

DULZURA TO UPPER OTAY

PIPE LINE

1025

THE FIELD BOOK

BY

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.

NEW YORK.
CHICAGO. SAN FRANCISCO. ST. LOUIS.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION

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	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

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Levels of Pipe line from Upper Otay Dam
to Harvey diverting dam on Dulzura
Creek Sta 0 - 134

P.P.s 2-24

All trestles on above line, pps 25-29.

Trestles, 1, 2, 3 + 4 (all)

List of grade changes from original
profile page 30

70

Correct

Numerator = Rod from same H.I as Station
Denominator = Distance out from R.
New Grade Old Grade

	7.27	496.36		489.09	486.09
B.M. #1			4.02	492.34	489.34
0			0.1	96.3	93.3
+10			1.0	95.4	92.4
+12			2.2	94.2	91.2
	1.09	484.71	12.74	483.62	
1			6.2	78.5	75.5
	1.25	473.13	12.83	471.88	
+85			4.5	68.6	65.6
2			5.7	67.4	64.4
+73			11.1	62.0	59.0
	2.06	462.96	12.23	460.90	
+83			8.3	54.7	51.7
3	Creek		9.8	53.2	50.2
+25			6.7	56.3	53.3
+35			6.5	56.5	53.5
+36			4.8	58.2	55.2
+50					
+75			6.0	57.0	54.0
4			5.1	57.9	54.9

= Peg 40 Lt. Sta 21+70
 = Peg 35 Rt. Sta 0+40
 493.30 x 493.30

Begin 3-11-16 1 P.M.

475.00 x 475.00 $\frac{74}{10}$ $\frac{48}{10}$

464.00 x 464.00 $\frac{58}{10}$ $\frac{60}{10}$

457.33 $\frac{98}{10}$ $\frac{98}{10}$

455.00 x 455.00

454.92 454.87 $\frac{56}{10}$ $\frac{53}{10}$
 454.75 451.0 x $\frac{56}{10}$ 538.09

11.67

37.80
 11.67

 26.13

No change of grade
 0+00 - 3+35

		462.96		Correct	New Grade	Old Grade	L	R	Old Cut	New Cut
4 +50										
5			48	458.2	455.2	454.57	450.5	47	0.42	+0.1
						454.40	450.0 x	10	0.78	-0.1
+40			56	57.4	53.4	454.22				
+50										
6			61	56.9	53.9	454.05	450.0	57	0.97	-0.5
								10		1.0
7			58	57.2	54.2	453.70	450.0	56		0.6
								10		1.0
8			65	56.5	53.5	453.35	450.0	63		0.5
+50								10		1.0
	4.72	461.33	635	456.61		453.17 x				
9			48	56.5	53.5	454.5	450.0 x	46		0.9
+50						453.00 x	450.0 x	10		1.0
+55			0.1	61.2	58.2	453.4	453.0 x			
+60										
	12.36	473.26	0.43	460.90		458.00 x				
10			5.1	68.2	65.2	462.0 x	457.9	47		0.5
						465.5	450.0 x	10		1.0
#										
B.M 2			2.27	470.99	467.99					
+25			1.1	71.9	68.9					
+35 x										
	12.31	484.96	0.61	472.65		470.00 x				0.2
+40			11.6	73.4	70.4	470 x				
+50						470.0				
+75			2.6	82.4	79.4	478.0 x				
	13.30	497.28	0.98	483.98						
11			9.0	87.3	84.3	483.45	480.0	88		0.7
						484.54		10		1.0
+30						490.00 x				
	8.88	505.30	0.86	496.42						
+50										
	51.57		9.23	505.30		493.00 x	490.0 x			
	7.23			462.96						
	42.34			42.34						

	505.30		Correct	NEW GRADE	Old R.	L.		
11+65		69	498.4	495.4 ^v				
+75								
12		50	500.3	497.3 ^v	495.5 ^x 497.5 ^x 496.67 ^x 498.00 ^x	494.0 ^x $\frac{40}{10}$	$\frac{52}{10}$	C 3.8 0.0 0.0 ^v
+30		35	0.18	0.18 ^v				
+50								
13		3.1	0.22	0.22 ^v	498.05 498.16	495.0 ^x 495.0 ^x	$\frac{26}{10}$ $\frac{42}{10}$	C 3.1 C 3.2 ^u -0.3 +0.0 ^u
+5.0		3.5	0.18	0.18 ^v	498.27	495.0 ^x	$\frac{25}{10}$ $\frac{47}{10}$	C 2.7 ^u -0.6 ^u
14		4.2	0.1.1	0.1.1 ^v	498.38 498.49	495.0 ^x	$\frac{35}{10}$ $\frac{50}{10}$	C 2.6 ^u -0.8 ^u
15		2.5	0.2.8	0.2.8 ^v	498.60	495.0 ^x	$\frac{15}{10}$ $\frac{33}{10}$	C 4.0 ^u C 4.2 ^u +0.5 ^u +0.6 ^u
	11.28	513.30	3.28	502.02				C 3.4 -0.3
16		11.2	0.2.1	0.2.1 ^v	498.82	495.0 ^x	$\frac{10.1}{10}$ $\frac{123}{10}$	C 3.4 ^u -0.7 ^u
+5.0		12.3	0.1.0	0.1.0 ^v	498.93	495.0 ^x		C 3.3 -0.6
+6.0		11.1	0.2.2	0.2.2 ^v	499.0 ^x			
+8.0		11.6	0.1.7	0.1.7 ^v				
+8.5					499.5 ^x			
17		10.2	0.3.1	500.1 ^v	499.9 ^x 500.5 ^x	496.0 ^x	$\frac{10.6}{10}$ $\frac{26}{10}$	C 5.0 ^u +1.1 ^u
+1.0								
+1.3								
+2.4 ^u								
+2.5								
+5.0								
55		6.2	0.7.1	0.4.1 ^v	502.9	500.0 ^x		C 4.4 +1.5 ^v
+5.5								
18		4.2	0.9.1	0.6.1 ^v	505.0 ^x 505.4 ^x	502.0 ^x	$\frac{42}{10}$ $\frac{51}{5}$ $\frac{52}{6}$	C 3.9 ^u +0.5 ^u
+5.0					507.0 ^x	503.0 ^x	$\frac{22}{5}$ $\frac{24}{10}$	C 3.9 ^u +0.1 ^u
19		2.4	1.0.9	0.7.3 ^v	506.33 ^x 506.33	504.0 ^x	$\frac{30}{10}$	C 3.9 +0.9 ^u
+5.0								
	11.28	513.30	3.28	505.30				C 3.4 +0.2 ^u
	3.28			505.30				
	8.00			8.00				

✓ 8.00

✓ 8.00

10.2 Bottom pipe
(500.1 Elev. Bottom)

31 52 48 (Road)
5 6 10
22 24
5 10 Road

517.85

Correct

New Grade Old Grade

Lt.

23+85

8.2 503.7 506.7

~~505.22~~ 502.65

+1.1

24

76 510.3 073

~~502.31~~ 502.0 x 10 ³⁰

$\frac{72}{3}$ $\frac{119}{6}$ $\frac{113}{10}$ R

+4.6
+1.8

+15

87 092 062

~~505.00~~ 504.0 x

+50

+65

73 106 076

+90

52 127 097

25

52 127 109.7

~~506.6~~ 505.0 x $\frac{55}{10}$

$\frac{50}{5}$ $\frac{70}{7}$ $\frac{68}{10}$ R

+2.1
+2.5

+25

+50

+65

62 117 087

~~508.0~~ 505.0
507.36

+2.6
+0.2

25+15

26

55 124 094

~~505.0~~ 505.0 $\frac{55}{10}$

$\frac{54}{1}$ $\frac{34}{5}$ $\frac{33}{10}$ R

+0
+1.2

+50

+65

32 147 117

509.3 x 508.0
511.40 x

+1.0
+0.2

679

524.86

0.28 517.57

+85

63 18.1 15.1

27

64 18.0 19.0

514.0
514.15 511.0 $\frac{60}{10}$

$\frac{62}{10}$ R ⁴⁵ +5.2
+2.1

+40

27+50

+75

+80

43 20.1 17.1

516.8 x 514.0 x

+4.8
+7.0

28

08 23.6 20.6

~~517.00~~ x 516.0 x $\frac{09}{10}$

$\frac{13}{3}$ $\frac{49}{7}$ $\frac{37}{10}$ R ⁴⁶

+0.8
+1.2

+10

+30

+50

+75

10 23.4 20.4

518.75 x 515.0 x

+1.0
+0.4

28 21.5 18.5

679

524.36

0.28

28

517.85

√651

√651

	12	13	Correct	New Grade	Old Grade	Rt	Lt	8
38+50	516.57							
38+65		54	511.2	5082	507.0	502.0		+4.2
39		7.5	09.1	06.1	504.0	502.0	$\frac{7.5}{10}$	$\frac{6.5}{6}$ $\frac{6.4}{10}$ +4.2
+30		10.1	06.6	03.6				
+50		103	06.4	034	498.0	497.34	$\frac{12.0}{3}$ $\frac{12.9}{3}$	$\frac{7.5}{7}$ $\frac{7.0}{10}$ +4.6
+65						495.0		+4.2
+70		125	04.1	5011				
+80		162	00.4	4974				
+75					496.5			
+85		152	01.4	984				
+95								
40+00		145	02.1	499.1	496.5	495.0	$\frac{10.9}{10}$	$\frac{13.5}{7}$ $\frac{11.5}{10}$ +3.0
+25					498.0			$\frac{11.5}{10}$ +2.8
+50		128	03.8	5008		497.4	$\frac{13.1}{10}$	
Top of Deck of cattle pass		7.2	09.4	604				Sta 39+80 ±
B.M #5		9.48	509.03	504.03				Req 50 Lt sta 40+30. (beside angle post)
+65					501.0			
+85		11.1	05.5	025				
41		8.7	07.9	04.9	503.8	499.8	$\frac{10.2}{10}$	$\frac{7.2}{5}$ $\frac{6.2}{10}$ +2.8 -0.7
+45		8.0	08.6	05.6				
+50					507.0	502.2		+4.7 +0.9
+80		39	12.7	09.7				
42		4.7	11.9	08.9	509.00	504.6	$\frac{5.2}{10}$	$\frac{3.9}{5}$ $\frac{3.5}{10}$ +3.4 -0.8
+30	11.99	524.00	458	512.01				
+50			9.5	145	115			+2.9 -0.1
	11.99 456 √7.43	524.00 16.57 √7.43				510.00		502.0

	524.00		Correct	New Grade	Old Grade	R	L4	9
43			10.5	513.5	510.5	123 511.0 511.70x 512.50 515.00	75 7	71 10 R +2.8 +0.0
+35								
+50								
4			6.0	18.0	15.0	82 509.6 512.2	30 7	31 10 R +1.9 +1.0 -1.0 -1.8
+50			0.52	520.48	520.48	517.50 514.8		+0.6 -2.1 End 3-11-16 4 R
	1053	531.01		520.48				
45			2.0	21.1		123 520.00 522.50	04 5	06 10 R +2.8 -0.4
+50								
46			5.0	25.1		525.00x 526.50x 526.5 526.50	54 5	53 10 R +2.8 -1.5
+50								
4			4.0	27.0		526.50x 526.57 526.64	40 3	24 7 10 R +2.8 +3.7 -0.9 -2.6
+50								
8			3.7	27.3		526.67 526.64	30 3	00 8 10 R +2.8 +3.1 -2.8 -0.9
	1280	541.62	2.25	528.76	526.71	525.0 526.71		+1.9 -0.1
			1.00	31.6		526.78 526.85	84 5	63 10 8.46 +2.1 +2.1
+50								
+75								
56			2.0	38.7		526.92 526.92	28 5	15 6 10 R +2.8 +7.6 +10.2 +11.5 +9.8 +9.8
+25								
+50			0.4	41.2		x527.00 527.0	02 10	02 10 R +14.2 +14.2 +13.1 +13.1
+75	4.32	545.12	0.82	540.80				
B.M. # 6			2.26	542.30		526.92		
51			5.0	39.8		526.92 526.85	53 10	53 10 R +12.5 +12.5 +11.1 +11.1
+25								
+50			8.1	37.0		526.85 527.0	73 3	69 7 10 R +11.1 +9.6 +9.6
+75			2.4	36.7				+9.1 +9.1
2			0.7	35.7		526.78 526.71	10 10	8 5 10 R +7.7 +7.7 +5.7
+50	27.71 3.07	545.12 520.48	3.07					
	24.64	545.12 520.48						

545.12

53			13.2	531.9
+150				
	334	535.82	12.64	532.48
54			5.7	30.1
+20				
54 +25			8.5	27.5
+50				
55			10.6	25.2
+50				
	906	524.90	10.98	524.84
56			20	220
6+140				
+50			26	22.3
+85				
			44	20.5
57			36	21.3
+40				
+50			61	18.8
+75				
			55	19.1
8			71	17.8
+20				
+45			67	18.2
+50				
+61.5 2.0			6.3	18.6
			74	17.5
9			78	17.1
+40				
+50			85	16.4
+80				
	346	4512	2362	
		2490	540	
		2072	422	

New Grade Old Grade

Rt.

