.26 (3' par edge)	TP, 0.30	⟨π 177.11⟩	12.30 176.81
0+50		184.4 / 4.2	184.40 / 4.71 (3' par edge)	4+00	178.2 / 10.2	
0+00 Reset Hub		181.4 / 7.4	182.04 / 7.04 (3' par edge)	3+78	181.6 / 7.5	
0-50		178.8 / 10.3	178.94 / 10.17 (3' par edge)	3+68	182.23 / 6.88 (par edge)	
0-100		175.2 / 13.9		3+38	182.25 / 6.86 (par edge)	
BM	7.25 ⟨π 189.11⟩		181.86 SE BM Alg. & Market	3+35 Reset Hub Angle Page 36 86°03' Reset	182.5 / 6.6	R Pitta St
					⟨189.11⟩	

Line m from W 24 8 Victory Manor

Line m to 5+44 St

	Lt	℄	Rt
4+00	126.0 / 8.8 / 10	125.9 / 8.9 / 9	121.7 / 13.1	121.8 / 13.0 / 10
3+50	127.0 / 7.8 / 10	126.8 / 8.0 / 9	122.7 / 12.1	122.7 / 12.1 / 10
3+00	127.8 / 7.0 / 10	127.5 / 7.3 / 9	124.0 / 10.8	124.0 / 10.8 / 10
2+50	129.2 / 5.6 / 10	124.5 / 10.3	125.0 / 9.8 / 10
2+00	129.9 / 4.9 / 10	129.8 / 5.0 / 9	125.9 / 8.9	126.6 / 8.2 / 10
1+50	131.2 / 3.6 / 10	130.8 / 4.0 / 7	128.6 / 6.2	124.1 / 5.7 / 10
1+00	132.2 / 2.6 / 10	132.0 / 2.8 / 8	129.9 / 4.9	130.6 / 4.2 / 10
0+50	133.2 / 1.6 / 10	132.8 / 2.0 / 7	130.6 / 2.2	131.4 / 3.4 / 10
wly 0+00			131.7 / 3.1
=s 1+45.82 Fly	5.73	134.81	Dal
	6.73	~~133.81~~	129.08

P31

	Lt	℄	Rt
8+05.35 L. Lt. 92°15'			117.2 / 13.05 on H46
7+75	120.1 / 7.7 / 12	119.7 / 8.1 / 9	116.6 / 11.3	115.3 / 12.5 / 3	115.4 / 12.6 / 10
7+50	120.5 / 7.3 / 12	120.1 / 7.7 / 9	116.0 / 11.8	116.0 / 11.8 / 8	117.2 / 10.6 / 12
7+00	120.9 / 6.9 / 10	120.1 / 7.1 / 9	117.0 / 10.8	117.1 / 10.7 / 8	118.4 / 9.4 / 12
6+50	121.9 / 5.9 / 10	121.6 / 6.2 / 8	118.8 / 9.0	118.1 / 9.7 / 3	117.8 / 10.0 / 8	118.5 / 9.3 / 12
6+00	122.6 / 5.2 / 10	122.4 / 5.4 / 8	119.4 / 8.4	119.1 / 8.7 / 8	120.0 / 7.8 / 12
5+50	123.5 / 4.3 / 10	123.3 / 4.7 / 8	120.6 / 7.2	119.0 / 8.8 / 2	120.1 / 7.7 / 8	121.1 / 6.7 / 12
5+00	124.4 / 3.4 / 10	124.3 / 3.5 / 9	120.5 / 7.3	119.8 / 8.0 / 2	119.7 / 8.1 / 8	121.5 / 6.3 / 12
4+50	125.5 / 2.3 / 10	125.4 / 2.4 / 8	121.9 / 5.9	121.0 / 6.8 / 3	121.0 / 6.8 / 10
		127.77	Dal		125.81	Dal
TP 1.96		~~125.77~~		9.00	~~126.81~~

