1019

TRANSIT-BOOK
1309

7/12/17 Gregory Moore Miller. Survey of Road from E. L Beverly to West End of Sutter St. 66' wide

13+23.41 E.C.

12+87 △ 42°40' R. $R = 100$ $T_s = 39.06$ $Lc = 74.47$

12+47.94 P.C.

7+95.93 ⊙ P.O.T.

1+53.26 E.C.

1+0.0 △ 15°21' R. $R = 400$ $T_s = 53.90$ $Lc = 107.16$

0+46.10 P.C.

0+0.0

21+43.95 E.C.

21+04.48 Δ 4°00' R R = 1131.6, Ts = 39.52, Lc = 78.99

20+64.96 P.R.C.

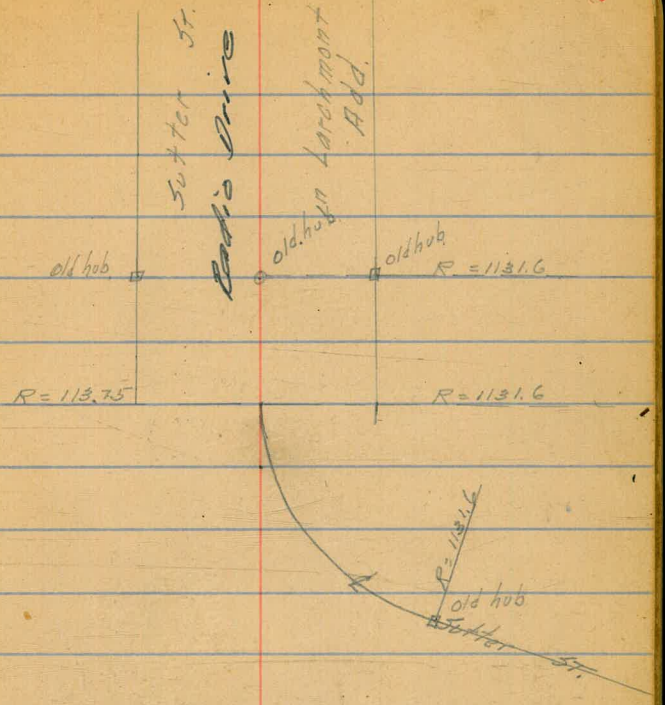
20+30.63 Δ 35°48' L R = 113.75, Ts = 36.74, Lc =

19+93.89 P.C.

18+17.75 E.C.

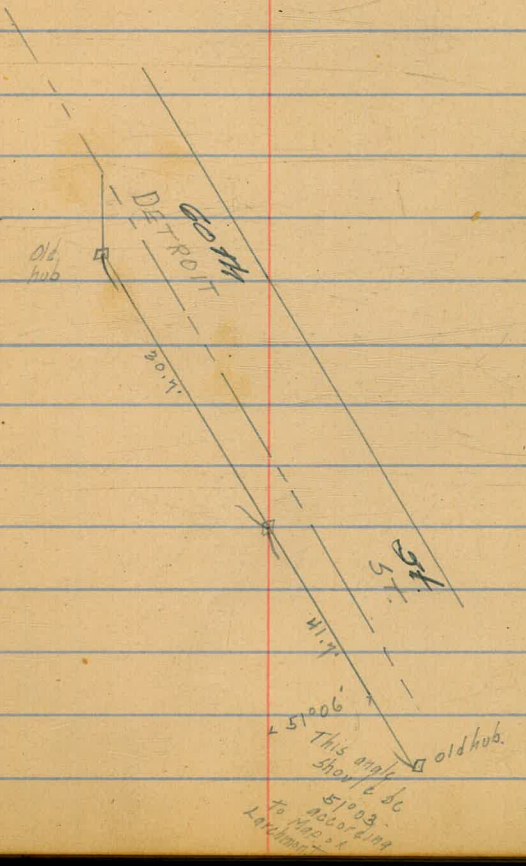
17+65 Δ 42°30' L. R = 150', Ts = 58.08, Lc 110.83

17+06.92 P.C.



25 + 93.95 Δ 10°00 R R=1143 T3=100 = W. L. DETROIT

24 + 93.95 P.C.



4/3/17 Gregory Moore Miller

Levels on Survey from Lookout to Sutter

5

B.M.	12.90	271.67	258.77 Hubbell Lookout Handhole	
N.B. All distances are on ℄ of 60' St.				
E. L. Randolph St.				
S		9.8	261.9	
C		10.1	261.6	
N		9.5	262.2	
25' E				
C		8.9	262.8	
116.10' E = P.C.				
N		7.8	263.9	
C		6.2	265.5	
S		7.5	264.2	
99.68' E = C.C.				
S		4.7	267.0	
C		5.0	266.7	
N		4.8	266.9	
1+53.26 = E.C.				
N		2.9	268.8	
C		2.1	269.6	
S		2.1	269.6	
T.P.	12.45	284.01	0.11	271.56

2+00		
S	12.4	271.6
C	12.8	271.2
N	13.1	270.9
2+50		
N	10.2	273.8
C	10.7	273.3
S	11.2	272.8
3+00		
S	10.3	273.7
C	9.2	274.8
N	8.5	275.5
3+50		
N	7.4	276.6
C	8.5	275.5
S	10.0	274.0
4+00		
S	9.2	274.8
C	7.8	276.2
N	6.7	277.3

		284.01		
		4+50		
N		5.7	278.3	
C		6.4	277.6	
S		6.8	277.2	
		5+00		
S		7.3	276.7	
C		5.8	278.2	
N		4.2	279.8	
		5+50		
N		3.4	280.6	
C		4.8	279.2	
S		6.1	277.9	
		6+00		
S		2.5	281.5	
C		2.9	281.1	
N		2.0	282.0	
T.P.	6.47	290.33	0.15	283.86
		6+50		
N		5.7	284.6	
C		6.6	283.7	
S		6.8	283.5	
		7+00		
S		4.0	286.3	
C		4.3	286.0	
N		4.6	285.7	
		7+50		
N		3.3	287.0	
C		3.2	287.1	
S		3.1	287.2	
		8+00		
S		2.7	287.6	
C		2.8	287.5	
N		2.8	287.5	
		8+50		
N		3.2	287.1	
C		3.5	286.8	
S		3.8	286.5	
		9+00		
S		5.6	284.7	
C		5.3	285.0	

R90.33

N		4.6	285.7	C		
	9+50			S		
N		6.6	283.7			
C		7.7	282.6	S		
S		8.8	281.5	C		
	10+00			N		
S		13.1	277.2			
C		11.6	278.7	N		
N		9.8	280.5	C		
	10+50			S		
N		12.0	278.3			
TP	0.55	278.41	12.47	27.86		
C			2.0	276.4		
S			4.3	274.1	S	
	11+00				C	
S			4.7	273.7	N	
C			2.9	275.5		
N			1.0	277.4	N	
	11+50				C	
N			2.0	276.4	S	

	3.7	274.7	
	5.3	273.1	
12+0			
	5.9	272.5	
	4.5	273.9	
	3.2	275.2	
12+47.94 = PC			
	7.9	270.5	
	7.9	270.5	
	7.0	271.4	
13+8.5.17 = CC			
	9.2	269.2	
	13.0	266.4	
	11.8	266.6	
13+27.41 = EC.			
	13.0	265.4	
	19.3	259.1	
	13.2	265.2	

TP	0.56	266.55	12.42	265.99	PI hub 12+87
		13+50			
S			2.8	263.8	
C			9.0	257.6	
N			1.7	264.9	
		14+00			
N			1.3	262.3	
C			11.2	255.4	
S			10.2	256.4	
		14+50			
S			16.0	250.6	
C			15.0	251.6	
N			10.0	256.6	
TP	0.17	253.94	12.78	253.77	
		15+00			
N			1.8	252.1	
C			6.0	247.9	
S			7.4	246.5	
		15+50			
S			13.6	240.3	
C			9.5	244.4	
N			5.0	248.9	
		15+65			
S			15.3	238.6	
		16+00			
N			7.5	246.4	
C			18.9	241.0	
TP	3.33	244.93	12.34	241.60	
S			9.6	235.3	
		16+50			
S			11.6	233.3	
C			6.4	238.5	
N			0.0	244.9	
		17+06.92 = PC			
N			3.7	241.2	
C			9.3	235.6	
S			15.6	229.3	
		17+62.33 = C.C.			
S			19.1	225.8	
C			13.7	231.1	

		244.43			
N			9.0	235.9	
T.P.	0.05	232.31	12.67	232.26	
B.M.			2.80	229.46	P.I. Hub 17+65
		18+17.75			
N			1.5	230.8	
C			6.9	225.4	
S			12.2	220.1	
		18+50			
S			14.5	217.8	
C			8.8	223.5	
N			5.7	226.6	
		18+85			
N			12.9	219.4	
TP	0.55	220.00	12.86	219.45 ~~219.40~~	
C			2.8	217.2	
S			5.4	214.6	
		19+00			
S			9.2	210.8	

		19+22			
S			17.8	202.2	
C			16.7	203.3	
N			14.1	205.9	
		19+30			
N			15.4	204.6	
		19+35			
S			14.6	205.4	
		19+45			
C			9.4	210.6	
		19+60			
N			4.2	215.8	
C			5.5	214.5	
S			11.8	208.2	
B.M.	9.32	226.9 ~~226.85~~	2.42	~~217.53~~ 217.58	PI hub 20+30.63
		19+93.89 = P.C.			
S			17.3	209.6	
C			10.9	216.0	
N			7.9	219.0	

~~226.85~~
226.9

20+29.42 = C.C.

N	5.5	221.4
C	8.6	218.3
S	17.7	209.2

20+64.96 = P.R.C.

S	16.3	210.6
C	6.8	220.7
N	2.8	224.1

21+04.46 = C.C.

