

1023

TRANSIT-BOOK

1309

MICROFILMED
DEC 17 1964

28496

LOCATION OF CANTONMENT
PIPE LINE ACROSS SAN DIEGO RIVER

copied from
Book 1009

N.B. - From No. end
of No. Trestle, ditch
follows City Boundary
Line

N. End of
N. Trestle

So. End of
No. Trestle

Ditch
997.40

North End of
South Trestle

S. end of S. Trestle

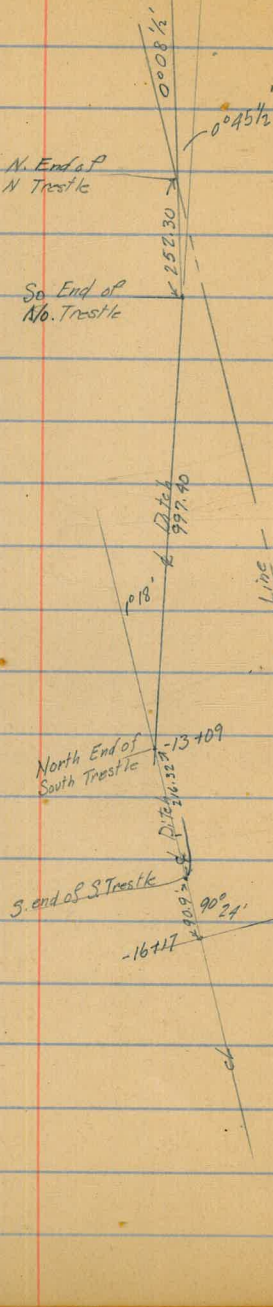
-16+17

90° 24'

14' 00"

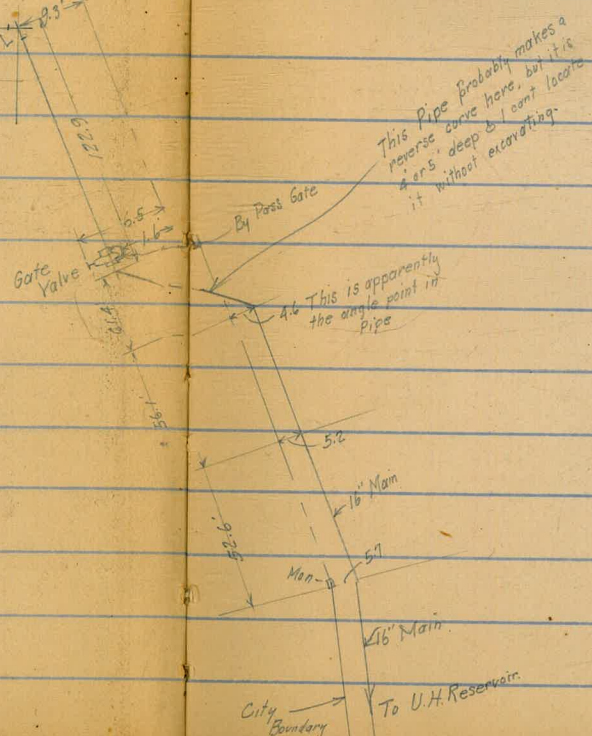
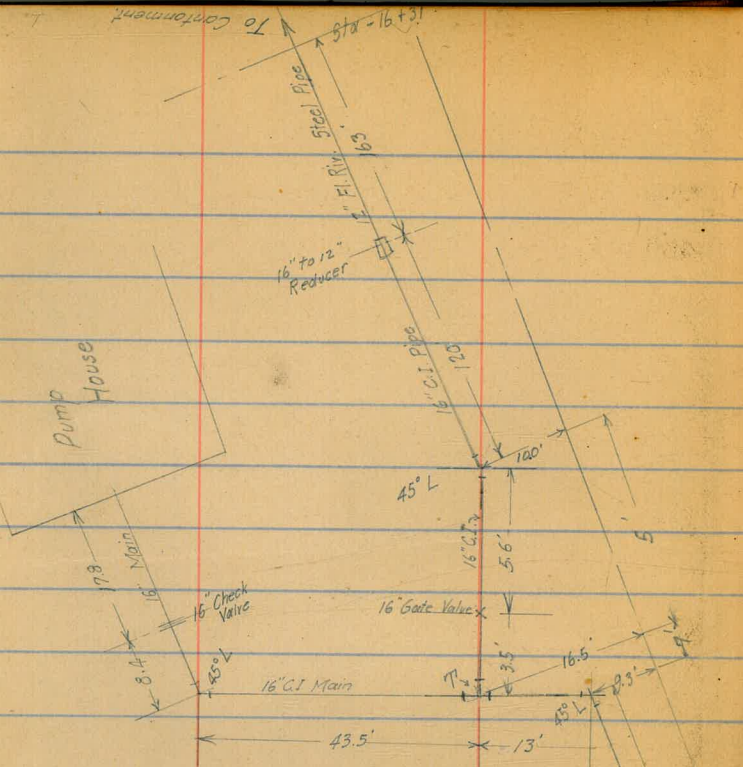
100'

Mon on City
Boundary at
Angle Point



Layout of Mains at Mission Valley Pumping Station
to Connect with Containment Pipe Line.

Copied from Book 1009 p. 54.



This Pipe probably makes a
reverse curve here, but it is
4 or 5' deep & I can't locate
it without excavating.

This is apparently
the angle point in
the Pipes

City Boundary
To U.H. Reservoir.

Final Survey of Cantonment
Pipe Line

(Copy) B 1009 p 58.

3

-16+31

-17+74.20

-17+92.2

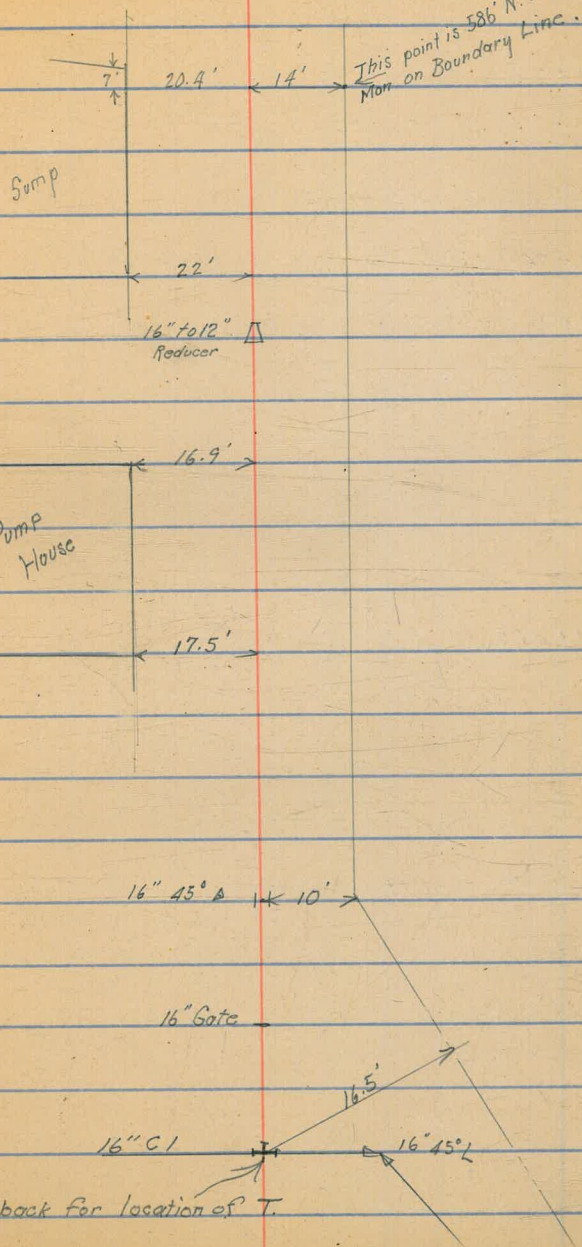
-18+25.4

-18+62.4

-19+12.2 45° L

-19+17.8

-19+21.3



0+00

-0+60.68 $\Delta 0^{\circ} 08\frac{1}{2}' L$

-0+70

-1+00

-3+12.38 $\Delta 0^{\circ} 45\frac{1}{2}' L$

-4+97.5

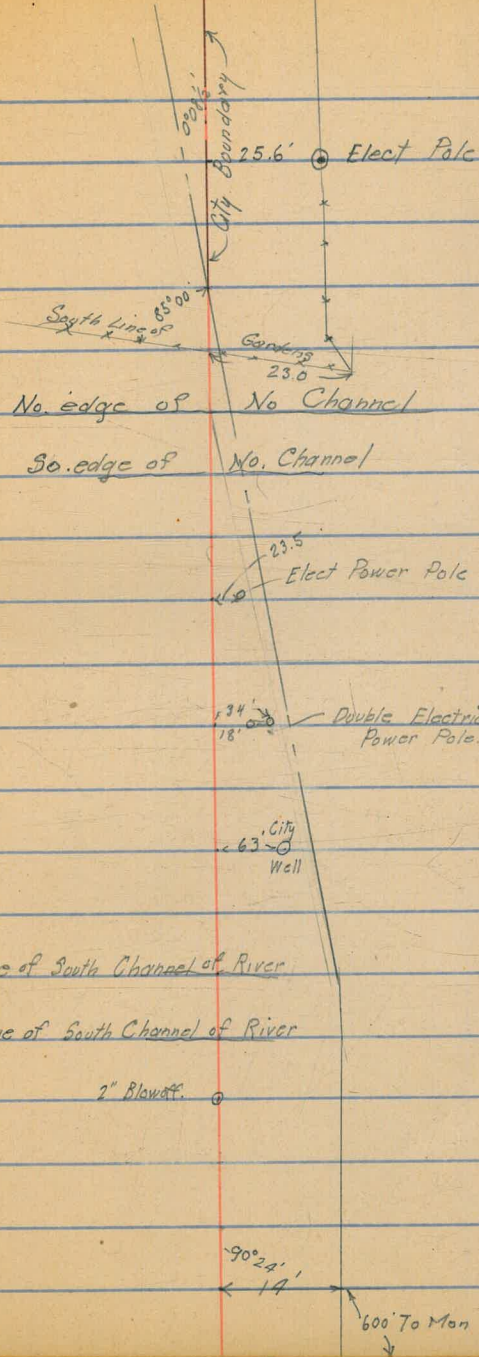
-9+25.5

-10+28

-13+09.78 $\Delta 1^{\circ} 18' R$

-15+26

-15+31

-16+17 $\Delta 0^{\circ} 28' R$ 

7+20

← 35.30 Elect Pole

6+44

Check Valve

62° 35'

36'

5+99.5

← 33.5 Elect Pole

Irrigating

3+92.0

Ditch

3+92

3+51

← 29.5 Elect Pole

Chinese Gardens

← 21.0 Irrigating Well

← 28.5 Elect Pole

1+57

1+48

15151

12179

12174

12110

11179

10185.5

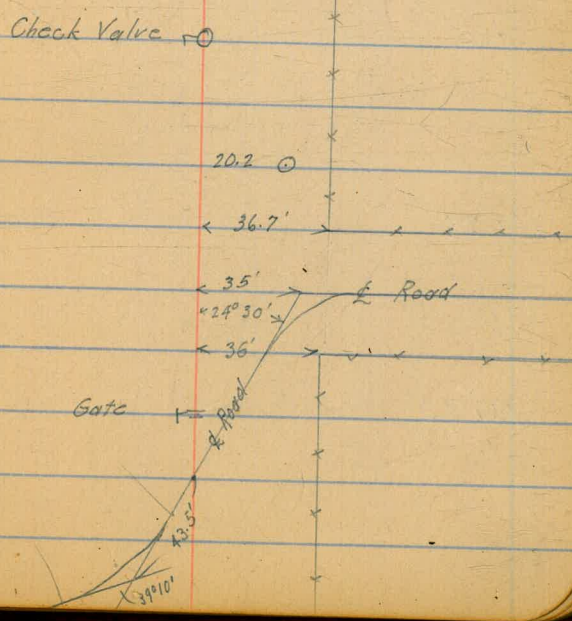
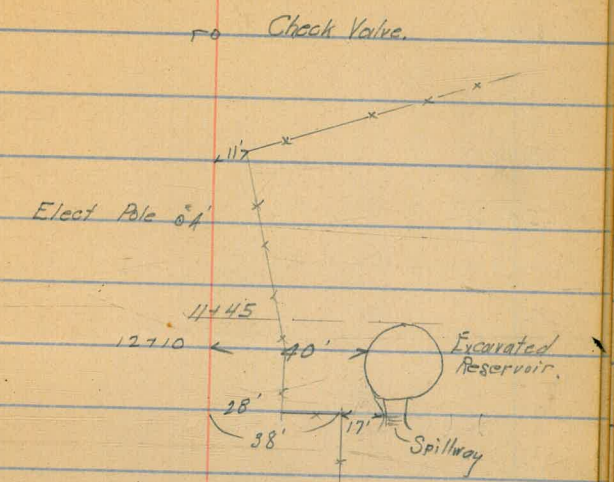
9125

9112.5

8172.4

8161.2

8127



26+24

Elect Pole @ 4.5

23+23

Elect Pole @ 4.5

20+23

Elect Pole @ 4.5

18+50

@ Blowoff.

18+00

Pipe is exposed here for 20'
 & is a good place to slough off
 during rains - Should be braced

17+65

@ Check Valve

16+24

Elect Pole @ 4.5

15+93

@ 2" Blowoff.