TP, 11.03 125.81
8.09 145.82
Hub 131.20
7.76 136.84 129.08

129.08

BM Starting 6.33 129.09

135.42
TP2 8.92 136.42 1.27 126.50

1004-D.
8+57.39 ℄ Existing SMH #45 119.76 117.8
E of 54th St 8.01 14.0
rim 9d

8+45 118.3
9.5

8+30 119.6
8.2

8+17 119.7
8.1

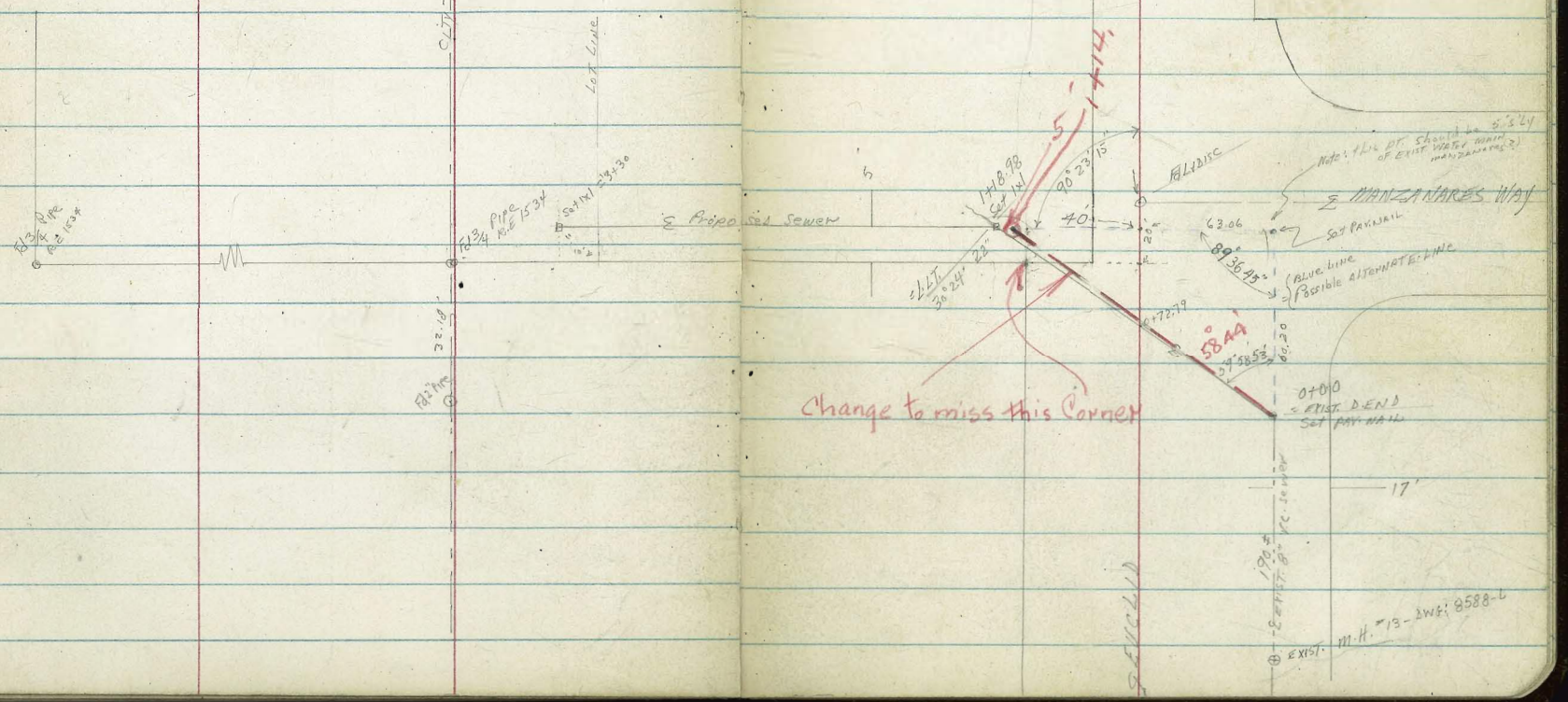
127.77 Dot
~~128.27~~

Clark
Shepherd
Bruner
O'Neil
11-5-54
W.O. 62394

PROPOSED SEWER - LOT 53 - EX-
MISSION LANDS (SWLY EUCLID &
CHURCHWARD -

REF: T.P.S. 3325
DWG: 8588-L

Sketch not to scale:
Notes: Pg 49



Proposed Sewer - Lot 53
EX-MISSION LANDS

1+04 = B.W.

0+79.50 = W'Ly Edge Conc. Pav. (outs along Edge-Pav) grd Flush-Pav

0+68.30 = ℄ EXIST. Conc Pav.

