

50

1030

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LEVEL BOOK.

No. 410

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Shogren T. H.  
Lot 7 Subdiv  
Punka Lot 1113  
Peter Ricard -

MICROFILMED  
DEC 17 1964

3, 4, 5 + 6.  
of Punka Lot 1113

C.H.S. No. 1

Notes covering individual tests  
of City Pump wells in Mission Valley

5284  
5241  
41  
45  
2239  
22

Repairing pump  
No 116.  
Pumping Water 117.  
Clipper No 4  
Belt-lining

# Test of

Time	Gauge	Wier	amp.	Gal Per M.	Head.
12 M.	14 1/2	3 7/16	9	477	20.5 + 5"
1 PM	14 1/2	3 7/16	9	"	"
2 "	14 1/2	3 7/16	9	"	"
3 "	14 1/2	3 7/16	9	"	"
4 "	14 1/2	3 7/16	9	"	"
5 "	14 1/2	3 7/16	9	"	"
6 "	14 1/2	3 7/16	9	"	"
7 "	14	3 7/16	9	"	"
8 "	14	3 7/16	9	"	"
9 "	14	3 7/16	9	"	"
10 "	14	3 1/2	9 1/4	"	"
11 "	14	3 7/16	9 1/4	"	"
12 "	14	3 7/16	9	"	"
1 AM.	14	3 7/16	9	"	"
2 "	14	3 7/16	9	"	"
3 "	14	3 7/16	9	"	"
4 "	14	3 7/16	9	"	"
5 "	14	3 7/16	9	"	"

54'-3" pipe

NEW N° 9.

Well #1

Mission Valley

NOV 16, 1914.

Head	HP Water	HP Motor	Eff.	Curve at 1685 RPM
25.5'	3.06	7 1/2	40.7	37

Pump REVOLUTIONS

1706
1720
1712
<u>1713</u> avg per MIN.

Assume gauge 22" at start, engine  
with test by Kral.

$$22" = 34.1 \text{ etc. } \frac{6.12}{40.22} \text{ " U.S.S.}$$

# Test of

Time	Gauge	Wier	amp.	
6 AM.	14	$3\frac{7}{8}$	9	477
7 "	14	$3\frac{1}{2}$	9	
8 "	14	$3\frac{1}{2}$	9	
9 "	14	$3\frac{1}{2}$	9	
10 "	14	$3\frac{1}{2}$	9	
11. "	14.	$3\frac{1}{2}$	9.	

Well #1  
New No 9.

Mission Valley.  
Nov. 17<sup>th</sup> 1914.

14<sup>#</sup> Gauge Pressure = W.S. Elev.  
of  $+15.6 + 6.12 = 21.72$  U.S.G.S

# Test of

Time	Gauge	watt meter	Wier
2 P.M.	17	.0001	$3\frac{1}{8}$
3 "	17	.0001 $\frac{1}{4}$	3
4 "	17	.0001 $\frac{3}{4}$	3
5 "	17	.0002 $\frac{1}{2}$	3
6 "	17	.0003 $\frac{1}{4}$	3
7 "	17	.0003 $\frac{3}{4}$	3
8 "	17	.0004 $\frac{1}{2}$	3
9 "	17	.0005 $\frac{1}{4}$	3
10 "	17	.0005 $\frac{3}{4}$	3
11 "	17	.0006 $\frac{1}{2}$	3
12 .	18	.0007	$2\frac{3}{4}$
1 A.M.	18	.0007 $\frac{3}{4}$	$2\frac{3}{4}$
2 "	18	.0008	$2\frac{3}{4}$
3 "	18	.0008 $\frac{3}{4}$	$2\frac{3}{4}$
10 A.M.	17	.0009 $\frac{1}{4}$	$3\frac{1}{4}$
11 "	17	.0009 $\frac{3}{4}$	$3\frac{1}{4}$
12 M.	17	.0010 $\frac{1}{4}$	$3\frac{1}{4}$
1 P.M.	17	.0011	$3\frac{1}{4}$

NEW NUMBER 8.  
Well #2

Mission Valley  
Nov. 19<sup>th</sup> 1914.

Pump Revolutions

per minute

1582

1588

1586

1585 avg.

Shot down on acct. of belt climbing up pulley.

Tightened belt.

Gage about 2" at start M28

# Test of

Time	Watts	Wier.	Gauge	Gal Per Min	Head-
2 PM.	.0011 $\frac{3}{4}$	3 $\frac{1}{2}$	18"	504	22' total.
3 "	.0012 $\frac{1}{2}$	3 $\frac{1}{4}$	18"		
4 "	.0013	3 $\frac{1}{4}$	16	.56 x 900. = 504.	
5 "	.0014	3 $\frac{1}{2}$	16		
6 "	.0014 $\frac{1}{2}$	3 $\frac{1}{2}$	16		
7 "	.0015 $\frac{1}{4}$	3 $\frac{1}{2}$	16		
8	.0016	3 $\frac{1}{2}$	16		
9	.0019	3 $\frac{1}{2}$	16		
10	.0017 $\frac{1}{2}$	3 $\frac{1}{2}$	16		
11	.0018 $\frac{1}{4}$	3 $\frac{1}{2}$	16		
12	.0018 $\frac{3}{4}$	3 $\frac{1}{2}$	16		
1 AM	.0019 $\frac{3}{4}$	3 $\frac{1}{2}$	16		
2	.0020 $\frac{1}{4}$	3 $\frac{1}{2}$	16		
3	.0021	3 $\frac{1}{2}$	16		
4	.0021 $\frac{3}{4}$	3 $\frac{1}{2}$	16		
5	.0022 $\frac{1}{2}$	3 $\frac{1}{2}$	16		
6	.0023 $\frac{1}{2}$	3 $\frac{1}{2}$	16		
7	.0024 $\frac{1}{2}$	3 $\frac{1}{2}$	16		
8	.0025	3 $\frac{1}{2}$	16		
9	.0025 $\frac{3}{4}$	3 $\frac{1}{2}$	16		
10	.0026 $\frac{1}{2}$	3 $\frac{1}{2}$	16		
11					
12					

NEW NUMBER 8.

