

Otago Case

1022

TRANSIT

398

H. S. CROCKER COMPANY

DRAWING MATERIALS AND
SURVEYING INSTRUMENTS

SAN FRANCISCO

TABLES FOR EXCAVATIONS AND EMBANKMENTS

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING

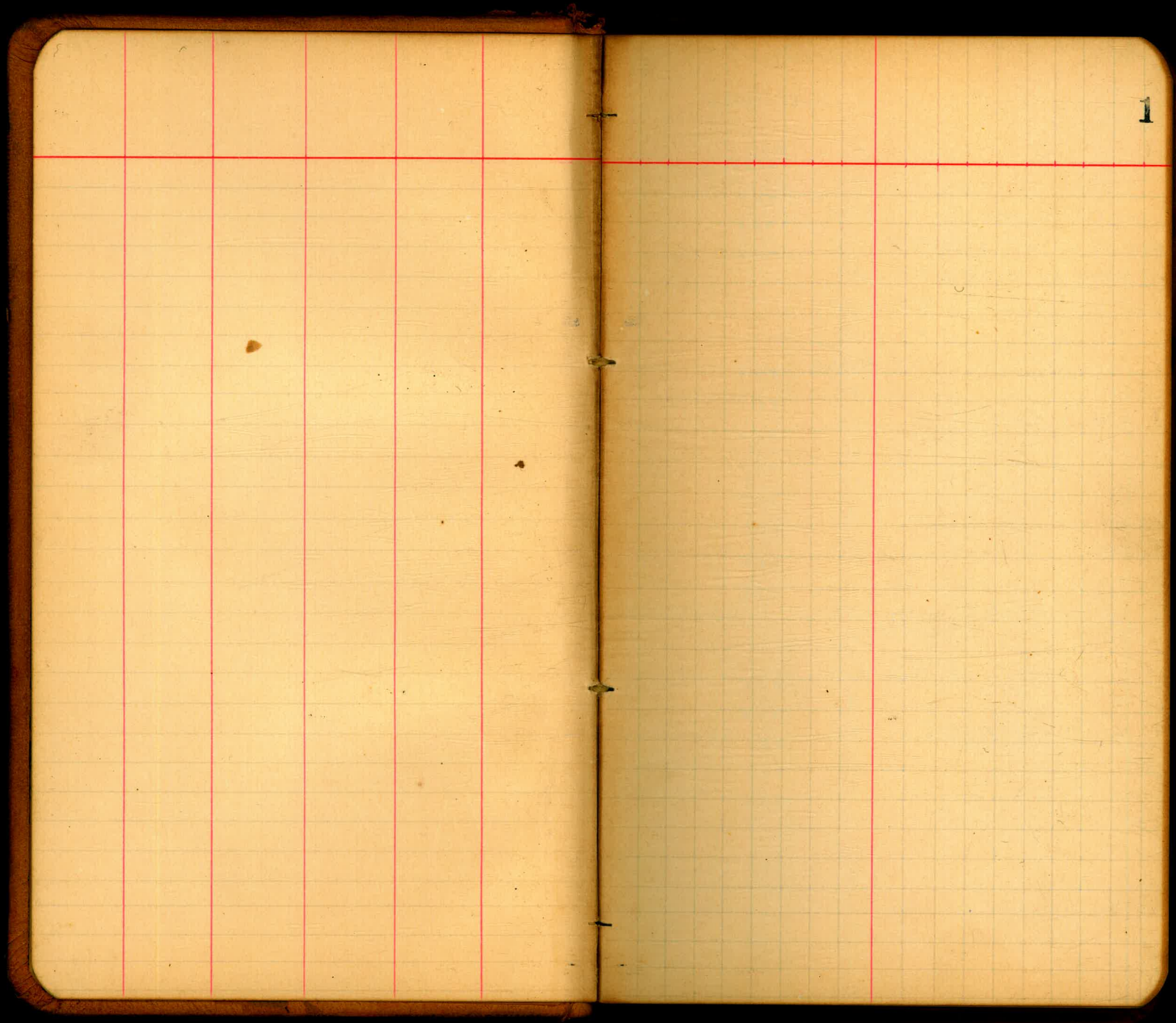
Roadway 18 Feet Wide. Side Slopes 1 to 1.
For Single Track Excavation.

"Copyright, 1895, by Kueffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

FROM
Loring's Book Store
SAN DIEGO, CALIF.



10/26/17
 W. Gregory
 C. Moore
 F. D. Miller

CROSS SECTION OF
 OTAY CREEK
 NEAR OLD MCHENRY RANCH

+	HI	-	Elev.
			96.76
1.48	101.48		100.00
			98.0
Top of Stone wall		+ 0.2	101.7
			93.8
Ground at hole = Sta 0100.		4.0	97.5
			94.6
Half way up Opening of hole		3.2	98.3
{ Hole is 2.0 high } { " 2.1 wide } { " 4.5 deep. }			
			97.8
0+28		5.0	96.5
			91.9
+29		5.9	95.6
			90.4
+41		7.4	94.1
			88.1
+43		9.7	91.8
			86.2
+54		11.6	89.9
			84.6
+73		13.2	88.3
			85.4
1+00		12.4	89.1
			87.5
1+08	9rd 7' to right	10.0	91.5
			85.5
1+11		12.3	89.2
T.P.	7.44	96.69	12.23
			89.25
			83.6
1+16		9.4	87.3
			88.4
1+16	9rd 27.4' to left.	4.6	92.1
			88.1
1+22		9.9	86.8
			83.5
1+24		9.5	87.2
			83.6
1+22		9.1	87.3
			86.6
1+54		6.4	90.3
			86.8
1+71		4.2	92.5
			89.1
1+89		3.9	92.8
			88.3
1+96		4.7	92.0
			86.4
2+00		6.6	90.1

= Top of 2" plank bolted to old Tree stump on South bank of deepest portion of So. Channel.

= Top of old Tree stump on South bank of South Channel.

= Center of present stream

= No. edge of - - -

= S.W. edge of No. channel

	HI.				
	46.69			86.0	
2+14			7.0	84.7	= bottom of No. channel
2+20			6.1	86.9	
2+25			4.9	90.6	
2+50			2.8	88.1	
2+60			2.5	91.8	
2+65			0.9	90.2	
T.P.	951	104.81	1.39	93.9	
2+85			8.1	90.5	
3+00			5.9	94.2	
				92.1	
				95.8	
				95.30	
				92.0	
				96.7	
				95.4	
				98.91	

10/26/17

R.M. Gregory
C.S. Moore
F.D. MillerTRAVERSE LINE
From Sta. 1422 on
CROSS SECTION
LINE SHOWN ON
PAGE 2READINGS ALL IN CREEK BOTTOM
EXCEPT AS NOTED

on T.P.	2.55	91.80	89.25	T.P. on page 2	23+00	56	77.5
Sta 1422 on Page 2 = 00		5.0	83.1		24+00	64	76.5
1+00		5.8	86.8		25+00	70	73.0
2+00		6.2	87.3		26+00	77	75.7
3+00		7.0	86.0		T.P.	3.02	78.61
T.P.	3.60	90.44	81.9		27+00	47	75.59
4+00		5.8	85.6		28+00	51	70.2
5+00		5.7	81.1		29+00	57	73.9
6+00		5.5	84.8		30+00	62	69.8
7+00		6.0	80.9		31+00	66	73.5
8+00		6.0	84.6		32+00	71	69.2
9+00		6.3	80.7		33+00	77	72.4
10+00		6.9	84.4		34+00	85	68.3
T.P.	3.34	88.23	80.7		35+00	88	72.0
11+00		4.5	84.4		36+00	94	67.8
12+00		5.1	80.4		T.P.	3.79	73.10
13+00		6.0	84.1		37+00	63	69.31
14+00		6.5	79.9		38+00	75	63.1
15+00		7.0	83.6		39+00	80	66.8
16+00		7.7	80.0		40+00	85	61.4
17+00		8.3	83.7		41+00	88	65.6
18+00		8.7	79.4		T.P.	4.91	69.31
19+00		9.2	83.1		42+00	55	61.4
T.P.	2.15	82.09	78.5		43+00	62	65.1
20+00		3.5	82.2		44+00	69	60.9
21+00		4.3	78.0		45+00	73	64.6
22+00		4.9	81.7		46+00	79	60.6
			77.5		47+00	84	64.3
			79.0				60.1
			74.9				63.8
			78.6				59.4
			74.1				63.1
			77.8				58.7
			73.5				62.4
			77.2				58.3
							62.0
							57.7
							61.4
							59.2
							60.9

8209

23+00	56	77.5
24+00	64	76.5
25+00	70	73.0
26+00	77	75.7
T.P.	3.02	78.61
27+00	47	71.4
28+00	51	75.1
29+00	57	70.7
30+00	62	74.4
31+00	66	75.59
32+00	71	70.2
33+00	77	73.9
34+00	85	69.8
35+00	88	73.5
36+00	94	69.2
T.P.	3.79	73.10
37+00	63	72.4
38+00	75	68.3
39+00	80	72.0
40+00	85	67.8
41+00	88	71.5
T.P.	4.91	69.31
42+00	55	67.2
43+00	62	70.9
44+00	69	66.4
45+00	73	70.1
46+00	79	66.1
47+00	84	69.8
		65.5
		69.2
		69.31
		63.1
		66.8
		61.4
		65.6
		61.4
		65.1
		60.9
		64.6
		60.6
		64.3
		60.1
		63.8
		59.4
		63.1
		58.7
		62.4
		58.3
		62.0
		57.7
		61.4
		59.2
		60.9

4

69.31.

48+00	8.8	56.8
49+00	9.3	60.5
50+00	10.0	56.3
51+00	10.6	60.0
		55.6
		59.3
		55.0
		58.7

10/26/17
Gregory
Moore
Miller
Earle

CROSS SECTION
AT STA. 44+17
ON TRAVERSE
LINE

EAST SIDE OF TRAVERSE

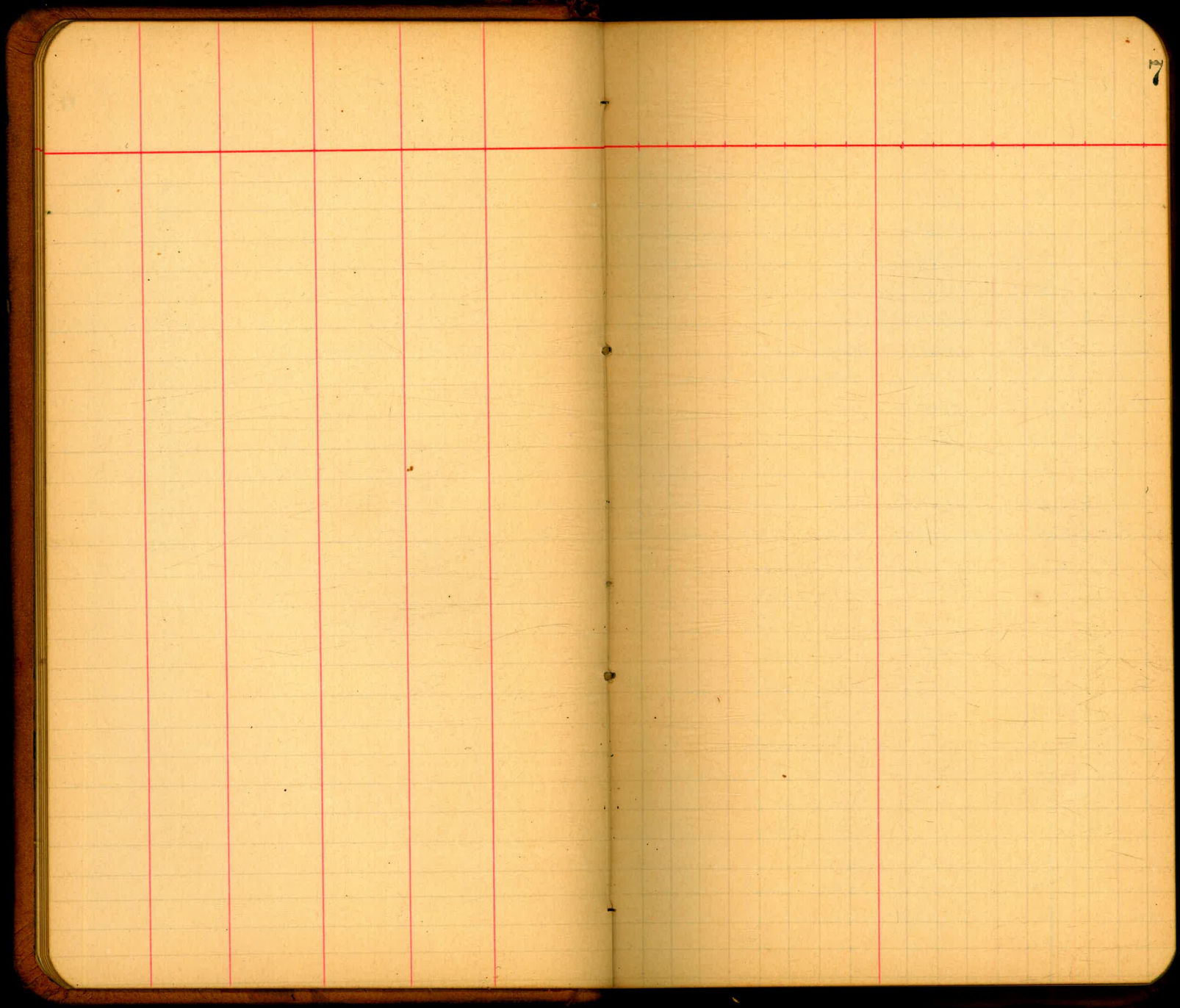
Station	Distance	Offset	Elevation
Sta 44+17 on Traverse = 00	69.31	6.4	59.2
00+13 East of TRAVERSE		6.8	60.9 58.8 62.5
+16 East ✓		5.2	60.4 64.1
+30 East ✓		4.1	61.5 65.2
+65 East -		4.2	61.4 65.1
+71 East ✓		3.7	61.9 65.6
T.P. 810	76.98	0.43	67.98
+72 East of TRAVERSE		8.1	65.7 68.9 70.8
+86 ✓		2.5	74.5
T.P. 1240	88.30	1.08	75.90
+94 East of TRAVERSE		11.4	73.2 76.9
+96		1.5	83.1 86.8
T.P. 816	95.99	0.47	87.83
1+05		7.5	84.8 88.5
1+20		2.6	89.7
1+32		0.6	93.4 94.7 95.4

10/26/17
Gregory
Moore
Miller

CROSS SECTION
AT STA 44+17
ON TRAVERSE LINE

WEST SIDE OF TRAVERSE

Station	Distance	Offset	Elevation
NI. 69.31 from page 4			
00+20 WEST OF TRAV.	6.8		58.8 62.5 59.5
+21 ✓	6.1		63.2 59.0
+39 ✓	6.6		62.7 60.5
+46 ✓	5.1		64.2
T.P. 1231	81.19	0.43	68.88 ← 65.14 page 9
+48 WEST OF TRAVERSE	12.7		64.8 68.5 64.0
+51 ✓	13.5		67.7 73.1
+53 ✓	14.4		76.8 75.2
+56 ✓	2.3		78.9 75.0
+60 ✓	2.5		78.7 77.8
+62 ✓	4.7		76.5 72.6
+75 ✓	4.9		76.3 71.9
+82 ✓	4.6		76.6
T.P. 1244	93.97	0.06	81.13
1+20 WEST OF TRAVERSE	8.8		81.5 85.2
1+43 ✓	4.3		86.0 89.7
1+56 ✓	0.8		89.5 93.2
T.P.	0.08		93.89



10/21/21
 R. Gregory
 C.S. Moore
 F.D. Miller

TRAVERSE LINE
 UP OTAY CREEK
 From site of Lower Otay Dam
 To a point 1200' above old
 McHenry Ranch
 Elevations taken in bed of stream

	+	HI.	-	Elek				
					14		88	74.1
					15		85	74.4
B.M.	3.49	151.20		147.71	16		82	74.7
T.P.	1.27	139.49	12.98	138.22	17		79	75.0
T.P.	0.79	129.58	12.70	126.79	18		77	75.7
T.P.	0.22	114.35	12.95	114.63	19		73	75.6
T.P.	0.46	102.44	12.87	101.98	20		70	75.9
T.P.	0.56	90.09	12.91	89.53	21		66	76.3
T.P.	0.25	77.54	12.80	77.29	T.P.	6.45	32.05	62.7
T.P.	0.74	65.77	12.51	65.02	22		65	76.6
T.P.	0.30	53.11	12.96	52.81	23		61	77.0
T.P.	2.18	42.52	12.77	40.24	24		58	77.3
T.P.	0.04	29.64	12.92	29.60	25		50	28.1
			12.0	17.6	26		47	76.4
				11.6	27		43	76.8
1				10.9	28		37	79.4
2				11.4	29		34	79.7
3				11.2	30		29	30.2
4				11.0	31		25	30.5
5				10.4	32		1.9	31.2
6				10.3	33		1.7	31.4
7				10.2	T.P.	12.59	44.07	1.57
8				9.6	34		12.0	32.1
9				7.2	35		11.7	32.4
10					36		11.1	33.0
T.P.	4.81	32.87	1.58	28.06	37		10.7	33.4
11				10.0	38		10.4	33.7
12				9.5	39		9.8	34.3
13				9.3				

B.M. on top of
 concrete old
 dam west end
 of OTAY DAM. B.M.
 is marked 147.71
 elevation = 147.71
 northing datum = 147.71

= bed of stream

		44.07		
40			9.4	34.7
41			9.1	35.0
42			8.4	35.7
43			8.0	36.1
T.P.	9.08	45.37	7.78	36.29
44			8.6	36.8
45			8.2	37.7
46			7.8	37.6
47			7.4	38.0
48			7.1	38.3
49			6.3	39.1
50			5.1	40.3
51			5.1	40.3
52			4.6	40.8
53			4.1	41.3
T.P.	9.49	51.26	3.60	41.77
54			9.6	41.7
55			9.3	42.0
56			8.9	42.6
57			8.3	43.0
58			7.7	43.6
59			7.3	44.0
60			6.8	44.5
61			6.4	45.0
62			5.9	45.4
T.P.	9.18	55.92	4.52	46.74
63			10.1	45.8

		55.92		
64			9.6	46.3
65			9.2	46.7
66			8.8	47.1
67			7.9	48.0
68			7.0	48.9
69			6.4	49.5
70			5.7	50.2
71			5.3	50.6
72			4.9	51.0
73			4.2	51.7
T.P.	10.39	62.55	3.76	52.16
74			10.1	52.5
75			9.5	53.1
76			9.2	53.4
77			8.5	54.1
78			7.9	54.7
79			7.5	55.1
80			7.0	55.6
81			6.4	56.2
82			5.9	56.7
83			5.4	57.2
84			5.0	57.6
85			4.5	58.1
88 = Sta 44+17 page 4)			3.3	59.3
T.P.	12.97	72.22	3.30	59.25
T.P. check			7.08	65.14 = 68.88 T.P. 6
T.P.	12.30	83.64	0.88	71.34
T.P.	11.27	88.63	6.28	77.36