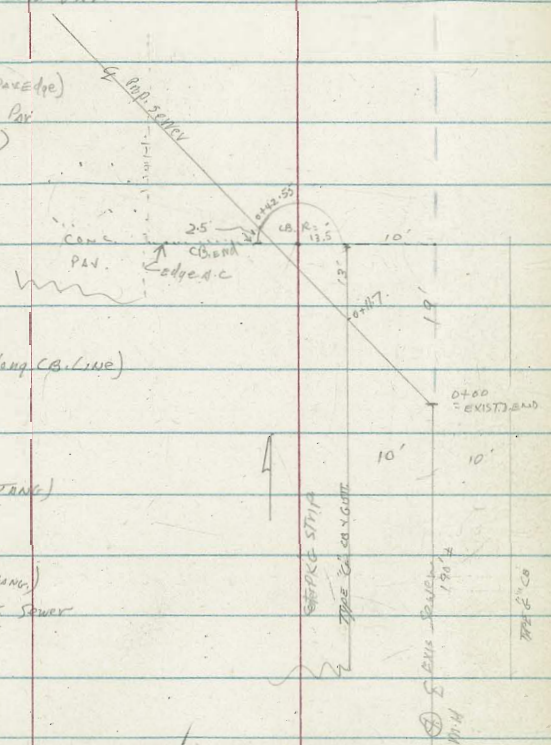
0+57.10 = edge Conc. Pav (meets A.C.) (outs along Pav Edge)

0+42.55

0+11.7 (outs along CB. Line)

0+00 (Sect. 90° For Tank)

(Sect. at 90° BK Tank)
0+00 : Approx. D.END EXIST. Sewer



T.P. 1.02 (174.07) 12.99 (173.05)

B.M. 0.90 (186.02) ~~184.22~~ 185.12 = S.E. BP
Imperial & Churchward

LT. ℄ RT.

169.0 / 5.1 / 10
169.07 / 5.0 / Top Bank
170.9 / 3.2 / 7
171.7 / 2.4 / 10

169.06 / 5.01 / 10
169.81 / 4.26
170.50 / 3.57 / 10

169.63 / 4.44

168.49 / 5.58 / 10
169.27 / 4.80
170.18 / 3.89 / 10

167.6 / 6.5 / 10 / grd.
168.69 / 5.38 / 2.5 / CB (end CB)
168.09 / 5.98 / 2.5 / G
168.80 / 5.27 / CB / ℄
168.22 / 5.85 / G / ℄
168.87 / 5.20 / 10 / on A.C

169.49 / 4.58 / 10 / CB
169.04 / 5.03 / 10 / G
169.93 / 4.14 / CB / ℄
169.49 / 4.58 / G / ℄ grd Flush TT CB
169.83 / 4.24 / 13.0 / G
170.29 / 3.78 / 13.0 / CB

168.87 / 5.20
169.05 / 5.05
169.32 / 4.75 / 10

169.23 / ~~4.84~~ / 10 / G
169.05 / 5.05
168.73 / 5.34 / 10 / G

(174.07)

Prop. Sewer LOT. 53 (cont.)

Note: End Levels Alternate-Line

1+63.26 = -1x1 = (1+18.98 L LT on Proposed-Line)

1+39 Tp. Bank

1+35 -toe

1+29 = W'ly Edge-Pav.

1+19 = ℄ Exist Con. Pav

1+09 E'ly Edge Con. (meets A.C.)

1+02.5 4' RT = ℄ Exist. Gate-Valve - Water

+60.20 - L LT

0+00 +50 (on Alternate Line = Blue-Line Sketch Pg 48)

Note: Cont. Levels on Proposed ℄ on Pg 51 - Beg Levels on Alternate Line here

1+18.98 L LT (outs 90° for tang.)

1+18.98 L LT 30° 24' 22" (outs 90° back tang.)

LT	℄	RT
	170.5	
	3.6	
	171.7	
	2.4	
	170.9	
	3.2	
	171.37	
	2.70	
	171.82	
	2.25	
	172.04	
	2.03	
	172.1	
	2.0	
	171.42	
	2.65	

168.9	168.6	170.1	170.5	171.9
5.2	5.5	4.0	3.6	2.2
10	6	3		10
	toe	tp		

rises

168.5	169.8	170.5	171.8
5.6	4.3	3.6	2.3
10	5		10
toe	TP BANK		

(174.07)

Proposed Sewer Lot 53 (Cont.)

