

1026

FIELD BOOK

1308

MICROFILMED
DEC 17 1964

A. Line
 Transit time for x sec 85
 Lower Dry Dam site
 S-side of Dam going East

Sta	L	ANGLE B	Dis-	C.C.	M.C.
A9	0		25.00		
A8	0		25.00		
A4	A	35°05'	100.0	S 61°05' E N 83° 4'	
A7	0		25.68		
A6	0		25.68		
A5	0		25.68		
A4	A	21°55'	25.68	S 71°10' E 18°10'	
A3	0		30.52		
A3	A	14°50'	30.52	N 83° E	
A2	0		24.63		35°
A0	A	20°10'	24.63	S 82°10' E	
		90	90°	S 62° E	
				N 28° E N 28° E	

4997 $\Delta 6^{\circ}48'$

3-24-16
 Huston
 Shoemaker
 Bellamy
 Correll
 Magsfield
 P.M.
 Kneeshaw

R.D. TO DAM = AXIS -
 CENTER LINE OF DAM.

Sta	ANGLE	R	DIS.	C.C.
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A 16

A 15	°		31.20	
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A 14	°		31.20	
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A 13	°		31.20	
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A 12	△	36.50	31.20	N 81° 15' E
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A 11	◊		25.00	
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A 10	°		25.00	S 61° 55' E
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36.45

B-line

Fast from South End of Dam

3-24-14

3

Sta	Angle	DIS	C.C.
B8	0		
B7	31°35'	29.24	S87°20'W 30°40'
B6	0	53.69	
B5	0	53.69	
B4	18°05'	53.69	S55°45'W 42°15'
B3	0	34.85	
B2	26°40'	34.85	S73°20'W 44°10'
B1		21.21	
B0	17°30'	26.21	N79°30'W
B0	90°		N62°W N28°E

B1 To Center line of Dam

= A0

A-line

West from North End of Dam.

Sta	Angle	B	Dis	C.C.
A-10 ^o			26.93	
A-9 ^o			26.93	
A-8 ^o			26.93	
A-7 ^o			26.93	
A-6 ^o			26.93	
A-5 ^o			26.93	
A-4 ^o			26.93	
A-3 ^Δ	21°50'	26.93	540°10'E	
A-2 ^o		25.00		
A-1 ^o		25.00		
A-0 ^Δ	90°00'	25.00	562°E	

N38°E

C-LINE OF DAM.

A' Line

Sta	Angle	A	B	Dis - C.C.
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A' 16				
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A' 15				2502
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A' 14				2502
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A' 13				2502
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A' 12				2502
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A' 11	34°10'			2502
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SLW' 21'E

54°10'E

3-25-46

Huston
Breadshaw
Stoemaker
Bellamy
Corrall
Mansfield

5^r

B-Line

East from North End of Dam

Sta	Angle	R	Dist	C.C.
B-8	0		50.25	
B-7	0		50.25	
B-6	0		50.25	
B-5	0		50.25	
B-4	0		50.25	
B-3	0		50.25	
B-2	Δ	N40°15'	50.25	N1°50'W
B-1	0			
B-0	Δ	N°55'	26.00	N46°25'W N42°W N38°E

N40°

255.80 N-PP-C-410 C of Dam from H-0

90°

x Sections: Lower Otay Dam Site.

3-30-16

77

	1092.	151.92		141.00
B ₂ 0+00			19	500
A 0+00			19	500
B ₂ 0+13			87	43.2
B ₂ 0+30			104	415
A 0+25			110	409
B ₁ 0+00			10	509
B ₁ 0+22			112	40.7
B ₁ 0+47			124	395
	099	141.99	1092	141.00
A 0+50			47	34.3
A 1+00			64	35.6
A 1+40			66	35.4
A 1+12			65	35.5
B ₃ 0+55			68	35.2
B ₁ -1+10			132	28.8
B ₁ -1+02			110	310
B ₂ 0+40			50	370
B ₁ 0+72			100	320
	226	143.26	099	141.00
B ₈ 1+67			113	32.0
B ₇ 1+35			58	37.5
B ₇ 1+50			100	33.3
B ₆ 1+05			59	37.4
	1417	1417	1191	143.26
		1191		141.00
		226		226

143.26

B ₆ 1+20			7.2	136.1	
B ₅ 0+89			8.0	35.3	
B ₅ 1+05			9.7	33.6	
B ₄ 0+85			14.0	23.3	
	10.68	152.32	16.2	141.64	
B' ₈ 0+00			68	45.5	
B' ₈ 0+27			103	42.0	
B' ₇ 0+00			76	44.7	
B' ₆ 0+00			66	45.7	
B' ₆ 0+50			114	40.0	
B' ₅ 0+00			55	46.8	
B' ₄ 0+00			41	48.2	
B' ₄ 0+40			58	46.5	
B' ₃ 0+00			18	50.5	
B' ₂ 0+00			22	50.1	
B' ₃ 0+77			117	40.6	
B' ₄ 1+02			108	41.5	
	543	15136	6.39	145.93	
B' ₃ 0+54			58	45.6	681
B' ₁ 0+00			12	50.2	144.55
B' ₁ 0+15			4.0	47.4	6.81
A' ₁ 0+00			1.4	50.4	
B' ₁ 0+35			10.4	41.0	
B' ₂ 0+31			8.8	42.6	
	1611	15136			
	801	14326	8.01		
	√810	√8.10			

		151.36		
	0.53	139.36	12.53	138.83
B ₁₈ 1+00			7.5	31.9
B ₈ 2+02			14.0	25.4
B ₈ 1+50			10.6	28.8
B ₇ 1+80			10.7	28.7
B ₇ 1+50			10.5	28.9
B ₆ 1+00			3.4	36.0
B ₆ 1+50			5.0	34.4
B ₆ 2+00			10.1	29.3
B ₅ 1+50			3.1	36.3
B ^{10 up} B 1+10			10.8	28.6
B ₄ 1+32			3.1	36.3
B ₃ 1+04			7.1	32.3
B ₂ 0+57			4.7	34.7
B ₂ 0+80			13.7	25.7
B ₁ 0+65			11.1	28.3
	0.05	127.03	12.38	126.98
B ₂ 0+94			3.1	23.9
B ₂ 1+00			4.4	22.6
B ₂ 1+18			10.4	16.6
B ₃ 1+22			2.4	24.6
B ₁ 1+25			12.1	14.9
A 1+40			1.5	25.5
B ₅ 2+00			6.5	25.5
B ₆ 2+50			6.0	21.0
	0.58	151.36 127.03 24.33	24.91 5.0	

N.B.

	127.03		
B'7 2+75		112	115.8
B3 1+00		45	22.5
B'7-2+25		1.6	25.4
B3 1+12		50	22.0
B'8 2+00		58	21.2
B'8 2+50		5.1	21.9
B4 1+10		30	24.0
B'8 2+75		9.5	17.5
B4 1+35		103	16.7
B5 1+45		43	22.7
B6 1+76		63	20.7
B6 2+11		116	15.4
B'1 1+70		95	18.5
B7 2+43		150	14.0
B'1 1+95		18	25.0
B7 2+15		67	20.3
B'2 2+21		75	19.5
B8 2+40		90	18.0
B2 2+69	Bad (4 (222))	35	23.5
	1321	137.02	3.22
B'1 2+30		76	29.4
A'0 ③			39.0
B'1 3+10		132	29.8
B'1 3+60		109	26.7
	1321	137.02	
	322	127.03	
	✓ 9.99	✓ 9.99	

		137.02		
A' 1+25			33	133.7
A' 0+85			3.0	34.0
A' 0+60			28	31.2
A' 1+45			7.1	29.9
A' 1+90			55	31.5
A' 2+40			80	23.0
A' 2+76			22	34.8
A' 3+26			20	35.0
A' 3+40			7.8	29.2
B' 1.5+25			140	24.0
	143	125.24	1321	123.81
A' 3+57			80	17.2
B' 1.6+07			108	14.4
B' 1.5+75			94	15.8
B' 1.5+53			26	22.6
B' 1.5+00			90	16.2
B' 1.4+50			7.6	17.6
B' 1.4+00			47	20.5
B' 2.3+78			123	12.9
B' 2.3+29			50	20.2
B' 3.2+85			130	12.2
	070	113.16	1278	112.46
B' 1.1+30			46	086
B' 2+65			23	10.9
	213	137.02	2599	
		113.16	213	
		✓23.86	✓2386	

113.16

B ₈ 2+83	63	106.9
B ₈ 3+00	116	01.2
B'2 1+19	4.2	09.0
B'3 1+50	40	09.2
B'2 1+41	119	01.3
B'2 2+78	59	07.3
B ₆ 2+40	70	06.2
B ₅ 1+90	16	11.6
B'4 2+07	57	07.5
B'4 1+62	46	08.6
B ₃ 1+44	20	11.2
B ₃ 1+55	89	04.3
B'5 2+50	73	05.9
B'6 3+00	98	03.4
B'7 3+40	117	01.5
B'7 3+20	63	06.9
B'7 3+00	44	08.8
B'8 3+25	75	05.7
B ₃ 1+33	46	08.6
B ₂ 1+56	94	03.8
B ₂ 1+65	126	00.6
B'2 1+80	32	10.0
B'3 2+58	48	108.4
B'4 3+34	133	99.9

113.16

B'3 3+52		10.1	103.1
B'3 3+87		107	02.5
B1 1+71		132	100.0
BH + 56		85	104.7
BH + 46		1.6	11.6
A 1+40	②	1.0	112.2
A 1+60		1.8	111.4
A 1+79		140	99.2
B'2 4+06		4.1	109.1
B'2 4+48		115	01.7
B'2 4+78		117	01.5
B'2 5+06		124	00.8
B'2 5+36		66	06.6
B'2 5+70		9.0	04.2
B'2 6+00		104	02.8
B'4 4+00		75	105.7
B'1 6+50		136	99.6
	0.92	101.16	1292
			100.24
A 1+90		95	91.7
B 21+91		120	89.2
B' 6+37	B'2 ✓	27	98.5
B 3 2+05		122	89.0
B 3 1+47	1+74 Cor ✓	42	97.0
B 4 2+00		60	95.2

$$\begin{array}{r} 113.16 \\ 101.16 \\ \hline 12.00 \end{array}$$
 ✓ 12.00

B'2 8.8

= 174

101.16

B'35+97		10.5	90.7
B5 2+35		4.8	96.4
B7 3+13		6.0	95.2
B6 2+80		7.5	93.7
B'35+41		13.6	87.6
B'3 4+31		7.4	93.8
B'4 4+05		12.8	88.4
B'4 3+63		3.6	97.6
B'4 3+04		4.6	96.6
B'4-2+77		12.0	89.2
B'3-1+95		5.0	96.2
B'4-2+35		7.8	93.4
B'7-3+65		11.0	90.2
B'8-3+75		8.4	92.8
B'8 3+90		11.6	89.6
	049	88.71	1294
B'8 3+44		3.6	85.1
B'8 3+62		9.7	79.0
B'8 4+05		4.4	84.3
B'7 3+54		9.2	79.5
B'7 3+38		1.0	87.7
B'6 3+40		8.4	80.3
B'6 3+00		2.2	86.5
B'5 3+00		6.5	82.2

$\sqrt{101.16}$
 $\sqrt{88.71}$
 $\sqrt{1294}$

$\sqrt{1294}$
 $\sqrt{49}$
 $\sqrt{1245}$

	8871		
B'4-2+54		50	83.7
B6 3+40		126	76.1
B5 3+15		136	75.1
B5 3+35		73	81.4
B5 ^{10UP} 2+80		112	77.5
B'5 3+75		33	85.4
B'5 4+25		97	79.0
B5 2+89		77	81.0
B'5 4+50		148	73.9
B5 2+63		14	87.3
B4 2+92		20	86.7
B'4 4+77		00	88.7
B'4 4+81		92	79.5
B'3 5+01		20	86.7
B'8 7+40		105	78.2
B3 2+18		83	80.4
B'3 2+05		00	88.7
B'3 5+67		42	84.5
B2 2+00		90	79.7
B1 1+88		48	83.9
A1+98		124	76.3
B'2 6+54		14	87.3
B'1 6+85		42	84.5
1.53	77.69	1258	76.16

8871
7769
√1102

153
√1102

7769

B ² 7+01	00	77.7
B ⁸ 6+75	64	71.3
B ¹ 2+13	87	69.0
B ³ 7+39	100	67.7
B ⁸ 7+25	45	73.2
B ¹ 2+22	128	64.9
B ⁸ 7+80	23	75.4
B ³ 7+06	60	71.7
B ³ 2+36	45	73.2
B ³ 6+88	00	77.7
B ³ 2+52	98	67.9
B ⁴ 6+65	67	71.0
B ⁴ 2+65	56	72.1
B ⁵ 3+01	123	65.4
B ⁴ 6+21	122	65.5
B ⁶ 3+40	18	75.9
B ¹ 4-5+45	82	69.5
B ⁷ 3+89	62	71.5
B ⁵ 5+15	69	70.8
B ⁸ 3+81	79	69.8
B ⁵ 5+05	90	68.7
B ⁵ 4+90	31	74.6
B ⁶ 4+15	99	67.8
B ⁶ 3+65	113	66.4

77.69

B8 3+71

45

73.2

0.92

66.06

12.55

65.14

B7 4+15

45

61.6

B8 4+55

83

57.8

B8 4+65

120

54.1

B8 4+75

111

55.0

B7 4+50

140

52.1

B8 5+25

53

60.8

B8 5+75

77

58.4

B6 4+65

2.1

64.0

B8 6+25

67

59.4

B6 5+15

76

58.5

B8 4+26

118

54.3

B8 4+38

76

58.5

B7 4+34

10.0

56.0

B7 4+09

3.1

63.0

B7 6+5.

