

1001

1001

LEVEL BOOK

No. 410 T

EUGENE DIETZGEN CO.,

Drawing Materials and Surveying Instruments.
 NEW YORK. CHICAGO. SAN FRANCISCO.

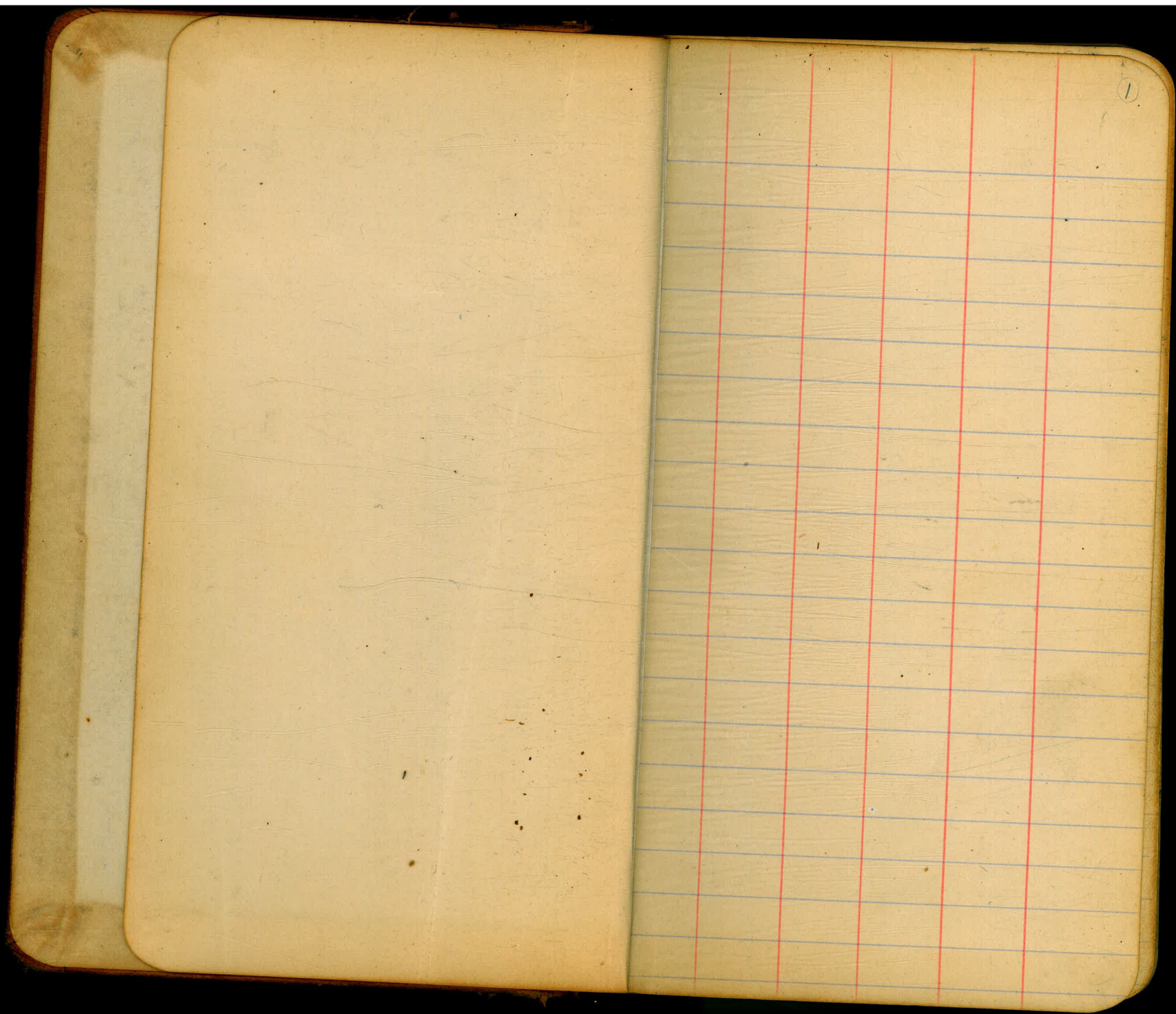
TABLES FOR EXCAVATIONS AND EMBANKMENTS.
 DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING
 ROADWAY 20 FEET WIDE. SIDE SLOPES 1 TO 1.
 FOR SINGLE TRACK EXCAVATION.

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MICROFILMED
 DEC 16 1964

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	0
1	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	1
2	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	2
3	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	3
4	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	4
5	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	5
6	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	6
7	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	7
8	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	8
9	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	9
10	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	10
11	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	11
12	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	12
13	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	13
14	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	14
15	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	15
16	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	16
17	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	17
18	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	18
19	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	19
20	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	20
21	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	21
22	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	22
23	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	23
24	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	24
25	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	25
26	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	26
27	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	27
28	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	28
29	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	29
30	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	30
31	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	31
32	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	32
33	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	33
34	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	34
35	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	35
36	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	36
37	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	37
38	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	38
39	49.0	49.1	49.2	49.3	49.4	49.5	49.6	49.7	49.8	49.9	39
40	50.0	50.1	50.2	50.3	50.4	50.5	50.6	50.7	50.8	50.9	40

Calculated by F. E. Paradis, C. E.



80' St.
14' marks La Jolla Boulevard
13' Quarters

6191

3

ang

0.71 HI 61.91 61.20
Sect. BC

22' North Sect AB

W		3.0	58.9	cl	11.0	50.9
+11		2.0	58.9	1/4	2.8	59.1
cl ③		3.9	58.0	+4	2.7	59.2
1/4 ①		2.9	59.0	3.0	58.9	
C		2.2	59.7	3.7	58.2	
1/4 ②		1.5	60.4	2.8	59.1	
cl ③		1.7	60.2	1/4	2.0	59.9
+3		1.1	60.8	cl	1.6	60.3
E		0.8	61.1	E	1.5	60.4

25' north

	Sect AB			E	1.5	60.4
E		0.74	61.17	cl	1.6	60.3
+9		1.1	60.8	1/4	2.1	59.8
+10		1.8	60.1	C	3.0	58.9
cl.		1.7	60.2	+6	3.6	58.3
1/4		1.6	60.3	+7	2.9	59.0
C		2.2	59.7	1/4	2.6	59.3
1/4		3.0	58.9	+12	2.8	59.1
+12		4.0	59.9	cl.	3.6	58.3
cl.		3.1	58.8	W	10.5	51.4
W.		3.0	58.9			

La Jolla Boulevard

6191

50' north

W	9.6	52.3
ch	7.1	54.8
+10	5.8	56.1
1/4	4.6	57.3
+6	2.2	59.7
C	2.1	59.8
+9	2.5	59.4
1/4	3.4	58.5
	3.0	58.9
ch	2.2	59.7
E	1.7	60.2

75' north

E	2.1	59.8
ch	2.9	59.9
+2	3.2	58.7
+4	1.9	60.0
1/4	2.0	59.9
+6	1.8	60.1
C	4.2	57.7
1/4	6.9	56.0
ch	8.2	53.7
W	11.1	50.8
30' west slope.	22.8	39.1

619

(4)

79' north

30' west slope	24.1	37.8
W	14.4	47.5
ch	8.7	53.2
1/4	5.8	56.1
C	4.3	57.6
+7	1.8	60.1
1/4	1.8	60.1
+11	1.9	60.0
ch	2.4	59.5
+1	3.2	58.7
E	2.2	59.7

90' north

E	2.5	59.4
+7	3.0	58.9
+8	1.9	60.0
ch	1.8	60.1
+10	1.8	60.1
1/4	2.6	59.3
C	4.6	57.3
1/4	5.6	56.3
ch	13.0	48.9
W	18.5	43.4
45' W slope. bottom down	28.8	33.1

LA JOLLA BOULEVARD

61.91

100' north

40' W slope	25.4'	36.5
25' W slope bottom draw	27.1	34.8
W line	23.8	38.1
cl	19.2	42.7
+11'	13.5	48.4
1/4	7.3	54.6
C	5.4	56.5
1/4	3.6	58.3
+11	1.9	60.0
cl	1.8	60.1
+11'	2.2	59.7
+12'	2.9	59.0
E	2.9	59.0

117' north

E	1.8	60.1
+10	2.0	59.9
cl	4.0	59.9
1/4	11.4	50.5
C	20.7	41.2
1/4	23.5	38.4
cl	25.8	36.1
W	27.8	34.1
20' W slope	20.0	41.9

61.9

55

125' north

20' W slope	10.0	51.9
W	18.6	43.3
cl	26.3	35.6
1/4	25.6	36.3
C	24.6	37.3
1/4	14.4	47.5
cl	7.5	54.4
+7'	1.8	60.1
E	1.8	60.1

135' north

E	1.9	60.0
+5'	2.1	59.8
cl	8.7	53.2
1/4	17.0	44.9
C	10.2	51.7
+6'	25.8	36.1
1/4	25.6	36.3
+5'	25.1	36.8
cl	23.1	38.8
	19.8	42.1
W	14.3	47.6
10' W slope	7.0	54.9

LA JOLLA BOULEVARD

6191

138' north

E	19	60.0
+5'	2.3	59.6
cl	8.8	53.1
1/4	17.0	44.9
C	10.6	51.3
+6'	25.6	36.3
1/4	25.0	36.9
+5'	22.0	39.9
cl	17.7	44.2
W	8.2	53.7

150' north

W	4.6	57.3
+10'	6.3	55.6
cl	6.2	53.7
+6'	7.8	54.1
1/4	10.2	51.7
C	18.0	43.9
+5'	20.8	41.1
1/4	15.4	46.5
cl	8.7	53.2
+10'	2.1	59.8
E	1.8	60.1

J.P. 1098 H.I. 71.34 1.55 60.36

6
6

71.34 H.I.

175' north

W	9.6	61.7
cl	10.8	60.5
1/4	10.4	60.9
C	10.6	60.7
1/4	10.6	60.7
cl	13.3	58.0
+9'	11.1	60.2
E	11.0	60.3

200' north

E	10.1	61.2
cl	9.6	61.7
1/4	8.8	62.5
C	8.9	62.4
1/4	10.0	61.3
+2'	9.6	61.7
+4'	8.0	63.3
cl	8.1	63.2
W.	7.6	63.7

LA JOLLA BOULEVARD

7134

225' north

W	6.6	64.7
cl	6.6	64.7
1/4	6.9	64.4
C	7.0	64.3
1/4	7.1	64.2
cl	8.1	63.2
E	9.3	62.0

250' north

E	8.8	62.5
+9'	8.2	63.1
+10'	7.0	64.3
ab.	6.6	64.7
1/4	6.2	65.1
C	5.8	65.5
1/4	5.6	65.7
cl	5.6	65.7
W	5.5	65.8

7134

79

275' north

W	4.6	66.7
cl	4.7	66.6
1/4	4.9	66.4
C	4.8	66.5
1/4	5.0	66.3
+10'	5.6	65.7
+11'	7.0	64.3
cl	7.4	63.9
+12'	7.9	63.4
E	8.7	62.6

300' north

E	7.1	64.2
+10'	7.7	63.6
+11'	6.8	64.5
cl	6.7	64.6
1/4	6.0	65.3
+12'	4.3	67.0
C	4.2	67.1
1/4	4.1	67.2
cl	4.0	67.3
W	3.9	67.4

325' north

W	3.4	67.9
ch	3.4	67.9
1/4	3.5	67.8
+12'	3.7	67.6
C	4.0	67.3
+2'	5.3	66.0
1/4	5.7	65.6
+5'	5.7	65.4
+6'	6.2	64.4
ch	6.2	65.1
E	5.0	66.3

350' north

E	3.5	67.8
ch	4.5	66.8
1/4	5.4	65.9
+6'	6.0	65.3
+7'	4.9	66.4
+10'	4.8	66.5
1/4	4.3	67.0
ch	3.3	68.0
ch	3.2	68.1
W	2.7	68.6

376.59' north sect A.B.

W	2.49	68.85
ch	3.3	68.0
1/4	3.9	67.4
+3'	4.9	66.4
C	4.2	67.1
1/4	3.5	67.8
ch	2.9	68.4
E	3.1	68.2

So. End of curves. (sect 40 E)

E	3.1	68.2
ch	2.9	68.4
1/4	3.4	67.9
C	4.1	67.2
+11'	4.8	66.5
1/4	3.9	67.4
ch	3.3	68.0
W	2.49	68.85

LA JOLLA BOULEVARD

71.34

(99)

6909

Center of curves (sect 85)