		LT	℄	RT.	
4+75			160.6 / 13.5		
4+50			161.6 / 12.5		grd rises
4+00			164.3 / 9.8		grd rises
3+30	= Pt. 10±W'ly of E'ly Line of Lot owned by Vance.	162.6 / 11.5 / 10 — 164.1 / 10.0 / 6	165.0 / 9.1	166.6 / 7.5 / 10	
3+20	4.8 LT. = S.W. Corn. Fence (and E+W. Fence) ℄ Crosses N+S 4' Wire Fence				
3+00	℄ crosses 4' Post + Wire Fence N+S (4.7 LT. ℄ E+West Fence continues)	162.8 / 11.3 / 10	163.6 / 10.5	164.9 / 9.2 / 10	rises
2+60	(4.9' LT = S.E Corn. Fence - Fence L W'ly at Corn. + Continues 4' wire + Post - Fence N+South Line				
2+50		162.6 / 11.5 / 10	164 / 9.9	164.9 / 9.2 / 10	rises
2+00		165.4 / 8.7 / 10 — 165.3 / 8.8 / 8 — 166.9 / 7.2 / 5	167.1 / 7.0	167.8 / 6.3 / 10 — 169.6 / 4.5 / 25	rises
1+50		168.3 / 5.8 / 10 — 168 / 5.9 / 9 — 170.1 / 4.0 / 7 to Bank	170.6 / 3.0 — ⟨170.5⟩	171.4 / 2.7 / 10 — 173.4 / 0.7 / 25	rises
1+18.98			⟨174.07⟩		

Note: Cont. Lewis Proposed Line here

Sewer Lot 53 (Cont.)

					Lt.	℄	Rt.
Chk.			1.74	185.10 = 185.12 = STG B.M.			
T.P.	13.33	186.84	0.56	173.51			
5+25		grd rises ahead - ℄ -				161.5 ✓ 12.6	Rises
4+90	= Low-pt of N+S gully - grd rises ahead on ℄					158.6 ✓ 15.5	Rises
						⟨174.07⟩ ✓	

