

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
SLOPE 1 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.10	0.20	0.30	0.40	0.50	0.60	0.70	0.80	0.90	0
1	1.00	1.10	1.20	1.30	1.40	1.50	1.60	1.70	1.80	1.90	1
2	2.00	2.10	2.20	2.30	2.40	2.50	2.60	2.70	2.80	2.90	2
3	3.00	3.10	3.20	3.30	3.40	3.50	3.60	3.70	3.80	3.90	3
4	4.00	4.10	4.20	4.30	4.40	4.50	4.60	4.70	4.80	4.90	4
5	5.00	5.10	5.20	5.30	5.40	5.50	5.60	5.70	5.80	5.90	5
6	6.00	6.10	6.20	6.30	6.40	6.50	6.60	6.70	6.80	6.90	6
7	7.00	7.10	7.20	7.30	7.40	7.50	7.60	7.70	7.80	7.90	7
8	8.00	8.10	8.20	8.30	8.40	8.50	8.60	8.70	8.80	8.90	8
9	9.00	9.10	9.20	9.30	9.40	9.50	9.60	9.70	9.80	9.90	9
10	10.00	10.10	10.20	10.30	10.40	10.50	10.60	10.70	10.80	10.90	10
11	11.00	11.10	11.20	11.30	11.40	11.50	11.60	11.70	11.80	11.90	11
12	12.00	12.10	12.20	12.30	12.40	12.50	12.60	12.70	12.80	12.90	12
13	13.00	13.10	13.20	13.30	13.40	13.50	13.60	13.70	13.80	13.90	13
14	14.00	14.10	14.20	14.30	14.40	14.50	14.60	14.70	14.80	14.90	14
15	15.00	15.10	15.20	15.30	15.40	15.50	15.60	15.70	15.80	15.90	15
16	16.00	16.10	16.20	16.30	16.40	16.50	16.60	16.70	16.80	16.90	16
17	17.00	17.10	17.20	17.30	17.40	17.50	17.60	17.70	17.80	17.90	17
18	18.00	18.10	18.20	18.30	18.40	18.50	18.60	18.70	18.80	18.90	18
19	19.00	19.10	19.20	19.30	19.40	19.50	19.60	19.70	19.80	19.90	19
20	20.00	20.10	20.20	20.30	20.40	20.50	20.60	20.70	20.80	20.90	20
21	21.00	21.10	21.20	21.30	21.40	21.50	21.60	21.70	21.80	21.90	21
22	22.00	22.10	22.20	22.30	22.40	22.50	22.60	22.70	22.80	22.90	22
23	23.00	23.10	23.20	23.30	23.40	23.50	23.60	23.70	23.80	23.90	23
24	24.00	24.10	24.20	24.30	24.40	24.50	24.60	24.70	24.80	24.90	24
25	25.00	25.10	25.20	25.30	25.40	25.50	25.60	25.70	25.80	25.90	25
26	26.00	26.10	26.20	26.30	26.40	26.50	26.60	26.70	26.80	26.90	26
27	27.00	27.10	27.20	27.30	27.40	27.50	27.60	27.70	27.80	27.90	27
28	28.00	28.10	28.20	28.30	28.40	28.50	28.60	28.70	28.80	28.90	28
29	29.00	29.10	29.20	29.30	29.40	29.50	29.60	29.70	29.80	29.90	29
30	30.00	30.10	30.20	30.30	30.40	30.50	30.60	30.70	30.80	30.90	30
31	31.00	31.10	31.20	31.30	31.40	31.50	31.60	31.70	31.80	31.90	31
32	32.00	32.10	32.20	32.30	32.40	32.50	32.60	32.70	32.80	32.90	32
33	33.00	33.10	33.20	33.30	33.40	33.50	33.60	33.70	33.80	33.90	33
34	34.00	34.10	34.20	34.30	34.40	34.50	34.60	34.70	34.80	34.90	34
35	35.00	35.10	35.20	35.30	35.40	35.50	35.60	35.70	35.80	35.90	35
36	36.00	36.10	36.20	36.30	36.40	36.50	36.60	36.70	36.80	36.90	36
37	37.00	37.10	37.20	37.30	37.40	37.50	37.60	37.70	37.80	37.90	37
38	38.00	38.10	38.20	38.30	38.40	38.50	38.60	38.70	38.80	38.90	38
39	39.00	39.10	39.20	39.30	39.40	39.50	39.60	39.70	39.80	39.90	39
40	40.00	40.10	40.20	40.30	40.40	40.50	40.60	40.70	40.80	40.90	40
41	41.00	41.10	41.20	41.30	41.40	41.50	41.60	41.70	41.80	41.90	41
42	42.00	42.10	42.20	42.30	42.40	42.50	42.60	42.70	42.80	42.90	42
43	43.00	43.10	43.20	43.30	43.40	43.50	43.60	43.70	43.80	43.90	43
44	44.00	44.10	44.20	44.30	44.40	44.50	44.60	44.70	44.80	44.90	44
45	45.00	45.10	45.20	45.30	45.40	45.50	45.60	45.70	45.80	45.90	45
46	46.00	46.10	46.20	46.30	46.40	46.50	46.60	46.70	46.80	46.90	46
47	47.00	47.10	47.20	47.30	47.40	47.50	47.60	47.70	47.80	47.90	47
48	48.00	48.10	48.20	48.30	48.40	48.50	48.60	48.70	48.80	48.90	48
49	49.00	49.10	49.20	49.30	49.40	49.50	49.60	49.70	49.80	49.90	49
50	50.00	50.10	50.20	50.30	50.40	50.50	50.60	50.70	50.80	50.90	50

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, by or target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the sight adjustment necessary.

TABLE XIII—CORRECTIONS FOR TANGENTS AND EXTERNALS

These corrections are to be added to the approximate values, found by dividing the tangent, or external, for a 1° curve (Table VIII) by the degree of curve, in order to obtain the true tangents, or externals. Intermediate values may be obtained by interpolation.

FOR TANGENTS ADD

Central Angle	DEGREE OF CURVE														
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	
10°	.03	.06	.09	.13	.16	.19	.22	.25	.28	.31	.34	.38	.42	.46	
15°	.04	.10	.14	.19	.24	.29	.34	.39	.45	.51	.53	.58	.63	.68	
20°	.06	.13	.19	.26	.32	.39	.45	.51	.58	.65	.72	.79	.84	.90	
25°	.08	.16	.24	.33	.40	.49	.58	.67	.75	.83	.90	.99	1.06	1.14	
30°	.10	.19	.29	.39	.49	.59	.69	.79	.89	.99	1.09	1.20	1.29	1.39	
35°	.11	.22	.34	.47	.58	.69	.79	.81	.92	1.04	1.29	1.42	1.54	1.66	
40°	.13	.26	.40	.53	.67	.80	.93	1.06	1.20	1.34	1.49	1.64	1.79	1.94	
45°	.15	.30	.44	.60	.76	.91	1.06	1.21	1.37	1.52	1.70	1.87	2.04	2.21	
50°	.17	.34	.51	.68	.85	1.02	1.19	1.36	1.54	1.72	1.91	2.10	2.29	2.48	
55°	.19	.38	.57	.76	.95	1.14	1.32	1.52	1.72	1.92	2.14	2.35	2.56	2.77	
60°	.21	.42	.63	.84	1.05	1.27	1.49	1.71	1.94	2.17	2.38	2.60	2.83	3.07	
65°	.23	.46	.69	.93	1.16	1.40	1.64	1.88	2.13	2.38	2.63	2.88	3.13	3.39	
70°	.25	.51	.76	1.02	1.28	1.54	1.80	2.06	2.33	2.60	2.88	3.16	3.44	3.72	
75°	.27	.56	.83	1.12	1.40	1.69	1.98	2.27	2.57	2.87	3.16	3.47	3.78	4.09	
80°	.30	.61	.91	1.22	1.53	1.84	2.15	2.46	2.78	3.10	3.44	3.78	4.12	4.46	
85°	.33	.66	1.00	1.33	1.68	2.02	2.36	2.70	3.05	3.40	3.77	4.14	4.55	4.89	
90°	.36	.72	1.09	1.45	1.83	2.20	2.57	2.94	3.32	3.70	4.10	4.50	4.91	5.32	
95°	.39	.79	1.19	1.55	2.00	2.40	2.80	3.20	3.61	4.02	4.40	4.98	5.38	5.83	
100°	.43	.86	1.30	1.74	2.18	2.62	3.06	3.50	3.95	4.40	4.88	5.37	5.85	6.34	
110°	.51	1.03	1.56	2.08	2.61	3.14	3.67	4.21	4.76	5.31	5.86	6.43	7.01	7.60	
120°	.62	1.25	1.93	2.52	3.16	3.81	4.45	5.11	5.77	6.44	7.12	7.80	8.50	9.22	

FOR EXTERNALS ADD

Central Angle	DEGREE OF CURVE														
	5°	10°	15°	20°	25°	30°	35°	40°	45°	50°	55°	60°	65°	70°	
10°	.001	.003	.004	.006	.007	.008	.009	.011	.012	.014	.015	.017	.018	.020	
15°	.003	.007	.010	.014	.018	.023	.027	.029	.032	.035	.039	.043	.047	.051	
20°	.006	.011	.017	.022	.028	.034	.038	.045	.051	.057	.063	.070	.076	.083	
25°	.009	.018	.027	.036	.046	.056	.065	.074	.083	.093	.106	.120	.127	.135	
30°	.013	.025	.038	.051	.065	.078	.090	.103	.116	.129	.149	.170	.179	.188	
35°	.018	.035	.054	.072	.086	.109	.131	.153	.175	.197	.213	.230	.247	.264	
40°	.023	.046	.070	.093	.117	.141	.172	.203	.234	.265	.277	.290	.315	.341	
45°	.030	.060	.093	.119	.153	.184	.216	.254	.289	.325	.351	.378	.411	.445	
50°	.037	.075	.116	.151	.189	.227	.266	.305	.345	.384	.425	.467	.508	.550	
55°	.046	.093	.142	.188	.236	.283	.332	.381	.420	.479	.530	.582	.641	.700	
60°	.056	.112	.168	.225	.283	.340	.398	.457	.516	.575	.636	.697	.774	.851	
65°	.067	.135	.204	.273	.343	.412	.483	.554	.625	.697	.771	.845	.922	1.01	
70°	.080	.159	.240	.321	.403	.485	.568	.652	.735	.819	.906	.994	1.08	1.17	
75°	.095	.182	.286	.383	.480	.578	.678	.777	.877	.977	1.07	1.18	1.29	1.39	
80°	.110	.220	.332	.445	.558	.671	.787	.903	1.02	1.13	1.25	1.38	1.50	1.62	
85°	.128	.259	.391	.524	.657	.790	.926	1.06	1.20	1.34	1.47	1.62	1.76	1.91	
90°	.149	.299	.450	.603	.756	.910	1.07	1.22	1.38	1.54	1.70	1.87	2.03	2.20	
95°	.174	.350	.522	.706	.885	1.06	1.25	1.43	1.62	1.80	1.99	2.18	2.38	2.58	
100°	.200	.401	.604	.809	1.01	1.22	1.43	1.64	1.85	2.06	2.28	2.50	2.73	2.96	
110°	.268	.536	.806	1.08	1.35	1.63	1.91	2.20	2.48	2.76	3.05	3.35	3.66	3.96	
120°	.360	.721	1.08	1.45	1.82	2.19	2.57	2.95	3.33	3.72	4.11	4.50	4.91	5.32	

Index

X-sec alley BIK 4 - East gate

1-14

Events - Garnett to Felspar 15-21

" Jefferson Trias to Twiggs 22-45

" Harnoy - Moore to Congress 46-54

" Conde St. " " 55-65

" Moore St. Trias to Ampudia 66-71

" " Ampudia to Arista 72-76

Arista St. Tie Points 77

X-sec Alley BIK 4 - Eastgate

LT = W 1/4

Q

Rt = E 1/4

2

0+10

354.8	3550	354.3	3540	3540	354.6	354.8
3 1/2	3 1/2	3 1/2	4 1/2	4 1/2	3 1/2	3 1/2
20	11	10	7	7	10	20

0+00^L 10° LT = begin 15' high rubble conc wall-

352.36	352.66
5 1/2	5 1/2
10 1/2	10 1/2
Foot	Gr

0+00 = N 1/4 Orange Ave - N 1/4 edge A.C.

353.02	352.69	352.46	352.79	353.19
5 1/2	5 1/2	5 20	5 37	4 27
10 1/2	10 1/2	5 20	10 1/2	10 1/2
cb	Gut		Gut	cb

0-14⁵ EC Alley returns - 15' Radius

352.83	352.26	352.89	353.04
5 33	5 20	5 27	5 12
cb	Gut	Gut	cb
EC	EC	EC	EC
10 1/2	10 1/2	10 1/2	10 1/2

352.0	351.52
6 1/2	6 1/2
10 1/2	10 1/2
cb	Gut

353.09	353.14
5 07	4 52
10 1/2	10 1/2
Gut	cb

0-16 = N 1/4 cb line orange Ave

352.44	351.83	352.31	352.18	352.17	352.17	352.31	352.33	353.04	352.63	353.26
5 72	6 33	5 34	5 28	5 29	5 29	5 25	5 43	5 12	5 53	4 20
5 0	5 0	11 1/2	11 1/2	10	10	10	11 1/2	11 1/2	5 0	5 0
cb	Gut	cb	bc	Gut	Gut	10	bc	bc	Gut	cb

REDUCED
MECHAN
4/10/53

BM. 4.22 358.16

NW 1/4 - 1/4 PL +
353.94 Orange

358.16

LT=W14

4

RT=ely.

3

0+52-12⁴ LT=SE, COR 2⁵ N+S CONC WALK

355.58

2⁵8

12⁴
SE COR
WALK

0+50

355.4

2⁸

25

355.4

2⁸

10

355.2

3⁰

355.3

2²

10

355.1

3¹

25

0+48-12⁰ LT=NE, COR 2' N+S CONC. WALK
9⁸ RT=begin 4⁵ high picket fence

355.34

2⁸2

12⁰
NE COR
WALK

0+25

354.9

3³

10

354.8

3⁴

354.7

3⁵

7

355.0

3²

10

0+12-12⁰ LT=S.E. COR 2' CONC WALK RUNNING N+S

354.91

3¹9

12⁰
WALK
SE COR

0+12-10⁰ LT=end 1⁵ high rubble conc wall-

354.1

4¹

10⁰

FOOT

354.6

3⁶

10⁰

Gr

358.16

X-sec Alley BIR 4- East gate.