98

56.3

B6 5+55

120

54.1

B7 7+00

15

64.6

B'5-5+37

72

68.9

B'5-5+78

132

52.9

B'5 6+06

132

52.9

B'8-8+30

64

59.7

B'4 5+83

29

63.2

77.69
66.06
11.63

12.55
92
11.63

66.06

B'7-7+15			10.1	56.0
B6-3+80			28	63.3
B'6-3+92			107	55.4
B'4-7+04			4.0	62.1
B'4-7+44			4.0	62.1
B5. 3+48			114	54.7
B5 3+34			6.1	60.0
B4 2+80			113	54.8
B3 2+55			54	60.7
B2 2+31			50	61.1
B'4 7+72			103	55.8
B1-2+21			11.1	55.0
A-2+14			11.0	55.1
	2.63	55.71	12.98	53.08
B'7 5+00			4.5	51.2
B'3 7+53			09	54.8
B3 2+62			60	49.7
B'7 5+50			50	50.7
B'7 6+00			110	44.7
B'3 7+63			4.7	51.0
B'6 5+55			1.7	54.0
B'2 7+21			3.4	52.3
B4 3+00			5.6	50.1
B'5 7+95			8.4	47.3

66.06
 55.71
 10.35

12.98
 2.63
 10.35

55.71

B4-3+10		68	48.9
B5 7+64		123	43.4
B7-7+67		10.1	45.6
B5-7+33		4.1	51.6
B5-3+53		52	50.5
B8 8+80		103	45.4
B6 3+95		120	42.7
B7 3+33 4+30		00	55.7
B7 4+39		11.1	44.6
B8 4+52		93	46.4
B8 4+59		11.6	44.1
B5 6+66		14.4	41.3
B5 6+37		7.6	48.1
B'6 5+85		14.2	41.5
	1.02	43.67	13.06
B'6 6+35		7.5	36.2
B'4 8+15		34	40.3
B'6 7+85	B'6-7+85	60	37.7
B'5 8+46		28	40.9
B'6 7+35		60	37.6
B'6-7+85		10.1	33.6
B'7-8+15		89	35.4
B'7 8+65		136	30.1
B 8-9+30		71	36.6

X

+ = 4.34

103.6

3.52

X MB

55.71
43.67
√ 12.04

13.06
1.02
√ 12.04

20°
 94.15
 B
 1' huge

	43.67			
B'8-9+60		120	31.7	
B4-3+17		21	41.6	
B4-3+29		119	41.8	
B3-3+15		116	32.1	
B3 3+02		80	35.7	
B3 2+80		20	41.7	
B2 2+44		30	40.7	
B2 2+80		128	30.8	
B1 2+45		132	30.5	
H 2+26		87	35.5	
	014	31.58	1223	31.44
A 2+58		124	19.2	
B8 9+90		74	24.2	
B7 9+15		33	28.3	✓
B6 8+85		34	28.2	✓
B8-10+10		117	19.9	
B7 9+40		80	23.6	
B7 9+65		94	22.2	
B7 9+68		119	19.7	
B6 9+23		95	22.1	
B6 9+27		118	19.8	
B5 8+74		119	19.7	
B1 2+65		57	25.9	
B1 2+70		122	19.4	

\checkmark 43.67
 31.58
 \checkmark 12.09
 12.23
 1.6
 \checkmark 12.09

	31.58			
B ₂ 3+60		123	19.3	
B ₂ 2+99		106	20.0	
B ₃ 3+26		122	19.4	
B ₃ 3+16		87	22.9	
B ₄ 3+51		104	20.2	
B ₄ 3+52		123	19.3	
B ₅ 3+85		123	19.3	
B ₅ 3+80		83	23.3	
B ₅ 3+63		58	25.8	
B ₆ 4+05		118	19.8	
B ₆ 4+06		121	19.5	
B ₇ 4+60		119	19.7	
B ₇ 4+57		62	25.4	
B ₈ 4+69		67	25.9	
B ₈ 4+81		115	20.1	
B ₈ 4+86		120	19.6	
B ₄ 8+35		121	19.5	
	5.95	26.37	11.16	20.42
B'3 8+00		7.2	19.2	
B'2 7+53		6.8	19.6	
B'1 7+58		6.6	19.8	
A' 4+80		6.6	19.8	
B'2 7+34		2.0	24.4	

31.58	11.16
26.37	5.95
<u>15.21</u>	<u>5.21</u>

U.S.G.S

10

0.50	139.91	0	139.41
0.43	131.61	8.73	131.18
SP		{ 7.53	124.08
		{ 7.50	124.11
		{ 7.50	124.11

6.18	106.18		100.00 U.S.BM
1.59		1.59	104.59

Assume

11.27	111.27		100.00 U.S.BM
6.56		6.56	104.71

Assume

Average = 104.65

Av. HI 111.27
 104.71 Long sight to short sight Av. = 104.65
 = 104.59 Short " " long sight "

2.91 108.30
 ∴ 147.71 - 8.30 = 139.41 = U.S.G.S.B.M.
 referred to Otay Working Datum. =
 486.56

= 8.30 Below 147.71 Otay Working Datum = U.S.G.S.B.M.

U.S.G.S.B.M Otay Dam

B₂ Line Bedrock 7' below WS

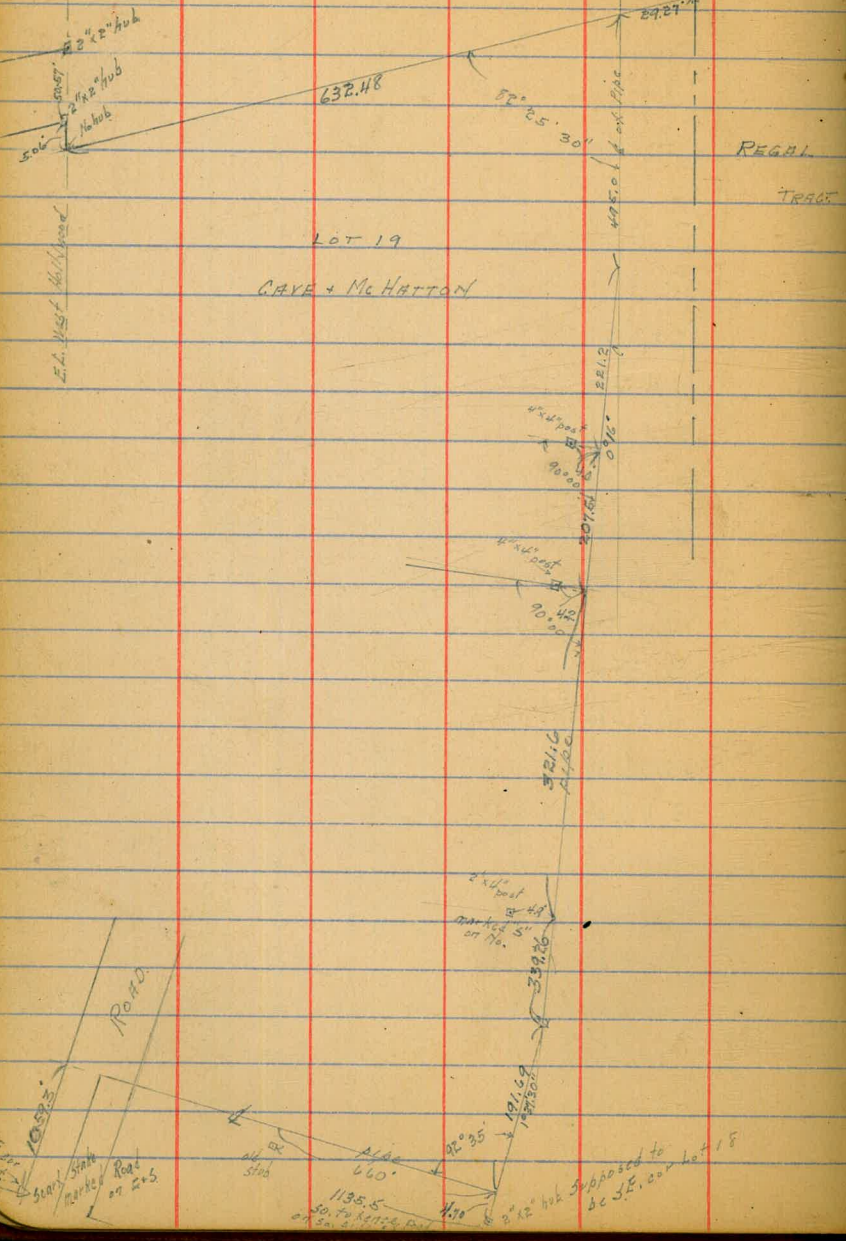
Sta 2+99 - N Bank

B ₃ Wine	"	11.3	"	"	Sta 8+17.0
"	"	12.0	"	"	8+50
"	"	12.0	"	"	8+65
B ₃	"	10.0	"	"	3+65
"	"	8.0	"	"	3+45
B ₁	"	7.7			3+40
A-6	"	9.0			3+40
A-6	"	10.9			3+60
A-6	"	10.0			3+80
A	"	10.0			3+80
A ₁	"	15.0	No bottom		3+60
A+5	"	16.0	"	"	3+60
B ₁		7.0	Bedrock		3+60
B ₂ +12		12.0	"		3+80
B ₂ +6		6.6	"		3+80
B ₂ +8		6.6	"		3+80
B ₂ +11.8		11.0	"		3+80
B ₂ +11.8		6.5	"		3+80 Upstream side of Concrete Plug
B ₂ +10.3		7.3			3+50 " " " "
B ₂ +12.0		10.0			3+50
A	Concrete	10.0			3+25
A+16.9		15.0	No Bottom		3+25 Downstream " " "

Gregory Moore Miller

Survey to Locate
Pipe Line
in Cave + McHattans Subd.
of Lot 144 Portion Lot 16
Ex Mission

2 1/2" Hub N.W.
Cave + McHattans
Tract



9/6/18
Gregory
Miller
Shaw

CROSS SECTION OF
STORK ST.
From N.L. County Highway
To S.L. Brooklyn Ave

60' Sta
15' obs
7.5' / 4's

BM	13.05	205.47		192.42	NW 63rd Ave
TP	5.16	207.85	0.78	207.69	
N.L. County Highway					
W			2.7	207.2	
cb			2.7	207.2	
1/4			2.6	207.3	
C			2.5	207.4	
1/4			2.4	207.5	
d			2.2	207.7	
E			2.2	207.7	

25' No. Taken parallel to last sect.

E			2.5	207.4	
cb			2.9	207.0	
1/4			3.0	206.9	
C			3.0	206.9	
1/4			3.1	206.8	
cb			3.3	206.6	
W			3.6	206.3	

31' No. Taken parallel to last

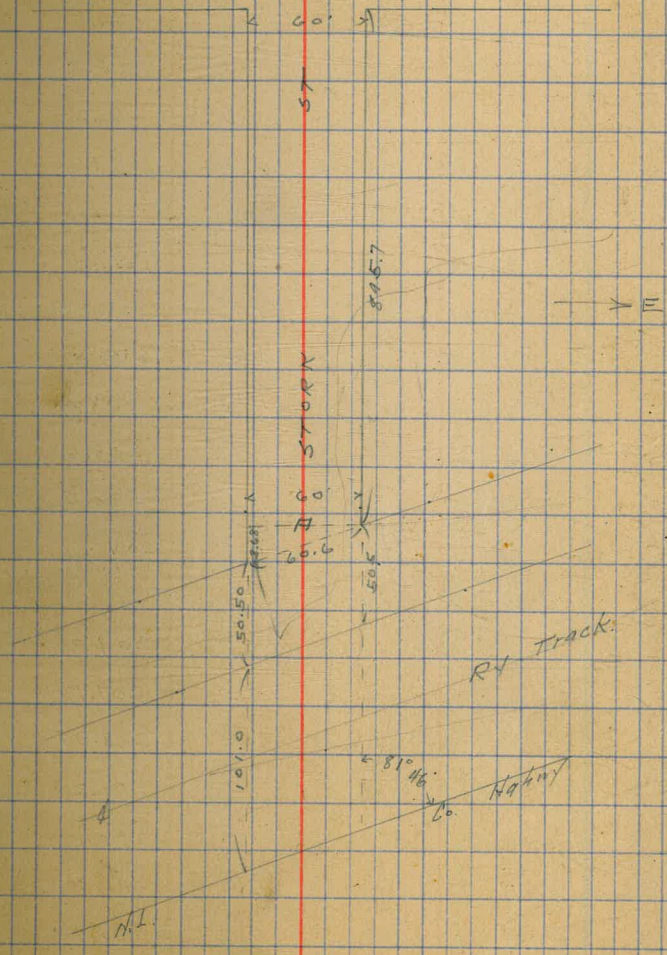
W			3.2	206.7	
cb			2.8	207.1	
1/4			2.3	207.6	
C			2.1	207.8	
1/4			2.0	207.9	
cb			1.9	208.0	

E
C
W

Co Highway

0.8	209.1
1.5	208.4
2.0	207.9

BROOKLYN 50' AVE



RV Track

81° 46' 00"

N.L.