N	+0.5	227.4
C	3.8	223.1
S	14.3	212.6

21+43.95

S	9.6	217.3
C	1.6	225.3
T.P. 10.99	~~236.32~~ ~~236.27~~ 1.57	~~225.33~~ ~~225.28~~
N	5.9	230.4

22+00

N	2.6	233.7
C	7.6	228.7
S	12.9	223.4

22+50

S	10.3	226.0
C	4.6	231.7
T.P. 7.78	~~242.93~~ ~~242.88~~ 1.17	~~235.15~~ ~~235.10~~
N	6.5	236.4

23+00

N	4.2	238.7
C	10.4	232.5
S	16.0	226.9

23+50

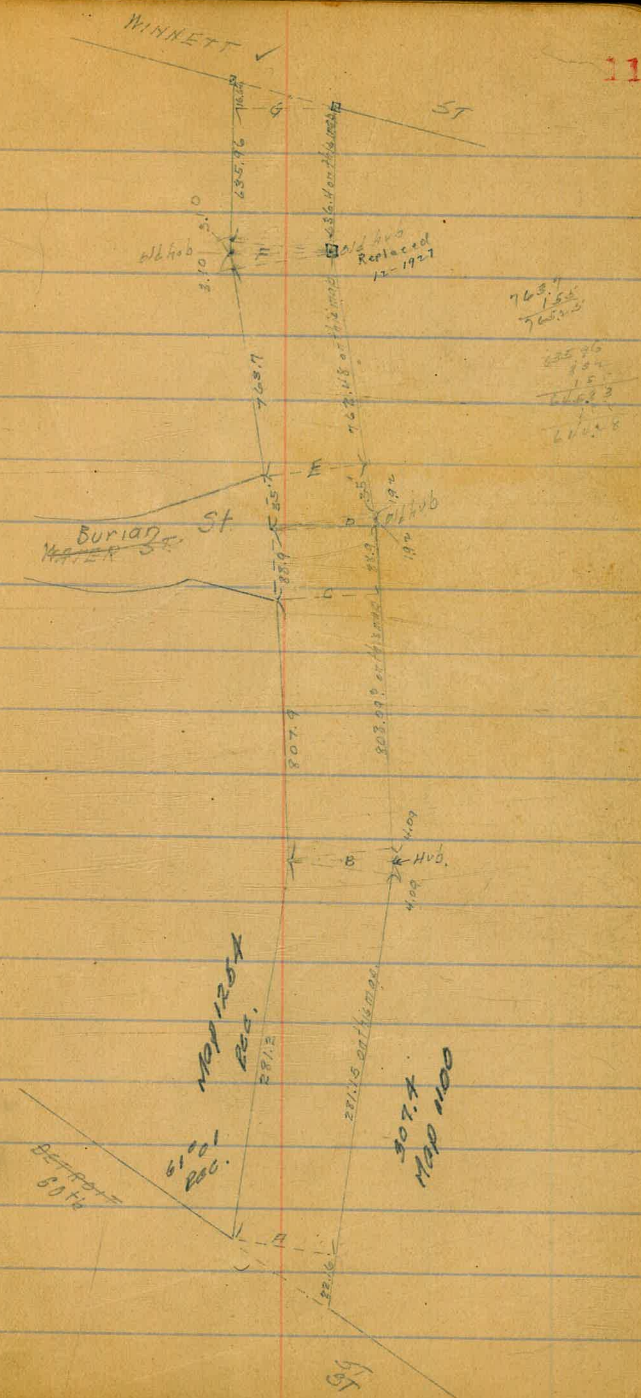
S	16.7	226.2
C	10.5	232.4
N	4.9	238.0

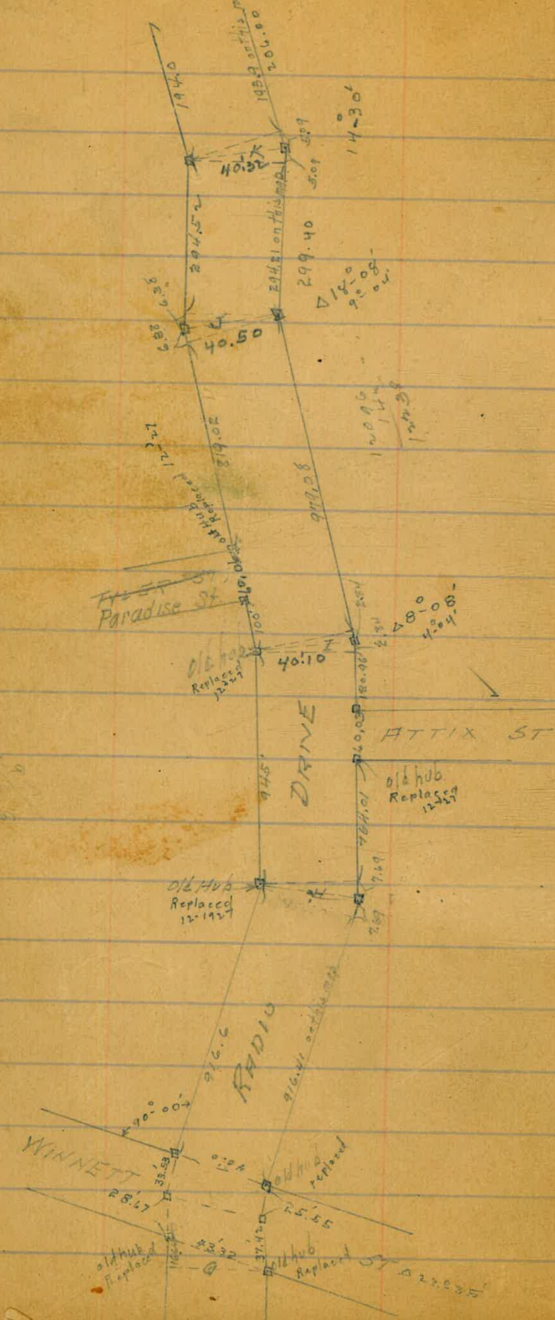
24+00

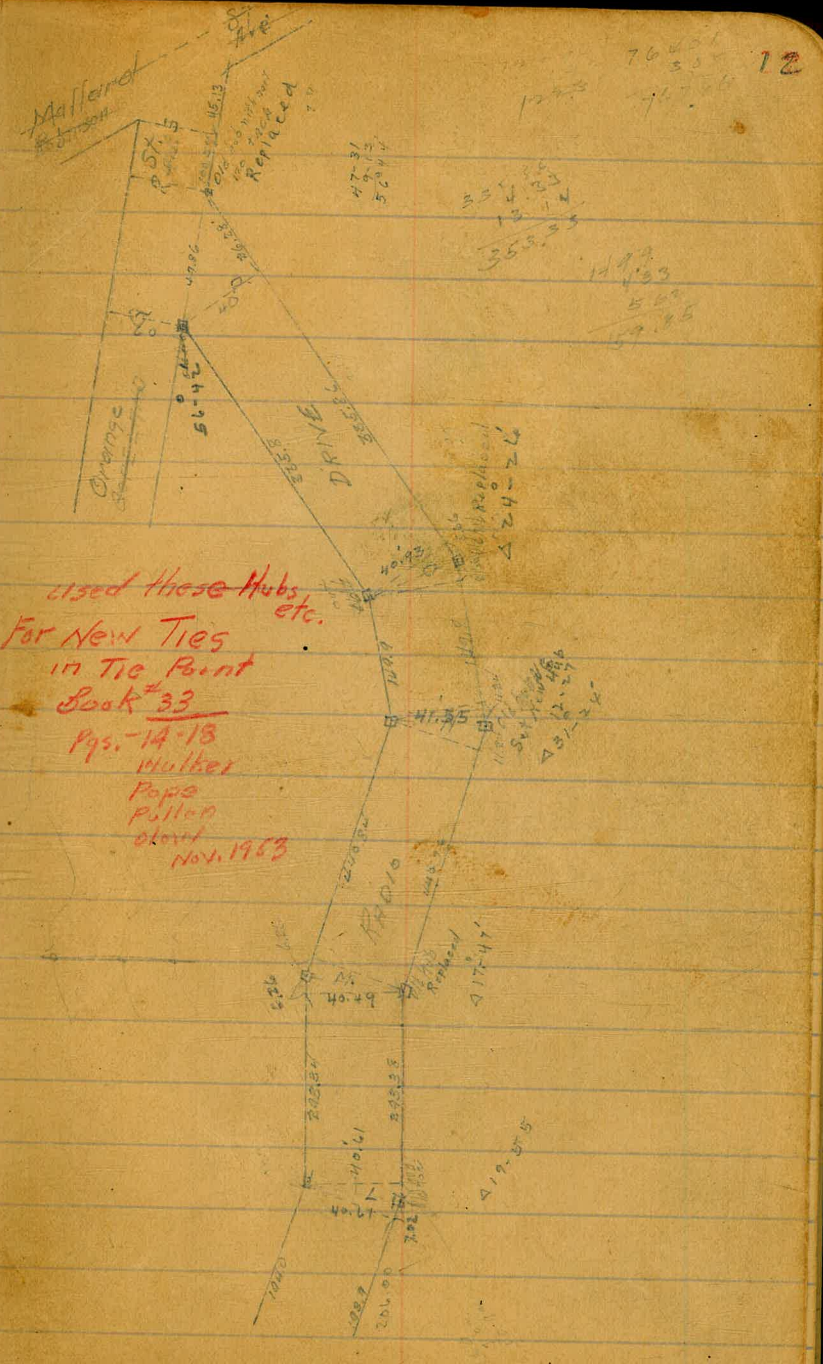
N	7.0	235.9
C	11.9	231.0
S	17.3	225.6

242.88

		24+50			
S			15.9	227.0	
C			10.1	232.8	
N			5.7	237.2	
		24+93.95 P.C.			
N			3.5	239.4	
C			8.7	234.2	
S			15.4	227.5	
		25+50 P.O.C.			
S			15.2	227.7	
C			7.2	235.7	
T.P.	9.95	248.37 ~~248.32~~	4.51	238.42 ~~238.37~~	on P.I. 25+[illegible] Hub
N			6.0	242.8 (4)	
This is on diagonal.		on Tangent 25+93.95 on ℄ = W.L. Detroit St.			60' wide
N			3.0	245.8 (4)	
C			10.4	238.0 ~~237.9~~	
S			20.5	227.8 (9)	







~~used these Hubs~~ etc.
For New Ties
in Tie Point
Book #33
Pgs.-14-18
Mulker
Pope
Pullen
Nov. 1953

7/19/11 Gregory Moots Miller

Levels on Sutter St 40 ft.
from E.L. Detroit
to N. City Boundary

BM	12.36	250.~~73~~ 65	238.~~37~~ 42	P.I. Hub Nr. Detroit

SEE SKETCH ON PRECEDING PAGE

E.L. DETROIT

N		7.8	242.9
C		12.5	238.2
S		18.1	232.6

22.16'E on So. 00 E. on No. } = A.

S		19.5	231.2
C		12'	238.6
N		7.8	242.9

25'E of A

N		7.0	243.7
C		11.8	238.9
S		14.7	2360 2359

50'E of A

S		14.1	236.6
C		11.7	2390 2385
N		7.6	243.1

100'E of A

N		4.8	245.9
C		9.1	241.6

RADIO DRIVE

Profile platted 7/21/11. (BMY)

13

S		11.2	239.5

13.5'E of A

S		8.0	242.7
C		6.1	244.6
N		2.2	248.5
T.P.	13.01	261.~~37~~	238 248.36

200'E of A

N		11.0	250.4
C		14.0	247.4
S		17.9	243.5

250'E of A

S		15.8	245.6
C		12.0	249.4
N		8.0	253.4

281.2 on No. 285.24 on So. } = B

N		6.4	255.0 254.9
C		10.0	251.4
S		13.7	247.7

		261.37	
	50' E of B on No		
	54.09 E - - - So		
S		12.3	249.1
C		8.6	252.8
N		4.2	257.2
	100' E of B on No		
	104.09 - - - So.		
N		2.9	258.5
C		7.6	253.4
S		11.5	249.9
	150' E of B on No		
	154.09 - - - So.		
S		9.5	251.9
C		6.3	255.1
N		1.9	259.5
	200' E of B on No		
	204.09 - - - So.		
N		10.1	261.5
C		4.4	257.0 256.9
S		7.9	253.5
	250' E of B on No		
	254.09 - - - So.		
S		7.2	254.2
C		3.1	258.3
TR	12.53	270.99 270.44	3.91 256.46

SUTTER I4
NON RADIO DRIVE

N		8.3	262.7
	300' E of B on No		
	304.09 - - - So.		
N		8.7	262.3
C		12.7	258.3
S		16.4	254.6
	350' E of B on No		
	354.09 - - - So.		
S		17.6	253.4
C		13.3	257.7
N		9.5	261.5
	400 E of B on No		
	404.09 - - - So.		
N		9.7	261.3
C		13.0	258.0 257.9
S		17.3	253.7
	450' E of B on No		
	454.09 - - - So.		
S		14.2	256.8
C		10.8	260.2
N		7.9	263.1
	500' E of B on No.		
	504.09 - - - So.		
N		4.4	266.6
C		7.4	263.6

		270.39		
S		10.3	260.7	
		550' E ox B on No		
		55409 - - - - So.		
S		7.8	263.2	
C		4.7	266.3	
N		1.3	269.7	
T.P.	12.43	280.70	272	268.27
		600' E ox B on No		
		60409 - - - - So.		
N		11.1	269.6	
C		13.8	266.9	
S		17.1	263.6	
		650' E ox B on No		
		65409 - - - - So.		
S		17.9	262.8	
C		15.9	264.9	
N		12.4	268.3	
		691.09' E ox B on So.		
S		21.1	259.6	
		700' E ox B on No.		
		70409 - - - - So.		
N		14.3	266.4	
C		15.3	265.4	
S		17.5	263.2	

		750' E ox B on No.		
		75409 - - - - So.		
S		14.5	266.2	
C		11.6	269.1	
N		8.2	272.5	
		807.9' E ox B on No.		= C. = W. L. WATER ST.
		812.18' - - - - So.		
N		3.0	277.7	
C		7.0	273.7	
S		10.0	270.7	
		50' E. ox C		
S		7.8	273.5	
C		3.4	277.3	
T.P.	12.17	290.56	12.31	278.39
N		10.5	280.1	
		88.9' E ox C on No.		= D
		90.52' - - - - So.		
N		9.0	281.6	
D		11.7	278.9	
S		15.8	274.8	
		35' E ox D on No.		= E = EL. WATER ST.
		36.92' - - - - So.		
S		15.2	275.4	
C		11.0	279.6	

240.56

N		6.8E	283.74 or 406
	50' E. of E		
N		6.8	283.8
C		10.8	279.8
S		16.6	274.0 / 273.9
	100' E. of E		
S		15.6	275.0 / 274.9
C		10.6	280.0 / 279.9
N		5.8	284.8
	150' E. of E		
N		4.0	286.1
C		9.5	281.0
S		14.7	275.9
	200' E of E		
S		11.7	278.9
C		6.9	283.7
T.P.	9.55	294.78 / 294.43	285.29 / 285.18
N		5.5	289.3
	250' E. of E		
N		2.9	292.0 / 291.9
C		8.9	285.9
S		13.6	281.2
	300' E. of E		
S		12.0	282.8
C		7.5	287.3
N		1.5	293.3
	350' E. of E		
N		2.0	292.8
C		8.8	286.0 / 285.9
S		13.5	281.3
	400' E. of E.		
S		14.9	279.9
C		10.6	284.2
N		4.7	290.1
	450' E of E		
N		5.9	288.9
C		10.5	284.3
S		14.1	280.7

294.78

500' E. of E

S		18.0	282.8
C		8.7	286.8
N		4.9	290.8

550' E. of E

N		2.2	292.5
C		5.8	289.0 / 288.9
S		8.1	286.7

600' E. of E

S		6.7	288.2
C		4.5	290.3
TP	6.51	4.28	290.50
N		3.0	294.0

650' E. of E

N		4.0	293.0
C		6.9	290.1
S		8.5	288.5

711' E. of E

S		10.4	286.6
C		9.4	287.6

SUTTER
RADIO DT. 17

N		7.2	289.8

725' E of E

N		13.2	283.8

727' E of E

S		16.2	280.8

740' E of E

N		8.0	289.0

747' E of E

N		11.9	285.1

766.8' E. of E on No
762.48' - - - So } = F

N		7.1	289.9
C		9.2	287.8
S		10.1	286.9

53.10' E of E on No
50' - - - So

S		9.7	287.3
C		7.4	289.6
N		3.3	293.7
TP	11.74	30420	4.55	292.46

304.20

103.1' E of F on No
100' - - - - So.

N	7.5	296.7
C	12.0	291.2
S	16.4	287.8

153.1 E of F on No
150' - - - - So.

S	16.3	287.9
C	12.6	291.6
N	8.1	296.1

203.1' E of F on No
200' - - - - So.

N	8.6	295.6
C	12.6	291.6
S	16.2	288.0

253.1 E of F on No
250' - - - - So.

S	16.5	287.7
C	11.9	292.3
N	8.2	296.0

303.1 E of F on No
300' - - - - So.

N	6.8	297.4
O	10.4	293.8
S	16.1	287.8

SUTTER
RADIO DR. 19

327' E of F

S	14.1	290.1

353.1' E of F on No
350' - - - - So.

S	18.8	285.4
C	9.4	294.8
N	5.7	298.5

364' E of F

S	24.7	279.5 creek

385' E of F

S	24.4	279.8 creek

403.1' E of F on No
400' - - - - So.