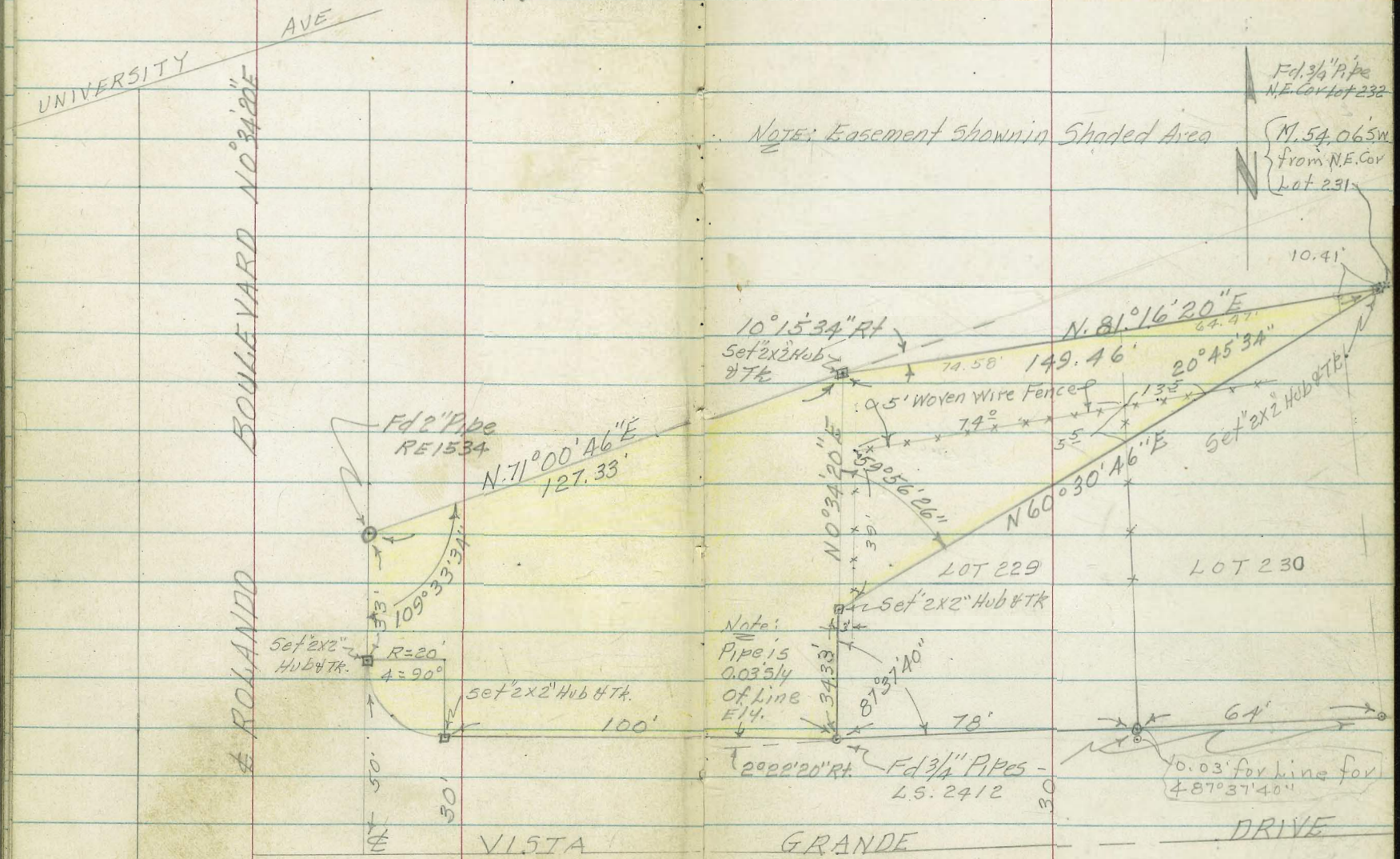
(Cont'd Pg. 54) 11-18-54

Stamper
Huffman
Nordahl
Elmore

SURVEY OF DRAINAGE EASEMENT AT ROLANDO BLVD & VISTA GRANDE DRIVE W.O. 20005-2

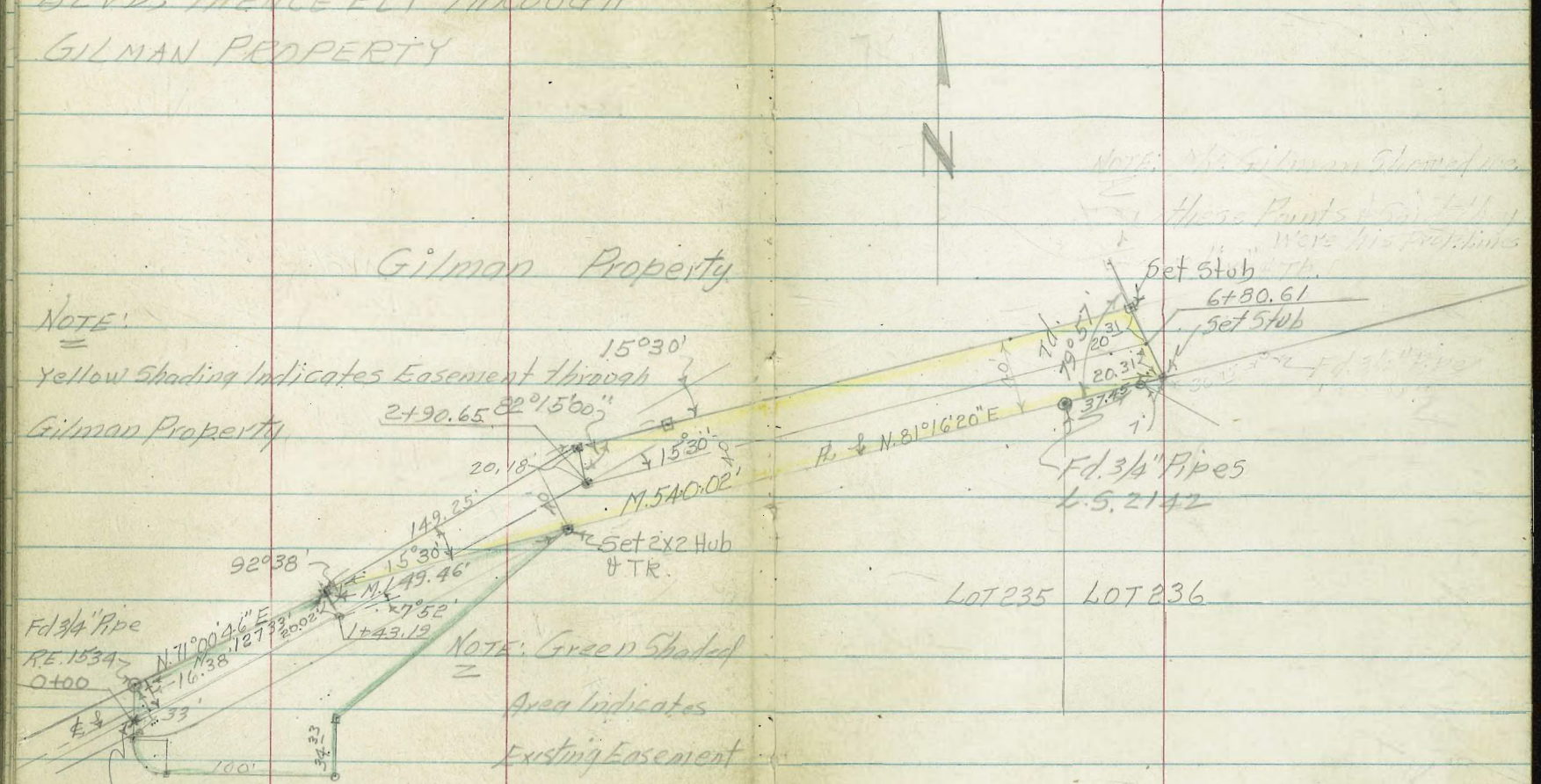
Ref Map 2762
Cosgrove Hts Annex No 2

NOTE: Easement shown in Shaded Area



12-2-54 Stamper