36+62.3

○ Check Valve

35+81

○ 5'

35+41

○ 2" Blowoff

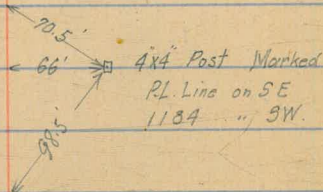
33+80

○ 2" Blowoff

32+24.5

Elec Pole ○ 3:1

32+00



31+00

28+75

El. Pole ○ 4.5

28+00

○ 1" Check Valve

53 + 75

Pole ○ 4.5' →

51 + 97.5

○ 2" Blowoff

50 + 74.6

Pole ○ 5' →

47 + 99.3

Line ○ Check Valve

46 + 76

Pole ○ 4.5' →

42 + 74.5

○ 5' →

Power

39 + 25.3

Pole ○ 5' →

36 + 99

○ 2" Blowoff

71+ 53

68+ 27

67+ 99

67+ 88.4

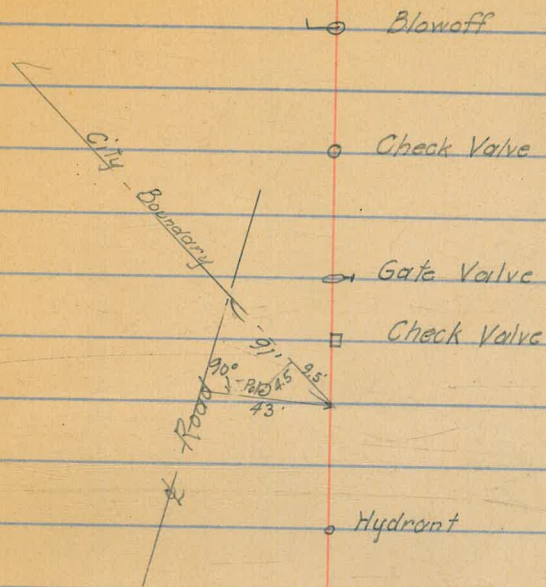
66+ 56.9 Δ 43° 35' R.

66+ 38

64+ 26

60+ 76.5

57+ 25.3



0.43
Elec Pole

Line

0.4
Pole

Power

0.35
Pole

92 + 79.0

91 + 72.5

89 + 64.0

88 + 07.0

87 + 28.0

86 + 81.0

86 + 38.5

84 + 98.5

80 + 03.5

Tel 5'
Pole

Tel 5'
Pole

Tel
Pole

Line
Tel
Pole

Hydrant

Tel
Pole

Multiple Wire

27'

~~Road~~

Blow off left out Hydrant
will do.

Check Valve

109+16

108+66.3

108+31.0

108+27.5

A 16° 30' Left.

107+10.5

105+98.5

105+48.5

103+89

102+25.5

100+62.5

99+04.5

98+08.5

97+47.0

95+89.0

94+98.5

94+28.7

Road

109+16.0

3.0 Tel Pole

Hydrant

Tel Pole
7'Line
27'Tel Pole
6.5'Tel Pole
6.5'Tel Pole
6'Tel Pole
6'Tel Pole
6'Tel Pole
6'Tel Pole
6'Tel Pole
6'Tel Pole
5'

27'

Mutt

Tel Pole
5'

Pole

Road

Check Valve Not in as yet.

128+72.4

129+62.4

128+39.1

127+80.7

127+62

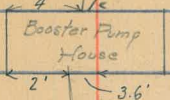
127+18.5

121+14

114+32.3

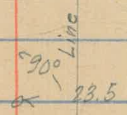
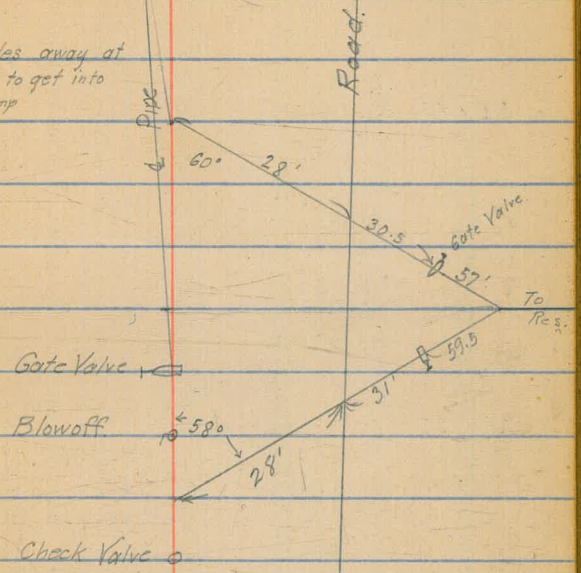
110+11.5

Elev Floor 413.98
Center Pump 1.9' above floor



gt 128+66 for ctr. Pump.

Pipe angles away at Gate Valve, to get into Booster Pump



Spike

White 4" x 4" nailed on S.E. Edge

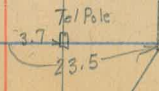
12-10

25.3

41.95

201.7

4x4



190+10

186+79.5

176+50

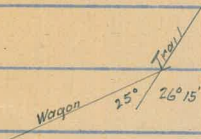
167+59.5

155+35

140+15

140+09.5

Check Valve



6' x 16.5'

Line

1" Check Valve

Tel

6' x 20'

Two Wire

Road

Multi Wire Tel Line

47'

Check Valve * End of St. Riv. Pipe & Beginning of M.B. Wood Pipe

218+33.5 Δ 4°13' L

216+91.8 → to Gov. B.M.

216+71.8

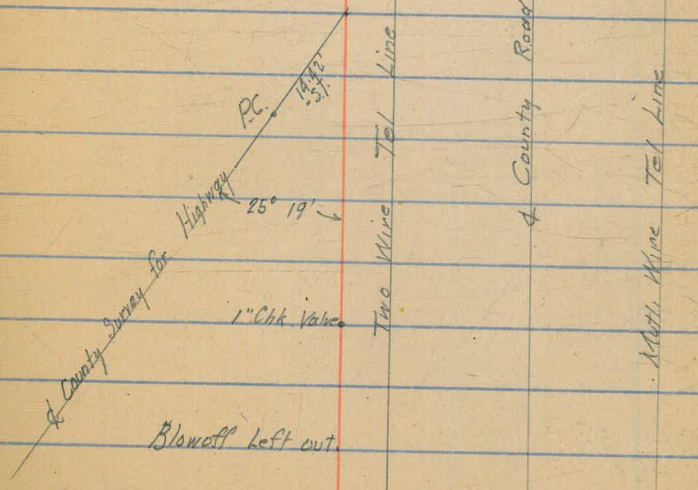
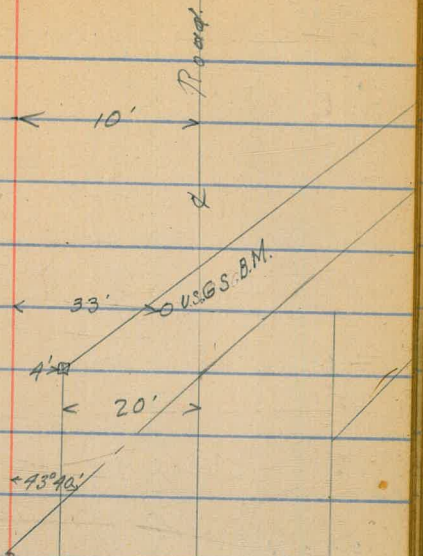
216+37.8

216+08.5

211+09.5

206+09.5

201+00 Δ 0°22' L



7.5 ← 20' × 20' →

3.5 is added to original stem back of this point
From this point on 6.6 is substituted from original stemming.

280 + 44.7 Δ 39° 23' R.

276 + 27

276 + 11

272 + 26.5

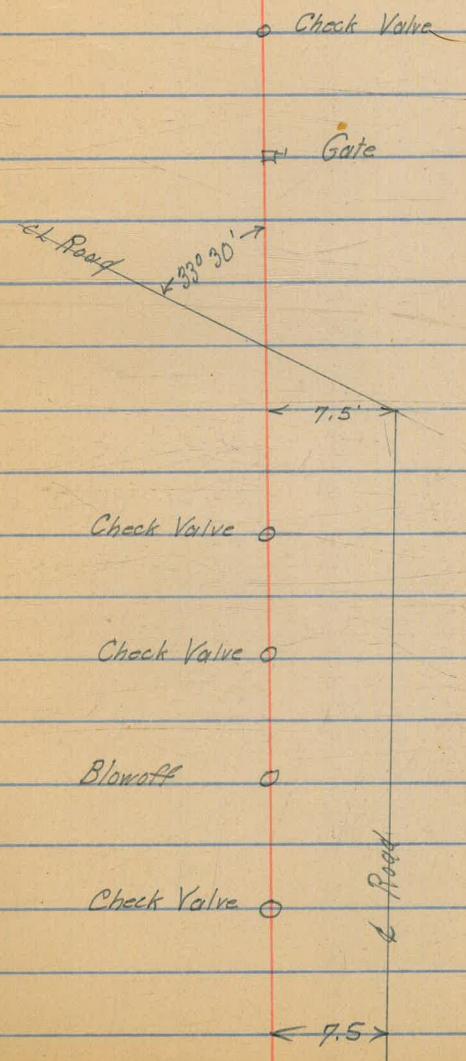
272 + 15.0

272 + 10

247 + 10

239 + 76

237 + 58.5



292 + 43.4

290 + 43.4

288 + 43.4

286 + 60

286 + 55

River

175' Head W.S. X 150' Head W.S. X 125' Head Wood Stave X 100' Head Wood Stave

Bank

○ Blowoff

319+92.4

3" Tapped Collar with Plug ○

314+93.4

3" Tapped Collar with Plug ○

309+93.4

3" Tapped Collar with Plug ○

305+93.4

2" Check Valve ○

304+93.4

3" Tapped Collar with Plug ○

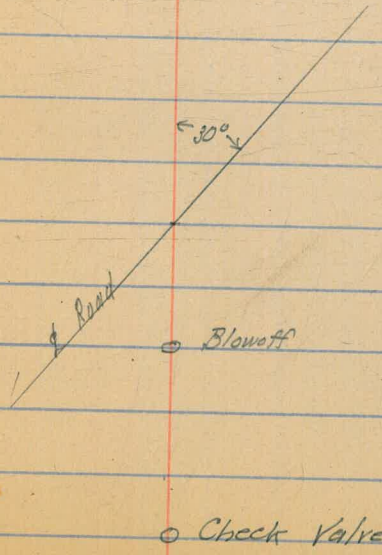
299+93

3" Tapped Collar with Plug ○

296+23

294+24.4

293+04.4



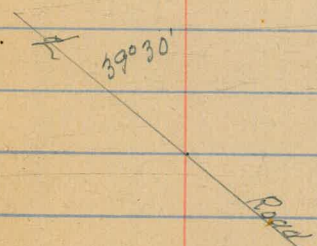
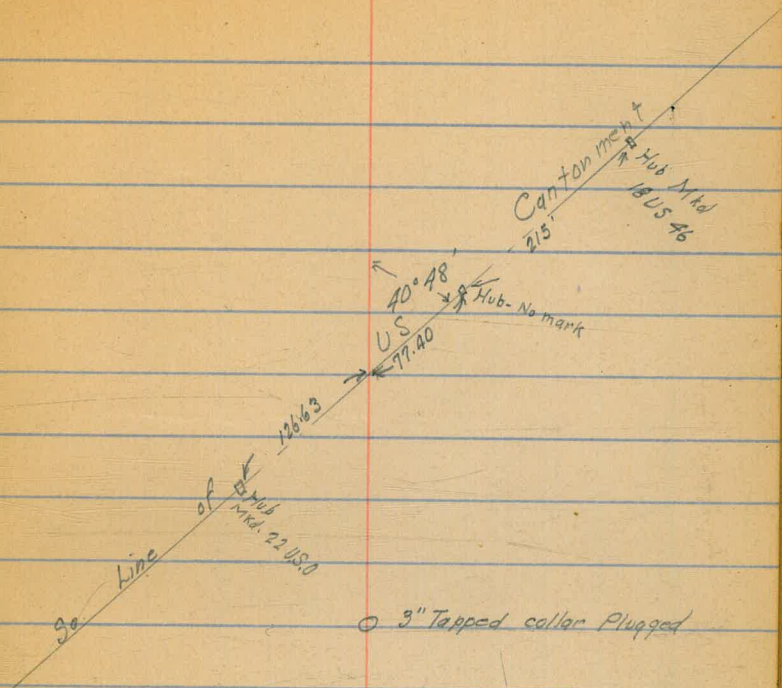
348 + 93.4 Δ 12° 00' R

347 + 63.8

329 + 88.7

325 + 46.8

324 + 90.1



3" Tapped Collar Plugged ○

371+54.6

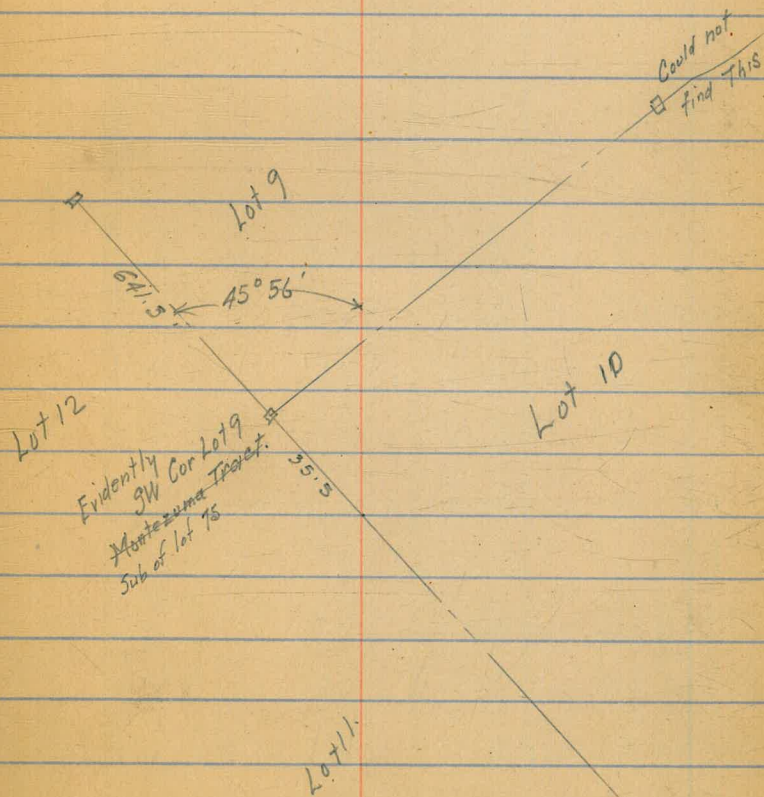
Hub Marked OUS 34

11.8'