Lt.

526.64	5220 x	$\frac{140}{10}$	$\frac{17}{9}$	$\frac{11}{7}$	$\frac{11}{10}$	+4.3
526.57	526.00					+3.0
526.5	525.00 x	$\frac{70}{10}$	$\frac{52}{4}$	$\frac{43}{6}$	$\frac{43}{10}$	+1.7
526.80	524.20	$\frac{113}{10}$	$\frac{9}{14}$	$\frac{8}{8}$	$\frac{7}{10}$	-0.8
x 526.20	523.40	$\frac{10}{10}$				-0.8
x 525.10	521.80					-1.1
x 523.80	520.20					-0.4
522.16	518.60	$\frac{40}{10}$	$\frac{0.4}{7}$	$\frac{0.4}{10}$	R	-1.0
	517.0 x					+0.1
		$\frac{50}{10}$	$\frac{7}{10}$	$\frac{28}{10}$		-0.1
						-2.1
						-1.0
						-0.2
						-1.2
						-1.9

524.90

~~see page 33~~

Rt.

Lt.

60

10.3 514.6

x 513.6

$\frac{126}{10}$

$\frac{85}{5}$ $\frac{86}{10}$ R

-1.7
-2.1

B.M.# 7

4.25 520.65

B.M. Peg 30 Lt Sta 60

424 517.53 11.61 513.29

+50

~~513.00 x~~

$\frac{80}{10}$ $\frac{55}{5}$

$\frac{28}{6}$ $\frac{27}{10}$ R

60+58 74.2 T

4.5 13.0

~~510.4 x~~

$\frac{97}{10}$ $\frac{75}{5}$

$\frac{46}{3}$ $\frac{40}{10}$ R

+60

1

5.8 11.7

~~506.8~~

~~507.0 x~~

~~504.9~~

+20

+30

8.2 09.3

♀

+40

+80

bottom 24" pipe

9.0 08.5



~~504.0~~

~~504.0 x~~

+80

of Ditch

11.8 05.7

2

7.1 10.4

$\frac{126}{10}$ $\frac{115}{7}$

$\frac{40}{5}$ $\frac{45}{10}$ R

3

6.9 10.6

$\frac{105}{10}$

$\frac{60}{6}$ $\frac{48}{6}$ $\frac{45}{10}$ R

4

10.0 07.5

$\frac{140}{10}$
~~503.0 x~~

$\frac{97}{4}$ $\frac{60}{8}$ $\frac{53}{10}$ R

9.02 515.75 10.86 506.67

+50

8.4 07.4

~~503.0~~

5

7.2 08.6

$\frac{92}{10}$
~~503.0~~

$\frac{66}{3}$ $\frac{47}{7}$ $\frac{43}{10}$ R

+45

abandoned

5.6 10.3

+82

pipe bottom 36"

10.2 05.6



+82

Ditch

11.0 04.8

66

9.3 06.6

3
~~503.0~~

$\frac{152}{10}$

$\frac{52}{5}$ $\frac{48}{10}$

13.52 524.90
515.75
13.32
1.915

22.47
13.32
9.15

	51575	71	508.7
66+50		77	08.1
7		87	07.1
+50		76	08.2
8		72	08.6
+26 ²⁰		83	07.5 ✓
+20	271	557	510.18
+50	51289	43	08.6
+85		38	09.1
9		50	07.9
+50		54	07.5
70		1269	500.20
BM#8		79	05.0
+50		89	04.9
1		89	04.0
+50		98	03.1
2		109	02.0
+50		119	01.0
+74	Pipe bottom (24")	125	00.0
+74	Ditch		

$$\begin{array}{r} 1575 \\ 1289 \\ \hline 286 \end{array}$$

$$\begin{array}{r} 557 \\ 271 \\ \hline 286 \end{array}$$

	503.0		
503.0	$\frac{104}{10}$	$\frac{56}{5}$	$\frac{53}{10}$ R
503.0	$\frac{104}{10}$	$\frac{54}{5}$	$\frac{50}{10}$ R
503.0	$\frac{69}{10}$	$\frac{25}{4}$	$\frac{22}{10}$ R
503.0	$\frac{82}{10}$	$\frac{50}{2}$	$\frac{35}{6}$
503.0	$\frac{114}{10}$	$\frac{40}{10}$	$\frac{46}{10}$ R
503.0	$\frac{131}{10}$	$\frac{412}{10}$	$\frac{66}{10}$ R
497.0			

Spike in Fence Post 40' R to 69+90



51289

70

+50

4

+50

5

+10
+15
+50
+730

6

+50
+10
+25

7

+50
+75

8

+250
+260
+35

+50

9

51289
50738
5.51

1268
717
5.51

95 503.4 502.4

86 04.3 503.0

106 07.3 501.1

7.17 507.38 1268 500.21

61 01.3 500.6

49 02.5 501.5

47 02.7 502.0

67 00.7 500.0

66 00.8 499.8

58 501.6 500.0

90 498.4 97.3

92 98.2 95.5

87 88.7 94.7

112 96.2 92.7

97 97.7 96.7

88 98.6

84 99.0

95 97.9 95.0

R

$\frac{116}{10}$

$\frac{127}{10}$

$\frac{66}{10}$

$\frac{92}{10}$

$\frac{100}{10}$

$\frac{136}{10}$

$\frac{123}{10}$

L

$\frac{77}{4}$

$\frac{102}{2}$

$\frac{27}{5}$

$\frac{58}{3}$

$\frac{82}{2}$

$\frac{60}{7}$

$\frac{82}{5}$

$\frac{74}{10}$

$\frac{78}{2}$

$\frac{27}{10}$

$\frac{30}{6}$

$\frac{58}{7}$

$\frac{62}{10}$

$\frac{80}{10}$

$\frac{76}{10}$

R

$\frac{38}{10}$

$\frac{55}{10}$

R

R

497.0 x

497.0 x

493.0 x

	507.38			offset RT.
	4.41	499.79	1203	495.29
79+50			4.2	95.5 93.5
80			6.2	93.5 91.4
+50			7.8	91.9 89.6
B.M #9			0.31	499.39
1			8.4	91.3
+50 ^o alt			8.6	91.1
+50			9.6	90.1
2			9.9	89.8
+50			10.6	89.1
83			10.6	89.1
	2.37	490.79	11.28	488.42
+50			1.6	89.2
4			2.3	88.8
+50			3.2	87.6
5			5.4	85.4
+07 ³⁵			5.5	85.3
+25			5.0	85.8
	678	507.38	499.39	
		490.79	678	
		√1659	√1659	

	84	56	35	38
	10	2	5	10
Peg	40	40	40	80+50
487.0 x	107	60	56	
	10	4	10	
	11.4	9.5	7.2	7.3
486.0 x	10	2	6	10
	12.2	10.4	8.8	8.7
486.0 x	10	4	7	10
	3.3	1.0	1.1	
	7.0	4	10	
	3.1	1.7	2.3	2.0
	10	6	4	10
	4.8	2.2	3.5	3.5
	10	4	5	10
	7.2	4.5	5.0	4.9
	10	4	5	10
	6.9	4.5	5.3	5.1
	10	4	5	10

490.79

15

85+50		6.6	484.2
+60		6.2	84.6
+75		6.5	84.3
86		8.1	82.7
+25		11.5	79.3
	082	480.39	11.22
+50		7.4	73.0
+60		8.8	71.6
+75		9.3	71.1
+90		10.0	70.4
+91		11.1	69.3
87		10.8	69.6
+02	± Pipe (bottom) (36")	9.8	70.6
+02		11.1	69.3
+06		10.3	70.1
+08		8.6	71.8
+25		6.8	73.0
+33		6.9	73.5

490.79	11.22
480.39	82
✓1040	✓1040

R4

L4

$$\begin{array}{r} 88 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 51 \\ 5 \\ \hline \end{array}$$

$$\begin{array}{r} 58 \\ 8 \\ \hline \end{array}$$

$$\begin{array}{r} 56 \\ 10 \\ \hline \end{array}$$

R

$$\begin{array}{r} 89 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 42 \\ 8 \\ \hline \end{array}$$

$$\begin{array}{r} 47 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 11 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 6 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 150 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 20 \\ 10 \\ \hline \end{array}$$

082 480.39 11.22 479.57

$$\begin{array}{r} 93 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 4 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 97 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 88 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 11 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 108 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 85 \\ 10 \\ \hline \end{array}$$

$$\begin{array}{r} 103 \\ 10 \\ \hline \end{array}$$

	48039		
87+50		40	4764
+60		25	77.9
+75 ^b		19	78.5
+90		18	78.6
8.		0.6	79.8
	1289	493.12	0.16
			480.23
+25		100	82.5
+45 ⁵³		110	82.1
+80		91	84.0
9		92	83.9
+07		90	84.1
+20		69	86.2
+50		46	88.5
+75		51	88.0
+95		30	90.1
90		30	90.1
B.M. #		0.33	492.79
+15		4.9	88.2
	1289	493.12	
	16	80.39	
✓	1273	✓12.73	

R	L
$\frac{38}{10}$	$\frac{38}{10}$
$\frac{10}{10}$	$\frac{15}{10}$
$\frac{10}{10}$	$\frac{10}{10}$
$\frac{116}{10}$	$\frac{102}{10}$
$\frac{115}{10}$	$\frac{109}{10}$
$\frac{9}{10}$	$\frac{81}{10}$
$\frac{33}{10}$	$\frac{33}{5}$
	$\frac{65}{5}$
	$\frac{65}{10}$
	R

Peg 40 Lt sta 90

493.12

R.

L.

30+35

38 489.3

+50

43 88.8

+70

35 89.6

+90

50 88.1

+50

48 88.3

$\frac{45}{4}$

$\frac{46}{10} R$

2

49 88.2

$\frac{40}{10}$

$\frac{24}{3}$ $\frac{25}{10} R$

33 89.8

881

497.74

4.19 488.93

+50

80 89.7

3

62 91.5

$\frac{89}{10}$

$\frac{4}{5}$

$\frac{58}{4}$ $\frac{58}{10} R$

+260

L.