LT = W 1/4

2 Lt = 1/4 - 4

1+83-11⁵ Lt = 2' Conc Walk

355.77
4 99
115
WIC
355.87
489
255

1+72-98 Lt = begin 4⁵ high picket fence

1+53-96 Lt = end 4⁵ high picket fence.

1+50

355.9
49
10
355.5
53
10
356.0
48
10

1+00

355.7
51
25
355.8
50
10
355.4
54
8
355.6
52
8
356.0
48
10
355.0
48
25

0+98-12⁴ LT = NE COR 2⁵ N+S, Conc Walk

355.76
500
12⁴
NE COR

TP₁ 5.46 360.76 2.86 355.30

360.76 x

0+75-9⁵ LT = 12" power pole - No Number

355.1
25
10
355.3
29
10
355.5
27
10

358.16 x

X-sec Alley BIK 4 - East gate

over hanging Alley -

also begin Berry & Honey Suckle planting

10³ LT = begin 4⁵' high picket fence

3+00-10³ LT = end 4⁵' high picket fence

2+94- 10⁸ RT = ϕ single garage - Conc Apron^{Floor}

2+75- 9⁸ RT = end 4⁵' high Lath fence

2+68- 9⁸ LT = ϕ 2⁵' Conc Walk

2+66- 10¹ LT = begin 4⁵' high picket fence

2+58- 12³ LT = ϕ single garage conc floor

2+50- 9⁶ RT = end 4⁵' high picket + begin 4⁵' Lath^{fence}

2+11- 9⁴ LT = ϕ 9" power pole # PA4231

2+10- 10⁰ LT = ϕ 6" pepper tree

2+00

1+94- 8⁹ LT = ϕ dead man

LT = W 14

ϕ RT = E 14 - 5

355.2

356

355.1

355.3

355.7

4⁶

4⁸

4⁷

4⁹

5¹

25

10

10

25

355.60

355.63

5¹⁶

5¹³

10⁸
Apron

14³
Floor

355.69

5⁰⁷

19⁸

355.59

5¹⁷

9⁸

Walk

356.28

4⁴⁸

12³
Floor

356.0

4⁸

25

356.0

4⁸

10

355.8

5⁰

355.7

5¹

10

355.6

5²

25

355.9

4⁹

25

355.9

4⁹

10

355.8

5⁰

355.8

5⁰

10

355.7

5¹

25

360.76 X

X-sec Alley B1E4 - East gate

LT = W14

RT = cly

6

3+74-11⁴ LT = 4 car garage

355.61

505

180
Floor

356.38

528

114
Apron

3+72-35³ RT = 2 single garage - gravel floor

355.4

63

353

3+65-10² RT = end 3' high board fence

Apron

3+56-11⁵ LT = begin 4 car garage - conc floor

356.68

508

180
Floor

356.43

523

115
Apron

TP2 555 361.66 4.65 356.11

361.66 x

9⁴ LT = 10" power pole #PA4251

356.3

45

25

356.2

46

10

356.0

48

10

356.0

48

10

355.8

50

25

3+50-10¹ LT = end 4' high picket fence

3+26-10⁰ LT = end floral planting over hanging board fence

3+24-10⁰ RT = N.W. cor shed + begin 3' high

3+14-9² RT = S.W. cor shed board floor

3+14-9⁹ RT = N.W. cor garage fly entrance

3+04-9⁸ RT = S.W. cor garage fly entrance

360.76 x

X-sec Alley BIK 4- East gate-

LT= W 14

Et= 24 - 2

4+26- 11² LT= 4 car garage conc floor + Apron

356.80

48⁶

17⁸
Floor

356.47

51³

12²
Apron

4+25- 10² Et= end 4⁸ high board fence + begin 4' high

LOTH fence

4+08- 11³ LT= begin 4 car garage - Conc Apron +

356.34

48²

17⁸
Floor

356.52

51⁴

11³
Apron

4+05- 15² LT= 2' conc walk

356.71

49⁵

25³
WK

356.60

50⁶

15²
WK

4+00

356.4

53

10

356.3

54

356.2

55

10

356.0

52

25

3+96- 15⁴ LT= 2' conc walk

356.64

50²

25⁴
WK

356.52

51⁴

15⁴
WK

3+93- 11¹ LT= end 4 car garage w/ Conc Floor

Apron

356.62

50⁴

18⁰
Floor

356.39

52⁷

11⁴
Apron

3+88- 9⁷ Et= begin 4⁸ high board fence

361.66 T

X-sec Alley BIK 4- Eastgate

4+87. 10³ LT= end 2 car garage - Conc Apron + Floor

4+69- 10¹ LT= begin 2 car garage - Conc Floor + Apron

4+69- 10¹ LT= N.E. COR CONC slab outside Apt

4+50- 9² LT= S.E. COR ^{conc} slab outside Apt-

4+48- 11⁰ LT= 5' CONC. Walk

4+44- 11¹ LT= end 4 car garage - Conc Apron + Floor

4+42 10³ Rt= 2' CONC Walk

LT= W 14

357.11	356.70
455	496
180	103
Floor	Apron

357.18	356.61
448	505
181	101
Floor	Apron

356.80	356.61
486	505
181	101
NW COR	NE COR
Conc Slab	Conc Slab

356.00	356.58	356.68	356.4	356.3.	356.0
506	508	51	53	54	57
18	99	99		10.	25
S.W COR	Slab	Gr.			
Conc Slab					

356.50	356.51
507	515
180	110
WIK	WIK

356.76	356.46
490	520
178	111
Floor	Apron

356.26	356.96
530	570
102	353
WIK	WIK

361.66 T

X-sec Alley BIK 4. Eastgate.

LT = W14

RT = 014-

9

5+21-9⁵ LT = S.E. COK CONC slab

356.36
428
132
SW COK
slab

356.72
442
93
SE. COK
slab

Walk + Drain

5+16-9⁸ LT = N.E. COK. Combination N+S 2' CONC

356.20
486
98
NE COK

5+11-9² LT = 10" power pole # PA4271-

5400

356.6	356.3	356.5	356.5
45	48	46	46
10		10	25

Combination Walk + Drain

4+92-10² LT = S.E. COK 2' wide N+S. CONC 'U' drain

356.61
453
102
SE COK

TP₃ 0.82 361.14 1.34 360.32

361.14 *

Walk Dipped Middle

4+91-10² LT = 2' CONC Drain + Walk

356.70	356.08
496	518
20	10
Walk	Drain
Drain	

4+88.75-10³ LT = 35' CONC Walk

351.11	356.70
455	496
182	102
WK	WK

361.66 *

6426-14³ LT=4 5⁵ CONC WALK

6408-14⁴ LT & single garage- CONC floor

6400

5473-14⁵ LT=4 13⁵ CONC WALK

5450-10² LT= end 4' latk fence + begin 4' picket fence

5438-9⁴ LT=4 double garage- CONC APRON + FLOOR

5429-9⁴ LT= N.E. COR CONC slab

LT= W14

2 10-04

10

356.19

4 9⁵

24³
WIK

356.18

4 9⁶

14³
WIK

356.12

4 7²

14⁴
Floor

356.4

4 2

25

356.3

4 8

10

356.3

4 8

356.2

4 8

10

356.2

4 8

25

356.14

4 20

24⁵
WALK

356.50

4 64

14⁵
WALK

356.2

4 8

25

356.6

4 5

10

356.4

4 2

356.5

4 6

10

356.4

4 7

25

356.92

4 22

13²
FLOOR

356.84

4 30

9 4
APRON

356.92

4 22

13²
N.W. COR
SLAB

356.78

4 36

9 4
N.E. COR
SLAB

361.14

7400-

.8 x 1.3 Grate - 3" pipe flowing to Ely
6+73-17² Rt = $\frac{1}{2}$ Home Made inlet (good work.)

6+68 15² Rt = $\frac{1}{2}$ North side double garage - Conc Floor +
AC Apron

6+58-7⁵ LT = S.E. Cor AC Parking Lot for Cafe

6+58-19¹ Rt = $\frac{1}{2}$ Conc Floor No Apron
South side double garage

6+53-9⁰ LT = $\frac{1}{2}$ 11" power pole # PA +287

6+50

6+38-10¹ Rt = end 4' picket fence

LT = W 1/4 -

356.73 356.59 356.49
441 455 466
25 10 73
AC AC AC
PK LOT

356.3 356.3 356.1
48 48 50
10 25

355.42 355.01
572 613
172 178
Grate IE
3" pipe

355.38 355.02
576 552
158 191
AC Floor
Apron

356.7
44
SECOR
PK LOT

355.54
560
191
Floor

356.3 356.4 356.2 356.2 355.4
48 47 49 49 57
20 10 10 20

361.14

7+49-11⁵ = 2 lookway to Cafe.

7+46-9³ LT = 2 Deadman.

7+39-10⁴ = S.E. cor. Cafe.

7+39-9⁴ LT = 2 10" power pile * JPA 4253

7+35

7+22-11⁵ LT = 2 5⁵ AC Walk

7+05 = 2 Sewer Man hole

LT = W/Y 2 et = ely - 12

355.5³
5⁵
11⁵
Floor
Cafe

355.0	355.9	356.1	356.1
5 ¹	5 ²	5 ⁰	5 ⁰
10	7 ⁵		10
AC	AC		

356.1 ³	355.8
49 ⁵	5 ³⁰
11 ⁵	21 ⁵
AC	
Walk	

356.37
4⁷⁷
P
SMH

361.14

NECOR Alley + sigline EL CAJON Blvd
 7+79.23-10° LT= end Alley Curb return

7+77-18° LT= NECOR Cafe.

TP₄ 5.44 359.58 7.00 354.14

7+62-13° LT= 4 Doorway Cafe rest rooms

7+60

7+57-12° LT= 4 Doorway - Cafe

LT= W14

LT= 1/3.

13

354.85

473

10°
cb

354.57

501

10°
Gor

359.58 x

355.74

540

Floor
Doorway

355.4

57

10
AC

355.1

60

85
AC

355.5

56

355.8

53

10

355.4

550

12 Z
Doorway
Floor

361.14 x

X-sec Alley Bldg 4 - East 99th

LT: W 14

RT: 14

TP5

6.56

353.008
353.02

BP S.W. COR 46th + EL CaJON

355.50

40⁸

100
cb

354.98

160

100
GUT

353.48

60

50
GUT

353.95

563

50
cb

352.91

667

100
GUT

353.41

617

100
cb

EL CaJON - Sec. taken along cb line

7+97.17 - Intersection of Alley and sly curb line

354.28

460

50
cb

354.50

508

50
GUT

354.60

498

120
cb

354.09

549

120
GUT

354.01

557

10
(±)

353.98

560

10
(±)

353.91

567

12
GUT

353.90

568

12
GUT

354.4

518

12
cb

7+95.17 - B.C.'s alley returns - 2' Radius

354.64

494

102
cb

354.03

555

102
GUT

353.05

563

92
GUT

354.10

518

92
cb

NW COR Alley + EL CaJON BND

7+82.65 - 9⁸ RT + 90° to 4 Alley = ^{sly} end Alley RT

354.48

510

92
GUT

354.26

482

92
cb

7+80.94 - sly line EL CaJON BND

36.26

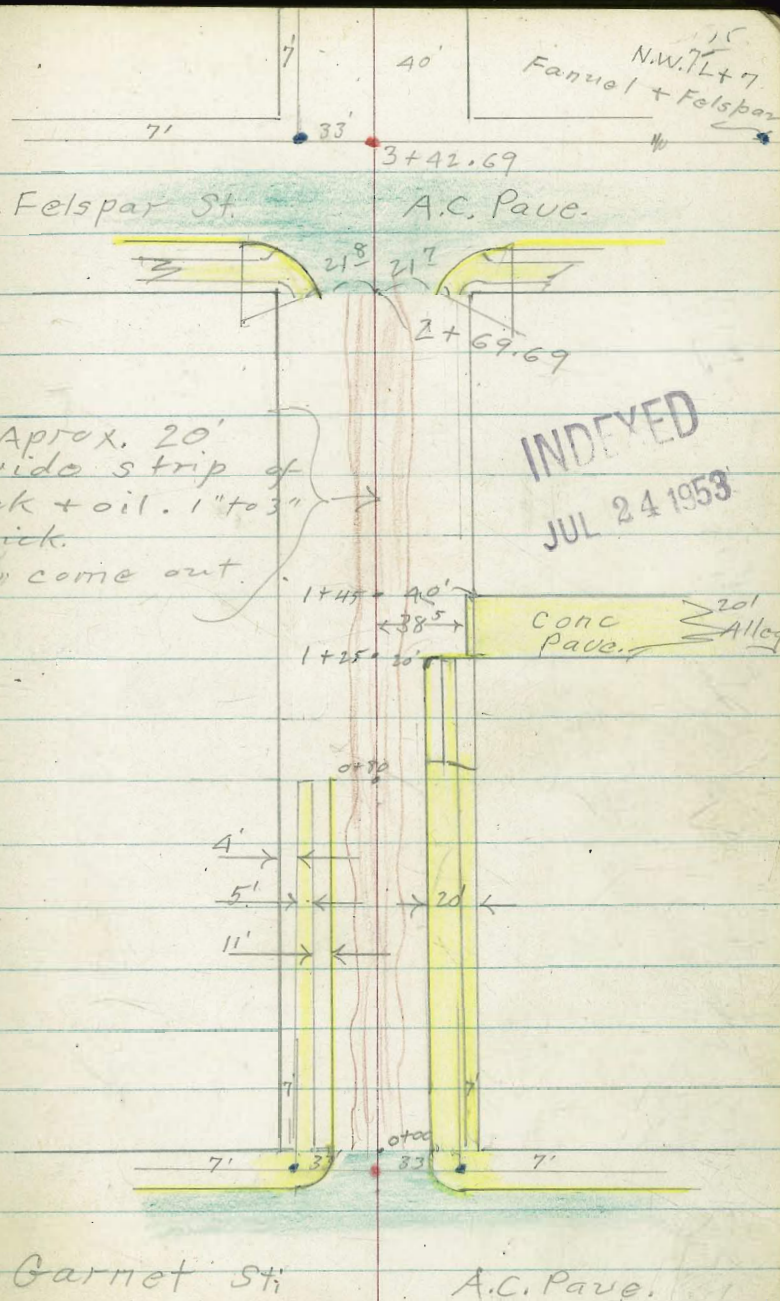
5.32

359.58

7-23-53
W.O. # 32161

•	denotes Ed. L+T. or disk
•	" Set Pk. Nail in pave
Yellow	" concrete
Green	" A.C. Pave.
Brown	" rock & oil pave.