Nov. 20. 1914.

Well # 2.

Mission Valley,

H.P. Water, H.P.M. H.P.

Nov 20 1914.

2.8. 9.4

H.P. Motor. 9.4. 85% Motor = 8 H.P.

10% Loss in belt. = 7.2 H.P. at pump.

$$\frac{2.8}{7.2} = 38.9\% \text{ curve } 39\%$$

Well # 2. Gauge 16" = U.S. Elev. of  
 23.4  
 + 26.9 City. + 6.12 = 33.02 U.S. G.S.

Final. Well. 0026 $\frac{1}{2}$

NEW NUMBER 7. Mission Valley<sup>5</sup>  
No 3

Test of Well

Time	Gauge	Wier	Watts	Cal/Pwr minute	Head-	$\frac{1}{4}$ " Pipe 53'-1" long, 22ft.	2.64 HP.	Nov. 24-1914
12 M.	16 lbs	$3\frac{3}{8}$ "	0026 $\frac{1}{2}$	477.	17+5=			Pump Revolutions
1 PM	16 "	$3\frac{3}{8}$ "	0027 $\frac{1}{4}$	"				per minute
2	16 "	$3\frac{3}{8}$ "	0027 $\frac{3}{4}$	"				1609
3	16 "	$3\frac{3}{8}$ "	0028 $\frac{1}{2}$	"				1607
4	16 "	$3\frac{3}{8}$ "	0029					1611
5	16 "	$3\frac{3}{8}$ "	0030					<u>1609</u> avg.
6	16 "	$3\frac{3}{8}$ "	0030 $\frac{3}{4}$					
7	15 $\frac{3}{4}$	$3\frac{3}{8}$ "	0031 $\frac{1}{2}$					
8	15 $\frac{3}{4}$	$3\frac{3}{8}$ "	0032					
9	15 $\frac{3}{4}$	$3\frac{3}{8}$ "	0033					
10	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0033 $\frac{3}{4}$					
11	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0034 $\frac{1}{4}$					
12	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0035 $\frac{1}{4}$					
1 AM.	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0035 $\frac{3}{4}$					
2	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0036 $\frac{1}{2}$					
3	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0037 $\frac{1}{2}$					
4	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0038 $\frac{1}{4}$					
5	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0039					
6	15 $\frac{1}{2}$	$3\frac{3}{8}$ "	0039 $\frac{3}{4}$					

KW. 7.75 = 10.37 HP.

85% 10.37 = 8.82 less 10% = 7.94

$\frac{2.64}{7.94} = 33\frac{1}{3}\%$  Eff. - curve. 39%.

Tightened Belt.

Gauge about 21 before start, Est. by K.S.

# Test of Well

#3 (Continued.)  
 NEW NUMBER, 7.

Nov 25-1914.

Time	Gauge	Wier	Watts	
7	15 $\frac{1}{2}$	3 $\frac{3}{8}$	0040 $\frac{1}{2}$	477
8	15 $\frac{3}{4}$	3 $\frac{3}{8}$	0041 $\frac{1}{4}$	
9	15 $\frac{3}{4}$	3 $\frac{3}{8}$	0042	
10	15 $\frac{3}{4}$	3 $\frac{3}{8}$	0042 $\frac{3}{4}$	
11	15 $\frac{3}{4}$	3 $\frac{3}{8}$	0043 $\frac{1}{2}$	
12	15 $\frac{3}{4}$	3 $\frac{3}{8}$	0044 $\frac{1}{4}$	
	20 $\frac{1}{4}$	at end of test.		

Gauge 15  $\frac{3}{4}$  = W. S. Elev. + 24.2  
 City + 6.12 = 30.32



# TEST OF WELL

N<sup>o</sup> 4.  
NEW NUMBER. 6.

Nov 27<sup>th</sup> 14.

TIME	GUAGE WIER	WATTS	Gal. Per Min	Head.	HP water.	60' Pipe -
9 A.M.	12 1/2 lb	3 1/2"	0045	432	32.2 + 5 = 37.5'	4.05-
10	12 1/2 "	3 3/8"	0045 3/4	"		Pump Revolutions per Minute 1613 1614 1616 <hr/> 1616 Average
11	12 1/2 "	3 3/8"	0046 1/2	"		
12	12 1/2 "	3 1/8"	0047 1/4	"		
1 pm	12 1/2 "	3 1/8"	0048	"		
2	12 1/2 "	3 1/8"	0048 1/2	"		
3	12 1/2 "	3 1/8"	0049 1/4			
4	12 1/2 "	3 1/8"	0050			
5	12 1/2 "	3 1/8"	0050 3/4			
6	12 1/4 "	3 1/8"	0051 1/2			
7	12 "	3 1/8"	0052 1/4			
8	12 "	3 1/8"	0053			
9	12 "	3 1/8"	0053 3/4			
10	12 "	3 1/8"	0054 1/2			
11	12 "	3 1/8"	0055 1/2			
12	12 "	3 1/8"	0056 1/4			
1 A.M.	12 "	3 1/8"	0056 3/4			
2	12 "	3 1/8"	0057 3/4			
3	12 "	3 1/8"	0058 1/4			

K.V. 7.25 = H.P. 9.7 less 85% = 8.25

less 10% 7.42 H.P. at Pump.