65 91.2

+50

63 91.4

$\frac{85}{10}$

$\frac{8}{5}$

$\frac{42}{4}$ $\frac{52}{10} R$

4

66 91.1

+50

67 91.0

$\frac{85}{10}$

$\frac{42}{4}$ $\frac{47}{10} R$

5

69 90.8

+50

66 91.1

$\frac{93}{10}$

$\frac{48}{5}$ $\frac{45}{10} R$

6

74 90.3

+50

72 90.5

881

4.19

4.67

497.74

493.12

4.62

	497.74		
97		54	492.3
+5.		55	92.2
+75° Δ R		5.1	92.6
98		5.7	92.0
	2.77	497.26	3.25 494.49
+5.		4.3	93.0
9		2.6	94.7
+40		1.7	95.6
+5.		2.0	95.3
100		4.0	93.3
+5.		7.1	90.2
B.M.# 11		3.47	493.79
+75		9.0	88.3
1		10.1	87.2
+39° 26' P.C.		11.2	86.1
+5.		10.8	86.5
+61 Pipe (bottom) 36" pipe		18.7	78.0
275		12.1	85.3
	$\begin{array}{r} 497.74 \\ 497.26 \\ \hline \sqrt{0.48} \end{array}$	$\begin{array}{r} 3.25 \\ 2.77 \\ \hline \sqrt{0.48} \end{array}$	



P.		LT.	
$\frac{86}{10}$		$\frac{35}{8}$ $\frac{36}{10}$ R	
$\frac{60}{10}$		$\frac{40}{3}$ $\frac{34}{7}$ $\frac{33}{10}$ R	
$\frac{41}{10}$		$\frac{24}{5}$ $\frac{32}{8}$ $\frac{32}{10}$ R	
$\frac{50}{10}$		$\frac{40}{2}$ $\frac{57}{4}$ $\frac{55}{10}$	
	Req 35	100 + 50	
$\frac{127}{10}$		$\frac{123}{4}$ $\frac{84}{6}$ $\frac{84}{10}$	
$\frac{102}{10}$		$\frac{90}{4}$ $\frac{88}{10}$	
$\frac{195}{10}$		$\frac{92}{6}$ $\frac{82}{10}$	
$\frac{144}{5}$			

	497.26		
102		1.6	485.7
+25		9.0	88.3
+5.0		8.3	89.6
	6.62	496.70	7.18
3		6.0	90.7
+2.0		6.8	89.9
+5.0		6.0	90.7
4		5.7	91.0
+5		4.9	91.8
+5.0		6.7	90.0
5		6.0	90.7
+5.0		6.0	90.7
+8.0		7.1	89.6
6		6.0	90.7
+5.0		6.2	90.5
7		7.1	89.6
+5.0		6.0	90.7
8		5.0	91.7

497.26	7.18
496.70	6.62
<u>10.56</u>	<u>0.56</u>

$\frac{120}{10}$	$\frac{114}{2}$	$\frac{92}{8}$	$\frac{91}{10} R$
$\frac{100}{10}$		$\frac{86}{10} R$	
$\frac{86}{10}$	$\frac{82}{9}$	$\frac{83}{10} R$	
$\frac{62}{10}$		$\frac{62}{10}$	$\frac{66}{10} R$
$\frac{66}{10}$		$\frac{53}{10} R$	
$\frac{74}{10}$	$\frac{46}{7}$	$\frac{54}{10}$	$\frac{53}{10} R$
$\frac{75}{10}$	$\frac{54}{4}$	$\frac{48}{7}$	$\frac{42}{10} R$
$\frac{74}{10}$		$\frac{44}{10} R$	
$\frac{61}{10}$	$\frac{61}{10}$	$\frac{52}{10}$	
$\frac{60}{10}$	$\frac{46}{5}$	$\frac{46}{10}$	

118

496.70

3.18

495.41

447

492.23

108+50

37

91.7

3

50

90.4

+35

61

89.5

+50

80

87.4

+90 Pipe bottom (12")

128

82.6

+90 Ditch -

137

81.7

+90

157

79.7

110

140

81.4

+50

90

86.4

BM # 12

677

488.64

+80

66

88.8

1

57

89.7

+50

65

88.5

2

69

88.5

+50

81

87.3

3

88

86.6

+50

69

88.5

496.70
495.41

1.29

447
3.18

1.29

R

L

20

$\frac{56}{10}$

$\frac{44}{8}$ $\frac{50}{10}$ R

$\frac{160}{10}$

$\frac{122}{6}$ $\frac{115}{10}$

Pegs to L Sta 110

$\frac{83}{10}$ $\frac{69}{1}$

$\frac{49}{2}$ $\frac{51}{10}$ R

$\frac{95}{16}$ $\frac{75}{2}$

$\frac{50}{2}$ $\frac{47}{10}$ R

$\frac{104}{10}$

$\frac{30}{5}$ $\frac{36}{10}$ R

$\frac{110}{7}$ $\frac{132}{10}$

$\frac{76}{3}$ $\frac{38}{10}$

49541

114			68	488.6
+50			6.2	89.2
105			6.2	89.2
	448	498.86	103	494.38
+50			9.1	89.8
6			9.0	89.9
+50			9.9	89.0
7			10.2	88.7
+50			11.2	87.7
+53	pipe bottom (12")		7.9	91.0
+53	ground		11.1	87.8
8			12.2	86.7
+50			11.5	87.4
9			11.4	87.5
+50			10.2	88.7
120			9.7	89.2
B.M #13			0.78	498.08
+50			7.7	91.2

448
 103
 345

498.86
 49541
 3.45

R

L

$\frac{102}{10}$		$\frac{11}{10}$ R
$\frac{105}{10}$		$\frac{12}{8}$ $\frac{11}{10}$ R
$\frac{140}{10}$	$\frac{118}{4}$	$\frac{42}{7}$ $\frac{46}{10}$ R
$\frac{150}{10}$	$\frac{121}{3}$	$\frac{51}{8}$ $\frac{49}{10}$ R
$\frac{160}{10}$		$\frac{55}{10}$
$\frac{142}{10}$		$\frac{42}{10}$
$\frac{132}{10}$		$\frac{31}{10}$



Peg 90 Lt sta 120 on bank road.

4

2

$$\frac{30}{10}$$

$$\frac{118}{10}$$

$$\frac{32}{4}$$

$$\frac{117}{10}$$

$$\frac{20}{7}$$

$$\frac{120}{10}$$

$$\frac{108}{10}$$

$$\frac{107}{10}$$

$$\frac{26}{10}$$

$$\frac{122}{10}$$

$$\frac{43}{10}$$

$$\frac{110}{10}$$

$$\frac{23}{10}$$

$$\frac{102}{10}$$

498.86

121

6.0 492.9

2.52 498.44 9.94 488.52

+5.0 54 93.0

2 62 92.2

+0.5 Pipe bottom (12") 7.0 91.4



+0.5 Ground 10.6 87.8

+5.0 6.0 92.4

3 64 92.0

+5.0 6.0 92.4

4 6.0 92.4

+5.0 7.0 91.4

5 8.5 89.9

+5.0 9.8 88.6

6 7.7 90.7

+5.0 7.8 90.6

7 6.9 91.5

8.36 500.71 6.09 492.35

+5.0 8.7 92.0

$$\begin{array}{r} 17.88 \\ 16.03 \\ \hline 1.85 \end{array}$$

$$\begin{array}{r} 500.71 \\ 498.86 \\ \hline 1.85 \end{array}$$

16.03

	500.71		
128		8.5	492.2
+30		8.7	92.0
+50		9.2	91.5
+77 ⁸³		10.0	90.7
9		9.6	91.1
+50		8.3	92.0
130		7.0	93.7
B.M. #14		4.25	496.46
+50		8.8	91.9
+940 P.O.T		9.2	91.5
1		9.5	91.2
+29 ⁹³ PC		10.6	90.1
+50		12.8	87.9
	278	491.07	1242
+90		10.4	80.7
2		10.0	81.1
+35		9.2	81.9
+37		10.5	80.6
	278	500.71	1242
		491.07	278
		√ 9.64	√ 9.64

Rt

Lt

$\frac{10.7}{10}$	$\frac{7.6}{2}$	$\frac{4.3}{10}$
$\frac{12.5}{10}$	$\frac{7.8}{7}$	$\frac{5.4}{10}$
$\frac{12.8}{10}$	$\frac{6.5}{4}$	$\frac{7.4}{8}$
	$\frac{7.5}{10}$	$\frac{7.5}{10}$

Peg 35 Lt station (on Lt bank road)

$\frac{13.2}{10}$	$\frac{8.0}{3}$	$\frac{8.7}{6}$	$\frac{10.4}{9}$	$\frac{10.4}{10}$
-------------------	-----------------	-----------------	------------------	-------------------

$\frac{10.6}{10}$	$\frac{9.8}{1}$	$\frac{4.2}{9}$	$\frac{4.2}{10}$
-------------------	-----------------	-----------------	------------------

491.07

132+75

11.1

480.0

3

9.6

81.5

±

+06 Pipe bottom 36"

10.8

80.3



+06 Ground 36"

11.0

80.1

+05

7.3

83.8

+12

10.2

80.9

+50

7.1

84.1

+75

3.6

87.5

4

2.6

88.5

261 488.46

±

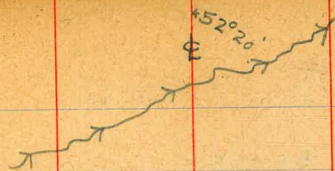
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B

L

24

Trestle #1	463.10	Elev	Grade		
Bent "A" Sta 2+71 ⁰⁰					
⊥ Ground.	3.8	459.8			
Ref. Hub	3.24	459.86	459.98	C ₀ ⁴⁸	C ₀ ^{1-5³/₄"}
Bent "B" Sta 2+86 ⁰⁰					
⊥ Ground.	11.4	451.7			
Ref. Hub	11.33	451.77	458.38	F ₀ ⁶⁰	F ₀ ^{6'-7³/₈"}
Bent "C" Sta 3+02 ⁰⁰					
⊥ Ground.	11.9	451.2			
Ref. Hub	12.31	450.79	457.37	F ₀ ^{6⁵⁸}	F ₀ ^{6'-7"}
Bent "D" Sta 3+17 ⁰⁰					
⊥ Ground.	10.8	452.3			
Ref. Hub	11.56	451.14	456.26	F ₀ ^{5³²}	F ₀ ^{5'-2⁵/₈"}
Bent "E" Sta 3+33 ⁰⁰					
⊥ Ground.	9.7	453.4			
Ref. Hub	9.77	453.33	455.35	F ₀ ^{2⁰²}	F ₀ ^{2'-00¹/₄"}



* Ref. hub set 3' back on ⊥

* Ref. hub set 3' back on ⊥

* Ref. hub set 3' back on ⊥

* Ref. hub set 3' back on ⊥

* Ref. hub set 3' ahead on ⊥

Transverse sections are
approximately level.

Trestle #2. 475.73 Elev. Grade

Bent "A" 86+48

± Ground

2.2 473.5

Ref. hub at 10' Lt.

476.86 474.0

Bent "B" 86+56

± Ground

3.3 472.4

Ref. hub at 10' Lt.

0.95 474.78 474.0

Bent "C" 86+71.38

± Ground

4.4 471.3

Ref. hub at 10' Lt.

4.14 471.55 474.0

Bent "D" 86+86.76

± Ground

5.0 470.7

Ref. hub at 10' Lt.

4.11 471.62 474.0

Bent "E" 87+02.14

±

6.0 469.7

Ref. hub at 10' Lt.

6.19 469.54 474.0

Bent "F" 87+17.52

± bent located on gravel fill

3.0 472.7

Original Ground

4.5 471.2

Ref. hub at 10' Lt.

4.20 471.53 474.0

Continued

C-2⁸⁶

C-2'10¹/₄"

R.P.

x

10'

o

10'

R.P.

x

C-0⁷⁸

C-0'9³/₈"

R.P.

x

10'

o

10'

R.P.

x

F-2⁴¹

F-2'-5"

R.P.

x

10'

o

10'

R.P.

x

F-2³⁸

F-2'-4¹/₂"

R.P.

x

10'

o

10'

R.P.

x

Line of 36" pipe
centers bet. bents "D" and "E"

±

x

36" pipe

F-4⁴⁶

F-4'-5¹/₂"

R.P.

x

10'

o

10'

R.P.

x

F-2⁴⁷

F-2'5⁵/₈"

R.P.

x

10'

o

10'

R.P.

x

Trestle #2 475.73 Ground Grade

Bent "G" 87+32.20

‡ bent is located on gravel fill 1.3 474.4

Original ground. 3.0 472.7

Ref. hub at 10 Lt. 1.24 473.79 474.0

F₀ 21

F₀' - 2 1/2"

R.P.

x 10'

R.P.

o 10'

x

Trestle is located on curve of 200' radius.
‡ chord of 15.38', so bents center 15.50' on outside.