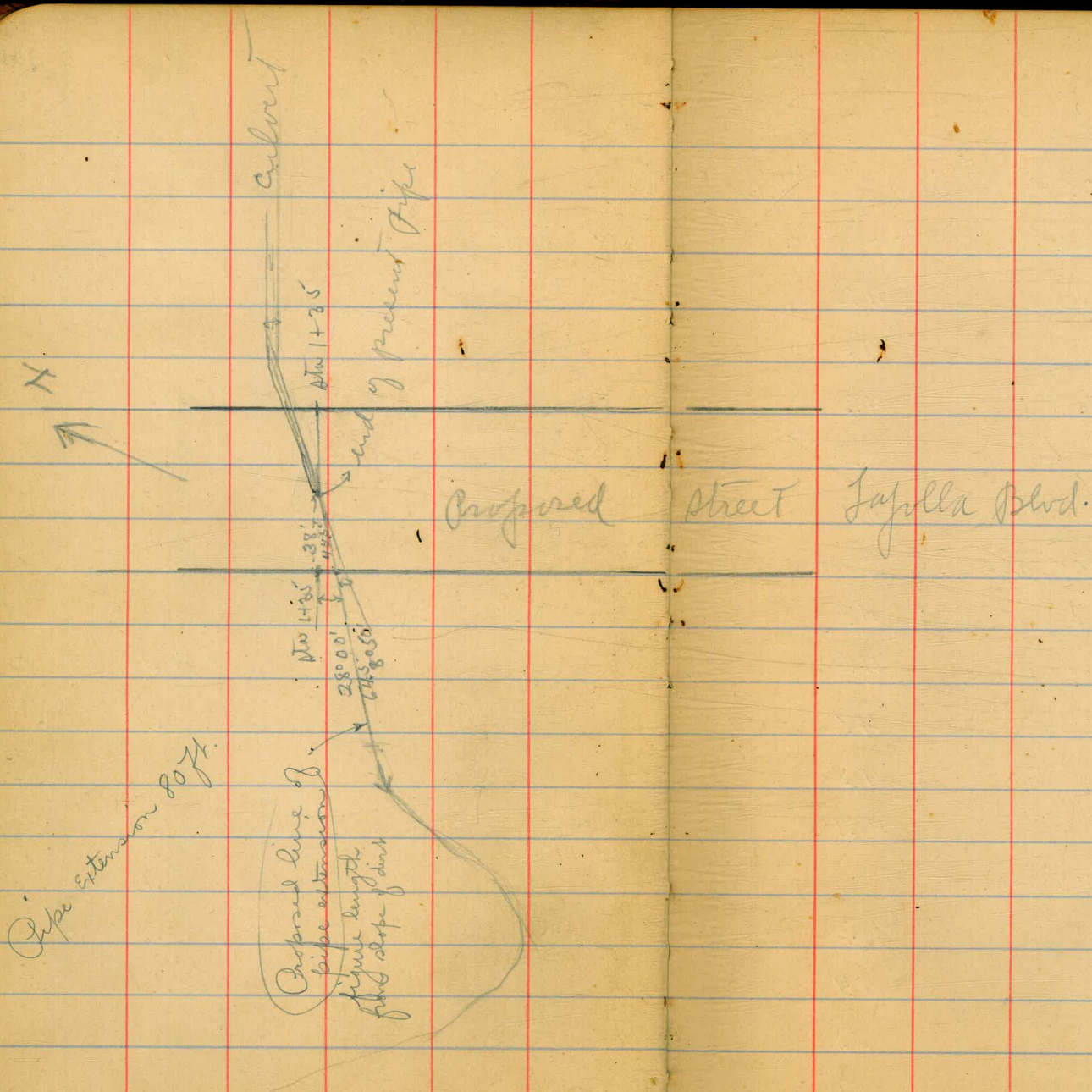
W		2.4	68.9
cl		3.0	68.3
+2'		3.1	68.2
+4'		4.0	67.3
1/4		3.5	67.8
c		2.9	68.4
1/4		2.7	68.6
cl		2.8	68.5
+3'		3.0	68.3
E		2.1	69.2
		2.0	69.3

north end of curves (sect 41)

E		1.8	69.5
cl		1	
quarter	cement curb.	2.1	69.04
1/4		2.7	68.6
		2.5	68.8
C		2.4	68.9
1/4		2.8	68.5
quarter		3.1	68.2
cl	cement curb	2.6	68.7
W		2.0	69.3
		3.34	68.00

on profile 9/5/16

S.W.G.



Pipe extension 80 ft.

Proposed line of pipe extension

figure length find slope of pipe

Proposed Street Jayella Blvd.

culvert

end of present pipe

Sta 1+35

Sta 1+35

28' 00"

27' 85"

38'



X sect. Ocean street from
Boulevard South. 20' street

H.I.
2.34 96.41 94.07

2058' So. coast Blvd. South (no. line Girard)

W. line

4.2

4.4

C

4.3

4.2

E. line

4.1

200' So. coast Blvd. South

E. line

4.5

4.6

C

4.8

4.5

White

4.3

175' So.

White

5.3

5.4

C

5.5

5.4

E. line

5.2

Girard to coast

5 foot readings

B.M. Girard 150' So.

E. line

C

White

White

C

E. line

E. line

C

White

Sept. 8/16

(11)

Chubb
Evans
Shaw

11

125' So.

5.8

6.2

6.3

6.5

6.3

8.4

8.3

8.2

8.1

7.7

108' So.

10.2

10.2

10.1

10.0

10.3

9641

100' 20.

White

11.0

C

11.1

11.5

J.P.

1.96

H.I.

85.85

12.02

83.89

E line

1.5

0.7

75' 20.

E line

6.6

7.2

C

7.3

7.1

White

7.4

50' 20.

White

11.7

11.4

C

12.0

12.1

E line

11.5

12⁽²⁾

J.P.

1.60

H.I.

74.81

12.64

73.21

A

25' 20.

E line

7.4

8.1

C

8.1

8.0

White

8.4

J.P.

4.66

H.I.

67.50

11.97

62.84

Smith line Coast Blvd. South.

White

5.8

5.7

C

6.1

5.9

E line

5.1

5' north of South line.

E line

11.7

11.8

C

11.8

11.9

W line

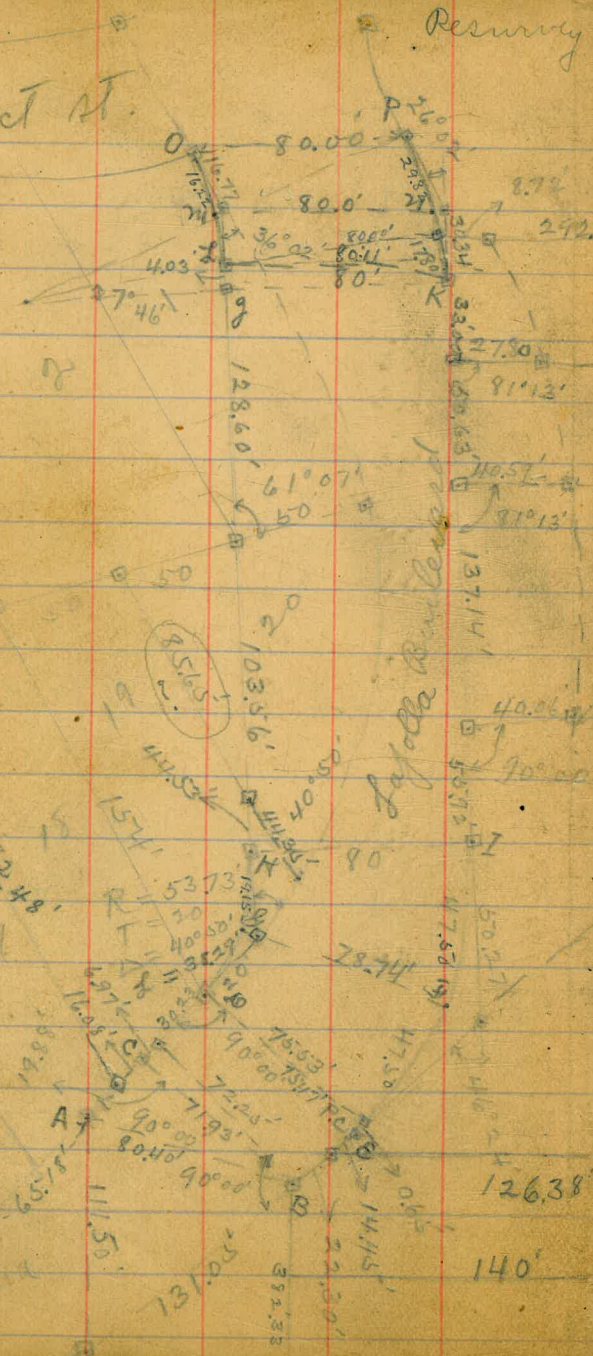
11.8

J.P.

22' west across at prop grade 12.19 55.31

Prospect St.

R = 51.56
T = 16.77
Δ = 36° 02'
L = 32.43'



Safolla Blvd. 80' street
14' walks 13' quarters

1114

R = 131.25'
T = 30.34'
Δ = 26° 02'
L = 59.64' H

Sept. 21 to 26/16 } Childs
Evans
Shaw

264.0

243.5

276.69

R = 117.29'
T = 50.27'
Δ = 46° 24'
L = 94.99'

Area at C = 5100

30.23
5.47
19.55
19.55
17.31
Δ

LA JOLLA BLVD.

0.75^{H.F.} 61.95 61.28

sect AB.

White	2.91	59.04
	3.1	58.8
	3.9	58.0
	3.1	58.8
C	2.2	59.7
	1.6	60.3
	1.7	60.2
+2' Blue	1.3	60.6
	0.8	61.1

sect BC

Blue +12	0.8	61.1
	1.0	60.9
	1.8	60.1
	1.6	60.3
	1.8	60.1
	2.7	59.2
+10 gutter	3.8	58.1
	3.0	58.9
White	2.8	59.1

61.9

15
15

sect DE P.C.

White	2.1	59.8
	2.6	59.3
gutter	3.4	58.5
	2.3	59.6
C	1.7	60.2
	1.7	60.2
	1.8	60.1
+4' Blue	0.8	61.1
	0.57	61.3

sect FG

Blue	1.3	60.6
	1.7	60.2
	1.6	60.3
C	1.7	60.2
	2.4	59.5
	3.2	58.7
+9	2.1	59.8
+10	2.1	59.8
White	1.8	60.1
	2.5	59.4

LA JOLLA BLVD.

61.9

61.9

10

	sect	H.I.	P.C.
White			4.04 57.9
			2.6 59.3
+3'			2.0 59.9
			1.9 60.0
+3'			1.0 59.9
26			3.0 59.9
			2.6 59.3
			1.8 60.1
			1.6 60.3
Elms			1.90 60.0
	10' north	sect H.I.	
Elms			1.7 60.2
			1.7 60.2
			2.1 59.8
			2.9 59.0
+3'			1.9 60.0
			2.0 59.9
+5'			2.0 59.9
do.			3.7 58.2
			8.2 58.7
			5.7 56.2
White			
10' W	Slope.		5.9 56.0

	25' north		
30' W	Slope	26.5	35.4
White		23.7	38.2
		13.6	48.3
		4.5	57.4
+4'		2.0	59.9
		1.9	60.0
+2'		2.2	59.7
+3'		2.9	59.0
		2.4	59.5
		1.7	60.2
Elms		1.8	60.1
	41' north		
Elms		1.6	60.3
		1.7	60.2
		2.7	59.2
		2.9	59.0
		3.0	59.9
		1.9	60.0
		4.4	59.5
		7.8	54.1
		16.0	45.9
White	Center, culvert bottom	24.8	37.1
28' W	of pipe slope	25.0	36.9

61.9

50' north

20' w slope.	18.2	43.7
White	20.6	41.3
	15.5	46.4
	9.2	52.7
+10	2.1	59.8
C	1.8	60.1
+11	1.8	60.1
	2.9	59.0
	1.9	60.0
E line	1.5	60.4
	67' north	
E line	1.3	60.6
	2.0	59.9
+10	2.6	59.3
	1.6	60.3
C	1.7	60.2
	9.0	54.9
	7.1	54.8
+10	7.0	54.9
White	5.6	56.3
10' w. slope	4.8	57.1

17

61.95

75' north

10' w slope.	2.7	59.2
White	3.0	58.9
	2.2	59.7
	3.2	58.7
+10	3.3	58.6
C	1.7	60.2
	1.4	60.5
+3'	1.6	60.3
+4'	2.4	59.5
	1.9	60.0
E line	1.1	60.8
J.P.	10.50	72.06
	0.39	61.56
	83' north	
E line	11.1	61.0
	11.9	60.2
+7	12.4	59.7
+10	11.3	60.8
	11.3	60.8
C	10.8	61.3
	9.8	62.3
	9.6	62.5
White	9.9	62.2

72.1

LA JOLLA BLVD

100' north

White	10.3	61.8
	9.7	62.4
	9.7	62.4
C	10.7	61.4
	10.8	61.3
+6'	10.7	61.4
+10'	11.9	60.2
	11.5	60.6
Elm	10.5	61.6

125' north

Elm	9.7	62.4
	10.7	61.4
+2'	11.0	61.1
+4'	10.2	61.9
	10.0	62.1
C	8.6	63.5
	7.9	64.2
	7.9	64.2
White	8.0	64.1

72.1

18

150' north

White	6.6	65.5
	6.6	65.5
	6.8	65.3
C	7.2	64.9
+6'	7.7	64.4
+9'	9.0	63.1
	9.3	62.8
+8'	9.3	62.8
+9'	10.1	62.0
	10.0	62.1
Elm	8.7	63.4

175' north

Elm	7.6	64.6
	8.7	63.4
+6'	9.3	62.8
+8'	8.3	63.8
	8.2	63.9
+7'	7.7	64.4
+10'	6.1	66.0
	6.1	66.0
	5.5	66.6
	5.6	66.5
White	5.6	66.5

LA JOLLA BLVD.

72.1

200' north

white	4.9	67.2
	4.9	67.2
+8 +11	5.0	67.1
	5.7	67.0
	6.9	65.2
	7.1	65.0
	7.5	64.6
+2'	8.5	63.6
	7.3	64.8
Elmo	6.0	66.1

225' north

Elmo	4.7	67.4
	5.7	66.4
	6.8	65.3
+6 +7	7.5	64.6
	6.7	65.1
	6.4	65.7
+9	6.0	66.1
	4.4	67.7
	4.3	67.8
white	4.3	67.8

72.1

19

250' north

white	3.8	68.3
	4.0	68.1
+6 +8	4.1	68.0
	5.1	67.0
	5.3	66.8
+10 +11	5.6	66.5
	5.7	65.4
	6.6	65.5
	5.4	66.7
	4.3	67.8
Elmo	4.0	68.1

276.69' north (sect 9K)

Elmo	2.8	69.3
+5	4.1	68.0
	3.6	68.5
	4.0	68.1
	4.8	67.3
	5.7	66.4
+2'	4.7	67.4
	4.2	67.9
+4"	3.5	68.6
white	3.38	68.7

Lafolla Boulevard

72.1

Sect. L.K.

White	3.3	68.8
+10'	3.7	68.4
	4.1	68.0
+10'	4.6	67.5
	5.6	66.5
C	4.7	67.4
	4.0	68.1
	3.6	68.5
+9'	4.0	68.1
E line	2.8	69.3

Sect. M.J.

E line	2.7	69.4
+10'	2.8	69.3
	3.7	68.4
	3.4	68.7
C	3.6	68.5
	4.1	68.0
+10'	4.7	67.4
	3.7	68.4
White	3.1	69.0

72.06

20

Sect O.P.