188.70'

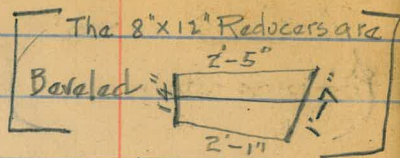
Hub marked
OUS 36

387 + 88.5



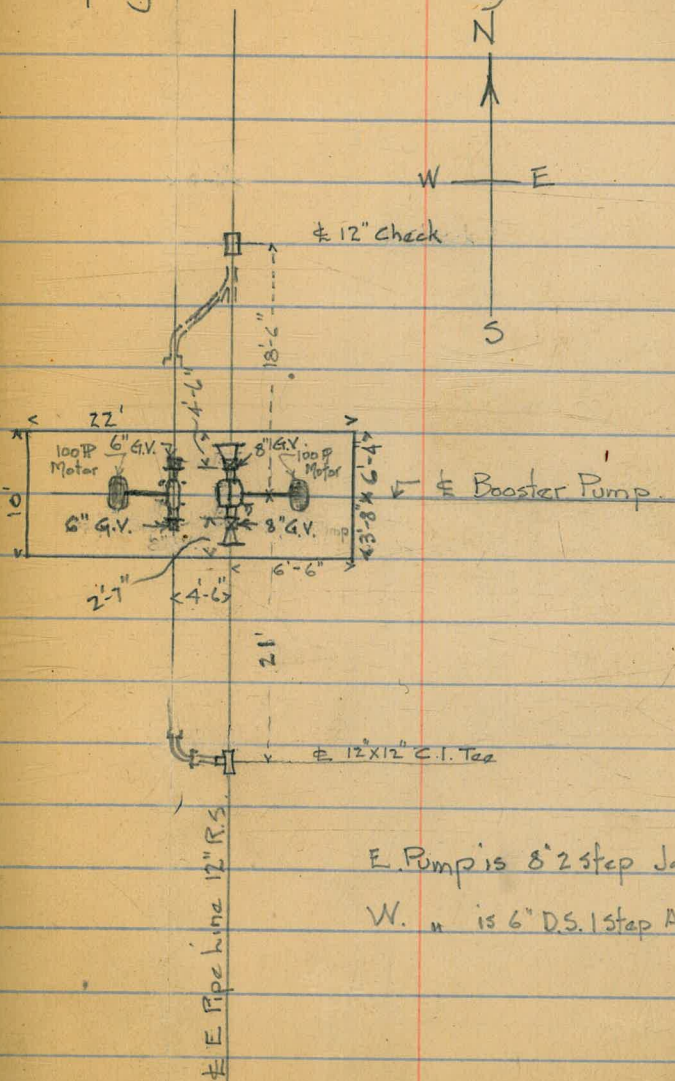
Required

2 - 6" x 12" Flanged Reducers
(not banded)



Sketch Showing Details of Linda Vista Booster Pumping Station.

May 1st 1918. G.C.



On Hand at Pump.

1 Pc 12" RS. 12'-0" 1 Flange

1 " " 4'-0" " "

1 " " 3'-1" 2 " 10° Bend ±

1 " " 3'-0" 6 J. 45° " ±

On Hand at Yard

1 - 12" x 12" x 12" 45° Y

2 - 6" Fl. Gates

2 - 8" " "

1 - 12" 90° El.

1 - " 45° "

E. Pump is 8' 2 step Jackson Church

W. " is 6" D.S. 1 step Allis Chalmers

B.S.

H.I.

F.S.

Elev

405.57

Floor of Pump House
Gregorys Elev 413.98

West Pump

1.72

407.24 Center of Shaft

.84

406.36 Intake Pipe

.84

406.36 Discharge Pipe

East Pump

1.88

407.40 Center of Shaft

1.84

407.36 Intake Pipe

1.84

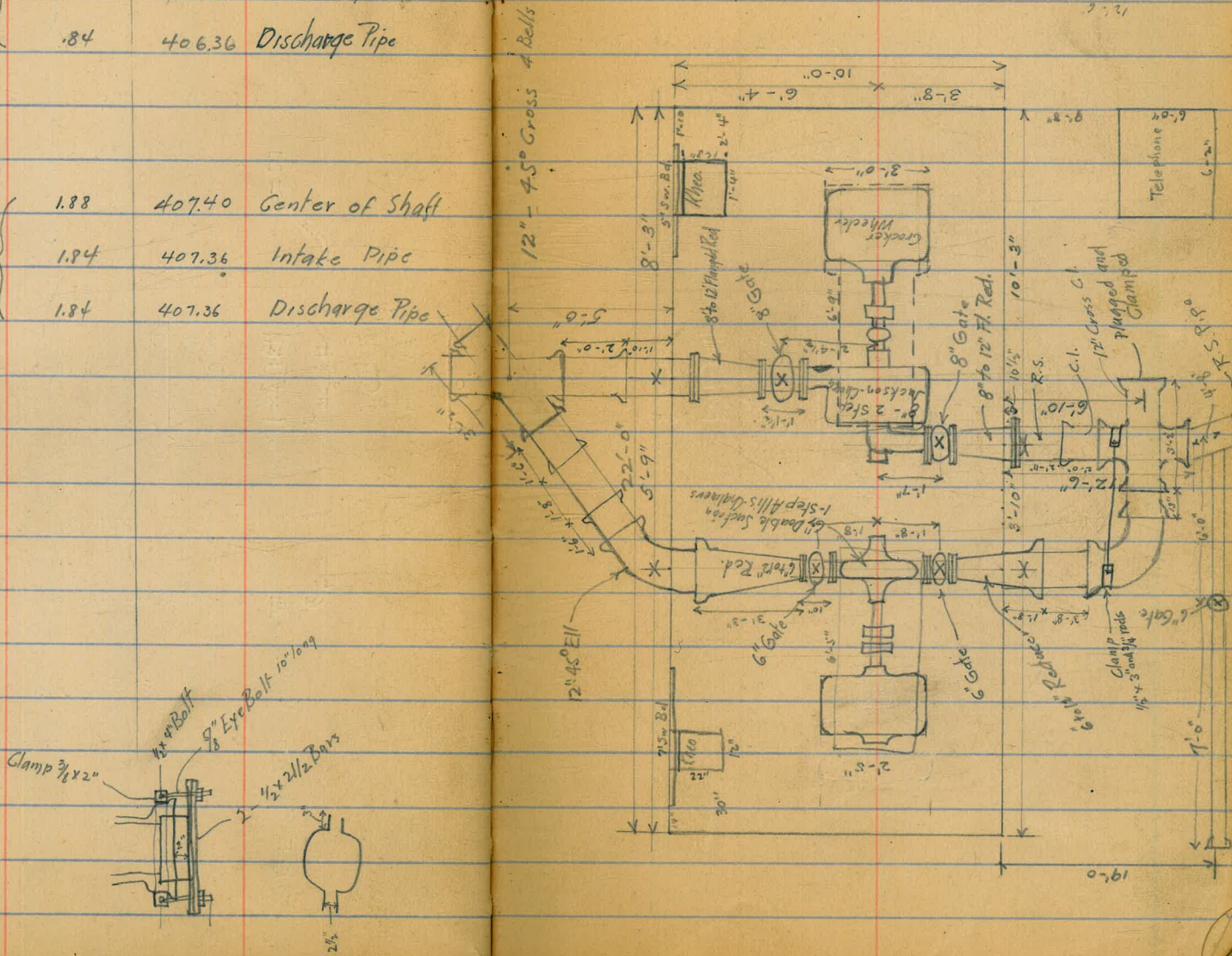
407.36 Discharge Pipe

Linda Vista Booster Pump
Schmidt-Hayler-Offen
May 11, 1918.

See N.B # 1015

22

1015
14-1



Linda Vista Auxiliary Reservoir

May 11, 1918
Hayler Level
often Rod

B.S.	H.I.	F.S.	Elev.	
4.60	410.12		405.52	Floor of Pump Ho.
9.61	416.46	3.27	406.85	B.M. <small>2"x2" Flush with ground S. Side of Shooting Sign over pipe line.</small>
		5.24	411.22	Water Level May 11,
		2.74	413.72	Top of Dyke over
		2.72	413.74	Hub in Top of Dyke

→ City Datum 0 = +8.46 Pipe Line
 Survey Datum used in Book 1015
 1918 11:00 A.M. To obtain elev. referred
 to Pipe Line datum add
 8.46 to elevations given
 in these notes. G. Cromwell.

Cross-Section Linda Vista Auxiliary Reservoir

7 Drip
1-5 Hance
18 B/ro

1+50

	415.35	
P.50	414.35	406.85
	^{.52} 0+76.32	E.C.
15 L - TS	7.7	407.7
2 L	1.2	414.2
C	1.1	414.3
4 R	1.4	414.0
1.5 R	3.6	411.8
15 R	7.9	407.5
	1+00	
15 R - TS	8.1	407.3
4 R	1.3	414.1
C	1.2	414.2
3.5 L	1.8	413.6
6 L	3.7	411.7
15 L	8.0	407.4

Location of Sump

2+46.2

61°10'

E 41°0'

0+76.32

14 L - TS	7.9	407.5
4 L	1.0	414.4
C	1.2	414.2
2 R	1.1	414.3
3.5 R	3.7	411.7
16 R	7.9	407.5
	1+27.33	P.C.
15 R	7.7	407.7
7.5 "	3.7	411.7
3 "	1.2	414.2
C	1.5	413.9
3.5 L	1.5	413.9
13 L - TS	7.1	408.3
	2+00	
13 L - TS	6.8	408.6
2 L	1.2	414.2
C	1.1	414.0
4 R	1.2	414.2
1.5 R	3.7	411.7
16 R	6.9	408.5

2+25
414.35
415.35

2+90.36 E.C.

15 R	7.3	408.1
6.5"	3.4	412.0
2.5"	1.1	414.3
C	1.4	414.0
2.5 L	1.3	414.1
13 L T.S.	6.4	409.0

14 L T.S.	7.2	408.1
3'	1.3	414.1
C	1.3	414.1
3 R	1.0	414.4
6"	3.5	411.9
12"	6.1	409.3
17"	7.2	408.2

2+50

3+50

15 L T.S.	7.3	408.1
2.5"	1.2	414.2
C	1.3	414.1
3 R	1.2	414.2
6.5"	3.2	412.2
16"	7.4	408.0

17 R	7.4	408.0
12"	6.2	409.2
6"	3.5	411.9
3"	1.2	414.2
C	1.1	414.3

2+75

19 R	7.5	407.9
11"	5.7	409.7
5	3.2	412.2
3	1.4	414.0
C	1.4	414.0
2.5 L	1.3	414.1
14" T.S.	7.3	408.1

5 L	1.4	414.0
14" T.S.	6.8	408.6

4100 ¹⁴ P.C.414.35
415.35

12' L = T.S.	6.2	409.2
3 "	1.2	414.2
C	1.3	414.1
3 R	1.4	414.0
5 "	3.4	412.0
17 "	6.4	409.0

4125

15 R	6.5	408.9
10 "	4.7	410.7
5.5 "	3.1	412.3
3.5 "	1.3	414.1

C	1.5	413.9
3.5 L	1.5	413.9
12' L = T.S.	6.5	408.9

4150

10' L = T.S.	5.3	410.1
3 "	1.3	414.1
C	1.5	413.9
4 R	1.4	414.0
6 "	3.8	412.1
14 "	6.7	409.2
20 "	7.0	408.4

Cross Section bet 4150 to 24+25

0+00 = C 4150	1.5	413.9
+50	7.4	408.0
1	8.4	407.0
150	9.1	406.3
2	10.7	404.7
150	10.6	404.8
3	10.9	404.5
+50	10.3	405.1
4	8.9	406.5
5ump	10.8	404.6

Cross Section bet. 5+492 & 23+00

4	9.0	406.4
+50	10.3	405.1
3	10.0	405.4
+50	9.9	405.5
2	9.8	405.6
+50	9.5	405.9
1	10.3	405.1
+50	9.1	406.7

0+00 = 5+492

415.35

417.75
+16.35
415.35

512.5

12' L = T.S.	6.3	409.1
0 "	1.2	414.0
C	1.5	413.9
4' R	1.4	414.0
5 "	3.2	412.2
14 "	6.1	409.3
22 "	7.2	408.2

16' L = T.S.	6.0	409.4
4 "	2.0	413.4
C	1.6	413.8
5.5 R	1.7	413.7
8 "	3.6	411.8
16 "	5.7	409.7
30 "	7.2	408.2

510.0

514.92 = F.C.