Transverse sections are approximately
level.

Trestle #11	546.85	Ground	Grade
Bent "A" Sta. 124+50.0			
£ Ground			
Ref. hub	553	541.32	540.0
Bent "B" Sta. 125+65.5			
£ Ground			
Ref. hub	1043	536.42	540.0
Bent "C" Sta. 125+81.0			
£ Ground			
Ref. hub	1324	533.61	540.0
Bent "D" Sta. 125+96.5			
£ Ground			
Ref. hub	1307	533.78	540.0
Bent "E" Sta. 126+12.0			
£ Ground			
Ref. hub	535	541.50	540.0

C122	C1'-3 3/4"	+6.0 10	x Ref. hub set's back on £ £ as 0.0 -5.8 7 -10.0 10
F358	F3'-7"	+7.2 10	x Ref. hub set's back on £ £ as 0.0 -5.5 8 -6.5 10
F639	F6'-4 5/8"	+7.7 10	x Ref. hub set's back on £ £ as 0.0 -6.3 10
F622	F6'-2 5/8"		x Ref. hub set's back on £ £ as 0.0
C15	C1'-6"		x Ref. hub set's ahead on £

Transverse slope of Bents "A" and "E"
approx. level, others as shown on
opposite page.

Trestle # 3 545.03

Bent "A" 200+97.6
201+22.5

Ref. hub 4.77 540.26 540.0

Bent "B" 201+07.5

Ref. hub 9.09 535.94 540.0

Bent "C" 201+23.0

Ref. hub 10.99 534.04 540.0

Bent "D" 201+30.7
201+38.5

Ref. hub 5.44 532.59 540.0

C026 C0'-03"

F406 F4'-00³/₄"

F596 F5'-11¹/₂"

F041 F0'-4⁷/₈"

x Ref. hub set 3' back on

x Ref. hub set 3' back on

W.W. about 10' wide

x Ref. hub set 3' back on

x Ref. hub set 3' ahead on

Transverse sections are
approximately level.

Changes made from profile Grade.

101+50 485.0 to 483.0

110+00 485.0 to 482.0

180+00 530.0 to 526.0

181+00 532.0 to 530.0

changed to get clearance for roadway

184+50 531.3 to 531.0

185+50 530.0 to 526.0

185+75 made 526.0

22+60 extend pipe of road in place of trestle

109+20± extend 12" pipe 15'± in place of trestle.

185+75 - 15' of 12" pipe in place of trestle.

192+55 - 15' of 12" pipe " "

198+31± - 15' of 24" pipe " "

214+10 provision for a drainage area of 70± ft.

519	+			492.79
B.M. #10				
81+00 P.O.T.		495.05	4.9	490.1
+50			6.3	488.7
82			7.9	487.1
		488.39		
+50			3.1	485.3
83			4.2	484.2
+50			6.7	482.2
		488.39		
84			7.7	480.7
+33			13.2	475.2
+50	518	473.00	5.3	467.82
+57			11.2	461.8
+60			11.7	461.3
+64			11.2	461.8
85			9.5	463.5
+50			7.1	465.9
T.P.	00	480.57	12.40	480.57
86			11.6	469.0
+50			8.0	472.6
87			5.9	474.7
+50			3.3	477.3
88		492.97	13.0	480.0
+50			10.4	482.6
89+00			9.5	482.5
+25			7.6	484.4
+50			7.6	484.4

Sta		Elev.
90	49+17	5.4 487.6
+ 42 = ^{ART} 91+49	5 Old Line	4.4 488.6

old PT₃

New PT. • Sta 60+00

#2 change of Line

	F	H.I.		Elev.	Grade	Grade Stake
BM.	0.18	520.83		520.65	x513.6	
60			0.3	514.5	511.2	-1.7 ^{+0.3}
+20					x513.2	-2.1
+50			9.5	511.3	x511.2	-2.0 ^{+0.1}
T.P.	2.30	511.65	11.48	509.35		-2.2
61			5.0	506.6	x511.4	-2.1 ^{+0.1}
+20					x507.60	-3.6 ⁵⁰
+50			9.4	507.2	x505.2	-4.2 ⁵⁰
+60					x505.6	-5.0
+75			10.7	501.0		
+70					504.6	
62			9.5	502.2	504.6	-4.8 ^{+0.3}
+50			7.3	504.4	503.7	-2.0 ^{+1.0}
63			5.8	05.9	503.7	-0.5 ^{corner}
+50			7.6	04.1	503.1	-1.7 ^{+1.0}
64			9.3	02.3	x503.0	-3.7 ^{-0.7}
+27			10.8	00.8		
+50			9.3	02.3	503.0	-2.6 ^{-0.7}
65			5.9	05.7	503.0	+0.8 ^{+2.7}
+35			4.0	07.6		
+50			5.6	06.0	503.0	
+64	$\Delta 17^{\circ} 21' R$ (13' offset)		8.3	03.3		-2.7 ^{ED}
T.P.	8.35	512.30	7.70	503.95		+0.2
+91			14.4	497.9		
66			11.0	501.3	503.0	-3.9 ^{-1.7}
+50			7.7	04.6	503.0	-1.5 ^{+1.6}
67			8.2	04.1	503.0	-1.4 ^{+1.1}

	512.30			
67+50		8.5	503.8	503.0
68		9.1	^{02.3} 23.2	503.0
+25 ² ED +26 ¹¹ Δ 18°01' Lt (16' offset)		8.1	04.2	
+50		4.0	^{02.2} 21.3	503.0
69		9.7	02.6	503.0
+38 Δ 9°33' Lt (5' offset ahead)		9.3	03.0	
+50		9.0	03.3	503.0
70		8.4	03.9	503.0
+50			03.6	503.0
69+38 - 80 was offset + 5' - use same stationing				
71			03.4	503.0
+20				x 503.0
+50			02.5	502.6
+85				501.5
72			501.2	501.2
+40				x 501.2
+50			499.3	501.2
73			502.4	501.2
+50			503.0	501.2
74			501.1	x 501.2
+50			500.6	501.2
75			501.5	501.1
+50			501.5	x 500.6

						-1.7
						+0.8
						+1.3
						+1.6
						-1.9
						+1.2
						-0.8
						-3.4
						-0.4
						-3.3
						-0.4
						-2.7
						+0.8
						-0.8
						-3.6
						-3.8
						-3.0
						-1.2
						-0.8
						-1.7
						+0.6
						-1.0
						-1.0

Sta Elev. Grade

76 499.8 ~~499.8~~

+50 500.0 x 499.10

77 497.3 ~~495.16~~

+50 95.5 x 496.40

78 94.7 496.12

+28 96.7 ~~495.66~~

+50 ~~495.10~~

79 95.6 ~~494.78~~

+50 493.5 x 492.20

+90 x 492.2

RI = 8' over in sta next curve

Line Change - Short Cut-off

BM	+	H.L.		
				493.79
98+60	2.8	496.59	4.1	492.5
99			3.8	97.8
+50			4.5	92.1
100			7.5	89.1
+50			10.5	
T.R.	4.78	488.52	12.85	483.74
101			8.6	479.9
+30			12.8	75.7
+34	Ditch		13.8	74.7
+38			11.8	76.7
+50			10.6	77.9
+73			6.4	82.1
102			6.2	82.3
+26		496.59	17.7	84.5
+50			9.5	87.1
+63			10.3	86.3
+76			7.9	88.7
103				
+50			7.7	88.9
+76.5 = 104 + 13°			6.6	90.5

14 + 665 =
Sum 825

old pt now P.O.T. on hand 1/2 high

Line Change Long Cut off

$$579 - 80 - 109 + 226 = 111 + 336$$

10'
offset

Bm.	0.28	499.67		499.39			
80+00	old ear	15.05R	7.3	493.4	x490.7	-2.0	+0.0
+25	0.5				490.6	-1.9	
+50			10.8	488.9	x488.2	-1.6	+0.0
81	0.76	487.67	12.76	486.91			
			3.2	484.5	x485.0	-1.3	0.0
+50			6.0	481.7	481.7	-1.3	0.0
82			8.9	478.8	479.4	-2.2	0.0
+50			11.5	476.2	476.5	-1.2	0.0
83			13.2	474.5	473.8	+0.5	+1.0
	1.28	476.20	12.75	474.92			
+50			3.5	472.7	x470.9	+0.7	+1.0
+60			4.0	472.2			
+90					x466.6	+0.5	
84			11.3	64.9	x467.0	-1.5	
+10					x465.1	-1.0	
+30			15.3	460.9	x464.4	-1.0	
+50			18.1	58.1	x463.3		
+61			16.3	59.9			
+83			14.9	461.3	463.3		
85			11.4	64.8	x463.3	-0.5	
+30					x463.3	+0.5	
+50					x463.3	+0.7	+0.5
86			7.7	68.5	x468.5	+0.6	+0.1
+20					x471.0	-0.5	
+50			5.5	70.7	x471.2		
+80					x472.4	-0.4	
87			3.1	73.1	473		
+20					x473.3	+0.1	+0.1
+50			2.3	73.9			
88	5.80	479.75	21.25	473.95			+0.8
			5.3	74.9	473.4	+0.0	+1.0
+50			6.2	73.5	473.5	-0.5	+0.1

84+61 D. 724

El. Hub 492.22

84 467.0

84+50 463.3

462.75

El. Hub 472.55

+0.1

+0.8

+0.7

+0.7

89	479.75	5.8	474.0	473.6	-0.3	+0.4	+0.7
+50		4.7	75.1	473.7	+1.3	+1.4	+0.6
90		7.1	72.7	473.8	-0.9	-1.1	-0.1
+50		7.1	72.7	473.9	-1.6	-1.2	-0.3
91		6.6	73.2	474.0	-1.2	-0.8	-0.2
+50		6.1	73.7	474.1	-1.2	-0.4	+0.2
92		5.4	74.4	474.2	-0.2	+0.2	+0.6
+50		4.4	75.4	474.3	+0.6	+1.0	+0.8
93		4.3	75.5	474.4	+0.8	+1.2	+0.7
+50		5.1	74.7	474.50	-0.2	+0.2	+0.3
94		6.1	73.7	474.6	-1.5	-0.9	
+20			75.7				
+50		4.7	75.1	474.7	-0.1	+0.3	
95	83.0	8.8	⁵⁴ 74.2	x474.8	-0.5	-0.6	
+50		7.3	75.7	475.05	+0.4	+0.7	+0.2
96		7.0	76.0	476.1	+0.7	+0.0	
+50		5.9	77.1	476.8	+1.2		
+60			78.2	x477.0	+1.2		
97		5.5	77.5	477.0			+0.8
+20		3.0	80.0		+2.0		
+50		4.0	79.0	477.0			
98		2.9	480.1	477.0	+3.0	+3.1	

98+50	82.0	5.4	76.6	477.0	-0.8	-0.3
99		8.2	73.8	477.0	-3.6	-3.1
+30		11.1	70.9			2' deep
+50		7.0	75.0			
+60				x477.0	-2.0	
+80				x477.3	-2.2	-0.9
100	91.2	13.6	78.2	x478.2	-0.7	+0.1
+35				480.4	-0.3	-0.6
+50		9.5	81.7	481.4	+0.2	+0.4
+60				482.0		
101		6.5	84.7	x484.6	-0.9	+0.3
+50		4.7	86.5	486.55	+0.4	+0.0
102		4.6	89.6	x488.5		
+35 E.P.			88.4		+0.1	+0.2
+04 ⁵ - 104 + 132 P.I.		0.80	490.4			
End of Charge - Long Cut-off.						
+45			489.4	489.6	-0.7	-0.2
+50						

102+94⁹ = 105+00 Old Line.