White	2.7	69.4
gravel	3.11	68.95
cement curb.	3.7	68.4
	3.6	68.6
C	3.1	69.0
	3.2	68.9
gravel	3.4	68.7
cement curb	2.78	69.28
E line	2.6	69.5

3596

3720

3829

50

16145

3720

1624

1488

1860

372

57288

16145 23000 154

16145

88550

80725

78250

14384

17980

3596

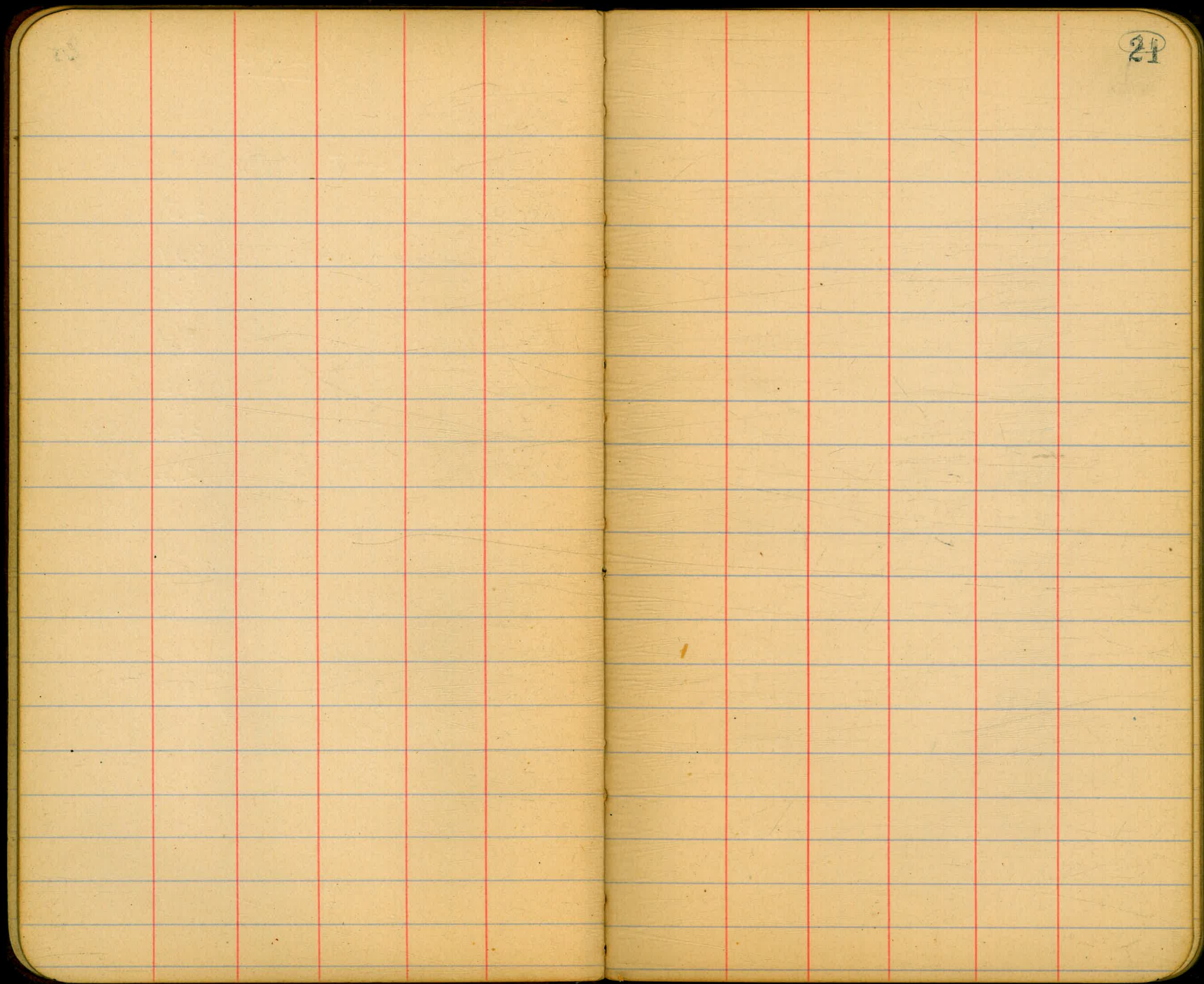
5537840

56.5

77

5722

5



21

12/27/16
Gregory
Moore
B Moore

CROSS-SECTION OF
QUINCE ST
From Union to Columbia

80' wide
25' walks
7.5' Quarters

QUINCE

22
22

BM	H. L. UNION ST.						
0.86	210.63		209.77	Top Hydrant, 5th Redwood & Union	+10	7.6	203.0
N.		5.3	205.3		N	7.3	203.3
+14		5.6	205.0				
+15		6.9	203.7		N	9.4	201.2
cb		7.1	203.5		+16	9.4	201.2
1/4		7.0	203.6		+17	11.5	199.1
C		6.9	203.7		cb	11.8	198.8
1/4		7.2	203.4		+4	11.1	199.5
cb		7.6	203.0		1/4	10.8	199.8
S		7.5	203.1		C	10.9	199.7
	20' W				1/4	11.2	199.4
S		9.6	201.0		cb	11.7	198.9
+5		9.9	200.7		+10	12.1	198.5
cb		9.8	200.8		S	12.8	197.8
1/2		9.7	200.9				
C		9.3	201.3		S	13.3	197.3
1/2		9.0	201.6		cb	12.4	198.2
+4		9.2	201.4		1/2	12.5	198.1
cb		9.8	200.8		C	12.1	198.5
+7		9.3	201.3		1/4	12.1	198.5

35' W

45' W

210.63

+3			12.6	198.0
cb			13.3	197.3
+6			13.1	197.5
+8			11.3	199.3
N			10.8	199.8
	50' W			
N			11.4	199.2
+15			11.9	199.7
T.P.	0.66	19824	13.05	197.58
+18			1.4	196.8
cb			1.4	196.8
+4			0.6	197.6
1/4			0.3	197.9
c			0.2	198.0
1/4			0.1	198.1
cb			0.2	198.0
+15			0.6	197.6
5			1.3	196.9
	60' W			
5			2.9	195.3

Quince

(23)
23

+15			2.9	195.3
cb			2.6	195.6
1/4			1.5	196.4
c			0.1	198.1
1/4			1.7	196.5
cb			3.0	195.2
+7			3.0	195.2
+10			0.7	197.5
N			0.7	197.8
	65' W			
N			1.6	196.6
+15			1.6	196.6
+17			3.6	194.6
cb			3.7	194.5
+3			3.1	195.1
1/4			2.3	195.9
c			2.5	195.4
1/4			2.9	195.3
cb			3.5	194.7
5			3.3	194.9

190.24

95' W

S	7.7	190.5
cb	8.5	189.7
1/4	8.6	189.6
c	8.6	189.6
1/4	8.8	189.4
cb	8.6	189.6
+12	8.3	189.9
N	7.5	190.7
120' W		
N	12.0	186.2
+10	12.6	185.6
cb	12.3	185.9
+2	13.3	184.9
1/4	13.8	184.4
c	13.9	184.3
1/4	13.0	185.2
cb	12.4	185.8
S	11.5	186.7

Quince

24

125.5' W = E side of Cement walk

S	12.45	185.79
5cb	12.89	185.35
T.P.	0.71	186.06
	12.89	185.35

137' W = W side of Cement walk

S	1.67	184.39	use this for back section on cement
S	8.1	177.7	use this for forward section
+10	2.5	183.6	use for forward section on 1/4
cb	2.30	183.76	use for back section on cement
cb	3.5	182.6	use for forward section
1/4	4.9	181.2	both sections
+3	5.8	180.3	
c	5.7	180.4	
1/4	5.5	180.6	
+2	5.6	180.5	
cb	2.8	183.3	
+2	2.1	184.0	
N	1.7	184.4	

145' W

N	2.2	183.9
---	-----	-------

186.06

+23	2.8	183.3
cb	36	182.5
1/4	7.7	178.4
c	7.9	178.2
+3	8.2	177.9
1/4	7.0	179.1
cb	5.8	180.3
+8	4.3	181.8
+15	4.7	181.4
5	9.8	176.3
170' W		
5	17.0	169.1
+10	13.7	172.4
cb	12.8	173.3
1/4	13.8	172.9
c	12.2	173.9
1/4	11.4	174.7
cb	4.3	181.8
N	3.8	182.3

Quince

25

193' W

N	5.1	180.0
cb	5.5	180.6
1/4	11.2	174.9
c	16.6	169.5
+3	17.7	168.4
1/4	18.0	168.1
cb	14.5	166.6
+12	21.9	164.2
+17	22.5	163.6
+20	21.3	164.8
5	21.5	164.6
205' W		
5	25.1	161.0
+18	25.0	161.1
cb	22.0	164.1
1/4	18.2	167.9
c	14.5	171.6
1/4	8.9	177.2
+3	6.2	179.9

186.06

Quince.

(2026)

cb 6.0 180.1

N 5.5 180.6

220 W = E.L. STATE ST 35' wide

N 5.8 180.3

cb 7.0 179.1

1/4 7.1 179.0

+3 7.2 178.9

c 11.3 174.8

1/4 15.0 171.1

cb 19.8 166.3

+7 23.9 162.2

+20 27.0 159.1

S 26.0 160.1

center of State

S 27.4 158.7

+7 24.4 161.7

+20 20.8 165.3

cb 18.6 167.5

1/4 14.3 171.8

c 8.4 177.7

1/4 7.9 178.2

cb 7.7 178.4

N 5.1 180.0

N.L. State

N 8.3 177.8

cb 8.5 177.6

1/4 8.6 177.5

c 8.8 177.3

+5 9.0 177.1

1/4 11.1 175.0

cb 17.0 169.1

+10 20.3 165.8

S 21.4 161.7

23 W.

S 22.3 163.8

+20 15.3 170.8

cb 11.7 174.4

+2 9.8 176.3

1/4 9.5 176.6

c 9.5 176.6

1/4		9.2	176.9
cb		9.1	176.0
+7		9.2	176.9
+20		9.0	177.1
N		8.9	177.2
	25' W		
N		4.5	181.6
+5		6.2	179.9
+18		8.1	178.0
cb		9.1	177.0
1/4		9.2	176.9
C		9.5	176.6
1/4		9.5	176.6
+5		9.8	176.3
cb		11.9	174.4
+5		15.5	170.6
3		22.0	164.1
	35' W		
3		19.9	166.2
+18		14.8	171.3

cb		10.3	175.8
1/4		9.9	176.2
c		9.7	176.4
1/4		9.6	176.5
cb		9.7	176.4
+1		9.7	178.4
+8		5.6	180.5
+13		3.2	182.9
N		2.5	183.6
	37' W		
N		2.5	183.6
+7	3	3.2	182.9
+12		5.2	180.9
cb		7.8	178.3
+1		9.6	176.5
1/4		9.6	176.5
c		9.7	176.4
1/4		9.9	176.2
cb		10.3	175.8
+8		14.8	171.3

186.06

Poince

28
28

S		12.9	166.2
	45' W		
S		18.6	167.5
+15		15.1	171.0
+21		10.6	175.5
cl		10.1	176.0
1/4		10.2	175.9
C		9.9	176.2
1/4		10.0	176.1
+1		9.9	176.2
+4		7.3	178.8
cl		6.5	179.6
+12		3.7	182.4
N		2.6	183.5
	70' W		
N		2.5	183.6
+10		3.6	182.5
cl		5.8	180.3
1/4		6.7	179.4
C		7.8	178.3

+5		10.6	175.5
1/4		10.6	175.5
cl		10.8	175.3
+5		10.8	175.3
+7		10.3	175.8
+12		10.1	173.0
S		11.0	172.1
	28' W		
S		13.3	172.8
+13		10.8	175.3
+16		11.9	174.2
cl		11.6	174.5
+3		11.7	174.4
1/4		9.1	177.0
C		7.4	178.7
1/4		6.6	179.5
cl		5.9	180.8
+12		4.9	181.2
N		3.8	182.3

186.06

98.5 W.

N		3.8	182.3	
+8		4.9	181.2	
cb		7.1	179.0	
1/4		8.2	177.9	
c		9.5	176.6	
1/4		11.2	174.9	
+4		11.7	174.4	
cb		11.6	174.5	
+9		11.9	174.2	
+7		10.8	175.3	
5		13.3	172.8	
T.P.	1.15	182.72	181.57	
		100' W		
N		0.0	182.7	07 step
		102 W.		
5		9.8	172.9	
+8		7.7	175.0	
+15		9.1	173.6	
cb		8.5	174.2	

90.1700

229

+3		8.4	174.3	
1/4		7.6	175.1	
c		6.2	176.5	
1/4		4.8	177.9	
cb		3.8	178.9	
+15		1.4	181.3	
N		1.3	181.4	
		103 W.		
N		1.3	181.4	
+10		1.4	181.3	
cb		2.1	180.6	
1/4		2.9	179.8	
c		3.2	179.5	
1/4		4.3	178.4	
+4		5.2	177.5	
+6		8.5	174.2	
cb		8.5	174.2	
+10		9.1	173.6	
+12		7.7	175.0	
5		9.8	172.9	

182.72

116' W

5	9.4	173.3
+8	7.6	175.1
+13	7.7	175.0
+15	10.0	172.7
cb	9.8	172.9
+1	10.1	172.6
+4	5.3	177.4
1/4	4.5	178.2
+2	3.4	179.3
0	3.3	179.4
1/4	3.1	179.6
cb	2.9	179.8
+10	2.8	179.8
N	1.8	180.9
126' W		
N	3.8	178.9
+20	4.7	178.0
cb	4.2	178.5
1/4	4.3	178.4

Quinnoc

(30)

0	4.7	178.0
1/1	5.4	177.3
+3	5.9	176.8
+6	11.2	171.5
cb	11.0	171.7
+9	11.2	171.5
+11	8.0	174.7
+18	8.0	174.7
5	9.5	173.2
145' W		
5	10.5	172.2
+8	9.5	173.2
+16	9.9	172.8
+18	13.6	169.1
cb	13.2	169.5
+3	13.1	169.6
1/4	8.0	174.7
0	7.0	175.7
1/4	7.9	174.8
cb	6.9	175.8