20' R	7.1	408.3
12 "	5.9	409.5
5.5 "	3.6	411.8
3	1.4	414.0
C	1.2	414.2
5' L	1.9	413.5
12' L = T.S.	6.2	409.2

25' R	7.1	408.3
15 "	6.3	409.1
4.5 "	3.1	412.3
3 "	1.4	414.0
C	1.3	414.1
4.5 L	1.3	414.1
11' L = T.S.	5.9	409.5

T.P. 1.36

(415.53) ✓
414.53

(414.17) ✓
413.17 = 414.53 - 1.36

6+00
~~414.53~~
 415.53

7+00

13L = T.S.	66	408.9
16.	16	413.9
C	12	414.1
3R	14	413.9
5	26	413.1
6.5"	34	412.1
12"	49	410.6
19"	71	408.4

13L = T.S.	69	408.6
4.5	16	413.9
C	16	413.9
3R	18	413.7
4.5"	31	412.4
10.5"	49	410.6
13"	62	409.1
18"	77	407.8

6+50

7+50

16R	76	407.9
12.	62	409.3
11	48	410.7
5.5"	32	412.3
4.5"	18	413.7
C	16	413.9
3.5L	14	413.9
12L = T.S.	64	409.1

20R	75	408.0
13.	61	409.4
11	48	410.7
5	32	412.3
C	18	413.7
↓L	20	413.5
13L = T.S.	68	408.7

415.53

Cross Section bet Sta 6+00 to Sta 7+00

0+00 = Sta 6+00			
+50	89	406.6	
	10.7	404.8	
+50	100	405.5	
✓	106	404.9	
+50	97	405.8	
3	96	405.9	
+50	75	408.0	

Cross Section bet Sta 7+00 to Sta 8+50

+50	82	407.3	
3	102	405.3	
+50	103	405.2	
✓	100	405.5	
+50	96	405.9	
1	110	404.5	
+50	88	406.7	

0+00 = Sta 7+00

8+00			
13.1 L-T.S.	68	408.7	
5	17	413.8	
C	16	413.9	
3 R	15	414.0	
4	32	412.3	
10.6	48	410.7	
13 "	63	409.2	
19 "	76	407.9	

8+50

17 R	75	408.0	
13 "	65	409.0	
11 "	49	410.6	
8 "	32	412.3	
3.5 "	20	413.5	
C	16	413.9	
4.6 L	17	413.8	
13.6 L-T.S.	75	408.0	

415.53

9+00

13.5 L T.S.	72	408.3
4 "	17	413.8
C	17	413.8
2.5 R	21	413.4
3.5 "	31	412.4
10 "	49	410.6
17.5 "	61	409.4
18 "	75	408.0

9+29.99 PC

20 R	71	408.4
13.5 "	61	409.1
11 "	49	410.6
6.5 "	38	411.7
3.5 "	20	413.5
C	17	413.8
4.5 L	19	413.6
14 L T.S.	70	408.5

Cross-section bet Sta 8+00 & Sta 19+82.0

450	95	406.0
3	97	405.8
+50	97	405.8
Y	98	405.7
+50	97	405.8
1	102	405.1
+50	88	406.7

0+00 = Sta 8+00

Cross-section bet Sta 9+00 & Sta 18+50

4	92	406.3
+50	99	405.6
3	98	405.7
+50	95	406.0
Y	94	406.1
+50	94	406.1
1	98	405.7
+50	91	406.4

0+00 = 9+00

415.53

Cross-Section bet Sta 9+39.89 & Sta 10+00

+50	77	407.8
H	104	405.1
+50	95	406.0
3	95	406.0
+50	94	406.1
Y	93	406.2
+50	92	406.3
1	95	406.0
+50	92	406.2

0+00 = Sta 9+39.89

Cross-Section bet Sta 11+15.30 & Sta 10+00

+50	99	405.6
3	99	405.6
+50	91	406.4
Y	94	406.1
+50	91	406.4
1	89	406.6
+50	82	407.3

0+00 = Sta 11+15.30

31

Cross-Section bet Sta 12+50 & Sta 10+00

+50	96	405.9
Y	95	406.0
+50	92	406.3
1	95	406.0
+50	92	406.3
0+00 = Sta 12+50		

Cross-Section bet Sta 14+43.96 & Sta 16+92.57

+50	82	407.3
1	89	406.6
+50	98	405.7
0+00 = Sta 14+43.96		

1199	412.84	406.85
T.P. 1.85	415.89 9+75	414.02
13" T.S		7.2 408.7
2"		20 413.9
C		1.9 414.0
4R		2.2 413.7
5.5"		3.8 412.1
11"		5.1 410.5
14		6.9 409.0
17		8.0 407.9

10408
415.89

415.89

10450

18 R	79	408.0
13 "	68	409.1
10 "	52	410.7
4 "	36	412.3
3 "	20	413.9
C	19	414.0
4 L	20	413.9
14 L-T.S.	75	408.4

10425

15 L-T.S.	78	408.1
45 "	20	413.9
C	20	413.9
4.5 R	20	413.9
5.5 "	(4.2) [?] 12	411.7
12 "	58	410.1
18 "	77	408.2

15 R	76	408.3
11 "	58	410.1
3.5 "	21	412.5
2 "	18	414.1
C	17	414.2
4 L	20	413.9
13 L-T.S.	74	408.5

10475

15 L-T.S.	79	408.0
3.5 "	23	413.6
C	20	413.9
3 R	23	413.6
4 "	36	412.3
10 "	52	410.7
12 "	66	409.3
16 "	79	408.0

$11+00$
 415.89

17 R	79	408.0
14 "	67	409.2
11 "	52	410.7
5 "	35	412.4
4 "	20	413.9
C	17	414.2
4.5 L	22	413.7
16 " = T.S.	80	407.9

 $11+15^3 = EC$

14 L = T.S.	74	408.5
5 "	19	414.0
C	1.9	414.0
2 R	20	413.9
5 "	38	412.1
11 "	52	410.7
14 "	67	409.2
20 "	77	408.2

 415.89
 $11+50$

17 R	77	408.2
12 "	65	409.4
9 "	52	410.7
3 "	36	412.3
1 "	1.9	414.0
C	20	413.9
6 L	20	413.9
12 L = T.S.	57	410.2

 $12+00$

13 L = T.S.	72	408.7
3.5 "	18	414.1
C	1.8	414.1
2 R	17	414.2
4 "	37	412.2
10.5 "	52	410.7
14 "	67	409.2
18 "	77	408.5

12+50
415.89

20 R	76	408.3
14 "	65	409.4
12 "	52	410.7
5 "	33	412.6
3.5 "	16	414.3
C	17	414.2
3.5 L	16	414.3
12 L T.S.	68	409.1

13+100

12 L T.S.	70	408.9
3 L	21	413.8
C	21	413.8
4.5 R	21	413.8
5 "	34	412.5
12 "	52	410.7
13 "	65	409.4
18 "	78	408.1

415.89

13+50

18 R	78	408.1
13 "	66	409.3
10.5 "	52	410.7
4.5 "	36	412.3
3 "	21	413.8
C	18	414.1
3.5 L	19	414.0
13 L T.S.	73	408.6

14+100

12 L T.S.	70	408.9
4 "	20	413.9
C	20	413.9
4 R	21	413.8
5.5 "	35	412.4
11 "	53	410.6
14 "	67	409.2
18 "	80	407.9

415.89
141429512C

17 R	76	408.3
13 "	66	409.3
10.5 "	53	410.6
5.5 "	36	412.3
4 "	23	413.6
C	2.0	413.9
4 L	22	413.7
13 L = T.S.	71	408.8

14175

13 L = T.S.	71	408.8
3 L	17	414.2
C	16	414.3
4 R	17	414.2
6 "	37	412.2
16.5 "	53	410.6
13 "	67	409.2
17 "	74	408.5

415.89
15100

14 R	78	408.1
11 "	66	409.3
8.5 "	52	410.7
4.5 "	37	412.2
2.5 "	19	414.0
C	19	414.0
4 L	23	413.6
14 L = T.S.	72	408.7

15125

15.5 L = T.S.	77	408.2
4 "	24	413.5
C	21	413.8
3 R	22	413.7
4 "	35	412.4
10 "	51	410.8
12.5 "	65	409.4
18 "	75	408.4

15+50
415.89

22 R	25	408.5
12 "	6.5	409.4
6 "	47	411.2
35 "	34	412.5
✓	19	414.0
C	21	413.8
3.5 L	22	413.7
15 " = T.S	84	407.5

15+75

14 L = T.S	8.5	407.4
3 L	22	413.7
C	23	413.6
3 R	21	413.8
4 "	32	412.7
6.5 "	45	411.4
10 "	50	410.9
13	67	409.2
15	78	408.1

415.89

16+00

15 R	79	408.0
10.5 "	5.1	410.8
5.5 "	3.5	412.4
4 "	21	413.8
C	23	413.6
4 L	22	413.7
15 L = T.S	83	407.6

16+75

17 L = T.S.	8.5	407.4
2.5 L	1.7	414.2
C	19	414.0
3.5 R	20	413.9
6 "	4.5	411.4
10.5 "	5.3	410.6
16 "	7.7	408.2

16+50
215.89

15 R	79	408.0
17.5	65	409.4
10 "	50	410.9
6 "	38	412.1
3 "	25	414.4
C	18	414.1
3 L	17	414.2
16 L-TS	79	408.0

16+75

16 L-TS	78	408.1
3 "	18	414.1
C	20	413.9
4 R	18	414.1
7.5	43	411.6
11 "	51	410.8
16 "	75	408.4

415.89
16+93.52 EC.

16 R	84	407.5
10 "	50	410.9
6 "	42	411.7
3.5	20	413.9
C	20	413.9
3.5 L	19	414.0
16 L-TS	89	407.0

17+50

14 L-TS	76	408.3
3.5 L	20	413.9
C	22	413.7
3 R	22	413.5
5.5 "	43	411.6
10 "	52	410.7
15 "	80	407.9

T.P 266 416.70 1.85 414.04

18400
416.70

14 R	86	408.1
11 "	73	409.4
8.5 "	57	411.0
5.5	47	412.0
2 "	25	414.2
C	25	414.2
4.5 L	25	414.2
14" = T.S.	80	408.7

18450

14" = T.S.	83	408.4
4.5 "	27	414.0
C	25	414.3
2.5 R	25	414.2
6 "	46	412.1
10 "	57	411.0
14 "	85	408.2

416.70

19400

16 R	89	407.8
13.5 "	79	408.8
9 "	57	411.0
6 "	45	412.2
4 "	27	414.0
C	23	414.4
4 L	27	414.0
13 L = T.S.	79	408.8

19412²³ = P.C.

12.5 L = T.S.	74	409.3
3.5 "	29	413.8
C	27	414.0
6 R	31	413.6
7 "	50	411.7
10 "	58	410.9
13 "	80	408.7

19+50
416.70

19' R	23	408.4
12 "	72	409.5
8 "	56	411.1
5 "	46	412.1
3 "	23	413.4
C	18	413.9
6.5 L	30	413.7
15 L = T.S.	75	409.2

19+82.10 EG

15 L = T.S.	80	408.7
5.5 "	29	413.8
C	30	413.7
2.5 R	31	413.6
6 "	48	411.9
12 "	58	410.9
15 "	88	407.9

416.70
20+50

16' R	90	407.7
10.5 "	72	409.5
5.5 "	52	411.5
2 "	30	413.7
C	28	413.9
5 L	28	413.9
12 L = T.S.	62	410.5

20+67 40 PC

12 L = T.S.	67	410.0
4.5 "	27	414.0
C	28	413.9
3 R	28	413.9
8 "	58	410.9
11 "	72	409.5
17 "	87	408.0

214.00
416.70

25' R	89	407.8
13 "	70	409.7
75 "	48	411.9
5 "	30	413.7
C	25	414.2
3 L	27	414.0
11 " T.S.	64	410.3

214.25

10 L T.S.	59	410.8
3 "	56	414.1
C	29	413.8
U R	30	413.7
7 "	50	411.7
12 "	18	409.9
36 "	82	408.5

20

416.70

214.50

35' R	82	408.5
15 "	72	409.5
75 "	52	411.5
35 "	26	414.1
C	28	413.9
3.5 L	27	414.0
9' L T.S.	56	411.3

214.25 = EC

10 L T.S.	61	410.6
4' L	25	414.2
C	27	414.0
3 R	25	414.2
8 "	50	411.7
15 "	72	409.5
25 "	80	408.3

222.50
416.70

17' R	87	408.0
12"	75	409.2
6"	48	411.9
4"	3.0	413.7
C	28	413.9
4.5 h	27	414.0
11" - T.S.	71	409.6
	23400	
12 L - T.S.	73	409.4
4.5	31	413.6
C	32	413.5
2.5 R	32	413.5
6"	50	411.7
15"	87	408.0
	23+662 PC	
15' R	91	407.6
10.5"	75	409.2
5.5	51	411.6
3.	37	413.5
C	31	413.6
5 h	31	413.6
15 L - T.S.	83	408.4

21

	922	415.87	406.85
		24400	
16 L - T.S.	83	407.6	
5"	21	413.8	
C	21	413.8	
2 R	22	413.7	
4.5	41	411.8	
7.5	52	410.7	
10.5	73	408.6	
	24425		
14 R	80	407.9	
10	65	409.4	
5	43	411.6	
2"	22	413.6	
4	22	413.7	
4.5 h	21	413.8	
13 L - T.S.	74	408.5	