209.85

E	1.7	208.2	
	31' No. of E } 36' - W } = 2' 30" of rail of siding		
E	1.7	208.2	
cb	1.6	208.3	
1/2	1.8	208.1	
C	1.9	208.0	
1/2	2.1	207.8	
cb	2.3	207.6	
W	2.3	207.6	
	55' No. of Co. Highway = No. 2' Line of R.R. to then parallel to RR Highway on rail		
W	2.0	207.9	
cb	1.9	208.0	
1/2	1.6	208.3	
C	1.5	208.4	
1/4	1.3	208.6	
cb	1.4	208.5	
E	0.6	209.3	
	58' No. of Highway + parallel to on rail		
E	0.7	209.2	
+8	2.0	207.9	
cb	1.9	208.0	
1/4	1.7	208.2	
C	1.8	208.1	
1/4	2.1	207.8	
cb	2.1	207.8	
W	2.4	207.5	

209.85

STARK

264

	65' No. of Highway + parallel to	
W	4.2	205.7
cb	4.0	205.9
1/2	4.1	205.8
C	4.0	205.9
1/2	4.0	205.9
cb	3.6	206.3
E	3.5	206.4
	101' No. of Highway + parallel to = 51' Atkin 50' 31' 10" cb	
E	4.9	205.0
cb	5.1	204.5
1/2	5.3	204.6
C	5.1	204.8
1/2	5.1	204.8
cb	5.2	204.7
W	5.3	204.6
+50	5.2	204.7
+100	5.7	204.2
	So. Curb parallel to SL.	
W	5.6	204.3
cb	5.8	204.1
1/4	6.1	203.8
C	6.2	203.7
1/4	6.2	203.7
cb	6.1	203.8
E	5.2	204.7

209.85

So. Quarter parallel to So L

E	6.8	203.1
cb	7.2	202.7
1/4	7.0	202.9
c	6.9	203.0
1/4	6.4	203.5
cb	5.9	204.0
W	6.4	203.5

6' No. of So 1/4 parallel to SL

W	6.6	203.3
cb	6.7	203.2
1/4	6.6	203.3
c	7.4	202.7
1/4	7.5	202.4
cb	7.7	202.2
E	7.8	202.1

Center AKin

E	8.0	201.9
cb	7.9	202.0
1/4	7.8	202.1
c	7.3	202.6
1/4	7.2	202.7
cb	7.0	202.9
W	9.3	200.6
+15	6.4	203.5

STARK

277

209.85

No. Quarter

-27	6.9	203.0	
-19	19.0	190.9	= crack
W	18.2	191.7	= ✓
cb	15.3	194.6	= ✓
+3	12.3	197.6	
1/4	12.0	197.9	
c	9.6	200.3	
+4	8.3	201.6	
1/4	8.6	201.3	
cb	8.6	201.3	
E	8.2	201.7	
+50	7.3	202.6	= ch. road
1400	6.8	203.1	+ ✓

No. Corb

E	9.0	200.9	
cb	9.8	200.1	
1/4	10.0	199.9	
c	12.3	197.6	
1/4	16.2	193.7	= crack
cb	16.4	193.5	= ✓
W	19.0	190.9	= ✓
+20	18.8	191.1	= ✓

No. Line AKin

-20	14.9	195.0	
W	15.4	194.5	

209.85

+11			15.5	194.4	= creek
cb			16.7	193.2	= ✓
1/4			16.2	193.7	= ✓
o			16.4	193.5	= - bank
1/4			12.9	197.0	
+2			10.9	199.0	Top bank
cb			10.6	199.3	
+11			10.1	199.8	
E			9.2	200.7	= ground
E			8.2	201.7	end of = cement walk which runs out
E	868' No. on W 00 - - E	Section A = first section at right angles to st.	9.2	200.7	
+11			10.1	199.8	
cb			10.6	199.3	
1/4			11.7	198.2	
+1			11.6	198.3	sq. corner = 0/100
T.P.	2.83	20109	11.59	198.26	
+1.5			6.9	194.2	
o			8.1	193.0	
1/4			7.9	193.2	
cb			8.0	193.1	
+5			7.7	193.4	
+6			5.3	195.8	
W			4.6	196.5	

STORK

28
29

201.09

					7' 1/2" oX "A"
				W	4.8 196.3
				+11	4.3 196.8
				+13	6.9 194.2
				cb	7.1 193.7 = creek
				1/4	7.1 193.7
				C	7.9 193.2 = SW edge bridge
				1/4	8.2 192.9
				+5.5	8.5 192.6 = creek
				cb	2.7 198.4 = SE edge bridge
				E	2.4 198.7
				E	0.8 200.3
					14' No.
				E	1.5 199.6
				+7.5	2.3 198.8 = bank hole
				cb	7.9 193.2 = creek
				1/4	7.9 193.2 = creek
				C	7.9 193.2 =
				+3	7.2 193.9 = edge
				+4	2.8 198.3 = NW edge
				+5	2.8 198.3
				1/4	3.3 197.8
				cb	6.3 194.8
				cb	7.1 194.0
				+1	4.5 196.6
				W	4.9 196.2
				W	4.7 196.4
					17' No.

201.09

STORM

2929

201.09

+13	41	197.0	
cb	51	196.0	
+14	62	194.9	
	3.8	197.3	
1/4	3.5	197.6	
C	27	198.4	= N.W. edge bridge
+2	2.6	198.5	= top
1/4	8.3	192.8	
cb	7.9	193.2	
+8.5	7.1	193.7	
	2.5	198.6	
E	23	198.8	
	22	No.	
E	3.2	197.9	
+5.7	2.5	198.6	top bank
	7.4	192.7	bot. creek
cb	8.2	192.9	
1/4	6.5	194.6	
	2.6	198.5	= N.W. cor. bridge
C	2.7	198.4	
1/4	3.3	197.8	
cb	4.7	196.4	
+2	4.1	197.0	
W	4.7	196.4	
	27	No.	
W	4.3	196.8	
+13	4.0	197.1	
cb	5.2	195.9	
1/4	3.4	197.7	

C	2.9	198.2	
+5	2.7	198.4	
1/4	4.3	196.8	
+1	6.5	194.6	
cb	7.9	193.2	
+10	7.2	193.9	
E	5.3	195.8	= top bank
	4.4	196.7	
	50	No.	
F	4.6	196.5	
+3	5.3	195.8	top bank
+5	6.9	194.2	bottom
cb	7.4	193.7	
+2	7.2	193.9	bottom
+3	3.9	197.2	top
1/4	4.0	197.1	
C	3.9	197.2	
1/4	4.1	197.0	
cb	4.8	196.3	
W	4.9	196.2	
	100	No.	
W	3.8	197.3	
cb	4.1	197.0	
1/4	3.8	197.3	
C	3.5	197.6	
1/4	3.3	197.8	
+4	3.6	197.5	top bank

201.09

+5	63	194.8	bottom
cb	69	194.2	
+5	68	194.3	
+10	53	195.8	
E	29	198.2	

130' No.

E	31	197.7	
+7	56	195.5	
cb	62	194.9	
+1/2	58	195.3	bottom
1/2	31	198.0	top
c	31	198.1	
1/2	31	197.7	
cb	37	197.4	
W	44	196.7	

142' No.

W	42	196.9	
cb	36	197.5	
1/2	30	198.1	
c	30	198.1	
1/2	31	197.7	
cb	61	195.0	
+7	63	194.8	
E	54	195.7	

175' No.

E	53	195.8	
---	----	-------	--

E bank of st.
turns toward
East here

STARK

30³⁰

201.09

53	195.8	bottom
27	198.4	top
25	198.6	
23	198.8	
28	198.3	
31	198.0	

181' No. west bank angle east.

W	30	198.1	
cb	29	198.2	
1/2	22	198.9	
c	23	198.8	
1/2	22	198.9	
cb	2.5	198.6	use this for forward sect.
	4.8	196.3	back
E	19	199.2	use this for forward sect.
	5.2	195.9	back

210' No.

E	1.5	199.6	
cb	1.9	199.2	
1/2	1.5	199.6	
c	1.8	199.3	
1/2	1.5	199.6	
cb	2.0	199.1	
W	2.5	198.6	

235' No.

0.8	200.3	
-----	-------	--

201.09

db		1.1	200.0
1/4		1.0	200.1
C		1.0	200.1
1/4		1.0	200.1
db		1.1	200.0
E		1.0	200.1
T.P.	11.91	21229	0.71 20038 ✓

300' No

E		9.0	203.3
+4		9.5	202.8
db		9.8	202.5
1/4		9.4	202.9
C		9.6	202.7
1/4		10.0	202.3
db		10.2	202.1
W		10.1	202.2

340' No

W		8.7	203.6
db		8.3	204.0
1/4		8.0	204.3
C		7.8	204.5
1/4		7.7	204.6
db		7.9	204.4
E		7.5	204.8

370' No

E		5.6	206.7
---	--	-----	-------

STORK

313

212.29

+9		60	206.3
db		59	206.4
1/4		57	206.6
C		58	206.5
1/4		60	206.3
db		65	205.8
W		66	205.7

400' No

W		37	208.6
db		33	209.0
1/4		31	209.2
C		27	209.6
1/4		27	209.6
db		31	209.2
E		27	209.6

12.24 224.05

435' No

T.P.	12.24	224.05	0.48	211.81 ✓
E		10.6		213.5
+7		11.5		212.6
db		10.3		213.8
1/4		9.9		214.2
C		9.9		214.4
1/4		10.0		214.1
db		10.3		213.8
W		10.8		213.3

22405

465' No

W	4.0	220.1
df	4.4	219.7
+1	5.1	219.0
3/4	5.1	219.0
c	5.0	219.1
1/2	5.2	218.9
df	4.7	219.4
+2	4.6	219.5
+7	6.1	218.0
F	6.0	218.1

480' No

E	1.6	222.5	drive to base	
df	3.0	221.1		
1/4	2.4	221.7		
c	2.3	221.8		
1/2	2.4	221.7		
+4	2.5	221.6		
df	1.3	222.8		
W.	0.2	223.9		
T.P.	11.98	235.28	0.75	223.30

510' No

W	5.1	229.9
df	6.3	229.0
+2	8.3	227.0
1/2	8.5	226.8

235.28

STORK

2232

c	8.5	226.8
1/2	8.4	226.9
df	8.7	226.6
+0.5	8.0	227.3
F	7.8	227.5

545' No

F	1.0	234.3		
df	1.3	234.0		
+1	2.9	232.4		
1/4	3.1	232.2		
c	2.8	232.5		
1/2	2.9	232.4		
+5	2.9	232.4		
df	0.8	234.5		
W	0.5	234.8		
T.P.	12.43	247.51	0.50	234.78

600' No

W.	6.9	240.2	drive to base
+10	7.0	240.2	
df	7.9	239.3	
+2	9.0	238.2	
1/4	8.6	238.6	
c	8.4	238.8	
1/2	8.6	238.6	
df	9.0	238.2	
+2	7.8	239.4	
F	7.9	239.3	

247.21

650' No

E	30	244.2
cb	32	244.0
1/4	32	244.0
c	30	244.2
1/2	34	243.8
+6	37	243.5
cb	22	245.0
W	19	245.3
T.P.	12.60	259.80

700' No.

W	9.6	250.2
cb	10.1	249.7
1/4	10.4	249.4
c	10.2	249.6
1/4	10.4	249.4
cb	10.4	249.4
E	10.2	249.6

760' No.

E	45	255.3
+13	41	255.7
cb	48	255.0
1/4	42	255.6
c	46	255.2
1/4	50	254.8
+5.5	55	254.3

259.80

STORK

37.33

cb	48	255.0
W	38	256.0
800' No		
W	1.0	258.8
cb	1.0	258.8
+1	1.8	258.0
1/4	1.4	258.4
c	1.2	258.6
1/2	1.5	258.3
cb	2.0	257.8
E	1.8	258.0

T.P. 12.92 242.34 0.38 259.42

850' No

E	10.1	262.2
cb	10.3	261.8
1/4	10.1	262.2
c	10.0	262.3
1/4	10.4	261.9
+6	10.7	261.6
cb	9.8	262.5
W	9.6	262.7

895.7' No = 5L. Brook Hwy

-500	4.1	265.2
-100	6.9	265.4
W	6.2	266.1

ob	66	265.7
1/4	67	265.6
C	65	265.8
1/4	66	265.7
ob	68	265.5
E	66	265.7
+70	8.0	264.3
+130	11.1	261.2
+180	15.0	257.3

Center Brooklyn

-180	11.9	260.4
-130	7.5	264.8
-70	4.8	267.5
E	4.3	268.0
C	4.4	267.9
W	4.4	267.9
+100	5.0	267.3
+200	4.4	267.9

North Line Brooklyn

-		
-200	1.6	270.7
-100	3.1	269.2
W	2.6	269.7
C	2.4	269.9
E	2.8	269.5

+70	3.7	268.6
+130	6.3	266.0
+180	10.4	261.9
CHK	0.65	271.69

30. 637.0 Brook
= 271.75

10/15/18 Eraper Miller

Levels on
43rd St 60' wide
from Market to
Almond St.