	+	H I	-	Elev.
		88.63		
T.P.	11.93	93.98	6.58	82.05
T.P.	11.37	103.68	1.67	92.91
T.P.	4.48	105.46	2.70	100.98
T.P.	1.50	97.67	9.29	96.17
T.P.	3.27	88.68	12.26	85.41

Assumed elev of
10680 McHenry
Cross Section

TRAVERSE UP OTHY CREEK

from Sta 1+22 on McHenry X section

00 = Sta 1+22 on McH. X section.		5.8	74.2
1		5.1	82.9
2		4.7	83.6
T.P.	9.28	94.01	3.95
3		9.5	84.0
4		7.9	84.5
5		5.9	86.1
T.P.	6.60	96.41	4.20
6		7.1	88.1
7		5.5	89.3
8		4.2	90.9
T.P.	6.27	99.70	2.98
9		6.0	92.2
10		5.7	93.43
11		4.7	93.7
12		4.3	94.0
			95.0
			95.4

12/7/77
 W. Earle
 R. G. G. G.
 C. Moore
 E. Miller
 R. Schwartz

Cross section of
 Otav Creek
 at a point 1400 feet
 upstream from section
 taken at Pt. of Rocks

on B.M.	4.08	69.22	65.14	BM. on Rock N. 46° of stream at Pt. of Rocks see page 679
T.P.	8.48	74.81	66.33	
T.P.	5.63	78.77	73.14	
Sta 0400 = Ctr. of present stream			10.1	68.7
10' No. of 0400			9.5	69.3
15' ✓ ✓ ✓			8.5	70.3
40' - - ✓			8.0	70.8
48' - - ✓			8.9	69.9
58' ✓ ✓ ✓			8.9	69.9
80' - - ✓			7.8	71.0
85' ✓ ✓ ✓			8.3	70.5
91' - ✓ ✓			8.3	70.5
100' - - ✓			7.3	71.5
150' ✓ ✓ ✓			6.0	72.8
165' - - ✓			5.6	73.2
200' - - ✓			6.1	72.7
230' - - ✓			6.5	72.3
250' - - ✓			5.2	73.6
262' ✓ ✓ ✓			4.3	74.5 = location of Iron wedge
266' - - ✓			6.0	72.8
270' - - ✓			4.6	74.2
300' - - ✓			5.5	73.3
307' - - ✓			6.3	72.5
318' ✓ ✓ ✓			5.8	73.0
333' - - ✓			3.7	75.1 = Top of Bank

78.77

43' So. of 0400	9.8	69.0
49' - - ✓	8.4	70.4
60' - - ✓	4.6	74.2 = Top of Bank
BM.	6.41	72.36

07. Peak
 20' up stream
 from section

Apr 21, 1919

Tom Smallcomb
J.B. Evergreen
N.H. Ramage
Geo. Cromwell
W.C. Earle

12

Ditch about 3' from stone wall
Back of house 6' " " "

Depth of house back to front 30'

Back of house on ground level or 8" above
Front " 2 steps = 1 1/2 ft.

House to bridge all cultivated, oranges for
orchard ^{or. of house + to river} cottonwood trees

Water 1/2 way up in hole in wall
would flood floor of house - floor
of house about same level as
base of hole in wall - 1/2 way up
in hole = 10" to 12" higher than
floor

Hills at back of house settled & house
set in ground

From house to creek just a rock
in sight roadway down slope to
creek - unbroken straight gentle slope
from house to 1 to 1 1/2 ft below floor of br.

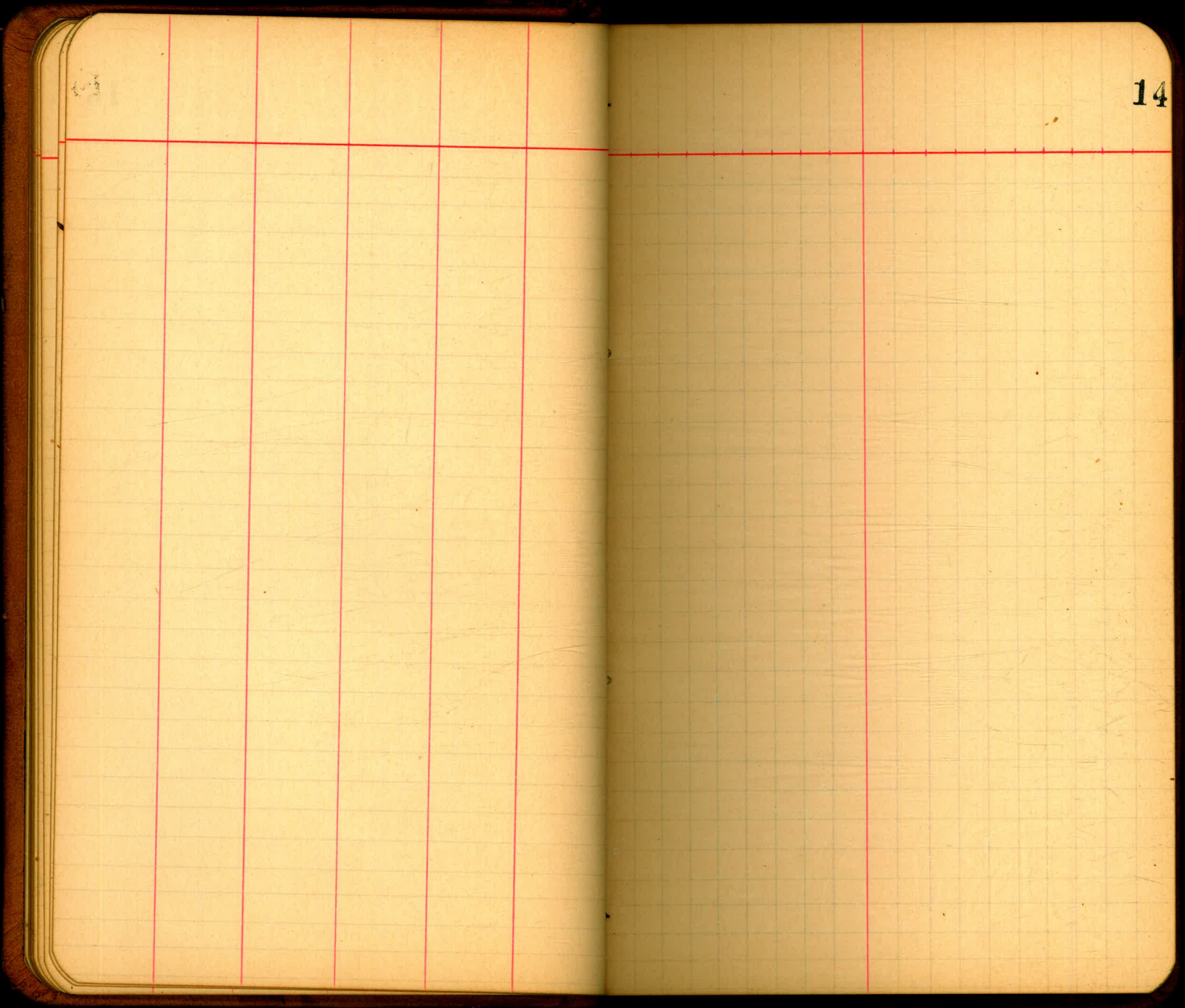
Environ at front of house = at least 6 ft

Point channel about same width
& depth as in 1895

Size then = 5 to 30'

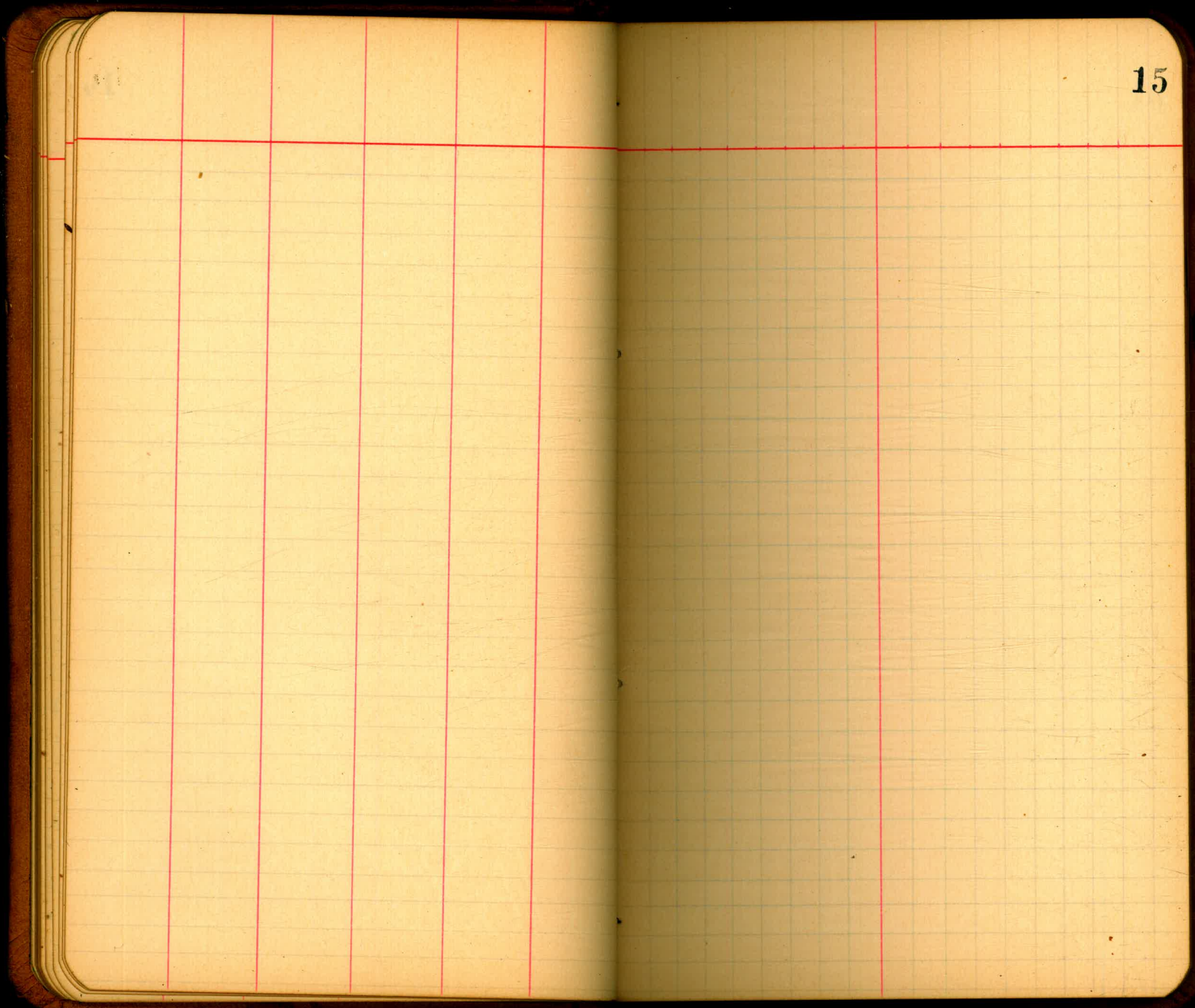
Stone wall on N side channel = approach
to bridge put in by himself

No. channel not in existence in 1895
Had barn, shop & peach orchard where
present no channel
Slope from stone wall gradual to
north to present ground