2450
415.87

16L = T.S	85	407.4
2.5L	19	414.0
C	20	413.9
3R	23	413.6
6"	42	411.7
8.5"	51	410.8
13"	78	408.1

24175

24'R	91	406.8
17"	88	407.1
10"	64	409.5
35"	42	411.7
3"	23	413.6
C	21	413.8
3L	23	413.6
17" T.S.	85	407.4

415.87
25100

15'L = T.S	86	407.3
2.5"	26	413.5
C	22	413.7
4'R	22	413.7
6.5"	42	411.7
13.5"	79	408.0
16"	87	407.2

25125

16'R	85	407.4
11"	64	409.5
7"	38	412.1
5"	20	413.9
C	21	413.8
2.5L	22	413.7
15'L = T.S.	87	407.2

25+51⁰⁴ EC = 0+76.32

LOT

R

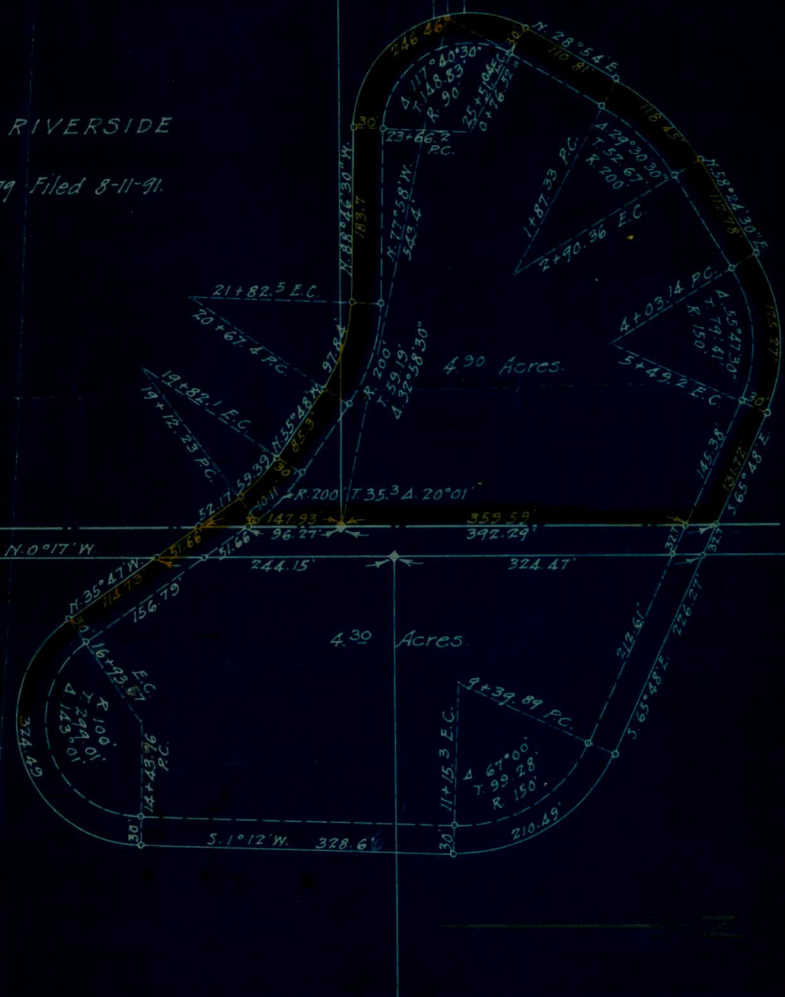
679

LOT 33

LOT 32

RIVERSIDE

679 Filed 8-11-91.



LOT 9.

LOT 8.

DAVID'S SUBDIVISION

Map No 707 Filed 3-17-92.

6/30/22
 Gregor Moore Ellis Shaw
 Cross section of 80' wide
 VERMONT ST
 from N.L. Pennsylvania
 to N.L. C/press
 284.50
 284.96 BP NE Penn

N 4

287.5

Cement return suit
 on N.E. cor 254

N.L. Pennsylvania 80. st. 287.5

E. on cement 285.2

cb ✓ ✓ 285

+ 0.0 = gutr. 284.53

1/2 284.58

0 284.5

1/4 284.08

+ 12.5 283.33

W cb on cement 284

+ 10 " "

wt 284.15

N. curb

wt 284

A

1/2

1/4

1/4

A

El Equitr

on cement curb 254

227 285.23

2.54 284.66

3.6 283.9

3.4 284.1

3.2 284.3

3.6 283.9

4.3 283.2

3.55 283.15

3.33 284.2

4.2 283.3

5.1 282.0

4.4 283.1

4.1 283.4

3.3 284.2

3.3 284.2

3.6 283.9

3.6 283.9

254 84.96

El

cb

+6

1/4

0

1/2

cb

wt

+10

-10

wt

cb

1/4

0

1/4

+7

cb

cb

Mortgage liquid
 Aug 4 1925
 See Book
 1921-2
 1813-1
 8-211?
 9-450 and?

C of Penn

3.2 284.3

3.7 283.8

4.0 283.5

3.5 284.0

3.4 284.1

4.0 283.5

4.6 282.9

5.3 282.2

6.4 281.1

6.2 281.3

5.5 282.0

5.0 282.5

4.4 283.1

3.6 283.9

3.8 283.7

4.0 283.5

3.7 283.8

3.0 284.5

287.50

S 1/4

287.50

247.50

45

S.L. = 0 + 00

EL	3.2	284.3
ct	3.9	283.6
+6	4.2	283.3
1/4	3.8	283.7
0	3.7	283.8
1/4	4.9	282.6
ct	5.2	282.3
wL	5.8	281.7
+10	6.7	280.8

S ct

-10	7.0	280.6
wL	5.8	281.7
ct	5.4	282.1
+8	5.5	282.0
1/4	5.3	282.2
0	4.0	283.5
1/4	3.9	283.6
ct	4.2	283.3
EL gutr.	3.6	283.9
cut. on cement	2.54	284.96

EL	2.6	284.9
+2	3.3	284.2
ct	3.7	283.8
1/4	4.2	283.3
0	4.2	283.3
1/4	5.4	282.1
ct	5.2	282.3
wL	5.8	281.7
+10	6.8	280.7

0 + 25

-5	6.4	281.1
wL	5.7	281.8
ct	5.5	282.0
1/4	5.3	282.2
0	4.1	283.5
1/4	4.1	283.5
ct	3.8	283.7
+13	3.3	284.2
EL on lower	2.7	284.8

	0+50	
EL on lawn	2.7	√84.8
+1	3.0	84.5
ct	3.4	84.1
+4	4.0	83.5
1/4	3.8	83.7
c	3.9	83.6
1/4	4.9	87.6
ct	5.3	87.2
wt	5.9	√81.6 ✓
+5	6.1	81.4

0+75

wt	5.1	√87.4
ct	5.1	√87.4
1/4	4.5	83.0
c	3.8	83.7
1/4	3.9	83.6
+12	3.8	83.7
ct	3.5	84.0
+3	3.1	84.0
+13	2.8	84.7
EL on lawn	2.4	85.1

	1+00	
EL	2.6	√84.9
+2	3.0	84.5
ct	3.4	84.1
+2	3.8	83.7
1/4	3.7	83.8
c	3.5	84.0
1/4	3.8	83.7
+9	4.5	83.0
ct	4.5	83.0
wt	4.3	√83.2 ✓

1+25

wt on lawn	3.1	√84.4
ct	3.3	√84.2
1/4	3.7	√83.8
c	3.6	√83.9
1/4	3.5	√84.0
ct	3.7	√83.8
EL on lawn	3.0	√84.5

287.50

1+50

EL	3.3	√84.2 ✓
cb	3.4	84.1
ly	3.6	84.1
o m. Hole	3.5	√84.0
ly	3.6	√83.9
ct	3.4	√84.1
wb	3.5	√84.0

1+75

wb	3.2	√84.3
cb	3.3	√84.2
ly	3.9	√83.6
o	3.5	√83.7
ly	4.0	√83.5
ct	3.7	√83.8
EL	3.6	√83.9

2+00

EL	4.5	√83.0 ✓
ct	4.4	√83.1
ly	4.3	√83.2

287.50 47

o	4.3	√83.2
ly	4.4	√83.1
cb	3.7	√83.8
wb	3.1	√84.2 ✓

2+25

wb	3.8	√83.7
cb	4.5	√83.0
ly	5.0	√82.5
o	5.0	√82.5
ly	5.2	√82.3
cb	5.4	√82.1
EL	5.7	√81.8

2+50

EL	7.0	√80.3 ✓
cb	7.0	70.5
ly	6.5	√81.0
o	6.2	√81.3
ly	5.7	√81.8
cb	5.0	√82.5
wb	4.8	√83.0 ✓

287.50

2+75

wk	4.5	283.0
ct	5.5	282.0
+9	6.4	281.1
4	7.1	280.4
6	7.9	279.6
4	9.6	277.9
ct ctr of gulch	11.2	275.7
+7	9.8	277.7
EL	7.8	279.7
	3+00	NK Cypress
EL	8.2	279.7
ct	14.2	278.7
+8. ctr of gulch	20.6	266.9
4	19.6	279.1
+5	19.6	268.9
c	13.8	273.6
+7	9.8	277.7
4	9.8	280.4
ct = edge road	6.3	281.4
		280.7

note Elevations
in circles taken
from Cypress
at R.B.
Crownpoint

287.50

281.8

282.4

5.3

wk

25' So. of NL

wk	5.4	284.1
ct edge road	8.9	278.6
+8	12.4	275.1
4	12.8	274.7
+3	13.0	274.5
c	18.8	268.7
+3	22.6	264.9
4 ctr of gulch	26.8	260.7
ct	20.9	266.6
+4	17.9	269.6
EL	15.1	272.4

Location of Culverts
Vermont + Cypress

Moore
Billis
Stout

284.96

48

194 286.90

W. Co. Vermont 0+00
N.L. Cypress

0+10

5.7 ✓81.2

6.3 ✓80.6

0+14

6.6 ✓80.3

0+20

8.2 ✓78.7

0+35

7.5 ✓79.4

0+70

7.4 ✓79.5

0+80 - Sta. of Cypress

7.5 ✓79.4

T. P. 0.29

274.18

13.01 272.89

E. Co. Vermont 0+00
N.L. Cypress

0+10

1.1 ✓73.1

3.7 ✓70.5

0+14

5.0 ✓69.2

0+20

6.7 ✓69.5

T. P. 1.90

262.53

12.55 261.63

0+70

12.5 ✓51.0

0+90

9.1 ✓54.4

Moore
8/11/45

CROSS SECTION OF
VERMONT ST
PENN TO CYPRESS

80' wide
14' SW
13' 1/4 S

288.33

49

Penn
NEOP VERMONT

337

288.33

284.96

Penn.
SL (VERMONT) = 0+00

50'S

EL	4.0	843
+ 1" Pepper tree 1 1/2" diam.	4.4	839
cb	4.6	837
1/4	4.9	834
c	4.9	834
1/4	6.0	823
cb	6.1	822
wk	6.4	819

25'S

wk	6.6	817
cb	6.2	821
1/4	6.1	822
c	5.0	833
1/4	4.9	834
cb	4.5	838
+ 2" pepper tree 1 1/2" D	4.3	840
EL	4.3	840

EL	3.9	844
+ 1" Pepper tree 1 1/2" diam	4.2	841
cb	4.4	839
+ 1/4	4.8	835
1/4	4.7	836
c	4.7	836
1/4	4.9	834
cb	6.0	823
wk	6.4	819

78'S

wk	5.9	824
cb	6.0	823
1/4	5.3	830
c	4.6	837
1/4	4.7	836
cb	4.5	838
+ 2" pepper tree 1 1/2" D	3.8	845
EL	3.6	847

101'S

EV	3.8	845
cb	4.2	841
1/4	4.6	837
C	4.3	840
1/2	4.7	836
cb	5.3	830
+3 pepper tree 14" D	5.1	832
WV	4.9	834

106'S on E side v'ant ^{3.8} 845
pepper tree 14" diam.

120'S

WV	4.1	842
+11	4.3	840
cb	4.5	838
1/4	4.5	838
C	4.3	840
1/4	4.4	839
cb	4.4	839
+2	3.9	844
EV	3.9	844

159.5'S

EV	4.2	841
cb	4.4	839
1/2	4.6	837
C	4.6	837
1/4	4.5	838
cb	4.1	842
+2 pepper tree 36" diam	3.9	844
WV	3.9	844

177'S

WV	4.0	843
cb	4.2	841
+2	4.8	835
1/2	5.0	833
C	5.0	833
1/4	4.9	834
cb	5.2	831
+3	4.6	837
+11.5 pepper Tree 14" diam	4.1	836
EV	4.1	838

200'S

EL	5.0	833
+ 2.5 pepper tree, 10" DIAM	5.3	830
+ 13	5.3	830
cb	5.8	825
1/4	5.7	826
c	5.6	827
1/4	5.5	828
cb	5.0	833
+ 1	4.5	838
WV	4.0	843

181'S = DEAD PALM 2" DIAM. 11' E of W.L.

202'S = pepper tree 16" ✓ ✓ ✓ ✓

225'S

WV	4.6	837
cb	5.0	829
+ 1	6.1	822
1/4	6.3	820
c	6.2	821
1/4	6.7	816

✓

6	6.9	814
+ 1	6.4	819
EL	6.0	823

242'S

EL	4.7	816
+ 3.5' = Eucalyptus 4" DIAM	7.0	813
+ 11	7.3	810
cb	7.7	806
1/4	7.5	808
c	6.9	814
1/4	6.8	815
+ 11	6.7	816
cb	6.3	820
+ 2	5.7	826
WV	5.2	831

245'S = pepper tree 14" DIAM 11' E of W.L.