Soil sample from 1-
15' west of ϕ Everts
100' North of Nly. line Garnet



Everts,

① +15- 20' Ht. = thru curb. start driveway

= End AC. Pave.
0 to 00 = NY line @ arnet

0-04 $\left. \begin{array}{l} 20' \text{ R} \\ 20' \text{ L} \end{array} \right\} = \text{E.C. } 10' \text{ Rad cl. Ret.}$

30' Rt. } = B.C. 10' Rad. Cl. Ret.
30' Lt. }

0-14 = Nly. cl. Garnet

0-40 = $\neq$ Garnet.

5,37	44.90	—	39.53
------	-------	---	-------

38.17	37.70	39.56	38.95	39.97	40.60	41.10	41.75
6.73	7.20	5.44	5.95	4.93	4.30	3.80	3.15
1.40	1.40	40	40	40	40	1.40	1.40
cl	G	cl	C	G	cl	G	cl
39.54	39.03	39.12	39.40	39.75	39.86	40.59	
5.30	5.87	5.78	5.50	5.15	5.04	4.31	
30	30	20		20	30	30	
cl	G				G	cl	
38.30	39.41	39.27	39.70	40.14	40.44	41.64	
6.60	5.49	5.63	5.20	4.76	4.40	3.20	
1.40	40	20		20	40	1.40	
44.90							
N.W. B.P. Garnet + Everts.							

EVERTS

0+80 { 31' Lt. = N.E. cor
20' Lt. = end ch

= end of walk.

5' wide walk

0+79 - 20' Lt. = end same

0+66 20' Lt. = start thru. curb drive way

0+50

T.R. 6.65 47.14 41.41 40.49

0+41 - 20' Lt. = end same.

41.44

5.7
40

41.39

5.75
36
walk

41.36

41.21

40.94

41.64

41.74

41.74

5.78
31
walk

5.93
20
cl

6.2
20

5.5

5.4
20

5.4
10
cl on roll
of drive

41.62

5.52
20
drive

41.51

5.63
20
drive

40.64

40.04

41.14

41.14

41.63

6.50
20
cl

7.1
20

6.0

6.0
20

5.51
20
cl

47.14

40.04

41.86
20
drive

44.90

Events

T.P. 4.61 ✓ 47.00 4.75 ✓ 42.39

38⁵ RT. = start alley pave.
22' RT. = E.C. 2' Rad. el. Rot.

1+25 - 51y line Alley

1+24 22' LT = 14" pole # P 4548

1+23 - 20' RT. = D.C. 2' Rad. el. Rot

22' LT = dead man

1+07 20' RT = start curb

1+00

Note (To make driveway
Ch. from 0+86 to 1+07 broken out)

0+86 - 20' RT. = end of el.

~~0+87 20' RT. driveway cut out.~~

41.54

42.14

41.74

40.64

42.44

5.6
40

5.0
25

5.4
16

6.5
12

4.17

42.44

4.7
28

43.09

4.05
22
cc-ec.

43.75

3.95
38⁵
pave

43.05

4.09

20
el. B.C.

42.72

4.42

20

41.54

41.64

41.04

41.94

41.94

5.6
40

5.5
20

6.1
14

5.2

5.2
20

No curb

42.29

4.85

20

el

47.14

Events

T.P. 6.35 ✓ 49.53 3.82 ✓ 43.18

1+80

1+73 26' RT = 10" diam Palm

1+62 - 26' RT = 3" diam tree

1+50 - 26' RT = 3" diam tree

1+49 { conc. walk along Bldg.
40' Lt = start 4' wide

1+45 { 38' RT = end alley pave.
Nly. line Alley

1+35 = E Alley

43.14 42.90 43.40 42.90 43.30 43.20 44.00 44.50

3.86 4.1 3.6 4.1 3.7 3.8 3.0 2.5

40 40 16 12 18 25 40

walk

42.52

41.48

40
walk

43.36

3.64

40
pave

42.30

42.70

41.90

42.80

42.40

43.40

43.93

43.50

4.7

4.3

5.1

4.2

4.6

3.6

3.67

3.5

40

20

12

20

22

38

40

pave end

40.80

42.99

43.77

6.2

4.01

3.23

40

100

on pave

41.40

41.80

42.00

42.70

42.40

42.96

5.6

5.2

5.0

4.3

4.6

4.04

40

20

12

20

38

conc.
pave

47.00

Everts,

2+89⁶⁹ } 50' Rt. } = E.C. 30' Rad. cl
 50' Lt. }
 Sly. cl line Felspar

T.P. 3.85 50.19 3.19 46.34

2+69⁶⁹ } 21⁸ Lt. } = start curb
 21² Rt. }
 Sly. line Felspar = start A.C. ^{pave.}

2+68 - 21' Lt. = Pole # 4598 (14")

2+65 - 26' Rt. = 10" diam. Palm

2+54 - 39⁷ Lt. = end conc. walk

2+42 - 26' Rt. = 16" diam Palm

2+31 - 26' Rt. = 5" diam tree

2+25

2+20 - 26' Rt. = 12" Palm

2+05 - 26' Rt. = 3" diam Tree

44.07	43.46	44.86	46.10	45.89	46.53
6.12	6.73	5.33	4.09	4.30	3.66
100	100	30	50	100	100
cl	C	cl	cl	Q	cl
44.21	44.49	44.91	45.26	45.23	45.47
5.98	5.70	5.28	4.93	4.96	4.70
50	40	20	50.19	20	40
Q				40	50
					Q

Set B.M. on N.W. 7' disk Felspar + Events

45.13	45.15	45.77	46.53
4.4	4.38	3.76	3.0
40	36	36	40
	S.W. cor	S.E. Cor.	
	walk	walk	
45.09	44.99	44.93	45.54
4.44	4.54	4.60	3.99
31	21 ⁸	21 ⁷	21 ⁷
S.E. cor	cl	Q	cl
walk			S.W. cor
			walk

44.78
 4.75
 39.2

44.03	44.33	43.73	44.30	44.13	44.83	45.53
5.5	5.2	5.8	5.1	5.4	4.7	4.0
40	17	13		21	24	40

49.53

EVERTS

21

L. Birdsell
August 3, 1953

Orig. B.M. (P-16) 7.11 39.53 (39.53)
T.P. 3.77 46.64 7.32 42.87

44.49

5.70
100

45.26

4.93
50

46.53

3.66
100

45.43

4.76
40

45.47

4.72
20

45.65

4.54

45.55

4.64
20

45.89

4.30
40

46.02

4.17
50

3 to 9 ⁶⁹ } $\pm$ Felspar

50.19

Cross Sec. Jefferson
Trias to Twiggs.

Trias to Twiggs.

10/5/53
W.O. 32209

C.H.S.
Begg
oltman
Schelling

Ref

FB. 1580 - 54 ✓

1787 - 49 -

2000 - 47

2068 - 19 + 25

2074 - 9

T.P. Sheets { 528
529
530

Sheet 4077-B.

* denotes Fd. Cross. in M.H. Rim.
• denotes Fd. L+T - or disk

- denotes Fd. C+T - or disk

1. Set. Conc. Mail (P.K.)

cut cross in M.H. film

T.W. denotes top of wall

B.W.	"	base	"	"
------	---	------	---	---

✱ denotes soil sample taken

R.P. Cross on
Walk.
Not on 4th Line
6-17-55 *alt*
INDEXED
James
OCT 22 1953

Ampudia

St.

 $2+99.93$

#1  $15' \leftarrow$

36' wide gutter

Wido gutter
Taffers 017

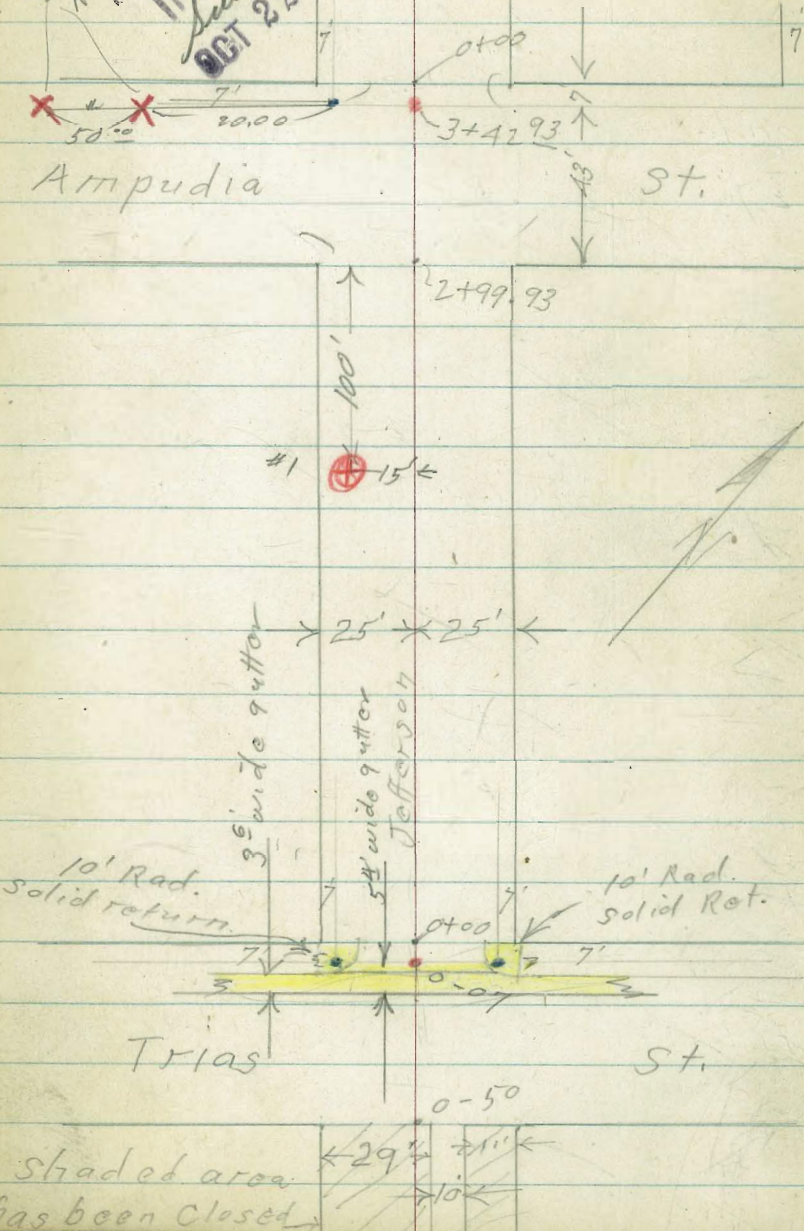
10' Rad.
Solid return.

10' Rad.
Solid Rot.

Trias

S. 7.

Shaded area
has been closed



why rip pipe
to disk
Moore +
Conde

INDEXED
M ER
DEC 23 1953

23

Conde

St. - 50' Street

Twigg

St.

2+99.73

Street
Closed

10' line
produced
from east

2+25.28 End of street

Jefferson

School

Jefferson

20' of
Rad

Paved.

Arista

12^E St. 50' street

Harney

St.

3700¹⁵

0+00
3+49.60

3+06.60

2+99.60

18x18+

20' of
Rad

25' 25'

43'
7'

7'

18[±] RT
18[±] LT = Face of cl. Ret.

0-08[±] = end Conc. gutter
= start 1" to 2" thick rock
& oil pave.

^{43.65} 8.34 18 [±] cl	^{43.71} 8.80 18 [±] G	^{43.91} 8.10	^{44.75} 7.26 18 [±] G	^{45.58} 6.43 18 [±] cl
---	--	--------------------------	--	---

^{40.55} 11.46 75 cl	^{39.74} 12.27 75 G	^{48.07} 3.94 68 G	^{48.76} 3.25 68 cl
---------------------------------------	--------------------------------------	-------------------------------------	--------------------------------------

25' RT } = B.C 10' Rad. cl. Ret.
25' LT }

0-10 = N.W. ly cl. Trias

^{43.51} 8.50 25 cl	^{42.74} 9.27 25 G	^{43.01} 8.90 15 conc. gutter	^{43.15} 8.26	^{44.40} 7.61 15 G	^{44.80} 7.21 25 G	^{45.59} 6.42 25 cl
--------------------------------------	-------------------------------------	--	--------------------------	-------------------------------------	-------------------------------------	--------------------------------------

0-13[±] = start Conc. gutter

^{39.94} 12.07 75	^{42.95} 9.06 25	^{43.30} 8.71 15	^{43.82} 8.19	^{44.55} 7.46 15	^{45.10} 6.91 25	^{45.83} 3.18 75
---------------------------------	--------------------------------	--------------------------------	--------------------------	--------------------------------	--------------------------------	--------------------------------

1" to 2" thick rock & oil pave - No grad.

0-25 = Trias st.

^{41.2} 11.8 75	^{48.3} 3.7 25	^{44.9} 7.1 52.01	^{45.7} 6.3 25	^{49.1} 2.9 75
-------------------------------	------------------------------	---------------------------------	------------------------------	------------------------------

2.97 52.01 3.60 49.04

8.89 52.64 43.75

S.E.B.P. Ampudia & La Jolla Blvd.

£ Nail - 1 + 00

Jefferson St.