182.72

N			6.8	175.9
		170' W		
N			11.1	171.6
+10			10.9	171.8
cl			11.2	171.5
1/4			10.6	172.1
C			11.3	171.4
+2			11.7	171.0
T.P.	0.60	170 1/2	12.90	169.82
+6			4.6	165.8
1/4			4.5	165.9
cl			4.1	166.3
+1			4.3	166.1
+4			0.6	169.8
+12			0.2	169.2
5			1.5	168.9
		145' W		
3			5.7	164.7
+15			4.9	165.5
cl			5.0	165.4

Quince St

31

+4			4.9	165.5
+6			8.6	161.8
1/4			8.3	162.1
C			8.3	162.1
+2			8.8	161.6
+5			5.6	164.8
1/4			4.9	165.5
cl			4.6	165.8
N			4.6	165.8
		210' W		
N			8.9	161.5
+7			7.5	162.9
cl			9.0	161.4
+2			9.3	161.1
+5			11.2	159.0
1/4			10.9	159.5
C			11.0	159.4
+4			11.6	158.8
+6			8.6	161.8
1/4			8.4	162.0

170.42

cb		7.9	162.5	
S		9.1	161.3	
	215' W			
S		10.6	159.8	
+5		11.4	159.0	
cb		10.5	159.9	
1/4		11.0	159.4	
+2		12.3	158.1	
C		11.9	158.5	
1/4		11.7	158.7	
cb		12.1	158.0	
+2		11.5	158.9	
N		10.4	160.0	
	220' W = E.L. Columbia Graded.			
N		11.6	158.8	162.8
T.P.	3.43	160.81	130.4	157.38
+10		4.7	156.1	
cb		3.5	157.3	
1/4		2.9	157.9	
C		3.2	157.6	

Quince

32

1/4		3.3	157.5	
cb		4.0	156.8	
+5		4.5	156.3	
+15		6.6	154.2	
S		4.0	156.8	170.4
	16.5 W of last = E.L. Columbia St. on No. + So. as graded.			
S		8.6	152.2	
+20		7.0	153.8	
cb		7.5	153.3	
1/4		6.4	154.4	
C		5.7	155.1	
1/4		6.7	154.1	
cb		6.9	153.9	
N		6.5	154.3	

cbk

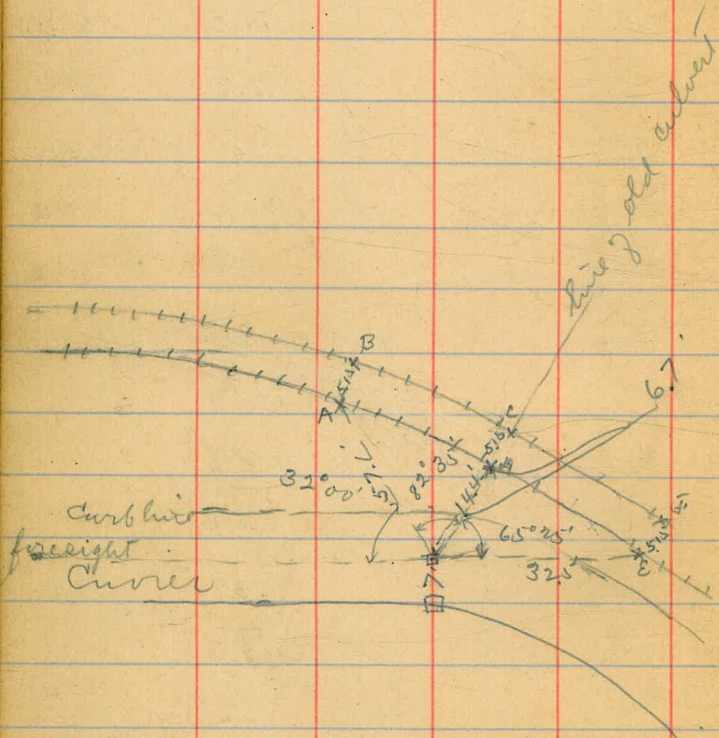
10.81

150.00

finish stake
Sta. Quince &
Columbia

Survey of track at curves

N.W. cor. Prospect & Currier 73.95



Prospect

73.95

6.18

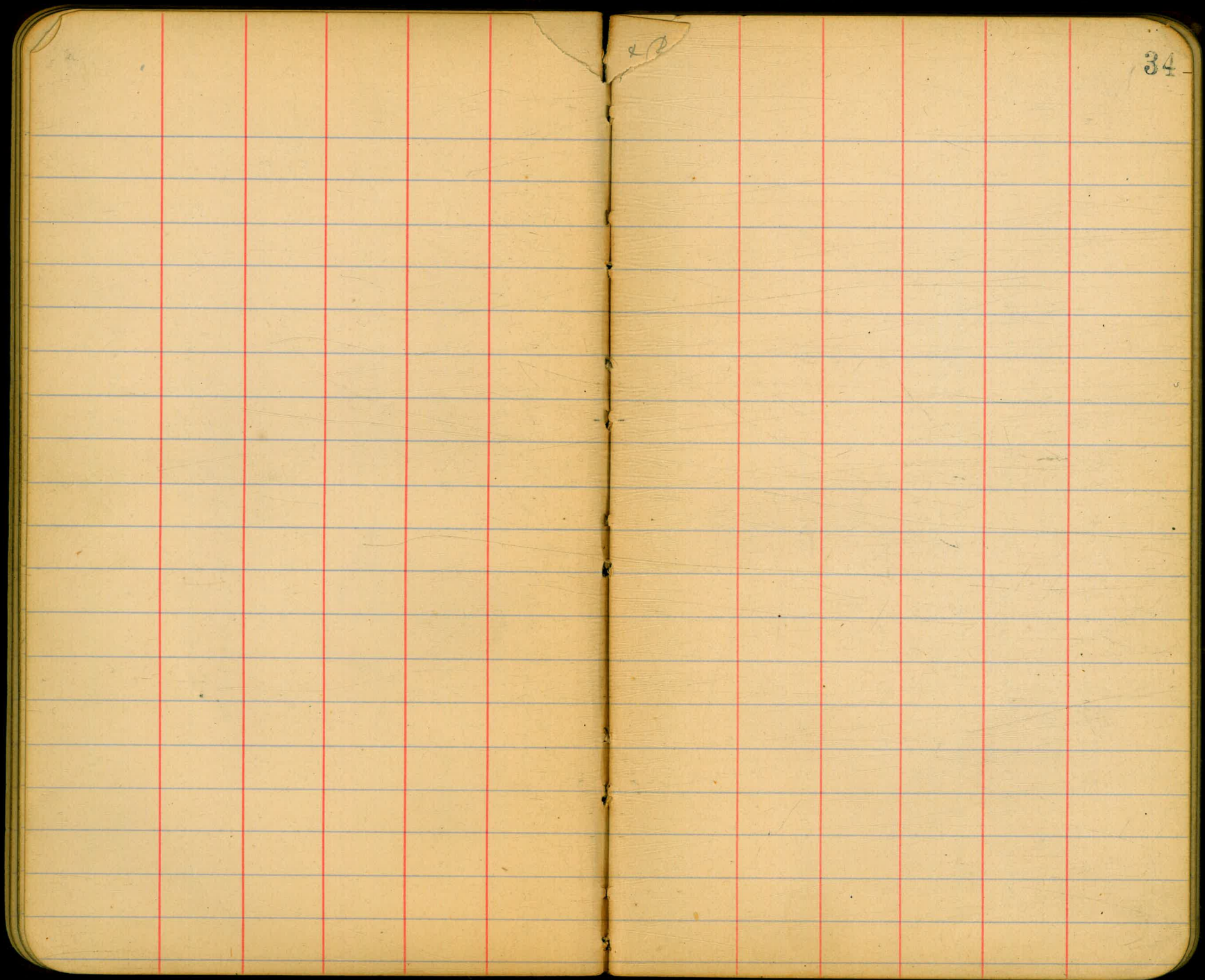
80.13 H.I.

Feb. 21/17

Lehilds
Evans
more

33
20

Sta.	H.I.		
	80.13		
A	5.12	75.01	
B	4.75	75.38	
C	4.80	75.33	
D	5.17	74.96	
E	5.13	75.00	
F	4.73	75.40	
return	5.15	74.98	

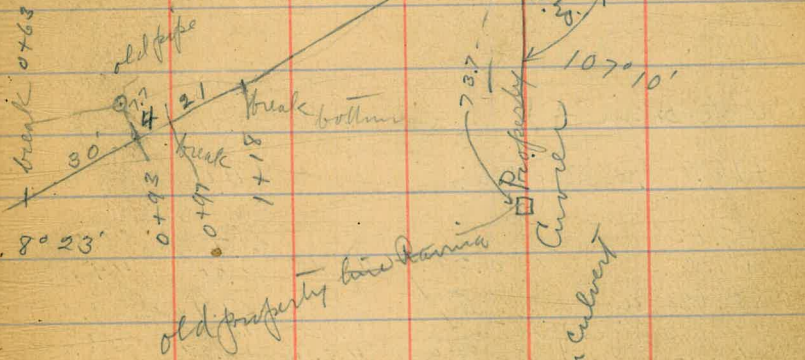
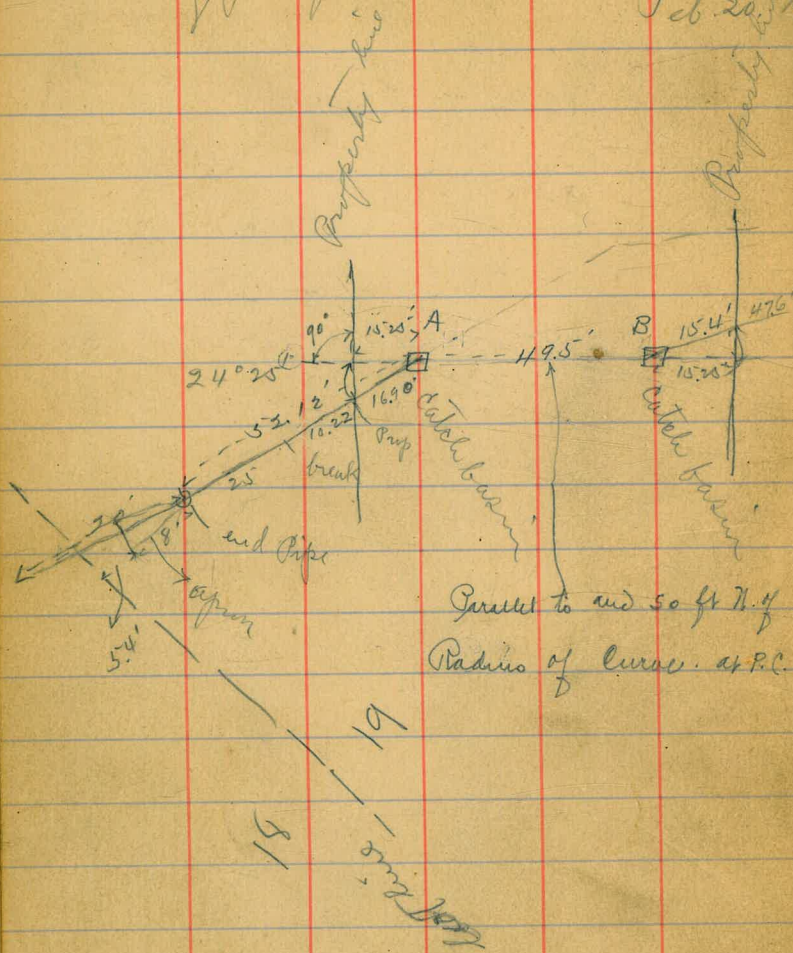


34

Survey of culvert in campus
south of Prospect St.

Feb 20, 1917

across Fayella Blvd.
Shields
Evans
Moore



(35)

see page 66

Levels for culvert

J.P.		H.I.		
	0.93	62.13	61.20	
Sta.				
Catch Basin A		Top of - 4.0	58.1	
		Top gate - 5.60	56.53	
+16.9	S.W. Property line	4.4	57.7	
+27.12	break	6.7	55.4	
J.P.	0.27	49.60	12.90	49.33
+52.12	end of present pipe culvert center	Top curb 9.7	39.9	
J.P.	8.41	45.14	12.87	36.0
+60.12	end of pipe	Top apron 10.2	34.9	
		ground - 10.7	34.4	
+72.12	bottom of camfer	11.0	34.1	
		(62.13)		
Catch Basin B		Top curb 3.13	59.0	
		Top gate - 4.13	58.0	
+15.4	N.E. Property line	cut bank 2.8	59.3	
		1.8	60.3	
+63		H.I.	1.1	61.0
J.P.	3.96	53.22	12.87	49.26
+93	opposite end of old culvert line	7.7	8.4	44.8
+97	break	10.1	43.1	
+118	bottom of camfer	12.6	40.6	
+88		9.5	43.7	
2+90.15	hub. S.W. property of Currier Street	7.3	45.9	

5.4

36

Sta		H.I.		
3+05		53.22	3.3	49.9
+24			5.4	47.8
+55	bottom of camfer		4.0	49.2
+59	hub. in small bank		3.12	50.10

56.53

X sect. Eads. ave. from
Coast Blvd. south 50' street

J.P. 0.75 ^{42.} 88.66 87.91

level on R.R. rails on line of culvert across
Prospect at ends ^{rod} inside 1.69 ^{rod} outside 1.54
Elev. 86.97 Elev. 87.12

west line prospect street

So. line

2.9 85.8

3.1 85.6

3.1 85.6

C

3.3 85.4

3.3 85.4

3.1 85.6

no. line

2.4 86.3

25' rd.

no. line

5.7 83.0

6.3 82.4

6.1 82.6

C

6.1 82.6

6.0 82.7

5.9 82.8

5.7 83.0

So. line

Prospect Street to no. 6117 ⁽³⁷⁾ to child
Eads
moore
6' walk on south 20' walk on north 6' quarters.

BM. S.E. prospect + Eads.

50' W.

saline

8.7 80.0

8.9 79.8

9.2 79.5

9.4 79.3

9.4 79.3

9.4 79.3

no. line

8.1 80.6

no. line

10.3 78.4

12.3 76.4

12.4 76.3

12.5 76.2

12.3 76.4

12.2 76.5

12.1 76.6

no. line

70' rd.