$\frac{4.05}{7.42} = 54 \frac{1}{2} \% - \text{curve } 53\%$

WELL N<sup>o</sup> 4. (CONTINUED)

Nov. 28<sup>th</sup> 14.

NEW NUMBER. 6.

TIME	GUAGE	WIER.	WATTS.	
4 A.M.	12	$3\frac{1}{8}$	0059 $\frac{1}{4}$	+32
5 "	12	$3\frac{1}{8}$	0059 $\frac{3}{4}$	
6 "	12	$3\frac{1}{8}$	0060 $\frac{3}{4}$	
7 "	12	$3\frac{1}{8}$	0061 $\frac{1}{4}$	
8 "	12 $\frac{1}{4}$	$3\frac{1}{8}$	0062	
9 "	12 $\frac{1}{2}$	$3\frac{1}{8}$	0062 $\frac{3}{4}$	

23 " at end of test.

23.5 " " Beginning " "

REMARKS.

Shut down to trim up  
wier. Blaw fuse  
Starting up. 5 min delay.

Gauge 12 $\frac{1}{2}$  = +12.7 City +6.12  
+18.22 U.S.G.S.

# TEST OF WELL No 5.

Nov. 30<sup>th</sup> 14.

NEW NUMBER. 5.

TIME.	GUAGE	WIER	WATTS
9 A.M.	44 lbs	3 $\frac{3}{8}$ "	0063 $\frac{3}{4}$
10			
11			
12 Noon.	17 lbs	3 $\frac{3}{8}$ "	0064 $\frac{3}{4}$ 477
1	17 "	3 $\frac{3}{8}$ "	0065 $\frac{1}{2}$
2	17 "	3 $\frac{3}{8}$ "	0066 $\frac{1}{4}$
3	17 "	3 $\frac{3}{8}$ "	0067
4	17 "	3 $\frac{3}{8}$ "	0067 $\frac{3}{4}$
5	17 "	3 $\frac{3}{8}$ "	0068 $\frac{1}{2}$
6	17 "	3 $\frac{3}{8}$ "	0069 $\frac{1}{4}$
7	17 "	3 $\frac{3}{8}$ "	0069 $\frac{3}{4}$
8	17 "	3 $\frac{3}{8}$ "	0070 $\frac{1}{2}$
9	17 "	3 $\frac{3}{8}$ "	0071 $\frac{1}{4}$
10	17 "	3 $\frac{3}{8}$ "	0072
11	17 "	3 $\frac{3}{8}$ "	0072 $\frac{3}{4}$
12 M	17 "	3 $\frac{3}{8}$ "	0073 $\frac{1}{2}$
1 P.M.	17 "	3 $\frac{3}{8}$ "	0074
2	17 "	3 $\frac{3}{8}$ "	0074 $\frac{3}{4}$
3	17 "	3 $\frac{3}{8}$ "	0075 $\frac{1}{2}$

Use 22.5" for  
sart

## REMARKS.

Start Guage 44 lbs.  
Shut down at 9<sup>45</sup>  
to clean out Guage  
Run started up 11<sup>30</sup> again  
Guage 22 lbs.

## Pump Revolutions

per minute

1607

1598

1595

1600 Average

WELL N<sup>o</sup> 5. (CONTINUED)

DEC. 1<sup>ST</sup> 1914.

Pipe in well 10  
60'

TIME	GAUGE	WIER	WATTS.	Gal per Min.	Head.
4 AM.	17"	3 $\frac{3}{8}$ "	0076 $\frac{1}{4}$	477	21+5 = 26'
5	17"	3 $\frac{3}{8}$ "	0077	"	
6	17"	3 $\frac{3}{8}$ "	0077 $\frac{3}{4}$	"	
7	17"	3 $\frac{3}{8}$ "	0078 $\frac{1}{2}$	"	
8	17 $\frac{1}{2}$ "	3 $\frac{3}{8}$ "	0079 $\frac{1}{4}$	"	
9	17 "	3 $\frac{3}{8}$ "	0080		
10	17 "	3 $\frac{3}{8}$ "	0080 $\frac{3}{4}$		
11	17 "	3 $\frac{3}{8}$ "	0081 $\frac{1}{2}$		
12 Noon.	17 "	3 $\frac{3}{8}$ "	0082		
22 "	at the end of test.				

HR  
water

3.12

K.W. 7.25. 9.71 - 85% = 8.23 -  
 $\frac{3.12}{7.42} = 42\%$  less 10% = 7.42  
 curve. 43%

Gauge 17" = 24.4 City + 6.12 =  
 30.52 U.S.G.S.

TEST OF WELL N<sup>o</sup> 6.

DEC. 1<sup>st</sup> 14.

60' Pipe in well.

NEW NUMBER. 4.

TIME.	GUAGE	WIER	WATTS	Gal per Min	Head.
3 pm.	19 lb	3 $\frac{3}{8}$ "	0082	477	16'+5' = 21'
4 "	19 "	3 $\frac{3}{8}$ "	0087 $\frac{3}{4}$		
5 "	19 "	3 $\frac{3}{8}$ "	0083 $\frac{1}{2}$		
6 "	19 "	3 $\frac{3}{8}$ "	0084 $\frac{1}{4}$		
7 "	19 "	3 $\frac{3}{8}$ "	0085		
8 "	19 "	3 $\frac{3}{8}$ "	0085 $\frac{3}{4}$		
9 "	19 "	3 $\frac{3}{8}$ "	0086 $\frac{1}{2}$		
10 "	19 "	3 $\frac{3}{8}$ "	0087 $\frac{1}{4}$		
11 "	19 "	3 $\frac{3}{8}$ "	0088		
12 M	19 "	3 $\frac{3}{8}$ "	0088 $\frac{3}{4}$		
1 AM	19 "	3 $\frac{3}{8}$ "	0089 $\frac{1}{2}$		
2 "	19 "	3 $\frac{3}{8}$ "	0090 $\frac{1}{4}$		
3 "	19 "	3 $\frac{3}{8}$ "	0091		
4 "	19 "	3 $\frac{3}{8}$ "	0091 $\frac{3}{4}$		
5 "	19 "	3 $\frac{3}{8}$ "	0092 $\frac{1}{2}$		
6 "	19 "	3 $\frac{3}{8}$ "	0093 $\frac{1}{2}$		
7 "	19" lb	3 $\frac{3}{8}$ "	0094 $\frac{1}{4}$		
8 "	19 "	3 $\frac{3}{8}$ "	0095		
9 "	19 "	3 $\frac{3}{8}$ "	0095 $\frac{3}{4}$		