Hoffman
Nordahl
Elmore

TIES TO PROPOSED EASEMENT FOR DRAINAGE DITCH FROM EXISTING BOX CULVERT @ ELY SIDE OF ROLANDO BLVD; THENCE ELY THROUGH GILMAN PROPERTY



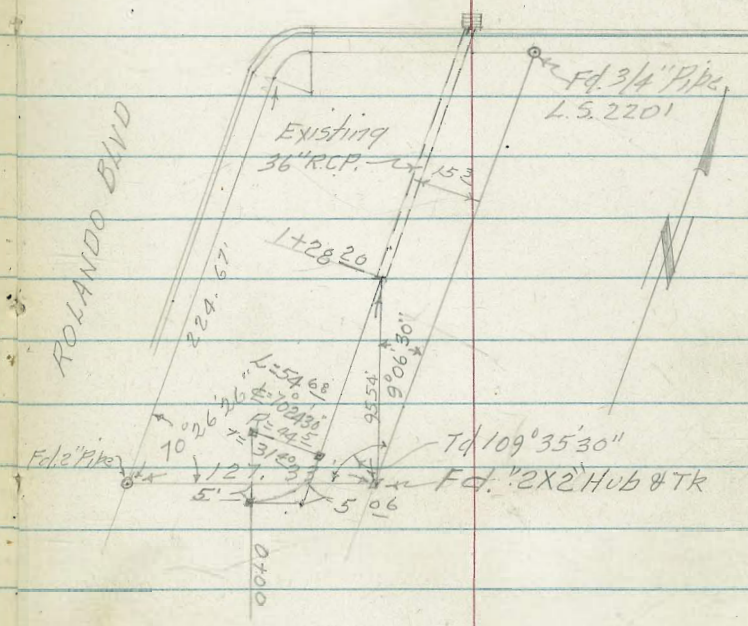
SURVEY TO EXTEND 36" R.C.P. TO CREEK CHANNEL @ SELY COR. ROLANDO BLVD & UNIVERSITY AVE W.O. 21306

(NOTES Pg. 57)