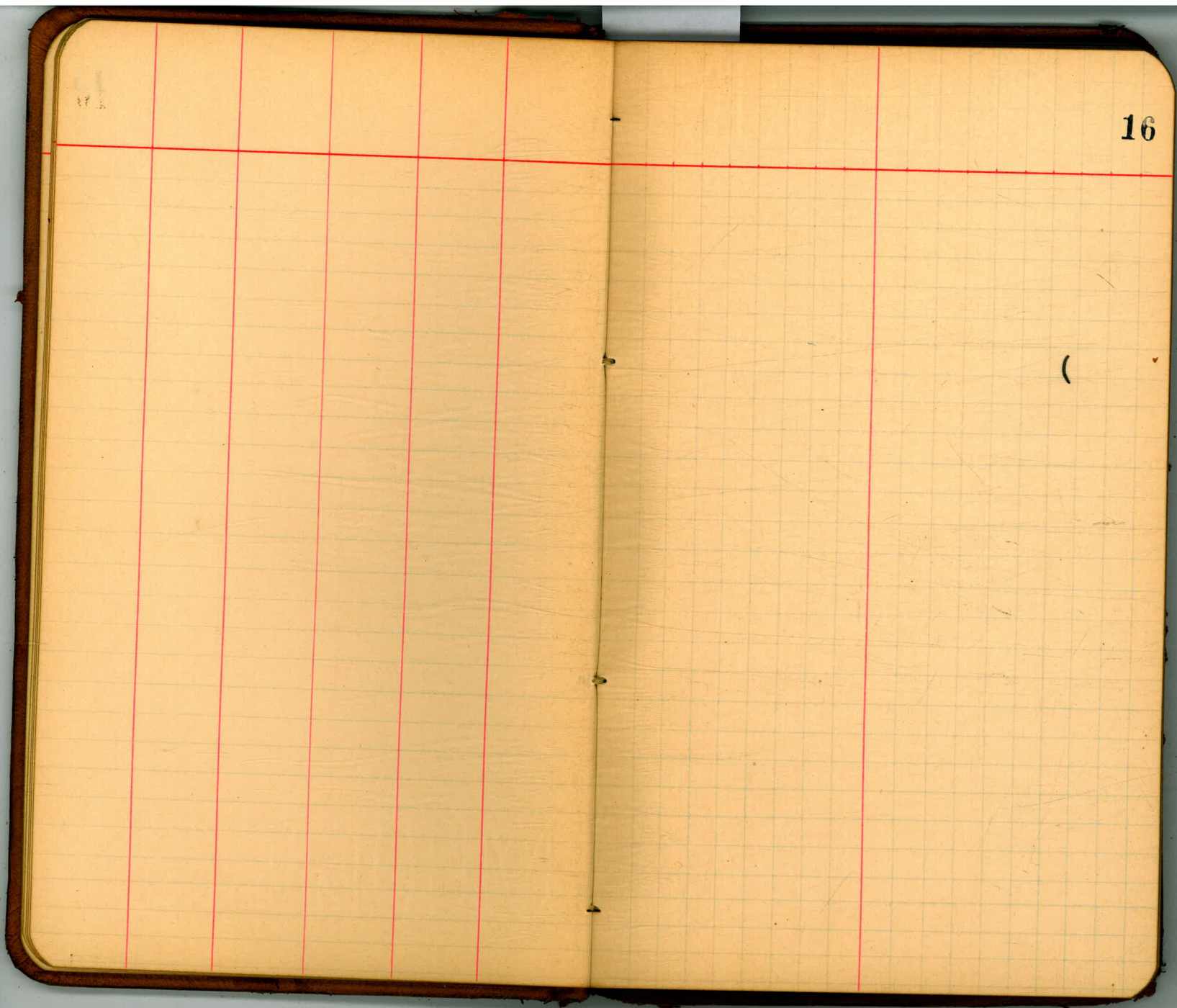


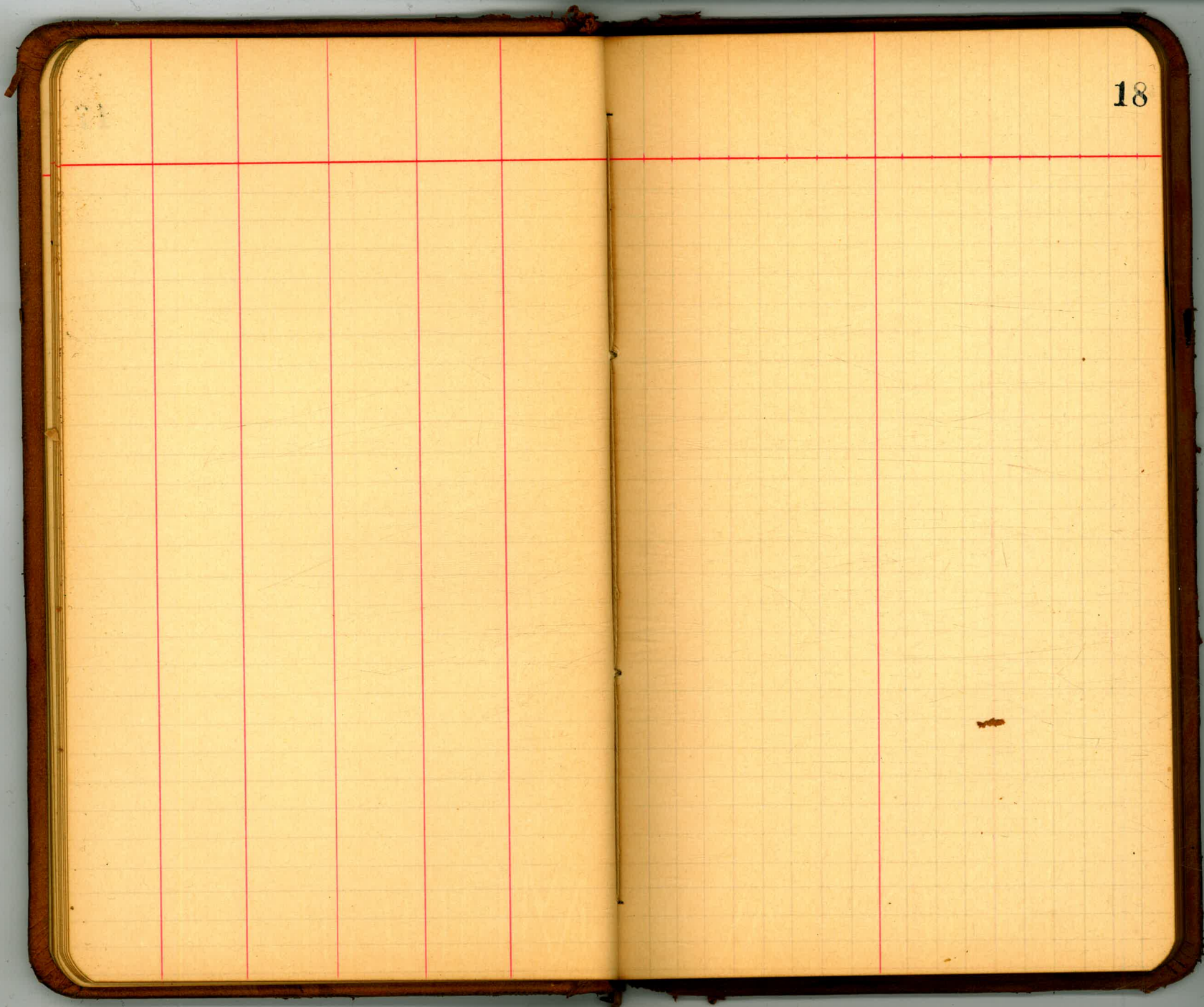
13

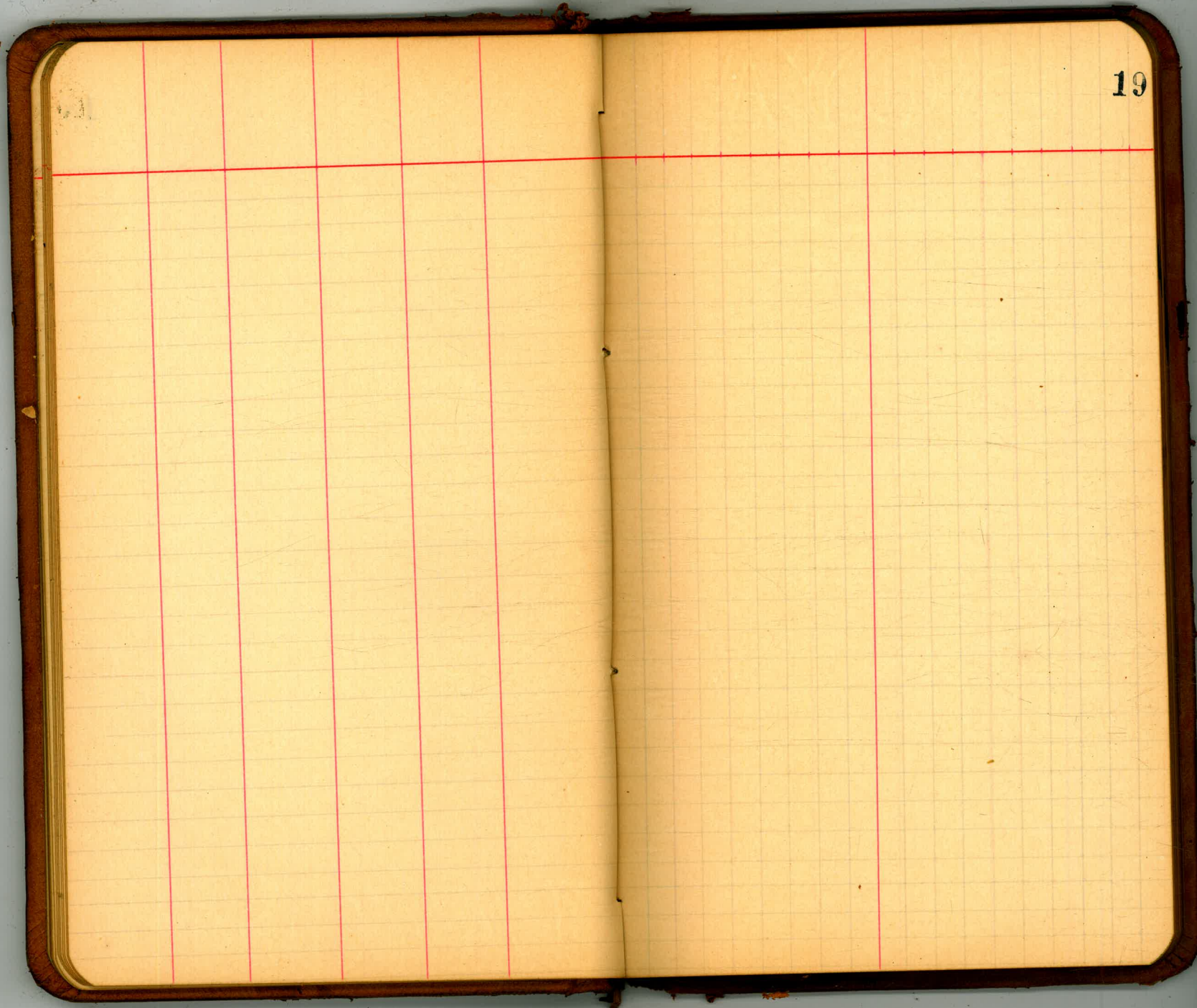
14



17



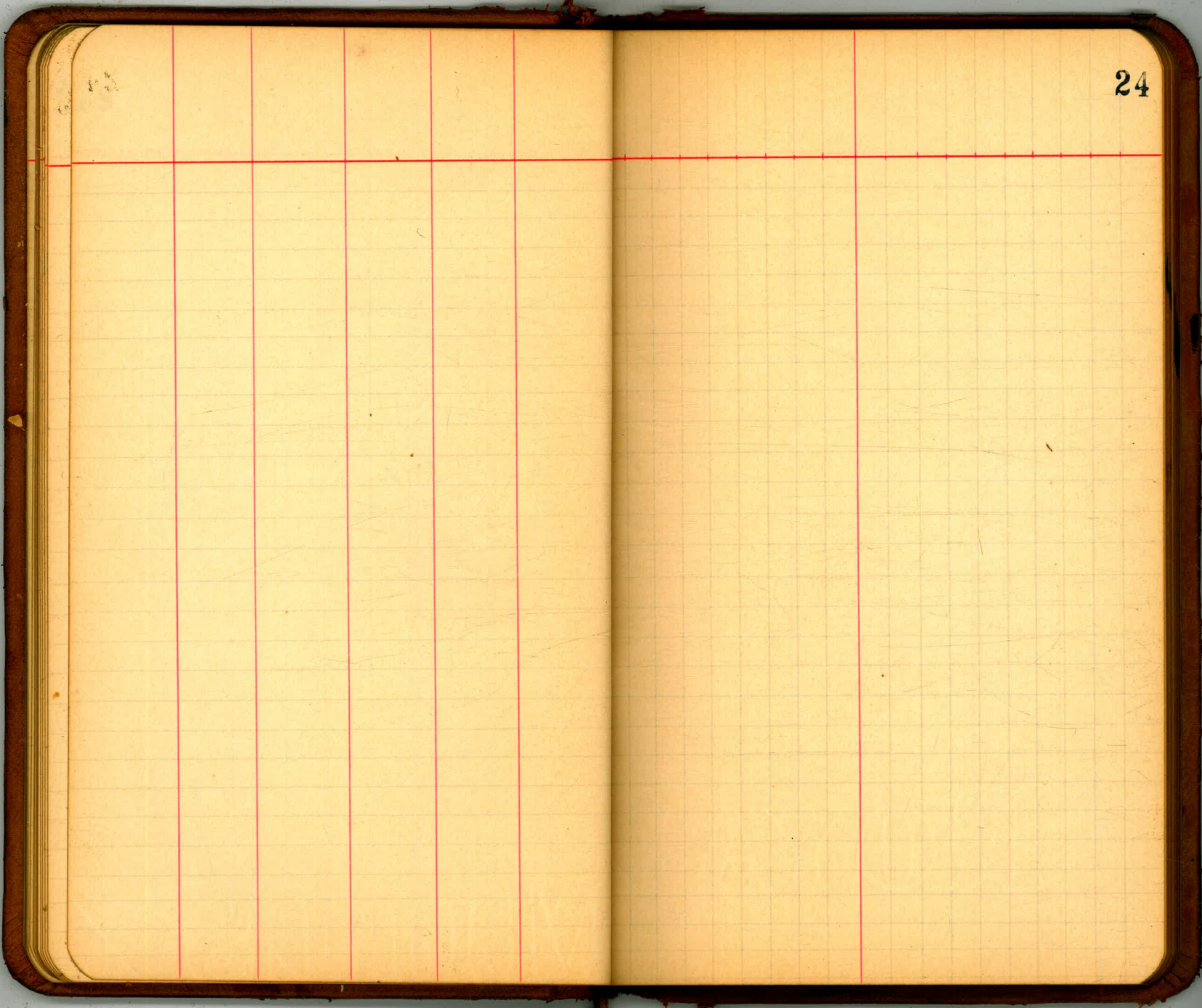


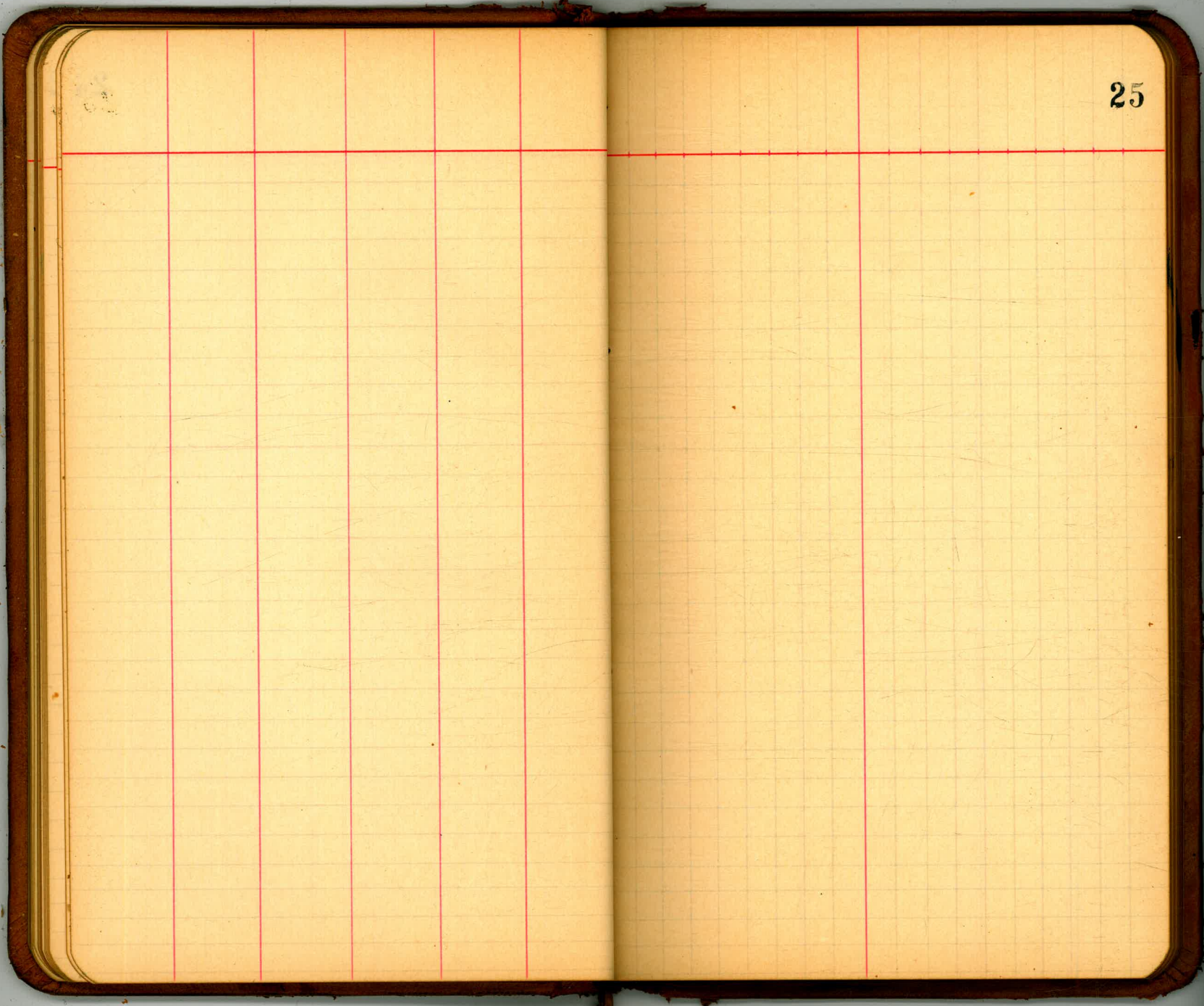


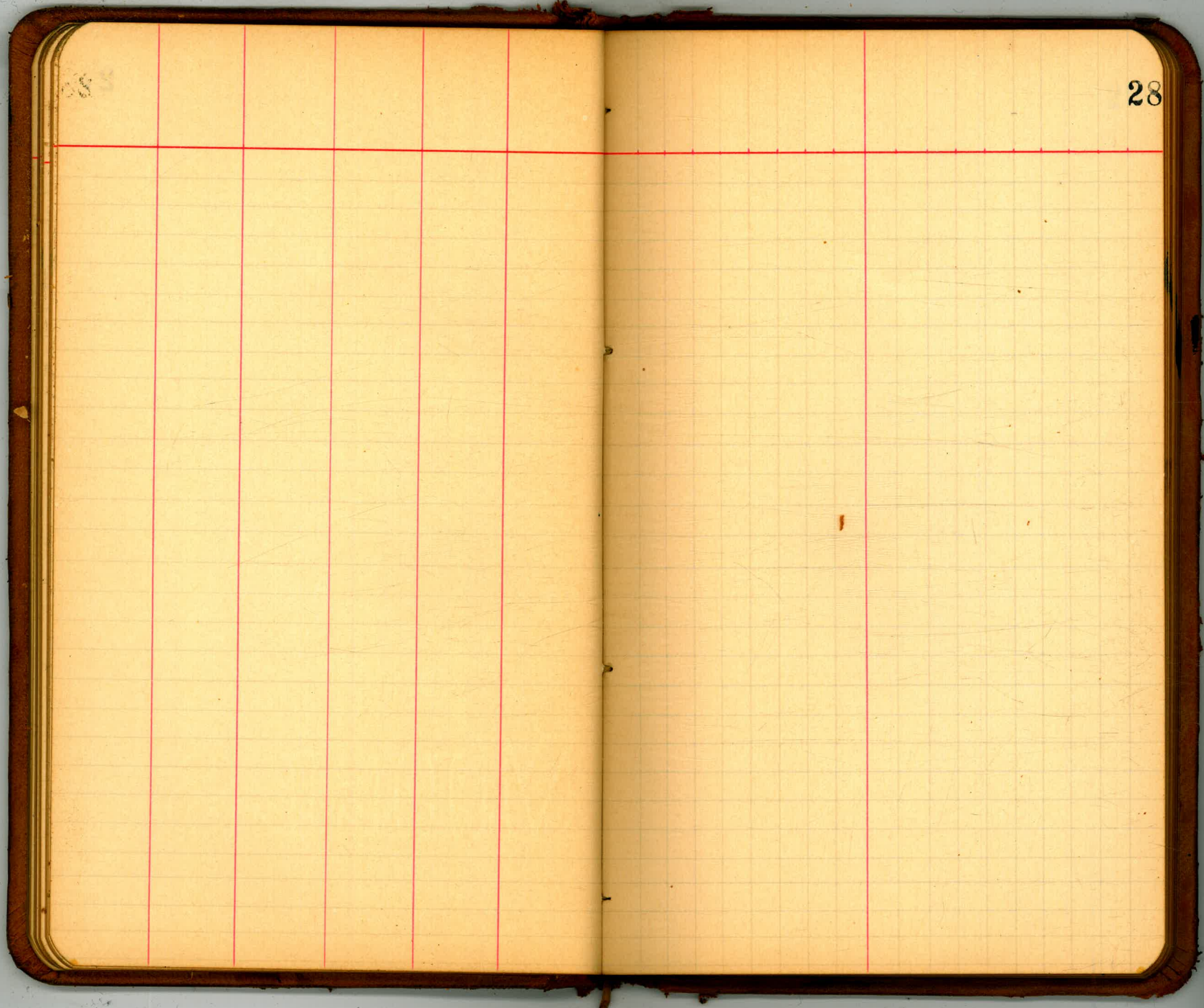
19

20







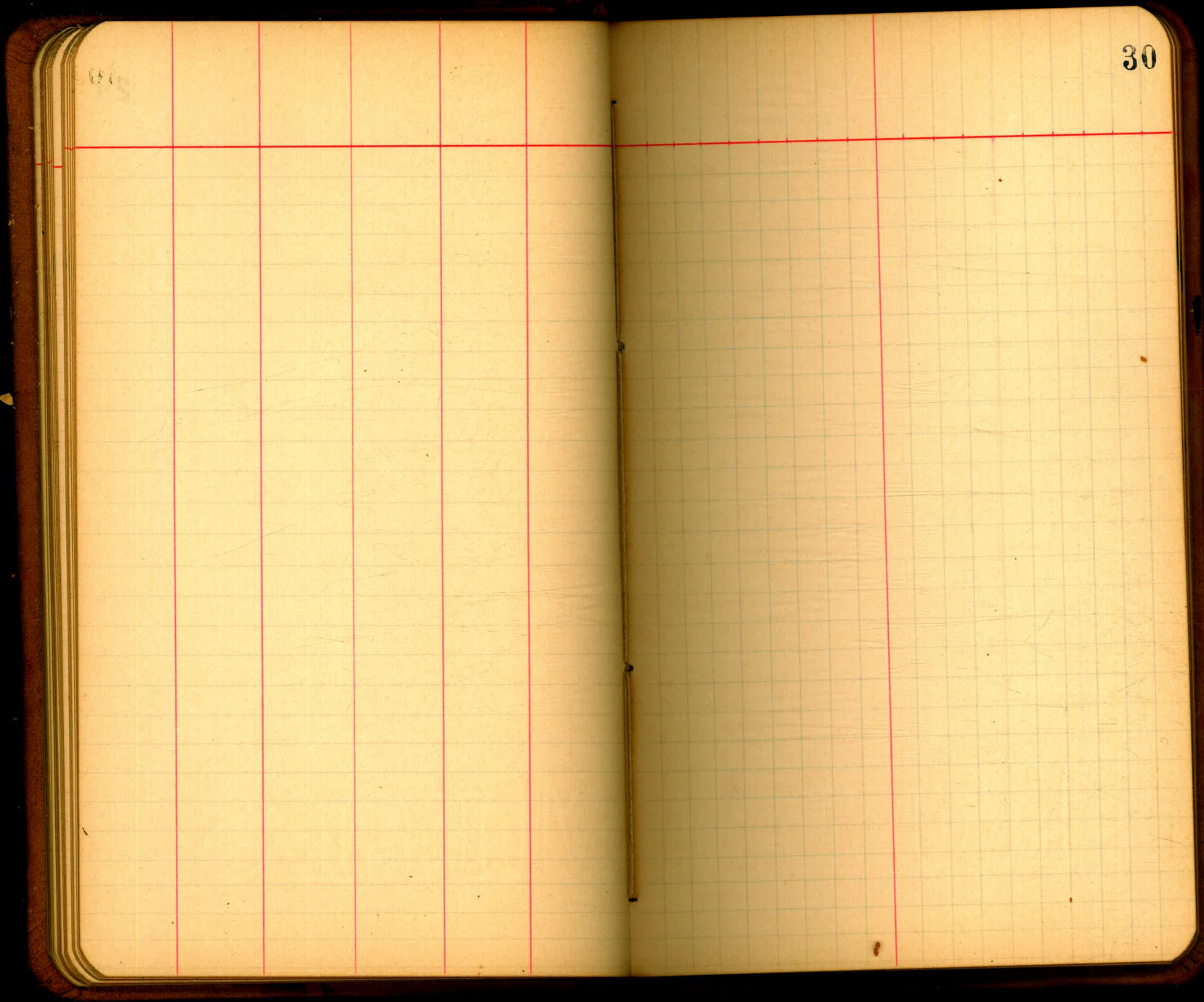