266'S

WV	5.9	824
cb	6.3	820
+ 6	6.9	814 ✓

288.33

2665

1/4	7.4	809
c	8.0	803
1/4	8.6	797
cf	8.9	794
+10 Eucalyptus 12" diam	8.4	799
+11 ✓ 10" ✓	7.3	810
EV	7.3	810
		810
EV	8.1	807
+3	8.8	795
cf	8.9	794
1/4	8.9	794
c	8.4	799
1/4	7.7	806
+10	7.4	809
cf	7.0	813
+3 = pepper 16" diam	6.8	815
w/c	6.3	820
		300'S = all eypress
w/c	6.6	817
+9	7.1	812

288.33

52

cf	7.7	806
1/4	8.0	803
c	8.8	795
1/4	9.4	789
cf	9.2	791
EV	8.7	796

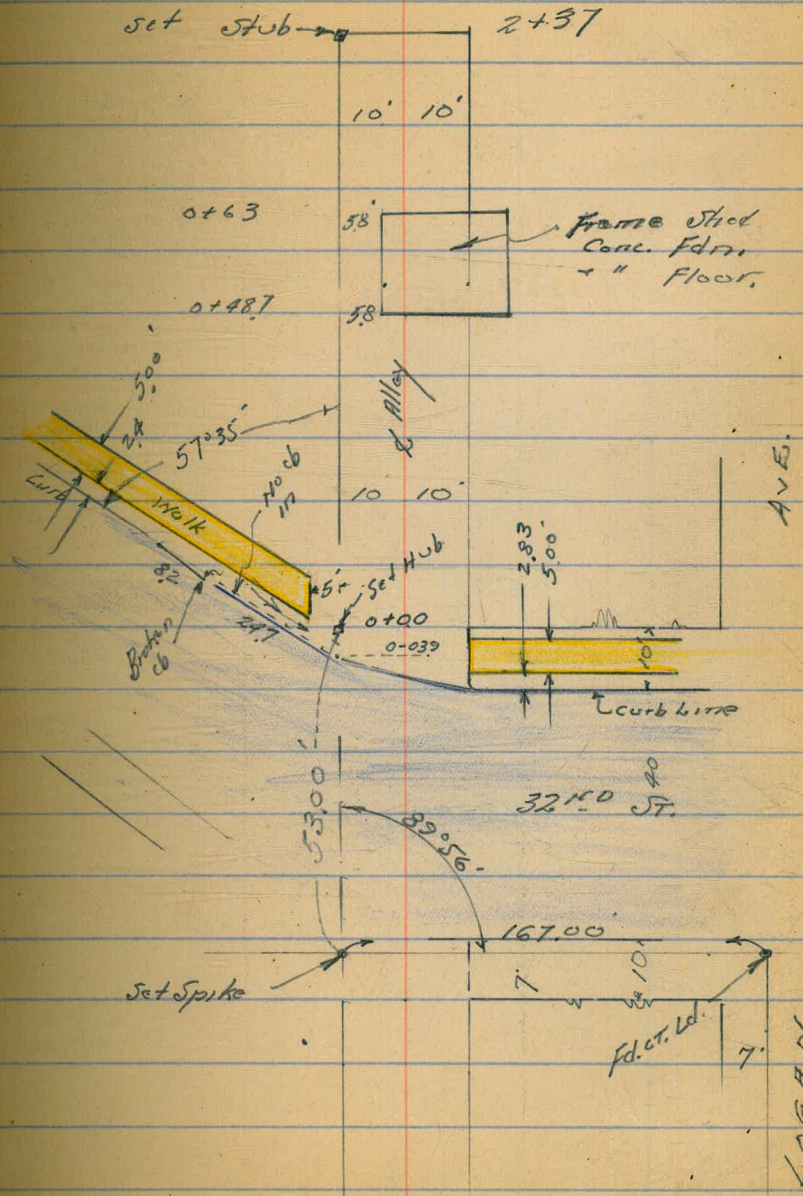
✓

CROSS SECTION ALLEY BLK 285
 Seaman And Choates
 Bet. Logan Ave ^{And Greely}
 from 32ND to East End.

Walker 140 250 20
 Pope
 Hoffman 10-19-51

Orig. Cross Sections FB 1624-69

INDEXED
 Law
 OCT 22 1951



0+32

0+32

0+04

0+00

0-03.9

0-10 = E. cb on Rt.

0-20

TP 12.9 41.46 1178 40.17
 0.88 51.95 51.07

Reduced & Plotted
 10-22-51
 G.S. R. King

Along E cb
 diag. Sec from 10' Lt.

33.2 34.0 39.0 41.8 42.5 43.6 43.6 54
 8.3 7.5 2.5 +0.3 +1.0 +2.1 +2.1
 20 10 6 10 10 10 20

34.36 34.6 35.9 37.1 42.6 42.7 43.0
 7.0 6.9 5.6 4.4 +1.1 +1.2 +1.5
 5 10 5 6 7 10 15
 on Walk

34.45 35.3 37.11
 7.01 6.0 4.35
 10 10
 on cb

31.52 32.24 32.07 32.44 33.64 34.15
 994 922 939 902 782 731
 329 329 347 247 161 10
 Gut. cb

34.03 34.71 35.41 36.89 36.35 37.08 38.24
 7.43 6.75 6.05 4.57 5.11 3.78 2.72
 20 10 10 10 10 326 326
 P.V. P.V. P.V. cb Gut Gut cb

34.39 35.20 36.05 36.91 37.84
 7.07 6.26 5.41 4.55 3.62
 20 10 10 10 20
 P.V. P.V. P.V. P.V. P.V.

41.46

B.M. N.W.B.R. Logon # 32 NO FB 1624
 69

2+15

2+00

1+97 = 2 Elec Pole #PF 322X 8.8' Rft

1+50

1+00

PR 3210 92' R1 = 2 Elec. Pole

0+63

0+40

TP 4.88 44.63 171 39.75

41.46

Lt.

2

Rft

55

32.9	36.6	39.1	39.1	39.6
11.7	8.0	5.5	5.5	5.0
23	10		10	20
Edge Bluff				

32.8	38.2	40.9	41.5	41.8
10.8	6.4	3.7	3.1	2.8
24	10		10	20
Edge Bluff				

32.9	36.0	39.3	40.3	41.5	42.3
12.2	6.6	5.3	4.3	3.1	1.3
40	29	16	10	10	25
Edge Bluff					

32.9	38.1	39.3	40.5	41.9	42.7	42.8	
11.7	9.1	6.5	5.3	4.1	3.7	1.9	0.8
43	22	18	10		10	12	20

40.75
3.88
Flout.

35.1	40.2	41.5	42.0	45.6	46.6
9.5	4.4	3.1	2.6	+1.0	+2.0
20	17	10		10	20

44.63

41.46

Alley 81k 285 - Seamus Chouter
Had

Lt.

L

Rt

56

FB 1624-71
 Chk Grd. 2+37 10'4 44 29.3 ✓

2+67

	19.0	17.3	20.9	21.4	21.9	22.8	24.4
20.7	16.4	12.8	12.3	11.8	9.9	9.3	
40 in dirt Road	14	13	10	0	10	20	

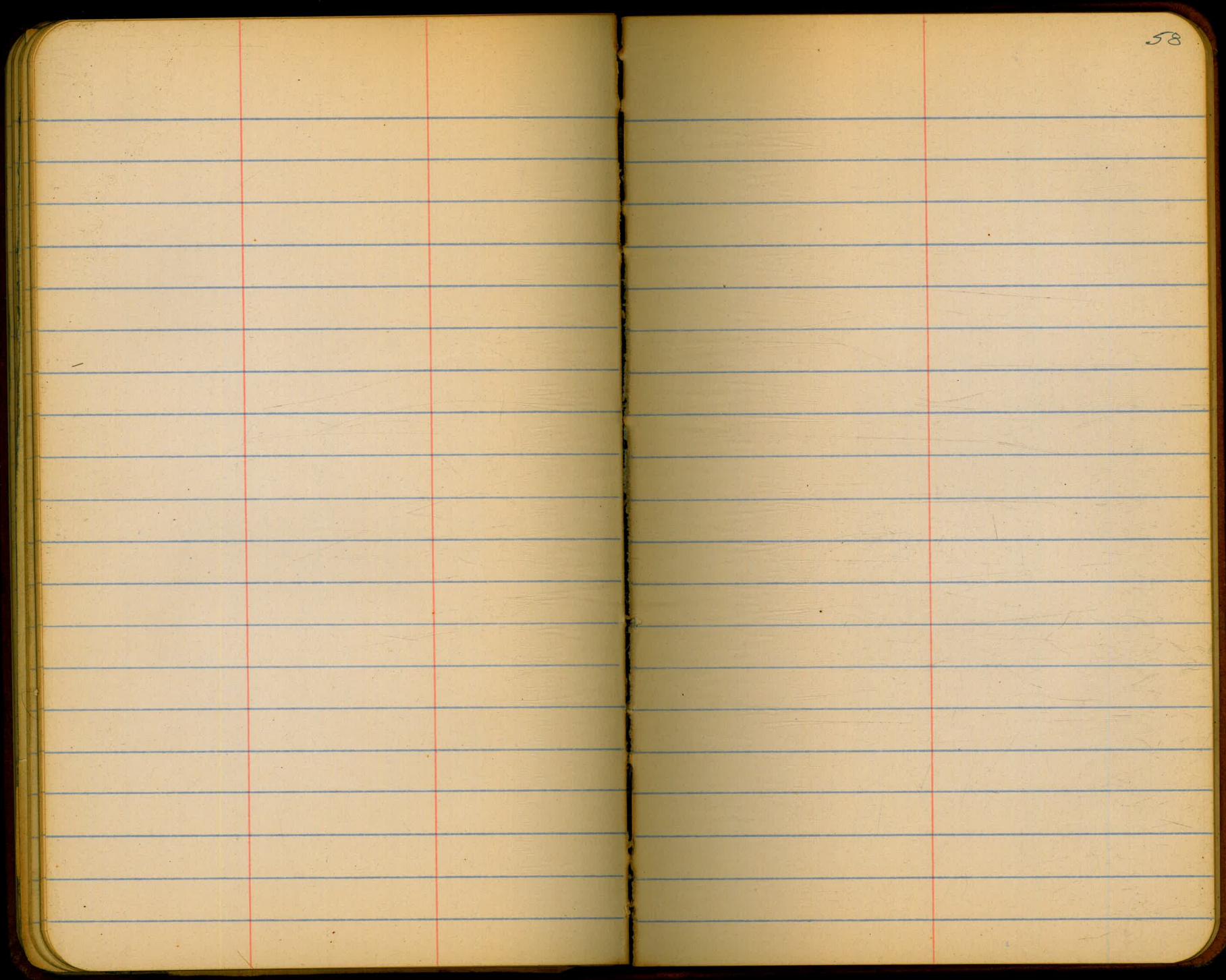
2+37 - End Alley

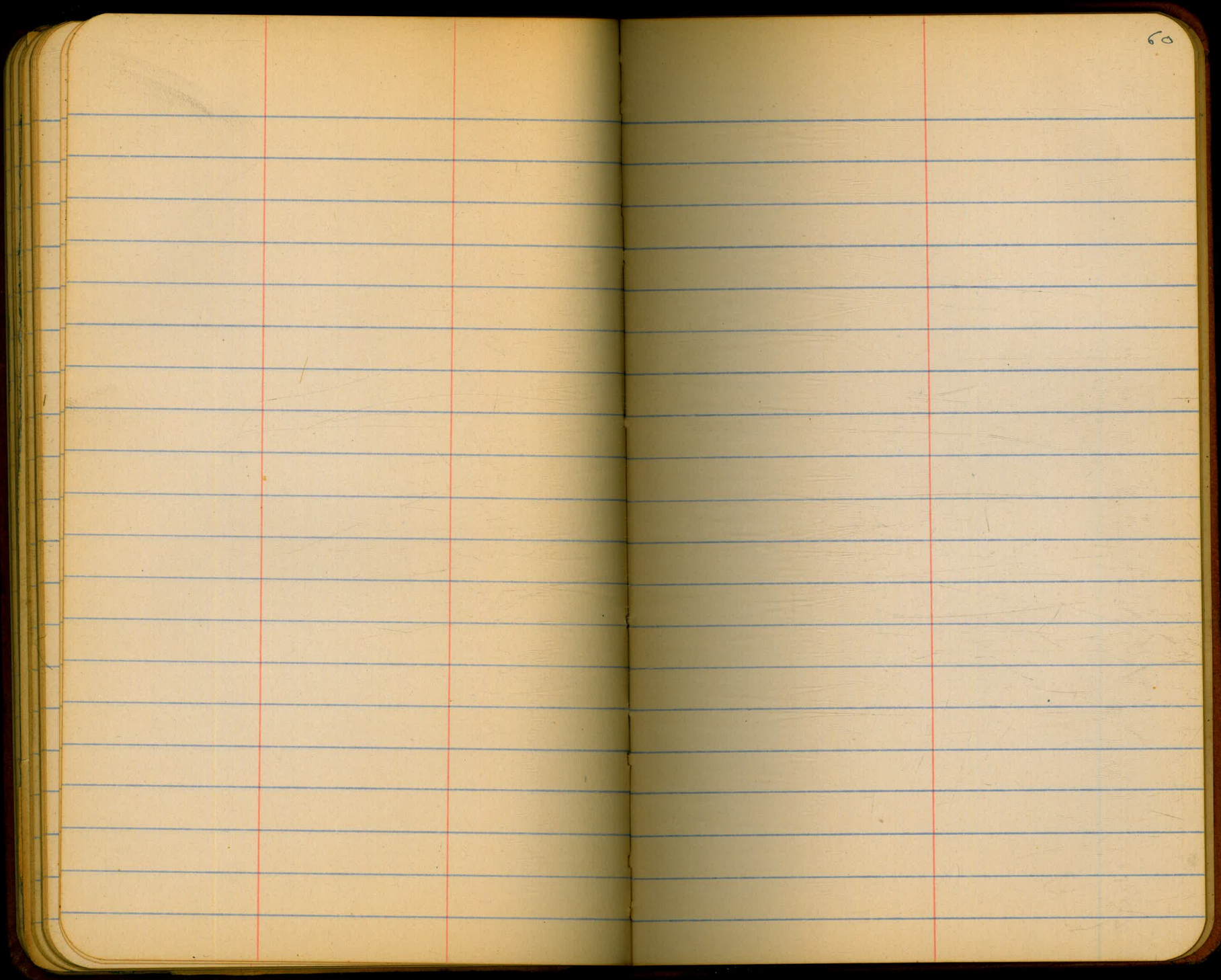
17.1	31.4	28.3	29.27	31.3	32.0	34.4
16.6	123	5.4	4.44	2.4	0.7	+0.7
40 Dirt Road	22	15	10 on stub		10	20