1-11-55

Ref Map No 2762
Ref Dwg No 5543-B

Stamper
Huffman
Sherwood
Elmore



■ = Set 2X2" Hub & Tack

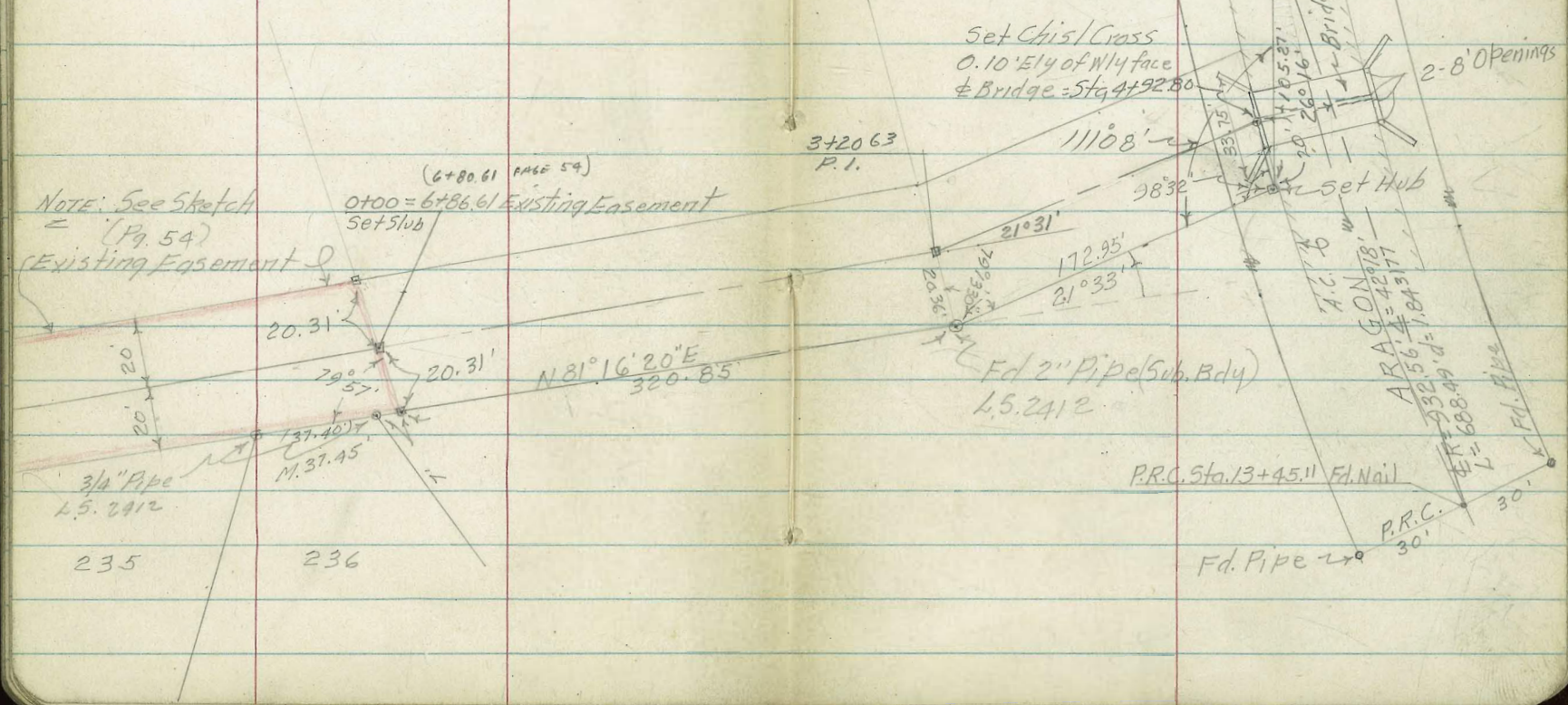
Ref F.B. 8-34/4

1-12-55

Stamper
Huffman
Sherwood
Elmore
Cota

SURVEY FOR EXTENSION OF CHANNEL ELY OF EASEMENT SHOWN ON 5543-B, TO CULVERT UNDER ARAGON DRIVE W.O. 21306

(Notes Pg 59)



1-12-55

NOTE: See Sketch Pg. 55

PROFILE FOR PROPOSED EXTENSION OF 36" R.C.P. DRAIN @ S.E.LY. COR OF ROLANDO BLVD & UNIVERSITY AVE W.O. 21306

	Lt.	℄	Rt.		
1+00	352.0 4.5 10	346.8 9.7 0	346.6 9.9 10	346.6 9.9 13 Toe	352.0 4.5 23 Top
0+75	348.8 7.7 10	347.0 9.5 0	345.4 11.1 2	346.7 10.3 10	
0+54.68 E.C.	346.6 9.9 10	346.2 9.6 0	347.7 8.8 10		
0+27.34 P.O.C.	346.1 10.4 10	346.2 9.6 0	346.6 11.9 24 channel		
	346.2 10.3 10	345.4 11.1 0	348.2 11.6 10 channel		

℄ = 70°24'30" R = 44.50 T = 31.40' L = 54.68
0+00 = B.C. Lt. (See Sketch 4 Pg. 55)

County Datum

B.M. +13.00 356.50 343.50
G-328-37

℄ 356.50

F.L. of E'ly ℄ of S'ly Opening Box Culvert @ Rolando Blvd & Vista Grande Drive

Lt. ℄ Rt.

1-12-55

PROPOSED EXTENSION 36" R.C.P. DRAIN

B. M. -13.00 343.50 ~ 343.50

1+28.20 = End 36" R.C.P. 349.08 7.42 F.L.

1+28.20 = End of Existing 36" R.C.P. 351.61 4.9 6 347.81 8.7 0 Ground 345.8 6.6 7

π 356.50 ← County Datum

1-12-55

Stamper
Huffman
Sherwood
Elmore
Cota

CROSS SECTIONS OF PROPOSED EXTENSION ELY FROM EASEMENT SHOWN ON DWG. 5543-B OF DRAIN CHANNEL TO CULV. @ ARAGON DRIVE

W.O. 21306

NOTE: See Sketch Pg. 56

NOTE: Rods Shown -(-0.0) are Plus and are to be added to H.I.