T.P. #1 5.03 46.41 6.67 41.38

0+37 25⁹ Lt. = end motel cabin

0+30

47.65
5.4
25.9

46.55
1.5
25
46.75
1.3
30

43.45	43.75	44.05	44.35	44.65	44.95	45.25	45.55	45.85
4.6	4.8	5.2	4.7	4.2	4.3	4.0	3.3	2.8
25	212	215	18		7	8	10	16
	on walk	E.P.			E.P.			

48.05

T.P. 3.66 48.05 7.62 4.4.39 £ Nail 0+00

0+10 20⁹ Lt. = line of walk

E.P. = edge of pave.

43.81	43.91	43.61	44.31	44.41	45.41	45.91	47.41
8.2	8.3	8.4	7.7	7.6	6.6	6.1	4.6
25	21	209		9	12	18	25
	walk	E.P.		E.P.			

0+06 25⁸ Lt. = start + cabin Motel office

0+02 23⁸ Lt. = start post + wire fence.

43.81
8.2
25⁸
end.

conc. walk. - No good.

22³ Lt. = start 2⁵ wide rough

22³ Lt. = edge rock + oil

0+00 = Newly line Trias

43.66	43.65	43.81	44.41	44.81	45.61	45.76
8.35	8.36	6.2	7.6	7.2	6.20	6.35
25	15	15		12	15	25
walk	cc	pave		E.P.	cl.	walk
+ end.					+ end.	end.

52.01

Jefferson

T.P. 4.19 41.55 9.05 37.36

1+50 25' Lt. = line of fence

1+49 24' Rt. = end post & wire fence + start picket fence

1+45 17' Lt. = 10" pole # 2321.

1+30

1+29 17' Lt. = dead man

1+24 16' Rt. = 10" pole # 414262H

1+02 - 15' Rt. = dead man

(conc.) burner.

1+00 22' Lt. = Ctr. 4' x 4' trash

{ 26' Lt. = start board fence

0+90 { 25' Lt. = 12" pepper tree.

23' Lt. = end walk.

0+63 - 26' Lt. = end Bldg.

0+53 - 17' Lt. = w.

0+50 26' Lt. = start stucco Bldg.

0+46 - 25' Lt. = 8' wide conc. car. port

26

39.7' 38.9' 38.4' 38.8' 38.6' 39.7' 41.3'
7.2 7.5 8.0 7.6 7.8 6.7 5.1
25 16 11 11 17 25
E.P. E.P.

40.0' 39.8' 39.7' 39.7' 39.6' 41.6' 43.4' 49.7'
6.4 6.6 7.2 6.7 6.8 4.8 3.0 2.7
25 17 13 10 15 25 30
E.P. E.P.

39.8' 41.0' 40.7' 41.3' 41.9' 41.9' 43.1' 44.4'
6.6 5.4 5.7 5.1 4.5 4.5 3.3 2.0
50 25 20 16 7 12 25
E.P. E.P.

47.1' 47.1' 47.7' 47.5' 47.6' 47.9' 44.1' 45.3' 45.6'
4.3 4.3 4.7 3.9 3.4 3.5 2.3 1.1 0.8
25 23.5 23.5 12 C 12 24 25
walk E.P. E.P.

47.1' 47.5'
4.0 3.9
30 25

46, 41

2+75 - 16' R+ = 10" pole # 537245 H

2+60

2+55 17' Lt = ~~10~~ 14" pole # P2339

2+44 25' Lt = start picket fence

2+38 17' Lt = ϕ 2' diam pepper tree

2+35 24' R+ = start picket fence

2+30

2

2+17 25' Lt = ϕ 3' wide Conc. walk

2+11 50' R+ = ϕ sing. Gar. dirt floor

2+01

2+00 25' R+2
25' Lt = end fence

35.95	35.85	35.75	35.65	35.65	35.75
5.6	5.7	6.2	5.9	5.9	4.8
25	13	10		10	25
		E.P.		E.P.	

37.05	36.85	36.15	36.55	36.45	37.65	37.65
4.5	4.7	5.4	5.0	5.1	3.9	3.9
25	13	10		10	25	30
		E.P.		E.P.		

37.35	37.55
4.20	4.00
35	25
walk	

38.05
3.5
50 floor

37.75	37.15	37.05	37.35	37.35	38.15
4.3	4.4	4.5	4.2	4.2	3.4
25	18	9		11	25
		E.P.		E.P.	

38.75	38.05	37.05	37.35	37.35	38.75
3.3	3.5	4.5	4.2	4.2	3.3
25	18	9	41.55	11	25
		E.P.		E.P.	

Jefferson

3+24⁹³ = $\pm$ Ampudia

3+10⁹³ = S.Ely. ab time Ampudia
 = $\left. \begin{array}{l} 25' \text{ RT} \\ 25' \text{ LT} \end{array} \right\} = \text{E.C. } 10' \text{ Rad. ab. Ret}$

2+99⁹³ = $\left\{ \begin{array}{l} 25' \text{ RT} = \text{end fences.} \\ 25' \text{ LT} = \text{Cor. of Ret.} \\ 15' \text{ LT} = \text{B.C. } 10' \text{ Rad. ab. Ret.} \\ 148' \text{ RT} = \text{B.C. } 10' \text{ Rad. ab. Ret} \end{array} \right.$
 = Start A.C. Pave
 = S.Ely. Ampudia

2+98 = End rock + oil pave.

28

^{37.95} 8.60 75	^{37.75} 7.80 25	^{34.05} 7.50	^{34.35} 7.20 25	^{35.65} 5.90 75
--------------------------------	--------------------------------	--------------------------	--------------------------------	--------------------------------

^{33.60} 7.95 75 cl.	^{33.07} 8.53 75 G	^{36.29} 5.26 75 cl.
---------------------------------------	-------------------------------------	---------------------------------------

^{34.55} 7.00 25 cl.	^{33.90} 7.65 25 G	^{33.95} 7.60 15	^{34.11} 7.44	^{34.74} 7.26 15	^{34.57} 7.03 25 G	^{34.95} 6.60 25 cl.	^{35.84} 5.71 75 G
---------------------------------------	-------------------------------------	--------------------------------	--------------------------	--------------------------------	-------------------------------------	---------------------------------------	-------------------------------------

^{34.81} 6.74 25 walk + Gnd.	^{34.50} 7.05 15 cl	^{34.16} 7.39 15 G	^{34.56} 6.99	^{34.67} 6.93 148 G	^{35.01} 6.54 148 cl	^{35.71} 6.28 25 walk + Gnd.
--	--------------------------------------	-------------------------------------	--------------------------	--------------------------------------	---------------------------------------	--

^{35.55} 6.0 25	^{34.75} 6.8 15	^{34.35} 7.2 9 E.P.	^{34.75} 6.8	^{34.75} 6.8 11 E.P.	^{35.55} 6.0 25
-------------------------------	-------------------------------	--------------------------------------	-------------------------	---------------------------------------	-------------------------------

41.55

wly. 7'4" + t.

T.P. 1.09 34.64 8.00 33.55

0 to 4 16' RT. = 12" pole # A14261H

0 to 2 21' RT. = 4' diam Eucalyptus
(Should come out.)

0 to 1

be rebuilt.

pushed up by tree. Should

Return on right has been

25' Lt. = start Conc. wall

25' Lt.

24' RT. } = corner return

14' RT.

15' Lt.

B.C. 10' Rad, Solid Return.

3 + 49.93 = N. wly line Ampudia

25' RT.

25' Lt.

B.C. 10' Rad cl. Ret.

3 + 40 = N. wly cl. Ampudia

33.65	33.75	33.05	33.35	33.15	34.15	34.45
7.9	7.8	8.5	8.2	8.4	7.4	7.1
25	18	13		10	18	25

35.75	34.95	33.65	34.45
5.8	8.6	7.9	7.1
25	25	25	25
T.W.	B.W.	Grd.	Grd.

33.64	33.47	33.07	33.78	33.40	34.15	34.59
7.91	8.13	8.48	8.27	8.15	7.40	6.96
25	15	15		14.8	14.8	24.8
walk	cl	G		G	cl	walk

37.85	37.75	34.75	35.31
8.70	9.30	6.80	6.24
75	75	75	75
cl	G	G	cl

33.60	33.03	33.73	33.33	33.45	33.53	34.08
8.05	8.52	8.32	8.22	8.10	8.02	7.47
25	25	15		15	25	25
cl	G			G	G	cl

41.55

Jefferson

should come out

1+19 208 Rt. = 30" diam Eucalyptus
18' Lt. = deadman
1+13 18 Lt. = deadman
1+06 25 Lt. = Level 8' wide Conc. drive

0+88 Lt. = end Conc. wall

0+75

0+56 25 Lt. = 8' wide Conc. drive thru wall.

0+50

0+25

0+22 16' Rt. = deadman

29.04
5.60
41
Bar. floor
29.04
5.80
25
drive

28.34 29.24 29.44 29.14 28.94 29.64 31.64 33.34
6.3 5.4 5.2 5.5 5.7 5.0 3.0 1.3
25 25 14 8 20 25 30
B.W.

30.24 30.84 30.44 30.04 30.04 30.64 32.14 33.64
4.4 3.8 4.2 4.6 4.6 4.0 2.5 1.0
25 25 14 6 16 25 35
B.W.

32.04 31.83
2.60 2.81
51 25
Bar. floor drive

31.34 31.84 32.34 31.94 31.54 31.44 32.34 32.74 34.24
3.3 2.8 2.3 2.7 3.1 3.2 2.3 1.4 0.4
25 25 16 14 7 19 25 30
B.W.

32.64 33.14 32.24 32.74 32.64 32.34 34.04 34.64
2.0 1.5 1.4 1.9 2.0 2.3 0.6 0.0
25 25 16 13 7 25 30
B.W.

34.64

Jefferson

Iron pin in wall
25' Lt of 2+00

T.R. 4.46 28.45 10.65 23.99
2+00 Lt = 6" wide Conc. wall

1+81 25' Lt = 2' wide Conc. walk

drain - from school

1+75 22' Rt = 4" Cast Iron pipe

1+60 82' Lt = double Car. Conc. floor

1+55

should come out.
21' Rt = 3' diam Eucalyptus.

1+49 173' Lt = 12" pole # P 2309

1+34 18' Lt = (W)

1+30

21.64 23.84 25.64 24.44 24.70 25.34 31.44 31.64
13.0 10.8 11.0 10.2 10.4 9.3 3.2 3.0
40 40 25 15 25 37 50
Grid to Grid. Grid. Grid.
North To + T.W.
of South
wall of wall

24.09 24.16
10.55 10.48
35 25

26.04 27.12 29.34
8.60 7.52 5.30
22 25 32
I.E. Top of pipe

22.64
12.0
82
Floor

23.34 25.14 25.94 25.64 26.44 28.44 30.14 32.14
11.3 9.5 8.7 9.0 8.2 6.2 2.5 2.5
40 25 18 22 25 35 45

28.64 28.54 27.94 26.94 26.64 26.44 29.44 37.84 37.94
6.0 6.1 6.7 7.7 8.0 8.2 5.2 1.8 1.7
35 27 25 20 16 25 32 40

34.64

2+59 18' Lt. = (W)

2+52 } 27' Lt. = start conc. wall.

2+51 } 27' Lt. = start conc. block wall

27' Lt. = Ctr. Barbague &

2+50 - 25' Lt. = start board fence.

2+35 - 23' Lt. = 4' wide Conc. Walk.

2+28 26' Lt. = Bldg. - (School grounds)
sly. cor. frame

2+25 - 17' Lt. = (W)

2+17

19.35 19.35
9.1 9.1
40 30
on paved patio

21.5 21.75 21.45 21.05 21.35 21.45 21.45 30.85
6.9 6.7 5.10 5.4 5.1 4.10 +1.0 +2.4
27 25 18 11 11 25 27
T.W. at Bldg.

21.75 21.65 21.45 21.55 21.45 30.85
6.2 4.8 5.0 3.9 +1.0 +2.4
25 18 11 25 27

21.75 21.60 21.10
6.10 5.85 5.75
32 25 23.8
on walk

21.95 21.75 21.65 21.35 21.85 21.45
5.5 4.7 4.8 4.1 +0.4 +2.0
25 19 11 25 26.2
at Bldg.

21.75 21.05 21.45 21.45 21.75 31.45
5.2 4.4 4.6 4.0 2.7 +3.0
25 18 15 25 34
28.45

Jefferson

33

Abso-25' Lt = start A.C. Pavc.

curb (S.W.ly + N.E.ly)

3+07.5 25' Lt = existing Typo G.

25' Lt = end board fence.

3+00.15 182 Lt = 12" pole # 2399
= S.W.ly line Ariste.

link fence

2+97 25' Rt = start 8" high chain

2+80

2+72 27' Lt = end wall

2+64-26.5 Rx = end Bldg.

10.65
9.80 7.26
25 25
C. 06

19.75 27.25 27.65 27.95 27.65 27.55 26.65
8.7 6.2 6.8 6.5 5.8 6.9 1.8
25 17 12 18 25 35

20.35 27.95 27.95 27.25 27.45 27.95 27.45 27.45 27.25 27.45
8.1 5.5 5.5 6.2 6.0 5.5 5.0 5.0 5.6 5.6
25 21 13 12 9 10 16 23 25

19.75 27.105
9.2 7.4
28 27
Patio T.W.

20.75 27.75 27.45 27.75 27.85 27.45 27.45 29.05
7.7 5.7 5.0 5.7 5.6 5.0 4.0 10.6
25 20 16 12 8 13 25

28.45

Jefferson

T.P. 5.82 24.09 10.18 18.27

3+40¹⁵ = N.W. q. Arista

16.40
12.25 15.70
75 85 75 85
K cc. G
17.44 17.47 18.40 20.15 20.25 21.25 22.35 24.55 25.25
10.51 10.98 10.25 8.3 7.7 7.2 6.1 8.9 6.2
25 25 25 13 10 23 25 30
Q.B.C. G pave

See plans for I.E. Elev.

3+39⁵ 14⁵ Lt. = Ctr. storm drain

20.10
8.35
14.5
Rim

steps to school yard

3+30 - 25' Rt. = 4' wide conc.