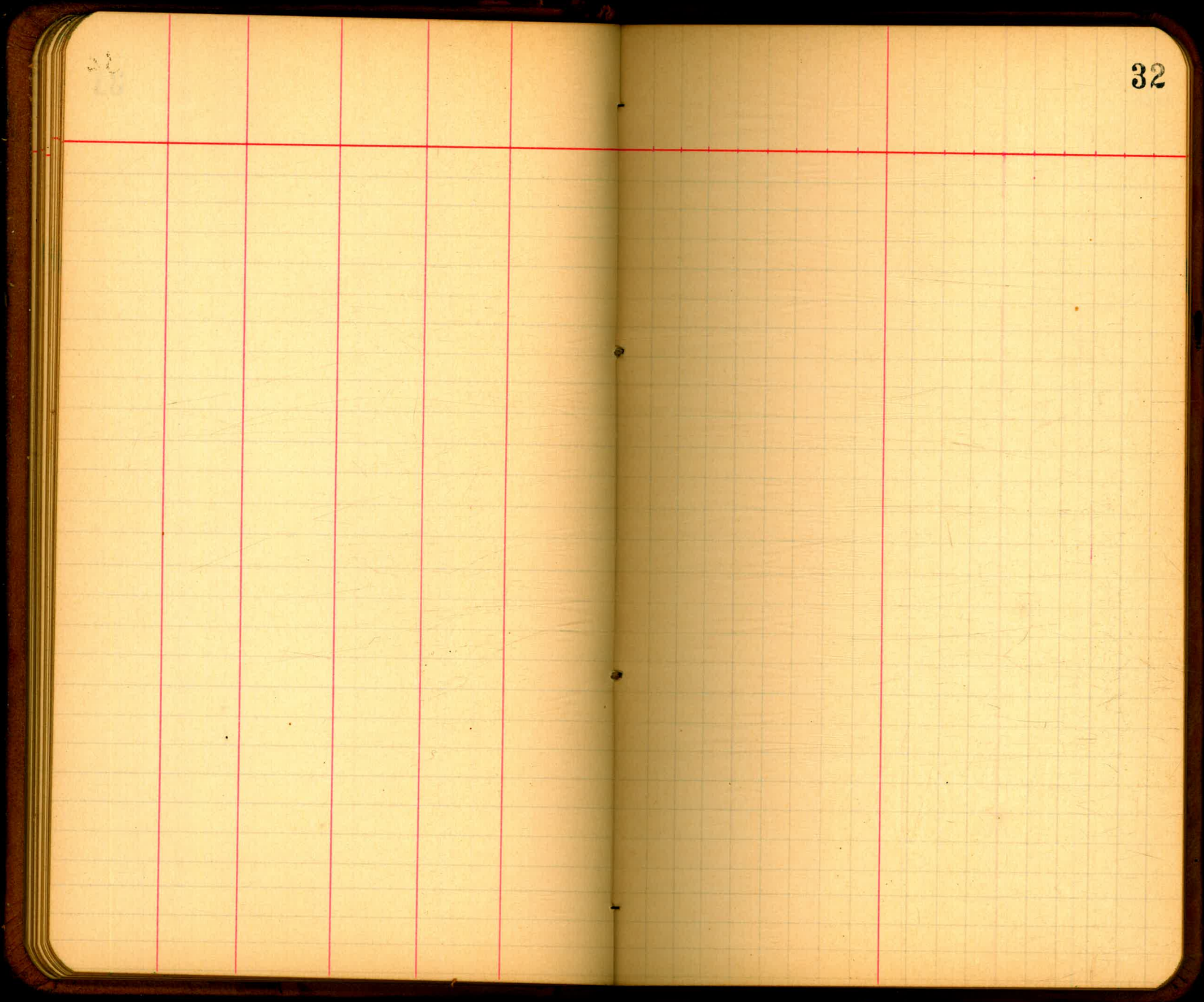
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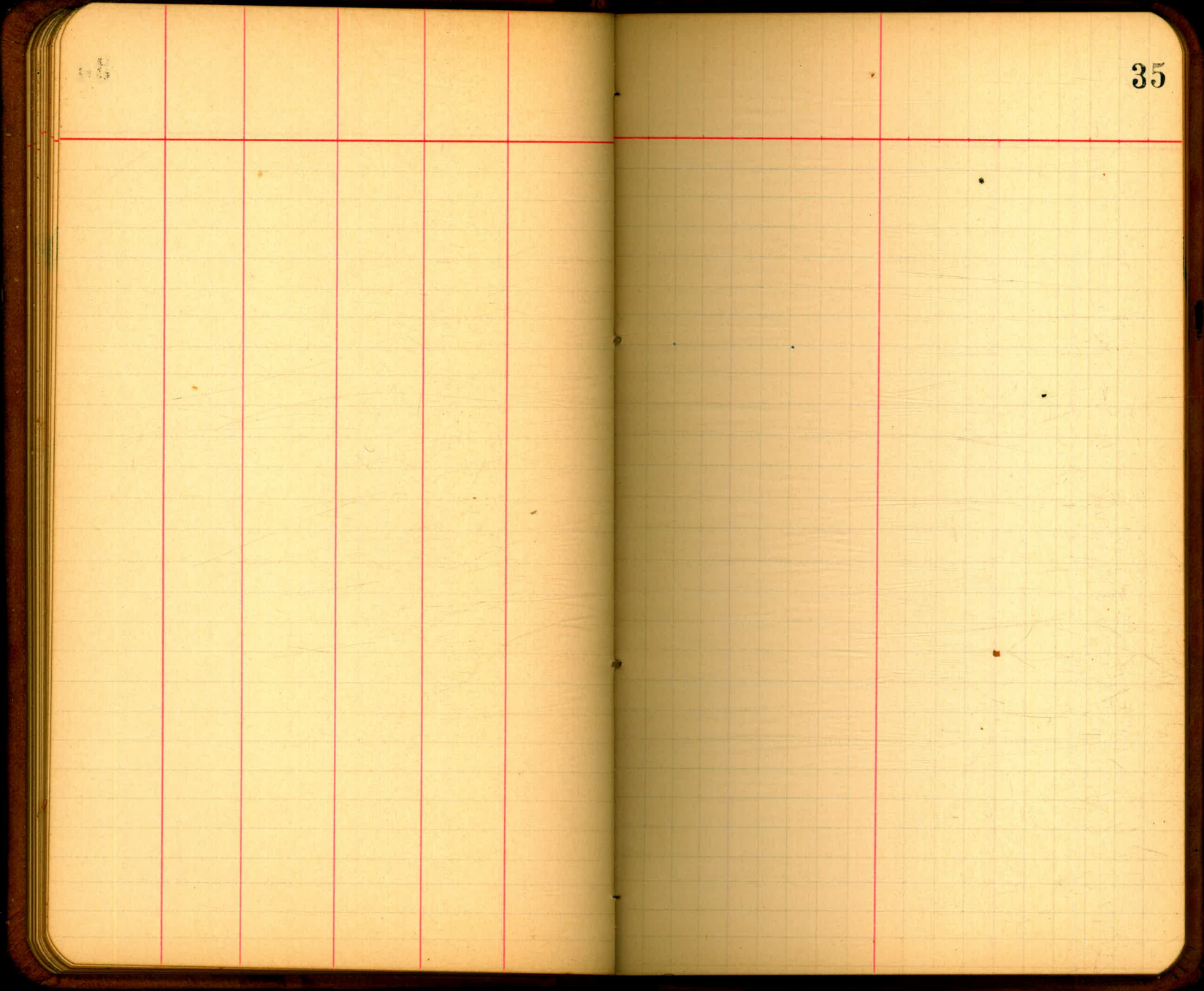




32

32

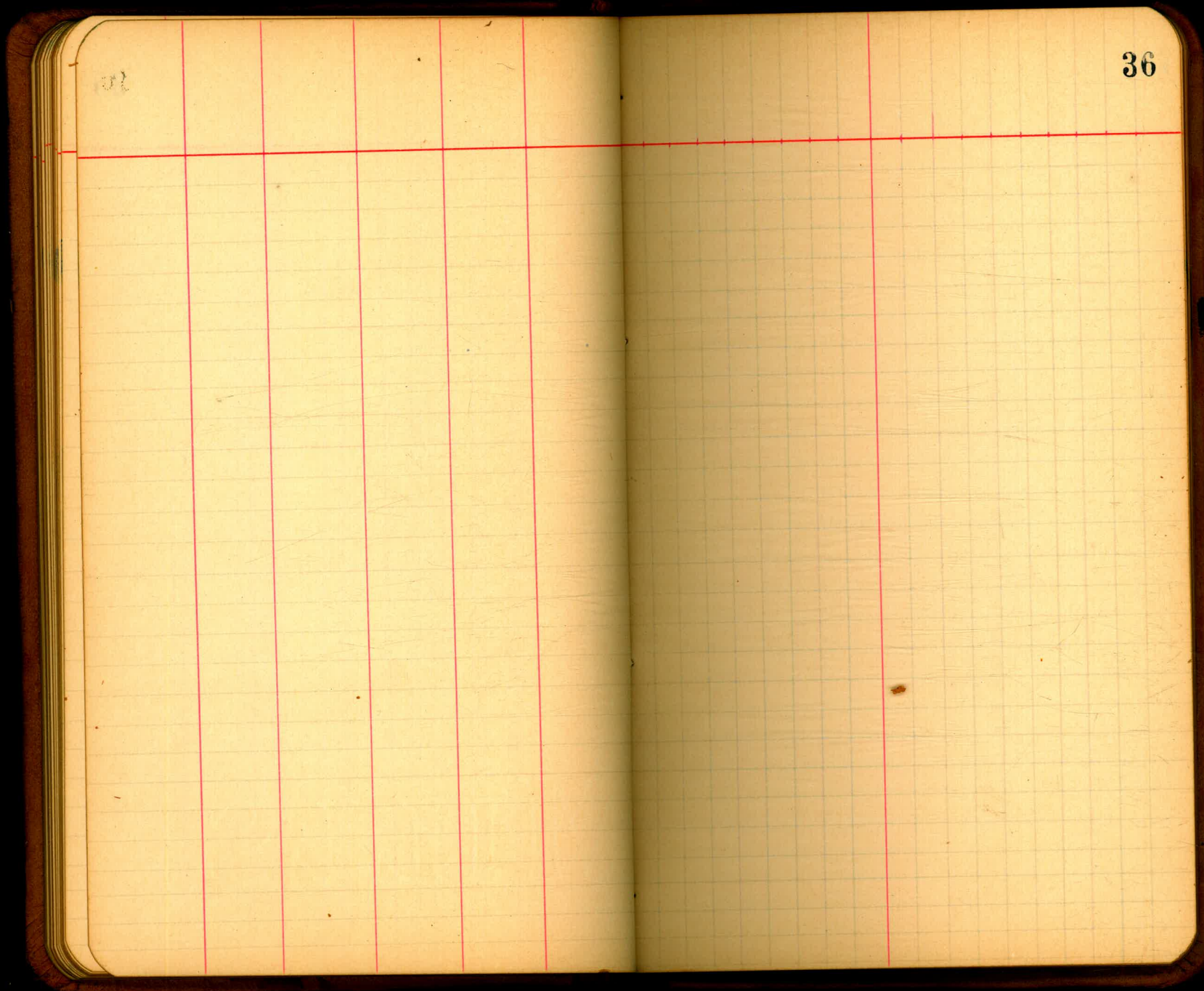
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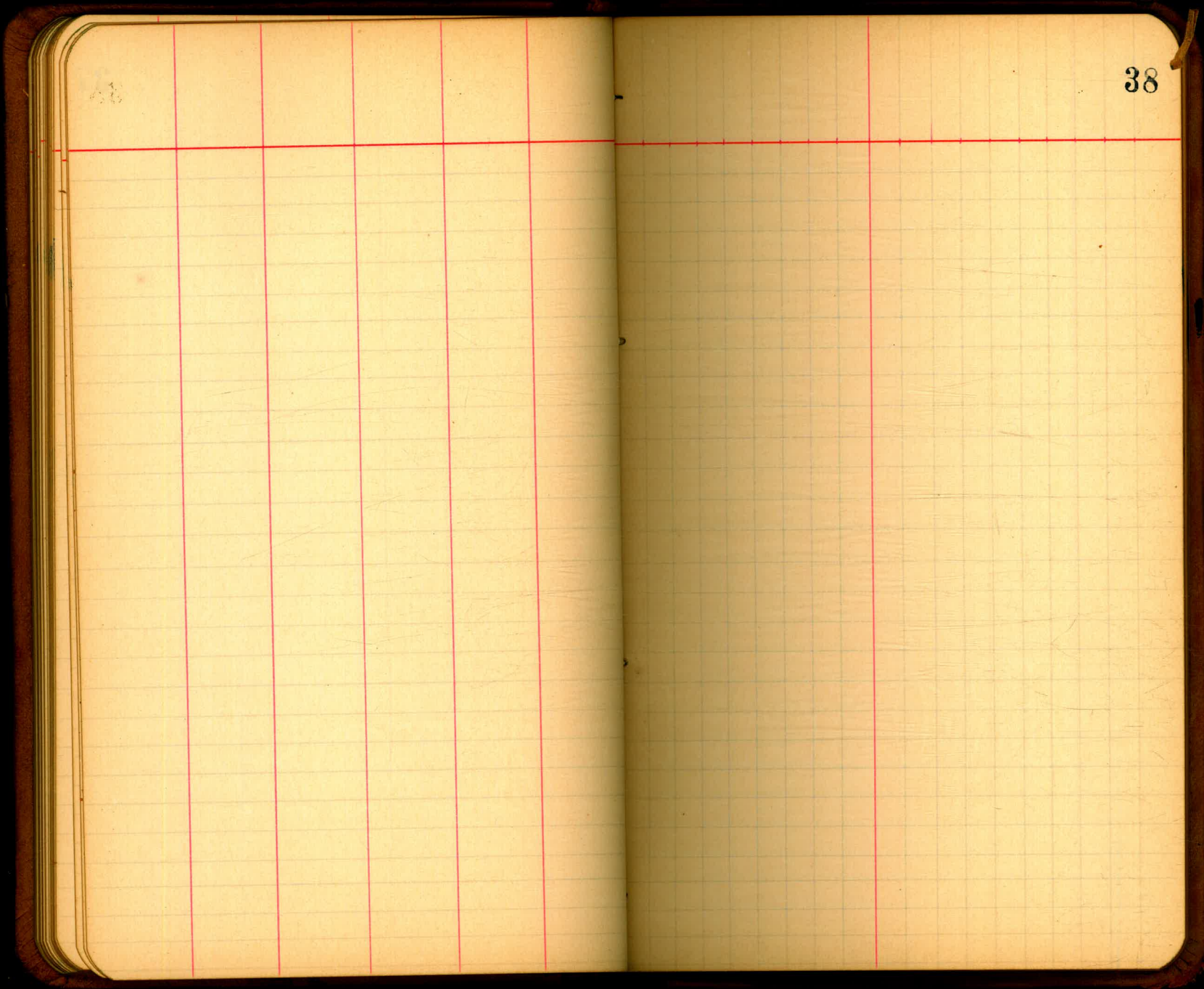