	Lt.				℄				Rt
2+00	359.6	355.2	355.4	357.5	357.1	353.8	355.5	355.8	356.8
	6.7	6.1	5.9	6.8	7.2	7.5	5.8	5.4	4.4
	50	20	9	5	0	8	11	20	30
1+50	359.0	353.9	359.7	353.7	352.8	353.3	353.8	354.8	359.7	359.8
	7.3	7.4	6.6	7.4	8.4	8.0	7.5	6.5	6.6	6.4
	50	20	14	6	0	7	10	16	20	30
1+00	359.0	357.7	359.0	352.8	352.1	352.4	358.3	359.2	359.6
	7.3	7.6	7.3	8.5	9.2	8.9	7.0	7.1	6.7
	50	20	11	8	0	12	14	20	30
0+50	353.8	353.8	359.7	357.0	357.8	357.7	353.9	357.1	359.3
	7.4	7.5	6.6	9.3	9.4	9.6	7.4	7.2	7.0
	50	20	14	11	0	7	14	20	30
0+00 = ℄ Sta. 6+80.61 = Ely End Existing Easement.	359.3	357.4	359.3	357.1	357.0	357.7	358.2	358.2	358.4
	7.0	6.9	7.0	10.0	10.3	9.6	8.1	8.4	7.9
	50	30	20	12	0	12	18	20	30

℄ 361.26

T.P.	+8.11	361.26	-3.35	353.15
B.M.	+13.00	356.50		343.50

County Datum

See Pg 57

EXTENSION OF CHANNEL SECTIONS

Lt. ℄ Rt.

1-12-55

4+50	358.8	359.1	358.8	355.8	355.4	355.5	357.2	359.3	360.3
	8.0	6.7	7.0	10.0	10.4	10.3	8.6	6.5	5.5
	50	20	15	8	0	4	10	20	30
4+00	358.4	357.6	357.7	355.8	355.3	355.8	358.4	362.6	366.1
	9.4	8.2	8.1	10.0	10.5	10.0	7.4	2.2	-(-0.3)
	50	20	12	9	0	4	10	20	30
3+50	355.9	357.4	358.1	355.0	354.5	356.2	359.0	369.3	368.2
	9.9	8.4	7.7	10.8	11.3	9.6	6.8	1.5	-(-2.4)
	50	20	13	10	0	6	10	20	30
3+20.63 P.I. Sec on Split Angle	355.6	357.3	358.0	357.7	354.5	355.1	358.4	369.0	368.7
	10.2	8.5	7.8	11.1	11.3	10.7	7.4	1.8	-(-2.9)
	50	20	15	10	0	6	8	20	30
3+00	355.5	357.0	357.7	357.3	357.2	357.3	357.1	360.2	362.5	366.7
	10.3	8.8	8.1	11.5	11.6	11.5	8.8	5.6	3.3	-(-0.9)
	50	20	11	6	0	6	8	17	20	30
2+50	354.6	356.0	356.7	354.5	357.2	353.8	356.1	357.8	359.0
	11.2	9.8	9.1	11.3	11.6	12.0	9.7	8.0	6.8
	50	20	12	5	0	6	10	20	30

T.P. +9.96 365.77 -5.45 355.81

℄ 365.77 ← County Datum

℄ 361.26

Lt. ℄ Rt

1-12-55

EXTENSION OF CHANNEL SECTIONS

B.M.

B.M.		-0.75	373.14	~ 373.32	See B-34/4 chisl "□" 112' N'ly of ℄ Univ (BM #7A) N.E. Cor Aragon & Univ
T.P.	+9.90	373.89 -1.78	363.99	S'ly End Curb	S.W. Cor Aragon & Univ.

4+92.80 = W'ly End Box Culvert

356.00
9.77
0 4
F.L.

4+85 W'ly End of Wing Wall

363.0	362.7	361.26	357.5	355.8	357.21	361.25	361.8	362.8
2.8	3.1	4.51	8.3	10.0	8.6	4.52	3.9	3.0
30	21	17.7	14	0	14	16	20	30
		Top Wing Wall				Top Wing Wall		

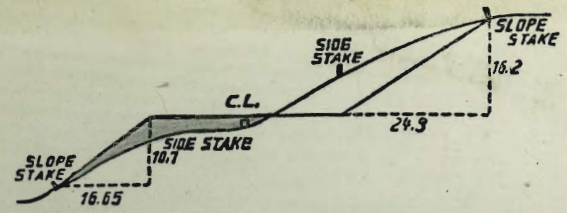
π 365.77 ← County Datum

2178.23
19 29 88
2 48 35
19 38 13
21 86 48
11 92 95
23 79 43

23 71 18
21 78 23
1 9295

1943813
2988
8,25

190.09
8.66
181.43



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.20	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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