N	7.1	297.1
C	11.5	292.7
S	22.6	281.6

453.1 E of F on No
450' - - - - So.

S	14.6	289.6
C	7.5	296.7
N	4.3	299.9

304.26

	503.1' E of F on No 500 " " " " So.		
N		3.1	301.1
C		7.6	296.6
S		10.0	294.2
	525' E of F.		
S		10.0	294.2
	553.1 E of F on No 550' " " " " So		
S		11.9	292.5
C		7.7	296.5
N		1.8	302.4
T.P. 12.75	307.80	9.15	298.05 hub SW Winnett
	603.1 E of F on No 600' " " " " So		
N		6.0	301.8
C		11.2	296.6
S		11.9	295.9
	635.96' E of F on No 636.4' " " " " So } = G.		
S		12.8	295.0
C		11.5	296.3
N		8.4	299.4

307.8 SUTTER

	W. L. WINNETT ST.		
N		9.7	298.1
C		11.4	296.4
S		12.8	295.0
	E. L. WINNETT ST.		
S		11.6	296.2
C		9.7	298.1
N		7.4	300.4
	50' E		
N		3.6	304.2
C		6.8	301.0
S		9.1	298.7
	100' E		
S		9.1	298.7
C		5.9	301.9
N		1.9	305.9
	150' E		
N		1.6	306.2
C		5.5	302.3
S		8.2	299.6

307.80

200' E

S		6.8	301.0
C		4.8	303.0
N		1.1	306.7

250' E

N		1.0	306.8
C		4.6	303.2
S		7.0	300.8

300' E

S		5.8	302.0
C		4.7	303.1
N		3.8	304.0
TP	12.33	315.45	303.12

350' E

N		11.0	304.45
C		12.1	303.34
S		13.0	302.45

400' E

S		11.2	304.23
C		10.1	305.01

N

450' E

N		9.0	306.54
C		6.2	309.32
S		7.7	307.87
		8.5	307.0 306.87

500' E

S		6.9	308.56
C		5.2	310.33
N		2.8	312.76

550' E

N		0.2	315.32
C		3.4	312.13
S		6.5	309.0 309.7

600' E

S		7.1	308.34
C		3.7	311.87
TP	12.84	328.27	315.43
N		12.2	316.01

328.27

650' E

N		11.9	316.8
C		16.4	311.9
S		18.2	310.1

700' E

S		15.5	312.6
C		14.1	314.2
N		9.5	318.8

750' E

N		5.6	322.7
C		9.8	318.5
S		11.4	316.9

800' E

S		7.5	320.8
C		5.5	322.5
N		2.2	326.8
T.P.	12.85	340.61	0.51	327.76

850' E

N		11.9	328.7
C		16.1	324.5

340.6

S		17.4	323.2

900' E

S		16.4	324.2
C		14.4	326.2
N		11.0	329.6

916.6 E of WINNETT on No
924.1 " " " " So } = H.

N		11.0	329.6
C		13.5	327.1
S		16.2	324.4

50' E of H on No
57.69 " " " So

S		13.9	326.7
C		12.0	328.6
N		8.6	332.0

100' E of H on No
107.69 " " " So

N		7.1	333.5
C		10.6	330.1
S		12.9	327.7

150 E of H on No
157.69 " " " So

S		12.9	327.7
C		10.4	330.2

340.61

N	6.1	334.5	
	200' E of H on No		
	207.69 - - - So		
N	5.7	334.9	
C	10.0	330.6	
S	12.1	328.5	
	250' E of H on No		
	257.69 - - - So		
S	11.7	328.9	
C	8.9	331.7	
N	5.3	335.3	
	300' E of H on No		
	307.69 - - - So		
N	4.2	336.4	
C	8.4	332.2	
S	10.6	330.0	
	350' E of H on No		
	357.69 - - - So		
S	9.0	334.6	
C	7.1	338.5	
N	3.7	336.9	
	400' E of H on No		
	407.69 - - - So		
N	3.2	337.4	
C	6.9	333.7	

S	8.7	331.9	
	450 E of H on No		
	457.69 - - - So		
S	7.6	338.0	
C	5.5	335.1	
T.P. 11.79	348.47	3.93	336.68
N	11.2	337.3	
	500' E of H on No		
	507.69 - - - So		
N	8.7	339.8	
C	11.5	337.0 336.9	
S	13.0	335.5	
	550' E of H on No		
	557.69 - - - So		
S	14.6	333.9	
C	11.5	337.6 336.9	
N	8.7	339.8	
	600' E of H on No		
	607.69 - - - So		
N	7.7	340.8	
C	11.0	337.5	
S	14.3	334.2	

348.47

650'E ox H on No
657.69 - - - So.

S	13.1	335.3
C	9.9	338.5
N	6.9	341.5

700'E ox H on No
707.69 - - - So.

N	4.4	347.0
C	8.7	339.5
S	11.8	336.3

750'E ox H on No
757.69 - - - So.

S	11.1	337.4
C	7.0	341.5
N	3.0	345.5

764.01'E ox H on No
771.70 - - - So } = W.L. ATTIX ST. 60' wd.

N	2.7	345.8
C	6.8	341.7
S	10.0	338.5

E.L. ATTIX ST.

S	8.0	340.5
C	5.4	343.1
	1.3	347.2

TP 11.99 359.96 0.50 347.97

50'E

N	11.6	348.4
C	14.7	345.3
S	18.8	341.2

100'E

S	17.6	342.4
C	13.6	346.4
N	10.4	349.6

120.96'E ox ATTIX on No
123.80 - - - So } = I

N	10.1	349.9
C	13.9	346.1
S	17.2	342.8

50'E ox I on No
52.84 - - - So

S	15.9	344.1
C	12.6	347.4
N	8.2	351.8

100'E ox I on No
102.84 - - - So } = W.L. TYLER ST. 60' wd.

N	8.2	351.8
C	12.4	347.6

359.96

Plate

BM		9.36	(35.060 353.55	NW Pole at Tyler
S		15.0	345.0 344.9	

E L TYLER ST ✓

S		12.6	347.3	4
C		8.2	351.5	4
N		4.9	355.1	1
TP	12.50	372.18	0.28	359.68

50' E

N		13.8	358.3	4
C		18.3	353.8	9
S		22.5	349.6	7

100' E

S		20.9	351.8	3
C		16.0	356.7	7
N		12.1	360.6	1

150' E

N		10.9	361.8	3
C		14.2	358.0 ~~357.9~~	
S		17.6	354.5	6

372.18

SUTTER 24

200' E

S	17.0	355.1	2
C	12.6	359.5	6
N	8.5	363.6	7

250' E

N	6.8	365.3	4
C	11.0	361.1	7
S	16.0	356.1	2

300' E

S	12.0	360.1	2
C	8.7	363.4	5
N	4.6	367.5	6

350' E

N	3.0	369.1	2
C	6.5	365.6	7
S	9.3	362.8	9

400' E

S	8.1	364.0	1
C	4.9	367.2	5
N	1.6	370.5	6

372.18

450' E

N		1.3	370.8
C		4.5	367.6
S		8.4	363.7

500' E

S		8.8	368.4
C		4.3	367.9
T.P.	12.84	383.00	1.42 370.16
N		10.2	372.8

550' E

N		11.0	372.0
C		15.5	367.5
S		19.1	363.9

600' E

S		17.9	365.1
C		14.6	368.4
N		9.6	373.4

650' E

N		8.4	374.6
C		13.1	369.9

383.0

S		16.7	366.3

700' E

S		15.4	367.6
C		12.4	370.6
N		8.1	374.9

750' E

N		6.3	376.7
C		10.5	372.5
S		13.5	369.5

780' E

C		11.4	371.6
N		8.6	374.4

800' E

S		12.7	370.3
C		10.5	372.5
N		5.1	377.9

825.4' E of Tyler on No. 819.02 - - - - 50 } = J

N		2.0	381.0
C		6.0	377.0
S		11.1	371.9

383.00

		56.38' E of J on No 50 " " " " So		
S			10.7	372.3
C			6.7	376.3
N			1.6	381.4
		106.38' E on No 100 " " So		
N			0.6	382.4
C			5.4	377.6
S			9.8	373.2
		156.38' E on No 150 " " So		
S			8.4	374.6
C			2.9	380.1
T.P.	12.73	394.96	0.77	382.23
N			11.6	383.~~3~~4
		206.38' E on No 200 " " So		
N			9.5	385.~~4~~5
C			13.5	381.~~4~~5
S			18.5	376.~~4~~5
		256.38' E on No 250 " " So		
S			16.1	378.~~8~~9
C			11.5	383.~~4~~5

394.96

N		7.9	387.~~0~~1
	300.4' E on No 249.3 " " So } = K.		
N		7.2	387.~~7~~8
C		11.6	383.~~3~~4
S.		16.9	378.~~0~~1
	50' E on No. 55.09 " " So		
S		12.1	382.~~8~~9
C		7.7	387.~~2~~3
N		5.2	389.~~7~~8
	100' E on No 105.09 " " So		
N		2.7	392.~~2~~3
C		5.6	389.~~3~~4
S		11.1	383.~~8~~9
	150' E on No 155.09 " " So		
S		9.7	385.~~2~~3
C		4.8	390.~~1~~2
N		1.9	393.~~0~~1
	194' E on No 206.01 " " So } = L		
N		1.4	393.~~5~~6
C		4.2	390.~~7~~8

		394.96		
S			10.0	~~384.9~~ 385.0
		50' E on No 57.02 " " So		
S			6.4	388.~~5~~6
T.P.	12.04	406.74	0.26	394.70
C			13.0	393.7
N			9.2	397.5
		100' E on No. 107.02 " " So.		
N			7.8	398.9
C			11.4	395.3
S			16.1	390.6
		142.02' E on So.		
S			16.3	390.4
		147.02' E on So.		
S			19.3	387.4
		150' E on No 157.02 " " So		
S			18.7	388.0
C			12.9	393.8
N			6.6	400.1
		192.02' E on So		
S			16.6	390.1

		406.7		
		200' E on No. 207.02 " " So.		
N			4.7	402.0
C			9.0	397.7
S			13.2	393.5
		232.02' E on So.		
S			12.4	394.3
		250' E on No 257.02 " " So		
S			13.8	392.9
C			7.0	399.7
N			2.7	404.0
		299.6' E on No 300.4 " " So } = M.		
N			1.9	404.8
C			4.4	402.3
S			10.0	396.7
		54.46' E on No 50' " " So		
S			8.2	398.5
C			4.6	402.1
N			2.0	404.7
T.P.	12.42	418.57	0.59	406.15

	418.57		
	106.26' E on No		
	100' ↙ - So.		
N	10.6	408.0	
C	13.7	404.9	
S	17.8	400.8	
	156.26' E on No		
	150' ↙ - So.		
S	14.5	404.1	
C	10.2	408.4	
N	6.5	412.1	
	206.26' E on No.		
	200 ↙ - So.		
N	4.2	414.2	
C	7.7	410.7	
S	12.7	405.9	
	256.26' E on No		
	250' ↙ - So.		
S	10.8	407.8	
C	5.9	412.7	
N	2.0	416.6	
T.P. 1246	430.40 0.63	417.94	
	306.26' E on No.		
	300' ↙ - So.		
N	11.3	419.1	
C	15.2	415.2	

	430.4		
S	19.4	411.0	
	356.26' E on No		
	350' ↙ - So.		
S	17.4	413.0	
C	12.7	417.7	
N	8.5	421.9	
	406.26' E on No		
	400' ↙ - So.		
N	6.3	424.1	
C	10.0	420.4	
S	14.1	416.3	
	447.10' E on No		
	452' ↙ - So. } = N/		
S	13.1	417.3	
C	9.2	421.2	
N	6.7	423.7	
	50' E on No		
	61.24 ↙ - So.		
N	1.1	429.3	
C	5.2	425.2	
S	10.9	419.5	
	100' E on No		
	111.24 ↙ - So.		
S	9.8	420.6	
C	2.6	427.9	

TP	12.15	442.10	0.45	429.95
N			9.6	432.5
		149.7' E on No 169.7' ~ ~ So. } = O		
N			8.6	433.7
C			11.6	430.5
S			18.8	423.3
		50' E on No 58.66 ~ ~ So		
S			12.8	429.3
C			7.3	434.8
N			4.2	437.9
		100' E on No 108.66 ~ ~ So		
N			1.5	440.6
C			4.0	438.1
S			7.9	434.2
		150' E on No 158.66 ~ ~ So		
S			2.3	439.8
C			1.0	441.1
T.P.	12.55	454.54	0.11	441.99
N			10.1	444.4

454.5

SUTTER 29

200' E on No
208.66 ~ ~ So

N	7.3	447.2
C	9.6	444.9
S	9.5	445.0

250' E on No
258.66 ~ ~ So

S	5.5	449.0
C	5.5	449.0
N	4.5	450.0

300' E on No
308.66 ~ ~ So

N	1.8	452.7
C	2.6	452.1
T.P. 9.44	462.60 1.38	453.16
S.	9.2	453.4

335.8' E on No. } = P
344.52 ~ ~ So }

S	7.6	455.0
C	8.6	454.0
N	7.5	455.1
BM.	7.48	455.12 Hub SW Sutter + Copeland

60' E on No
66.48 ~ ~ So = S.L. ORANGE COPELAND AVE

N	7.5	455.1

462.6

C	7.9	454.7
S	7.2	455.4
SECT Q		
S	7.5	455.1
C	6.8	455.8
N	5.5	457.1
SECT R.		
N	5.8	456.8
C	5.1	457.5
S	7.2	455.4
[79.4]: E	= Rt Ls to 406 on 16	
S	5.1	457.5
C	4.7	457.9
N	4.2	458.4
S.L. Robinson Ave.		
N	4.2	458.4
C	2.6	460.0
S	2.6	460.0

11/17 Gregory Moore Miller

CROSS SECTION OF HOLLYWOOD DRIVE from W.L. of West Hollywood To E.L of Sutter St.