New Line - Cont. from p 38.				Grade stakes		
Sta	+	H.I.	-	Elev	Grade	±
100	+60					
	+0.62	494.41		493.79		+0.4 -0.6
+35			17.8	479.6		
101			11.2	483.2	483.0	+0.8 ^{+0.2}
+50			8.0	86.4		+3.4 +1.6
+75			9.1	85.3		
102			9.7	84.7	483.0	+1.7 +1.2
+25			10.0	84.4		
+50			10.1	84.3		+1.3 +0.4
+80			9.0	85.4		
103			10.4	84.0	483.0	+1.0 +0.8
+50			10.6	83.8		+0.1
104			10.7	83.7	483.0	+0.7 -0.6
+20			9.7	84.7		
+50			11.4	83.0		+0.4 -2.0
+75			10.9	83.5		
105			12.4	82.0	483.0	-1.0 -2.2
+50			10.7	83.7		+0.7 -1.0
106			9.7	84.7	483.0	+1.7 -0.1
+50			9.95	484.46	IP 483.0	+1.4 -0.5
+90			4.6	83.2	483.0	+0.1 -1.6
107+412	PC.	487.84	6.2	81.6	483.0	-0.7 -3.4

		487.84					
107+84	FD		9.6	78.2	483.0	-6.4	
108+10					x483.0		
108+08			6.6	81.2	x483.2	-1.6	
+50					x485.1	-0.5	
108+23 ²	P.T.		5.3	482.5	x485.1	-0.4	
+35						-0.8	
109			0.8	487.0	x486.0	-0.8	+1.0
+22 ⁶	=111+33 ⁶	P.C.	1.3	486.5	486.0	-1.4	+0.5
111+30			1.4	86.4	486.0		
111+81				86.1		-2.4	+0.1
112+26 ⁶	P.T.			86.8		-4.1	+0.8
	0.68	498.76		498.08			
113	3.28	491.09	10.75	487.81	486.0	-0.9	
			6.0	485.1		-4.7	
+50			5.5	85.6		-4.1	-0.4
114			4.5	86.6	486.0	-2.6	+0.6
+50			4.1	487.0		-2.7	+1.0
115			4.0	487.1	486.0	-2.8	+1.1
+50			4.3	86.8		-2.4	
116			4.6	86.5	486.0	-2.6	+0.5
+50			4.6	86.5		-3.0	+0.5
117			5.2	85.9	486.0	-3.4	-0.1
+50			6.1	85.0		-3.9	
118			6.3	84.8	486.0	-4.5	-1.2
+50			5.1	86.0		-4.2	
119			5.3	85.8	486.0	-3.0	-0.2
+50			5.0	86.1	486.0	-2.6	

12" pipe - Trough over.

				Grade		offset	
120	491.09		3.7	487.4	486.0	-2.3	^{+1.4}
+50				486.6	486.0	-2.4	
121	494.62		7.7	486.9	486.0	-2.5	+0.9
+50			7.9	486.7	486.0	-2.8	+0.7
122			8.3	486.3	486.0	-3.8	+0.3
+50			9.3	485.3	486.0	-4.7	-0.7
123				486.5	486.0	-3.5	+0.5
+50			8.5	486.1	486.0	-4.0	+0.1
124			6.9	487.7	486.6	-4.2	+1.1
+50			6.45	488.2	487.4	-3.6	+0.8
125			7.4	487.2	488.1	-3.5	-0.9
+50			5.6	489.0	488.8	-3.4	+0.2
126			3.9	490.7	489.5	-1.8	+1.2
+50			3.0	491.6	490.3	-2.0	+1.3
+90			3.6	488.42	491.0	-2.6	+0.6
127	+ 8.88	497.30	6.1	491.6	491.0	-3.6	+0.6
+50			6.1	491.2	491.1	-3.0	+0.1
128			5.5	491.8	491.2	-2.1	+0.6
+50			6.35	491.0	491.3	-4.3	-0.3
+77			6.35	491.0	491.4	-3.8	-0.4
129			6.15	491.1	491.4	-3.2	-0.3

123+0.5 12" pipe - Trough over

	497.30	9.2	4.5	492.8	491.5	-3.4	+1.3
129+50		9.2					
130		3.65	93.7	x491.4		+1.6	+2.1
+50		5.94	492.3	x490.8		-0.5	
+70		7.20		x491.4		-0.5	
+95		16.10	491.2	x489.6		-0.1	+1.6
131		8.40		x488.0		+0.8	
+29.23 P.C.		7.1	490.2	x488.0			
+65				x485.3			
+40				x486.2		+2.2	
+60				x483.2		+4.9	
+80				x481.2		+6.0	
132	496.99	16.0	481.0	x483.0		+5.3	-0.2
+50				x482.6		-	
+75				x482.6			
133		15.5	481.5	x483.7		-1.6	-2.5
+50				485.1		+1.8	
134		8.5	488.5	486.2		+3.3	+2.3
134+50				x487.2		+3.2	
135			88.0	487.7		+3.6	+0.3
+50				x488.2		+4.9	
+80				x488.8		+5.5	
136			489.1	489.5		+5.2	-0.4
+50			91.3	491.2		+5.8	-0.3
137			94.5	493.0		+5.8	+0.9

	Current	Grades	10' offset	2
137+50	494.8	494.8	+3.6	^{-0.8}
+90		x496.6	+2.9	
138	497.6	497.8		^{-0.2}
138+10		498.4	+3.8	
+50	501.4	501.25		+0.0
+85		x504.0	+3.1	
139	506.7	504.8	+3.0	+0.8
+10		x505.4	+3.0	
+50	505.7	507.0	+1.5	
140	508.6	509.0	+1.0	^{-0.4}
+25		x510.0	+0.4	
+50		x510.4	+0.8	
+90		x510.4	+0.9	
141	510.7			+0.2
141+10		x510.7	+1.5	
+50	512.0	511.9	+1.0	
142	512.7	x513.0	+0.2	^{-0.7}
+25		x514.5	+0.4	
+50	516.2	x515.9	+1.2	
143	519.5	519.5	+0.8	0.0
+50	522.5	522.6		
+76 ^{1/2}		x524.3	+0.5	
144	527.4	527.05	+2.5	+0.8
+50	531.0	x530.2	+1.4	

144+75	532.4 531.2	+1.1
145	532.4 x 531.8	+0.8 +0.6
+25	x 532.0	+0.7
+50	532.8 x 531.6	+1.1
+75	x 530.8	+1.1
146	529.7 529.5	+2.1 +0.2
+50	528.0 527.0	+2.6
147	524.6 x 524.6	+3.0 +0.0
+50	522.6 522.7	+2.7
148	523.1 520.9	+2.5 +2.2
+50	518.3 519.1	+0.6
149	518.3 517.3	+1.7 +1.0
+50	514.9 515.5	+1.1
150	515.7 513.7	+1.5 +2.0
+25	x 512.6	
+50	512.0 x 510.1	
151	504.8 x 504.4	
+50	501.9 x 499.7	
152	500.6 x 497.3	
+50	499.7	
+70	x 494.9	
153	496.8 494.4	

2/24

Gregory

CROSS SECTION OF
MONROE AVE
from E.L. TEXAS80' ST.
14' CBSSE Texas
and Monroe351 $\frac{1}{2}$

	12.52	351.48	338.96	cb	10.8	340.6	✓	
		E. L. TEXAS		$\frac{1}{4}$	10.8	340.6	✓	
S		12.1	339.3	✓	10.6	340.8	✓	
cb		12.50	338.9	✓ on cement	10.6	340.8	✓	
$\frac{1}{4}$		12.4	339.0	✓	10.4	341.0	✓	
c		12.1	339.3	✓	10.1	341.3	✓	
$\frac{1}{2}$		12.2	339.4	✓				
+10		12.2	339.4	✓	100' E	9.1	341.3	✓
cb		11.60	339.8	✓ on cement	9.3	341.1	✓	
N		11.3	340.1	✓	9.5	341.9	✓	
		3' E		c	9.6	341.8	✓	
N		11.0	340.2	✓	$\frac{1}{2}$	9.6	341.8	✓
cb		11.2	340.4	✓	cb	9.8	341.6	✓
$\frac{1}{2}$		11.2	340.4	✓	S	10.0	341.4	✓
c		11.3	340.1	✓		150' E		
$\frac{1}{4}$		11.6	339.8	✓	S	9.1	341.3	✓
cb		11.7	339.7	✓	cb	8.4	343.0	✓
S		11.2	340.0	✓	$\frac{1}{4}$	8.4	343.0	✓
		50' E		c	8.5	341.9	✓	
S		11.0	340.4	✓	$\frac{1}{4}$	8.3	343.1	✓

351.48

351.4

cb	8.1	343.3	✓
N	7.7	343.7	✓
200° E			
N	6.2	345.1	✓
cb	6.4	345.0	✓
1/4	6.6	344.6	✓
c	6.9	344.5	✓
1/4	7.1	344.3	✓
cb	7.2	344.1	✓
S	7.2	344.1	✓
+10	8.0	343.1	✓

235 E

-10	7.3	345.1	✓
S	6.2	345.2	✓
cb	5.6	345.8	✓
1/4	5.6	345.8	✓
c	5.5	345.9	✓
1/4	5.1	346.3	✓
cb	4.9	346.5	✓
N	4.5	346.9	✓

MONROE

50

270° E 351.4

-5	1.9	349.5	✓
N	2.1	349.3	✓
cb	2.4	349.0	✓
1/4	2.7	348.7	✓
c	2.6	348.9	✓
1/4	2.7	348.7	✓
cb	2.9	348.5	✓
S	3.6	347.8	✓
+10	4.1	347.3	✓

293° E

-7	2.1	349.3	✓		
S	1.0	350.1	✓		
cb	0.3	351.1	✓		
T.P.	11.88	<u>36308</u>	0.28	351.20	✓
1/4				<u>36308</u>	
1/4			11.6	351.4	✓
c			11.5	351.5	✓
1/4			10.9	351.1	✓
cb			10.8	351.1	✓
N			11.4	351.6	✓
+7			11.4	351.6	✓

36308
300' E = 36308
W.L. Arizona

N		9.4	353.6	✓
cb		10.2	354.8	✓
	on cement	(9.13)	353.45	✓
1/4		10.1	352.9	✓
c		10.5	354.5	✓
1/4		11.1	351.9	✓
cb		11.3	351.7	✓
	on cement	10.74	354.34	✓
S		10.7	354.2	✓

E.L. Arizona

S		87	351.3	✓
+13		88	352.4	✓
cb	(cement covered)	8.1	352.9	✓
1/4		8.1	352.9	✓
c		7.9	355.1	✓
1/4		7.6	355.2	✓
cb		7.1	355.9	✓
	on cement	7.50	355.5	✓
N		6.4	352.6	✓

MONROE
3' E 36308
47

N		3.5	359.5	✓
cb		4.1	358.9	✓
+4		6.6	356.1	✓
1/4		6.8	356.2	✓
c		7.3	355.7	✓
+8		6.4	356.6	✓
1/4		4.2	358.8	✓
cb		4.3	358.7	✓
S		4.8	358.5	✓

12' E

S		3.7	359.3	✓
cb		3.3	359.7	✓
1/4		3.2	359.8	✓
c		5.5	357.5	✓
1/4		5.2	357.8	✓
+8		4.6	358.1	✓
cb		2.8	360.2	✓
N		1.0	362.0	✓

36308

25' E

N	0.4	362.6	✓
cb	1.2	361.8	✓
+3	2.8	360.4	✓
1/4	3.4	359.6	✓
c	3.7	359.3	✓
+4	3.6	359.2	✓
+8	2.6	360.4	✓
1/4	2.7	360.3	✓
cb	2.4	360.6	✓
S	2.1	360.9	✓
T.P.	11.93	374.08	0.93 362.15

45' E

S	11.7	362.2	✓
cb	11.1	362.9	✓
1/4	11.3	362.7	✓
+5	10.7	363.2	✓
+8	12.1	361.9	✓
c	12.4	361.6	✓
1/4	11.8	362.2	✓