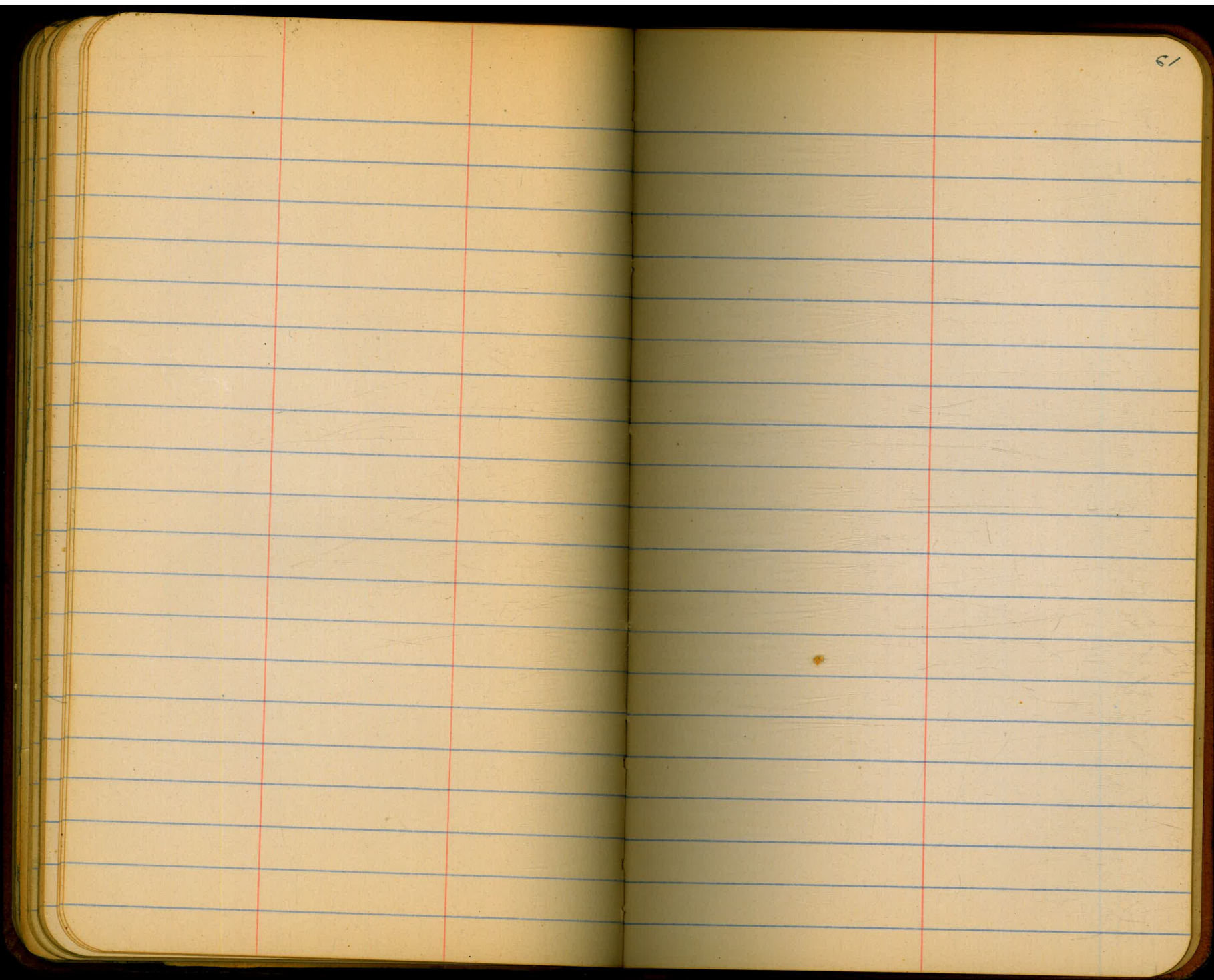
T.P. 166 33.71 12.58 32.05

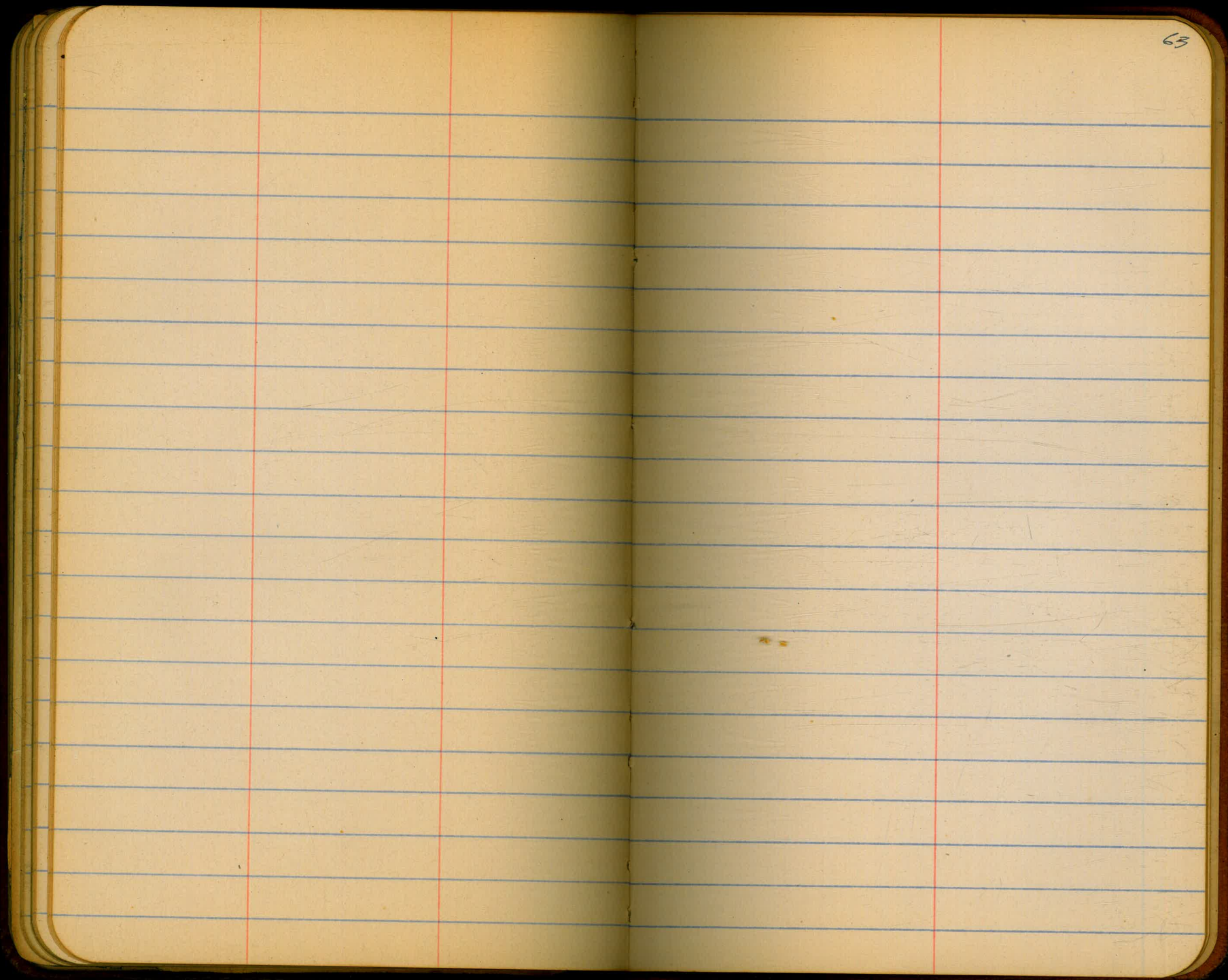
33.71

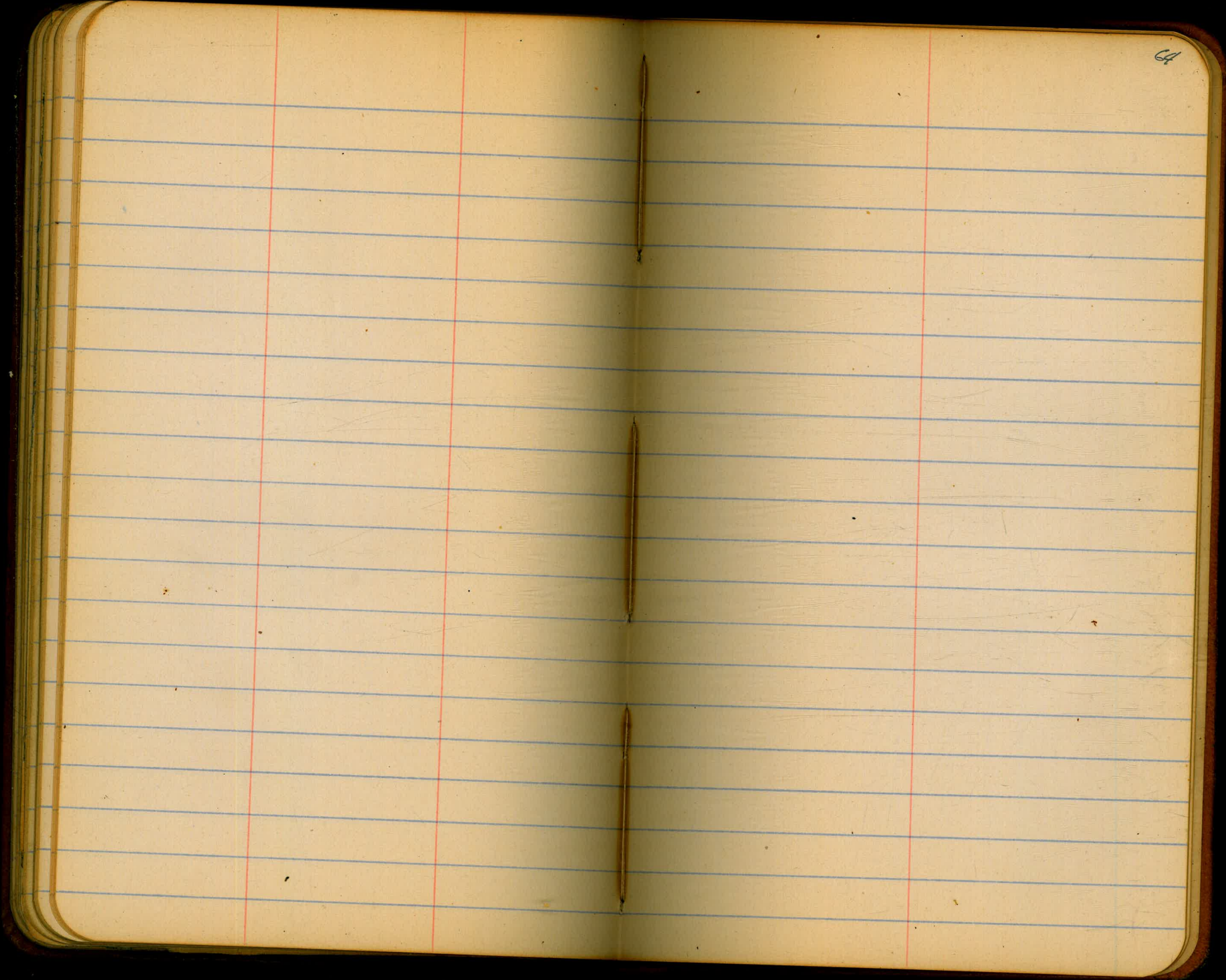
44.63

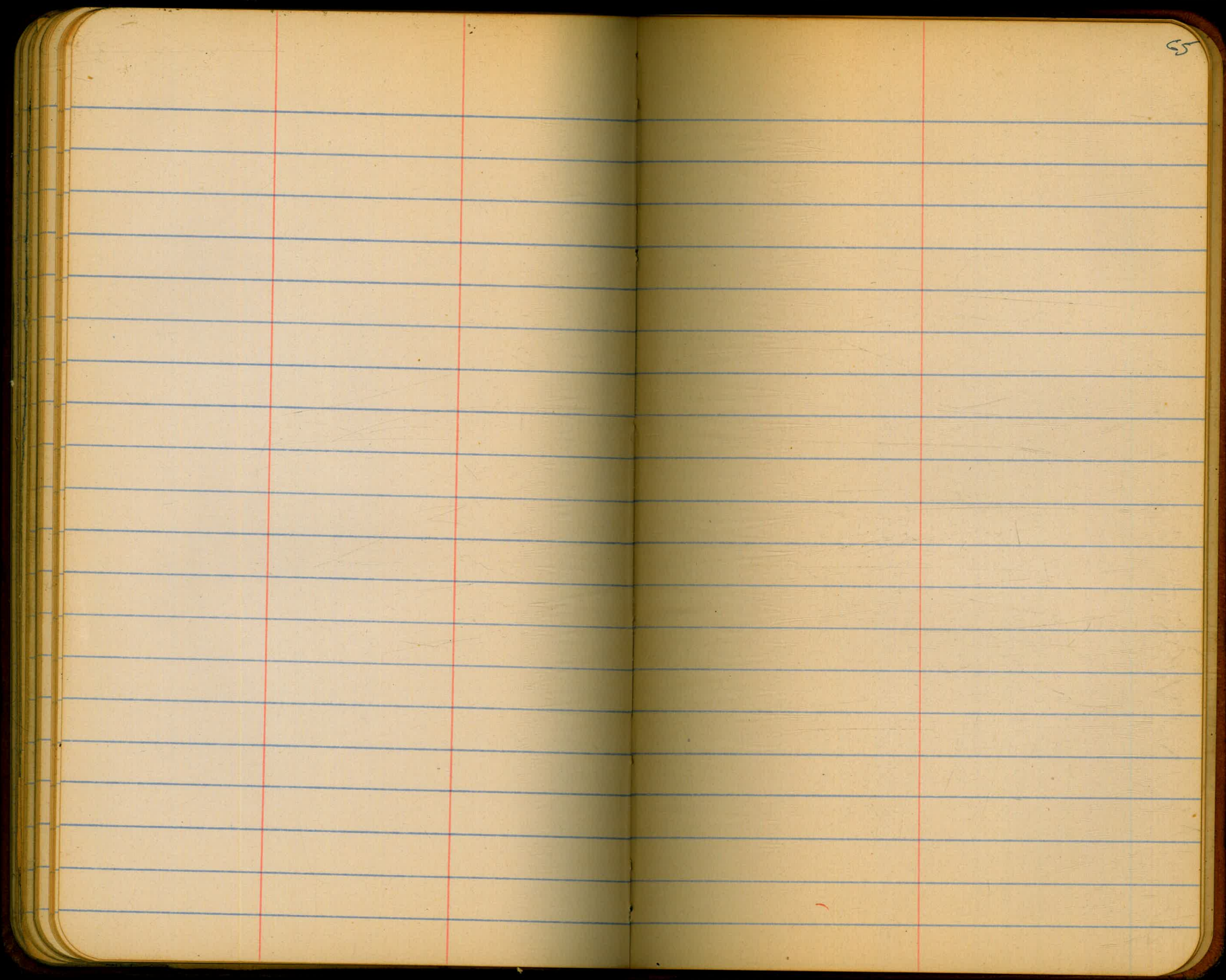




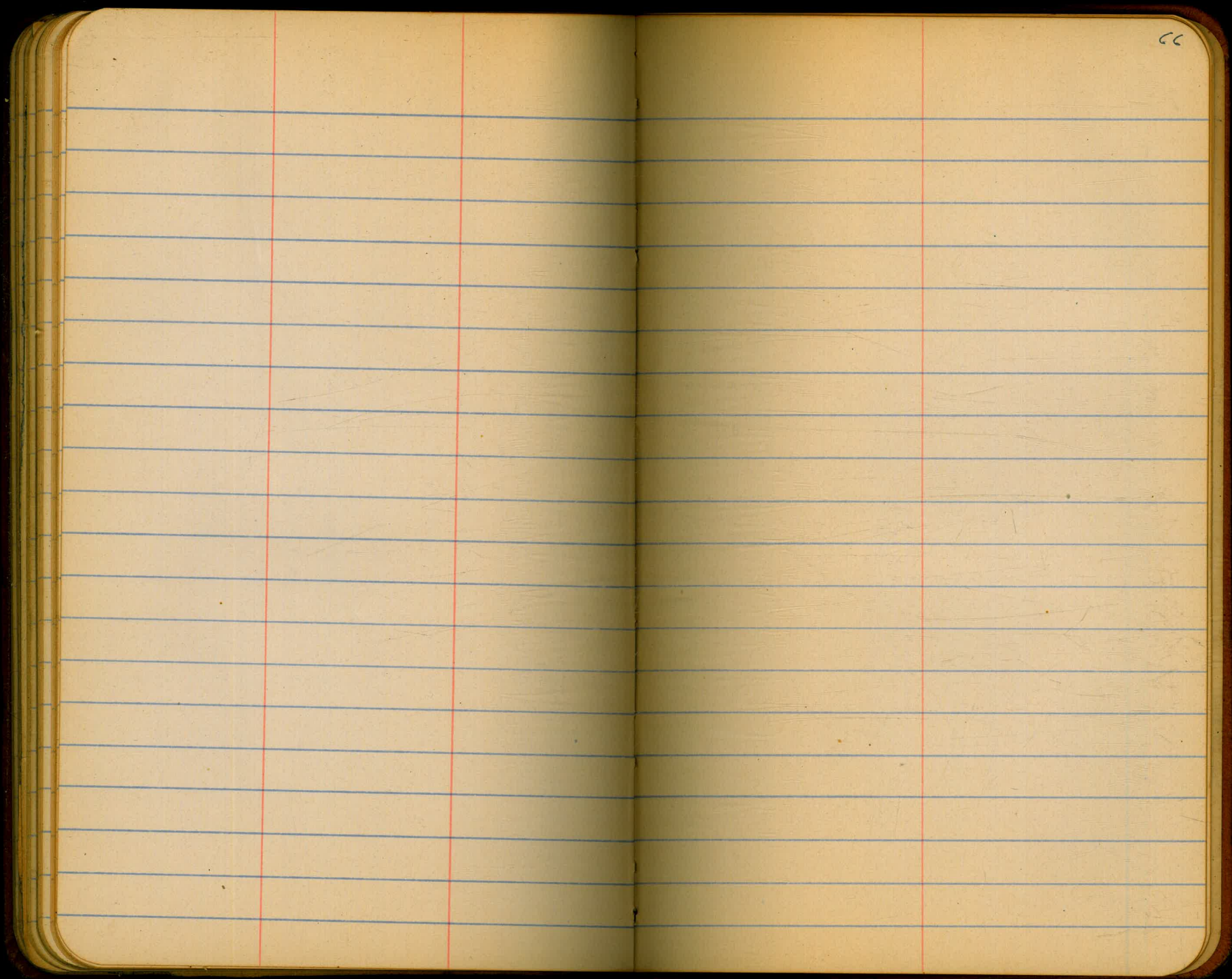




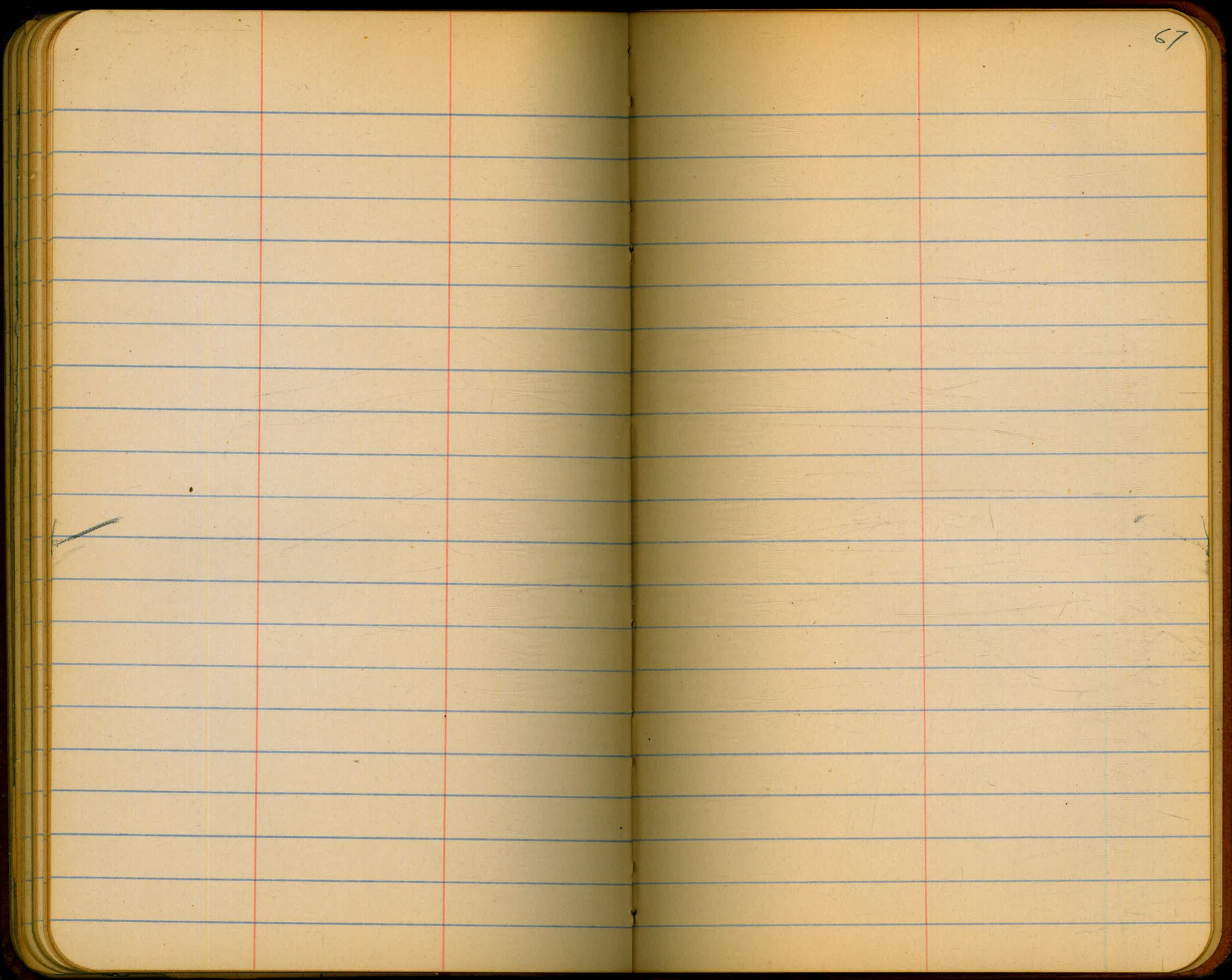




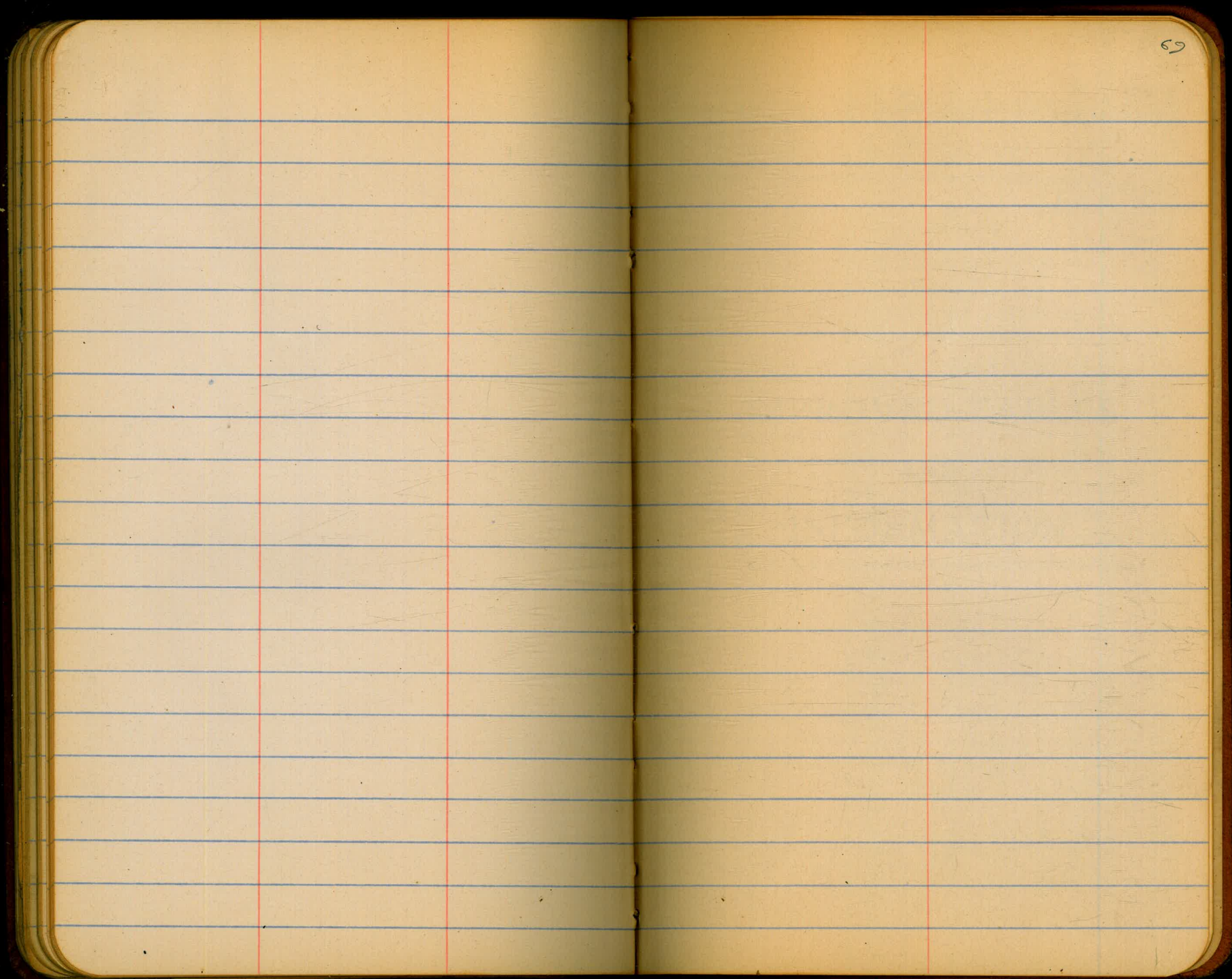
5



22



58



69

Inverlev. 8.46 lower than Gregory's levels

413.98
8.46
405.52

DIRECTIONS FOR USE OF TABLES

411.22 413.72
8.46 8.46
402.68 405.18

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

IMPROVED TABLES
AND
INFORMATION

necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

21+67.

$$\begin{array}{r} +5 \\ -51 \\ \hline 155 \end{array}$$

+40

$$\begin{array}{r} 46 \\ \hline 00 \end{array}$$

$$\begin{array}{r} 00 \\ \hline 8 \end{array}$$

57°35'