40' wide 10' curbs 5' quarters

So 1/2 of St. graded.

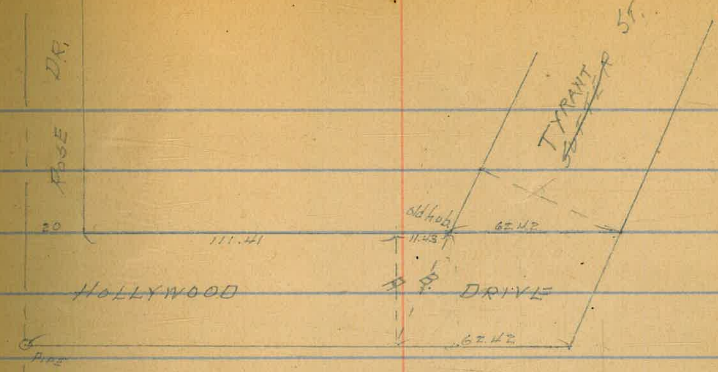
B.M.	3.89	167.76		163.87	R.R. spike in pole So. side Co. Blvd opposite yellow house W. W. Hollywood
T.P.	9.58	169.26	8.08	159.68	

W.L of West Hollywood

H	3.8	165.5	
cl	4.4	164.9	
1/4	4.6	164.7	
c	4.8	164.5	
1/4	5.0	164.3	
cl	5.3	164.0	
S	5.2	164.1	= grade

5' East

S	5.7	163.6	= grade
cl	5.4	163.9	
1/4	5.2	164.1	
c	5.0	164.3	
1/4	4.8	164.5	
cl	4.5	164.8	
H	4.1	165.2	



10' East

H	3.7	165.6	
cl	5.0	164.3	
1/4	5.4	163.9	
c	5.6	163.7	
1/4	5.4	163.9	
cl	5.6	163.7	
S	5.8	163.5	= grade

20' East = E.L Rose Dr

S	6.1	163.2	= grade
cl	6.6	162.7	
1/4	6.0	163.3	
c	5.9	163.4	
1/4	5.8	163.5	
cl	4.2	165.1	
H	3.2	166.1	

2' East.

N	2.1	167.2
cl-	3.0	166.3
1/4	4.4	164.9
C	6.3	163.0
1/4	6.3	163.0
cl-	6.9	162.4
S	6.2	163.1 = grade

25' East.

S	7.6	161.7 = grade
cl-	8.0	161.3
1/4	7.2	162.1
C	7.2	162.1
+3	6.4	162.9
1/4	2.9	166.4
cl-	2.6	166.7
N	2.4	166.9

47' E

N	3.6	165.7
cl-	4.6	164.7

+2	5.1	164.2
1/4	7.5	161.8
+2	8.4	160.9
C	8.7	160.6
1/4	8.8	160.5
cl-	9.0	160.3
S	9.3	160.0 = grade

50' E

S	10.1	159.2 = grade
cl-	9.9	159.4
1/4	9.9	159.4
C	10.0	159.3
1/4	10.1	159.2
cl-	11.0	158.3
N	10.9	158.4

64' E

N	12.6	156.7
cl-	12.2	157.1
1/4	11.4	157.9
C	10.5	158.8

169.26

1/4	10.3	159.0	
cb	10.0	159.3	
S	10.4	158.9	=grade
75' E			
S	11.2	158.1	=grade
cb	10.9	158.4	
1/4	11.3	158.0	
c	11.5	157.8	
1/4	13.0	156.3	
cb	13.2	156.1	
N	13.3	156.0	
11.41' E = SECT A.			
N	12.5	156.8	
cb	13.5	155.8	
1/4	13.3	156.0	
c	12.7	156.6	
1/4	12.5	156.8	
cb	12.5	156.8	
S	12.6	156.7	

11.43' E. of A on No. } = W.L. Sutter St.
" " " " " So.

S	12.6	156.7
cb	12.6	156.7
1/4	12.6	156.7
c	12.8	156.5
1/4	13.6	155.7
cb	13.6	155.7
N	13.4	155.9
10.4' E = N. Curb of Sutter		
N	13.2	156.1
cb	13.5	155.8
1/4	13.3	156.0
c	12.9	156.4
1/4	13.0	156.3
cb	12.9	156.4
S	13.2	156.1
10.4' E = W 1/4 of Sutter		
S	13.3	156.0
cb	13.0	156.3
1/4	13.1	156.2

169.26

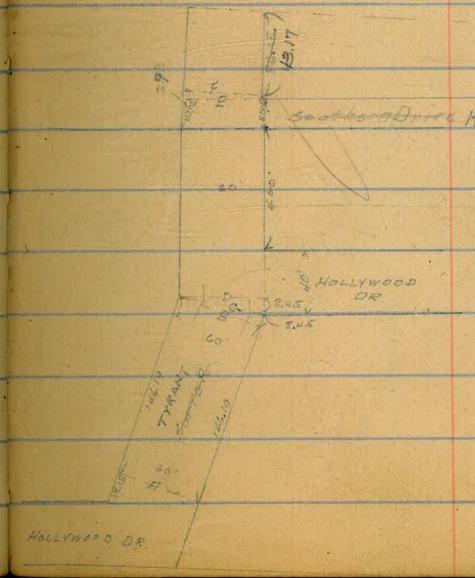
C	130	156.3
1/4	132	156.1
cb	130	156.3
N	125	156.8
10.41 E = Center Sutter St		
N	127	156.6
cb	130	156.3
1/4	129	156.4
C	130	156.3
1/4	132	156.1
cb	132	156.1
S	134	155.11
10.41 E = E 1/4 Sutter St		
S	144	154.9
cb	137	155.6
1/4	136	155.7
C	135	155.8
1/4	137	155.6
cb	135	155.8
N	146	154.7

TP 328	161.03	1145	157.81
10.44 E = E Cb Sutter St			
N		68	154.2
cb		65	154.5
1/4		64	154.6
C		63	154.7
1/4		62	154.8
cb		62	154.8
S		61	154.9
10.44 E = E-L Sutter St			
S		62	154.8
cb		63	154.7
1/4		63	154.7
C		64	154.6
1/4		66	154.4
Cb		66	154.4
N		68	154.2

8/24/17 Gregory Moore Miller

CROSS SECTION OF DARANT ~~SUTTER~~ STREET. 60' St
From No. Line of Hollywood Dr. 10' walks
To Detroit St. 10' 1/2's

BM.	8.21	166.02	157.81	T.P. on preceding page
		N.L. HOLLYWOOD DR.		
W		10.1	155.9	
ch		10.1	155.9	
1/2		9.3	156.7	
C.		9.5	156.5	
1/2		11.5	154.5	
ch		11.7	154.3	
E		11.8	154.2	
	17.15 No on West 00 " East	= SECT. A.		
E		11.8	154.2	
ch		11.8	154.2	
1/2		11.5	154.5	
+5		9.3	156.7	
C.		9.2	156.8	
1/2		8.9	157.1	
ch		9.2	156.8	
W		9.6	156.4	



166.0 ↵

50' N/O.

W	6.9	159.1	
⌀	6.4	159.6	
1/4	6.2	159.8	
C	6.0	160.0	
+7	6.2	159.8	
1/4	8.4	157.6	
+7	12.3	153.7	
⌀	12.4	153.6	
E	12.5	153.5	

78' N/O.

E	12.5	153.5	
⌀	5.5	160.5	
+3	3.8	162.2	
1/4	3.9	162.1	
C	3.9	162.1	grade
1/4	4.3	161.7	
⌀	5.7	160.3	
W	8.4	157.6	=creek

106' N/O.

W	8.4	157.6	creek
⌀	8.5	157.5	creek
+2	8.2	157.8	creek
1/4	4.9	161.1	
C	2.6	163.4	=grade
1/4	2.4	163.6	
⌀	2.2	163.8	
E	2.6	163.4	
+20	12.9	153.1	

146.11 N/O = SECT. B

E	0.3	165.7	
⌀	0.4	165.6	=grade
1/4	1.5	164.5	
C	7.1	158.9	
+4	8.3	157.7	=creek
1/4	8.2	157.8	creek
⌀	8.3	157.7	creek
W	7.6	158.4	creek
+10	6.0	160.0	

SECT C = S.L. of Hollywood on East

-10			6.0	160.0	
W			7.6	158.4	creek
cl			8.5	157.5	creek
1/4			8.2	157.8	creek
+6			8.1	157.9	creek
C			7.1	158.9	
1/4			1.5	164.5	
cl			0.3	165.7	
E			0.0	166.0	grade
TP	6.33	172.06	0.39	165.73	

SECT D.

E			.58	166.3	
cl			6.2	165.9	
+8			7.1	165.0	
1/4			9.2	162.9	
+8			13.2	158.9	creek
C			13.6	158.5	creek
1/4			14.2	157.9	creek
cl			14.3	157.8	creek
W			13.6	158.5	creek

+10			12.1	160.0	

So. Curb of Hollywood Dr.

-10			12.0	160.1	
W			13.7	158.4	creek
cl			14.3	1578	creek
1/4			14.2	157.9	
C			13.6	158.5	
+3			13.2	158.9	creek
1/4			9.2	162.9	
+3			7.1	165.0	
cl			6.2	165.9	
E			5.8	166.3	

So. Quarter.

E			5.9	166.2	
cl			6.3	165.8	
+6			6.8	165.3	
1/4			10.0	162.1	
+5			12.6	159.5	creek
C			13.4	158.7	"
1/4			14.2	157.9	"

1725.6

cb	13.6	158.5	creek
W	13.5	158.6	〃
+10	10.9	161.2	
Center			
-10.	9.8	162.3	
W	12.9	159.2	
+2	13.6	158.5	creek
cb	13.6	158.5	〃
1/4	14.2	157.9	〃
c	13.8	158.3	〃
+4	12.7	159.4	〃
1/4	10.4	161.7	
+6	7.0	165.1	
cb	6.3	165.8	
E	5.8	166.3	
No. Quarter			
E	5.9	166.2	
cb	6.3	165.8	
+2	6.6	165.5	
1/4	11.5	160.6	

+3	13.0	159.1	creek
c	13.3	158.8	creek
1/4	14.1	158.0	〃
+6	14.2	157.9	〃
cb	13.5	158.6	〃
W	12.2	159.9	
+10	9.2	162.9	
No. Curb			
-10	8.2	163.9	
W	11.2	160.9	
cb	13.3	158.8	
+5	14.2	157.9	creek
1/4	14.1	158.0	〃
c	13.7	158.4	〃
+7	13.0	159.1	
1/4	11.1	161.0	
+8	6.9	165.2	
cb	6.3	165.8	
E	5.8	166.3	

17206

N/L. HOLLYWOOD DR

1			
E	5.8	166.3	
cb	6.2	165.9	
+3	6.9	165.2	
1/2	11.5	160.6	
+3	13.1	159.0	
c	13.4	158.7	creek
1/2	14.3	157.8	" "
cb	13.8	158.3	" "
+7	12.3	159.8	
W0	9.5	162.6	
+5	8.2	163.9	
	15' N0.		
-5	6.8	165.3	
W	8.3	163.8	
cb	12.6	159.5	
+2	13.8	158.3	creek
1/2	13.9	158.2	" "
c	13.0	159.1	" "
1/2	11.9	160.2	" "

+7	6.4	165.7	
cb	5.9	166.2	
E	6.5	165.6	
	27' N0		
E	5.4	166.7	
cb	5.7	166.4	
1/2	11.6	160.5	
+2	12.7	159.4	creek
c	13.1	159.0	" "
1/2	13.4	158.7	" "
cb	14.0	158.1	" "
+5	14.0	158.1	" "
W	13.0	159.1	" "
+10	8.2	163.9	
	15' N0		
-15	12.2	159.9	
W	13.9	158.2	creek
cb	13.3	158.8	" "
1/2	13.0	159.1	" "
c	12.7	159.4	" "

	172.26		
1/4			
	10.1	162.0	
ab	5.1	167.0	
E	4.7	167.4	grade cut 2
	75 No.		
E	3.9	168.2	grade
ab	3.9	168.2	
1/4	4.7	167.4	
1/4	7.9	164.2	
C	9.9	162.2	
1/4	11.3	160.8	
ab	12.4	159.7	
W	12.4	159.7	
+30	13.4	158.7	creek
	100 No.		
-35	12.8	159.3	creek
W	10.4	161.7	
ab	9.1	163.0	
1/4	8.8	163.3	
C	7.0	165.1	
1/4	5.7	166.4	

+5	3.4	168.7	
ab	2.6	169.5	
E	2.5	169.6	grade cut 1.5
TP. 10.73	182.19	060	171.46
	150' No.		
E	7.5	174.7	grade cut 1.5
ab	8.1	174.1	
1/4	9.4	172.8	
C	10.8	171.4	
1/4	12.1	170.1	
ab	13.6	168.6	
W	15.1	167.1	
+13	22.7	159.5	creek
+30	22.4	159.8	" "
	175 No.		
-35	22.4	159.8	creek
-25	21.2	160.8	" "
-10	15.1	166.8	
W	12.7	169.5	
ab	10.9	171.3	