HP.  
Water

2.52

REMARKS.

Pump Revolutions

per Minute

1598

1590

1596

1595 Average

Tightened Belts

WELL No. 6. CONTINUED.

NEW No. 4.

TIME	GUAGE	WIER	WATTS.	
3 p	10 A.M.	19 lbs	3 $\frac{3}{8}$ "	0096 $\frac{1}{2}$ 477
4	11 "	19 "	3 $\frac{3}{8}$ "	0097 $\frac{1}{4}$
5	12 Noon	19 "	3 $\frac{3}{8}$ "	0098
6	1 p.m.	19 "	3 $\frac{3}{8}$ "	0098 $\frac{3}{4}$
7	2 "	19 "	3 $\frac{3}{8}$ "	0099 $\frac{1}{2}$
8	3 "	19 "	3 $\frac{3}{8}$ "	0100 $\frac{1}{4}$

At the end of Test 22 lbs

Must assume about 23.5 for start <sup>1/221</sup>

DEC. 2<sup>nd</sup> 14

12.

REMARKS

$$K.W. 7.75 = 10.4 H.P.$$

$$85\% \text{ of } 10.4 = 8.82 \text{ less } 10\% 7.93$$

$$\frac{2.52}{8.82} = 32\% \text{ eff. - curve } 38\%$$

Gauge 19" = U.S. Elev. 29.0 City  
+ 6.12 = 35.0 U.S.G.S.

WELL N<sup>o</sup> 7.Dec 3<sup>rd</sup> 1460' pipe in well<sup>13</sup>H.P.  
water.

NEW NUMBER 3.

REMARKS.

TIME	GUAGE WIER	WATTS	Gal per min	Head		
11 A.M	20 lbs 3 $\frac{1}{2}$ "	0100 $\frac{1}{4}$	504.	14 ft	+5 = 19'	2.42
12 Noon	20 " 3 $\frac{1}{2}$ "	0100 $\frac{3}{4}$	"			
1 P.M	20 " 3 $\frac{1}{2}$ "	0101 $\frac{1}{2}$	"			Motor running Hot.
2 "	20 " 3 $\frac{1}{2}$ "	0102	"			
3 "	20 " 3 $\frac{1}{2}$ "	0102 $\frac{3}{4}$	"			
4 "	20" 3 $\frac{1}{2}$	0103 $\frac{1}{2}$	"			This pump very noisy
5 "	20" 3 $\frac{1}{2}$	0104 $\frac{1}{4}$	"			Shaft not true
6 "	20" 3 $\frac{1}{2}$	0105	"			Similar to Pump at N <sup>o</sup> 3.
7 "	20" 3 $\frac{1}{2}$	0105 $\frac{3}{4}$	"			
8 "	20" 3 $\frac{1}{2}$	0106 $\frac{1}{2}$	"			Pump Revolutions
9 "	20" 3 $\frac{1}{2}$	0107	"			per Minute
10 "	20" 3 $\frac{1}{2}$	0107 $\frac{3}{4}$	"			1590
						1584
						1592
						<u>1589</u> Average
11 "	20" 3 $\frac{1}{2}$	0108 $\frac{1}{4}$	"			
12 M	20 3 $\frac{1}{2}$	0109 $\frac{1}{4}$	"			
1 AM	20 3 $\frac{1}{2}$	0110	"			
2 "	20 3 $\frac{1}{2}$	0110 $\frac{1}{2}$	"			
3 "	20" 3 $\frac{1}{2}$	0111 $\frac{1}{4}$	"			
4 "	20 3 $\frac{1}{2}$	0112	"			
5 "	20 3 $\frac{1}{2}$	0112 $\frac{3}{4}$	"			

WELL N<sup>o</sup> 7. DEC. 4<sup>th</sup> 14.

TIME	GUAGE	WIER	WATTS	
6 AM	20"	3 1/2	0113 1/2	507
7 "	20 lbs	3 1/2"	0114 1/2	"
8 "	20 "	3 1/2"	0115	"
9 "	20 "	3 1/2"	0115 3/4	"
10 "	20 "	3 1/2"	0116 1/2	"
11 "	20 "	3 1/2"	0117 1/4	"

At the end of Test - 22 lbs

NEW NUMBER 3. 14

REMARKS

$$7.25 - K.W. = 9.71$$

$$85\% \text{ of } 9.71 = 8.25 - 10\% = 7.42$$

$$\frac{2.42}{7.42} = 32.6\% \text{ eff.}$$

Curve. 35%

$$\text{Gauge } 20" = \text{w. S. Elev. } + 37.6 \text{ City} \\ + 6.12 = 40.72$$