11/1/17 1000
Post 60' 30' ok
52 12.140
Back 1004-11

B.M.	12.81	134.81	132.00
0+00 Center of Market St see book 1004 0092.11			
E		11.0	123.8
C		10.5	124.3
W		10.0	124.8
+10 = N.E. Market St.			
W		8.1	126.7
C		8.5	126.3
E		10.7	124.1
+100 No. of G			
E		10.8	124.0
C		9.1	125.7
W		7.7	127.1
+150 No. of G			
W		7.5	127.3
C		8.6	126.2
E		10.0	124.8
+200			
E		7.7	127.1
C		7.4	127.4
W		5.9	128.9
+250			
W		4.2	130.6
C		5.3	129.5

E	6.4	128.4
3+00		
E	5.2	129.6
C	3.2	131.6
W	2.9	131.9
3+50		
W	2.7	132.1
C	3.6	131.2
E	4.1	130.7
3+70		
E	2.7	132.1
C	2.3	132.5
W	1.1	133.7
4+00		
W	1.4	133.4
C	2.3	132.5
E	3.9	130.9
4+30		
E	4.7	130.1
C	1.4	133.6
W	1.2	133.6
4+50		
W	0.5	134.3
C	2.6	132.2
E	5.8	129.0

13481

5+00

E	6.2	128.6
C	5.2	129.6
W	2.4	132.4

5+35

W	2.9	131.9
C	2.9	131.9
E	6.2	128.6

T.P.	12.88	11/200	5.60	129.21
------	-------	--------	------	--------

5+60

E	12.8	129.3
C	11.3	130.8
W	9.4	132.7

6+00

W	7.4	132.7
C	10.1	132.0
E	11.9	130.4

6+10

E	11.3	130.5
C	8.4	133.7
W	8.1	132.0

6+30

W	9.5	132.6
C	8.1	132.0
E	11.5	130.6

13482 5+ 364

6+50

E	11.4	130.7
C	10.4	131.7
W	9.1	133.0

6+74 (S.L. E 5+)

W	8.4	133.7
C	9.9	132.2
E	10.3	131.8

7+00

E	9.8	132.3
C	9.2	132.9
W	8.4	133.7

7+30

W	8.7	133.4
C	9.3	132.8
E	9.9	132.2

7+50

E	9.7	132.4
C	9.3	132.8
W	8.8	133.3

8+00

W	8.7	133.4
C	9.3	132.8
E	10.5	131.6

14209

8+50

E	9.5	132.6
C	9.3	132.8
(+15.)	(7.7)	134.4 = ctr grade
W	8.3	133.8

9+00

W	7.4	134.4
(+15)	(6.8)	= ctr grade
C	7.4	134.4
F	6.7	135.4

9+50

E	3.4	138.4
C	4.8	137.3
(+15)	(5.2)	ctr grade
W	5.5	136.6

10+00

W	3.9	138.2
C	3.0	139.1
E	1.4	140.9

10+50

E	0.8	141.3
C	1.8	140.3
(+15)	(1.9)	ctr grade
W	2.9	139.2

13rd St 377

11+00

W	1.3	140.5
T.P.	12.50	153.64
C	0.95	141.14
E	12.6	141.0
E	12.1	141.5

11+50

E	11.8	142.3
C	11.5	142.1
W	11.0	142.6

12+00

W	9.2	144.4
C	9.5	144.1
E	9.2	144.4

12+50

E	6.6	147.0
C	6.4	147.4
W	5.6	148.0

12+958

W	2.6	151.0
C	2.5	151.1
E	2.5	151.1
T.P.	10.45	163.76
	0.63	153.01

(S.L. H/170116)

 Nord
 443

10/15/18 Gregory Miller Levels on Almond St 50 wide from 43rd East 2000 ft. No. Line is 5' So. of So. Line Marietta or 5' 13 25' on each side of Pueblo Ave.

BM	10.75	163.76	153	153.01	Max elev Almond = 43		4400	
		11 L. 43 rd St.				S	4.1	159.7
						C	3.0	160.8
So.		12.8		151.0		N	1.8	162.0
C		9.7		154.1				
N		8.3		155.5			3+00	
		0+75 43 rd St = 0+00				N	3.6	160.2
N		7.2		156.6		C	4.4	158.9
C		10.2		153.6		S	5.9	157.9
S		12.7		151.1			3+50	
		0+30 (E.L. 43 rd)				S	6.9	156.9
S		12.7		151.1		C	6.0	157.8
C		10.1		153.7		N	5.4	158.4
N		8.4		155.4			4+00	
		0+75 from d 43				N	6.0	159.8
N		9.0		154.8		C	6.6	157.2
C		9.6		154.2		S	8.3	155.5
S		12.1		151.7			4+50	
		1+30 from d 43				S	8.3	155.5
S		9.6		154.2		C	7.0	156.8
C		7.7		156.1		N	6.4	157.4
N		6.9		156.9			5+00	
		1+90 from d 43				N	6.4	157.4
N		2.1		161.7		C	7.5	156.3
C		3.7		160.1		S	8.3	155.5
S		3.5		160.3				

163.76

5+50

S	9.2	154.6
C	8.6	155.2
N	9.0	154.8

6+00

N	9.6	154.2
C	9.7	154.1
S	10.1	153.7

6+50

S	9.8	154.0
C	9.5	154.3
N	8.8	155.0

6+80

N	8.7	155.1
C	8.8	155.0
S	8.9	154.9

7+20

S	10.9	152.9
C	10.6	153.2
N	9.8	154.0

8+00

N	9.6	154.2
C	10.4	153.4
S	11.4	152.4

Almond

39

8+50

S	10.7	153.1
C	9.9	154.1
N	8.6	155.2

9+00

N	7.2	156.6
C	8.2	155.6
S	9.9	153.9

9+50

S	9.0	154.8
C	7.5	156.3
N	6.9	156.9

TP	10 W	168.74	7.23	156.53
----	------	--------	------	--------

10+00

N	9.9	158.8
C	11.2	157.3
S	13.1	155.6

10+50

S	11.9	156.8
C	10.2	158.5
N	8.9	159.8

11+00

N	7.8	160.9
C	8.6	160.1
S	10.2	158.5

16874

11+50

S	7.9	160.8
C	6.3	162.1
N	5.8	162.9

12+00

N	3.5	165.2
C	4.1	166.6
S	5.1	163.6

12+50

S	4.2	164.5
C	2.4	166.3
N	1.9	166.8

13+00

N	1.5	167.2	
C	2.6	166.1	
S	3.7	165.0	
TP	4.52	169.78	
		3.48	165.26

13+63

S	6.0	163.8
C	4.3	165.5
N	2.9	166.2

14+13

N	3.1	166.7
C	3.9	165.9
S	5.3	164.5

Almond

400

14+63

S	5.0	164.8
C	4.0	165.8
N	3.5	166.3

15+13

N	4.7	165.1
C	5.6	164.2
S	5.9	163.9

15+33

S	7.9	161.9
C	6.1	163.7
N	5.5	164.3

15+63

N	5.1	164.4
C	5.9	163.9
S	6.5	163.3

16+13

S	4.5	165.3
C	4.0	165.8
N	3.7	166.1

16+63

N	1.6	168.2
C	1.6	168.2
S	2.1	169.7

169.78

Almond 41

T.P.	7.82	177.15	0.15	169.33
		17+13		
S			6.1	171.1
C			5.7	171.5
N			5.7	171.5
		17+63		
N			3.1	174.1
C			4.1	173.1
S			5.0	172.2
		18+13		
S			4.0	173.2
C			3.2	174.0
N			1.7	175.5
		18+63		
N			1.2	176.0
C			2.9	174.3
S			3.5	173.7
		19+13		
S			3.1	173.8
C			3.7	173.5
N			2.8	174.4
		19+63		
N			7.6	169.6
C			7.5	169.7
S			7.3	169.9

				20+13			
					S	12.4	164.8
					C	11.3	165.9
					N	11.0	166.2
					T.P.	12.5	165.79
						12.61	164.54
						20+63	
					N	3.4	162.4
					C	3.6	162.2
					S	4.1	161.7
						21+13	
					S	7.2	158.6
					C	6.5	159.3
					N	5.7	160.1
						21+63	
					N	4.8	161.0
					C	5.8	160.0
					S	7.2	158.6
						22+13	
					S	5.8	160.0
					C	5.5	160.5
					N	4.7	161.1
						22+53	
					N	3.4	162.4
					C	4.3	161.5
					S	4.6	161.2

165.79

22+93

S	3.1	1627
C	33	1625
N	1.5	1643

23+13

N	2.3	1635
C	32	1626
S	28	1630

23+63

S	23	1635
C	32	1626
N	1.9	1637

24+03

N	3.2	1626
C	40	1618
S	37	1621

24+33

S	8.1	1597
C	61	1597
N	58	1600

24+58

N	78	1580
C	9.9	155.9
S	11.4	156.4

Almond

42

24+80

S	10.6	155.2
C	11.3	154.5
N	10.2	155.6

25+08

N	10.2	155.6
C	9.2	156.6
S	9.6	156.2

25+53

S	48	1610
C	78	1580
N	90	156.8

25+73

N	80	157.8
C	7.2	158.6
S	61	159.7

26+23 (W.L. Magnolia)

S	23	163.5
C	50	160.5
N	66	159.2

26+53 = (Magnolia) see book 1021-1029

N	2.7	163.1
C	2.56	163.23 Mod
S	1.3	164.5

Gregory
Miller
Shaw

CROSS-SECTION OF
CONGRESS ST. 50' ST 10' walks
from S.L. Mason St to
Santa Fe Ry

B.M.	1.42	24.00	27.60	S.W. Mason & San Diego Spk			
		S.L. TAYLOR ST 50' wide			1/2	55	185
E		50	190		C	53	187
cb		52	186		1/2	54	186
+4		57	183		+4.5	58	182
1/2		53	187		cb	56	184
C		51	189		+2	53	187
1/2		51	189		W	48	192
+5		56	184				
cb		51	189		Center		
W		48	192		W	49	191
		So. Curb.			+8	53	187
W		47	193		cb	56	184
+7		49	191		+3	59	181
cb		54	186		1/2	55	185
+2.5		58	182		C	54	186
1/2		53	187		1/4	56	184
C		52	188		+3	59	181
1/4		54	186		cb	57	183
+5		57	183		E	52	188
cb		55	185				
E		50	190		No 1/4		
		So 1/4			E	54	188
E		52	188		cb	59	181
cb		55	185		1/4	58	182
+2.5		59	181		C	54	185
					1/4	56	184
					+3	60	180
					cb	56	184

2402

CONGRESS 1.144

W	50	19.0
No. Curb		
W	50	19.0
ob	57	18.3
+4	60	18.0
1/4	57	18.3
c	55	18.5
1/4	59	18.1
ob	59	18.1
E	52	18.8
No. Line Mason St.		
E	52	18.8
ob	59	18.1
1/4	60	18.0
c	56	18.4
1/4	58	18.2
+5	62	17.8
ob	58	18.2
W	51	18.9
50' No.		
W	58	18.2
ob	65	17.5
+3	68	17.2
1/4	65	17.5
c	64	17.8
1/4	66	17.4

ob	64	17.6
E	58	18.2
100' No.		
E	63	17.7
ob	71	16.9
1/4	70	17.0
c	68	17.2
1/4	71	16.9
+6	73	16.7
ob	68	17.2
W	64	17.6
150' No.		
W	72	16.8
ob	74	16.6
+2	76	16.4
1/4	75	16.5
c	73	16.7
1/4	77	16.3
ob	76	16.4
E	71	16.9
200' No.		
E	77	16.3
ob	82	15.8
1/4	82	15.8
c	80	16.0
1/4	81	15.9

24.02

CONGRESS

23

+6	84	156
cb	79	161
W	76	164

250' No

W	84	156
cb	88	152
+1.5	91	149
1/4	88	152
C	87	153
1/4	89	151
+3	91	149
cb	87	153
E	83	157

300' No = 6L of SMITH ST 50' wide

E	85	155
cb	90	150
1/4	95	145
C	92	148
1/4	93	147
cb	98	142
+3	91	149
W	91	149

30 Curb

W	11.1	129
cb	9.9	141
1/4	9.3	147

E	94	146
1/4	98	142
cb	94	146
E	85	157

So. Quarter

E	85	155
cb	96	144
1/4	99	141
C	97	143
1/4	96	144
cb	99	141
W	109	131

Center

W	12.0	120
cb	98	142
1/4	10.0	140
C	99	141
1/4	10.2	138
cb	10.0	140
E	87	153

No. Quarter

E	87	153
cb	10.0	140
+2.5	10.6	134
1/4	10.1	139
C	10.1	139

1/2			10.1	13.9
cb			10.8	13.2
W			13.5	10.5
T.P.	323	16.01	11.24	12.78
		No. Carb		
W			6.2	9.8
cb			3.2	12.8
1/4			2.3	13.7
C.			2.3	13.7
1/4			2.4	13.6
+5			3.1	12.9
cb			1.9	14.1
E			1.1	14.9
		No. Lino SMITH	5T	
E			1.2	14.8
+1			1.0	15.0
+2			1.6	14.4
cb			2.4	13.6
+2.5			3.3	12.7
1/4			4.6	13.2
C.			2.7	13.3
1/4			2.7	13.3
cb			4.0	12.0
W			7.1	8.9

		40' No		
W			9.4	6.6
cb			8.0	8.0
1/2			5.6	10.4
C			5.5	10.5
1/4			5.5	10.5
+5			5.4	10.8
cb			4.5	11.5
+7			3.7	12.3
+8			3.0	13.0
E			2.9	13.1
		80' No		
E			10.7	5.3
cb			10.4	5.6
1/4			10.4	5.6
C			11.0	5.0
1/4			11.7	4.3
cb			12.3	3.7
W			12.3	1.7
+10			14.2	1.8
		95' No		
-10			14.7	1.3
W			14.6	1.4
cb			14.1	1.9
1/4			13.5	2.5
C.			12.5	3.5

1/4			11.8	4.2
cb			11.6	4.1
E			11.8	4.2
T.P.	2.22	5.67	12.56	3.45
		117' No		

E			2.0	3.7
cb			3.3	2.4
1/4			3.2	2.3
C			3.5	2.2
1/4			3.9	1.8
cb			4.4	1.3
W			4.8	0.9
+10			5.0	0.7

Colvert needed here. 128' No.