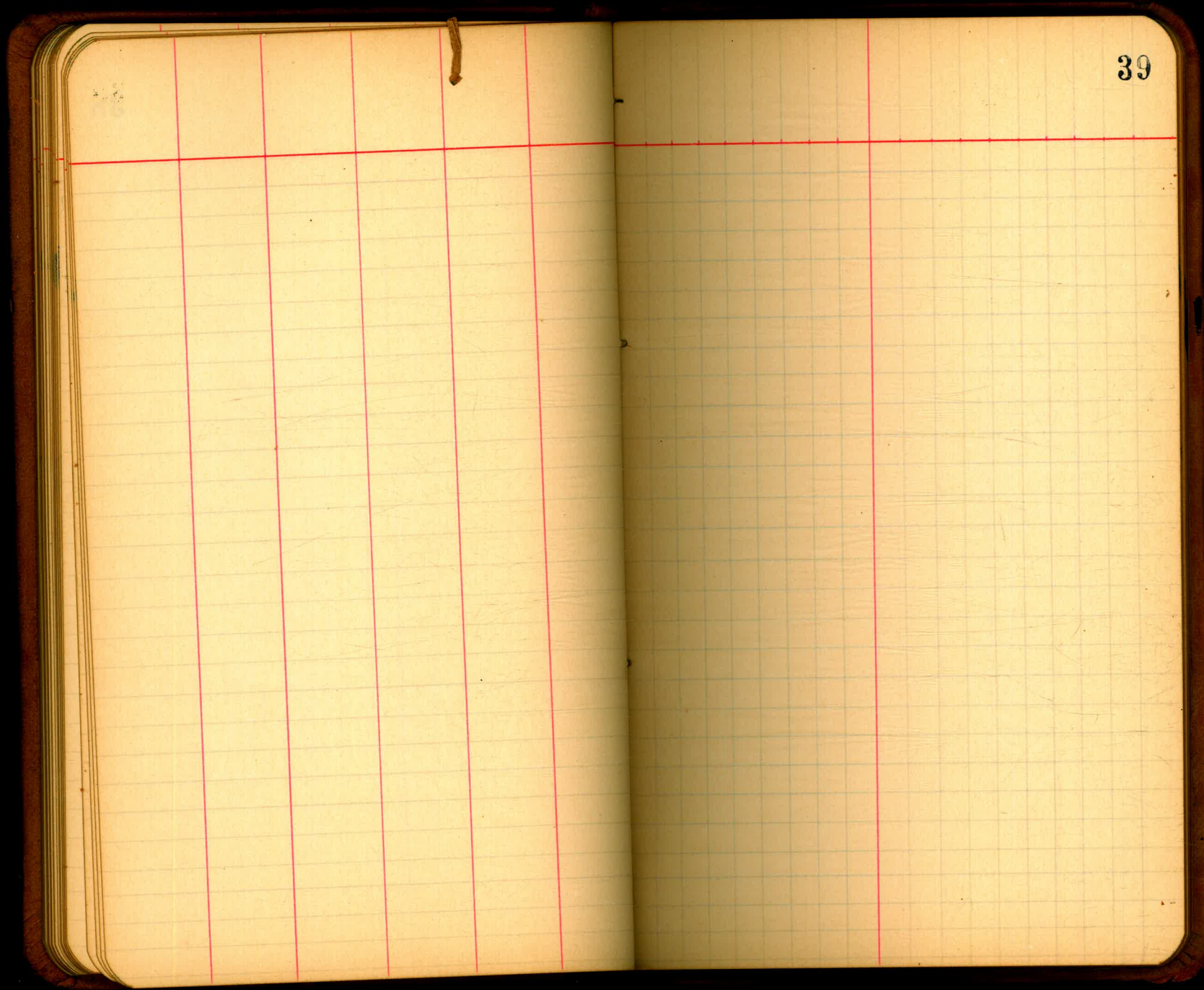
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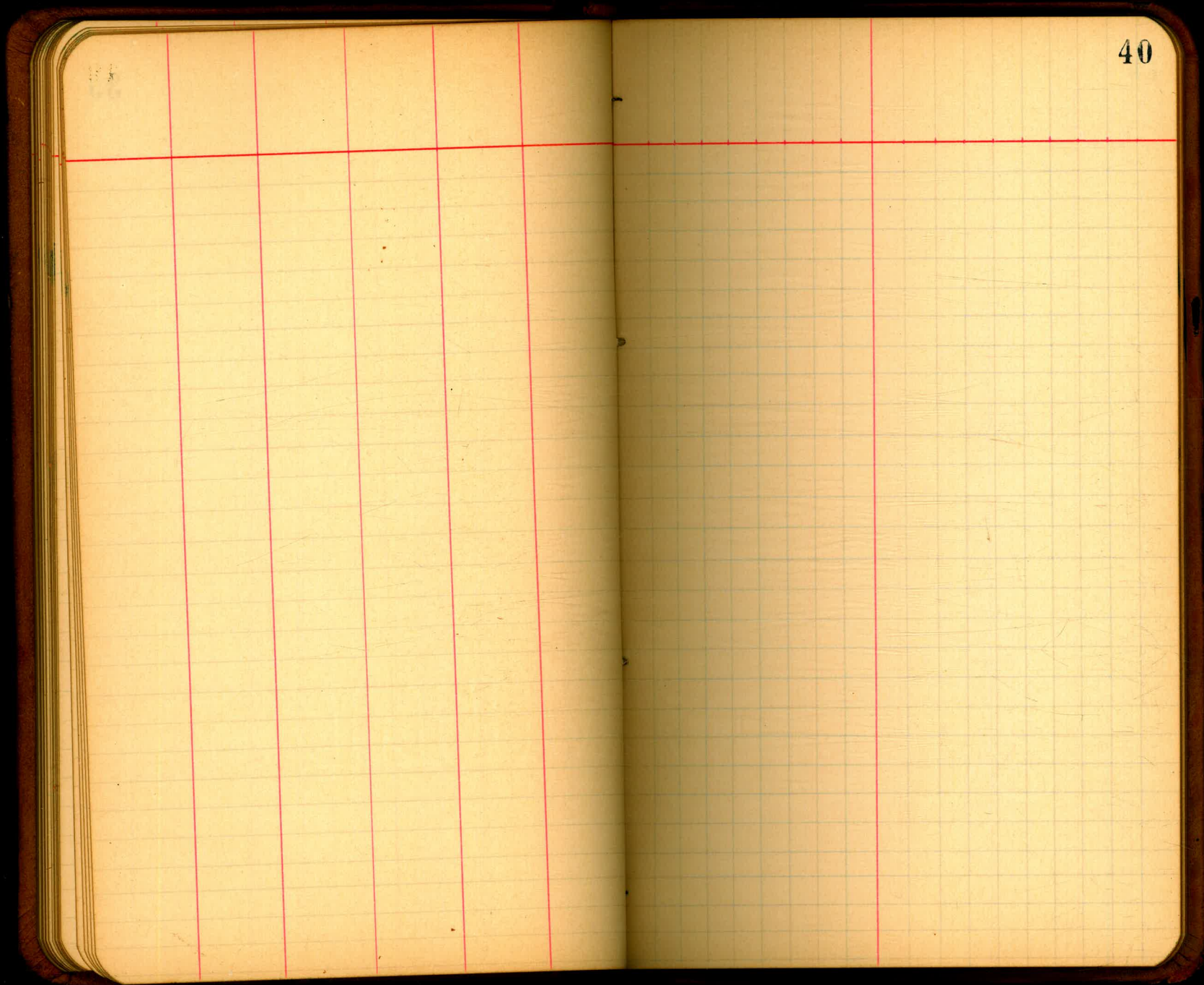
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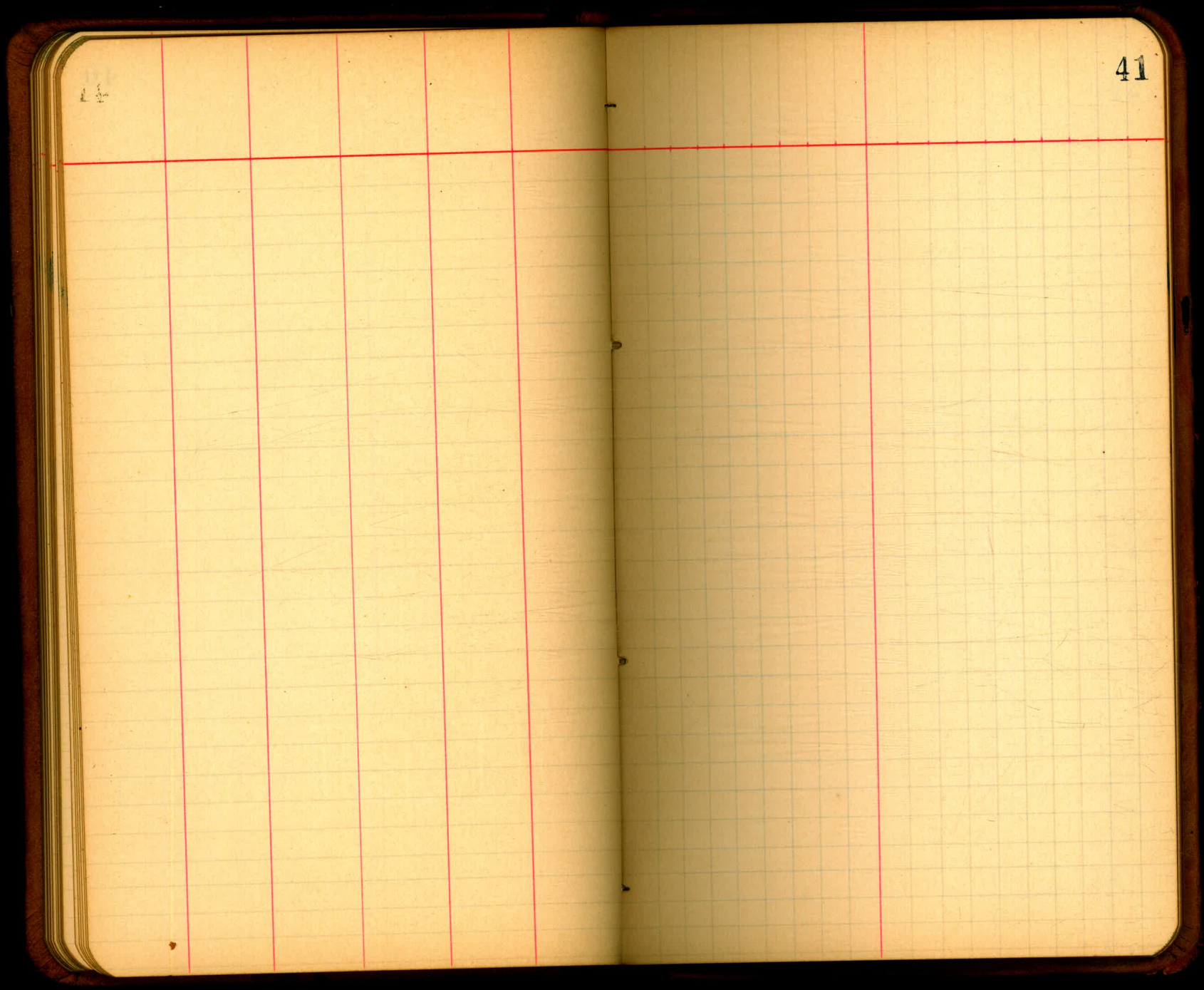
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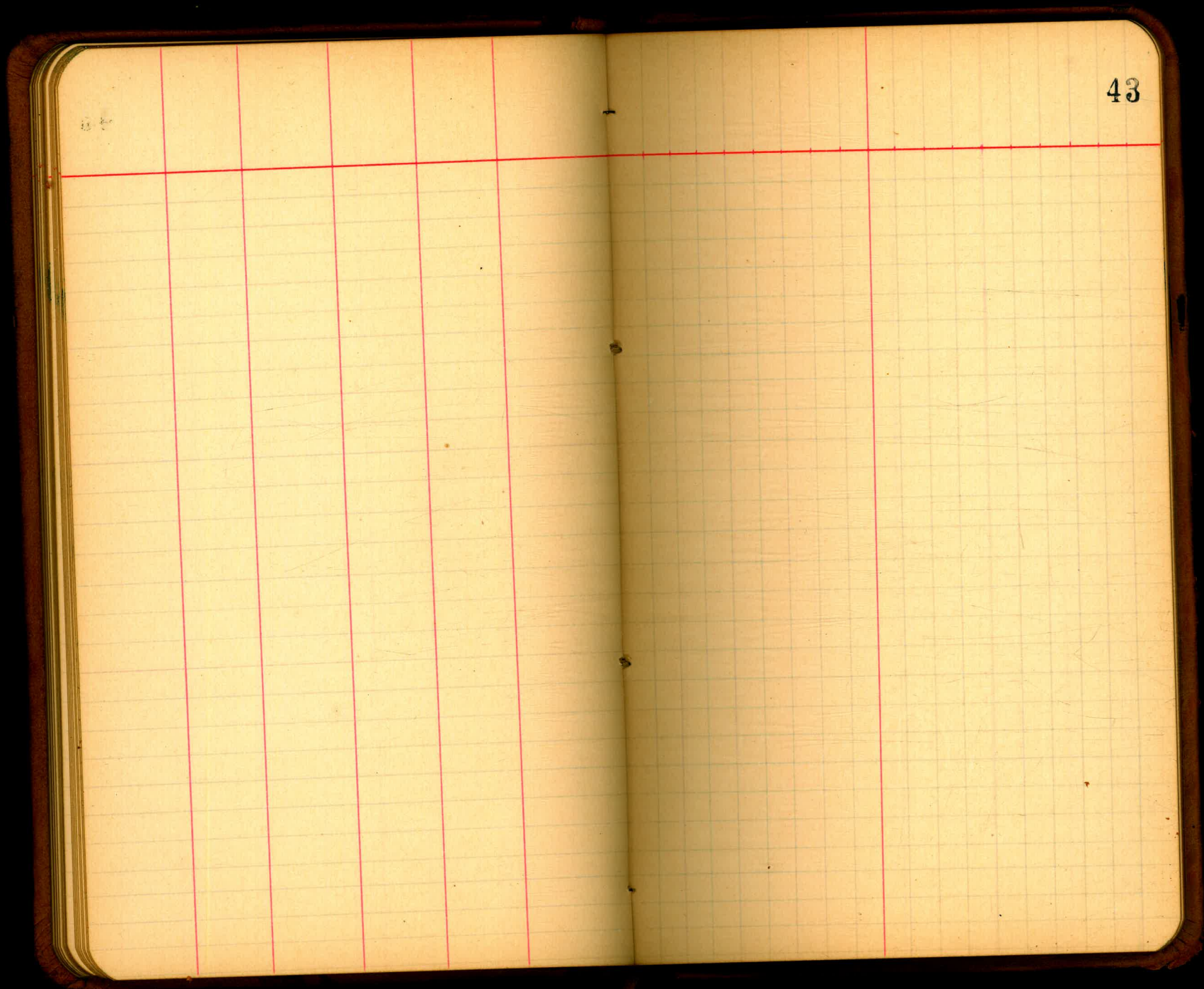