# TEST OF WELL N<sup>o</sup> 8.

DEC. 4<sup>th</sup> 14

NEW N<sup>o</sup> 2

15

TIME	GUAGE	WIER	WATTS	Gal per MIN	Head	REMARKS.
2 <sup>30</sup> pm	23 lbs	3 $\frac{3}{8}$ "	0117 $\frac{1}{2}$	477	7+5 = 12'?	23 lbs at Start
3 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0118 $\frac{1}{4}$	"		
4 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0119	"		Motor Heating
5 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0119 $\frac{3}{4}$	"		
6 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0120 $\frac{1}{2}$	"		Pump Revolutions
7 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0121 $\frac{1}{4}$	"		per Minute
8 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0122	"		1612
9 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0122 $\frac{3}{4}$	"		1608
10 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0123 $\frac{1}{4}$	"		1610
11 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0124 $\frac{1}{4}$	"		<u>1610</u> Average
12 <sup>30</sup> <sup>12:05</sup> AM	23	3 $\frac{3}{8}$ "	0125-	"		
1 <sup>30</sup> "	23	3 $\frac{3}{8}$ "	0126-	"		
2 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0126 $\frac{3}{4}$	"		
3 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0127 $\frac{1}{2}$	"		
4 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0128 $\frac{1}{4}$	"		
5 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0129-	"		
6 <sup>30</sup> "	23 "	3 $\frac{3}{8}$ "	0129 $\frac{3}{4}$	"		
7 <sup>30</sup> "	23 lbs	3 $\frac{3}{8}$ "	0130 $\frac{3}{4}$	"		Lightened Belt.
8 <sup>30</sup> "	23 lbs	3 $\frac{3}{8}$ "	0131 $\frac{1}{2}$	"		

60' Pipe

TEST OF WELL N<sup>o</sup> 8. DEC. 5<sup>TH</sup> 1914.

(CONTINUED)

KEY NUMBER. 2.

16

TIME GAUGE WIER WATTS.

REMARKS.

9 <sup>30</sup>	7 AM	23 lbs	3 $\frac{3}{8}$ inches	0.132 $\frac{1}{2}$	477
10 <sup>30</sup>	"	23 "	3 $\frac{3}{8}$ "	0.133	"
11 <sup>30</sup>	"	23 "	3 $\frac{3}{8}$ "	0.133 $\frac{3}{4}$	"
12 <sup>30</sup>	pm	23 "	3 $\frac{3}{8}$ "	0.134 $\frac{1}{2}$	"
1 <sup>30</sup>	"	23 "	3 $\frac{3}{8}$ "	0.135 $\frac{1}{4}$	"
2 <sup>30</sup>	"	23 "	3 $\frac{3}{8}$ "	0.136	"

At the end of Test - 23 lbs -

$$K.W. 7.75 = 10.4$$

$$85\% \text{ of } 10.4 = 8.82 \text{ lbs.}$$

$$10\% = 7.93$$

Gauge 23" = W.S. Elev. 43.1 C. + 7  
+ 6.12 = 49.22 U.S.G.S

TEST OF WELL N<sup>o</sup> 9. DEC. 6. 14

NEW N<sup>o</sup> 1. 17

TIME	GURGE	WIER	WATTS	GAL PER MIN.	HEAD	H.P. WATER.	REMARKS.	
11 <sup>30</sup> AM	7½ lbs	2 ¾ inch	136½	369.	42 ¾ +	5 = 47 ¾	4.44.	Start at 22 lbs - after
12 <sup>30</sup> pm.	7½ "	2 ¾	137 ¾	"				20 minutes run 7½ lbs.
1 <sup>30</sup>	7½ "	2 ¾	138	"				
2 <sup>30</sup>	7½ "	2 ¾	138 ¾	"				
3 <sup>30</sup>	7½ "	2 ¾	139 ½	"				
4 <sup>30</sup>	7½ "	2 ¾	140 ¾	"				
5 <sup>30</sup>	7½ "	2 ¾	141	"				
6 <sup>30</sup>	7½ "	2 ¾	141 ¾	"				
7 <sup>30</sup>	7½ "	2 ¾	142 ½	"				
8 <sup>30</sup>	7½ "	2 ¾	143 ¾					
9 <sup>30</sup>	7½ "	2 ¾	144					
10 <sup>30</sup>	7½ "	2 ¾	144 ¾					
11 <sup>30</sup>	7½ "	2 ¾	145 ½					
12 <sup>30</sup> AM	7½ "	2 ¾	145 ¾					
1 <sup>30</sup>	7½ "	2 ¾	146 ½					
2 <sup>30</sup>	7½ "	2 ¾	147 ¾					
3 <sup>30</sup>	7½ "	2 ¾	148 ½					
4 <sup>30</sup>	7½ "	2 ¾	149 ½					
5 <sup>30</sup>	7½ "	2 ¾	150					

TEST OF WELL No 9.

[CONTINUED] DEC. 7<sup>th</sup> 14.

TIME	GUAGE	WIER	WATTS	
6 <sup>30</sup> A.M.	7 $\frac{1}{2}$ in.	2 $\frac{3}{4}$ "	150 $\frac{3}{4}$	369
7 <sup>30</sup>	7 $\frac{1}{2}$	2 $\frac{3}{4}$ "	0151 $\frac{1}{2}$	
8 <sup>30</sup>	7	2 $\frac{3}{4}$ "	0152 $\frac{1}{4}$	"
9 <sup>30</sup>	7	2 $\frac{3}{4}$ "	0153	"
10 <sup>30</sup>	7	2 $\frac{3}{4}$ "	0153 $\frac{3}{4}$	"
11 <sup>30</sup>	7	2 $\frac{3}{4}$ "	0154 $\frac{1}{2}$	"

At the end of Test. 21 lbs.  
10 minutes after shutting down.

NEW NUMBER - 1.

18

REMARKS

K.W 8.00 = 10.7 H.P.