-10			4.9	0.8
W			4.9	0.8
cb			4.4	1.3
1/4			4.0	1.7
cb			3.8	1.9
1/4			3.8	1.9
cb			4.1	1.6
E			4.3	1.4

175.14' No. = 5L Wallace St 25 wide

E			4.6	1.1
cb			4.6	1.1
1/4			4.6	1.1

C			4.6	1.1
1/4			4.6	1.2
cb			4.6	1.1
W			4.6	1.1
+10			4.8	0.9

12.5' No = cb Wallace

-10			4.8	0.9
W			4.7	1.0
cb			4.7	1.0
1/4			4.7	1.0
C			4.8	0.9
1/4			4.6	1.1
cb			4.5	1.2
E			4.2	1.5

No L. Wallace

E			4.3	1.1
cb			4.4	1.3
1/4			4.5	1.2
C			4.5	1.2
1/4			4.4	1.3
cb			4.5	1.2
W			4.7	1.0
+10			4.8	0.9

50' No.

-10			6.0	-0.3
W			6.0	-0.3

567

ab	57	00
1/4	56	01
C	56	01
1/4	51	06
ab	49	08
E	50	07

74.06 No. 2 SECT. A

E	51	06
ab	52	05
1/4	55	02
C	60	-07
1/4	67	-10
ab	68	-11
W	67	-10
W	67	-10
W	67	-10

25.1 No. of A = SECT B

W	62	-05
ab	68	-11
1/4	69	-12
C	69	-12
1/4	68	-11
ab	58	-01
E	57	00

25.1 No. of B = C

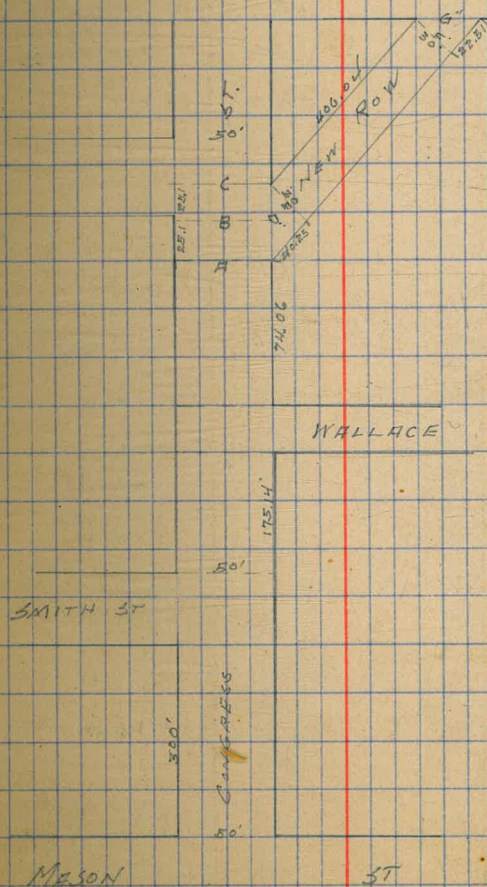
E	63	-06
ab	70	-13
1/4	70	-13

CONGRESS

48

C	78	-21
1/4	65	-08
ab	51	06
W	21	36

TAYLOR ST.



W. Gregory

CROSS SECTION OF
Road Thru Bldg 407 30' wide
Old Town
567 HI from Page 48

SECT D see page 48

N			6.3	-0.6
C			5.7	0.0
S			5.1	0.6
T.P.	6.48	6.71	5.4	0.23

SECT E

S			6.6	0.1
C			6.7	0.0
N			7.1	-0.4

50' E of E

N			6.3	0.4
C			6.5	0.2
S			6.6	0.1

100' E

S			6.6	0.1
C			6.5	0.2
N			6.5	0.2

150' E

N			6.5	0.2
C			6.6	0.1
S			6.3	0.4

200' E

S			5.9	0.8
C			5.8	0.9
N			5.4	1.3

250' E

N			4.6	2.1
C			5.1	1.6
S			5.2	1.5

300' E

S			4.9	1.8
C			4.9	1.8
N			4.5	2.2

350' E

N			4.4	2.3
C			4.4	2.3
S			4.9	1.8

370' E

S			5.3	1.4
C			4.6	2.1
N			5.7	1.0

385' E

N			4.3	2.4
C			4.8	1.9
S			5.2	1.5

406.04 E = SECT F

S			5.0	1.7
C			5.1	1.6
N			4.9	1.8

SECT G = S.L. TAYLOR ST

N			4.9	1.8
---	--	--	-----	-----

6.71

2

5.0

17

3

5.3

14

50⁰⁰

W. H. Gregory

CROSS SECTION OF
INTERSECTION OF SANDIEGO AVE
TAYLOR ST 974 ROAD ON
PRECEDING PAGE

6.71

SECT H. see page 45

So	4.9	1.8
+ 35	6.2	0.5
+ 50	6.7	0.0
+ 65	4.8	1.9
+ 80	2.0	4.7

Top of Sandiego
Dump

SECT I

No. Line Taylor	2.1	4.6
+ 8	4.2	2.5
+ 35	5.7	1.0
+ 50 = C	5.9	0.8
+ 65	4.7	2.0
+ 100 = S.L.	5.0	1.7

SECT J

S.L. of Taylor	5.3	1.4
+ 35	5.2	1.5
+ 50 = C	5.4	1.3
+ 65	5.8	0.9
+ 100 = N.L. Taylor	5.7	1.0

19.0' W of Ctr SANDIEGO AVE = Top of

N.L. Taylor	5.3	1.4
+ 35	4.7	2.0
+ 50 = C	4.5	2.2
+ 65	4.5	2.2

LA Jolla
Dump

+100 = S.L. Taylor 4.7 2.0

10.0' W of Ctr of SANDIEGO AVE = West side of Top
of LA Jolla
Dump

S.L. Taylor	1.1	5.6
+ 35	1.6	5.1
+ 50 = C	2.0	4.7
+ 65	2.3	4.2
+ 100 = N.L.	2.2	4.5

Ctr of SANDIEGO AVE

N.L. Taylor	1.2	5.5
+ 35	1.2	5.5
+ 50 = C	1.1	5.6
+ 65	0.9	5.8
+ 100 = S.L.	0.6	6.1

6' E of Ctr of SANDIEGO = E side of LA Jolla Dump

S.L. Taylor	1.3	5.4
+ 35	1.6	5.1
+ 50 = C	1.3	5.4
+ 65	2.1	4.6
+ 100 = N.L.	2.1	4.6

13' E of Ctr of S. D Ave = Top of Dump

N.L.	6.1	0.6
+ 35	5.8	0.9
+ 50	5.7	1.0
+ 65	5.9	0.8
+ 100 = S.L.	5.7	1.0

T.P. 10.93

17.47

0.17

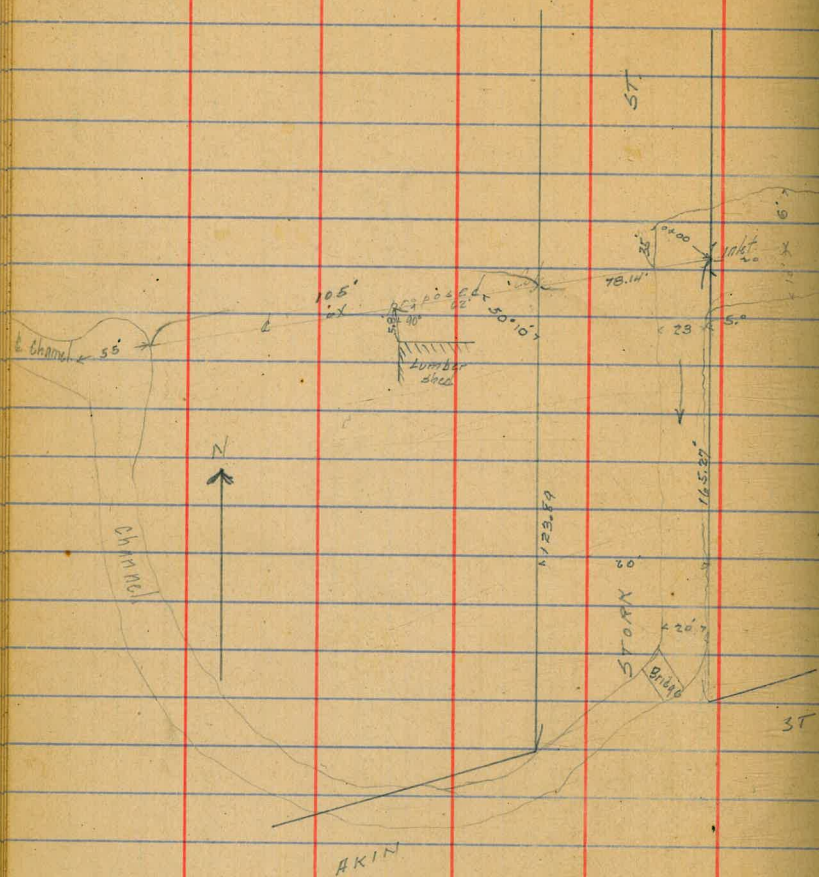
6.54

T.P.	10.93	17.47	0.17	6.54
T.P.	9.08	23.56	0.99	14.44
			0.97	25.59
			1.41	54.54
				5.00

54.54 S.D
+ Mass 57

3/5/19 Gregory
Miller
Span

LOCATION OF
CULVERT ON STORK ST
AND CROSS SECTION OF SAME



CROSS SECTION OF
PROPOSED CULVERT

Drainage Area
4.7 Sq Mi

52

CAPACITY OF CREEK ABOVE INLET = 400'

Distance from Inlet	Width	Depth	Area	Notes
9.37	20.179		192.42	NW 63rd
		4.0	199.39	NE Stork
		20' E of Inlet		
	6' No. of d	2.4	199.4	Top bank
	5.8	5.8	196.0	Bottom
		5.7	196.1	
	10' So. of d	5.6	196.2	
		10' E of Inlet		
	10' So. of d	5.6	196.2	
		6.1	195.7	
	10' No. of d	5.6	196.2	
	11'	5.4	196.4	= bank
	0+00			
	10' No. of d	5.9	195.9	
		6.9	194.9	
	10' So. of d	6.5	195.3	
	0+17			
	10' So. of d	6.8	195.0	
		6.6	195.2	
	10' No. of d	5.5	196.3	
	0+24			
	10' No. of d	3.5	198.5	Top bank
		6.1	195.7	Bottom
	10' So. of d	6.7	195.1	

0+33			1+50				
10' 30" of d	6.0	195.8	bottom bank	10' 30" of d	5.0	196.2	
d	3.9	197.9	TOP	d	4.7	196.5	
10' No. of d	3.5	198.3	✓	10' No. of d	4.7	196.5	
0+40			1+52				
10' No. of d	3.6	198.2		10' No. of d	5.5	195.7	
d	3.6	198.2		d	5.6	195.6	Top Bank
10' 30" of d	3.7	198.1	Top Bank	10' 30" of d	5.9	195.3	
0+55			1+83				
10' 30" of d	4.1	197.7		10' 30" of d	5.9	195.3	
T.P. 3.75	201.16	4.11	197.38	5.5 - -	6.3	194.9	Top Bank
d		3.8	197.7	3.0 - -	10.6	190.6	= Bottom -
10' No. of d		3.5	197.7	d	8.7	192.3	= - -
0+80			1+87				
10' No. of d	4.6	196.6		15' No. of d	8.2	193.0	= - -
d	4.5	196.7		2 - -	5.7	195.5	= Top -
10' 30" of d	3.9	197.3		10' - -	5.6	195.6	
1+00			1+90				
10' 30" of d	3.9	197.3		10' No. of d	5.8	195.8	Top Bank
d	4.2	197.0		7' - -	7.5	193.7	
10' No. of d	4.6	196.6		d	9.6	191.6	
1+25			1+90				
10' No. of d	4.6	196.6		2' 30" of d	10.5	190.7	
d	4.5	196.7		8' - -	10.3	190.9	
10' 30" of d	4.2	197.0		10' - -	6.3	194.9	
				10' 30" of d	6.1	195.1	Top Bank
				8' - -	10.0	191.2	Bottom

201.16

547

d		8.8	192.4	
10' No. of d		7.8	193.4	
	1493			
10' No. of d		7.9	193.3	
d		8.8	192.4	
10' So. of d		9.1	192.1	Bottom Bank
	205			
10' So. of d		9.6	191.8	
d		8.4	192.8	
8' No. of d		8.0	193.2	= Bank
	215			
10' No. of d		8.5	192.7	
d		10.0	191.2	Main Creek Bottom
10' So. of d		9.7	191.5	= ✓
	2+35			
10' So. of d		10.4	190.8	
d		10.1	191.1	= d. of creek
10' No. of d		10.1	191.1	