½	9.2	173.0
C	7.7	174.5
½	6.4	175.8
dr	5.3	176.9
E	4.9	177.3
	200' No	
E	2.9	179.3
dr	3.6	178.6
½	4.3	177.9
C	5.7	176.5
½	7.2	175.0
dr	9.2	173.0
W	11.7	170.5
+20	18.5	163.7
+30	20.7	161.5
+40	21.3	160.9
	240' No	
−40	20.5	161.7 creek
−20	18.3	163.9
W	11.4	170.8

dr	8.9	173.3
½	6.4	175.8
C	4.6	177.6
½	2.9	179.3
dr	1.7	180.5
+8	0.8	181.4
E	0.0	182.2
	260' No	
E	1.3	180.9
+5	1.7	180.5
dr	3.0	179.2
½	5.1	177.1
C	6.3	175.9
½	8.3	173.9
dr	11.4	170.8
W	14.3	167.9
+16	19.4	162.8
+35	20.8	161.4 creek
	273 No.	
−25	20.2	162.0

-10		20.7	161.5 creek
W		18.9	163.3
dr		16.2	166.0
1/4		13.5	168.7
C		10.9	171.3
1/4		9.2	172.8
dr		7.4	174.8
E		4.9	177.3
	285' No.		
E		10.3	171.9
dr		13.2	169.0
TP	4.25	17.461	11.83 170.36
1/4		7.0	167.6
C		9.1	165.5
1/4		10.3	164.3
dr		11.6	163.0
W		13.1	161.5 creek
+10		13.1	161.5 " "
+20		11.6	163.0

	292' No.		
-20		9.4	165.2
-10		11.5	163.1
W		13.1	161.5 creek
dr		13.0	161.6 " "
1/4		11.6	163.0
C		10.9	163.7
1/4		10.0	164.6
dr		8.4	166.2
E		5.2	169.4
+10		1.7	172.9
	316' No.		
20		10.9	163.7
E		12.7	161.9 creek
dr		12.8	161.8 " "
+5		12.8	161.8 " "
1/4		11.9	162.7
C		10.9	163.7
1/4		9.2	165.4
dr		7.7	166.9

17461

W	7.0	167.6
+10	5.8	168.8
323' No.		
-10	4.4	170.2
W	5.3	169.3
ob	6.5	168.1
1/4	7.2	167.4
C	8.3	166.3
1/4	9.7	164.9
ob	11.4	163.2
E	12.6	162.0 creek
+25	12.4	162.2 "
335' No.		
-25	9.6	164.8
E	8.2	166.2
ob	6.5	168.1
1/4	5.6	169.0
C	4.5	170.1
1/4	3.9	170.7
ob	3.3	171.3

W	2.5	172.1
+10	1.8	172.8
T.P 951	18348	0.64 173.97
350' No		
W	8.4	175.1
ob	9.3	174.2
1/4	10.1	173.4
C	11.0	172.5
1/4	11.9	171.6
ob	13.0	170.5
E	14.3	169.2
+25	17.2	166.3
375' No.		
-25	16.3	167.2
E	12.1	171.4
ob	10.6	172.9
1/4	9.1	174.4
C	7.6	175.9
1/4	6.3	177.2
ob	5.3	178.2

18348.

W			4.3	179.2	
		400' No. = N.L. W. Hollywood = S.L. Southern Dr. (40 St, 10' abv)			
W			0.9	182.6	
cl			2.0	181.5	
1/4			3.5	180.0	
c			5.3	178.2	
1/4			7.4	176.1	
cl			9.5	174.0	
E			11.5	172.0	
+25			16.9	166.6	
T.P.	6.49	185.84	4.13	179.35	Pipe Ctr. Sutter & Southern Dr.
		So. Curb ~~Southern Drive~~ Kenwood St			
-25			19.4	166.4	
E			14.1	171.7	
cl			11.5	174.3	
1/4			9.6	176.2	
c			7.3	178.5	
1/4			5.0	180.8	
cl			3.2	182.6	
W			2.1	183.7	

	So. 1/4		
W		1.6	184.2
cl		2.8	183.0
1/4		4.6	181.2
c		7.2	178.6
1/4		9.6	176.2
cl		11.8	174.0
E		14.2	171.6
+25		19.4	166.4
	Center		
-25		19.6	166.2
E		14.3	171.5
cl		12.0	173.8
1/4		9.4	176.4
c		6.8	179.0
1/4		4.3	181.5
cl		2.2	183.6
W		1.1	184.7
	No. 1/4		
W		0.7	185.1

185.84

cb		1.9	183.9
1/4		4.2	181.6
c		7.1	178.7
1/4		9.6	176.2
cb		12.0	173.8
E		14.3	171.5
+25		19.3	166.5
	No. Curb		
-25		19.3	166.5
E		15.1	170.7
cb		12.0	173.8
1/4		9.7	176.1
c		7.1	178.7
1/4		4.1	181.7
cb		1.8	184.0
W.		0.5	185.3
Sect E	No. Line ~~Southern Dr.~~ Kenwood St.		
W		0.8	185.0
cb		2.3	183.5
1/4		4.8	181.0

c		7.7	178.1
1/4		10.2	175.6
cb		12.6	173.2
E		16.3	169.5
+25		19.5	166.3
	00 No. of NL on East 2.93 - - - - - West } = SECT. ~~IX~~ F		*
-25		19.5	166.3
E		16.3	169.5
cb		12.8	173.0
1/4		10.3	175.5
c		7.8	178.0
1/4		4.8	181.0
cb		2.4	183.4
N		0.9	184.9
	20' No.		
W		1.4	184.4
cb		4.5	181.3
1/4		7.4	178.4
c		10.4	175.4
1/4		13.1	172.7

185.84

ab	16.2	169.6
E	17.3	168.5
+15	18.8	167.0
+25	22.4	163.4 creek
(484.17)	43.17' No. = PC.	
-15	16.3	169.5
-7	21.7	164.1 creek
E	18.7	167.1
ab	17.2	168.6
1/4	16.2	169.6
C	13.5	172.3
1/4	10.6	175.2
ab	7.3	178.5
W	4.1	181.7
	12.78' No. on West of PC	
	12.11' - - East "	
W	6.2	179.6
ab	9.8	176.0
1/4	13.3	172.5
C	16.1	169.7
1/4	17.0	168.8

ab	18.2	167.6
+6	21.5	164.3 creek
E	21.6	164.2 creek
+15	18.3	173.5
	25.56 No. of PC. on W	
	24.22 " " " E	
-10	10.9	174.9
E	16.0	169.8
ab	18.9	166.9
1/4	21.5	164.3 creek
C	17.6	168.2
1/4	16.3	169.5
ab	13.0	172.8
W	10.2	175.6
	38.34' No of PC. on W	
	36.33' " " " E	
-15	16.6	169.2
-10	19.6	166.2 creek
W	20.8	165.0 "
ab	21.0	164.8 " "
1/4	21.0	164.8 " "
C	17.8	168.0

185.84

1/4		16.6	169.2
cl		15.7	170.1
E		11.7	174.1
+10		7.5	178.3
	42.34' No. of P.C. on W		
	40.11 " " " E		
+15		7.4	178.4
E		11.1	174.7
cl		14.8	171.0
1/4		16.1	169.7
C		17.0	168.8
1/4		17.7	168.1
cl		19.6	166.2
W		20.8	165.0 creek
+10		20.8	165.0 "
+15		19.2	166.6
+25		13.7	172.1
	51.13' No. of P.C. on W		
	48.44 " " " E		
-15		16.6	169.2
-17		20.2	165.6 creek
-W		17.0	168.8

W		16.7	169.1
cl		16.5	169.3
1/4		16.5	169.3
C		15.6	170.2
1/4		14.7	171.1
cl		12.3	173.5
E		9.3	176.5
+10		6.3	179.5
	63.42' No. of P.C. on W		
	60.55 " " " E		(5T46 51)
-10		4.4	181.4
E		7.3	178.5
cl		10.7	175.1
1/4		12.1	173.7
C		13.0	172.8
1/4		14.0	171.8
cl		14.5	171.3
W		14.8	171.0
+15		16.6	169.2
+25		19.0	166.8 creek
+29		19.1	166.7 "

1858 ft

76.70' No. o X P.C. on W
72.69' " " " " E

-30'			19.0	166.8	
-23			15.7	170.1	
W			14.2	171.6	
cb			13.2	172.6	
1/4			12.0	173.8	
c			10.6	175.2	
1/4			9.4	176.4	
cb			8.8	177.0	
E			8.0	177.8	

102.26' No. o X P.C. on W
96.90 " " " " E

E			2.7	183.1	
cb			3.8	182.0	
1/4			5.3	180.5	
c			7.2	178.6	✓
1/4			9.1	176.7	
cb			10.8	175.0	
W			12.3	173.5	
+25			15.6	170.2	
+30			18.6	167.2	creek

127.83' No. o X P.C. on W
121.12 " " " " E

-25			14.1	171.7	
-15			18.5	167.3	creek
W			12.1	173.7	
cb			9.6	176.2	
1/4			6.9	178.9	
c			4.7	181.1	✓
1/4			2.5	183.3	
T.P.	5.16	189.56	1.44	184.40	
cb			3.9	185.7	
E			2.7	186.9	

153.39 No. o X P.C. on W
145.35 " " " " E

E			1.7	187.9	
cb			3.5	186.1	
1/4			6.1	183.5	
c			9.0	180.6	✓
1/4			12.1	177.5	
cb			15.7	173.9	
W			19.4	170.2	
+1			20.9	168.7	creek

	189.56	
+25	14.0	175.6
	166.17 No. of PC on W	
	157.46 - - - - - E	
-25	12.6	177.0
W	20.5	169.1 creek
cl.	17.4	172.2
1/4	14.2	175.4
C	10.5	179.1 ✓
1/4	7.3	182.3
cl.	4.2	185.2
E	1.7	187.9
	178.95 No. of PC on W	
	169.57 - - - - - E.	
E	2.5	187.1
cl.	5.2	184.2
1/4	8.7	180.9
C	11.7	177.9 ✓
1/4	16.5	173.1
cl.	17.3	172.3
+4	18.0	171.6
+7	20.4	169.2 creek
W	19.2	170.4

+25	13.1	176.5
	204.52 No. of PC on W	
	192.80 - - - - - E	
-20	10.5	179.1
W	15.4	174.2
cl.	18.2	171.4
+2	20.1	169.5 creek
+5	20.2	169.4 ✓
1/4	17.2	172.0
C	15.1	174.5 ✓
1/4	11.7	177.9
cl.	8.0	181.6
E	4.1	185.5
	230.08 No. of PC on W	
	218.02 - - - - - E	
E	5.5	184.1
cl.	10.0	179.6
TP. 8.65	187.11	11.08 178.48
1/4	11.6	175.5
C	14.3	172.8 ✓
+3	16.5	170.6
+8	17.4	169.7 creek

¼	15.6	171.5
ab	12.7	174.4
W	9.7	177.4
+15	7.6	179.5
255.65' No. of PC on W 342.75 " " " E		= E.C.
-10	5.4	181.7
W	6.3	180.8
ab	8.4	178.7
¼	12.1	175.0
C	14.1	173.0 ✓
+3	14.7	172.4
+6	16.9	170.2 creek
¼	14.4	172.7
ab	9.9	177.2
E	4.0	183.1
20' No. of EC.		
-5	4.3	182.8
E	6.9	180.2
ab	13.7	173.4
+3	16.3	170.8 creek
+5	16.3	170.8 ✓✓

¼	19.3	173.8
C	18.3	174.8 ✓
¼	9.1	178.0 ~~183.0~~
ab	6.3	180.8
W	4.2	182.9
35' No. of EC.		
W	3.1	184.0
ab	5.2	181.9
¼	8.1	179.0
C	10.5	176.6 ✓
¼	12.4	174.7
ab	14.0	173.1
+2	14.8	172.3
+3	16.5	170.6 creek
+6	16.5	170.6 ✓✓
E	12.9	174.2
+10	5.1	182.0
45' No.		
-10	8.8	178.3
E	16.1	171.0 creek

ab	13.0	174.1
1/4	11.6	175.5
c	9.7	177.4 ✓
1/4	7.7	179.4
ab	5.6	181.5
W	3.6	183.7
	55' N.	
W	4.6	182.7
ab	6.8	180.3
1/4	8.6	178.5
c	10.1	177.0 ✓
1/4	11.4	175.7
ab	13.0	174.1
E	13.3	173.8
+3	15.9	171.2 creek
+6	16.0	171.1 " "
+15	9.1	178.0
	84' N.	
-25	8.0	179.1
-17	13.8	173.3 creek

13	13.9	173.2 creek.
E	11.4	175.7
ab	10.4	176.7
1/4	9.7	177.4
c	9.3	177.8 ✓
1/4	9.3	177.8
ab	9.6	177.5
W	9.5	177.6
+20	7.0 ← (?) wire	
	125' N.	
W	1.2	185.9
ab	1.3	185.8
1/4	3.0	184.1
c	4.9	182.2 ✓
1/4	6.8	180.3
ab	8.3	178.8
E	9.3	177.8
+30	11.3	175.8
+35	13.1	174.0 creek

140' No.

-25	12.9	174.2 creek
-10	11.0	176.1
E	11.5	175.6
cl-	12.0	175.1 creek
1/4	11.9	175.2 "
+5	11.7	175.4 "
C	10.4	176.7 ✓
1/4	9.0	178.1
cl-	6.5	180.6
W	2.7	184.4

148' No.

-5	2.8	184.3
W	5.2	181.9
cl-	8.5	178.6
1/4	9.5	177.6
C	11.8	175.3 ✓ creek
1/4	10.5	176.6
cl-	11.1	176.0
E	12.7	174.4 creek

+20	11.9	175.2
+25	10.0	177.1

156' No.