85% of 10.7 = 9.1 less 10% =  
8.19

$\frac{4.44}{8.19} = 54\frac{1}{4}\%$  eff.  
curve. 57% -

Gauge 7.5" = W.S. Elev. +14.3  
City +6.12 = 20.42 U.S.G.S

TEST OF WELL No 10.  
DEC 21. 14

TIME	GUAGE	WEIR	WRITS	Cals per min
2 <sup>30</sup> pm	12 lbs	3 <sup>3</sup> / <sub>16</sub> "	0154 <sup>3</sup> / <sub>4</sub>	477
3 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0155 <sup>1</sup> / <sub>2</sub>	"
4 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0156 <sup>1</sup> / <sub>4</sub>	"
5 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0157 <sup>1</sup> / <sub>4</sub>	"
6 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0158	"
7 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0158 <sup>3</sup> / <sub>4</sub>	"
8 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0159 <sup>1</sup> / <sub>2</sub>	"
9 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0160 <sup>1</sup> / <sub>4</sub>	"
10 <sup>30</sup>	14 "	3 <sup>3</sup> / <sub>8</sub> "	0161	"
11 <sup>30</sup>	14	3 <sup>3</sup> / <sub>8</sub> "	0161 <sup>3</sup> / <sub>4</sub>	"
DEC 22 <sup>nd</sup> 12 <sup>30</sup> AM	14	3 <sup>3</sup> / <sub>8</sub> "	0162 <sup>1</sup> / <sub>2</sub>	"
1 <sup>30</sup>	14	3 <sup>3</sup> / <sub>8</sub> "	0163 <sup>1</sup> / <sub>4</sub>	"
2 <sup>30</sup>	14	3 <sup>3</sup> / <sub>8</sub> "	0164 <sup>1</sup> / <sub>2</sub>	"
3 <sup>30</sup>	14	3 <sup>3</sup> / <sub>8</sub> "	0165 <sup>1</sup> / <sub>4</sub>	"
4 <sup>30</sup>	14	3 <sup>3</sup> / <sub>8</sub> "	0166	"
5 <sup>30</sup>	14	3 <sup>3</sup> / <sub>8</sub> "	0166 <sup>3</sup> / <sub>4</sub>	"
6 <sup>30</sup> *	14	3 <sup>3</sup> / <sub>8</sub> "	0167 <sup>1</sup> / <sub>2</sub>	"
7 <sup>30</sup>	14 lbs	3 <sup>1</sup> / <sub>2</sub> "	0168 <sup>1</sup> / <sub>4</sub>	504
8 <sup>30</sup>	14 "	3 <sup>1</sup> / <sub>2</sub> "	0169	"

56'0" of <sup>1</sup>/<sub>4</sub>" Pipe.

19

REMARKS-

21 lbs at Start-

Lower Bearing on  
this Pump runs Hot.

Pump Revolutions

per minute

1590

1584

1592

1589 Average

Tightened Belt-

TEST OF WELL No 10.  
(CONTINUED) DEC. 22<sup>nd</sup>

TIME	GUAGE	WIER	WATTS	
9 <sup>30</sup> AM	14 lbs	3½"	0169 $\frac{3}{4}$	SDY
10 <sup>30</sup>	14 "	3½"	0170 $\frac{1}{2}$	"
11 <sup>30</sup>	14 "	3½"	0171 $\frac{1}{4}$	"
12 <sup>30</sup> pm	14 "	3½"	0172	"
1 <sup>30</sup>	14 "	3½"	0172 $\frac{3}{4}$	"
2 <sup>30</sup>	14 "	3½"	0173 $\frac{1}{2}$	"

At the end of Test. 21 lbs - "

REMARKS -

at 1<sup>05</sup> pm. water got so  
muddy - impossible to see  
screen. 1<sup>25</sup> pm. Fairly

Clear again -

Very dirty at end of  
Test.

14\* GUAGE = W.S. Elev = 13.1 City  
+ 6.12 = 19.2 ~

TEST of WELL No. 11.  
Dec. 23<sup>rd</sup> 1914.

56' 0" of  $\frac{1}{4}$ " Pipe. 21

TIME.	GUAGE	WIER	WATTS.	
1 <sup>30</sup> pm.	11 lbs	3 inches	0174 $\frac{1}{4}$	414
2 <sup>30</sup> "	10 $\frac{1}{2}$ "	3 "	0174 $\frac{3}{4}$	"
3 <sup>30</sup> "	10 $\frac{1}{2}$ "	3 "	0175 $\frac{1}{4}$	"
4 <sup>30</sup> "	10 $\frac{1}{2}$ "	3 "	0176 $\frac{1}{4}$	"
5 <sup>30</sup> "	10 $\frac{1}{2}$ "	3 "	0177	"
6 <sup>30</sup> "	10 $\frac{1}{4}$ "	3 "	0177 $\frac{1}{4}$	"
7 <sup>30</sup> "	10 $\frac{1}{4}$ "	2 $\frac{7}{8}$ "	0178 $\frac{1}{4}$	397
8 <sup>30</sup> "	10 $\frac{1}{4}$ "	2 $\frac{7}{8}$ "	0179	"
9 <sup>30</sup> "	10 $\frac{1}{4}$ "	2 $\frac{7}{8}$ "	0179 $\frac{1}{2}$	"
10 <sup>30</sup> "	10 $\frac{1}{4}$ "	2 $\frac{7}{8}$ "	0180 $\frac{1}{4}$	"
11 <sup>30</sup> "	10 $\frac{1}{2}$ "	2 $\frac{7}{8}$ "	0181	"
12 <sup>30</sup> <sup>Dec. 24.</sup> A.M.	10 $\frac{1}{2}$ "	2 $\frac{7}{8}$ "	0181 $\frac{3}{4}$	"
1 <sup>30</sup> "	10 $\frac{1}{2}$ "	2 $\frac{7}{8}$ "	0182 $\frac{1}{2}$	"
2 <sup>30</sup> "	10 $\frac{1}{2}$ "	2 $\frac{7}{8}$ "	0183 $\frac{1}{4}$	"
3 <sup>30</sup> "	10 $\frac{1}{2}$ "	2 $\frac{7}{8}$ "	0183 $\frac{3}{4}$	"
4 <sup>30</sup> "	10 $\frac{1}{2}$ "	2 $\frac{7}{8}$ "	0184 $\frac{1}{4}$	"
5 <sup>30</sup> "	10 $\frac{1}{2}$ "	2 $\frac{7}{8}$ "	0185	"
6 <sup>30</sup> "	10 "	3 "	0185 $\frac{3}{4}$	414
7 <sup>30</sup> "	8 lbs	3 inches	0186 $\frac{1}{2}$	