+9

cb

N

N

cb

1/4

c

1/4

cb

+11

S

S

+4

cb

1/4

c

S

MONROE
374.08

48

11.1 362.9

9.3 362.7

9.4 362.6

65' E

7.7 366.3

8.5 365.5

9.4 362.6

9.7 362.3

10.1 363.9

9.1 364.9

9.2 364.8

11.3 362.7

79' E

10.7 363.3

8.9 365.1

8.9 365.1

8.8 365.2

7.3 366.7

81' E

8.4 365.6

37408

5740

cb	8.8	365.7 ✓
+11	8.8	365.7 ✓
1/4	8.1	365.9 ✓
c	6.7	367.3 ✓
1/4	6.5	367.5 ✓
cb	6.2	367.8 ✓
N	6.1	367.4 ✓
90° E		
N	5.6	368.2 ✓
cb	5.5	368.5 ✓
1/4	5.2	368.8 ✓
c	5.5	368.8 ✓
1/4	7.2	366.8 ✓
cb	7.3	366.7 ✓
5	7.3	366.7 ✓
105° E		
5	5.9	368.1 ✓
+3	5.1	368.3 ✓
cb	5.9	368.1 ✓
1/4	6.4	367.6 ✓

MONROE

3740

49

c	6.2	367.8 ✓
1/4	5.5	368.5 ✓
cb	5.0	369.0 ✓
N	4.3	369.7 ✓
118° E		
N	4.1	369.9 ✓
cb	4.3	369.7 ✓
1/4	4.7	369.3 ✓
c	5.6	368.4 ✓
1/4	5.7	368.3 ✓
cb	5.7	368.3 ✓
5	5.7	368.3 ✓
133° E		
5	5.5	368.5 ✓
cb	4.9	369.1 ✓
1/4	3.9	370.1 ✓
c	4.3	369.7 ✓
1/4	2.3	371.7 ✓
cb	1.9	372.1 ✓
+3	1.5	372.5 ✓

374.08

+5 3.8 370.4 ✓

N 3.7 370.3 ✓

140' E

N 3.6 370.4 ✓

+7 3.3 370.7 ✓

+9 2.3 371.7 ✓

cb 1.8 371.4 ✓

1/4 2.2 371.8 ✓

c 2.2 371.8 ✓

+3 3.4 370.6 ✓

1/4 3.2 370.8 ✓

cb 4.3 369.7 ✓

5 5.3 368.7 ✓

155' E

5 3.6 370.4 ✓

cb 3.8 370.4 ✓

1/4 3.8 370.4 ✓

c 3.0 371.0 ✓

1/4 2.5 371.5 ✓

cb 2.5 371.5 ✓

374⁰ MONROE

50

3.0 371.0 ✓

165' E

2.5 371.5 ✓

3.0 371.0 ✓

3.5 370.5 ✓

3.4 370.6 ✓

3.7 370.3 ✓

3.7 370.3 ✓

3.4 370.6 ✓

174' E

3.3 370.7 ✓

3.1 370.9 ✓

3.1 370.9 ✓

3.0 371.0 ✓

3.2 370.8 ✓

2.3 371.7 ✓

1.5 371.5 ✓

194' E

1.6 371.4 ✓

2.0 371.0 ✓

374.08

374.0

1/4	2.5	371.5	✓
c	1.7	372.3	✓
18	0.8	373.2	✓
1/4	1.3	372.7	✓
cb	1.9	372.1	✓
S	2.6	371.4	✓

220' E

S	1.8	372.2	✓
cb	1.8	372.1	✓
1/4	2.0	372.0	✓
c	2.2	371.8	✓
1/4	1.4	372.6	✓
cb	0.9	373.1	✓
N	0.6	373.4	✓

T.R	6.82	380.60	0.30	373.78
-----	------	--------	------	--------

240' E

N	6.3	374.3	✓
cb.	6.0	374.6	✓
1/4	6.1	374.5	✓
c	7.0	373.6	✓

MONROE

380.6

51

1/4	7.4	373.2	✓
cb	7.2	373.4	✓
S	7.6	373.0	✓

255' E

S	7.2	373.4	✓
cb.	7.6	373.0	✓
1/4	7.2	373.4	✓
c	6.5	374.1	✓
1/4	6.5	374.1	✓
cb	6.1	374.5	✓
N	6.0	374.6	✓

275' E

N	5.5	375.1	✓
cb	6.0	374.6	✓
1/4	6.3	374.3	✓
c	6.3	374.3	✓
1/4	6.0	374.6	✓
cb.	6.6	374.0	✓
S	6.7	373.9	✓

380.60

300' E

380.6

W. Line Hamilton

S		6.1	374.5 ✓
cb.	Cement	6.13	374.7 ✓
+2		6.5	374.1 ✓
1/4		6.0	374.6 ✓
C		6.1	374.5 ✓
1/4		6.2	374.4 ✓
+12		6.5	374.1 ✓
cb.	Cement	5.51	375.09 ✓
N		5.6	375.0 ✓

E. Line Hamilton

N		4.6	376.0 ✓
cb.	Cement	4.72	375.98 ✓
cb.		5.5	375.1 ✓
1/4		5.1	375.5 ✓
C		5.2	375.4 ✓
1/4		5.4	375.2 ✓
cb		5.8	375.8 ✓
cb.	Cement	5.30	375.3 ✓
S		4.8	375.8 ✓

25' E

380.6

MONROE

52

S		4.7	375.9 ✓
cb		4.7	375.9 ✓
1/4		4.7	376.2 ✓
C		4.7	376.2 ✓
1/4		4.7	375.9 ✓
cb		4.9	375.7 ✓
+1		4.6	376.0 ✓
N		4.5	376.1 ✓

35' E

N		4.4	376.2 ✓
cb		4.4	376.2 ✓
1/4		4.7	375.9 ✓
C		4.5	376.1 ✓
1/4		4.6	376.0 ✓
cb.		4.8	375.8 ✓
S		4.0	376.2 ✓

50' E

S		5.1	375.5 ✓
cb.		4.8	375.8 ✓

~~380.6~~

1/4	4.5	376.1 ✓
C	4.6	376.0 ✓
1/4	4.7	375.9 ✓
cb.	4.7	375.9 ✓
N	4.1	376.5 ✓
	62' E	
N	4.0	376.6 ✓
+12	4.2	376.4 ✓
cb.	4.8	375.8 ✓
1/4	4.6	376.0 ✓
C	4.5	376.1 ✓
1/4	4.5	376.1 ✓
cb.	4.7	375.9 ✓
S	5.1	375.5 ✓
	83' E	
S	3.4	377.2 ✓
cb.	4.7	375.9 ✓
1/4	4.6	376.0 ✓
C	4.3	376.3 ✓
1/4	4.3	376.3 ✓

~~380.6~~ MONROE

cb.	4.5	376.1 ✓
+2	4.0	376.6 ✓
N	3.9	376.7 ✓
	100' E	
N	3.8	376.8 ✓
+12	3.8	376.8 ✓
cb.	4.3	376.3 ✓
1/4	4.1	376.5 ✓
C	4.1	376.5 ✓
+10	4.1	376.5 ✓
1/4	4.5	376.1 ✓
cb.	4.8	375.8 ✓
S	4.9	375.7 ✓
	150' E	
S	3.3	377.3 ✓
cb.	4.1	376.5 ✓
1/4	4.3	376.3 ✓
C	3.8	376.8 ✓
1/4	3.8	376.8 ✓
cb.	3.8	376.8 ✓

380⁶

N		3.5	377.1 ✓
	185' E		
N		3.0	377.6 ✓
+13		3.2	377.4 ✓
cb		3.8	376.8 ✓
1/4		3.5	377.1 ✓
c		3.7	376.9 ✓
1/4		4.1	376.5 ✓
cb.		3.9	376.7 ✓
s		3.5	377.1 ✓
	205' E		
s		3.5	377.1 ✓
cb.		3.4	377.4 ✓
1/4		3.7	376.9 ✓
c		3.7	377.4 ✓
1/4		3.4	377.4 ✓
cb.		3.6	377.0 ✓
+1		3.0	377.6 ✓
N		3.9	377.7 ✓

Monroe 54

225' E 380⁶

N		2.7	377.9 ✓
+13		2.8	377.8 ✓
cb		3.4	377.4 ✓
1/4		3.1	377.5 ✓
c		3.2	377.4 ✓
1/4		3.6	377.0 ✓
cb.		3.5	377.1 ✓
s		3.4	377.4 ✓
	240' E		
s		3.2	377.4 ✓
cb.		3.2	377.4 ✓
1/4		2.8	377.8 ✓
+7		2.7	377.9 ✓
c		3.3	377.3 ✓
1/4		3.3	377.3 ✓
cb.		3.3	377.3 ✓
+1		2.7	377.9 ✓
N		2.6	378.0 ✓

380.60

265.1' E

N		2.5	378.1 ✓
+12		2.6	378.0 ✓
cb.		3-3	377.3 ✓
1/4		3-0	377.6 ✓
c		3-1	377.5 ✓
1/4		3-3	377.3 ✓
cb.		3-2	377.4 ✓
S		2.6	378.0 ✓
	299.7' E.	W. Line Oregon	
S		2.1	378.5 ✓
cb.		2.7	377.9 ✓
cb.	Cement	2.33	378.17 ✓
1/4		2.4	377.8 ✓
C		2.8	377.8 ✓
1/4		2.8	377.8 ✓
cb.		2:8	377.8 ✓
+1	Cement cb.	2.41	378.19 ✓
N		2.1	378.5 ✓

E. Line Oregon

380.6 Monroe

55

N		1.5	379.1 ✓
cb.		2.0	378.6 ✓
cb.	Cement	1.60	379.0 ✓
+1		2.3	378.3 ✓
1/4		2.1	378.5 ✓
C		1.8	378.8 ✓
1/4		2.2	378.5 ✓
+12		2.1	378.5 ✓
cb.	Cement	1.33	379.07 ✓
T.P.	163	380.78	1.45 379.15
		17' E	
cb.	Cement	380.7 1.42	378.9 ✓
+1		2.4	378.3 ✓
1/4		2.3	378.4 ✓
C		2.4	378.3 ✓
1/4		2.5	378.5 ✓
cb.		2.2	378.5 ✓
N		2.0	378.7 ✓

N.D. Cement
cb. & sidewalk
Completed from
Oregon to
Idaho

380.78

35' E

380.7

N	1.9	378.5 ✓
cb.	1.5	379 ✓
1/4	2.0	378.7 ✓
c	2.4	378.3 ✓
1/4	2.3	378.4 ✓
+12.8	2.1	378.6 ✓
	65' E	
cb. + 0.2	2.1	378.6 ✓
1/4	2.2	378.5 ✓
c	2.4	378.5 ✓
1/4	2.5	378 ✓
cb.	2.7	378.0 ✓
N	2.4	378.3 ✓
	80' E	
N	1.3	379.4 ✓
cb.	2.0	378.7 ✓
1/4	2.6	378.1 ✓
c	2.6	378.1 ✓
1/4	2.3	378.4 ✓

+12.8

108' E

cb.	Cement	2.57	378.4 ✓	56
+1		2.2	378.5 ✓	
1/4		2.2	378.5 ✓	
c		2.2	378.5 ✓	
+7		1.6	379.1 ✓	
1/4		2.5	378 ✓	
cb.		2.1	378.6 ✓	
N		1.8	378.9 ✓	
	125' E			
N		1.0	379.7 ✓	
cb.		0.7	380.0 ✓	
1/4		2.1	378.6 ✓	
c		2.4	378.3 ✓	
1/4		2.5	378 ✓	
cb.	Cement	2.47	378.5 ✓	
	152' E			
cb. + 0.2		2.9	377.8 ✓	
1/4		3.0	377.7 ✓	

380.78

2.3

378.4

		380.78	
c		2.7	378.0 ✓
1/4		2.5	378.1 ✓
cb.		2.3	378.2 ✓
N		2.2	378.3 ✓
	170' E		
N		1.8	378.9 ✓
+3		2.9	377.8 ✓
cb.		3.4	377.3 ✓
1/4		3.3	377.2 ✓
c		3.2	377.5 ✓
1/4		3.3	377.1 ✓
+12.8		3.1	377.6 ✓
	220' E		
cb.	Cement.	3.55	377.25 ✓
+1		3.4	377.3 ✓
1/4		3.6	377.1 ✓
c		3.8	376.9 ✓
1/4		3.6	377.1 ✓
cb.		3.3	377.4 ✓
+12		3.0	377.7 ✓