-25	7.9	179.2
-15	10.5	176.6
E	10.6	176.5
cl.	9.7	177.4
1/4	9.7	177.4
C.	10.8	176.3 ✓
+2	11.8	175.3 creek
+5	11.8	175.3 creek
1/4	10.4	176.7
cl.	8.9	178.2
W	7.6	179.5
+10	3.3	183.8

190 No.

-20	5.0	182.1
W	9.0	178.1
+6	11.1	176.0 creek
cl-	10.9	176.2 "
1/4	7.1	180.0

187.11

C	5.0	182.1 ✓
1/4	4.4	182.7
cl	3.6	183.5
E	2.7	184.4
+10	1.6	185.5
204' No.		
-	+ 1.0	188.1
E	0.3	186.8
cl	1.6	185.5
1/4	2.5	184.6
C	3.4	183.7 ✓
1/4	4.7	188.4
cl	7.8	179.3
E — MUST MEAN W-WSC	10.9	176.2 check
+7	10.9	176.2 ✓
+20	5.4	181.7
225' No.		
-23	8.3	178.8
W	6.7	180.4
cl	4.9	182.2

1/4	2.7	184.4
C	1.2	185.9 ✓
1/4	0.1	187.0
TP 1211 199.05 175.8	0.17	186.94
cl	10.7	188.4
E	9.3	189.8
260 No.		
E	5.4	193.7
cl	6.3	192.8
1/4	7.7	191.4
C	9.7	189.4 ✓
1/4	18.0	187.1
cl	15.0	184.1
W	16.7	182.4
+25	19.5	179.6
300 No. = PC		
-25	22.0	177.1
W	15.0	184.1
cl	12.6	186.5
1/4	10.2	188.9

199.05

C		7.9	191.2	✓
1/4		6.0	193.1	
ob		4.1	195.0	
E		2.69	196.4	on hub
	25.59 No. of P.C on W 24.28 - - - - E			
E		1.7	197.4	
ob		3.6	195.5	
1/4		5.4	193.7	
C		7.1	192.0	✓
1/4		8.8	190.3	
ob		11.0	188.1	
W		14.0	185.1	
+20		20.4	178.7	creek
	5118' No. of P.C. on W 4856' - - - - E			
-20		20.0	179.1	
W		14.3	184.8	
ob		11.1	188.0	
1/4		8.8	190.3	
C		6.7	192.4	✓
1/4		5.0	194.1	

ob			3.1	196.0	
E			0.9	198.2	
T.P.	5.01	202.61 ~~203.61~~	1.45	197.60 ~~198.60~~	
		4677' No. of P.C on W 7284 - - - - E			
E			2.5	200.1	
ob			3.9	198.7	
1/4			5.9	196.7	
C			8.1	194.5	✓
1/4			10.4	192.2	
ob			13.4	189.2	
W			17.7	184.9	
+13			23.4	179.2	creek
+18			23.3	179.3	
+20			22.2	180.4	
		102.36' No of P.C on W 97.17' - - - - E } = S.L. Brooklyn 40' wide 10' cbs 5 1/4			
-25			20.4	182.2	
-19			23.3	179.3	creek
-16			23.3	179.3	
W			17.7	184.9	
ob			12.5	190.1	

	~~203.6~~ 202.61		
1/4		9.0	193.6
C		6.9	195.7 ✓
1/4		5.1	197.5
ab		3.0	199.6
E		0.7	201.9
	11.34' No. of 3L on W 10.76' " " " E		= So Curb
E		0.4	202.2
ab		2.8	199.8
1/4		4.5	198.1
C		6.6	196.0 ✓
1/4		9.1	193.5
ab		12.7	189.9
W		18.3	184.3
+15		22.7	179.9 creek
+18		22.7	179.9 " "
+25		19.2	183.4
	5.67' No. of 26 on W 5.38' " " " E		= So. Quarter
-25		19.0	183.6
-18		23.0	179.6 creek
-15		23.0	179.6 ✓

W		18.7	183.9
ab		13.6	189.0
1/4		9.8	192.8
C		6.7	195.9 ✓
1/4		4.4	198.2
ab		2.9	199.7
E		0.5	202.1
	5.67' No. of 1/4 on W 5.38 " " " E		= Center
E		0.5	202.1
ab		2.9	199.7
1/4		4.6	198.0
C		7.0	195.6 ✓
1/4		10.3	192.3
ab		14.0	188.6
W		18.8	183.8
+14		23.0	179.6 creek
+16		23.0	179.6 ✓
+25		19.0	183.6
	5.67' No. of Center on W 5.37 " " " E		= No. Quarter
		18.6	184.0

~~203.61~~ 202.61

-16	23.0	179.6
-12	23.0	179.6
-8	20.0	182.6
W	18.7	183.9
d	14.7	187.9
1/4	10.6	192.0
c	7.5	195.1 ✓
1/4	5.1	197.5
d	3.3	199.3
E	0.5	202.1

5.67' No. of No. 1/4 on W } = No. Curb
5.38' " " " " on E

E	0.8	201.8
d	3.4	199.2
1/4	5.4	197.2
c	8.3	194.3 ✓
1/4	10.9	191.7
d	15.2	187.4
W	18.7	183.9
+9	20.3	182.3
+14	23.0	179.6 creek

+16	23.0	179.6 creek
+20	20.0	182.6

11.36 No. of N. curb on W } = N.L. Brooklyn Ave.
10.75 No. of " " " E

-20	20.4	182.2
-16	22.5	180.1 creek
-14	22.5	180.1 "
-8	19.7	182.9
W	19.0	183.6
d	15.8	186.8
1/4	12.0	190.6 –
c	8.4	194.2 ✓
1/4	5.8	196.8
d	3.3	199.3
E	1.1	201.5

31.30' No. of N.L. on W
29.78' " " " " E

T.P. 4.71	202.24 ~~203.24~~	5.08	197.53 ~~198.53~~
E		0.9	201.3
d		3.5	198.7
1/4		5.8	196.4
c		9.3	192.9 ✓
1/4		12.8	189.4

	203.24 202.24		
cl-	17.0	185.2	
W	18.7	183.5	
+10	22.0	180.2	creek
+12	22.0	180.2	✓
+25	16.6	185.6	
	56.48 No. of NL on W 54.06 " " " E		= EC
-20	14.6	187.6	
W	20.9	181.3	creek
+5	18.8	183.4	
cl-	17.8	184.4	
1/4	14.5	187.7	
C	9.6	192.6	✓
1/2	5.7	196.5	
cl-	3.3	198.9	
E	1.3	200.9	
	15' No. of EC.		
E	1.6	200.6	
cl-	3.5	198.7	
1/2	6.2	196.0	
C	9.5	192.7	✓

1/2	14.8	187.4	
cl-	20.2	182.0	creek
+3	20.6	181.6	
W	18.3	183.9	
+20	13.0	189.2	
	40' No. of EC.		
-20	12.5	189.7	
W	16.8	185.4	
cl-	17.3	184.9	
+6	17.5	184.7	
1/4	19.0	183.2	
+5	20.3	181.9	creek
C	18.0	184.2	✓
+7	13.5	188.7	
1/4	10.9	191.3	
cl-	5.0	197.2	
E	0.9	201.3	
T.P 3.44	205.07 206.07	0.61	201.63 202.63
	65 No. of EC.		
E	3.5	201.7	

~~206.07~~ 205.07

ob		10.4	194.7	
1/4		16.4	188.7	
c		21.5	183.8	✓
+5		22.4	182.7	creek
1/4		20.6	184.5	
ob		19.5	185.6	
W		18.7	186.4	
+20		14.7	190.4	
	85' No.			
-20		14.4	190.7	
W		19.0	186.1	
+8		22.0	183.1	creek
ob		22.0	183.1	✓✓
+4		22.0	183.1	✓✓
1/4		19.7	185.4	
+7		19.4	185.7	
c		18.6	186.5	✓
1/4		14.0	191.1	
ob		7.8	197.3	
E		3.2	201.9	

	91' No			
E		2.9	202.2	
ob		7.3	197.8	
1/4		12.6	192.5	
c		18.0	187.1	✓
+5		19.4	185.7	
1/4		19.6	185.5	
ob		21.8	183.3	creek
W		22.0	183.1	✓✓
+10		17.1	188.0	
+20		14.9	190.2	
	110' No			
-20		16.0	189.1	
-10		21.0	184.1	creek
-6		21.0	184.1	✓✓
W		19.4	185.7	
ob		19.0	186.1	
1/2		17.5	187.6	
c		13.8	191.3	✓
1/4		8.5	196.6	

~~206.07~~
205.07

cl-	4.7	200.9
E	2.2	202.9
	135' No.	
E	1.3	203.8
cl	3.1	202.0
1/4	4.9	200.2
C	7.9	197.2
1/4	12.2	192.9
cl-	16.0	189.1
W	17.9	187.2
+8	21.0	184.1 creek
+11	21.0	184.1 "
+20	18.6	186.3
	185' No. = PC.	
-30	17.6	187.5
-22	20.6	184.5 creek
-20	20.6	184.5 "
W	12.9	192.2
cl-	10.2	194.9
1/4	7.4	197.7

SUTTER .59

C	5.6	199.5 ✓
1/4	3.7	201.4
cl-	2.0	203.1
E	0.5	204.6
	49.25' No. of PC on W	
	46.84' " " " E	
E	+0.3	205.4
cl-	1.7	203.4
1/4	3.5	201.6
C	4.7	200.4
1/4	5.8	199.3
cl-	7.1	198.0
W	8.2	196.9
+20	12.7	192.4
	98.50' No. of PC on W	
	92.45' " " " E	
-20	9.1	196.0
W	6.3	198.8
cl-	4.8	200.3
1/4	4.0	201.1
C	3.3	201.8
1/4	2.3	202.8

~~206.07~~
205.07

cb		1.2	203.9
T.P. 4.75	208.74 ~~204.74~~	2.08	203.99 ~~204.99~~
E		3.6	205.1
	147.75' No. o X P.C. on W 188.72 " " " " E		
E		2.7	206.0
cb		3.6	205.1
1/4		4.6	204.1
c		5.5	203.2
1/4		6.3	202.4
cb		7.2	201.5
W		8.0	200.7
+20		10.9	197.8
	147.00' No. o X P.C. on W 184.96 " " " " E		
−20		12.5	196.2
W		6.8	201.9
cb		5.6	203.1
1/4		5.2	203.5
C		4.6	204.1
1/4		3.8	204.9
cb		2.9	205.8

E		1.8	206.9
	212' No. o X P.C. on W 199.05' " " " " E		
E		1.6	207.1
cb		2.6	206.1
1/4		3.6	205.1
C		4.5	204.2
1/4		5.4	203.3
cb		6.5	202.2
W		8.1	200.6
+15		13.0	195.7
	221.62' No. o X P.C. on W 208.07' " " " " E		
−20		19.0	189.7 creek.
−15		14.0	194.7
W		13.7	195.0
cb		9.8	198.9
+5		7.1	201.6
1/4		6.2	202.5
c		4.6	204.1
1/4		3.4	205.3
cb		2.3	206.4
E		1.3	207.4

~~209.74~~
208.74

227.62' No. of P.C. on W
213.71' - - - - E

V

E		1.0	207.7
cb		2.1	206.6
1/4		3.4	205.3
C		4.8	203.9
1/4		6.9	201.8
cb		12.7	196.0
W		19.5	189.2 creek
+20		18.0	190.7
	246.25' No. of P.C. on W 231.18' - - - - - E } = EC		
-20		16.4	192.3
W		17.5	191.2
+4		19.3	189.4 creek
+6		19.4	189.3 "
cb		15.8	192.9
1/4		10.0	198.7
C		5.5	203.2
1/4		3.4	205.3
cb		1.8	206.9
E		0.6	208.1

26' No

E		+0.6	209.3
cb		0.6	208.1
1/4		2.4	206.3
C		5.1	203.6
1/4		9.8	198.9
cb		14.1	194.6
+8		18.9	189.8 creek
W		18.9	189.8 "
+6		15.5	193.2
+20		14.0	194.7

35' No

-20		13.6	195.1
-7		15.7	193.0
-2		18.8	189.9 creek
W		18.9	189.8 "
cb		13.3	195.4
1/4		9.3	199.4
C		5.0	203.7
1/4		2.4	206.3
TP	5.07	211.48 ~~216.46~~	8.33	206.41 ~~207.41~~

~~21248~~
21148

c.b.		3.0	208.5
E		1.5	210.0
	50' No. of EC		
E		1.7	209.8
cl-		3.4	208.1
1/4		5.6	205.9
C		8.4	203.1
1/4		12.1	199.4
cl-		16.1	195.4
W		19.3	192.2
+3		21.3	190.2
+5		21.3	190.2
+12		17.5	194.0
+20		16.0	195.5
	75' No.		
-20		15.0	196.5
-10		12.9	193.6
-6		20.7	190.8
-W		20.7	190.8
W		17.9	193.6
cl-		15.3	196.2
1/4		11.3	200.2
C		7.7	203.8
1/4		4.9	206.6
cl-		2.8	208.7
E		1.4	210.1
	100' No.		
E		0.9	210.6
cl-		2.1	209.4
1/4		4.3	207.2
C		7.4	204.1
1/4		11.1	200.4
cl-		15.1	196.4
W		18.6	192.9
+4		20.2	191.3 creek
+20		14.3	197.2
	105' No.		
-20		13.8	197.7
W		20.1	191.4 creek

cl-		15.3	196.2
1/4		10.5	201.0
C		6.9	204.6
1/4		4.2	207.3
cl-		2.0	209.5
E		0.8	210.7
	115' No.		
E		0.7	210.8
cl-		2.8	209.3
1/4		3.6	207.9
C		6.9	204.6
1/4		10.7	200.8
cl-		15.0	193.5
+5		19.2	192.3 creek
W		17.5	194.0
+20		13.3	198.2
	120' No.		
-20		13.0	198.5
W		16.5	195.0
cl-		19.0	192.5 creek
1/4		15.0	193.5
C		9.5	202.0
1/4		6.8	204.7
cl-		2.6	208.9
E		0.6	210.9
	125' No.		
E		0.8	210.7
+8		3.0	208.5
1/4		5.7	205.8
		11.3	200.2
C		18.5	193.0 creek
1/4		19.1	192.4
+5		19.2	192.3
cl-		17.7	193.8
W		16.0	195.5
+20		13.3	198.2
	130' No.		
-20		12.7	198.8
W		15.5	196.0