T.P. 0.88 ^{H.I.} 76.78 12.76 75.90

center walk (drifts outage) 83.5' W.

no. line	1.50	75.3
	1.64	75.1
	1.7	75.1
C	1.7	75.1
	1.5	75.3
	1.4	75.4
no. line	-0.6	77.4

100' W.

no. line	1.0	75.8
	3.4	73.4
	3.7	73.1
C	3.7	73.1
	3.7	73.1
	3.5	73.3
no. line	3.3	73.5

76.78

125' W.

no. line	6.8	70.0
	7.0	69.8
	7.1	69.7
C	7.0	69.8
	7.0	69.8
	6.6	70.2
no. line	3.9	72.9

150' W.

no. line	7.7	69.1
	9.9	66.9
	10.3	66.5
C	10.7	66.1
	10.4	66.4
	10.5	66.3
no. line	10.5	66.3

76.78

H.I.

1.13 65.34 13.57 64.21

200' W.

Center auto. drive (not lined) 169' W.

no. line

1.6 63.7

no. line

5.3 60.0

1.7 63.6

5.2 60.1

1.7 63.6

c

5.2 60.1

c

1.5 63.8

5.1 60.2

1.3 64.0

5.5 59.8

1.2 64.1

no. line

5.7 59.6

no. line

-1.2 66.5

225' W.

lower edge drive 175' W.

no. line

4.6 60.7

no. line

0.2 65.1

9.2 56.1

1.9 63.4

9.0 56.3

2.0 63.3

c

9.0 56.3

c

2.0 63.3

9.0 56.3

2.0 63.3

8.7 56.6

2.3 63.0

no. line

8.5 56.8

no. line

2.0 63.3

8.4 56.9

65,34

250' W.

no. line		11.7	53.6
		12.0	53.3
		12.2	53.1
c		12.2	53.1
		12.3	53.0
		12.4	52.9
no. line		12.3	53.0
J.P.	0.35	53.31	52.96

275' W.

no. line		3.5	49.8
+ 1/2		3.4	49.9
		4.3	49.0
		4.6	48.7
		4.6	48.7
c		4.4	48.9
		4.3	49.0
		4.1	49.2
no. line		3.2	50.1

53,31

40

300' W.

no. line		6.2	47.1
+ 1'		7.6	45.7
		8.1	45.2
		8.4	44.9
c		8.5	44.8
		8.0	45.3
		8.2	45.1
		8.8	44.5
		6.6	46.7
		6.6	46.7

300' W. (Cement floor Garage)

no. line		7.0	46.3
+ 1'		7.0	46.3
+ 1/2		9.3	44.0
		8.9	44.4
		8.6	44.7
c		9.2	44.1
		9.7	43.6
		9.4	43.9
no. line		9.3	44.0

5331

318' AN.

So. line	cement	9.6	43.7
	cement	9.9	43.4
	cement	10.1	43.2
C		10.1	43.2
		9.7	43.6
		9.8	43.5
		9.9	43.4
no. line		7.5	45.8
		8.2	45.1

320' W.

no. line		10.1	43.2
		10.0	43.3
		9.9	43.4
C		10.2	43.1
		10.3	43.0
		9.9	43.4
So. line		9.7	43.6
		7.5	45.8

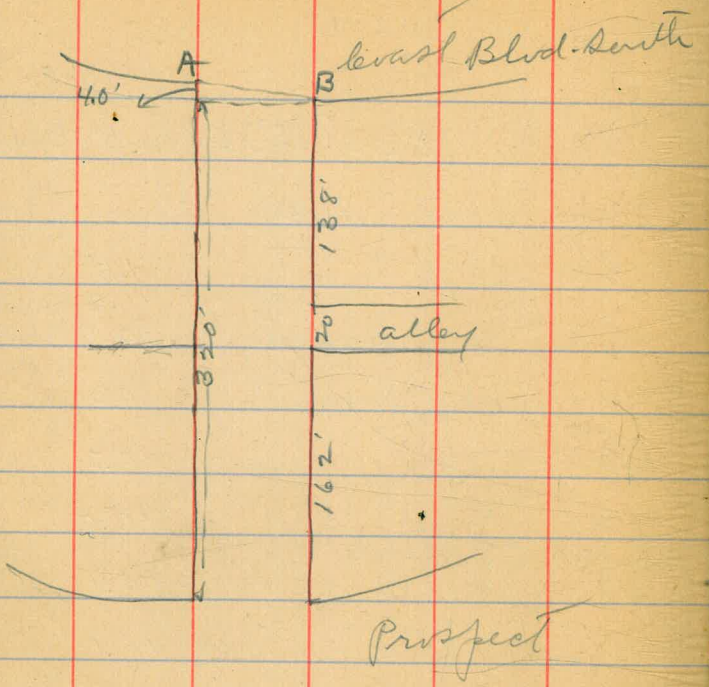
5331

41

East line, East Blvd. South

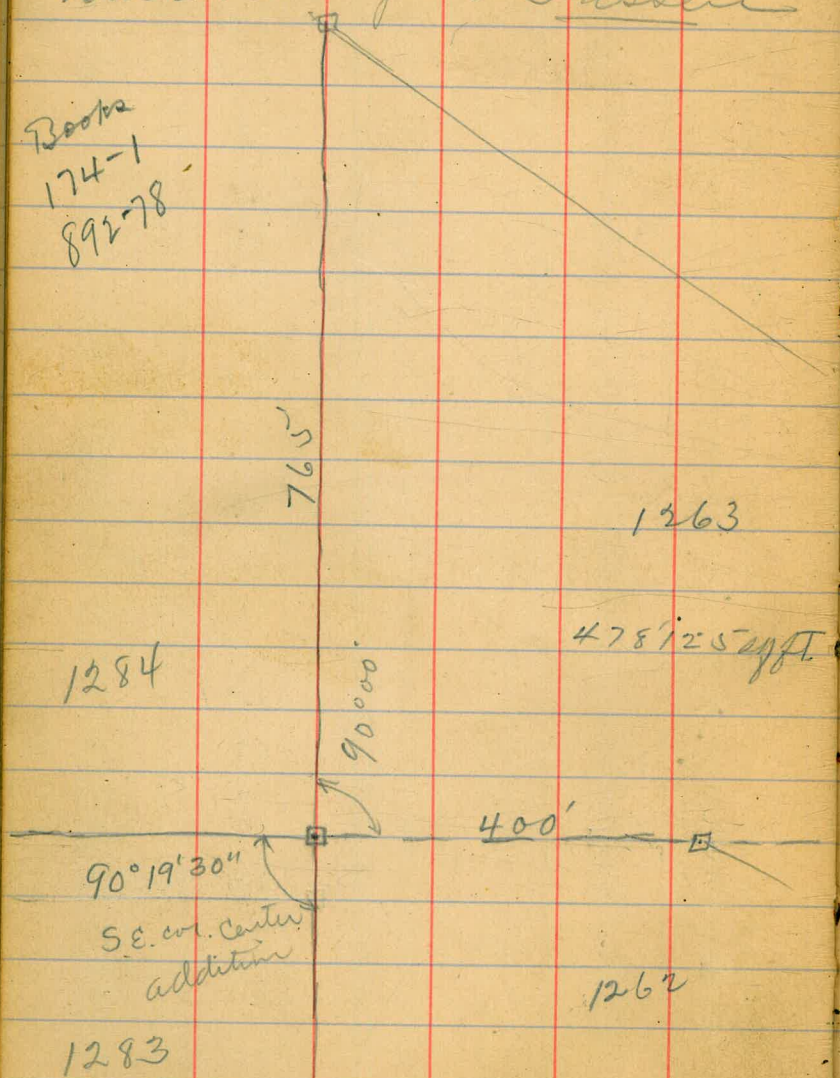
sect. A B

So. line		7.6	45.6
+1'	cement	10.0	43.3
	cement	10.1	43.2
	cement	10.2	43.1
C		10.2	43.1
		10.0	43.3
		10.1	43.2
no. line		10.1	43.2
		10.3	43.00



Survey of acreage of
which belongs to Gassen

Books
174-1
892-78

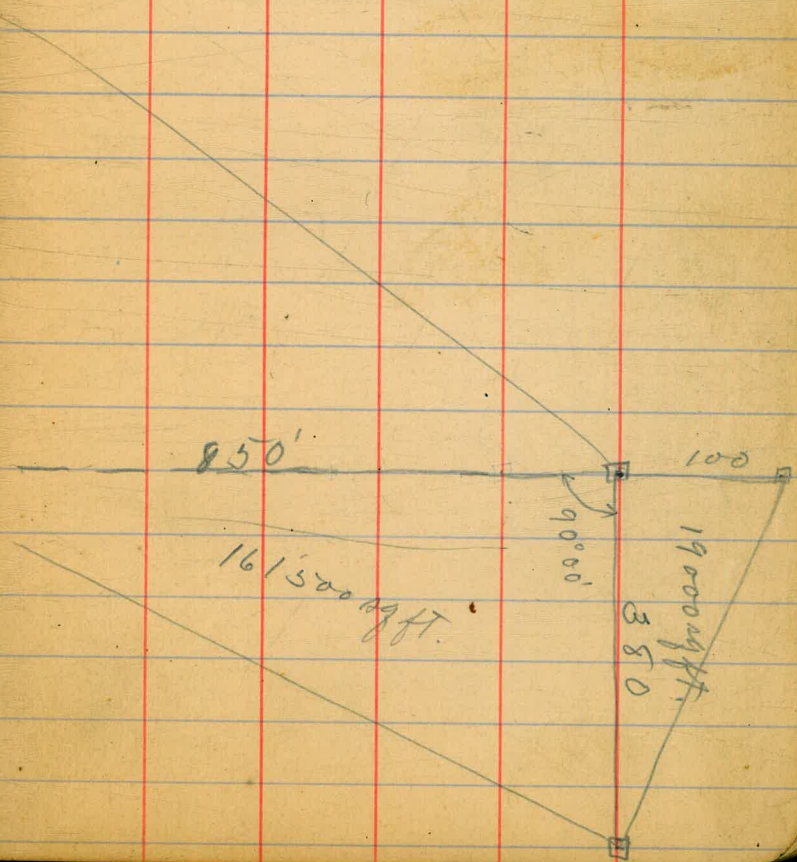


Golf Club
Mar. 30 / 17

Childs 43
Evans
moore

Pueblo 1263 478,125 sq ft.
" 1262 180,500 sq ft.
658,625

658,625 sq ft = 15.1 acres.



44

8/17

CROSS SECTION OF
The So. 30' feet of VINE ST. (80' wide)
from the West Line of Columbia
to the West Line of State
10' Sidewalk on South Side
10' Quarter Centers on
Original Center
of Street

B.M.	11.67	81.23	70.06	NW India 27.11/20
T.P.	12.96	93.24	1.15	70.28 NCT NW Vine + India
T.P.	13.19	106.16	0.21	93.03
T.P.	12.73	118.46	0.43	105.73

West Line Columbia St. 75' wide
12' walks
12.75' / 10.5'

3		6.9	111.6
+7		7.3	111.2
		8.2	110.3
cb.		8.5	110.0
1/2		8.4	110.1
+3		8.3	110.2
+5		7.6	110.9
-0		11.0	107.5
+2.5		27.0	91.5
+3.5		30.3	88.2

West Curb.

-35		27.7	90.8
-20		23.1	95.4
C		9.9	108.6
+7		6.9	111.6

118.5

45

1/2		7.1	111.4
cb		7.5	111.0
30.		7.8	110.7

Curb + 6

30.		7.1	111.4
cb		7.3	111.2
1/2		6.8	111.7
+3		7.0	111.5
+4		7.3	111.2
C		10.2	108.3
+17		21.4	97.1
+25		26.1	92.9

Curb + 7

-35		25.9	92.6
-17		21.4	97.1
C		14.2	104.3
+6		13.5	105.0
+7		7.4	111.1
1/2		7.0	111.5
cb		7.3	111.2

118.46

5		7.1	111.4
	Curb + 9		
5		7.1	111.4
cb		7.2	111.3
1/4		7.2	111.3
+3		7.6	110.9
+4		13.5	105.0
C		14.3	104.2
+17		21.0	97.5
+35		25.3	93.2
	West Quarter		
-35		24.8	93.7
-17		20.4	98.1
-5		16.2	102.3
C		14.3	104.2
1/4		7.4	111.1
cb		7.2	111.3
5		6.9	111.6
	Quarter + 2		
5		6.5	111.7

119.5

VINE

46

cb		7.1	111.4
1/4		7.2	111.3
C		13.1	105.4
+5		15.6	102.9
+17		19.6	98.9
+35		24.5	94.0
	Quarter + 4		
-35		24.5	94.0
-17		19.3	99.2
-5		12.4	106.1
C		9.1	109.4
1/4		7.3	111.2
cb		7.1	111.4
5		6.8	111.7
	Center		
5		6.5	112.0
cb		6.8	111.7
1/4		7.0	111.5
+5		7.1	111.4
C		8.7	109.8

118.46

+10		14.7	103.8
	Center + 6		
-10		14.0	104.5
C		8.3	110.2
+7		6.7	111.8
$\frac{1}{4}$		6.7	111.8
cb		6.7	111.8
5		6.5	112.0
	Center + 8		
5		6.5	112.0
cb		6.6	111.9
$\frac{1}{4}$		6.8	111.7
+3		9.0	109.5
C		11.0	107.5
+10		13.8	104.7
	Center + 11		
-10		12.9	105.8
C		10.4	108.1
+7		8.5	110.0
$\frac{1}{4}$		7.2	111.3

118.5VINE

47

cb		6.4	112.1
5		6.5	112.0
	East Quarter		
5		6.5	112.0
cb		6.4	112.1
$\frac{1}{4}$		6.6	111.9
+3		6.7	112.8
C		7.6	110.9
+10		12.5	106.0
	East Curb		
5		6.3	112.2
$\frac{1}{4}$		5.9	112.6
cb		5.9	112.6
5		6.1	112.4
	E.L. COLUMBIA		
5		5.6	113.5
+3		3.8	114.7
cb		4.1	114.4
$\frac{1}{4}$		4.5	114.0
C		4.7	113.8

118.46

2' East

C	4.5	114.0
1/4	4.3	114.2
cb	3.6	114.9
+9	2.7	115.8
5	2.8	117.7

T.P.	12.75	130.74	0.47	117.99
------	-------	--------	------	--------

25' E

5	9.2	121.5
+1	10.3	120.4
cb	10.9	119.8
+4	10.9	119.8
+6	12.3	118.4
1/4	13.8	116.9
+4	14.8	115.9
C	15.8	114.9
+10	16.8	113.9

50' E

-10	14.4	116.3
C	13.7	117.0

130.7

VINE.