3+25¹⁵ = 4' Arista

18.07 18.72 19.05 20.75 21.35
10.43 9.73 9.4 7.7 7.1 6.9 5.6 8.0 5.0
35 25 21 9 11 18 25 33
pave.
21.55 22.05 20.42 23.40
8.10 5.02
25 33+
lower stop top stop

12.14 12.57 9.99
85 85 35
Q.C. G Q.E.C.

3+10¹⁵

18.01 18.83 19.15 21.15 21.65 22.45 20.85 25.05
10.44 9.62 9.3 7.3 6.8 6.0 7.6 3.4
35 35 25 21 11 17 25 35
Q.C. G pave.

28.45

Jefferson

35

0+55- 24¹ Lt. = start picket fence.
25¹ Lt. = end hedge

9.7
27⁵
ditch
15.49
8.6 8.8 9.1 8.8 6.1 9.0 9.1
25 17 10 23 24 25

0+28- 24⁵ Lt. = 3' wide Conc. walk

16.55
7.54 6.85 6.82
34⁵ 25 24⁵

0+20 27⁵ Rt. = start 5' wide cold
lay ditch.

17.79 18.29 18.59 18.79 19.59 21.79 17.89 17.29
6.3 5.8 5.5 5.3 4.5 2.3 6.2 6.8
35 25 19 9 21 25 27⁵
ditch

0+13- 18' Lt. = (W).

0+05- 23⁸ Rt. = ctr. Fire Hydr.

0+00 25' Lt. = start 5' High hedge.

3+50¹⁵ = N. Wly. line Arista

18.29 19.59 20.19 20.79 22.99 21.79 19.69
5.8 4.5 3.9 3.3 1.1 2.3 4.4
25 17 11 20 23 25

curb.

3+42⁶ 25' Lt. = existing type G

18.27 17.81
5.82 6.28
25 25
ch a

24.09

Jefferson

previous notes

1+91 - 15' Lt. = $\pm$ cl. inlet. - (See

previous notes on drain)

1+81 25' Lt. = $\pm$ drain - (see

1+65 20' Lt. = (W)

1+50 25' Lt. = end fence

up base.

I would take all day to dig
board plans for base.

This wall is deep - check school
Ret. wall

1+09 25' Rt. = start 6" wide conc.

1+01 16' Lt. = 15" pole # 2417

T.P. 2.21 15.25 11.05 13.04

0+80

$\pm$

36

7.5	7.17	7.98	7.1	6.1	3.8	3.49
25	15	15	12	25	25	T.W.
	cc	cc				

6.13	6.9	7.13	6.7	3.7	3.38	4.2
25	16	15	25	25	25	275
					T.W.	$\pm$ ditch

5.13	5.4	5.9	5.4	4.7	2.6	3.40	4.0
25	14	13	10	23	25	275	$\pm$ ditch

15.25

12.79
11.3
275
 $\pm$ ditch

10.9	11.6	11.8	11.6	9.5	10.6
25	15	11	24	25	

24.09

Jefferson

37

Top end of wall 25' Rt. of Sta. 2+50

T.P. 6.03 18.47 2.81 12.44

2+60 27⁵ ditch
Rt. = Δ to North in.

8.85 9.75 8.75 9.05 9.95 11.05 11.05
6.4 6.0 6.5 6.2 5.3 3.4 4.2
25 20 17 15 25 275
ditch

2+56 - 25' Rt. = end of wall.

17.44
2.81
25
T.W.

2+53⁵ = 4' gate thru fence.

2+51 25' Rt. = step up in wall

11.85 17.44
3.40 2.82
25 25
T.W. TO T.W. TO
to S.E. N.W.

2+35 25⁵ Lt. = end wall
25' Lt. = start picket fence.

2+30 - 17' Rt. = 12" pole # 505505 H

2+13 17' Rt. = deadman

8.05 8.45 7.95 8.75 8.85 11.05 11.85 10.95
7.2 6.8 7.3 7.0 6.4 4.2 3.40 4.3
25 25 15 11 25 25 275
B.W. T.W. ditch

2+05 25⁵ Lt. = start 6" wide 2⁵ high
Conc. wall.

7.7 6.7 6.9 7.8 7.3 6.1 4.3 3.40 4.4
25 25 16 13 12 25 25 275
B.W. T.W. ditch

2+01 - 16" Lt. = 16" pole # 2433

15, 25

Jefferson

38

3+41

8.1 7.3 6.5 6.3 6.8
25 12 15 25

T.P. 7.81 25.04 1.24 17.23

25.04

3+24⁷³ - $\frac{1}{2}$ Conde.

3.0 1.8 2.0
25 25

3+05

5.0 4.5 3.8
25 25

2+99⁷³ = 25' Lt. = end fence.
S. Fly line Conde

5.1 5.2 4.2 2.0
25 20 25

2+85

7.4 7.0 7.6 7.2 6.6 5.8 3.0 6.0
25 19 17 13 19 25 50

2+67 { 25' Lt. = $\frac{1}{2}$ 3' wide conc. walk
conc. to come out.
22' Lt. = Ctr. 24 sq. ft. 2"

9.87 9.47
35 25

2+65 - 25' Lt. = end fence.

18.47

Jefferson

39

0+20

0+19 14' Lt. = (W)

0+18 14' Lt. = (W)

0+14 13' Lt. = (W)

0+13 13' Lt. = (W)

0+12 - 13' Lt. = (W)

0+01 17' Lt. = 14" Pole # P2451

Disk 18' Rt. of 0+03

T.P. ✓ 8.77 28.78 5.03 20.01

25' Lt. = start conc. wall.

26' Rt. = start 4' high hedge

22' ^{10'} back of walk.

17' Rt. = start conc. walk

15' Rt. = start curb

= 0+00.

23+49 ⁷³ = N. W. ly. line Condo

Note See Pg 78 For ADD. Levels this area (Chas)

3+43

71.38	71.58	71.08	71.48	71.38	71.32
7.4	7.3	7.7	7.4	7.5	7.46
25	18	12		15	15
				66	

28.78

18.84	19.91	19.64
6.2	5.13	5.4
25	22E	25
B.W.	walk	

18.84	18.84	18.44	19.54	19.64	19.76	19.74
6.2	6.2	6.6	5.5	5.4	5.28	5.3
25	16	10		15	15	22E
				Grd	66	Grd

18.34	17.94	18.74	18.74	18.64
6.7	7.1	6.3	6.3	6.4
25	15		15	25

25.04

Jefferson

40

4

26³ Lt = start wire fence.

0+66 26³ Lt = end Conc. drive

27.98
51.80
26³
drive

0+52 26³ Lt = start Conc. drive

27.74
5.50 6.04
73 26³
Gar. floor drive

0+51 16⁵ Rt = 10" pole # JP 2458

0+50

27.78
6.0 5.13 5.16 5.79
25 15 15 06

25 Rt = end hedge.

0+47 - 27³ Lt = 3' wide Conc. step.

0+45 26¹ Lt = end flower planter

0+40

4.80 5.38
29.4 27.2
on porch stop
27.78 27.58 27.98 27.48 27.53
6.0 6.2 5.8 6.3 6.25
25 16 15 15 06

wall (flower planter)

0+30 26⁴ Lt = start 1' high Conc.

0+27 - 25² Lt = end wall.

0+23 - 15' Lt = (W)

0+22 15' Lt = (W)

0+21 16' Lt = (W)

27.58 27.68
7.2 7.1
25 25
B.W.

28.78

Jefferson
 25^E Lt. = line of fence
 17^E Lt. = pole # 2479 12"
 18^E Lt. = start Conc. walk
 2+00 15' Lt. = start Conc. cl

1+78-16' Rt. = (W)
 { = start wire fence
 1+50 25² Lt. = end picket fence

1+45 25⁸ Lt. = 7' wide Conc. drive.

1+22 18' Lt. = (W)

0+18- 16^E Rt. = (W)

T.P. 6.00 30.51 4.27 24.51

1+00 { 25⁸ Lt. = start picket fence
 26⁴ Lt. = end hedge
 17' Lt. = 12" pole # 2465

0+88- 16^E Rt. = (W)

0+87^E 1

0+70

0+69 { 26⁷ Lt. = start 5' high hedge.
 26³ Lt. = end fence

25.41
 51
 25
 25.39 25.30 25.73 24.91 25.71 25.31 25.81
 5.12 5.21 5.28 5.6 4.8 5.2 4.70
 23^E 18^E 15 15 15 15
 Back walk cl
 of walk + end.

24.61 24.41 25.11 24.71 25.36
 5.9 6.1 5.4 5.8 5.15
 25 14 15 15
 cl

24.41 24.57
 6.10 5.94
 50 25.8
 on car drive
 port.

30.51

23.88 23.88 24.38 24.78 24.68
 4.9 4.9 4.4 4.6 4.10
 25 15 15 15
 cl

23.68 23.48 23.88 23.68 23.87
 5.1 5.3 4.9 5.1 4.96
 25 15 14.9 14.9
 cl

28.78

Jefferson

T.B.M. 342 28.97 4.96 25.55

242' Rt. = start wire fence.
 = 0+00 25' Ltr start wire fence
 3+49⁶⁰ = Nly. line Harney

3+24⁵ = $\perp$ Harney

25' Lt. } Rot.
 25' Rt. } = E.C. 10' Rad. cl.
 3+09⁵ = sly. cl. line Harney

15' Rt. } cl. Rot.
 15' Lt. } = B.C. 10' Rad.
 2+99⁶⁰ = sly line Harney

2+98⁵ 18' Lt. = 12" pole # 24992+64 17⁵ Lt. = (W)

2+50

2+18 16⁵ Rt. = 10" pole # 574099H2+04 16⁵ Lt. = (W)

Jefferson & Harney

on Ely. 7' Lt. = 18' Rt. + Sta 3+06⁶⁰

25.01
 5.5 5.6 5.5
 25 25

24.91 25.31 25.51
 5.6 5.2 5.0
 25 25

25.14 24.71 24.91 25.11 25.71 25.31 25.61
 5.37 5.8 5.6 5.4 5.3 5.2 4.90
 25 25 15 15 25 25
 cl. E.C. cl. E.C.

25.36 26.36
 4.15 5.6 5.0 5.0 4.98
 15 15 15 15
 cl. cl. B.C.

25.31 25.21 25.71 25.51 25.81
 5.14 5.3 4.8 5.0 4.64
 15 15 15 15
 cl. cl.

30.51

Jefferson

4

4.3

1+60 16' Rt = dead man

on top of wall
wall - 2⁵ picket fence.
26¹ Lt = start 15' high conc.
26² Lt = end fence
wire fence on top of wall
24¹ Rt = 12" high wall 4' high
23² Rt = end Hedge
1+50 15⁵ Rt = 10" pole # J.P. 2550

23.36 23.66 23.66 23.66 24.06 24.16 24.46 24.16 24.66
5.3 5.0 5.0 5.0 4.6 4.5 4.2 4.5 4.0
26¹ 26 25 15 14 23 24² 24²
B.W. B.W. G.W.

28.66

T.P. 4.74 28.66 5.05 23.92

1+29 23⁵ Rt = start 3' high hedge

1+28 17' Lt = dead man

1+25 22' Rt = 7' wide conc. drive

1+21 23⁸ Rt = end picket fence

1+20 19' Lt = (W)

23⁵ Rt = start picket fence
26¹ Lt = end wire fence
1+00 26¹ Lt = start Lath fence

0+98 17' Lt = 12" pole # 2549
0+79 25² Rt = 5' wide wood steps to House
0+54 26¹ Lt = end fence

0+50

0+30 16' Rt = 9" pole # 464163H

23.87 24.17 24.27 24.57 24.77
5.1 4.8 4.7 4.4 4.2
25 13 15 25
24.37 24.17 24.47 24.77 24.67
4.6 4.8 4.5 4.2 4.3
25 15 16 25

28.97

Jefferson

44

2+05 17' Lt. = 14" pole # 2577

fence continues
26' Lt. = start conc. wall

2+00 25' Rt. = end fence

24.56 23.76 23.76 23.66 23.96 24.26
4.1 5.4 4.9 5.0 4.7 4.4
26 26 25 15 25
T.W. B.W.

1+92 23⁵ Rt. = 8' wide conc. drive

24.38 24.42 24.70
4.28 4.24 3.96
23.5 25 40
drive car floor

fence continues
1+91 26' Lt. = end wall

23.76 23.66
5.4 5.0
26 26
B.W.

fence continues
1+88 24² Rt. = end conc. wall

24.16 24.06
3.9 4.6
24 24
B.W.

thru wall.
1+81 25⁸ Lt. = 3' conc. walk

23.54 23.76
5.14 4.90
35.8 25.8
walk

1+69 17' Rt. = (V)

1+64 23² Rt. = 3' walk

{ 19' Rt. = ctr. 15 sq. ft. 4" }
conc. to come out.

24.70 24.76
3.96 3.90
23.2 25
on walk

28.66

Jefferson

3.11 25.55

see closing sheet

3+00²⁸ = sly line Twiggs produced

2+

18' Lt. = 8" diam. olive tree

2+30

18' Rt. = 4' diam palm "

2+25²⁸ = end of street

both wall 25'± high

sets on ground - No good.

0.7' wide conc. wall

16' Lt. Ely end 10' long

ground. - No good. 10' long,

wall. sets on top of

2+24⁵² cross 0.7' wide conc. block

2+24 26² Lt. = end wall & fence.

2+22 18⁵ Lt. = dead mag

= T.B.M. - P. 42 EL. = 2555

2206
6.6
25

2286
5.8

2226
5.4
25

2216
5.5
25

2236
5.3
15

2266
5.0

2406
4.6
25

INDEXED
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2246
4.2

2276
5.9

2306
5.6

26²
T.W.

26²
O.W.

26²

28.66

Harney St.
Moore to Congress W.O. 32209

10-19-53

C.H.S.
Bagg
oltman
schrelin

For Ref. See page 22

Congress St.

See page 22 left

0-76.7 = wly. rail.