REMARKS.

Gauge closed 20 lbs

before starting pumps.

Circuit Breaker thrown

out 7<sup>45</sup> AM Dec 24.

TEST of WELL No 17.  
 [CONTINUED] DEC. 24, 14.

TIME.	GUAGE	WIER.	WATTS	REMARKS.
8 <sup>30</sup> A.M.	8 lbs	3 Inches	0187½ 414	
9 <sup>30</sup>	7½ "	3 "	0188 414	
10 <sup>30</sup>	8 "	3 "	0188¾ 414	
11 <sup>30</sup>	7½ "	3 "	0189½ 414	
12 <sup>30</sup> P.M.	7¼ "	3 "	0190¼ 414	
1 <sup>30</sup>	7 "	3 "	0191 414	

15 min. after end of Test 20 lbs.

Average = 7.7 gal/gal

Gauge 7 = W.S. Elev. of -1.6 + 6.12  
 = 4.52 U.S.G.S

414	397
14	11
1656	397
414	397
5796	4367
4367	
25 ) 10163 (406	
100	
163	
150	

Water very clear.

Practically No Sand.



TEST of WELL No. 12.  
Dec. 26.14

23

TIME	GUAGE	WIER	WATTS	Gals per.min	REMARKS
12 <sup>30</sup> pm.	12 in.	3 $\frac{3}{8}$ "	0191 $\frac{1}{2}$	477	22 lbs before starting
1 <sup>30</sup>	12 "	3 $\frac{3}{8}$ "	0192 $\frac{1}{4}$	"	Pump very noisy -
2 <sup>30</sup>	12 "	3 $\frac{3}{8}$ "	0193	"	Water dirty - full
3 <sup>30</sup>	17 "	3 $\frac{3}{8}$ "	0193 $\frac{3}{4}$	"	of Sand.
4 <sup>30</sup>	17 "	3 $\frac{3}{8}$ "	0194 $\frac{1}{2}$	"	
5 <sup>30</sup>	17 "	3 $\frac{3}{8}$ "	0195 $\frac{1}{4}$	"	
6 <sup>30</sup>	17 "	3 $\frac{3}{8}$ "	0196	"	
7 <sup>30</sup>	17 "	3 $\frac{3}{8}$ "	0196 $\frac{3}{4}$	"	
8 <sup>30</sup>	17 "	3 $\frac{3}{8}$ "	0197 $\frac{1}{2}$	"	
9 <sup>30</sup>	17 "	3 $\frac{3}{8}$ "	0198 $\frac{1}{4}$	"	
10 <sup>30</sup>	11 $\frac{1}{2}$ "	3 $\frac{3}{8}$ "	0199	"	
11 <sup>30</sup>	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0199 $\frac{3}{4}$	"	
12 <sup>30</sup> A.M.	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0200 $\frac{1}{2}$	"	
1 <sup>30</sup>	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0201 $\frac{1}{4}$	"	
2 <sup>30</sup>	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0202	"	
3 <sup>30</sup>	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0202 $\frac{3}{4}$	"	
4 <sup>30</sup>	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0203 $\frac{1}{2}$	"	
5 <sup>30</sup>	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0204 $\frac{1}{2}$	"	
6 <sup>30</sup>	11 $\frac{3}{4}$ "	3 $\frac{3}{8}$ "	0205 $\frac{1}{4}$	"	

TEST OF WELL No 12.  
(CONTINUED) DEC 27. 14.

TIME. GUAGE WIER WATTS.

7<sup>30</sup> A.M. 11½ lbs 3⅜" 0206 "

8<sup>30</sup> " " 3⅜" 0206¾ "

9<sup>30</sup> " " 3⅜" 0207½ "

10<sup>30</sup> " " 3⅜" 0208 "

11<sup>30</sup> " " 3⅜" 0208¾ "

12<sup>30</sup> " " 3⅜" 0209½ "

Water very Sandy.

Wier Box. over ½ Full.

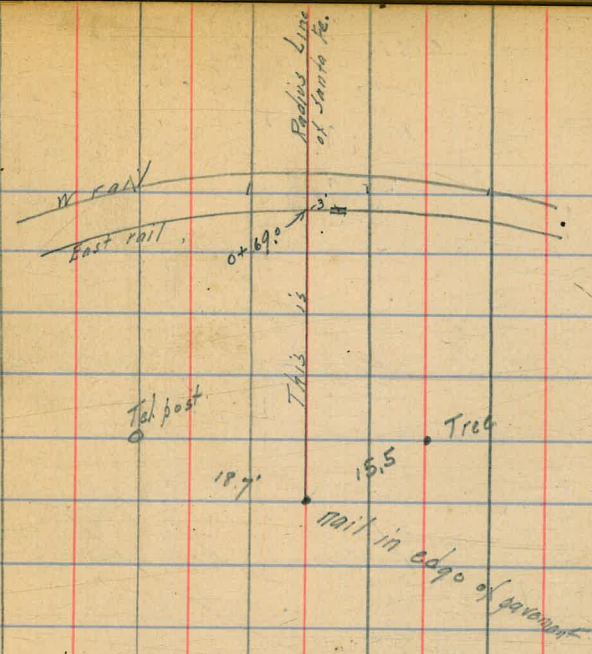
At the end of Test. 15 min. 22 lbs

Gauge 11.5# = W.S.Elev. of +7.4  
City + 6.12 = 13.52 U.S.G.S.