~~212.48~~
211.48

d		16.0	195.5	
1/4		15.6	195.9	
c		16.9	194.6	
+6		18.5	193.0	creek
+8		18.5	193.0	creek
1/4		18.0	193.5	
d		12.0	199.5	
E		6.2	205.3	✓
+5		2.8	208.7	
	158' No ✓			
-7		2.6	208.9	
E		6.9	204.6	
d		13.9	197.6	
1/4		17.9	193.6	creek
+5		18.0	193.5	"
c		16.0	195.5	
1/4		15.6	195.9	
d		15.5	196.0	
W		15.4	196.1	
+30		14.4	197.1	
	167' No ✓			
-30		16.3	195.2	creek
W		17.1	194.4	"
d		16.9	194.6	"
1/4		18.0	193.5	"
c		18.2	193.3	"
1/4		14.7	196.8	
d		10.5	201.0	
E		5.0	206.5	
+5		2.6	208.9	
	172' No			
-5		0.4	211.1	✓
E		3.0	208.5	
d		7.9	203.6	
1/4		13.0	198.5	
+5		14.8	196.7	
c		15.3	196.2	
1/4		15.2	196.3	
d		16.0	195.5	

W			15.2	196.3	
+20			14.8	196.7	
		188' No			
-20			13.1	198.4	
W			13.2	198.3	
d			12.4	199.1	
1/4			11.0	200.5	
c			7.7	203.8	
1/4			4.4	207.1	
d			1.8	209.7	
T.P.	5.14	215.55 ~~216.55~~	1.07	210.41 ~~211.44~~	
E			2.9	212.7	
		205' No			
E			2.9	212.7	
d			4.3	211.3	
1/4			5.6	210.0	✓
c			7.0	208.6	
1/4			8.6	207.0	
d			11.2	204.4	
W			13.8	201.8	
+20			16.3	199.3	
		230' No			
-20			18.7	196.9	creek
-1/2			19.0 / 18.0	196.6 / 197.6	
W			10.6	205.0	
d			8.1	207.5	
1/4			6.7	208.8	
c			5.7	209.9	
1/4			4.7	210.9	
d			3.7	211.9	
E			2.3	213.3	
		265' No			
E			0.7	214.9	
d			2.7	212.8	
1/4			4.0	211.6	
c			4.9	210.7	
1/4			6.3	209.3	
d			9.3	206.3	
W			13.4	202.2	

	216.55		
	215.55		
+11	18.3	197.3	creek
+14	18.3	197.3	" "
+20	15.8	199.8	
380' No.			
−10	18.3	197.3	creek
W	13.4	202.2	
cl-	10.6	205.0	
1/4	6.9	208.7	
C	4.5	211.1	
1/4	3.4	212.2	
cl-	2.3	213.3	
E	1.4	214.2	
350' No.			
E	1.0	214.6	
cl-	1.5	214.1	
1/4	2.6	213.0	
C	4.3	211.3	
1/4	6.3	209.3	
cl-	8.7	206.9	
W	12.2	203.4	
+10	13.3	202.3	
+20	16.8	198.8	creek
375' No.			
−20	16.3	199.3	
−12	13.8	201.8	
W	11.8	203.8	
cl-	9.1	206.5	
1/4	5.6	210.0	
C	3.1	212.5	
1/4	2.5	213.1	
cl-	2.0	213.6	
E	1.4	214.2	
400' No.			
E	1.5	214.1	
cl-	2.4	213.2	
1/4	3.4	212.2	
C	4.8	211.4	
1/4	6.1	209.5	
cl-	8.7	206.9	
W	11.8	203.8	
+11	16.3	199.6	creek

+12	16.0	199.6	creek
+20	13.7	201.9	
435' No.			
−20	11.3	204.3	
−10	15.5	200.1	creek
W	11.5	204.1	
cl-	9.8	205.8	
1/4	6.9	208.7	
C	4.9	210.7	
1/4	3.6	212.0	
cl-	2.8	212.8	
E	2.0	213.6	
465' No.			
E	2.1	213.5	
cl-	3.8	211.8	
1/4	6.3	209.3	
C	8.7	206.9	
1/4	10.3	205.3	
cl-	11.4	204.2	
W	14.2	201.4	creek
+19	14.7	200.9	" "
+20	11.6	204.0	
473 No.			
−20	12.8	202.8	
−16	13.7	201.9	creek
−12	11.5	204.1	
W	13.3	203.3	
+5	12.6	203.0	
cl-	14.1	201.5	creek
1/4	11.3	204.3	
C	9.9	205.7	
1/4	7.7	207.9	
cl-	4.8	210.8	
E	2.7	212.9	
485' No. = PC.			
−5	4.6	211.0	X
E	6.9	208.8	

	~~216.55~~ 215.55			
cb		9.7	205.9	
1/4		12.4	203.2	creek
C		10.7	204.9	
1/4		9.8	205.8	
cb		9.4	206.2	
W		8.3	207.3	
+20		8.9	206.7	
	25.59' No. of PC on W			
E	24.24' " " " E			
-10		2.5	213.1	
E — MUST BE W. (FIX)		3.4	212.2	
cb		4.9	210.7	
1/4		6.1	209.5	
C		8.1	207.5	
1/4		9.1	206.5	
cb		10.7	204.9	
+5		12.0	203.6	creek
E		10.5	205.1	
+15		5.5	210.1	
	51.18' No. of PC on W			
	~~48.54~~ " " " E			
-20		5.7	209.9	
-7		11.0	204.6	
E		10.6	205.0	
cb		7.9	207.7	
1/4		5.8	209.8	
C		3.2	212.4	
1/4		1.4	214.2	
cb		0.4	215.2	
T.P. 13.10	227.34	1.31	214.24	
W	~~240.34~~	11.3	~~215.34~~ 216.0	
	102.36 No. of PC on W			
	97.08 " " " E			
W		5.6	221.7	
cb		6.2	231.1	
1/4		7.3	220.0	
C		8.3	219.0	
1/4		10.2	217.4	
CO		12.9	214.4	
E		18.0	209.3	
+8		20.5	206.8	
+15		21.4	205.9	creek
+17		21.5	206.3	
+20		20.1	207.2	

	153.58' No. on W.			
	145.63 " " E		207.0	
-120		20.3		creek
-15		20.3	207.0	" "
E		15.4	211.9	
CO		11.5	215.8	
1/4		7.7	219.6	
C		5.1	222.2	
1/4		3.5	223.8	
cb		3.1	225.2	
W.		0.7	226.6	
T.P. 12.65	239.16	0.83	226.151	
	~~240.16~~		~~227.51~~	
	204.75' No. of PC on W			
	194.19 " " " E		= EC.	
W		8.7	230.5	
cb		10.2	229.0	
1/4		12.2	227.0	
C		13.7	225.5	
1/4		15.1	224.1	
cb		18.9	220.3	
E		21.6	217.6	
+20		25.8	213.4	
	56.05' No. or East of EC.			
-20		22.0	217.2	
S		15.2	224.0	
W		13.7	225.5	
1/4		11.7	227.5	
C		10.4	228.8	
1/4		8.5	230.7	
cb		6.8	232.4	
N		5.3	233.9	
	106.05 East			
N		2.4	236.8	
cb		4.2	235.0	
1/4		5.8	233.4	
C		7.3	231.9	
1/4		9.5	229.7	
cb		11.6	227.6	

	240 TC 239.16		
S		13.2	226.0
+20		17.8	221.4
	156.05' E		
-20		15.9	223.3
S		12.0	227.2
cb		10.1	229.1
1/4		8.4	230.8
C		6.4	232.8
1/4		4.4	234.8
cb		2.2	236.9
TP 5.61	242.14 243.44	6.63	236.53 ~~237.53~~
N		3.1	239.0
	206.05' E		
N		4.1	238.0
cb		6.2	235.9
1/4		7.8	234.3
C		9.6	232.5
1/4		11.7	230.4
cb		14.1	228.0
S		15.9	226.2
+20		21.4	217.7
	256.05' E		
-20		24.9	217.2
S		16.3	225.8
cb		14.6	227.5
1/4		12.5	229.6
C		11.0	231.1
1/4		9.7	232.4
cb		8.0	234.1
N		6.2	235.9
	306.05' E		
N		4.9	237.2
cb		6.6	235.5
1/4		7.9	234.2
C		9.2	232.9
1/4		10.9	231.2
cb		12.5	229.6
S		15.0	227.1
+20		23.3	218.8

	350' E = P.C.		218.3
-20		23.8	
S		14.6	227.5
cb		11.5	230.6
1/4		9.6	232.5
C		7.7	234.4
1/4		6.2	235.9
cb		4.2	237.9
N		2.7	239.4
	56.05 E of P.C. on Center Line		
N		0.4	241.7
cb		2.0	240.1
1/4		4.0	238.1
C		6.4	235.7
1/4		8.3	233.8
cb		10.9	231.2
S		15.3	226.8
+20		22.9	219.2
	75.82 E of P.C. on Center Line = W.L. of Detroit St. on So.		
-20		22.6	219.5
S		14.2	227.9
cb		10.2	231.9
1/4		7.3	234.8
C		5.5	236.6
1/4		3.3	238.8
TP 12.57	251.07	9.64	238.50 PI hub at Det.
cb		10.1	241.0
N		7.4	243.7
	96.64' E of P.C. on Center Line = W.L. Detroit		
N		5.6	245.5
cb		8.0	243.1
1/4		10.7	240.4
C		13.1	238.0
1/4		15.5	235.6

do	186	2325
5	230	228.1

5/26/19 Gregory, Miller, Shaw.

CROSS SECTION OF MERL[illegible] ~~GRANT~~ ST. = formerly Crescent Drive and HOLLYWOOD DRIVE from County Highway to Sutter St.

40' Sts
10' cbs
5' 1/4's.

on B.M.	2.09	165.96		163.87
℄ Co. Highway				
E			3.6	162.4
W			3.9	162.1
No. Line Co. Highway				
W			4.4	161.6
cb			4.4	161.6
1/4			4.2	161.8
c			4.1	161.9
1/4			4.1	161.9
cb			4.0	162.0
E			4.0	162.0
7.68 No. on W, 00 " " E } = 0.0				
E			4.0	162.0
cb			4.1	161.9
1/4			4.2	161.8
c			4.2	161.8
1/4			4.3	161.7
cb			4.5	161.5
W			4.8	161.2
20' No.				
W			5.9	160.1
cb			4.7	161.3
1/4			4.6	161.4
c			4.4	161.6
1/4			4.4	161.6
cb			4.3	161.7
E			4.4	161.6

36' No.				
-5			7.2	158.8
E			7.7	158.3
+5			7.6	158.4
cb			5.5	160.5
1/4			4.9	161.1
c			4.8	161.2
1/4			5.1	160.9
cb			5.7	160.3
+7			10.4	155.6
W			10.7	155.3
+10			12.1	153.9
42' No.				
-10			11.8	154.2
T.P.	5.49	161.01	10.44	155.52
W			7.0	154.0
+2			6.5	154.5
cb			1.1	159.9
1/4			0.3	160.7
c			0.2	160.8
1/4			0.4	160.6
cb			1.3	159.7
+7			5.5	155.5
E			5.8	155.2
+10			5.8	155.2
55' No.				
-10			5.8	155.2
E			6.0	155.0
+5			6.0	155.0
cb			2.9	158.1
+3			1.2	159.8
1/4			1.0	160.0
c			0.9	160.1
1/4			1.0	160.0
cb			1.7	159.3
+7			6.3	154.7
W			6.7	154.3
+10			6.9	154.1
58' No.				
-10			7.0	154.0
W			6.6	154.4
+2			6.0	
cb			1.6	159.6
+3			4.5	156.5
1/4			3.9	157.1