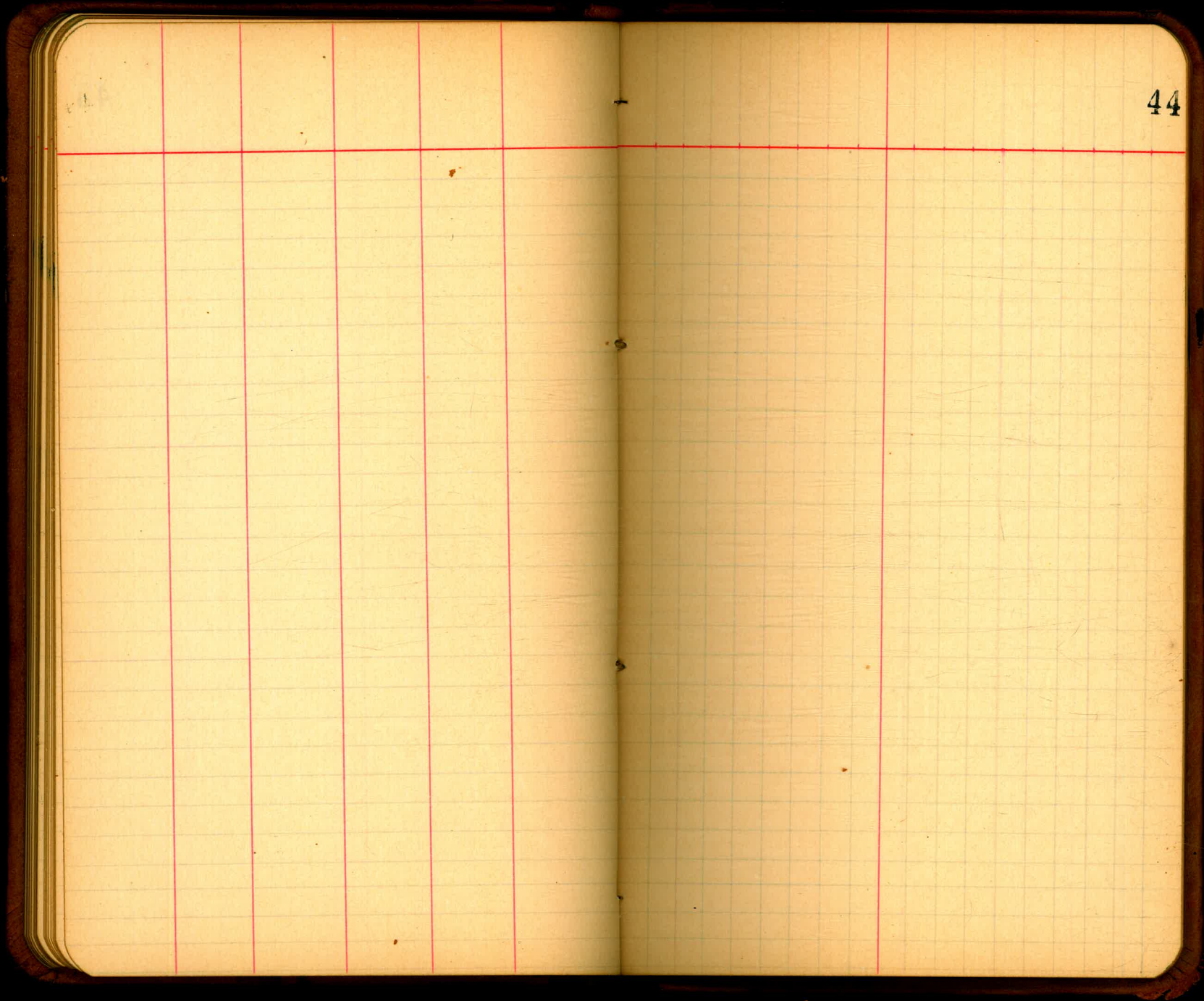




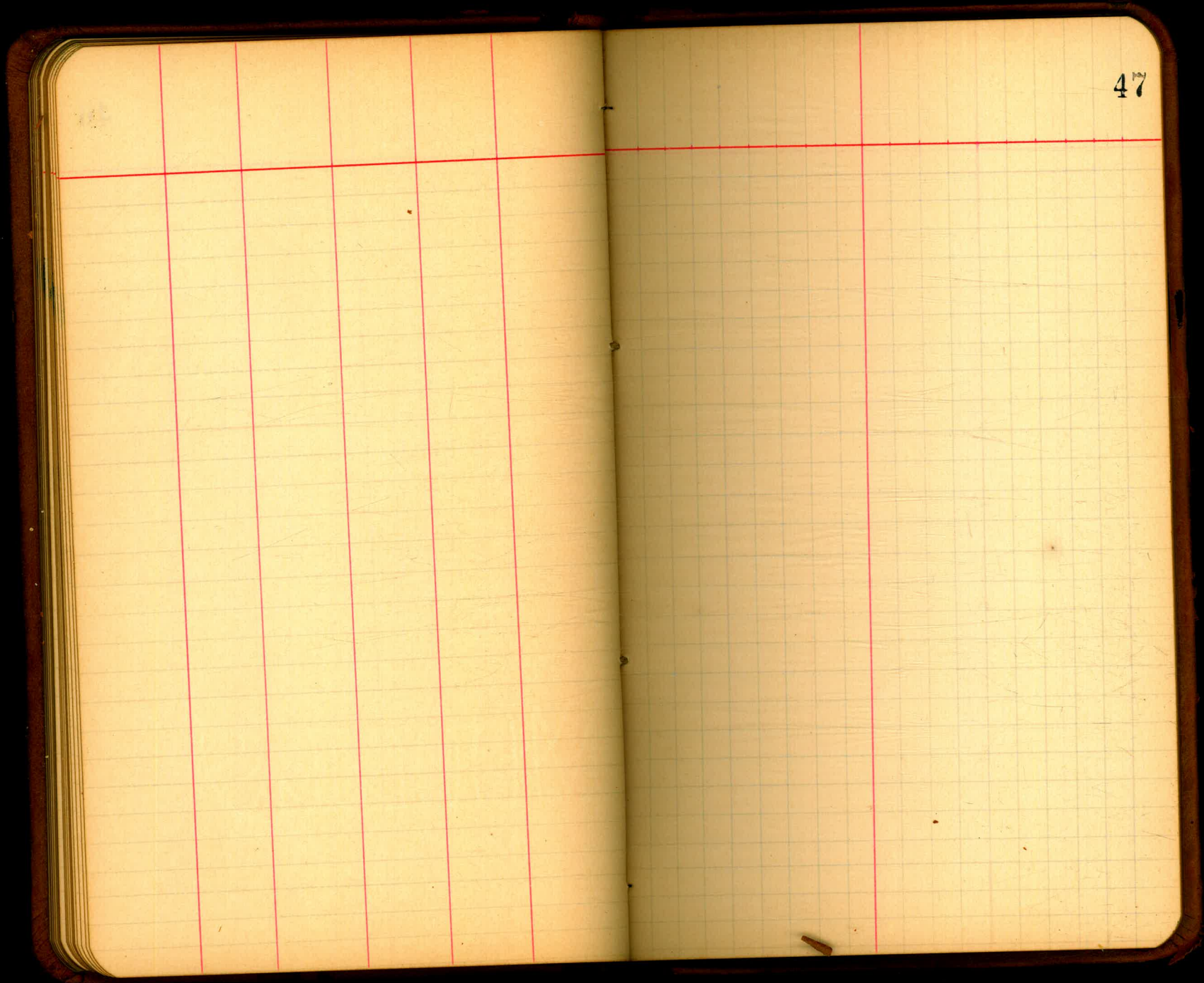


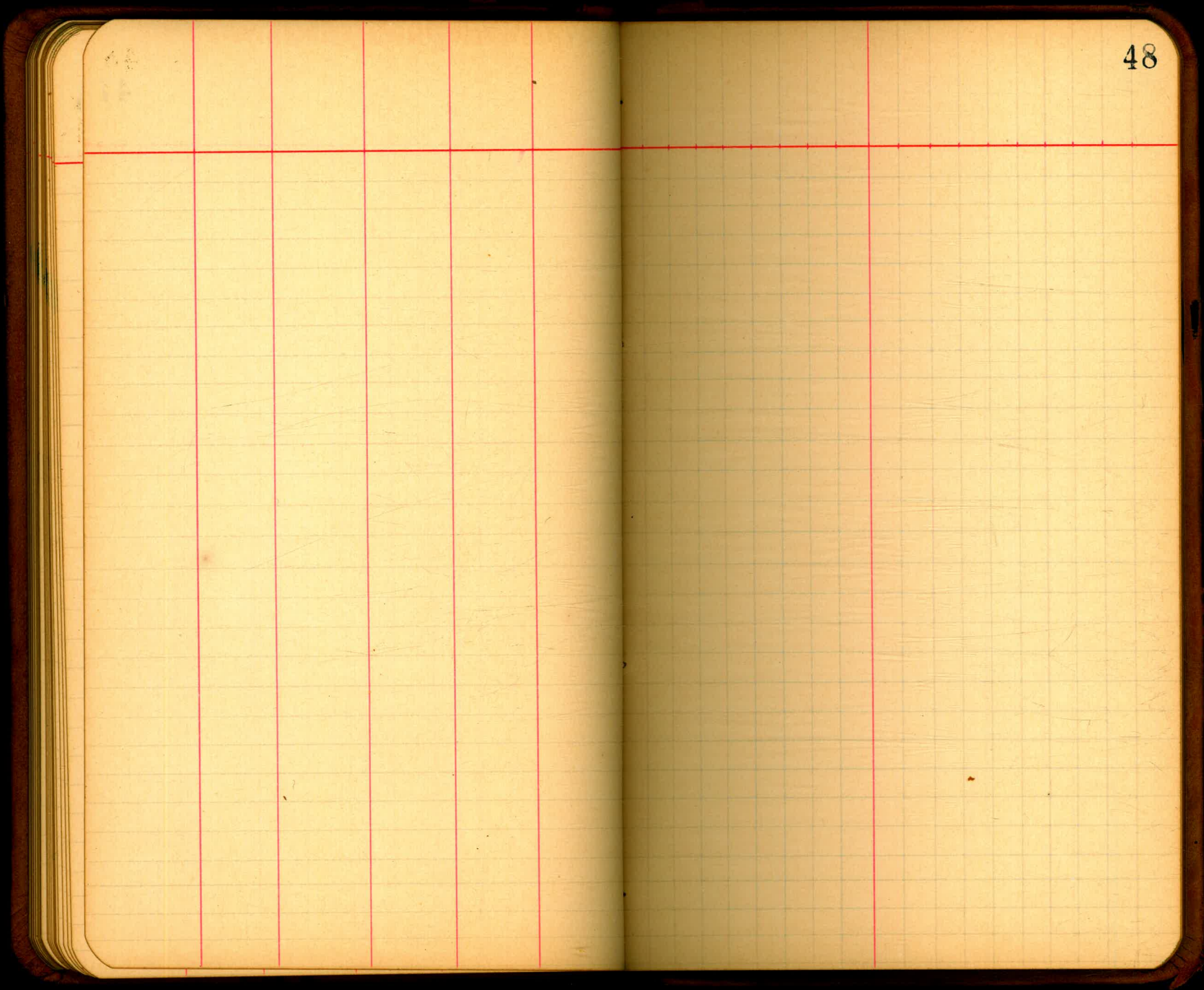
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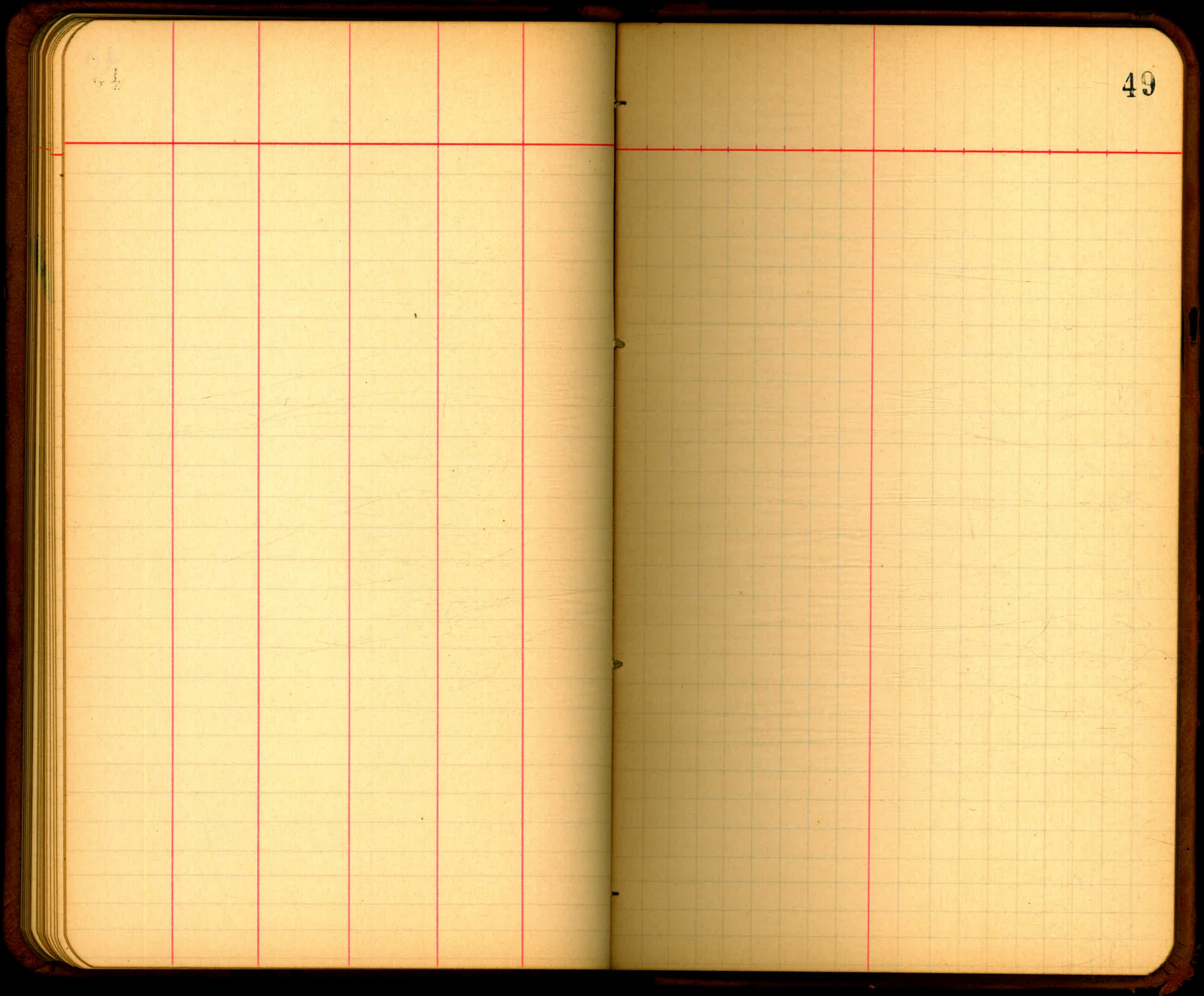




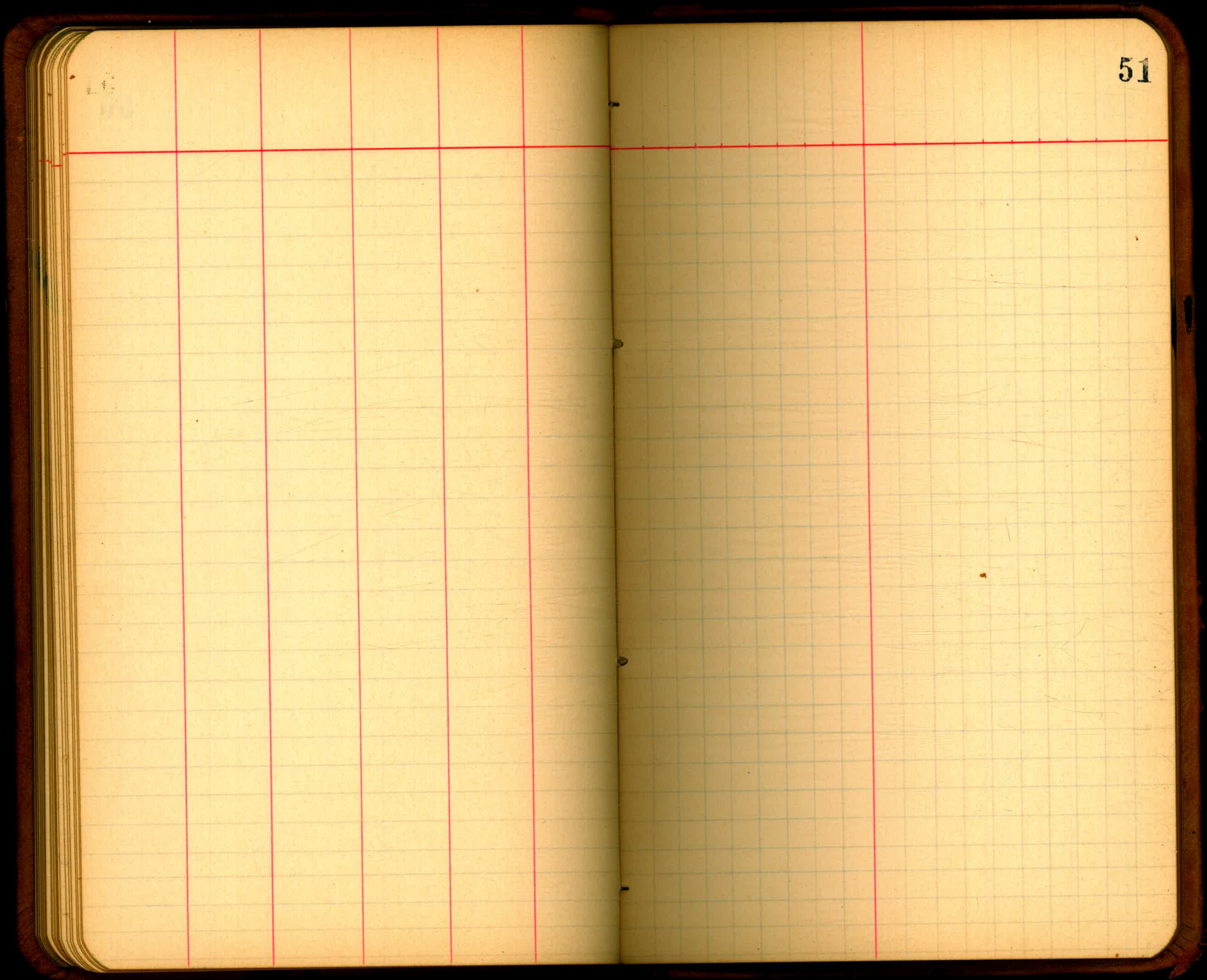
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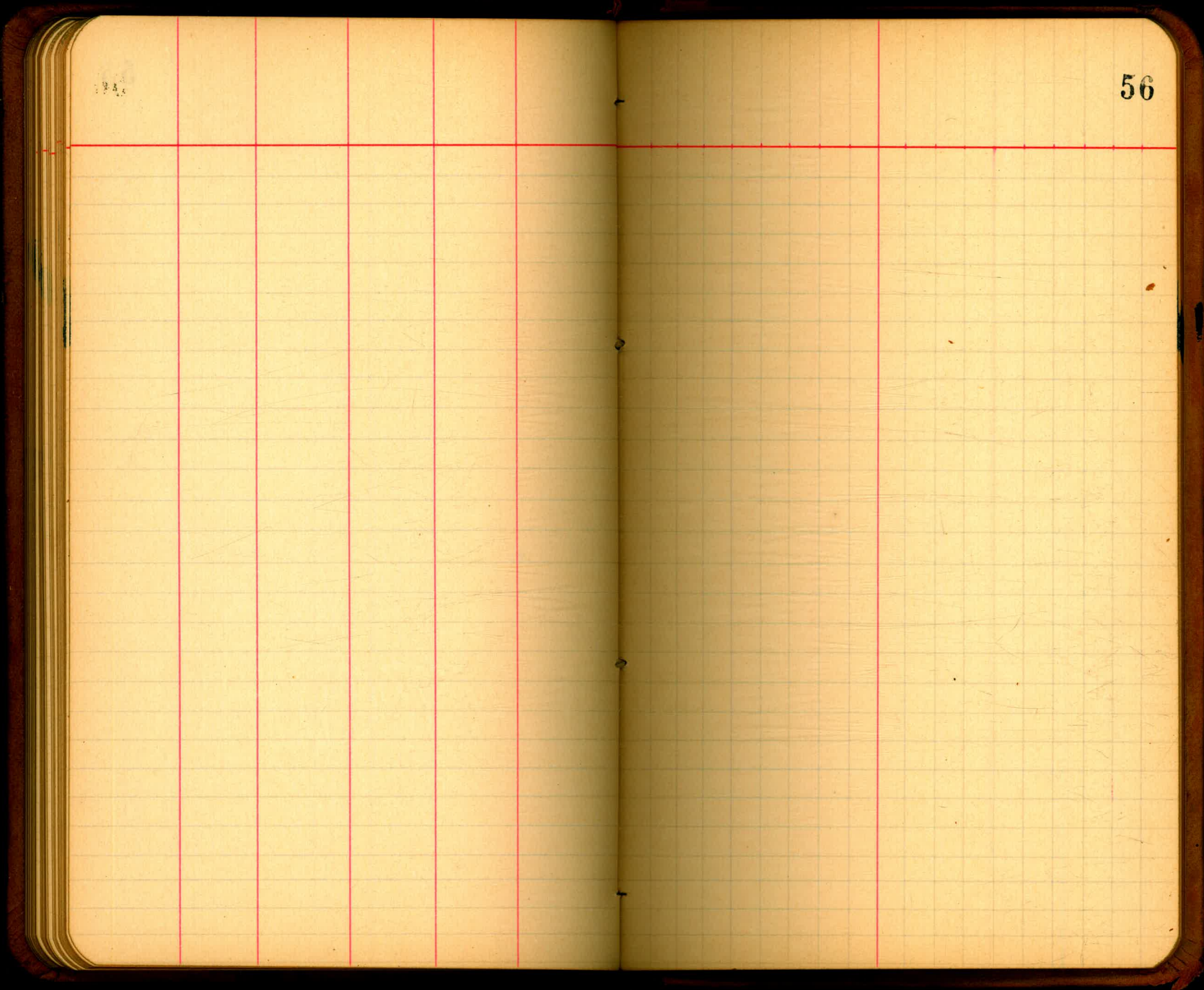
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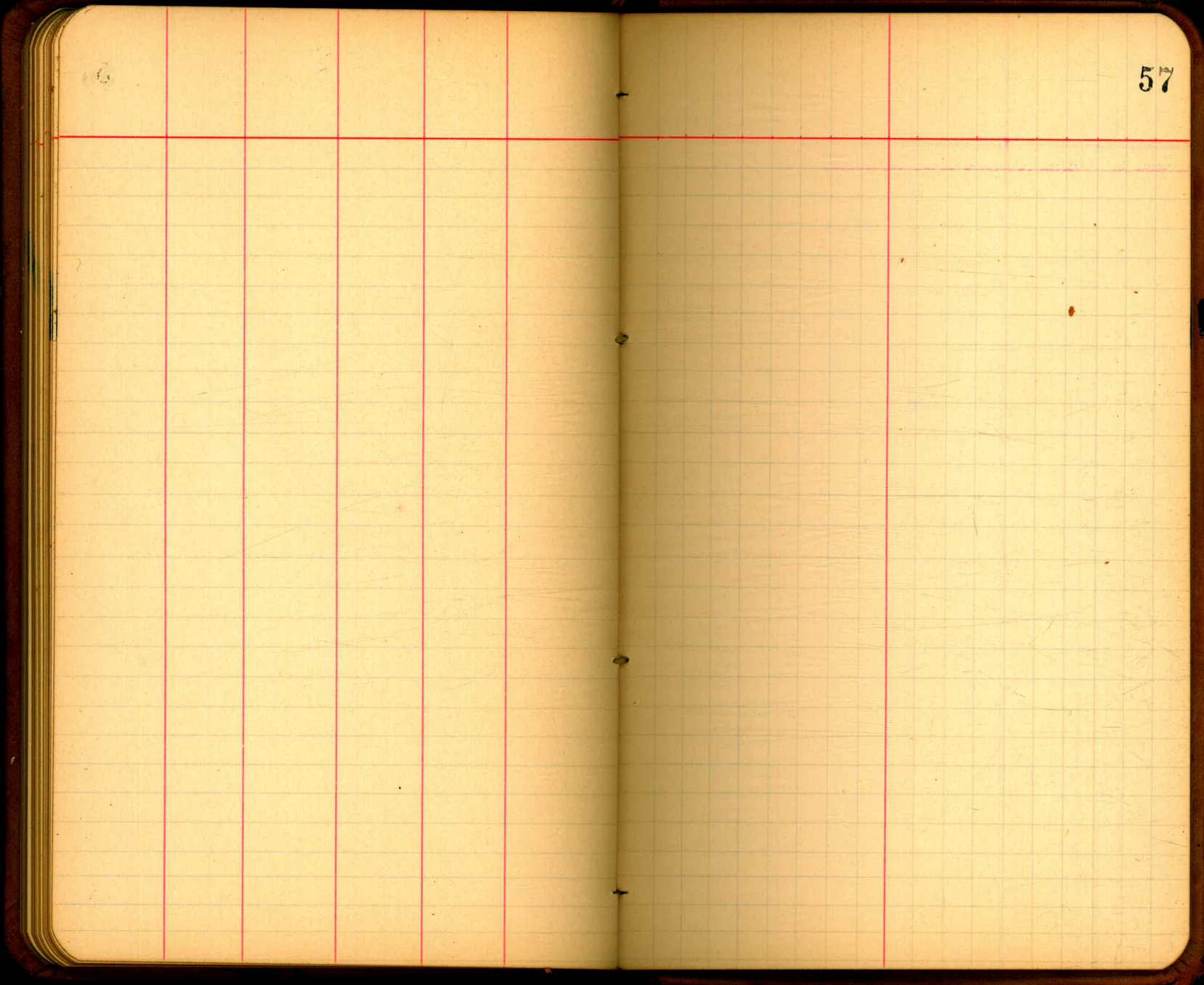
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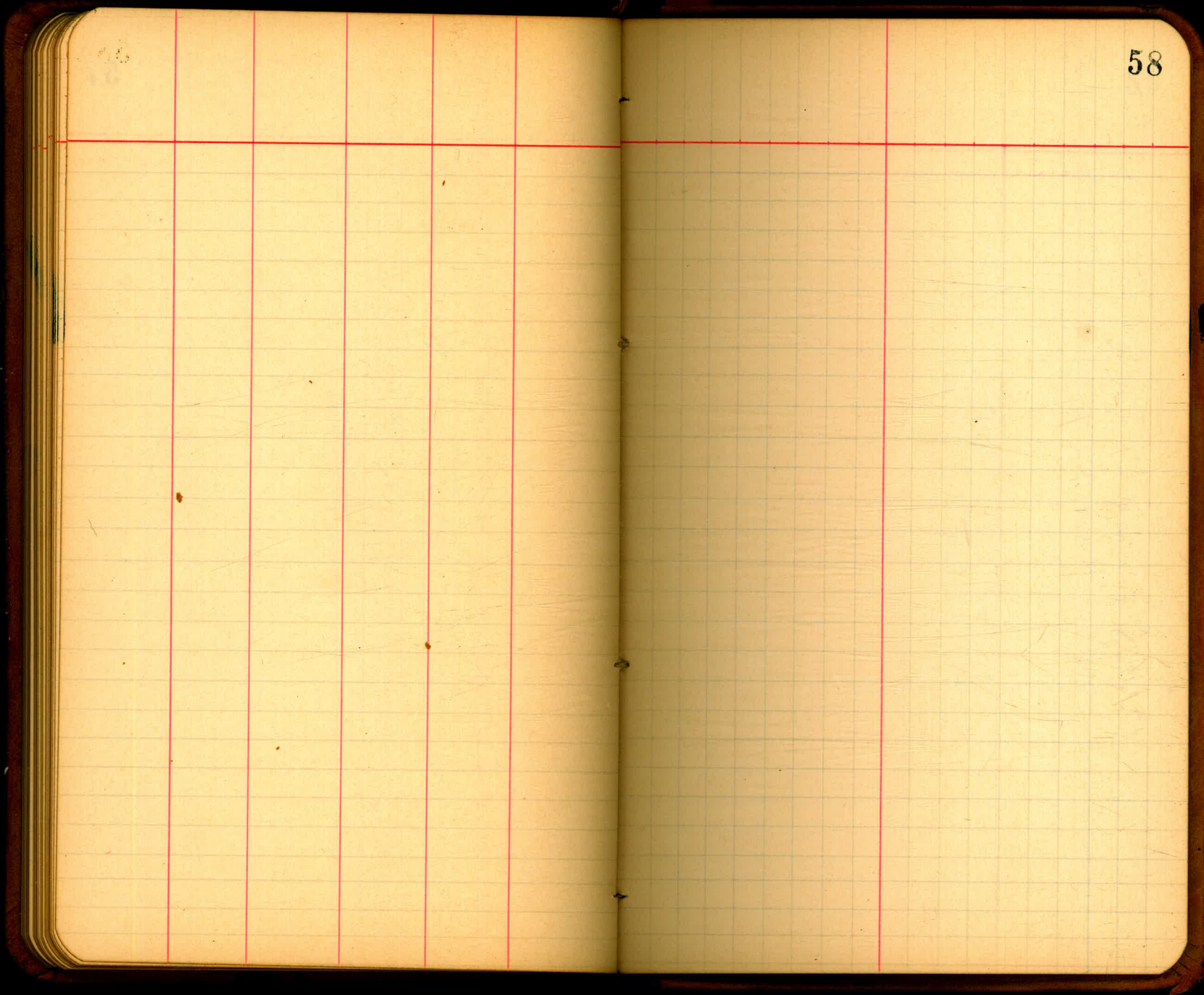
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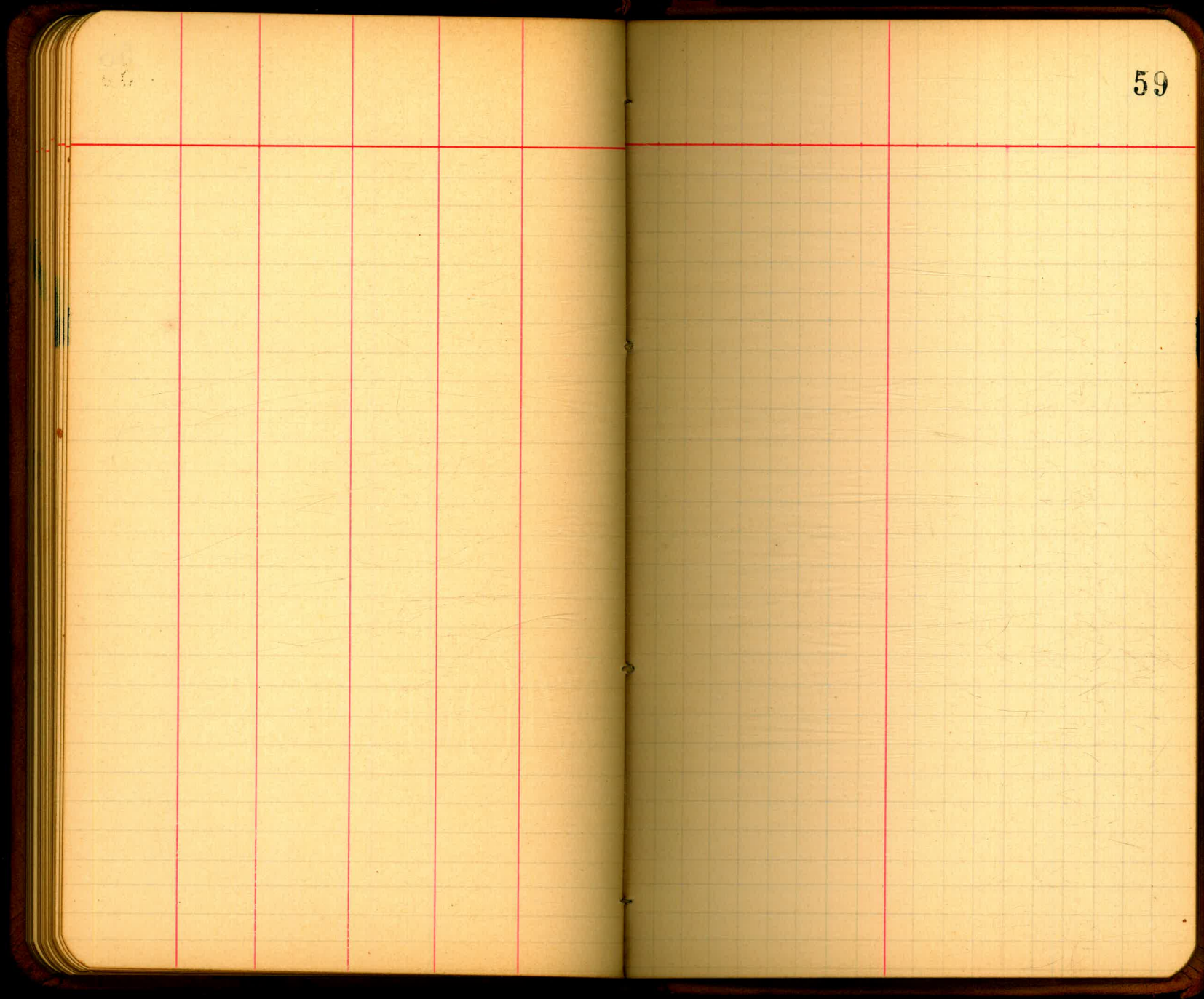