3/5/14

Gregory

LEVELS ON
BROOKLYN AVE
From 63rd to

55

07 B.M.	7.04	298.84	271.28	511 63 rd + Brooklyn
		E.L. 63 rd St		
S		8.7		
C		5.2		
N		1.8		
		40' E		
N		3.6		
C		6.7		
S		10.1		
		100' E		
S		11.5		
C		9.7		
N		5.8		
		150' E		
N		7.7		
C		10.3		
S		12.9		
		200' E		
S		14.0		
C		10.9		
N		9.3		
		235' E		
N		9.3		
C		11.5		
S		13.8		

270' E

13.3

11.3

9.4

300' E

9.4

10.9

13.0

335' E

12.6

10.8

9.2

366.6' E = N.L. STORK ST 60' wide

9.1

11.0

12.7

TP. 314 270.29 11.69 26715 SW Stork
for STORK ST see page 33
E.L. STORK

4.5

2.2

0.5

50' E

0.8

2.6

5.1

75' E

S	5.9
C	3.0
N	1.1

100' E

N	2.3
C	4.2
S	7.0

125' E

S	8.1
C	5.1
N	3.9

150' E

N	5.5
C	7.4
S	10.2

175' E

S	12.0
C	9.3
N	8.1

200' E

N	9.9
C	12.0
T.P.	2.74
S	1.7

260.22 12.79 257.50

235' E

S	6.4
C	3.2
N	0.7

265' E

N	3.4
C	7.0
S	10.7

200' E

S	13.9
C	8.5
N	5.4

325' E

N	6.5
C	10.3
T.P.	185, 251.28
S	10.79
	249.43
	6.8

350' E

S	9.8
C	3.0
N	+0.5

375' E

N	2.8
C	5.5
S	9.9

401.4' E = W.L. 64th or 30' inside.

S	12.7	
C	88	
N	68	
EL 64 th S	116	
C	137	
S	169	
T.R	1142	239.86

3/11 Gregory Miller

Cross Section of 28th St from Thorn to Upas 83' wide 20' cbs 10.75' 1/2's

333.7

262 333.66 331.04 NE Upas + 1/4" +3
Cement Curb and Sidewalk in on E. Side from S.L. Upas to 100' So. W

So. Line UPAS produced West 75' So

1786.0
1789.0
E.C.B.

1/6	4.84	328.82	on cement cd	W	5.9	327.8
	5.4	328.3		+16	5.2	328.5
	5.3	328.4		+18.5		
C	5.3	328.1		1/2	6.7	327.0
1/6	5.3	328.1		1/2	6.5	326.9
ob	5.2	328.0		1/2	6.2	327.4
W.	5.6	328.3		1/2	5.9	327.8

25' So.

W	5.5	328.2			6.2	327.5
+17	5.3	328.1		1/2	6.3	327.4
+18	5.8	327.9		1/2	6.3	327.4
1/6	6.0	327.7		1/2	6.3	327.4
1/6	5.6	328.1		1/2	6.2	327.5
C	5.2	328.5		1/2	6.3	327.4
1/6	5.5	328.2		1/2	6.3	327.4
ob	5.7	328.0		1/2	6.2	327.5

50' So.

E ob	6.1	327.6		1/2	6.2	327.5
1/6	5.9	327.8		1/2	6.2	327.5
0	5.5	328.2		1/2	6.2	327.5
1/6	6.0	327.7		1/2	6.2	327.5
ob	6.4	327.3		1/2	6.2	327.5
+2	6.4	327.3		1/2	6.2	327.5

100' So.

E	5.8	327.9		1/2	6.2	327.5
ob	6.2	327.5		1/2	6.2	327.5
	6.9	326.8		1/2	6.2	327.5
	6.5	327.2		1/2	6.2	327.5
	6.3	327.4		1/2	6.2	327.5
	6.6	327.1		1/2	6.2	327.5
	7.2	326.5		1/2	6.2	327.5
	7.2	326.5		1/2	6.2	327.5
	6.5	327.2		1/2	6.2	327.5
	6.4	327.3		1/2	6.2	327.5
	5.7	328.0		1/2	6.2	327.5

Not to be used for yardage (2.23) (327.43) on cement.

333.66

125' So.

W	6.0	3277
+17	6.6	3271
+18	7.4	3263
cb	7.5	3262
1/2	7.2	3265
C	6.8	3269
1/2	6.9	3268
cb	7.3	3264
+14	6.5	3272
+10	6.2	3275
E	6.8	3269
+3	7.2	3265
150' So.		
-5	7.7	3260
E	7.6	3261
+16	7.0	3267
+18	7.4	3263
cb	7.4	3263
1/2	7.4	3263
C	7.3	3264
1/2	7.5	3262
cb	7.4	3263
+12	6.7	3270
W	7.1	3266
TP	4.60	330.58
	7.68	325.98

330.6

28+457. 79

164' So.

W	4.1	3265
cb	4.2	3264
1/2	4.4	3262
C	4.4	3262
1/2	4.6	3260
cb	4.4	3262
+17	4.4	3262
E	4.8	3258
188' So.		
E	5.2	3254
cb	4.9	3257
1/2	4.7	3259
C	4.8	3258
1/2	4.6	3260
cb	3.6	3270
W	3.9	3267
205' So.		
W	4.4	3262
cb	4.4	3262
1/2	4.8	3258
C	4.9	3257
1/2	4.3	3263
cb	4.5	3261
E	5.3	3253

330 58

225 So.

E	5.4	325.2
cb	5.1	325.5
1/4	5.1	325.5
C	4.9	325.7
1/2	4.5	326.1
cb	3.9	326.7
W.	4.2	326.4

250 So.

W	4.4	326.2
cb	4.8	325.8
1/2	5.0	325.6
C	4.9	325.7
1/4	5.0	325.6
cb	5.1	325.5
E	5.4	325.2

275 So.

E	5.5	325.1
cb	4.9	325.7
1/4	4.8	325.8
C	4.7	325.9
1/2	4.6	326.0
cb	4.2	326.4
W	3.5	327.1

330.6

2874 57

60

303 So.

W	4.4	326.2
cb	4.5	326.1
1/2	4.4	326.2
C	4.7	325.9
1/4	4.9	325.7
cb	4.7	325.9
E	5.1	325.5

333 So.

E	5.6	325.0
cb	5.5	325.1
1/2	5.3	325.3
C	5.0	325.6
1/4	4.8	325.8
cb	4.6	326.0
W	4.4	326.2

355 So.

W	4.4	326.2
cb	4.7	325.9
1/4	4.6	326.0
C	4.7	325.9
1/2	4.6	326.0
cb	5.2	325.4
10	5.5	325.1
E	5.6	325.0

330.58

400' So.

E	5.4	325.2
dg	5.3	325.3
1/4	5.2	325.1
C	5.1	325.5
1/4	5.0	325.6
dg	4.8	325.8
W	5.0	325.6
T.P.	325	329.27
	5.26	325.32

435' So.

W	4.2	325.1
dg	3.6	325.7
1/4	3.5	325.8
C	4.0	325.3
1/4	4.3	325.0
dg	4.3	325.0
E	4.1	324.9

465' So.

E	4.1	325.2
dg	4.5	324.9
1/4	4.5	324.8
C	4.5	324.8
1/4	4.5	324.8
dg	4.5	324.8
W	4.3	325.0

329.27

425' So.

W	5.3	324.0
dg	5.2	324.1
1/4	5.3	324.0
C	5.2	324.1
1/4	5.2	324.1
dg	5.3	324.0
E	5.3	324.0

515' So.

E	5.5	323.8
dg	5.6	323.7
1/4	4.9	324.4
C	5.1	324.2
1/4	5.7	323.6
dg	5.9	323.4
W	6.1	323.2

540' So.

W	6.3	323.0
dg	6.5	322.8
1/4	6.2	323.1
C	6.3	323.0
1/4	6.5	322.8
dg	6.4	322.9
E	5.9	323.4

28th St. 61

329.27

555 So.

E	6.0	323.3
+8	5.6	323.7
cb	6.3	323.0
1/4	6.8	322.5
C	6.9	322.4
1/4	6.8	322.5
cb	6.8	322.5
W	6.6	322.7

575 So.

W	7.7	321.6
cb	7.6	321.7
1/2	7.5	321.8
C	7.6	321.7
1/4	7.4	321.9
cb	6.9	322.2
+10	6.4	322.9
E	6.6	322.7

600' So = NL Thorn St. 60' wide

E	7.1	322.2
cb	7.6	321.7
1/2	7.7	321.6
C	7.4	321.9
1/4	7.9	321.4
cb	8.5	320.8
W	8.9	320.4

329.3

28th St.

62

No. Corb

W	9.0	320.3
cb	8.4	320.9
1/4	8.0	321.3
C	7.6	321.7
1/4	7.7	321.6
cb	7.8	321.5
E	7.4	321.9

No. Quarter

E	7.8	321.5
cb	7.9	321.4
1/2	8.0	321.3
C	7.8	321.5
1/4	8.3	321.0
cb	8.6	320.7
W	9.2	320.1

Center Thorn St

W	9.5	319.8
cb	9.0	320.3
1/4	8.9	320.4
C	8.4	320.9
1/4	8.3	321.0
cb	8.4	320.9
E	8.1	321.2

319.27

So. Quarter

E	83	321.0
cb	84	320.9
1/4	87	320.6
C	93	320.0
1/4	94	319.9
cb	95	319.8
W	10.0	319.3

So. Curb.

W	10.2	319.1
cb	98	319.5
1/4	96	319.7
C	96	319.7
1/4	92	320.1
cb	89	320.4
1/2	88	320.5
E	85	320.8

So. Line Thorn St

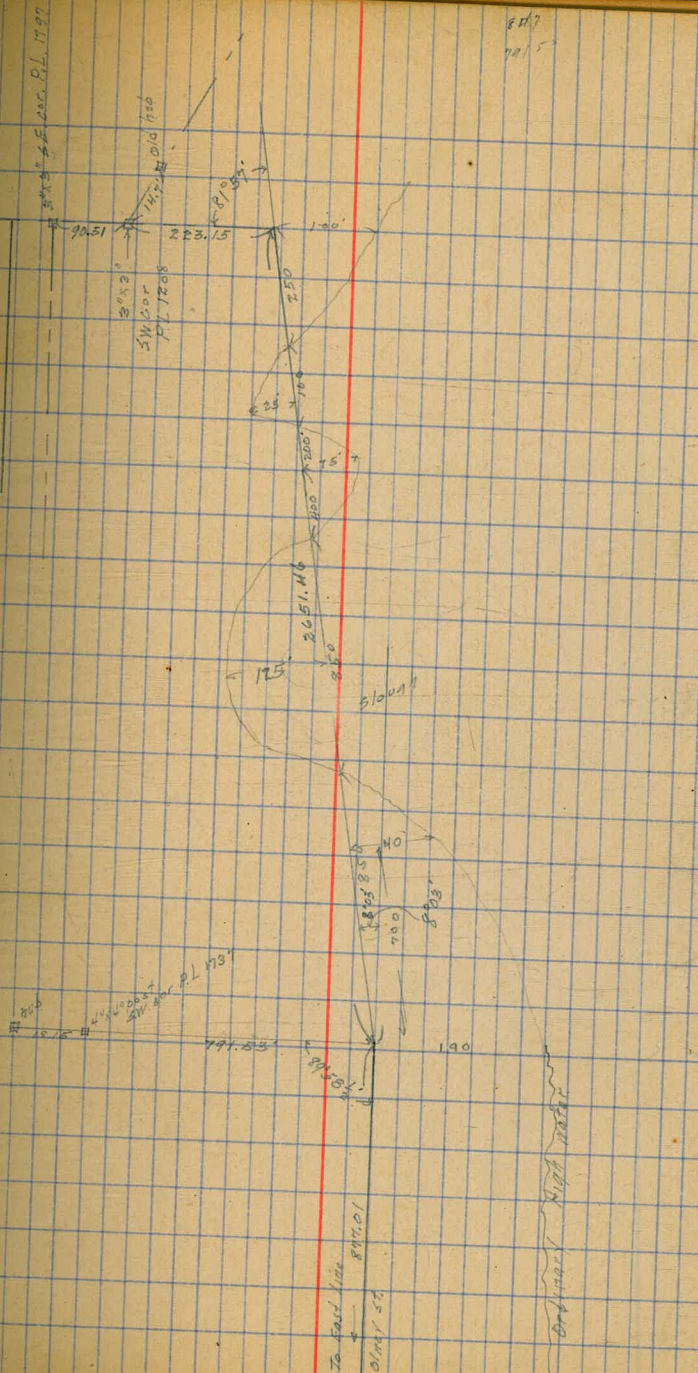
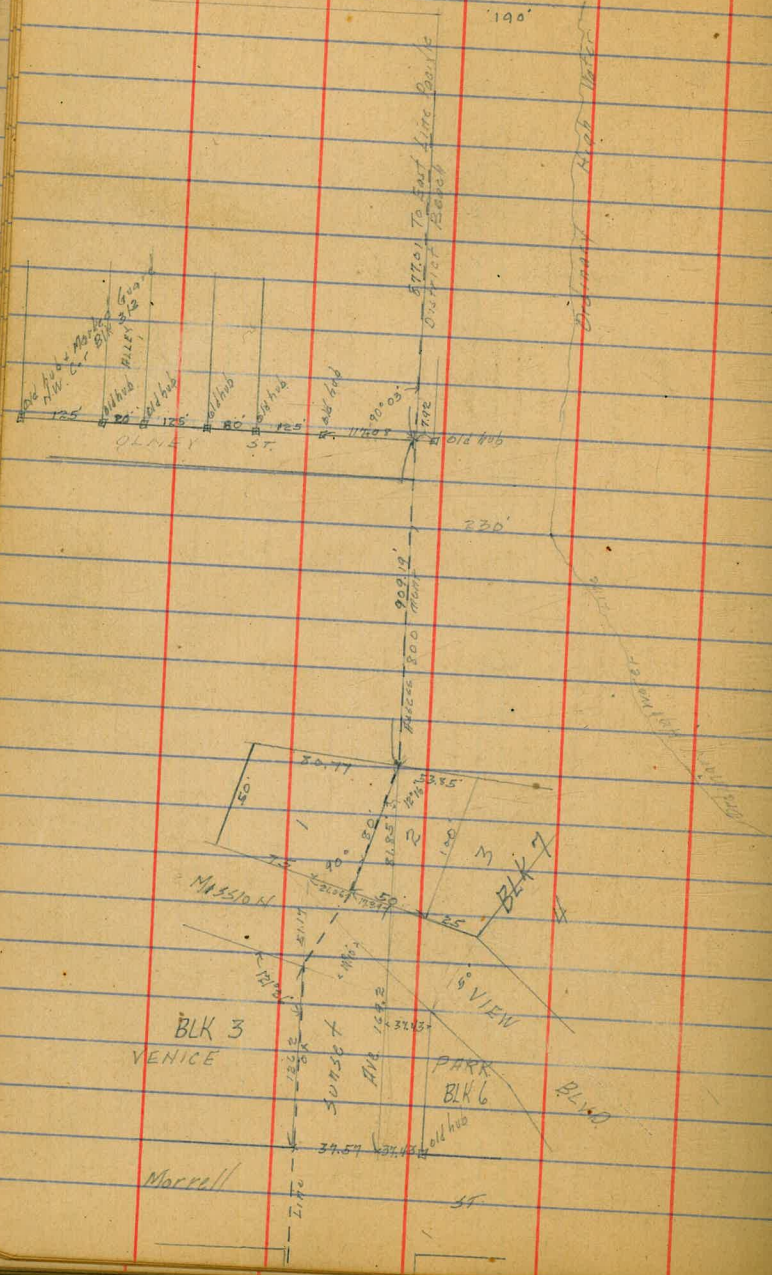
E	88	320.5
cb	92	320.1
1/4	95	319.8
C	97	319.6
1/4	98	319.5
cb	10.0	319.3
W	103	319.0
chk BM	579	323.48 = B.P. NE 323.44 Thorn + Grade