48

+5	12.5	118.2
1/4	10.5	120.2
+5	8.1	122.6
+8	5.8	124.9
cb	5.9	124.8
5	5.7	125.0

60' E

5	4.3	126.4
cb	4.2	126.5
1/4	5.3	122.4
+7	12.8	117.9
C	12.9	117.8
+10	14.1	116.6

67' E

-10	13.2	117.5
C	12.1	118.6
1/4	5.6	125.1
+7	2.8	127.9
cb	2.8	127.9
5	3.2	127.5

This bank
already cut 3'This bank
already cut 3'

130.74

75' E

5	1.8	128.9
cb	1.5	129.2
+4	1.2	129.5
1/4	3.9	126.8
C	7.8	122.9
+10	11.6	119.1

100' E

-15	7.2	123.5
C	3.1	127.6
TP	8.95	139.45
1/4	0.21	130.53
	7.2	132.3
+3	6.0	133.5
cb	6.1	133.4
5	5.6	133.9

= dirt runway
to garage 50.50

125' E

5	2.6	136.9
cb	4.7	134.8
1/4	5.3	134.2
C	8.9	130.6

139.5

VINE

+15

135 126.0

150' E

-20	140	125.5
C	7.5	132.0
1/4	3.9	135.6
cb	3.1	136.4
5	0.8	138.7

T.P.

7.92

146.66 0.74 138.74

175' E

5	3.9	142.8
+6	5.0	141.7
+7	6.8	139.9
cb	6.8	139.9
+6	7.5	139.2
1/4	8.5	138.2
C	11.5	135.2
+2.5	22.8	123.9

200' E = N.L. STATE (as is.)

-35	26.2	120.5
C	11.2	135.5

1/4			6.9	139.8
-----	--	--	-----	-------

+7			3.5	143.2
----	--	--	-----	-------

cb			3.3	143.4
----	--	--	-----	-------

+7			2.8	143.9
----	--	--	-----	-------

5			1.02	145.64
---	--	--	------	--------

446 511.
state

212.5 F = 114.0x state as contemplated.

5			1.2	145.5
---	--	--	-----	-------

cb			1.8	144.9
----	--	--	-----	-------

1/4			6.6	140.1
-----	--	--	-----	-------

C			11.5	135.2
---	--	--	------	-------

on T.P.	0.30	145.94		145.64
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T.P.	0.31	134.03	12.72	133.22
------	------	--------	-------	--------

Gregory
Moore
Miller

CROSS SECTION OF
The Center 50 ft
of STATE ST
from 15' No. of The No.
of Vine St to the
S.L. of Upper St

E & W. are points
10' wide
7.5' / 6's
25' from Ctr
of State

New Notes Book 1001
Page 74

134.0

51

				+10		1.8	132.2	
on T.P.	0.30	145.94	145.64	T.P.	12.64	145.86	0.81	133.22
T.P.	0.51	132.03	12.72					5' No. of Ctr. of Vine = N. of Vine as contemplated
		15' No. of N. Vine St						
-10		1.3	132.7	-20		6.3	139.6	
E		4.6	129.4	E		7.3	138.6	
cb		7.5	126.2	cb		7.2	138.7	
1/2		9.5	124.2	1/4		7.3	138.6	
C		12.6	121.4	C		7.9	138.0	
1/4		13.8	120.2	1/2		8.5	137.4	
cb		14.5	119.5	cb		9.7	136.2	
W		14.5	119.5	W		10.7	135.2	
		5' No. of N. Vine St						10' So. of N. as contemplated
-12.5		10.0	124.0	W		5.9	140.0	
W		9.7	124.3	cb		4.8	141.1	
cb		8.6	125.4	1/2		4.0	141.8	
1/4		8.4	125.6	0		3.4	142.5	
C		7.5	126.5	1/4		2.7	143.2	
1/4		6.9	127.1	1/2		3.0	142.9	
cb		7.1	126.9	E		3.9	142.0	
E		5.3	128.7			4.0	141.9	

145.86

TP.	12.62	158.26	0.22	145.64
10' So. of last = So. Curb of Vine St				
-10		12.9		145.4
E		12.6		145.7
cb		11.5		146.8
1/4		12.1		146.2
C		12.2		146.1
1/6		13.3		145.0
cb		13.8		144.5
W		13.6		144.7
So. Line of Vine St				
W		12.8		145.5
cb		11.4		146.9
1/4		10.7		147.6
C		9.6		148.7
1/6		9.5		148.8
cb		8.5		149.8
E		8.5		149.8
+10		7.9		150.4

Ctr 50 of State

152.3

52

10' So.

E		5.1		153.2
cb		6.3		152.0
1/4		6.6		151.7
C		8.7		149.6
1/6		10.0		148.3
cb		9.8		148.5
W		10.0		148.3
20' So.				
W		8.2		150.1
cb		7.5		150.8
1/4		6.7		151.6
C		7.0		151.3
1/6		6.3		152.0
cb		5.4		152.9
E		3.7		154.6
35' So.				
E		2.1		156.2
cb		3.1		155.2
1/4		3.7		154.6

158.26

C	4.2	154.1
1/4	5.1	153.2
cb	5.9	152.4
W	7.2	151.1
50' 30		
-12.5	6.9	151.4 = bank
	11.4	146.9 = Elev. of yard & ^{house} yard is level
W	5.8	152.5
cb	4.6	153.7
1/4	3.7	154.6
C	2.6	155.7
1/4	1.8	156.5
cb	1.2	157.1
E	0.5	157.8
70' 30		
E	+0.4	158.7
cb	0.8	157.5
1/4	1.5	156.8
C	2.4	155.9
1/4	3.3	155.0
cb	4.3	154.0

158.3

STATE

53

W	5.3	153.0
80' 30		
W	5.7	152.6
cb	5.2	153.1
1/4	4.5	153.8
C	3.6	154.7
1/4	2.5	155.8
cb	1.5	156.8
E	1.0	157.3
90' 30		These Notes OK from here South
E	5.3	153.0
cb	6.2	152.1
+3	4.6	153.7
1/4	4.3	154.0
C	5.3	153.0
1/4	6.1	152.2
cb	6.7	151.6
W	7.2	151.1
102' 30		
-12.5	11.1	147.2 graded yard

158.26

W		10.3	148.0
cb		10.3	148.0
1/4		10.1	148.2
C		10.0	148.3
1/4		9.8	148.5
cb		9.7	148.6
E		9.3	149.0
+10		7.0	151.3
	108' So		
-15		7.1	151.2
E		11.2	147.1
cb		12.1	146.2
1/4		11.4	146.9
C		12.2	146.1
1/4		12.0	146.3
cb		12.2	146.1
W		12.2	146.1
-12.5		11.2	147.1 = So. End of yard
T.P	0.46	13.07	145.19

145.6

STATE

54

			116' So		
		-12.5		2.1	143.5 = graded yard
W				2.5	143.1
cb				3.0	142.6
1/4				1.7	143.9
+7				1.5	144.1
C				3.6	142.0
1/4				4.7	140.9
cb				5.0	140.6
E				4.1	141.5
+15					
12.5 W. of 11.6			125' So	+3.8	149.5
				2.7	142.9 = End of Mark to house
			132' So		
-15				+3.1	148.8
-5				3.5	142.1
E				4.5	141.1
cb				5.1	140.2
1/4				6.4	139.2
C				7.0	138.6
1/4				7.7	137.9
cb				7.2	138.4

145.65

N	6.7	139.0
+7	2.6	143.0
+15	2.7	143.0 = yard
145' So		
-20	3.1	142.5 = yard
-13	6.2	139.4
W	11.0	134.6
cb	10.6	135.0
1/4	9.0	136.6
C	7.9	137.7
+4	2.0	138.6
1/4	4.2	141.4
cb	3.0	142.6
E	2.4	143.2
+7	0.8	144.8
+15	+3.2	149.0
150' So		
-15	+4.8	150.4
-7	+2.0	147.6
E	+0.6	146.2

145.6

STATE

55

cb	2.0	143.6
1/4	4.1	141.5
C	6.3	139.3
+2	8.0	137.6
1/4	9.0	136.6
cb	10.6	135.0
W	12.1	133.5
+5	11.5	134.1
+10	9.5	136.1
+20	3.5	142.1
T.P.	11.71	154.65
		142.94
158' So		
-25	20.0	134.6 on walk to side
-12.5	20.3	134.3 at house
	21.8	132.8 house 40' from 1100
W	21.2	133.4
cb	18.8	135.8
1/4	15.2	139.1
C	14.1	140.5
1/4	12.1	142.5
cb	9.5	145.1

154.65

E	6.1	148.5	
+15	2.0	152.6	
	165 30		
-8	0.2	154.4	
E	2.9	151.7	
cb	6.5	148.1	
1/4	2.6	145.0	
C	4.8	142.8	
1/4	13.4	141.2	
+6.5	1.6	140.0	
cb	17.4	137.2	
W	14.3	135.3	OK
+12.5	20.0	134.6	New OK
+7	23.5	130.8	
+12.5	24.1	130.5	
+12.5	19.9	134.7	use this for back section only
+12.5	24.1	130.5	use this for normal sect.
+3.5	20.2	134.4	use this for back sect.
+3.5	26.2	128.4	use this for normal sect.

N.E
4-10-26

154.65

STATE

56

180 30

-40	27.5	127.1	
-12.5	24.5	130.1	
-3	22.8	131.8	
W	17.2	137.4	
cb	11.8	142.8	
1/4	9.0	145.6	
C	5.7	149.0	
1/4	3.6	151.0	
cb	158.0	1.1	153.5
T.P.	5.83	157.96	2.52
E		2.2	155.8
	175 30		
E	1.5	156.5	
cb	3.5	154.5	
1/4	5.2	152.8	
C	8.0	150.0	
1/4	10.2	147.5	
cb	13.5	144.5	
W	23.4	134.6	

157.96

158.0

+5	25.8	132.2
+12.5	28.4	129.6
+40	30.0	128.0

195.50

-40	30.0	128.0
-14	29.2	128.8
-3	23.0	135.0

W	16.9	141.1
---	------	-------

cb	9.5	148.5
----	-----	-------

1/4	7.0	151.0
-----	-----	-------

c	5.9	152.1
---	-----	-------

1/4	4.2	153.8
-----	-----	-------

cb	2.6	155.4
----	-----	-------

E	0.6	157.4
---	-----	-------

202.50

E	0.5	157.5
---	-----	-------

cb	1.9	156.1
----	-----	-------

1/4	3.4	154.6
-----	-----	-------

c	5.0	153.0
---	-----	-------

1/4	2.5	151.5
-----	-----	-------

158.0

STATE

57

cb	8.0	150.0
----	-----	-------

W	11.3	146.7
---	------	-------

+10	16.1	141.9
-----	------	-------

+12.5	25.7	132.3
-------	------	-------

+17.0	29.5	128.5
-------	------	-------

+40	30.0	128.0
-----	------	-------

215.50

-40	29.4	128.6
-----	------	-------

-33	29.2	128.8
-----	------	-------

-33	21.2	136.8
-----	------	-------

-15	23.4	129.6
-----	------	-------

-12.5	21.4	136.6
-------	------	-------

-11.5	12.3	145.7
-------	------	-------

W	9.7	148.3
---	-----	-------

cb	7.0	150.6
----	-----	-------

1/4	5.9	152.1
-----	-----	-------

c	4.7	153.3
---	-----	-------

1/4	3.2	154.8
-----	-----	-------

cb	2.0	156.0
----	-----	-------

E	0.1	157.6
---	-----	-------

use 4/5 for
back sectionon porch of
house for
forward sect
onlyuse for back
section onlyon porch yard
of house
use for forward
section only
on bank above
house

injured

157.96

158.0

274' 50

E	1.0	157.0
cb	3.3	154.7
1/4	5.3	152.7
C	7.9	150.1
1/4	10.6	147.4
cb	14.0	143.6
+3	19.1	138.9
W	19.2	138.8
+12.5	23.0	135.0
+22.0	26.5	131.5
277' 50		
-22	26.7	131.3
-12.5	23.0	135.0
W	17.6	140.4
cb	13.3	144.7
1/4	10.4	147.6
C	7.1	150.9
1/4	4.3	153.7
cb	2.5	155.5

STATE

59

E	0.7	157.3
290' 50		
TR	6.63	163.69
E	0.40	157.06
E	5.9	157.8
cb	7.9	155.8
1/4	9.2	154.5
C	10.9	152.8
1/4	13.2	150.5
cb	17.3	146.4
W	20.9	142.8
+12.5	26.7	137.0
+22	31.4	132.3
300' 50		
-20	26.6	137.1
-12.5	22.8	140.9
W	19.0	144.7
cb	16.0	147.7
1/4	13.9	150.0
C	11.2	152.5
1/4	9.1	154.6

163.69

dt	7.8	155.9
E	6.0	157.7
310 So		
E	5.6	158.1
dt	7.1	156.2
1/4	8.6	155.1
C	9.9	153.8
1/2	11.3	152.4
dt	12.8	150.9
W	15.8	147.9
+12.5	18.8	144.9
320 So		
-12.5	17.2	146.5
W	14.1	149.3
dt	11.1	152.6
1/4	9.3	154.4
C	8.9	154.8
1/4	7.7	156.0
dt	6.6	157.1
E	4.9	158.8

163.7

STATE

60

335 So			
E	2.6	161.1	
dt	4.3	159.4	
1/4	6.2	157.5	
C	7.9	155.8	
1/4	9.0	154.7	
dt	10.4	153.3	
W	12.6	151.1	
+12.5	14.8	148.9	
345 So = N.L. DPAS St 50 wide roads			
-12.5	14.2	149.5	
W	11.1	152.6	
dt	8.5	155.2	
1/4	7.2	156.8	
C	6.1	157.6	
1/4	4.3	159.4	
dt	2.8	160.9	
E	0.8	162.9	
T.P.	12.15	171.66	2.48