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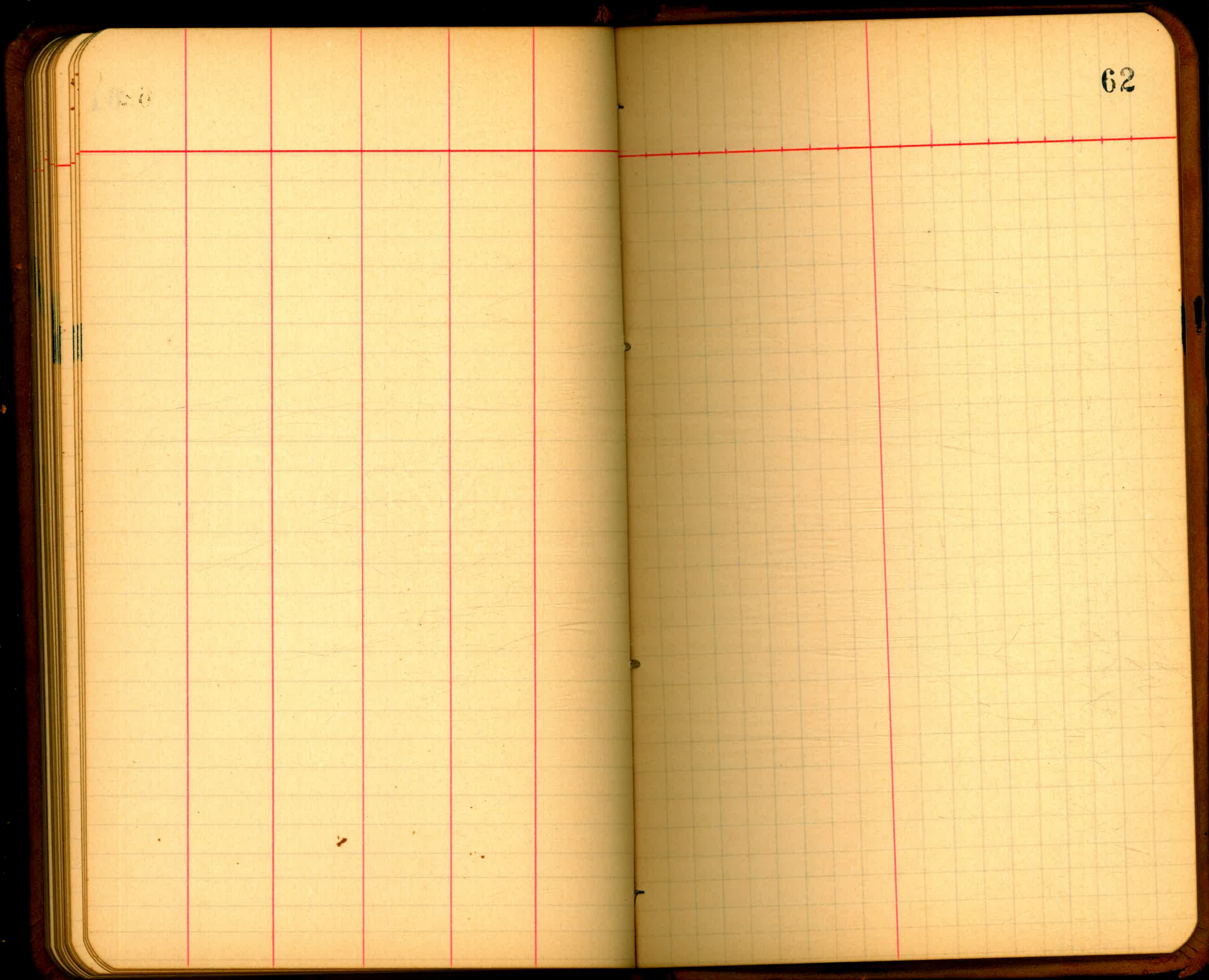
56