0-74.21 = $\frac{1}{2}$ AT+SF. Rt. of way $\left\{ \begin{array}{l} \text{FB 1422} \\ 75 \end{array} \right.$

0-71.7 = 3rd rail

0-61.8 = 2nd rail

0-56.8 = Ely. rail

Double track

Jefferson

FORM 291

SUBJECT



INDEXED
OCT 20

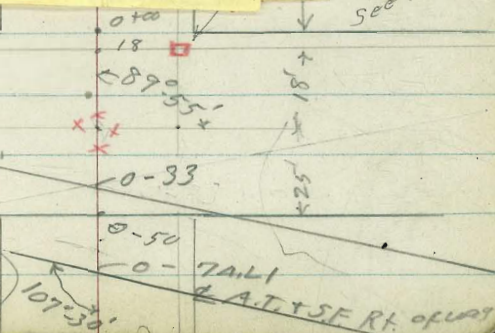
ON
SAN

Remains of
old R.W. Hub.
Reset.
See Note "A"

Note "A" Lines produced from East +
From South. Miss Ctr. of old Hub by
o.l.t. Used intersection of produced
lines to set disk in new Hub.
+ crosses on M.H. rim.

Moore St.

$\frac{1}{2}$ Storm drain
See Const. plans.



Amputia 7/4/73

ESTIMATING SHEETS
CITY OF SAN DIEGO

SUBJECT

FORM 331

DATE
BY

NO.

13

ARISTA

1400 RE

Condor

7x7' Pipe + Disk

50 50

Harney St.

Moore to Congress W.O. 32209

10-19-53

For Ref. See page 22

C.H.S.
Begg
oltman
schelin

See page 22 left

0-76.7 = wly. rail.

0-74.21 = $\frac{1}{2}$ AT+SF. Rt. of way. $\left\{ \begin{array}{l} \text{FB 1412} \\ 75' \end{array} \right.$

0-71.7 = 3rd rail

0-61.8 = 2nd rail

0-56.8 = Ely. rail

Double track

Note "A" Lines produced from East +
From South. Miss Ctr. of old hub by
o.i.t. Used intersection of produced
lines to set disk in new hub.
+ crosses on M.H. rim.

46

Congress St.

3+23.71
2+98.71

Aprox.
North.

25' 18' 7'

15' 3+47.03

Jefferson St.

2+97.03

INDEXED
OCT 22 1953

Fd remains of
old R.W. Hub.
Reset.
See note "A"

Moore St.

0-33

$\frac{1}{2}$ Storm drain
See Const. plans.

0-50

0-74.41

107.30' $\frac{1}{2}$ A.T.+S.F. Rt. of way

Harney

0+00 = W 1/4 Moore.

0-01 - 18' Rt. = 8" guy pole

0-07 - 18' Rt. = 1/2 Hub. 9.51 0.86

0-19 18' Rt. = deadman

0-25 = E Moore St.

0-26 = Ctr. sewer M.H.

0-56⁸ = Ely rail of A.T. + S.F. Ry.

0-74²¹ = E A.T. + S.F. Rt. of way.
 Δ 107° 30' turned to Rt.

T.B.M. #1 S.S. 7.52 2.85

T.P. 2.18 10.37 11.56 8.19

T.P. 0.90 19.75 9.28 18.85

2.58 28.13 — 25.55

1.67
8.7
25

1.87
8.5

1.97
8.4
25

1.37
9.0
25

1.97
8.4
Grd.

1.37
9.0
25

7.85
7.52
Rim

17.0
12.07
I.E

5.66
4.71
Top of rail

10.37

= Ely. Cross in M.H. Rim 0-24 ± Harney + Moore

10.37

Ely. 7' L + T. Harney + Jefferson (P-42)

Harnoy

O+80- 20' Lt. = 10" pole # P483C

(do not regard, it is no good)
rough' Conc. steps + walk

O+74- 24' Lt. = start 2' wide

O+70 17' Rx. = dead man

O+66 25' Rx. = dead man

Conduit rizer on pole.

O+61 45' Rx. = 14" pole # C2596

O+56 28' Rx. = 4' stub *Eucalyptus* tree trunk

O+50

T.P. 12.35 20.64 2.08 8.29

O+32

(Conduit rizer on pole.)

O+21 17' Rx. = 12" pole # 3801

O+17

7.94	8.14	12.84	13.54	14.24	15.34	15.14
12.7	12.5	7.8	7.1	6.4	5.3	5.5
45	35	30	25		25	40

6.84	7.14	9.64	10.44	10.94	10.24
13.8	13.5	11.0	10.2	9.7	10.2
40	25		15	25	50

20.64

4.17	3.87	5.57	5.47	6.77
6.2	6.5	4.8	4.9	3.6
25	15		13	25

3.07	7.57	7.47
7.3	7.8	7.9
25		25

19.37

Harney

49

18⁵ Lt. = dead man.

small trunks & small shoots.

← should come out.

1+49 21' Rt. = 18" stump. several

1' high conc. wall.

1+48 25⁵ Lt. = end hedge
{ = start 3' picket fence on

1+38 24⁷ Rt. = 11' wide A.C. drive

1+34

1+33 - 25² Lt. = 3' conc. walk.

{ 24⁸ Rt. = start picket fence

1+25 { 17' Rt. = 12" pole #3823 } on pole

1+20 - 25⁶ Lt. = start 4' high hedge
30' high bamboo.

1+14 27' Lt. = ctr. 4' x 4' clump

T.P. 8.16 27.01 1.79 18.85

look & oil: to come out.

0+97 - start 30' wide 1" thick

0+89 22² Lt. = end walk

7/31
5.70 5.60
352 252
on walk

20.81 20.61
6.2 6.4
25 15

22.01 21.91 21.5 21.5 21.61
5.0 5.1 4.5 4.5 4.4
15 24 25.50
drive

5.30
Rim

27.01

18.14 18.64 18.84 19.54
2.5 2.0 1.8 1.1
25 20 25

17.64 17.64 17.44
3.8 3.0 3.2
25 25
20.64

Harney

1+99 25³ Lt. = £ 4' wide conc. walk.

2336
3.65 3.78 3.9
353 253 25
on walk

1+95 { 24⁵ Rt. = end fence.
15 Rt. = start conc. ch.

+82 18' Lt. = (W)

1+81 25⁴ Lt. = start wire fence.

+72 19' Lt. = (W)

+71 25¹ Lt. = end wall

+71 19' Lt. = (W)

1+70 19' Lt. = (W)

1+68 22' Rt. = (W)

1+65 19' Lt. = 12" pole # 488074 H.

1+59 23⁸ Lt. = £ 3' wide Conc. walk

3.75 3.89 3.97
35 25 238

1+50

2301 2301 2341 2381 2341 2311 2351 2351
410 410 416 5.2 4.6 4.9 4.5 4.5
35 255 25 15 14 15 25
T.W.

27.01

Harney

4146 30101 25155

see page 42 for intersection

Harney + Jefferson
Ely. 7' L+T.

4146 25154 (25155)

= wly line Jefferson

25154 = end fence.

2+97⁰³

10' RT = B.C. 10' Rad. cl. Ret.

2+93 18' Lt = 14" pole # P3898

2+76 25⁹ Lt = $\pm$ 3' wide Conc. Walk

2+70

T.P. 5.48 30.00 2.49 24.52

2+67 - 18 Lt = (W)

2+45

S.E. / L+T. Harney + Jefferson

24.60 24.60 25.00 24.70 25.13
51.4 51.6 51.0 51.3 41.87
25 15 15 15
cl

24.60 24.66
51.40 51.34
36 259

24.40 23.90 24.60 24.70 24.70
51.6 6.1 51.4 51.8 51.30
25 15 15 15
30.00
cl

23.91 23.51 24.71 23.81 24.39
3.1 3.5 2.8 3.12 2.62
25 15 15 15
cl

27.01

Harnoy

4

52

TIP 4.72 29.90 4.83 25.18

1+48 25' Lt = end fence.

1+26 { 16⁵ Rt. = (W)
25' Lt. = 3' wide Conc. walk

1+21 17' Lt. = (W)

1+00

0+85 17' Lt. = (W)

0+79 25' Lt. = 3' wide Conc. walk

0+75' 16⁵ Rt. = (W)

0+66- 17' Lt. = 14" pole # P3908

0+50

0+35 16⁵ Rt. = (W)

0+24 25' Lt. = 4' wide Conc. walk

25' Lt. = start wire fence.
to 20' wide at this point
Rock + oil strip cuts down

0+00 Ely line Jefferson

15' Rt. = E.C. 10' Rad. cc. Ret

25.36
4.65 4.70
352 252

26.01 25.41 25.11 25.51 25.41 25.81
4.0 4.6 4.9 4.5 4.6 4.20
30 25 12 15 15 cc.

25.71 25.63
4.30 4.38
352 252
on walk

25.21 25.11 25.51 25.31 25.81
4.8 4.9 4.5 4.7 4.12
25 12 15 15 cc.

25.61 25.49
4.14 4.52
355 255
on walk

25.01 25.51 25.21 25.61
5.0 4.5 4.8 4.40
25 15 15 cc.

34.01

Harney

2

53

8" pole

2+85- 17' Lt. = 4880 724

Palm.

2+77 16' Rt. = 18" diam 15' high

2+70 - 16' Rt. = dead man

2+62 16' Rt. = 4" diam olive tree

2+60 15' Rt. = (W) 20' rock + oil, also = end

2+50

2+45 10' Rt. = 3" diam olive tree

2+39 17' Rt. = dead man

2+17 16' Rt. = 12" pole # 3973

2+00

25' Rt. = start board fence.

16' Lt. = 10" pole # J.P. 3926

1+99 15' Rt. = end conc. curb

1+81 16' Rt. = (W)

1+79 17' Lt. = dead man

1+50

24.60 24.60 23.90 24.30 23.70 23.90 23.80
5.3 5.3 6.0 5.6 6.2 6.0 6.1
25 17 13 10 15 25

25.10 25.10 24.50 24.90 24.70 25.10 25.70
4.8 4.8 5.4 5.0 5.2 4.8 4.7
25 16 13 15 16 25

25.73 25.40
4.67 4.50
15 22.5
cc. back of walk

25.10 24.9 24.30 25.70 25.55
4.8 5.0 4.6 4.7 4.35
25 10 15 15 cc

29.90

INDEXED
Survey
OCT 22 1953

Harney St. (25.55)
+ Jefferson
Ely. 7' L.H. Harney 3.52 25.53

See Congress Imp. plans.

30' Rt. }
30' Lt. } = E.C. 15' Rad. cl. Ret.

3+05.7 } wly. cl. line Congress

T.P. 5.60 29.05 6.45 23.45

No sidewalks.

2+98.71 } 174 Rt = start Conc. cl.
172 Lt. = start Conc. cl.

2+96 = start A.C. Pav.

2+88 - 16" Rt = 10" diam pole. # P3949

23.36 23.88 23.11 23.17
5.69 6.17 7.34 6.88
75 75 75 75
cl. G. C. cl.
23.69 23.19 23.45 23.17 23.98 23.58 23.04
5.36 5.86 5.60 5.83 6.07 6.47 6.01
30 30 15 15 30 30
cl. G. 15 G. cl. E.C.

29.05

24.70
5.7
25

23.50
6.4
25

23.91 23.49 23.67 23.50 23.10 23.50
5.93 6.41 6.23 6.40 6.80 6.40
172 172 16 174 174
cl. G. G. cl.

24.70 24.30 23.50 23.44 23.20 23.50 23.50
5.7 5.6 6.40 6.46 6.7 6.4 6.4
25 18 15 16 18 25
E.P.

29.90

Comde St.

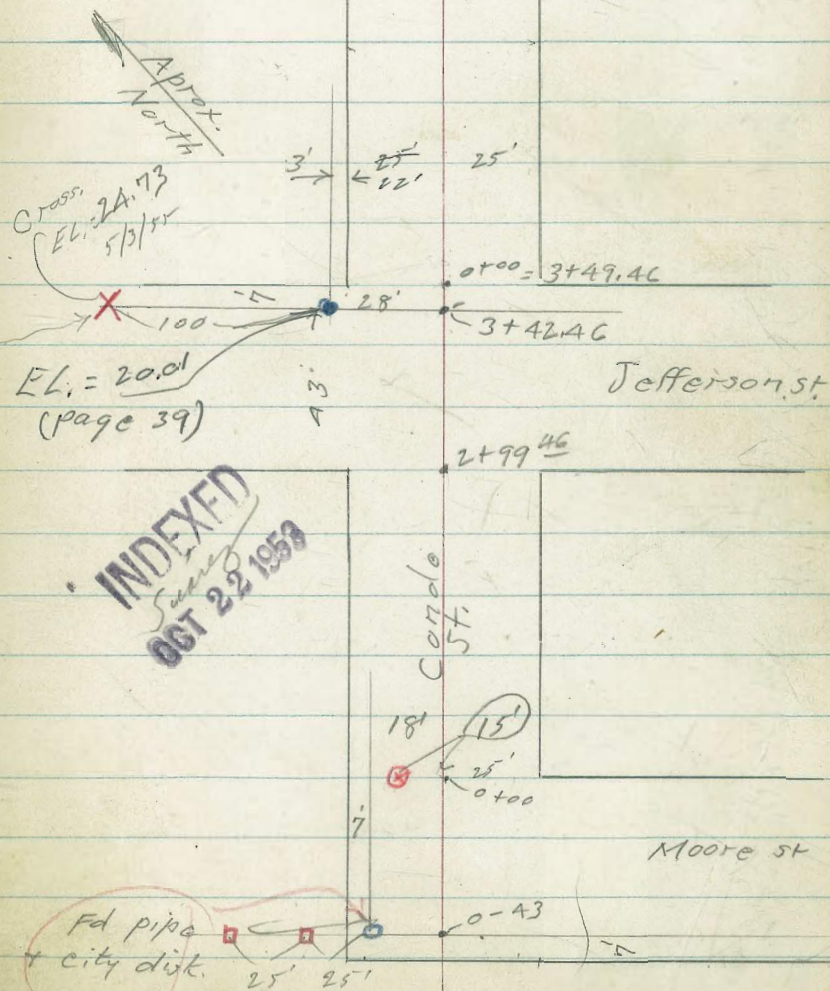
Moore to Congress

N.O. 32209
10-20-53

Ref. - See page 22

2+42	58' LT & GARAGE	" "	14.6
2+19	31' LT & HOUSE	" "	15.8
1+68	42' LT & HOUSE	" "	15.2
1+24	83' LT & HOUSE	" "	19.0
0+19	32' LT & HOUSE FLOOR LEVEL	EL. 22.9	

Nly. line Jefferson = 0+00



INDEXED
OCT 22 1953

Conde.