28457

63

Gregor Miller Shaw

Survey of Southern Line
of Assmt. Dist. for
the paving of
Garret St.



54

Cross of Channel 10' E. of
65th St.

65

4.19	216.99	212.80	NE 65 th Hill	0+22	8.8	208.2
		5.21	211.78 = Top of 600 on 87	0+34	5.8	211.2
		9.1	207.9 = Low pt. inclining below 87 1/2	0+63	4.7	212.3
0+00 = to Side Creek		4.8	212.2	0+70	4.2	212.8
+01.0		4.8	212.2	0+85	3.8	213.2
+02.0		6.9	210.1	1+00	3.8	213.2
+04.0		8.1	208.9	1+51	4.1	212.9
+09.0		9.1	207.9	1+60	2.2	214.8
+45.0		8.8	208.2			
+35.0		8.1	208.9			
+45		7.9	209.1			
+55		6.7	210.3			
+75		5.9	211.1			
1+00		5.7	211.3			
1+41		5.3	211.7			
1+45		4.5	212.5			
1+53		0.7	216.3			

CROSS SECTION 75' UP STREAM.

FROM ABOVE SECTION

on High water mark.	3.3	213.7
0+00	3.5	213.5
0+04.0	3.5	213.5
0+02.1	8.4	208.6
0+06.0	10.2	206.8 x
0+15	7.2	209.8
0+21	7.5	209.5

0+22	8.8	208.2
0+34	5.8	211.2
0+63	4.7	212.3
0+70	4.2	212.8
0+85	3.8	213.2
1+00	3.8	213.2
1+51	4.1	212.9
1+60	2.2	214.8

TRAVERSE LEVELS DOWNSTREAM FROM
FIRST X SECTION

0+00 = FIRST X SECT.	8.8	208.2	
1+00	9.9	207.1	
2+00	12.2	204.8	
T.P. 416	208.63	12.52	204.47
3+00	4.9	203.7	
4+00	5.6	203.0	
5+00	6.5	202.1	
T.P. 1.99	204.33	6.19	202.44
6+00	3.9	200.4	
7+00	5.1	199.2	
8+00	5.7	198.6	
9+00	6.8	197.5	
10	8.1	196.2	
T.P. 6.23	202.19	8.37	195.96 = EL. Stop
T.P. 4.26	199.32	7.13	195.06
High water mark on Water Stop.	3.02		

continued

199.32

Continuation of Traverse
Levels down a Cholla Creek.

0+00 = 2+35 page 54	8.1	191.1
1+00	9.8	189.5
2+00 ←	10.3	189.0
High water mark opp 2+00	6.2	193.1

CROSS SECTION OF CHANNEL AT
2+00

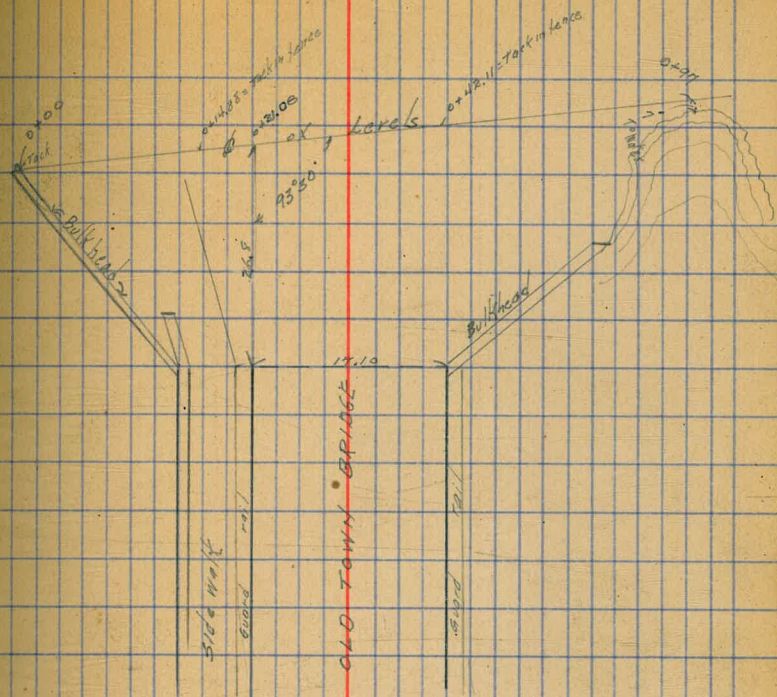
0+00 = to Bank.	6.0	193.3
0+10	6.8	192.5
0+17	10.9	188.4
0+26	10.1	189.2
0+44	10.1	189.2
0+49	8.3	191.0
0+50	6.4	192.9
0+55	6.4	192.9

1/28/19 Gregg
11/11/19
Shaw.

Levels for Sheet Piling
No. End Old Town Br.

	3.44	12.10		8.66	Top. H. Taylor & Whitman
	11.48	22.97	0.61	11.49	
	4.18	17.79			N.W. End of No.
0-10			9.36	13.61	
0+00			14.0	3.8	
			11.7	6.1	= Top of Bulkhead
0+00			13.5	4.3	= ground
0+06.0			11.3	6.5	
0+15			4.4	13.4	= edge road
0+27			3.9	13.9	
0+42			4.3	13.5	= edge road
0+57			12.4	5.4	
0+67			13.2	4.6	
0+71			15.7	2.1	
0+81			15.0	2.8	
0+97			16.7	1.1	Water 7' 50" = -0.2
1+06			15.3	2.5	
Floor of Bridge No. End			3.8	14.0	

See next page.