	161.01		
C		5.2	155.8
1/4		6.0	155.0
cl		5.7	155 3
E		6.0	155 0
+10		5.7	155 3
	60' No.		
-10		5.7	155 3
E		5.9	155 1
cl		6.3	154 7
1/4		6.4	154 6
C		6.3	154 7
1/4		5.8	155 3
cl		5.5	155 5
W		6.7	154 3
+10		7.2	153 8
	65' No.		
-10		7.1	153 9
W		7.0	154 0
cl		6.6	154 4
1/4		6.4	154 6
C		6.3	154 7
1/4		6.2	154 8
cl		6.0	155 0
E		6.3	154 7
+10		6.0	155 0
	70' No.		
-10		6.0	155 0
E		5.9	155 1
+6		5.6	155 4
cl		3.6	157 4
+4		1.5	159 5
1/4		3.2	157 8
C		3.8	157 2
1/4		4.1	156 9
cl		4.6	156 4
+2		3.2	157 8
W		6.3	154 7
+10		6.8	154 2
	74' No.		
-10		3.6	157 4
W		3.7	157 3
+5		3.8	157 2

cl		1.8	159 2
1/4		1.1	159 9
C		1.1	159 9
1/4		1.2	159 8
+2		1.6	159 4
cl		3.3	157 7
+6		5.5	155 5
E		5.7	155 3
+10		5.8	155 2
	80' No.		
-3		2.0	159 0
E		1.9	159 1
cl		1.4	159 6
1/4		1.0	160 0
C		1.0	160 0
1/4		1.1	159 9
cl		1.6	159 4
W		1.9	159 1
+3		1.8	159 2
	85.15' No. on West } = 2' from So. rail.		
	85.05 " " East }		
-3		1.3	159 7
W.		1.3	159 7
		0.56	160.43 = So. rail of West.
cl		1.2	159 8
1/4		1.0	160 0
C		0.9	160 1
1/4		0.9	160 1
cl		1.2	159 8
E		1.2	159 8
		0.48	161 53 = So. rail.
	94.15' No. on West } = 2' from No. rail.		
	94.05 " " " }		
E		1.4	159 6
cl		1.3	159 7
1/4		1.3	159 7
C		1.3	159 7
1/4		1.3	159 7
cl		1.2	159 8
W		1.4	159 6
	44' No.		
W		1.3	159 2
cl		1.6	159 4
1/4		1.6	159 4
C		1.7	159 3
1/4		1.6	159 4

cl		1.8	159 2
E		2.0	159 0
+5		1.9	159 1
	104' No.		
-10		4.1	156 9
E		4.2	156 8
+8		3.3	157 7
cl		2.5	158 5
1/4		1.2	159 8
C		1.1	159 9
1/4		1.1	159 9
cl		1.6	159 4
W		2.6	158 4
+7		2.4	158 6
	108' No.		
-10		5.8	155 2
W		5.6	155 4
+4		5.0	156 0
cl		2.2	158 8
+2		1.4	159 6
1/4		1.2	159 8
C		1.2	159 8
1/4		1.2	159 8
cl		2.9	158 1
+4		4.8	156 2
E		5.2	155 8
+10		5.3	155 7
	115' No.		
-10		5.0	156 0
E		5.1	155 9
+7		5.0	156 0
cl		3.1	157 9
1/4		1.4	159 6
C		1.4	159 6
1/4		1.4	159 6
cl		3.1	157 9
+5		5.2	155 8
W		5.8	155 2
+10		5.9	155 1
	119' No.		
-10		6.7	154 3
W		6.1	154 9
cl		5.3	155 7

1/4		5.2	155 8
C		5.1	155 9
1/4		4.7	156 3
cl		3.6	157 4
+4		5.2	155 8
E		5.4	155 6
+10		5.4	155 6
	121' No.		
-10		5.4	155 6
E		5.5	155 5
+5		5.5	155 5
+7		7.7	153 3
cl		7.9	153 1
1/4		7.0	154 0
C		7.2	153 8
1/4		7.8	153 2
cl		8.1	152 9
W		8.7	152 3
+13		9.6	151 4
	127' No.		
-13		9.5	151 5
W		9.1	151 9
cl		8.8	152 2
1/4		9.0	151 1
C		8.9	152 1
1/4		8.8	152 2
cl		8.8	152 2
E		9.2	151 8
+13		9.2	151 8
	136' No.		
-13		7.5	153 5
E		8.3	152 7
cl		9.0	152 0
1/4		9.1	151 9
C		9.2	151 8
1/4		9.2	151 8
cl		9.1	151 9
W		9.2	151 8
+13		9.5	151 5
	146' No.		
-13		8.6	152 4
W		8.6	152 4
cl		8.8	152 2

	161.01		
1/4		8.7	152.3
C		8.7	152 3
1/4		8.5	152 5
ob		8.3	1527
E		8.6	1524
+13		8.9	1521
	150' No.		
-13		9.8	151 2
E		8.4	152 6
ob		8.1	
1/4		6.9	1541
C		6.4	154 6
1/4		5.5	155 5
ob		4.7	156 3
W		6.9	154 1
+10		5.7	155 3
	154' No.		
-10		5.5	155 5
W		6.1	154 9
+4		5.6	155 4
ob		2.8	158 2
+3		1.5	159 5
1/4		1.4	159 6
C		1.3	159 7
1/4		1.4	159 6
ob		3.5	157 5
+4		4.9	156 1
E.		5.3	155 7
+7		5.4	155 6
	175' No.		
-7		5.0	158 0
E		5.2	155 8
+3		5.2	155 8
ob		2.1	158 9
+2		1.2	158 8
1/4		0.9	160 1
C		1.0	160 0
1/4		1.0	160 0
+3		1.1	159 9
ob		3.2	157 8
+5		5.7	155 3
W.		5.6	155 4

	200' No.		
-10		6.8	154 2
W		6.2	154 8
+3		6.2	154 8
ob		2.1	158 9
+3		0.8	160 2
1/4		0.9	160 1
C		1.0	160 0
1/4		0.5	160 5
ob		1.9	159 1
T.P.	7.09	0.51	160.50 ✓
+4	167.59 ✓	11.0	156 6
E		11.1	156 5
+10		11.5	156 1
	214' No.		
-10		11.5	156 1
E		10.8	156 8
+9		10.3	157 3
ob		8.9	158 7
1/4		6.8	160 8
C		6.8	160 8
1/4		6.8	160 8
+2		7.1	160 5
ob		8.9	158 7
+7		13.0	154 6
W		13.6	154 1
+10		13.9	153 7
	219' No		
-10		13.9	153 7
W		13.6	154 0
+4		12.1	155 5
ob		8.0	159 6
+2		6.9	160 7
1/4		6.6	161 0
C		6.6	161 0
+1		9.1	158 5
1/4		9.7	157 9
ob		10.0	157 6
E.		10.8	156 8
+10		11.6	156 0
	225' No.		
-10		12.1	155 5
E		11.1	156 5
+7		10.9	156 7

167.59

dr	9.1	158	5
1/4	6.7	160	9
+1	9.0	158	6
c	9.0	158	6
+1	6.5	161	1
1/4	6.4	161	2
+4	6.7	160	9
dr	7.4	160	2
+3	10.5	157	1
W	13.3	154	3
+10	13.6	154	0

435' No.

-10	13.2	154	4
W	13.1	154	5
+1	13.0	154	6
dr	6.6	161	0
+2	6.0	161	6
1/4	6.0	161	6
+3	6.1	161	5
+4	7.8	159	8
c	8.1	159	5
+3	7.8	159	8
1/4	6.2	161	4
dr	9.4	158	2
+3	11.5	156	1
E	11.5	156	1
+10	11.4	156	2

255' No.

-15	14.6	156	0
E	11.8	155	8
+5	11.6	156	0
dr	8.1	159	5
+3	5.5	162	1
1/4	5.3	162	3
+2	5.2	162	4
c	6.7	160	9
+2	6.7	160	9
+3	5.3	162	3
1/4	5.1	162	5
dr	5.2	162	4
W	11.7	155	9
+15	13.0	154	6

278' No

-10	7.4	160	2
W	6.3	161	3
dr	3.8	163	8
+5 1/4	4.0	163	6
+3	4.1	163	5
+3.1	5.0	162	6
c	5.2	162	4
+1	4.2	163	4
1/4	4.3	163	3
+2	4.7	162	9
dr	5.9	161	7
+6	10.0	157	6
E	11.1	155	5
+15	11.4	155	2

290' No

-10	5.5	162	1
E	3.9	163	7
+3	4.4	163	2
dr	2.9	164	7
1/4	2.7	164	9
+4	3.4	163	1
c	2.9	164	7
1/4	2.9	164	7
dr	2.7	164	9
+7	2.9	164	7
W	2.4	165	2

300' No

W	1.0	166	6
+2	1.8	165	8
dr	1.9	165	7
1/4	2.0	165	6
c	1.9	165	7
1/4	2.2	165	5
dr	1.9	165	7
+4	1.8	165	8
+7	2.4	165	1
E	1.7	165	9

308.73' No = S.L. Hollywood Dr.

E	1.1	166	5
dr	1.7	165	9
1/4	1.4	166	2
c	1.2	166	4

		167.59			
1/4			1.3	166	3
cb			1.2	166	4
M			0.6	167	0
T.P.	6.00	172.92 ✓	0.67	166.92 ✓	Hub SW Hollywood & Tyrant

40' wide CROSS SECTION HOLLYWOOD DR. from E.L. (Merlin) ~~Tyrant~~ To Saucer (Tyrant)

E.L. ~~Tyrant St.~~ Merlin Drive

So.		6.4	166	5
cb		5.9	167	0
1/4		5.6	167	3
C		5.4	167	5
1/4		5.2	167	7
cb		4.9	168	0
No		4.5	168	4
	E Curb			
No		4.6	168	3
cb		5.2	167	7
1/4		5.5	167	4
C		5.7	167	2
1/4		5.8	167	1
cb		6.4	166	5
So		6.9	166	0
	E Quarter			
So		6.8	166	1
cb		6.1	166	8
1/4		5.7	167	2
C		5.5	167	4
1/4		5.2	167	7
cb		5.0	167	9
No.		4.5	168	4
	Center			
No.		3.9	169	0
cb		4.7	168	2
1/4		5.2	167	7
C		5.5	167	4
1/4		5.6	167	3
cb		6.0	166	9
So.		6.6	166	3
	W. Quarter			
So		6.7	166	2
cb		5.9	167	0
1/4		5.5	167	4

c		5.2	167	7
1/4		4.9	168	0
cb		4.6	168	3
No		3.8	169	1
	W. Curb			
No		3.8	169	1
cb		4.5	168	4
1/4		4.9	168	0
c		5.2	167	7
1/4		5.5	167	4
cb		5.8	167	1
So.		6.6	166	3
	W. Line Tyrant.			
So		6.0	166	9
cb		5.5	167	4
1/4		5.2	167	7
c		4.9	168	0
1/4		4.7	168	2
cb		4.4	168	5
No		3.8	169	1
	25' West			
No.		4.8	168	1
cb		5.0	167	9
1/4		5.2	168	7
c		5.3	168	6
1/4		5.5	168	4
cb		5.7	168	2
So.		5.8	168	1
	50' West			
So		6.2	166	7
cb		5.6	167	3
1/4		5.2	167	7
c		5.0	167	9
1/4		4.9	168	0
cb		4.8	168	1
No		4.9	168	0
	100' West			
No		4.4	168	5
cb		4.8	168	1
1/4		4.8	168	1
c		4.9	168	0
1/4		5.3	167	6

	172.92		
dk	5.5	167	4
So.	5.8	167	1
	150' West		
So	5.7	167	2
dk	5.1	167	8
1/4	4.9	168	0
C	4.6	168	3
1/4	4.5	168	4
dk	4.5	168	4
No.	3.9	169	0
	200' West		
No	3.3	169	6
~~dk~~ +6	4.1	168	8
dk	4.1	168	8
1/4	4.2	168	7
C	4.4	168	5
1/4	4.5	168	4
dk	4.8	168	1
So	5.4	167	5
	233' West		
So.	5.5	167	5
dk	5.6	167	3
1/4	5.5	167	4
C	5.3	167	6
1/4	5.0	167	9
dk	4.9	168	0
No.	4.3	168	6
	258' West = EL Sutter St.		
No.	6.4	166	5
dk	6.3	166	6
1/4	6.5	166	4
C	6.6	166	3
1/4	6.5	166	4
dk	6.5	166	4
So.	6.8	166	1

Single Track. Data for Grade Xing at Tyrant.
3.10 164.35 160.45

36.7' W. of W.L. Tyrant = E. End Bridge 4.02 160.33 = Top rail
108.0 " " " " " " = W " " 4.50 159.85 " " "
200 " " " " " 5.78 158.57
300 " " " " " 6.12 158.23
460 " " " " " to Mouth of 9' cut. 400' long.

100' E of E.L. Tyrant 3.14 161.21 = Top rail
200 " " " " " 1.90 162.45 " " "
300 " " " " " 0.68 163.67 " " "

IMPROVED TABLES

AND

INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent lenth divided by twice the radius.

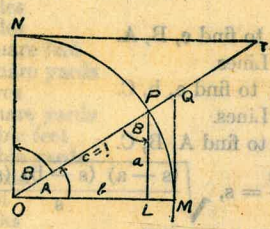


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

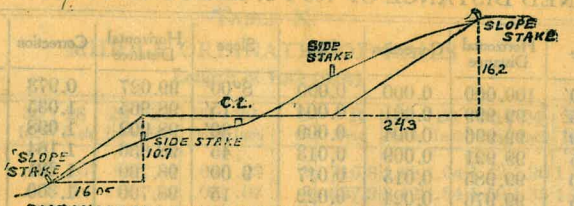
$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \text{Cos } A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \text{Cos } A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5.10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13 05	13.20	13.35	8
9	13 50	13.65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19 35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47 70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50 70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51 90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54.15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58 95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66 75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

151/8
.11
15
15
165
2
167
50
83.50

50 side Road. 250 W of Stratton
NE Encanto & A R 17 oppos yellow horse.

16387
17518

1.0197
4
4.0788.0

64.1
25
89.1
4.9
95

20
36
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70
74
80
85 = 2 So of trail
94 = 2 N
99
104
108
115
119
121
124
127
136 146
150
154
175
200
214
219
225
231
255
272
285
290
30 300

76 4 285
67 85

88.9
89.9
25

8733
873
78.60
765
79.65
1.000
89.65
4.5
85.15

18915
40
7955
308.73

18408
40
8733
3165
873
728

-10	10.9	-10	9.8	260	
W	13.5 cr	W	12.9	~~+ 120~~	~~18.8~~
cb	13.6 cr	+2	13.6	~~+ 80~~	~~20.7~~
1/4	14.2	cb	13.6	~~+ 40~~	~~21.3~~
C	13.4	1/4	14.2	+ 35	20.8 cr
+5	12.6	C	13.8	+ 16	19.4
1/4	10.0	+4	12.7		
+6	6.8	1/4	10.4		
	6.3	+6	7.0		
	5.9		6.3		
			5.8		

50.4

194
3.51
2.54
200.05

18911
40
7955
308.73

294.21
2.54
3.19
299.94
3.19
296.75

21.8
9999