10/20/53

0+15- 25' Rt. = E.C. 4" wall

conc. Ret. wall

40' Rt. = B.C. 15' Rad. 4" wide

0+100 } Ely line Moore

0-05 25³ Lt. = start wire fence

0-25 = E Moore

0-26 2A' Lt. = 14" pole # 2550

0-45 2A' Lt. = deadman

0-48 = 2A⁵ Lt. = deadman

0-50 = Wly. line Moore

0-55- 2A' Lt. = deadman

T.P. 4.72 8.07 3.69 3.35

4.19 7.04 — 2.85

56

^{3.77}
4.9 5.4 4.3
25 25 25
B.W. T.W.

^{3.77}
4.8 5.5 4.4
40 40 40
B.W. T.W.

^{7.87} ^{7.87} ^{7.77} ^{7.87} ^{7.77} ^{3.77} ^{3.77}
5.2 5.2 5.8 5.2 5.3 4.8 4.9
25 23 21 13 16 25

^{7.77} ^{7.57} ^{7.97}
5.8 5.5 5.1
25 25

^{2.37} ^{2.77} ^{2.97}
5.7 5.9 5.2
25 25

8.07

Nail in Pole # 2550

T.B.M. #1 - PA7 - Ely X - M.H. Rim. Harney & Moore.

Conde

±

57

T.P. 10.73 18.57 0.23 7.84

0+38- 25' Rte = end wall
= start picket fence.

4.57 4.07 5.77
3.5 4.0 2.8
25 25L 25L
B.W. T.W.

1+20

6.77 6.07 4.77 3.97 3.77 3.37 4.07
1.3 1.2 3.3 4.1 4.5 4.7 4.0
30 25.5 25 15 9 25

1+00

plank bulkhead:

0+90 25' Lt. start 2' high

0+80 - 25' Lt. = Thru wall.
3' conc. walk

4.27
3.8
25
T.W.

5.87 5.77 3.47 3.77 2.97 3.47 3.17
2.2 2.3 4.6 4.9 5.1 4.6 4.9
30 25.5 25 10 25 25
Top of bulkhead B.W.

3.57 4.00 4.37
4.5 4.07 3.70
25 25L 35L

0+50

2.97 2.97 2.47 1.87 2.77 3.07 3.07
5.1 5.1 5.6 5.2 5.3 5.0 5.0
50 25 20 7 8 25

8.07

Thru wall

2+24- 25' Lt. = 3' wide steps

11.97	15.47
0.6	3.1
30	25
Top step.	Bottom step

2+14 24' RT = start picket fence

2+09 23' RT = 9' wide level.
conc. drive

11.25	11.23	11.7
238	25	60
drive		Car Floor

2+06 25' Lt. = start 5' high Conc. wall

1+96 25' RT = end fence.

1+85- 25' RT = start picket fence.

13.97	14.17	17.77	9.57	8.57	1.57	7.87	1.07
4.6	4.4	6.3	9.0	10.0	11.0	10.7	11.5
25	25	12	11		11	13	25
B.W.							

1+80- 17' RT = Level 9' wide
conc. drive

5.87	5.89	5.97
12.72	12.68	12.60
17.9	25	48
drive		Car Floor

1+70 25' RT = end fence

11.67	9.87	6.97	6.77	5.57	5.97
6.9	8.7	11.6	12.3	13.0	12.7
25	13	11		12	25

1+56 { 16' Lt. = 12" pole # P3786
 17' RT = 12" pole # Guy pole
 24' RT = dead man

1+50 25' Lt. = end fence

8.87	6.87	5.17	4.87	4.27	4.47	4.97
9.7	11.7	12.8	13.7	14.3	14.1	13.6
25	14	12		9	14	25

18.57

Conde

4

10.77

8.30

35

walk

59

T.P. 6.36 22.01 2.92 15.65

2+75 21⁵ RT. = 3' Conc. walk

pipe - to come out.

2+62 18⁸ RT. = end 12" conc.

2+53 21⁵ RT. = 9' wide Conc. drive.

(to come out.)
covered by 4" grout.

2+46- 19⁶ RT. = start 1' Conc. pipe

2+45

2+35- 25' Lt. = start 6' wall
end 5' wall

17.57

1.0

2.5

16.97

1.6

16

15.47

3.1

14

13.97

4.6

17.87

5.7

12

17.17

6.40

2.5

walk

11.67

6.90

2.5

walk

+ Grd.

10.57

8.00

2.5

drive

10.17

8.40

2.5

drive

8.07

10.50

4.7

Con

floor

8.07

10.5

30

16.47

2.1

2.5

15.47

3.1

14

12.37

5.2

10

17.17

6.4

11.07

7.5

12

10.97

7.6

16

9.17

9.4

2.5

8.77

10.3

2.6

15.57

3.0

2.5

B.W.

15.07

3.5

2.5

B.W.

15.57

3.0

2.5

to east to west

18.57

Conde

¢

60

plans for confirmation.

street - check school board

base looks ^{to be} below grade of

0+84 25' Lt. = start conc. wall

17.8'	30'	17.3'	13.1'	13.1'	13.1'
8.2	9.0	8.7	8.9	8.9	8.9
25	18		25	25	35
			T.W.		

0+55 Lt. = start Conc. track wall.

17.0'	16.9'	15.3'	16.5'	14.6'	14.1'	13.3'	14.7'	13.7'	13.7'
5.0	5.1	6.7	5.5	7.4	7.9	8.7	7.8	8.8	8.8
30	16	26	25	17		20	25	35	40
		T.W.	B.W.						

0+30 - 26' Lt. = end hedge

18.4'	18.3'	16.4'	15.2'	14.0'	15.5'	13.3'
3.6	3.7	5.6	6.6	8.0	6.5	8.7
30	25	13		19	25	35

25' Lt. = start Fence chain link

= 0+00 = Ely. line Jefferson

3+49.46 26' Lt. = start 4' high hedge

19.6'	18.6'	18.7'	16.5'	14.7'	16.5'
2.4	3.4	3.8	5.5	7.3	5.5
25	18	16		20	25

See page 38 for intersection

Lt. = end 6' Conc. wall.

2+99.46 = wly line Jefferson

18.8'	19.0'	18.4'	17.0'	15.8'	13.5'	13.4'
3.2	3.0	3.6	5.0	6.5	8.5	8.6
25	25	18	16		20	25
B.W.						

2+98 21' Lt. = (W)

22.01

Conide

±

61

1+55

13.81
8.2
25
T.W.

13.81
8.2
30

1+49- 26⁵ Lt. = end Hedge

13.61
8.4
25
T.W.

1+37

18' RK } = ± 16' ch. inlet
18' Lt }

13.51 13.41 17.11 17.11 13.01 13.01 17.61 16.61 17.31
8.5 8.6 9.9 9.9 9.0 9.0 9.4 10.40 9.7
25 20 19 20 13 11 18 25
+ 0.6
18
top. ch.
+ 9.1 d.

1+25- 25⁵ Lt. = ± 3' Conc. walk

13.81 13.81
8.20 8.20
35 25
walk

1+20

13.61 13.71 17.71 17.91 13.41 13.61
8.4 8.8 9.3 9.1 8.6 8.4
25 16 25 25 35
T.W.

1+13- 26' Lt. = start 2' high Hedge.

26⁵ Lt. = end wall

1+00 24⁵ Lt. = 10" pole # 500351H

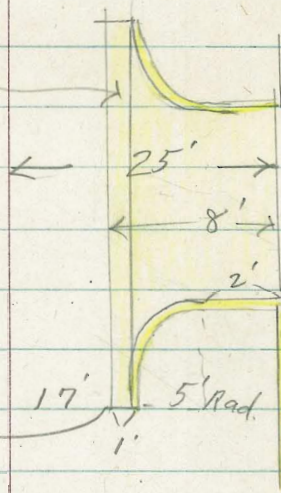
16.01 11.71 13.81
6.0 10.3 8.2
265 265 26
T.W. B.W.

22.01

Conde St.

62

12" wide
concr gutter



Sta. 2+29 →

ch. (see sketch)

18 Rt. = B.C. 6' wide conc.

2+29 { 24' Lt. end wall

18.85	14.05	14.55	14.35	14.01	13.77	14.15
3.3	8.1	7.6	7.8	8.14	8.43	8.0
24.9	24.9	24.9		18	18	25
T.W.	B.W.			9th	G	
				4th		

2+00 { 24' Lt. start Conc. wall.

18.55	14.15	14.15
3.6	8.0	8.0
24.5	25	35
T.W.	T.W.	

13.65	13.95	13.55	13.55	14.35	17.85
8.6	8.2	8.6	8.6	7.8	9.3
24.5	24.8	22.15	15	19	25
B.W.					

T.P. 8.52 22.15 8.38 13.63

1+58 - 17' Lt. = 12" pole # gone

22.01

22.01

Corrle

63

14.79	14.77	15.15	14.45
7.86	7.38	7.0	7.7
18	18	25	35
G	cli		

18' RT. = end curb.
 2+51- 16' RT. = end conc. gutter

15.05	15.05	15.15	14.95	14.37	14.85
7.1	7.1	7.0	7.2	7.78	7.3
25	13		16.8	16.8	18
			Grd.	Gutter	Grd.

16' RT. = edge conc.
 23' RT. = B.C. 5' Rad. ch.
 2+46- 25' RT. = start ch. + end drive

14.75
 7.40
 25
 ch. + drive

2+40- 16' RT. = E.C. drive

13.99 14.45
 8.16 7.70
 18 25
 drive drive

End E. + W. wall.
 25' RT. = end ch. also =
 2+34 - 23' RT. = E.C. ch.

14.75	14.45	13.94	13.87
7.4	7.7	8.23	8.28
	16	16.8	18
		Edge	G
		conc.	

14.17	14.55
7.98	7.6
25	25
G +	T.W.
22.15	46

Conole

4

64

3+01 E 21' Lt. = start conc. ch.
3

17.65 17.15
4.50 5.00
21.9 21.9
cc G

17.15 17.35
5.00 4.8
20.2 25
cc

18' Lt. = edge pave.
25' Rt. = end fence.
20' Rt. = start conc. ch.
2+99 E 4' = wly. Congress

17.95 17.70 17.35 16.75 16.67
4.12 4.95 4.80 5.40 5.48
25 18 20.5
E.P. G

19' Rt. = start A.C. Pave.
24' Lt.
23' Lt.
2+98 22' Lt. } 2 (V.I.)

16.65
5.50
19
pave

2+97 = start A.C. Pave, on E

17.75
4.93
pave

2+94 15' Lt. = start A.C. Pave
17.15 17.65 17.05 17.00 17.05 16.55 17.05 17.05
4.4 4.5 5.1 5.15 5.1 5.6 5.1 5.1
25 18 17 15 20 21 25
pave
6. Ord 22.15

Condo

INDEXED ~~+~~
Savins
OCT 22 1953

65

4145 25.57 (25.55)

T.P. 6.59 30.02 3.37 23.43

T.P. 6.94 26.80 2.29 19.86

Ely. 7' L.H.T. Harney & Jefferson - P-42

Ely. cross in M.H. Rim Congress
Harney T

just been finished.
intersection. This has
See const. plans for

33' RT = E.C. 15' Rad cl. Rot.

3+06^E = W. ly cl. line Congress

18.06 18.51
4.09 3.64
50 50
G cl.

18.30 17.87 18.07
3.85 4.33 4.13
50 50 33
cl G cl. E.C.

17.57 18.07
4.58 4.08
33 33
G cl.
E.C.

17.57 17.51 17.41 17.67 17.13 17.75
4.58 4.64 4.74 4.58 5.02 4.90
33 25 18 18 25
G

22.15

Begg
Oltman
Schelin

Trias

Street

66

INDEXED
OCT 22 1953

the Taffersden St

April:

1500/400 St

sample #2
of 4 samples

wide
conc.

Amputia

A. C. Pavlov

Moore St.
Trias to Ampudia

also = start wire fence.
paved trailer court
0-03 { 21' Lt. = start cold lay.

0-08 26' Lt. = 14" pole # T.P. 3848

0-10 = { Sly. cl. line Trias.

0-13⁵ 25' Rt. = sly. cor. 3⁵' wide
conc. gutter

Pave. Do not regard.
0-25 = ± Trias - Rock + oil + A.C.

T.P. 0.87 37.06 12.42 36.19
7.23 48.61 — 41.38

27.86
8.2
25

27.66 27.46 27.36 26.76
8.4 9.6 9.7 10.3
215 19 16 14

27.06 27.76
10.0 9.8 9.21
159 159
on curb.

27.71
7.85 7.02
75 75
0 0

27.46 26.96 26.66 27.06 27.76 27.12 27.92
9.6 10.1 10.4 10.0 9.8 9.94 9.13
75 25 15 15 15 25 25
G 0

27.36
7.70
25
cor. gutter

27.06 26.96 26.56 27.06 27.66 27.76
10.0 10.1 10.5 10.0 9.4 7.8
75 50 25 25 25 75

37.06

T.P. #1. P. 25

Moore St.

£

68

0+74 - 23' Lt. = 4" oleander

0+64 - 23' Lt. = 2" loguat. tree

0+54 23' Lt. = 2- 6" diam Tamarisk

0+51 - 15' ^{curb} driveway cut out 17' long
 Rt. = start 25' long

0+50

0+44 - 22' Lt. = 3" diam. oleander

0+24 - 22' Lt. = 2- 6" Tamarisk ^{trees}

0+20 } should be repaired
 to }

0+16 } Curb is broken.

0+15 - 22' Lt. = 3" diam pine

0+07 - 22' Lt. = 3" oleander

0+00 - { 15' Rt. = E.C. 10' Rad. ob. Reti.