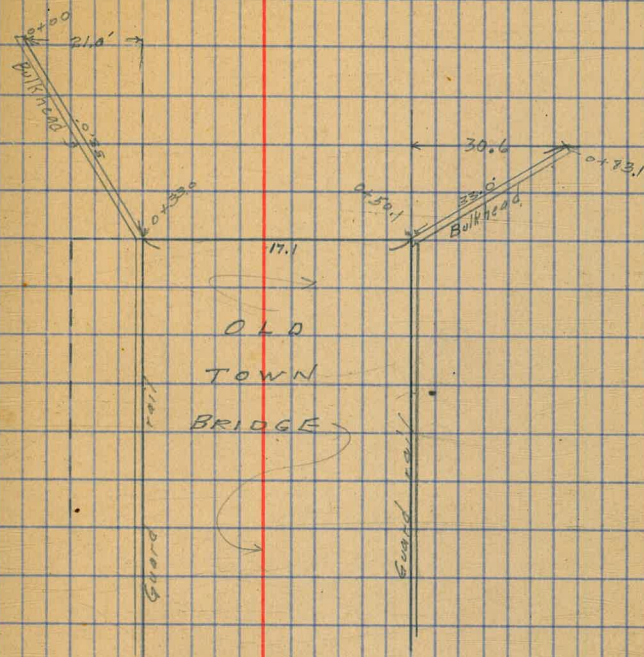
12/10/19 Gregory
Miller
Shaw

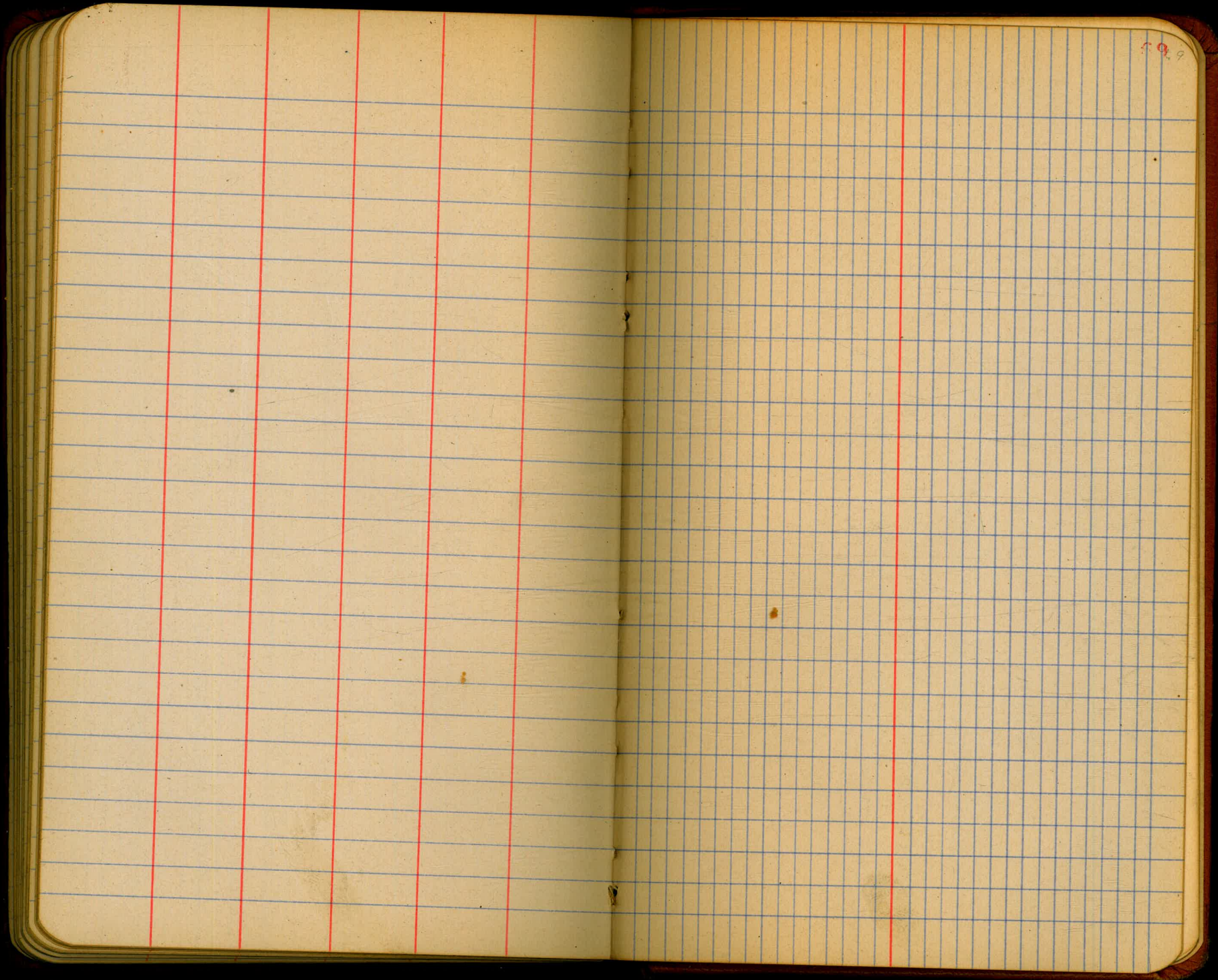
Levels for Sheet Piling
OLD TOWN BRIDGE

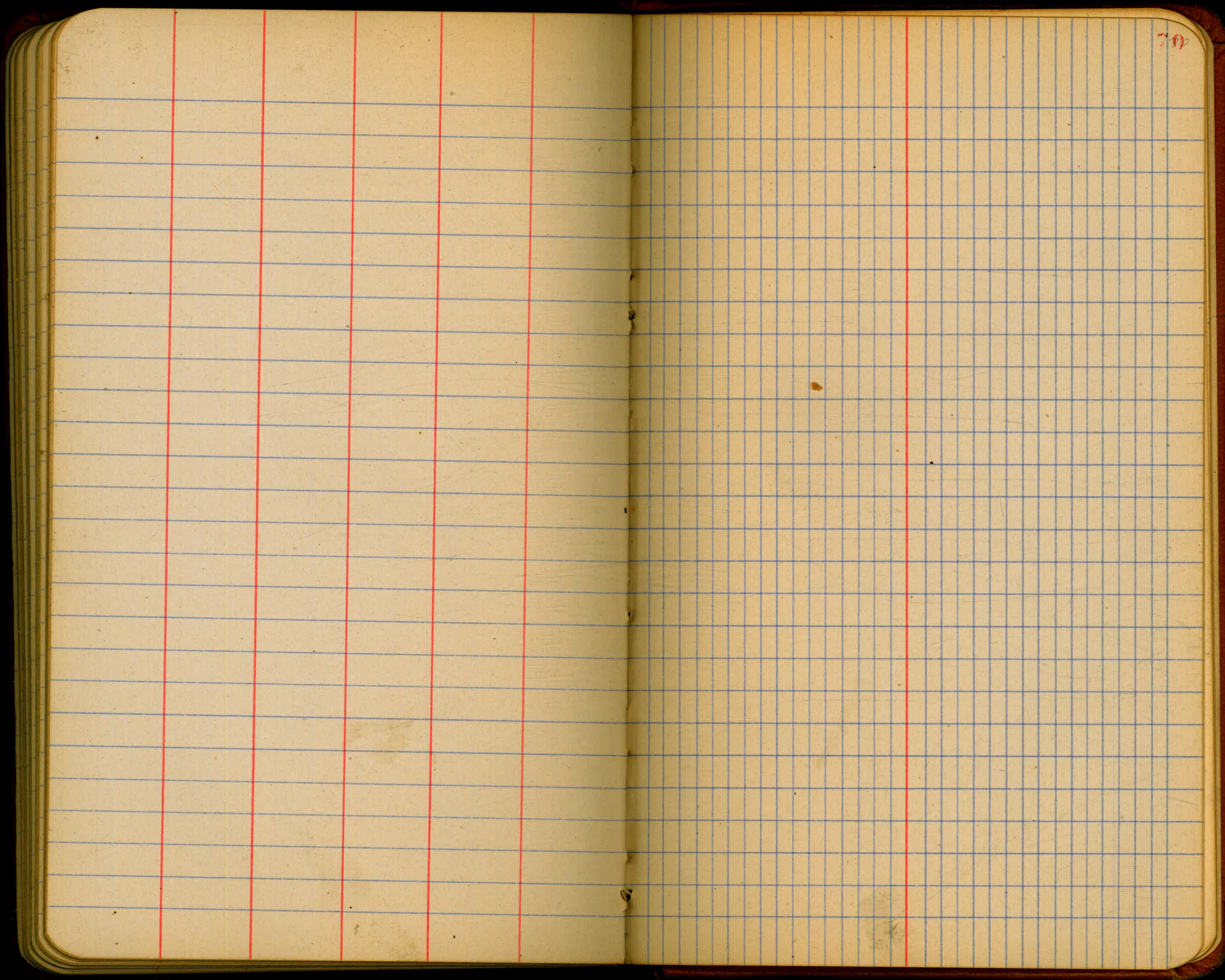
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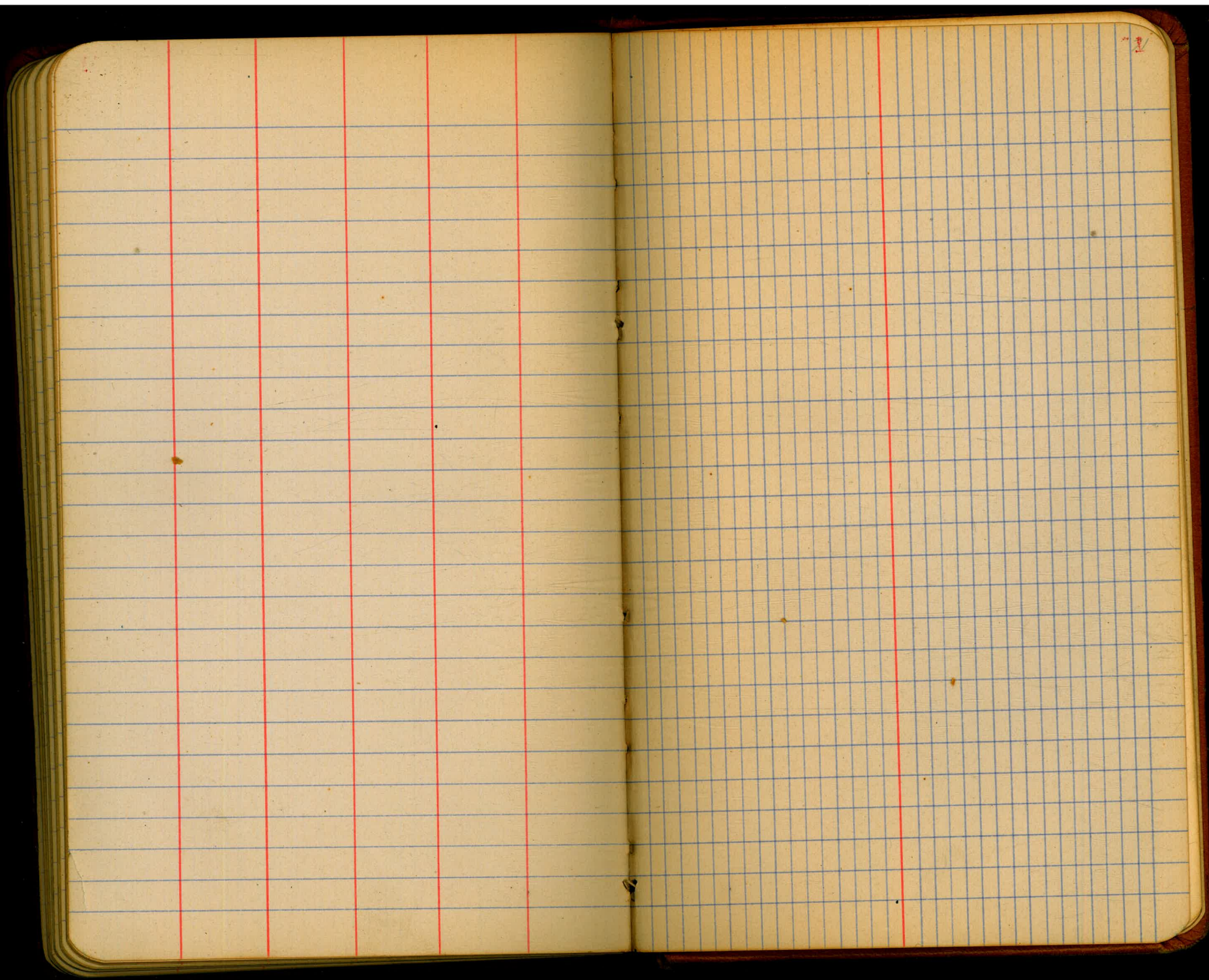
Levels Taken on Lines of Bulkheads + Abutment

	#63	18.24	13.61	T.P. on Page 67
0+00 ground		14.6	3.6	
0+00 Top of Bulkhead		12.2	6.0	
0+06.0		12.0	6.2	
0+15.		8.5	9.7	
0+26		5.5	12.7	
0+33 = 11' over Bridge		4.2	14.0	
0+50.1 = NE ✓ ✓		4.2	14.0	
0+64.0		7.7	10.5	
0+76.0		12.6	5.6	
0+83.0 = End of Bulkhead		16.3	1.9	
0+93.0		18.2	-0.2	
1+14		18.2	-0.2	
1+19		15.1	3.1	
1+29		15.3	2.9	









DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body

IMPROVED TABLES
AND
INFORMATION

necessary.

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

7679 30.000 39.07 6911 51900 4/43 70.75

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	2349	790	2423	808	2497	826	2572	844	3111	862	2723	38
52	880	2799	898	2876	916	2954	934	3032	951	3597	969	3190	37
53	986	3270	8004	3351	8021	3452	8039	3514	8056	4106	8073	3680	36
54	8090	3764	107	3848	124	3934	141	4019	158	4641	175	4193	35
55	192	4281	208	4370	225	4460	241	4550	258	5204	274	4733	34
56	290	4826	307	4919	323	5013	339	5108	355	5798	371	5301	33
57	387	5399	403	5497	418	5597	434	5697	450	6426	465	5900	32
58	480	6003	496	6107	511	6212	526	6319	542	7090	557	6534	31
59	572	6643	587	6753	601	6864	616	6977	631	8111	646	7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	8040	760	8165	774	8291	788	8418	802	8546	816	8676	28
62	829	8807	843	8940	857	9074	870	9210	884	9347	897	9486	27
63	910	9626	923	9768	936	9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	1.445	075	1.609	088	1.775	100	1.943	112	2.113	124	2.286	24
66	135	2460	147	2637	159	2817	171	2998	182	3183	194	3369	23
67	205	3559	216	3750	228	3945	239	4142	250	4342	261	4545	22
68	272	4751	283	4960	293	5172	304	5386	315	5605	325	5826	21
69	336	6051	346	6279	356	6511	367	6746	377	6985	387	7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	9042	465	9319	474	9600	483	9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	2.2041	555	2.2371	17
73	563	2709	572	3052	580	3402	588	3759	596	4124	605	4495	16
74	613	4874	621	5261	628	5656	636	6059	644	6470	652	6891	15
75	659	7321	667	7760	674	8208	681	8657	689	9136	696	9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	3315	750	3897	757	4494	763	5107	769	5736	775	6382	12
78	781	7046	787	7729	793	8430	799	9152	805	9894	811	5.0658	11
79	816	1.446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	5.5764	10
80	848	5.6713	853	5.7694	858	5.8708	863	5.9758	868	6.0844	872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	6.8269	899	6.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	999	57.290	999	68.750	999	85.940	999	114.58	1.000	171.88	1.000	343.77	0
90	60'	60'	50'	50'	40'	40'	30'	30'	20'	30'	10'	10'	deg
90	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	deg

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84

225
270
300
335 138 NE 4th
13733 13743 13833 13883 13933
591 521 471 421 371
14284 14683 14133 221
Elev gatter wand 138.44
Cent. 139.67
142
63
21
10.5
4

313.907 W
312.507 E

75
338
9162

16983
2525
14458
434
14024
2503
16527

83.42
20
250260

25.2
23.9
21.6
19.3
17.0
14.7
12.4
10.1
7.8
5.5
3.2
0.9

216.2
296
221.2

1245.3 5 post
4.9

SW Macon + SD 2w.60

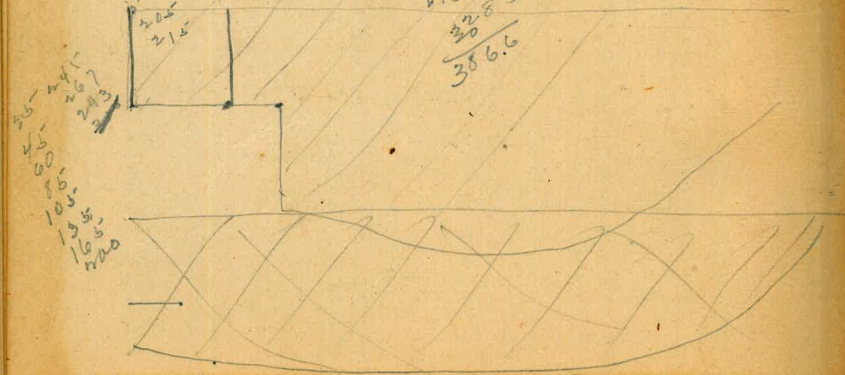
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2918

14458
434
14892
2503
12389

1620
35.44
1584.56 to A
1776.250 2nd A
1780.95 total

20
10
0500
+17
+4
+33
+55
+60
+00

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1135.5
116.76
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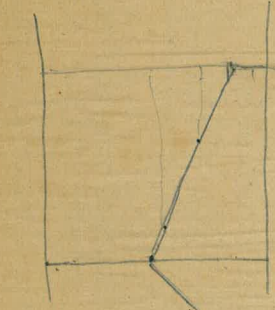


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9
1500
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29
56
85

1700 16 18
71
8500
11900
127500 89200
500
1790

1850
9000
9000

183
75
104



2640
2000.00
15480
12200
13200
20000

2640
591.0
5270
6300
5270
10200
10660
7920
22800