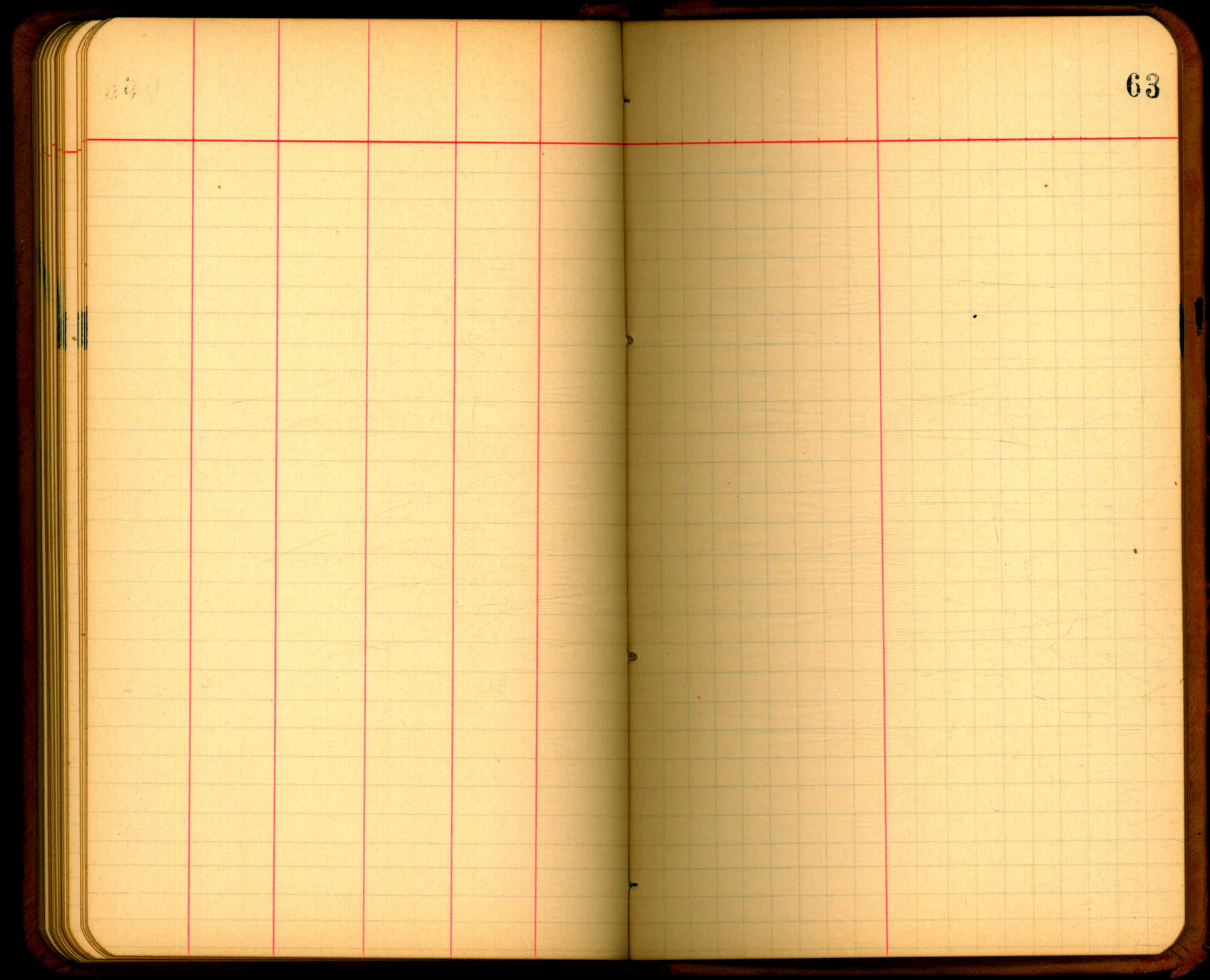


59



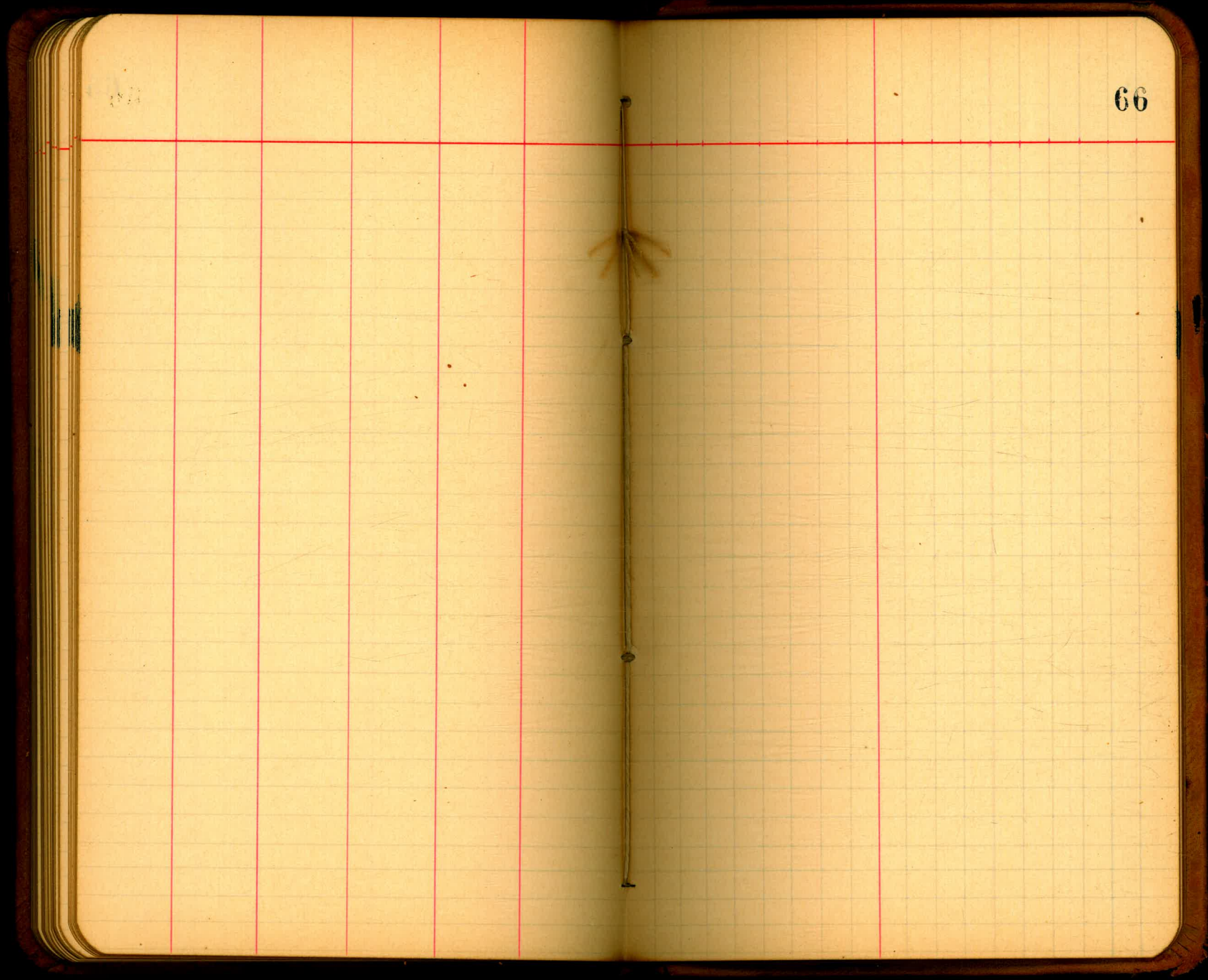
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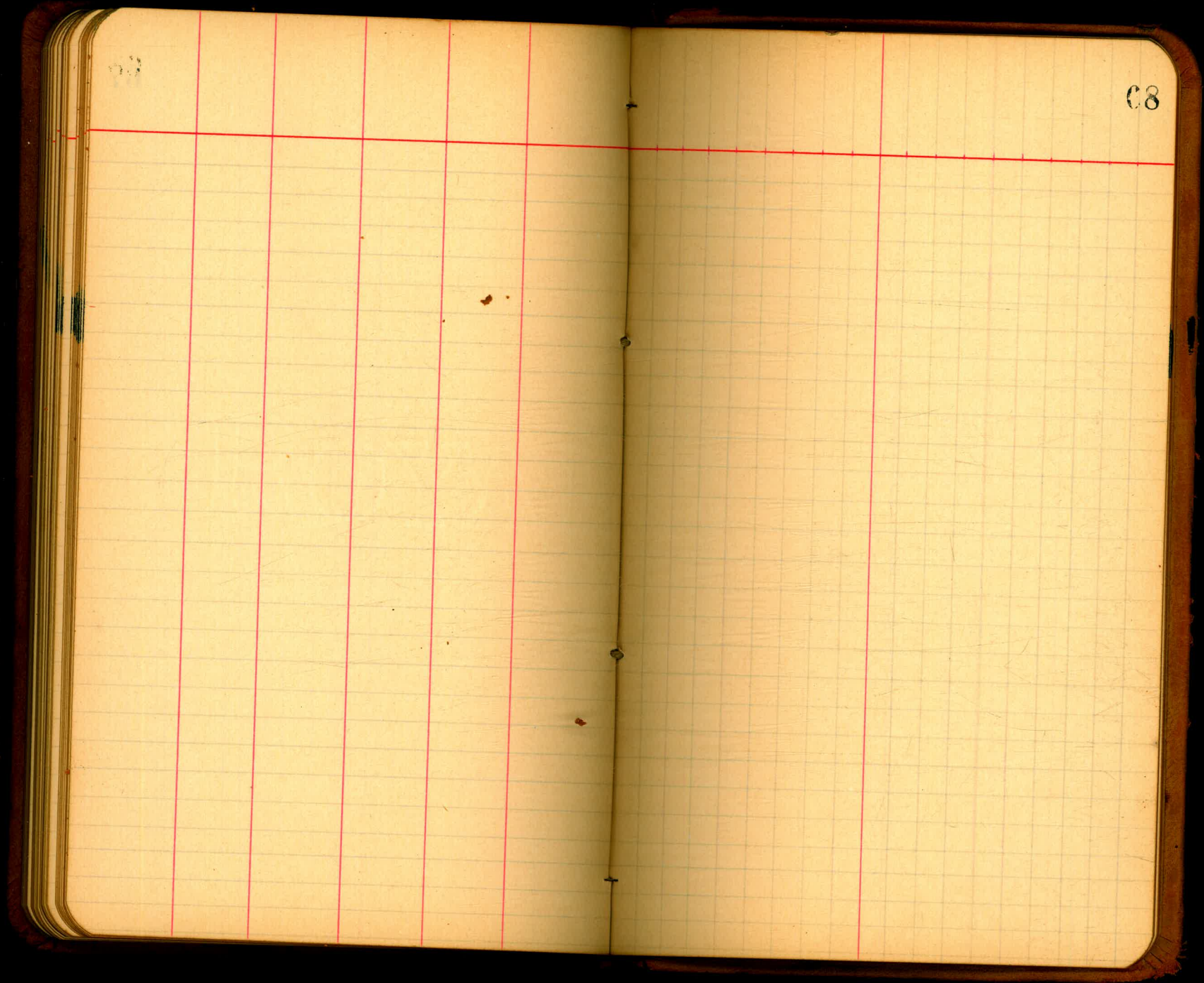
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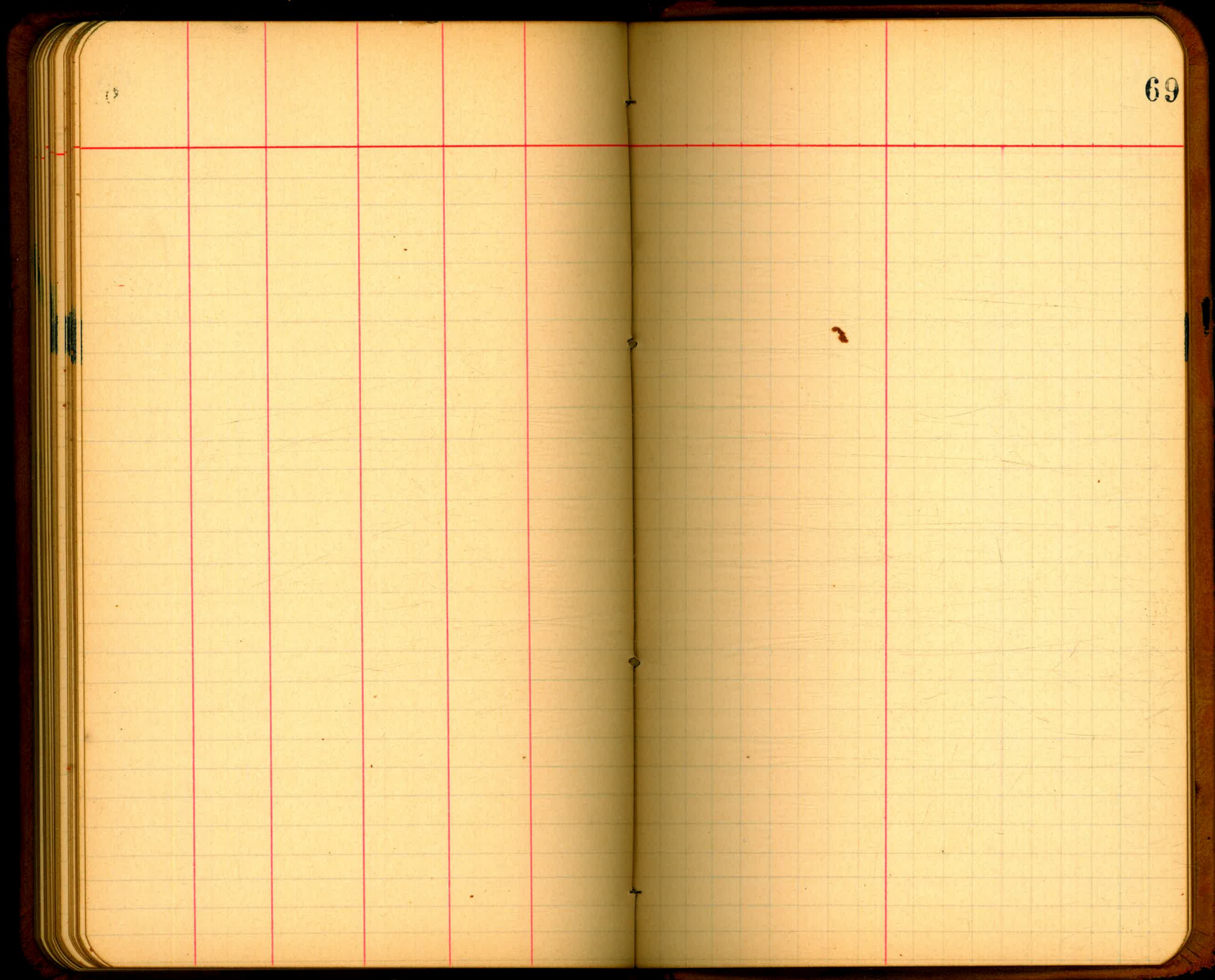
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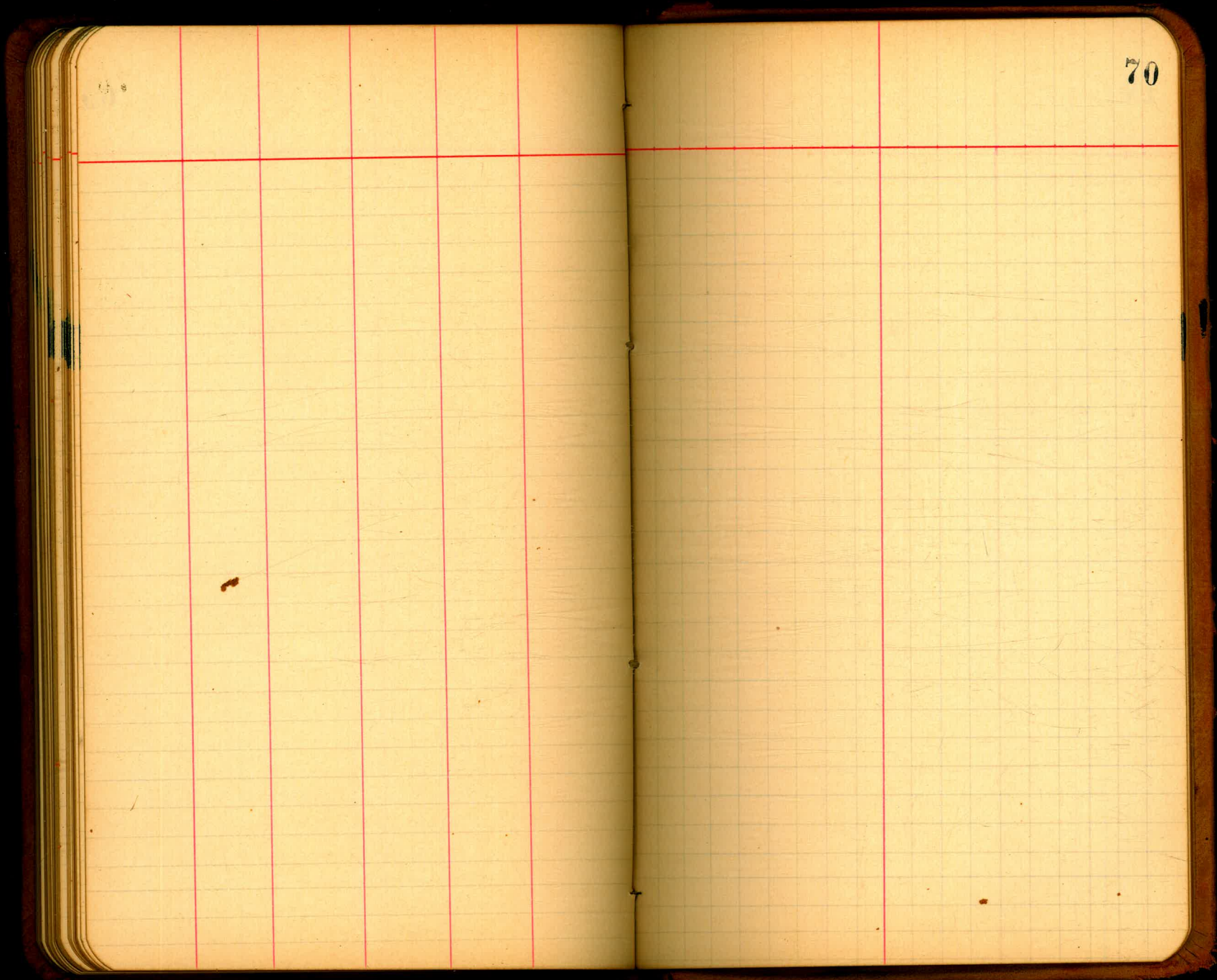
63





C8





68

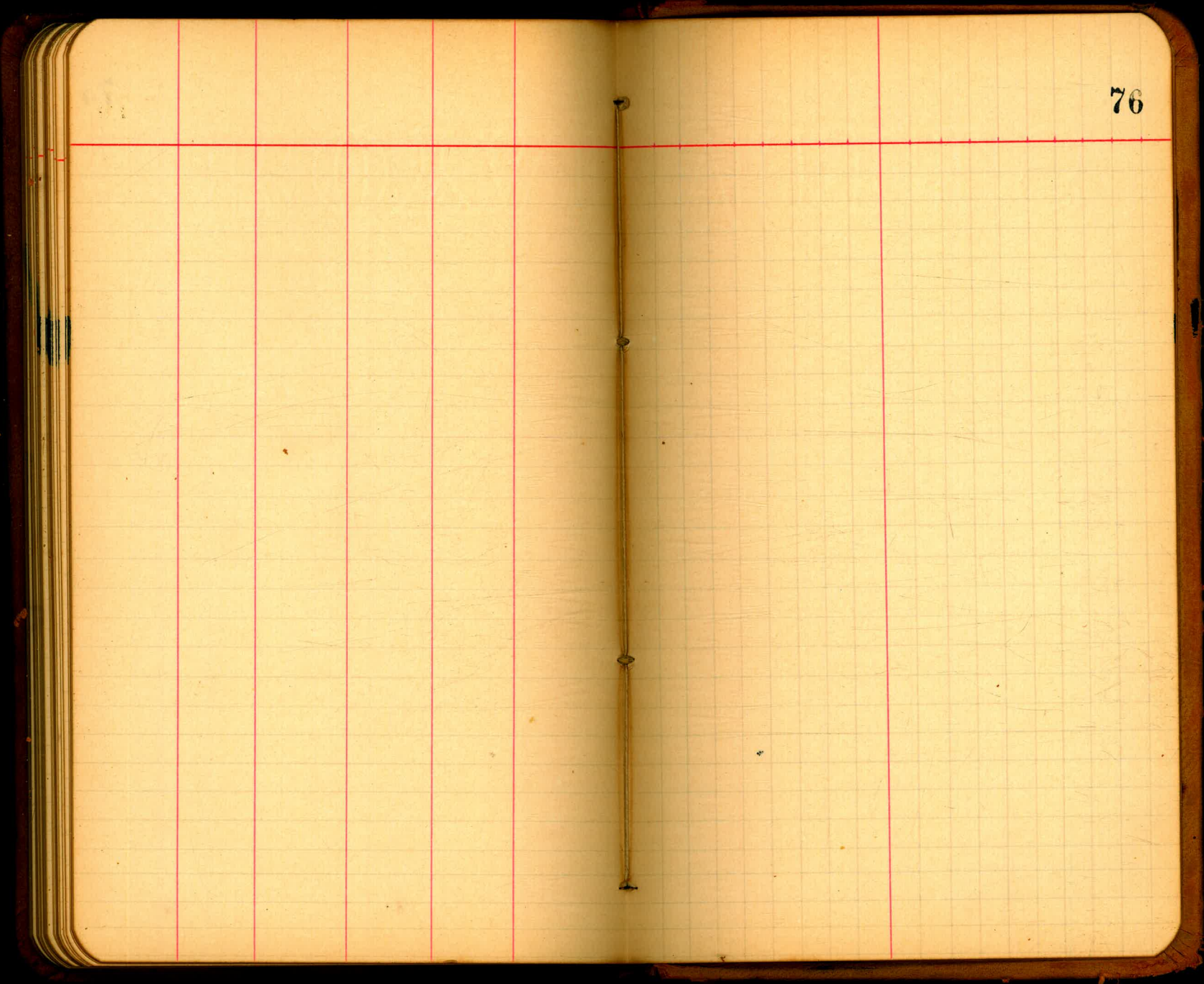
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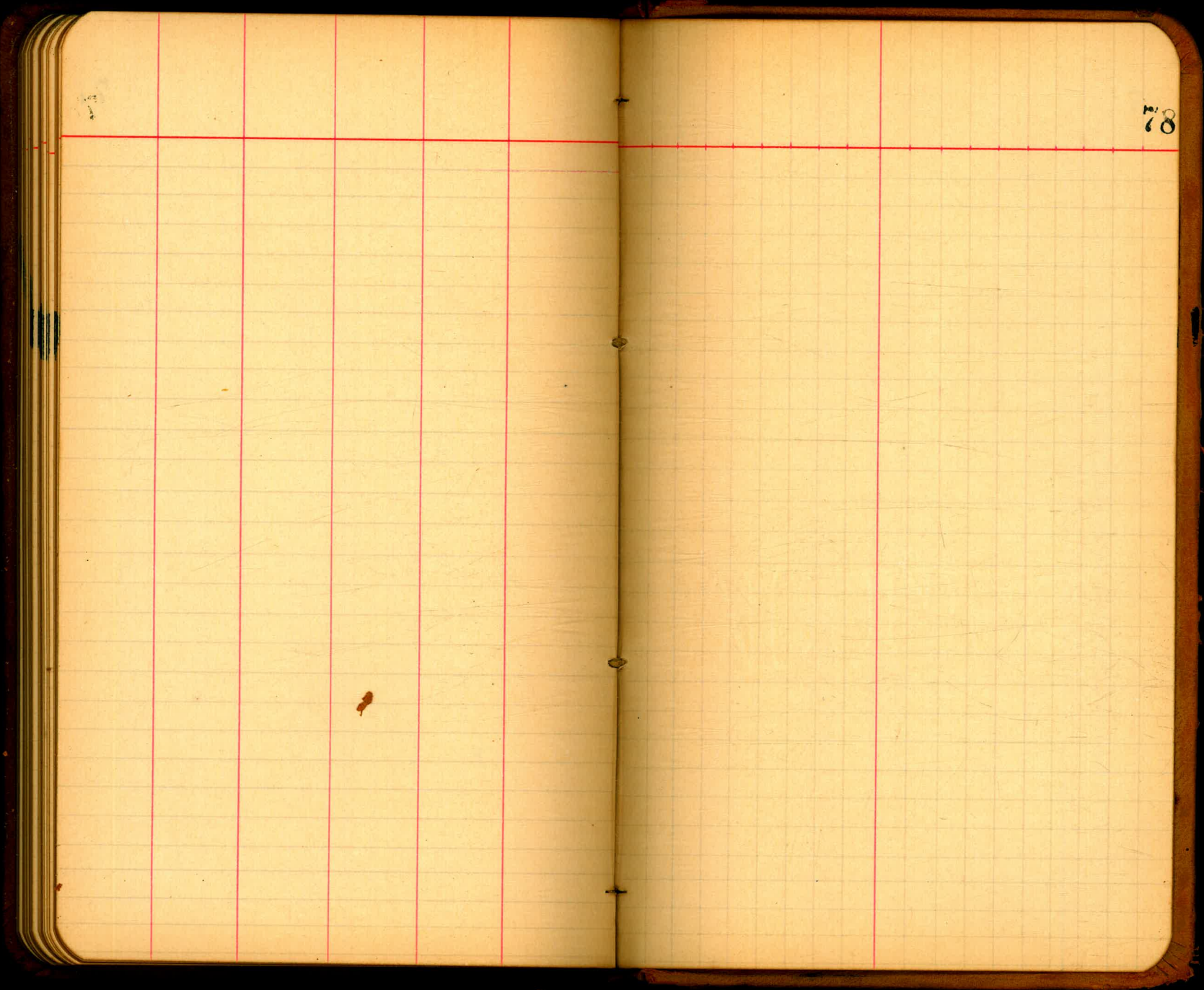
71

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73

74





7

78

68

79

4447

15.00

18.79
4.50
14.29
15.10
78.77

868

74.5
58.8
15.7

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

FOR SINGLE TRACK EMBANKMENT.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.