0-01 22' Lt. = £ 10" diam. Tree (Tamarisk)

6.25 33.29 10.02 27.04

37.06

28.89	28.89	27.29	27.49	28.29	29.04
4.4	4.4	6.0	5.8	5.0	4.25
25	21.5	12		15	15
	oil				cl

28.89	28.89
4.4	4.4
35	25

28.69	27.79	27.49	26.79	26.99	27.79	27.91
4.6	5.5	5.8	6.5	6.3	6.0	5.38
28.5	21	17	15		15	15
oil						cl

33.29

£ Nail 0-07

Moore St

1+86 23⁴ Lt. = 12' A.C. drive.

1+80

1+75- 23² Lt. = end fence.

1+65 23⁷ Lt. = 2" Oleander

1+60

1+55 24³ Lt. = 8" Tamarisk

1+45 23⁸ Lt. = 3" Oleander

1+40

T.P. 3.82 33.51 3.60 29.69

1+24 23⁵ Lt. = 3" Erythraea

1+20

1+14 24 Lt. = 6" Tamarisk

1+05 23' Lt. = 4" Oleander

1+00

0+95- 23^E Lt. = 4" diam Pine

0+85 23' Lt. = 8" diam Tamarisk

33.29

69

29.81 29.81 30.01
3.7 3.7 3.5
23.4 25 50

29.81 29.81 29.71 29.31 29.31 30.11 30.71
3.7 3.7 3.8 4.2 4.1 3.4 2.74
25 23.2 13 12 15 15
A.C.

30.11 30.11 29.71 29.41 29.41 30.41 30.81
3.4 3.4 3.8 4.1 4.1 3.3 2.70
25 23.2 13 11 15 15
oil

30.71 30.71 29.61 29.41 29.31 30.01 30.80
3.3 3.3 3.9 4.1 4.2 3.5 2.71
25 23 13 12 15 15
oil

33.51

30.09 30.09 29.89 29.19 29.09 29.79 30.59
3.2 3.2 3.4 4.1 4.2 3.5 2.70
25 22.8 22 11 15 15
oil

30.09 29.89 28.59 28.69 29.39 30.71
3.2 3.4 4.7 4.6 3.9 3.00
25 22.7 12 15 15
oil

33.29

Moore

2

70

25' Rt } Ret.
25' Lt } E.C. 10' Rad. cl.

3+40 - Sly. Cl. Ampudia

= start A.C. Pave.

15' Lt }
15' Rt } B.C. 10' Rad cl. Ret.

2+99 97 = Sly Ampudia

2+94 23' Lt } should come out.

2+66 23' Lt } = large cactus.

2+50

2+21 24' Lt. = end fence
lay.
+ end of oil + cold

2+00 26' Lt. = 4" tree

1+96 - 23' Lt. = start rail fence.

27.71
5.80 6.32 4.08 3.54
75 75 75 75
cl G G cl

28.04 27.61 27.84 28.11 28.51 28.66 29.05
5.47 5.90 5.67 5.40 5.00 4.85 4.46
25 25 15 15 25 25 25
cl G cl G cl cl

28.37 28.06 27.70 28.78 28.51 29.06
5.19 5.45 5.81 5.23 5.00 4.45
25 15 15 G 15
back of cl G 15 cl
walk
+ end.

28.91 28.81 28.41 28.71 29.01 29.78
4.6 4.7 5.1 4.8 4.5 3.73
25 15 12 15 15
cl

29.71
3.8
24' oil

29.71 29.71 29.41 29.01 29.31 29.71 30.50
3.8 3.8 4.1 4.5 4.2 3.80 3.01
25 232 13 11 15 15 17.2
oil 11/4 drive 07 walk

33.57

Moore

4

71

INDEXED
Sams
OCT 22 1953

page 29

(33.55)

wly. 7' L.H. Ampudia + Jefferson

5.12 33.56

T.P. 7.64 38.68 2.47 31.04

3 + 24 ⁹⁷ = 4 Ampudia

^{27.51} 6.00	^{27.87} 5.64	^{28.39} 5.12	^{28.89} 4.62	^{29.68} 3.83
75	25		25	75

33.51

Moore Street.

Arripudia to Arista 11/21/53

C.H.S.
Begg
Schelin
Pullan

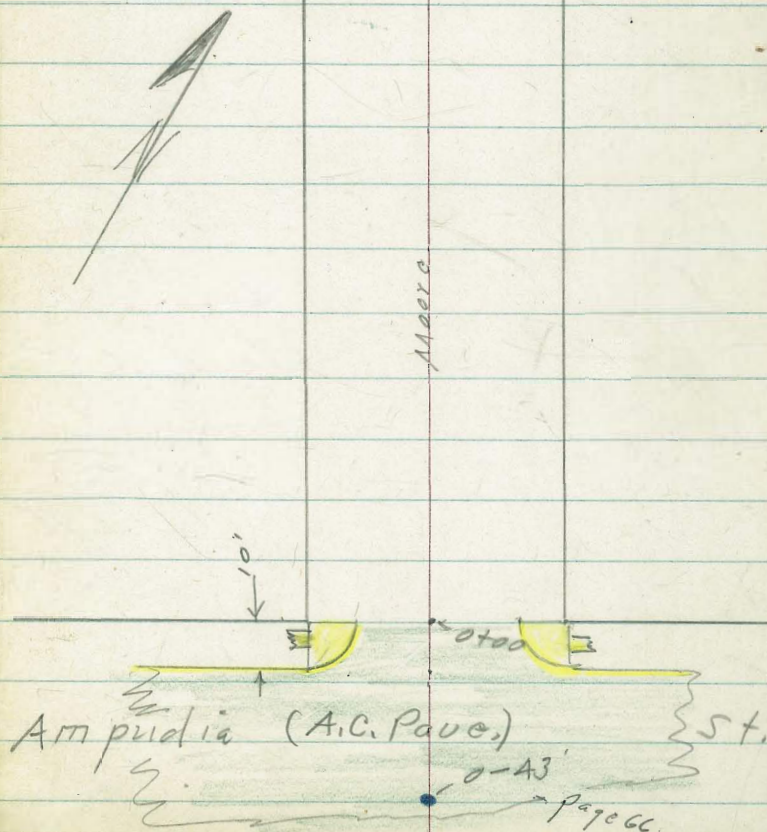
W.O. 32209

Arista

xx Fd 4 crosses on M.H.

• Fd. P.K. Conc. Nail

(N) = Ctr. water meter box



Moore St.

73

0+23- 24' Lt. = 2' conc. walk

78.57 78.47 78.47
4.4 4.55 4.55
35 25 243
← walk →

T.R. 4.92 32.97 7.50 28.05

32.97

25' Lt. = start wire fence.

0+01 17' Rt. = Pole # P2352 (14")

{ 25' Rt.
25' Lt. } = end walk.
{ 15' Rt.
15' Lt. } = end cl.

0+00 = } end A.C. Pav. = wly line Amp.
= radi

78.35 78.27 78.04 77.74 78.27 78.46 79.00 79.35 79.15
7.2 7.33 7.51 7.81 7.28 7.09 6.55 6.20 6.4
25 25 15 15 15 15 15 25 25
End walk cl G cl walk End

77.55
8.00
75
cl

79.78 79.73
6.27 5.82
75 75
G cl

0-10. { 25' Rt. } = B.C. 10' Rad. cl. Rot.
25' Lt. } = wly cl. Ampudia

77.73 78.05 77.54 78.03 78.55 79.01
8.42 7.50 8.01 7.52 7.00 6.48
75 25 25 25 25 25
G cl G 35.55 G cl

7.50 28.05

wly. 7' Lt. Ampudia + Moore

2.00 35.55 — 33.55

wly. 7' Lt. Ampudia + Jefferson (P29)

Moore.

74

T.P. 4.68 32.33 5.32 27.65

1+86 17^E Lt. = (W)

1+76 16^E Rt. = (W)

1+74 25^E Lt. = $\pm$ 3' conc. walk

1+50 Lt. = end fence.

drive
25' Rt. = $\pm$ good 7^E wide

1+43 21' Rt. = $\pm$ 7^E wide drive
Rough conc.

(17^E Rt. = (W))

1+25 { 25^E Rt. = $\pm$ 2' walk

1+14 17 Lt. = 18" pole # T2373

{ = start picket fence
(25' Lt.) = end wire fence

1+00 { 25' Rt. = $\pm$ 6" conc. block wall

0+99 17 Rt. = 14" pole # P2370

0+73 17 Rt. = (W)

0+54 17 Lt. = (W)

0+50

78.76 78.07
4.71 4.90
32 25^E
walk walk
78.77 78.17 77.87 77.97 77.77 77.97 78.17
4.7 4.8 5.1 5.0 5.2 5.0 4.8
25 14 12 14 15 25

78.17 78.31 78.50
4.8 4.65 4.97
21 25 45
Rough start on
conc. good drive
78.44 78.65
4.53 4.32
25^E 35^E
walk

78.17 78.07 77.87 77.97 77.97 78.37 77.77 77.87
4.8 4.9 5.1 5.0 5.0 4.6 5.2 3.1
25 14 13 12 25 8.0 7.0
25 25

78.27 78.27 77.87 78.07 78.07 78.77 78.27
4.7 4.7 5.1 4.9 4.9 4.7 4.7
25 14 13 12 14 25

32.97

Moore St.

+ A.C. Paue
3+07^E 25' RT. = start conc. ch.
(See Arista L-sheet.)

2+99^{9L} = Ely. line Arista

2+99 16 RT. = 14" pole # P 2398

2+83 18' Lt. = (W)

2+59 25^E Lt. = $\pm$ 7' wide level
Conc. Dr.

2+50 25³ Lt. = end fence

2+27 25⁴ Lt. = $\pm$ 3' walk

2+25 17' Lt. = (W)

2+01 16^E RT. = 14" pole # P 2380

2+00 = 25² Lt. = start picket fence

$\pm$

75

24.13
8.20
25
a

24.61
7.72
25
ac

28.13
4.12
25

27.93
4.14
14

27.63
4.17
13

27.73
4.16
13

27.33
5.0
13

27.93
7.4
16

27.73
4.6
25

28.53
3.80
40
drive

28.51
3.82
255

28.33
4.10
25

27.93
4.14
14

27.73
4.16
13

27.53
4.8
12

27.43
4.9
14

27.63
4.7
14

27.43
4.9
25

28.63
3.7
35
walk

28.4
3.83
254

27.93
4.14
25

27.83
4.5
14

27.73
4.6
13

27.63
4.7
12

27.43
4.9
14

27.73
4.6
14

27.63
4.7
25

32.33

Moore St.

±

76

3+42^E - 25' RT - 2 end A.C. Pavo. + curb.

23.61
8.72
25
C

24.10
8.23
25
C

21.50
10.83
60
C

21.97
10.36
60
C

3+39^I { 35' RT = B.C. 20' Rad. Cl. Ret.
why. cl. Arista

26.93
5.4
25

27.73
5.1
15

27.03
5.3
13

27.33
5.0
10

26.53
5.8
10

23.98
8.35
25
A.C.

23.77
9.06
35
C

23.68
8.68
35
C

3+24⁹¹ = ± Arista

27.03
5.3
25

27.53
4.8
15

27.33
5.0
12

27.49
4.49
10

27.84
4.49
10

27.03
5.3
10

27.36
7.97
25
A.C.

23.68
8.65
35
+ Gnd.

Sewer
I.E.

21.95
10.38
60
C

22.42
9.91
60
C

23.71
8.62
35
C

24.17
8.16
35
E.C. - 20' Rad
Cl. Ret.

3+09^I = Ely cl. Arista

27.83
4.5
25

27.83
4.5
15

27.73
4.6
12

27.73
4.6
10

27.13
5.12
10

24.43
7.90
25
A.C.

32.33
+ Gnd.

Tie Points Arista St.

At Moore

At Jefferson 12-21-53

C.H.S.

Boggs

Schelin

Pullen

INDEXED
MER
FEB 2 1954

Moore St. Arista to Conde)
Ed 4 crosses on M.H. (See X See.

77

Jefferson

35.00

Ed 4 crosses on
M.H. (See page 23)

St.

Set. P.K. Nail
in Pav.



Arista

Set. P.K. Nail
in Pav.

35.00

Moore

St.

Clark
Shagard
Bridger
ONeil
L-1-54
W.O. 32209

Nely Line
ADD: LEVELS: JEFFERSON ST.
100' N.W. CONDE ST.

(See sketch pg 23)

T.P.

7.83 = 20.01 - 18' RT 0403 Jefferson

1+00

INDEXED
JER
FEB 2 1954

0+57 15' RT & 10' Conde Dr.

0+40

0+20

0+00 N.W. 1/4, Tine Conde
CK, Co. on Pg. 35

B.M.

7.83 22.84

L.D.
N.W. 1/4 CK Prop
Conde
20.01 Ely Line
Jefferson
(837)

L+

R+

24.67
3.17
1.5
24.71
3.13
22.5
24.34
3.5
25
24.34
3.5
25

23.84
3.00
1.5
23.95
3.89
22.5
23.84
4.0
25
23.74
4.1
35

22.65
5.19
1.5
23.51
4.33
22.5
23.24
4.6
25
22.94
4.9
35

22.54
5.30
1.5
22.74
5.10
22.5
22.54
5.3
25
22.34
5.0
30

21.76
6.58
1.5
21.41
6.43
22.5
21.34
6.5
25
21.34
6.5
30

19.76
8.08
1.5
19.91
7.93
22.5
19.74
8.1
25
20.14
7.2
35

22.84

15.25
380
11.45

1971

11.45

826

25.10

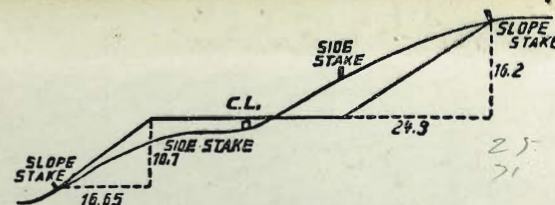
62

18.8

22.00

18.8

9.2



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

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