159.21 = Mon Ctr
 State USGS
 8100442 elev
 = 159.01

No. Curb

E	66	165.0
cb	91	162.5
1/4	10.6	161.0
c	12.2	159.5
1/4	13.3	158.4
cb	15.0	156.7
W	18.0	153.7
+12.5	22.4	149.3

No. Quarter

-12.5	22.2	149.5
W	17.4	154.3
cb	13.9	157.8
1/4	12.2	159.5
c	10.7	161.0
1/4	9.3	162.4
cb	8.2	163.5
E	5.5	166.2

Center

E	4.7	167.0
---	-----	-------

cb	7.0	164.7
1/4	8.2	163.5
c	9.7	162.0
1/4	10.6	161.1
cb	12.5	158.9
W	16.3	155.4
+12.5	21.4	150.3

So Quarter

W	12.3	159.4
cb	11.3	160.4
1/4	9.0	162.7
c	8.0	163.7
1/4	6.6	165.1
cb	5.4	166.3
E	3.2	168.5

So Curb

E	1.6	170.1
cb	4.0	167.7
1/4	5.4	166.3
c	6.9	164.8

171.66

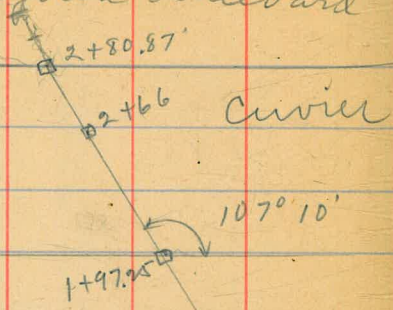
STATE

62

1/4	78	163.9
ab	91	162.6
W	110	160.7
So Line Wpas St.		
W	96	162.1
ab	80	163.7
1/4	65	165.2
c	54	166.3
1/4	39	167.8
ab	26	169.1
E	0.7	171.0

8m 9
5/11/17

X Sect. for culvert from
 of slope at Lafolla boulevard



to (see page 35) may 8/17
 to north line of Cuvier

leholds
 Evans 66
 Moore
 83.62
 197.25
 280.87
 359
 266

$$1+97.25 = 2+90.25 \text{ page 35}$$

$$2+66 = 3+59 \quad " \quad "$$



--- curb line

Lafolla Blvd.

Sta.	2.07 center E. Culvert	Rod 62.3 1.0	H.I. 63.27	center culvert	Rod	61.20	BM.	west of c culvert	Rod
0+00	+23			0+00	18.3'	45.0	+50'	0.0	63.3
							+42	4.8	58.5
							+27	11.4	51.9
							+17	17.4	45.9
+04	+23	1.0					+7	19.0	44.3
		62.1							
+04	+23	1.2	0.00	20.0	43.3		+50	0.0	63.3
							+42	4.8	58.5
							+27	10.6	52.7
							+8	22.6	40.7
+25	+8'	42.5	0.00	22.3	41.0		+44	0.0	63.3
		20.8					+37	3.2	60.1
		34.3					+22	7.9	55.4
	+25	9.0					+9	17.0	46.3
		61.1					+4	18.8	44.5
	+36	2.2							

63,27

Sta.	East side of culvert	Rod	Center of culvert	Rod	
0+50	+4'	42.1 21.2 44.0 79.3 45.8 17.5 50.9 12.4 60.4 2.9	000	22.0	41.3
	+7'				
	+17				
	+25				
	+40				
0+75	+12	46.1 17.2 54.3 9.0	0+00	20.1	43.2
	+25				
1+00	+21	55.9 7.4 47.1 16.2	0+00	16.4	46.9
	+9				
1+25	+25	57.4 5.9 48.5 14.8	0+00	17.2	46.1
	+10				

63,27

68

	West side of culvert	Rod	
+2'	20.6	42.7	
+6'	19.8	43.5	
+13	13.5	49.8	
+20	6.5	56.8	
+30	4.1	59.2	
+40	0.0	63.3	
+8'	20.4	42.9	
+15'	15.3	48.0	
+17	5.9	57.4	
+52	0.4	62.9	
+29	1.6	61.7	
+19	5.9	57.4	
+9	17.4	45.9	
+4	20.1	43.2	
+15	6.9	56.4	
+13	15.9	47.4	
+3	19.5	43.8	

63, 27

Sta	East center of culvert	Rod	Antery culvert	Rod	
1+50	+2'	45.3 18.0	0+00	5.2	59.1
	+4'	48.1 15.2			
	+12	49.2 14.1			
	+25	55.0 8.3			
1+75	+26	55.6 7.7	0+00	18.0	45.3
	+10	48.4 14.9			
	+2'	47.4 15.9			
1+97.25	+1'	48.6 14.7	0+00	17.3	46.0
Ro. line of creek	+7'	62.5 0.8			
	+20'	51.8 5.3			
2+19	+23	El. 67.8 -4.3	0+00	15.1	48.2
	+14'	60.1 3.2			
	+10'	56.9 6.4			
	+6	51.1 12.2			
J.P.		5.09	H.I. 64.72	3.64	59.63

69

West center of culvert	Rod	
+23	2.5	60.8
+13	14.7	48.6
+24	1.7	61.6
+20	7.5	55.8
+7'	15.6	47.7
+5'	17.0	46.3
+17'	5.1	58.2
+6'	17.0	46.3
+17'	2.0	61.3
+12	6.9	56.4
+4'	16.4	46.9
+2'	15.1	48.2

64,72

Sta	East center of culvert Rod	Center of culvert Rod		
2+50	+20	64.7 0.0	0+00	16.2 48.5
	+15	59.3 5.4		
	+10	54.3 5.4		
	+9	51.3 13.4		
	+5'	49.9 14.8		
	+2'	48.3 16.4		
2+66	+20	56.4 8.3	0+00	14.1 50.6
	+9	51.9 12.8		
	+8'	50.4 14.3		
	+5'	49.0 15.7		
2+80.87	+5'	49.0 15.7	0+00	12.3 52.4
No. line of Culvert at.	+7'	51.3 13.4		
	+19	53.6 11.1		
	+25	55.7 9.0		
	+32	58.9 5.8		

70

West Center of culvert Rod		
+13	-3.0	67.7
+7'	0.2	64.5'
+2'	16.0	48.7
+20	-1.3	66.0
+6'	11.2	53.5'
+11	3.2	61.5
+17	0.0	64.7

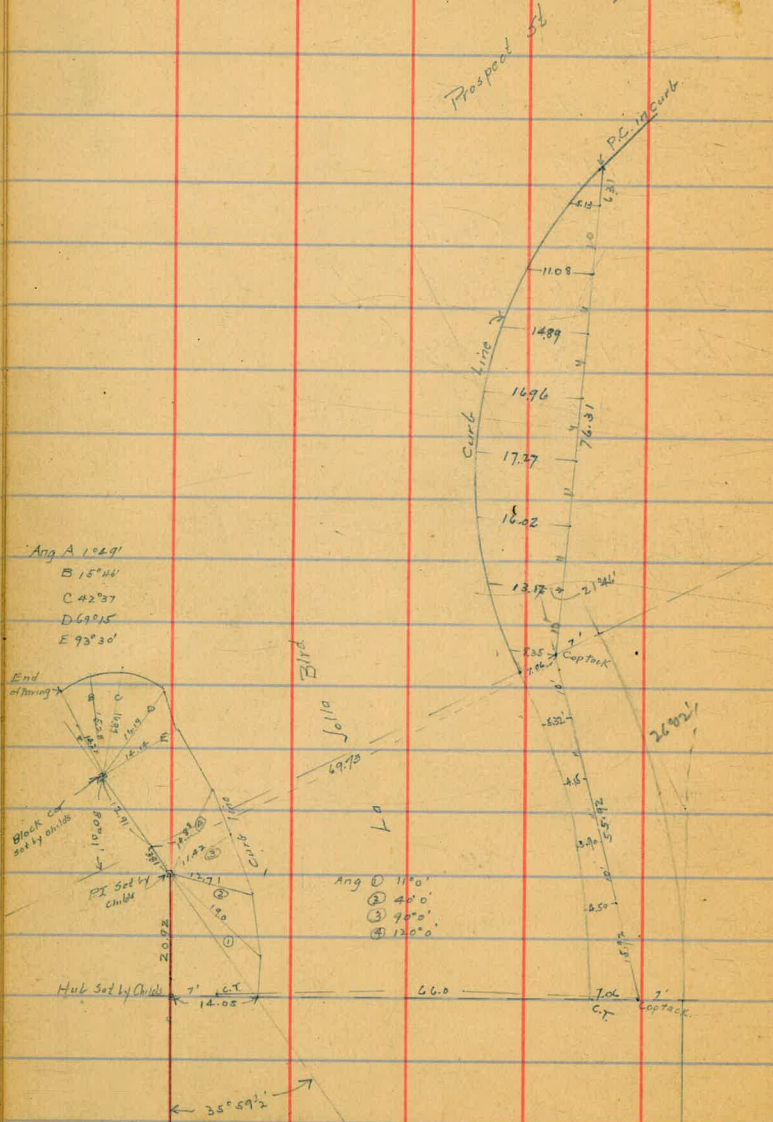
64,72

71

Sta	East center of culvert	Rod	center of culvert	Rod	West center of culvert	Rod
2+90.87	+27	<u>57.6</u> 7.1	0+00	13.1	57.6	+16 0.7 64.0
	+19	<u>54.4</u> 10.3				+7 11.9 52.8
3+00.87	+6	<u>52.3</u> 12.4	0+00	12.9	51.8	+19 5-66.1 -2.2 66.9
	+7	<u>53.8</u> 10.9				+17 6.8 57.9
	+17	<u>54.5</u> 10.2				+10 11.9 52.8
	+27	<u>58.5</u> 6.2				

Location of Curbs on Jolla Blvd & Prospect St

2 Dams
2 Byers
15 Hassard



(This number to be torn off by Inspector)

No 829

OFFICE

Ang A 302.4'
 B 7° 0'
 C 14° 0'
 D 36° 0'
 E 57° 30'
 F 89° 43'

Hut Set by Childs



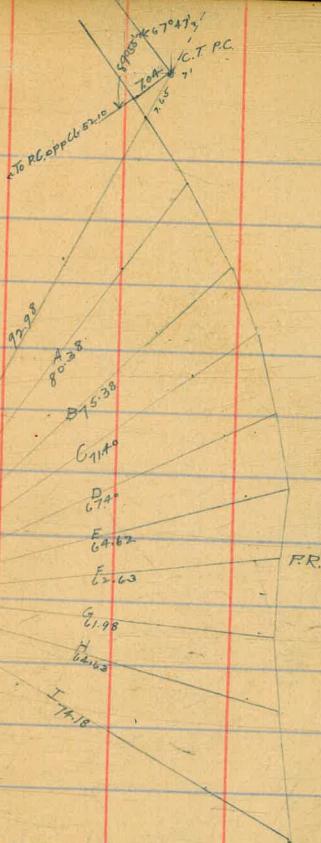
I Davis
 Honcock
 Byers

Location of Curbs
Ladelle B M & Rovina

9298
13

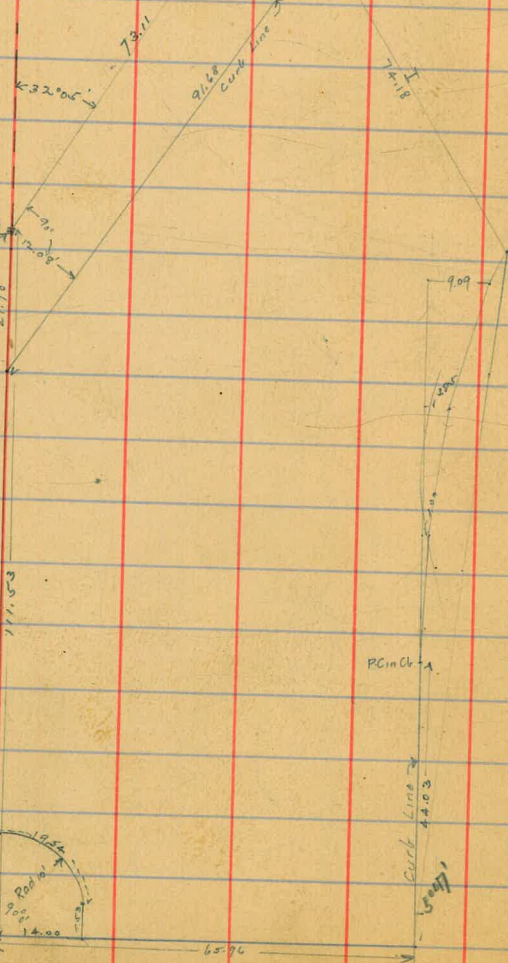
Ang A 8° 0'

B 17° 0'
 C 25° 30'
 D 36° 0'
 E 45° 30'
 F 54° 30'
 G 65° 0'
 H 76° 0'
 I 90° 0'



FR

Hut Set by Childs



PC in Cl A

Curb Line
44.03
50.07

65.96

X Sec. of Intersection of
Vine & State sts
old Notes Page 51 of 100
City 50' of State 10' do 75' 140

148.06

20'S. of Old N Line Vine

74

BM	0.76	159.97	159.21	str Mon slate & pas	E-12.5 = E line state	13.4	134.7	E wash
TP	0.71	148.06	12.62	147.35	E	15.0	133.1	
		10' N. of. old N Line Vine St			cl	16.0	132.1	
E		181	130.0		1/4	16.2	131.9	
cl		20.6	127.5		0	17.5	130.6	
1/4		22.6	125.5		1/4	18.3	129.9	
C		25.5	124.6		d	18.6	129.5	
1/4		28.4	119.7		W	17.6	130.5	
cl		30.0	118.1	Wash	+12.5	17.0	131.1	
W		31.3	116.8		5' N. of ϕ Vine St } = 35'S of old N. Line Vine = N. Line Proposed St		see Page 51	
+12.5 = W line slate		32.8	115.3		-12.5	7.3	140.8	
		10'S = Old N. Line Vine			-4	13.3	134.8	1/4 washout
W-125		27.8	140.3		-2	7.1	141.0	
W		27.8	140.3		W	7.4	140.7	
cl		27.5	120.6		cl	8.0	140.1	
1/4		27.2	120.9		1/4	8.2	139.9	
C		26.5	121.6	ϕ Wash	C	8.4	139.7	
1/4		23.8	124.3		1/4	8.9	139.7	
cl		21.8	126.3		d	9.2	138.9	
E		18.6	129.5		E	9.4	138.7	
					+12.5	8.5	139.6	

148.06

10' S. of last section

E-125	6.1	142.0
E	5.7	142.4
d	4.6	143.5
14	3.8	144.3
C	2.0	146.1
14	2.6	145.5
cl	3.0	145.1
W	4.2	143.9
+125	6.3	141.8

10' S. of above = New S. ch. of Vine St

-12.5 = W. line stake	5.66	148.4	on E. end cont cl
W	5.2	147.9	
cl	3.8	147.3	
14	2.3	145.8	
C	1.2	146.9	
14	0.5	147.6	
cl	1.1	147.0	
E	2.0	146.1	
+12.5	2.0	146.1	

T.P. 10.91 158.26 0.71 147.35

158.26

10' S. of above = New S. Line Vine

-10	7.9	150.2	75
E	8.5	149.8	
cl	8.5	149.8	
14	9.3	149.0	
C	10.2	148.1	
14	11.5	146.8	
cl	13.0	145.3	
W	14.2	144.1	
+12.5	15.3	143.0	use North
	13.0	145.3	use South

10' S

W	11.4	146.9
cl	9.8	148.5
14	10.1	148.7
C	9.3	149.0
14	8.2	150.1
cl	6.3	152.0
E	5.1	153.7

158.26

20' S.