		380.78	57
N		2.3	378.1 ✓
	100' E		
N		2.7	378.0 ✓
+8		2.9	377.8 ✓
cb		4.0	376.7 ✓
1/4		3.8	376.9 ✓
c		3.9	376.8 ✓
1/4		4.0	376.7 ✓
+12.8		3.8	376.9 ✓
	290' E		
		4.5	376.2 ✓
		4.4	376.3 ✓
		4.3	376.4 ✓
		4.4	376.3 ✓
		3.7	377.0 ✓
	w. line Idaho	300.8 E	
N		3.7	377.0 ✓
cb	cement	4.28	376.56 ✓
+1		4.8	375.9 ✓

380.78

380.78

1/4		4.4	376.5	✓
c		4.5	376.2	✓
1/4		4.5	376.1	✓
+ 12		4.8	375.9	✓
cb.	Cement	4.24	376.5	✓
Ch. B. M.		4.85	375.93	✓
			58 SP Idaho + Mont 375.94	
E. Line Idaho				
s		4.7	376.0	✓
cb	Cement	4.83	375.93	✓
+ 11		5.6	375.1	✓
1/4		5.3	375.4	✓
c		5.2	375.5	✓
1/4		5.4	375.3	✓
+ 12		5.8	374.9	✓
cb	Cement	4.92	375.86	✓
N		4.3	376.4	✓
15' E				
N		5.7	375.0	✓
cb		6.2	374.5	✓
1/4		5.7	375.0	✓

380.78

380.78

c		5.8	374.9	58 ✓
1/4		5.9	374.6	✓
cb.		5.8	374.9	✓
s		6.4	374.5	✓
42' E				
s		7.6	373.1	✓
cb.		7.6	373.1	✓
1/4		7.5	373.1	✓
c		7.6	373.1	✓
1/4		7.7	373.3	✓
cb.		7.0	373.7	✓
N		6.3	374.2	✓
65' E				
N		8.9	371.8	✓
cb.		8.9	371.8	✓
1/4		8.9	371.8	✓
c		8.7	372.0	✓
1/4		8.9	371.8	✓
cb.		8.7	372.0	✓
s		9.0	371.7	✓

380.78

85' E

380.2

S	9.7	371.0 ✓
cb	9.9	370.8 ✓
1/4	9.9	370.8 ✓
C	9.5	371.2 ✓
1/4	9.8	370.9 ✓
cb.	9.3	371.2 ✓
N	8.8	371.9 ✓

97' E

-5	10.1	370.6 ✓
N	10.5	370.2 ✓
cb.	10.5	370.2 ✓
1/4	10.1	370.6 ✓
C	9.9	370.8 ✓
1/4	10.3	370.6 ✓
cb.	10.4	370.3 ✓
S	10.4	370.3 ✓
+5	10.4	370.3 ✓

115' E

-5	10.9	369.8 ✓
----	------	---------

S
N

cb.	10.9	369.8 ✓
1/4	10.7	370.0 ✓
C	10.4	370.3 ✓
1/4	10.8	369.9 ✓
cb	10.8	369.9 ✓
N	9.6	371.1 ✓
+5	9.3	371.2 ✓

125' E

-5	10.7	370.3 ✓
N	10.8	369.9 ✓
cb.	10.9	369.8 ✓
1/4	10.8	369.9 ✓
C	10.6	370.1 ✓
1/4	11.0	369.7 ✓
cb.	11.0	369.7 ✓
S	11.1	369.6 ✓
+5	11.1	369.6 ✓

160' E

-5	11.6	369.1 ✓
----	------	---------

Monroe
380.7

59

10.9	369.8 ✓
10.9	369.8 ✓
10.7	370.0 ✓
10.4	370.3 ✓
10.8	369.9 ✓
10.8	369.9 ✓
9.6	371.1 ✓
9.3	371.2 ✓

10.7	370.3 ✓
10.8	369.9 ✓
10.9	369.8 ✓
10.8	369.9 ✓
10.6	370.1 ✓
11.0	369.7 ✓
11.0	369.7 ✓
11.1	369.6 ✓
11.1	369.6 ✓

11.6	369.1 ✓
------	---------

380.78

	380.78	
S	11.6	369.1 ✓
cb	11.1	369.6 ✓
+1	11.6	369.1 ✓
1/4	11.4	369.3 ✓
c	10.9	369.8 ✓
1/4	11.1	369.6 ✓
cb.	10.7	370.0 ✓
N	10.9	369.8 ✓
+5	11.1	369.6 ✓
	190' E	
-5	11.2	369.5 ✓
N	11.2	369.5 ✓
cb	11.3	369.2 ✓
1/4	11.2	369.5 ✓
c	11.2	369.5 ✓
1/4	11.5	369.2 ✓
+12	11.7	369.0 ✓
cb	11.3	369.2 ✓
S	11.7	369.0 ✓
+5	11.7	369.0 ✓

208' E

380.78

1000

60

	380.78	
-5	11.6	369.1 ✓
S	11.6	369.1 ✓
cb.	11.1	369.6 ✓
+1.	11.6	369.1 ✓
1/4	11.5	369.2 ✓
c	11.4	369.3 ✓
1/4	11.5	369.2 ✓
cb.	10.0	370.7 ✓
N	9.1	371.6 ✓
+5	9.1	371.6 ✓
	228' E	
-5	11.4	369.3 ✓
N	11.4	369.3 ✓
cb.	11.5	369.2 ✓
1/4	11.2	369.5 ✓
c	11.0	369.7 ✓
1/4	11.5	369.2 ✓
cb.	11.4	369.3 ✓
+4	10.2	370.5 ✓
+5	11.6	369.1 ✓

380.78

~~380.78~~

S	11.7	369.0 ✓
+5	11.7	369.0 ✓
	275' E	
-5	11.6	369.1 ✓
S	11.6	369.1 ✓
+6	11.3	369.2 ✓
+11	10.1	370.6 ✓
cb.	11.2	369.5 ✓
1/4	11.4	369.3 ✓
c	10.8	369.9 ✓
1/4	10.8	369.9 ✓
cb.	10.8	369.9 ✓
N	11.2	369.5 ✓
+5	10.8	369.9 ✓
	265' E	
N	9.7	371.0 ✓
+7	10.6	370.1 ✓
cb.	10.2	370.5 ✓
+6	9.6	371.1 ✓
1/4	10.8	369.9 ✓

170-1100
380.78

61

+7	10.3	370.4 ✓
c	10.6	370.1 ✓
1/4	11.4	369.3 ✓
cb	11.1	369.6 ✓
+4	10.2	370.5 ✓
+6	11.2	369.5 ✓
S	11.4	369.3 ✓
+5	11.4	369.3 ✓
	275' E	
-5	11.5	369.1 ✓
S	11.5	369.2 ✓
+6	11.2	369.5 ✓
+9	10.3	370.2 ✓
cb	11.2	369.5 ✓
1/4	11.3	369.2 ✓
c	10.7	370.3 ✓
+6	10.2	370.5 ✓
1/4	10.8	369.9 ✓
cb.	10.5	370.4 ✓
N	10.1	370.6 ✓

380.78

~~380.78~~

+5		10.1	370.6 ✓
	299.5' E	N. Line	Utah
N		9.3	371.2 ✓
cb.		9.3	371.4 ✓
cb.	Cement	9.76	371.0 ✓
+2		10.6	370.1 ✓
1/4		10.5	370.2 ✓
c		10.4	370.3 ✓
1/4		10.9	369.8 ✓
+12		10.1	370.6 ✓
cb.		10.9	369.8 ✓
cb.	Cement	10.39	370.39 ✓
S		11.0	369.7 ✓

423 380.17

E.L. Utah
~~380.17~~

S		9.4	370.2 ✓
+13		9.7	370.4 ✓
cb		10.2	369.9 ✓
1/4		10.1	370.0 ✓
C		9.4	370.7 ✓

375.94

50 1000
375.94~~380.17~~

100008

62

1/4		9.8	370.3 ✓
+12		9.6	370.5 ✓
cb	Cement	9.17	371.00 ✓
N		8.8	371.3 ✓
	10' E		
N		9.0	371.1 ✓
cb		9.3	370.8 ✓
1/4		9.2	370.5 ✓
c		9.4	370.7 ✓
1/4		10.1	370.0 ✓
cb.		10.2	369.9 ✓
S		9.7	370.2 ✓
	35' E		
S		9.4	370.2 ✓
cb.		9.5	370.6 ✓
1/4		9.4	370.7 ✓
C		8.6	371.5 ✓
17		8.6	371.5 ✓
1/4		9.4	370.7 ✓
cb		9.1	371.0 ✓

380.17

380.17

N

9.1 371.0 ✓

53' E

N

9.2 370.9 ✓

cb

9.2 370.9 ✓

1/4

9.4 370.7 ✓

+6

8.8 371.3 ✓

c

8.8 371.3 ✓

1/4

9.5 370.6 ✓

cb.

9.6 370.5 ✓

s

9.7 370.4 ✓

70' E

s

9.6 370.5 ✓

cb.

9.6 370.5 ✓

1/4

9.5 370.6 ✓

c

8.8 371.3 ✓

1/4

9.5 370.6 ✓

cb

9.4 370.7 ✓

N

7.6 371.5 ✓

95' E

N

8.9 371.1 ✓

Monroe
380.17

63

9.0 371.1 ✓

9.5 370.6 ✓

8.4 371.7 ✓

9.1 371.0 ✓

9.2 370.9 ✓

9.1 371.0 ✓

125' E

9.6 370.5 ✓

9.7 370.4 ✓

9.7 370.4 ✓

8.6 371.5 ✓

9.3 370.8 ✓

8.2 371.9 ✓

8.8 371.3 ✓

8.7 371.2 ✓

140' E

7.7 371.7 ✓

8.3 371.8 ✓

9.0 371.1 ✓

9.0 371.1 ✓

cb

1/4

c

1/4

cb.

s

s

cb

1/4

c

1/4

+5

cb

N

N

cb.

1/4

c

380.17

1/4	380.17	370.1 ✓
cb	9.7	370.7 ✓
S	9.4	370.4 ✓
	9.7	370.4 ✓
	160' E	
S	9.9	370.2 ✓
cb	9.4	370.7 ✓
1/4	9.2	370.9 ✓
C	9.0	371.1 ✓
1/4	9.5	370.6 ✓
cb	8.9	371.2 ✓
N	8.8	371.3 ✓
+2	8.9	371.2 ✓

180' E

-5	9.0	371.1 ✓
N	9.2	370.9 ✓
cb	8.0	372.1 ✓
+9	8.9	371.1 ✓
1/4	9.7	370.2 ✓
C	9.2	370.9 ✓
1/4	9.8	370.3 ✓

Monroe
380.17
10.3 369.8 ✓ 64

cb	10.3	369.8 ✓
S	10.3	369.8 ✓
	195' E	
S	10.6	369.5 ✓
cb	10.4	369.7 ✓
1/4	9.8	370.3 ✓
C	9.2	370.9 ✓
1/4	9.6	370.5 ✓
cb.	9.8	370.5 ✓
N	9.5	370.6 ✓
+5	8.9	371.2 ✓

220' E

-5	9.0	371.1 ✓
N	9.3	370.8 ✓
cb	9.4	370.7 ✓
1/4	9.8	370.3 ✓
C	9.7	370.7 ✓
1/4	9.8	370.3 ✓
cb	10.2	369.9 ✓
S	10.6	369.5 ✓

380.17

380.17

10.5

369.6 ✓

232' E

+5

10.5

369.6 ✓

5

10.0

370.1 ✓

cb

10.3

369.8 ✓

1/4

9.8

370.3 ✓

c

9.7

370.7 ✓

1/4

9.7

370.4 ✓

cb

8.2

371.9 ✓

N

9.2

370.9 ✓

+5

8.9

371.4 ✓

255' E

-5

8.9

371.4 ✓

N

9.2

370.9 ✓

cb

9.6

370.5 ✓

1/4

9.6

370.5 ✓

c

9.2

370.9 ✓

1/4

9.5

370.6 ✓

cb

9.8

370.3 ✓

5

10.0

370.1 ✓

380.17

380.17

10.7

369.7 ✓

65

275' E

+5

10.3

369.8 ✓

5

10.2

369.9 ✓

cb

10.0

370.1 ✓

1/4

9.6

370.5 ✓

c

9.0

371.1 ✓

1/4

9.7

370.4 ✓

+5

7.8

371.3 ✓

cb

8.6

371.5 ✓

N

8.8

371.3 ✓

+5

8.7

371.2 ✓

285' E

-5

8.7

371.2 ✓

N

8.8

371.3 ✓

cb

9.1

371.0 ✓

1/4

9.3

370.8 ✓

c

8.8

371.3 ✓

1/4

9.7

370.4 ✓

cb

10.0

370.1 ✓

380.17

		380.17		
S		10.2	3699	✓
+5		10.1	370.0	✓
300' E	W. Line	Kansas		
-5		9.6	370.5	✓
S		9.6	370.5	✓
cb		9.7	370.4	✓
cb	Cement	9.21	370.96	
1/4		9.6	370.5	✓
c		9.1	371.0	✓
1/4		9.3	370.8	✓
cb		9.0	371.1	✓
cb	Cement	8.20	371.9	✓
N		8.1	372.0	✓
	E. Line	Kansas		
N		6.9	373.2	✓
cb		7.8	374.3	✓
cb	Cement	7.30	374.8	✓
1/4		8.0	374.1	✓
c		8.1	374.0	✓
1/4		8.9	371.2	✓

		380.17			66
cb		8.5	371.6	✓	
cb	Cement	8.16	372.0	✓	
S		8.3	371.8	✓	
-5	30' E	8.4	371.7	✓	
S		8.4	371.7	✓	
cb		8.4	371.7	✓	
1/4		7.5	372.6	✓	
c		7.1	373.0	✓	
1/4		7.5	372.6	✓	
cb		6.9	373.2	✓	
N		6.9	373.7	✓	
	45' E				
N		5.6	374.5	✓	
cb		6.8	373.3	✓	
+6		7.3	373.8	✓	
1/4		7.1	373.0	✓	
c		6.8	373.3	✓	
1/4		7.0	373.1	✓	
cb		7.7	372.2	✓	
S		7.3	372.8	✓	

380.17

65' E 380.17

-5	7.9	374.4	✓
S	7.9	374.4	✓
cb.	7.0	373.1	✓
1/4	6.9	373.4	✓
c	6.6	373.5	✓
1/4	7.2	374.9	✓
+5	6.1	374.0	✓
cb	6.0	374.1	✓
N	5.7	374.2	✓

90' E

N	5.5	374.6	✓
cb	5.7	374.1	✓
+4	6.4	373.7	✓
1/4	6.6	373.5	✓
c	6.3	373.8	✓
1/4	6.8	373.5	✓
cb	7.2	374.9	✓
S	7.0	373.1	✓

Monroe

67

100' E 380.17

-5	7.3	374.8	✓
S	7.3	374.8	✓
cb	7.0	373.1	✓
1/4	6.2	373.9	✓
c	6.0	374.1	✓
1/4	6.6	373.5	✓
cb	5.2	374.4	✓
N	5.0	375.1	✓

120' E

N	5.3	374.8	✓
cb	6.3	373.8	✓
+5	6.4	373.7	✓
1/4	5.8	374.3	✓
c	5.8	374.3	✓
1/4	6.2	373.9	✓
cb	6.7	373.4	✓
S	7.1	373.0	✓
+5	7.1	373.0	✓

380.17

135' E

~~380.17~~

-5	6.4	373.7	✓
S	6.4	373.7	✓
cb	5.7	374.4	✓
1/4	5.8	374.3	✓
C	5.6	374.5	✓
+10	5.7	374.4	✓
1/4	6.4	373.7	✓
cb	5.2	374.9	✓
+10	4.0	376.1	✓
N	3.8	376.3	✓

135' E

-5	5.0	375.1	✓
N	5.0	375.1	✓
cb	4.4	375.7	✓
+8	4.8	375.3	✓
1/4	5.3	374.8	✓
C	5.5	374.6	✓
1/4	5.9	374.1	✓
cb	6.2	373.9	✓

Monroe

380.17

6.3

373.8

68

S	6.3	373.8	✓
+5	6.3	373.8	✓

170' E

S	5.1	375.0	✓
cb	5.0	375.1	✓
1/4	5.7	374.4	✓
C	5.3	374.8	✓
1/4	5.3	374.8	✓
cb	4.6	375.5	✓
N	5.0	375.1	✓
+5	4.0	376.1	✓

200' E

-5	5.1	375.0	✓
N	5.1	375.0	✓
cb	5.2	374.9	✓
1/4	4.8	375.3	✓
C	4.6	375.5	✓
1/4	5.5	374.6	✓
cb	5.0	375.1	✓

380.17

380.1

+7	4.0	376.1	✓
S	4.5	375.6	✓
220' E			
S	5.0	375.1	✓
+3	5.2	374.9	✓
cb	5.4	374.7	✓
1/4	4.9	375.4	✓
c	4.1	376.0	✓
1/4	4.2	375.9	✓
+3	3.3	376.8	✓
cb	3.0	377.1	✓
N	3.8	376.3	✓
+5	3.1	377.0	✓
240' E			
-3	3.4	376.7	✓
N	3.4	376.7	✓
cb	3.8	376.0	✓
1/4	3.7	376.4	✓
c	3.6	376.5	✓
1/4	4.1	376.0	✓

380.1

69

+3	3.2	376.2	✓
cb	4.1	376.0	✓
+7	4.6	375.5	✓
S	3.7	376.4	✓
255' E			
-3	3.4	376.7	✓
S	4.3	375.8	✓
cb	2.8	377.3	✓
+7	2.1	378.0	✓
+11	3.5	376.6	✓
1/4	3.5	376.6	✓
c	3.2	376.9	✓
1/4	3.6	376.5	✓
cb	3.6	376.5	✓
N	3.7	376.4	✓
+5	3.7	376.4	✓
270' E			
-5	2.5	377.6	✓
N	3.0	377.1	✓
cb	3.6	376.5	✓

380.17

380.17

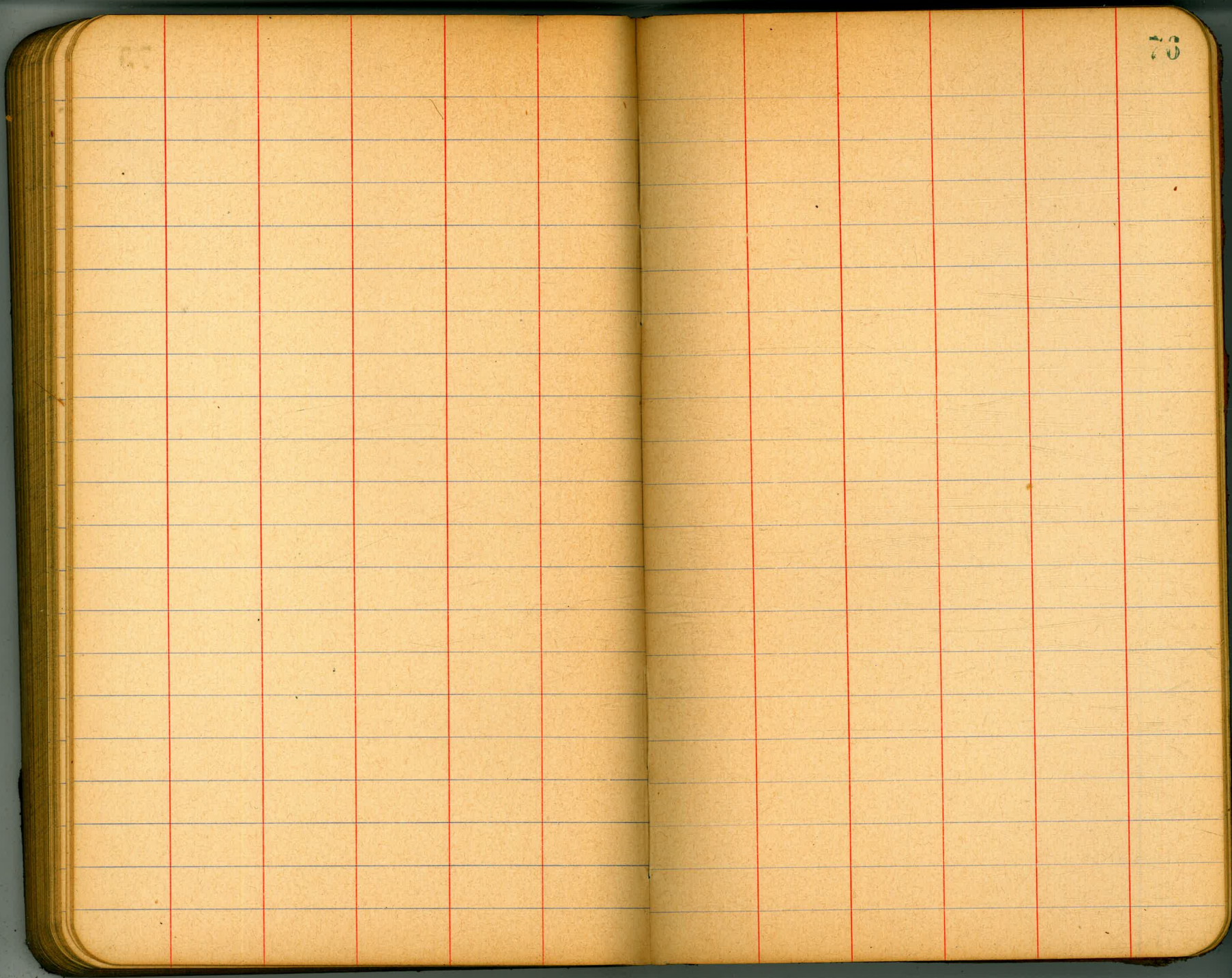
1/4	3.6	376.5 ✓
C	3.1	377.0 ✓
1/4	3.2	376.4 ✓
cb.	3.5	376.6 ✓
+10	3.8	376.3 ✓
S	2.9	377.4 ✓
+3	2.9	377.4 ✓
285' E		
-5	2.3	377.8 ✓
S	2.3	377.8 ✓
+1	3.3	376.5 ✓
cb	2.8	377.3 ✓
1/4	3.0	377.1 ✓
c	2.6	377.5 ✓
1/4	2.8	377.3 ✓
cb	2.0	378.1 ✓
N	2.9	377.4 ✓
+5	1.2	378.9 ✓
300' E = White 30" St.		
N	1.6	378.5 ✓

380.17 on 100

70

cb	2.0	378.1 ✓
cb. cement	1.13	379.0 ✓
1/4	1.6	378.5 ✓
c	1.5	378.6 ✓
1/4	2.0	378.1 ✓
cb.	1.9	378.4 ✓
cb cement	1.70	378.4 ✓
S	1.6	378.5 ✓
ch. B.M.	380.17	1.20 378.97

SE 30th +
Moynock
378.95



28

27

78

Prelim. change 100+35 - 109+77

	497.57		
100+35		14.0	480.6
+65		11.4	483.2
101		11.3	483.3
+70		8.2	486.4
102		9.8	484.8
+75		9.3	485.3
103		10.7	483.9
104		11.6	483.0
105		12.8	481.8
106		10.7	483.9
+50		11.1	483.5
107		11.5	483.1
+82	487.85	12.5	475.3
108		9.8	478.0
109		1.6	486.2
+77		1.9	486.0

(E. 111+81 P.)

54080
 54201
 30 + 6 378.95
 375.94
 320 ✓
 380
 10.40 531.6

67.5
 32.20
 104.70
 177.50

1. grade thru Harvey Ranch
 2. Pipe in fill 4119?
 3. Check on road
- Set 460 + 10
542.10*

Handwritten notes and calculations, including a large list of numbers and a circled '4'.

*Sta 60-R-300
Defl 50 = 4° 46.495*

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE. SIDE SLOPES $1\frac{1}{2}$ TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.