E	3.6	154.7
cl	5.0	153.3
72	4.5	151.8
ny	7.0	151.3
e	7.6	150.7
ny	6.7	151.6
cl	7.8	150.5
W	9.2	149.1

35' S.

W	6.7	151.6
cl	5.9	152.4
ny	5.1	153.2
e	4.4	153.9
ny	4.0	154.3
cl	3.4	154.9
e	2.4	155.9

50' S.

e	0.7	157.6
cl	1.4	156.9
ny	2.0	156.3

158.26

76

C	2.7	155.6
ny	3.7	154.6
cl	4.6	153.7
W	5.8	152.5

70' S.

W	5.3	153.0	same
cl	4.3	154.0	same
ny	3.3	155.0	"
e	2.4	155.9	"
ny	1.8	156.5	not
cl	0.8	157.5	same
e	4.0	158.5	not

80' S.

e	1.0	157.3	same
cl	1.6	156.7	"
ny	2.6	155.7	"
e	3.6	154.7	"
ny	4.5	153.8	"
cl	5.2	153.1	"
W	5.7	152.6	"

No more changes see
Notes Page 59. This Book

Levels + location of private impmts
 STATE ST Vine to UPAS
 Sections taken on previous stations
 See page 74 & 53 this book

17th Mo
 Moore

15968

77

75' wide

Mon	Out	159.68	159.1	UPAS STATE
	10' N of old N/L vine			
-10		23.2	136.5	
E		26.3	133.4	
W		38.7	121.0	
+20		39.4	120.3	
	10' S of old N/L vine			
-20		36.3	123.4	
W		35.6	124.1	
E		26.6	133.1	
+10		23.1	136.6	
	20' S of old N/L			
-10		22.5	137.2	
E		25.0	136.7	
W	on New fill	26.4	133.3	
+20	" " "	27.0	132.7	
	5' N of ϕ vine			
W	on paving	18.3	141.2	
10' E of EL		19.3	140.2	

5' S of ϕ vine		
10' E of EL	16.1	143.6
W on paving	17.8	141.9
10' S of ϕ vine		
W top cem cb	17.2	142.8
10' E of EL	13.4	146.3
E	14.1	145.6
10' E of EL	13.4	146.3
New SL vine = 0400		
E	8.5	151.2
W	17.0	142.7
W top retaining wall	14.6	145.1
10' S		
W	13.2	146.5
E	5.8	153.9
15' S		
9.5' W of ϕ cem walk	12.9	146.7
30' S		
E	3.3	156.2

159.68

w - w	12.0	147.7	
w	13.1	146.6	
+10 = N2 residence	13.0	146.7	in yard
35'S			
-10 approach	12.9	146.8	" "
w	13.2	146.5	
+2	9.3	150.4	
E	2.0	157.7	
50'S			
E	0.7	159.0	
w - w	8.7	151.0	
w in yard	13.1	146.6	
+10 against house	12.9	146.8	
70'S			
w in yard	12.5	147.2	
+w	11.7	148.0	
+4	8.1	151.6	
E	0.2	159.5	
+8.5' Nedge garage ^{9'} wide	+0.2	159.9	dirt floor

159.68

STATE

78

60'S			
E	1.1	158.6	
w - 5	8.2	151.3	
-3	11.6	148.1	
w	12.6	147.1	
+10 in yard (level)	13.0	146.7	
90'S			
w	12.7	147.0	
+3	11.8	147.9	
+5	9.2	150.5	
E	2.3	157.4	
102'S			
E	7.7	152.0	
10' w of wall	12.8	146.9	in yard
108'S			
10' w of wall	13.1	146.6	" "
E	8.2	151.3	
116'S			
+2.5 Nedge curb drive	0.3	159.4	7' wide
E	10.8	148.9	

15968

10' w of wall	16.1	143.6	in yard
# W	13.1	146.6	
134' S			
E.	13.5	146.2	
W	16.7	143.0	in yard
145' S			
E	12.6	147.1	
20' E of EL edge lawn	0.7	159.0	
150' S			
E	11.1	148.6	
W	21.7	138.0	
158' S			
E	7.5	152.2	
165' S			
E	4.0	155.7	
W top cem retaining wall	23.4	134.3	N edge wall
180' S			
2' w of wall sunken yard	30.9	128.8	garage ^{floor} elev.
W top wall	20.4	136.3	
ground E of wall	22.2	137.5	

15968

STATE

79

			E	0.0	159.7
			185' S		
			E	0.4	159.3
			W	22.2	137.5
			W top wall	20.4	136.3
			195' S		
			5' E of EL in yard	+1.0	160.7
			E	0.2	159.5
			W	22.2	137.4
			W top wall	23.4	136.3
			202' S		
			E	+0.4	160.1
			215' S		
			E	0.0	159.7
			W Top wall	23.4	136.3
			4' S edge sunken yard	31.0	128.7
			215.50 S		
			10' w of wall on lawn	22.9	136.8
			225' S		
			14' w of wall = N edge residence	22.9	136.8

159.68

W	229	136.1	
E	+03	160.0	
	250'S		
E	+0.2	159.9	
W	229	136.8	in yard
+ 14	against house	229	136.8
	256'S		
- 14	S edge "	229	136.8 " "
W	229	136.8	" "
E	0.3	159.4	
TP	90.2	167.19	15' 158.17 ✓
	264'S		
E	7.8	159.4	
W	S edge com walk	30.0	137.2
	274'S		
10' W of WL		35.1	132.1
W		30.1	137.1
	277'S		
E		7.6	159.6

167.19

STATE 80

	290'S		
E		7.1	160.1
W		29.1	138.1
10' W of WL		34.2	133.0
	300'S		
E		7.6	159.6
	310'S		
E		5.9	161.3
10' W of WL		27.9	139.3
	320'S		
10' W of WL		24.8	142.4
E		5.1	162.1
	335'S = 2' N of E house		165 wide
3' E of WL	edge of porch	18.2	149.0
" " " "	floor div	17.2	150.0
E		3.1	162.1
	345'S		
E		2.3	164.9
ch BM		7.8	159.2 ✓ 159.2 ✓

A + T - Br.

A3 Dist. Ver.

STANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING
ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.
FOR SINGLE TRACK EMBANKMENT.

0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
7.00	7.15	7.30	7.45	7.60	7.75	7.90	8.05	8.20	8.35	0
8.50	8.65	8.80	8.95	9.10	9.25	9.40	9.55	9.70	9.85	1
10.00	10.15	10.30	10.45	10.60	10.75	10.90	11.05	11.20	11.35	2
11.50	11.65	11.80	11.95	12.10	12.25	12.40	12.55	12.70	12.85	3
13.00	13.15	13.30	13.45	13.60	13.75	13.90	14.05	14.20	14.35	4
14.50	14.65	14.80	14.95	15.10	15.25	15.40	15.55	15.70	15.85	5
16.00	16.15	16.30	16.45	16.60	16.75	16.90	17.05	17.20	17.35	6
17.50	17.65	17.80	17.95	18.10	18.25	18.40	18.55	18.70	18.85	7
19.00	19.15	19.30	19.45	19.60	19.75	19.90	20.05	20.20	20.35	8
20.50	20.65	20.80	20.95	21.10	21.25	21.40	21.55	21.70	21.85	9
22.00	22.15	22.30	22.45	22.60	22.75	22.90	23.05	23.20	23.35	10
23.50	23.65	23.80	23.95	24.10	24.25	24.40	24.55	24.70	24.85	11
25.00	25.15	25.30	25.45	25.60	25.75	25.90	26.05	26.20	26.35	12
26.50	26.65	26.80	26.95	27.10	27.25	27.40	27.55	27.70	27.85	13
28.00	28.15	28.30	28.45	28.60	28.75	28.90	29.05	29.20	29.35	14
29.50	29.65	29.80	29.95	30.10	30.25	30.40	30.55	30.70	30.85	15
31.00	31.15	31.30	31.45	31.60	31.75	31.90	32.05	32.20	32.35	16
32.50	32.65	32.80	32.95	33.10	33.25	33.40	33.55	33.70	33.85	17
34.00	34.15	34.30	34.45	34.60	34.75	34.90	35.05	35.20	35.35	18
35.50	35.65	35.80	35.95	36.10	36.25	36.40	36.55	36.70	36.85	19
37.00	37.15	37.30	37.45	37.60	37.75	37.90	38.05	38.20	38.35	20
38.50	38.65	38.80	38.95	39.10	39.25	39.40	39.55	39.70	39.85	21
40.00	40.15	40.30	40.45	40.60	40.75	40.90	41.05	41.20	41.35	22
41.50	41.65	41.80	41.95	42.10	42.25	42.40	42.55	42.70	42.85	23
43.00	43.15	43.30	43.45	43.60	43.75	43.90	44.05	44.20	44.35	24
44.50	44.65	44.80	44.95	45.10	45.25	45.40	45.55	45.70	45.85	25
46.00	46.15	46.30	46.45	46.60	46.75	46.90	47.05	47.20	47.35	26
47.50	47.65	47.80	47.95	48.10	48.25	48.40	48.55	48.70	48.85	27
49.00	49.15	49.30	49.45	49.60	49.75	49.90	50.05	50.20	50.35	28
50.50	50.65	50.80	50.95	51.10	51.25	51.40	51.55	51.70	51.85	29
52.00	52.15	52.30	52.45	52.60	52.75	52.90	53.05	53.20	53.35	30
53.50	53.65	53.80	53.95	54.10	54.25	54.40	54.55	54.70	54.85	31
55.00	55.15	55.30	55.45	55.60	55.75	55.90	56.05	56.20	56.35	32
56.50	56.65	56.80	56.95	57.10	57.25	57.40	57.55	57.70	57.85	33
58.00	58.15	58.30	58.45	58.60	58.75	58.90	59.05	59.20	59.35	34
59.50	59.65	59.80	59.95	60.10	60.25	60.40	60.55	60.70	60.85	35
61.00	61.15	61.30	61.45	61.60	61.75	61.90	62.05	62.20	62.35	36
62.50	62.65	62.80	62.95	63.10	63.25	63.40	63.55	63.70	63.85	37
64.00	64.15	64.30	64.45	64.60	64.75	64.90	65.05	65.20	65.35	38
65.50	65.65	65.80	65.95	66.10	66.25	66.40	66.55	66.70	66.85	39
67.00	67.15	67.30	67.45	67.60	67.75	67.90	68.05	68.20	68.35	40

Calculated by F. E. Paradis, C. F.

15728
 7 44
 230 121
 6/95
 15.82
 1597
 167
 143
 15.82
 744
 15.28
 $11 \frac{36}{23} \sin 30^\circ 52' = \frac{R}{1190}$
 $\frac{3.52}{23} = \frac{R}{1190}$
 $R = \frac{3.52 \times 1190}{23} = 174.16$
 6/84.96
 14.16

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING
 ROADWAY 16 FEET WIDE. SIDE SLOPES 1½ TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	

Calculated by F. E. Paradis, C. E.

110/13.00 11.81
 1700 = T sin 1/2 Δ
 155 10.23 10 13.00 140/11.7
 100 9.00 13.00 140 11.7
 500 8.80 13.00 140 11.7
 400 20.78 11.41 170
 500 6.97 130 11.7 300
 5.16 30.23 229 13 280
 2.58 37.20 14.4 23 200
 200 21 14
 260 36.75 45 200 13.01
 44 65 630
 24 37.40 13.01 193.30
 13 13.01 630.30
 70 44 13 16.00 26.02
 5.60 179.00
 6/18.60 70 7.65 12.5
 19.160 78 20
 268/18.21 85.60 227.3 3.96 195.20
 11.2 12.78
 179 607 198.23 HZ
 140 35 190.90
 65 49.13 7.93
 114.55 3.76 227.3 2264 19.60
 32 203.60 440.057 3.36 198.33
 82 5.16 5.08 0.20 90
 508.76 2.88 198.03 HZ
 2.58 2.18 12.78 HZ
 27.34 203.60 203.0 210.98 HZ
 11.69 203.60 7.98 227.3
 2.58 7.38 0.98 4.11
 6.53 2.58 210.00 HZ
 3.58 3.80 13.03
 3.95 2.22 223.03 HZ
 22.15 2264 211.7 11.33
 1.33 5.36 214.6
 222.63 8.43
 9.13 HZ 228.0 221.0
 231.76 3.76 2.63
 224.20 228.60
 7.54 22.66
 22.36 22.15 5.16