Levels for Over King  
from Morena Blvd.

on Edge of paving. 0+00	-0.58	42 99.42	2.23
+09.0			2.4
+20			0.5
+23			0.9
+25			3.2
+45			5.6
+56			15.4
+65			15.2
+66			14.7
+69 = East rail 3' Set Joint			14.1
+74 = Mast			13.8
+77			14.2
+80			15.3
+86			15.6
+93			11.6
+07.0			13.7
+30			23.2
+50			26.1
+80			27.0

Assumed  
100.00 Top of  
post @ Hydro

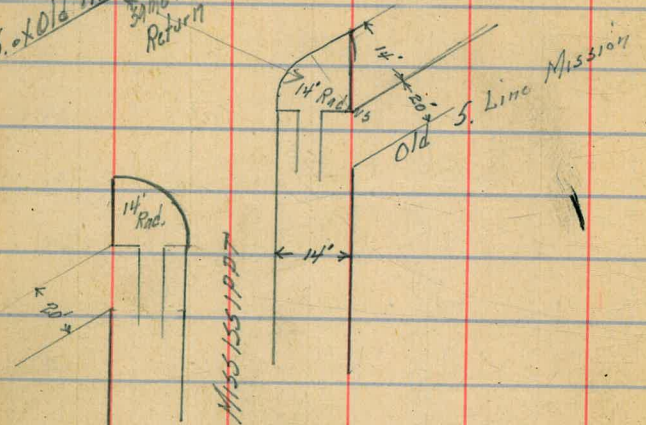


+95 23.0  
2+06.0 = center old La Bolla 22.0

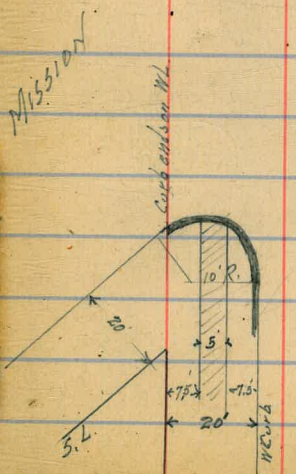
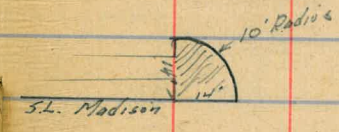
3/9/21 Gregory



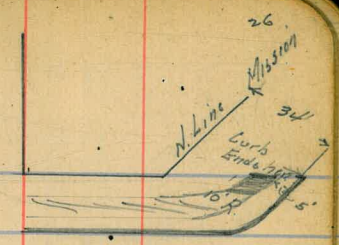
20' S. x Old N. Line  
Same Kind Return



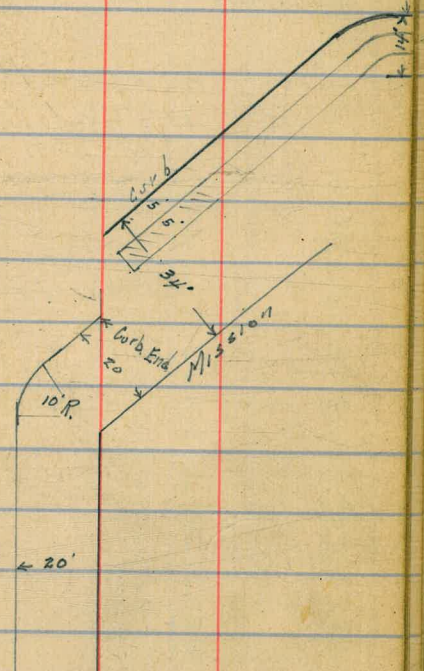
Madison



Louisiana



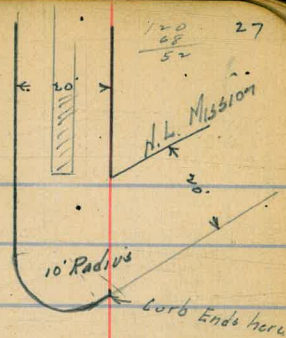
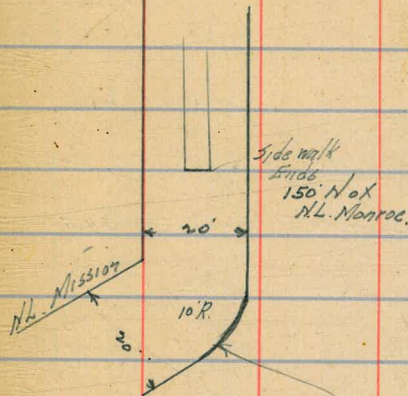
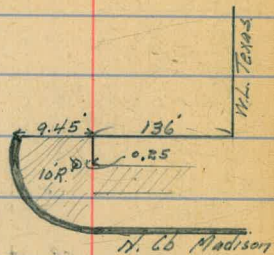
Ave



14' x 5' Curb Limit Madison

Mission

MADISON

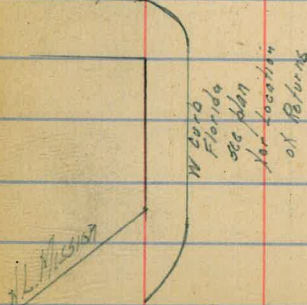


ALYSSA

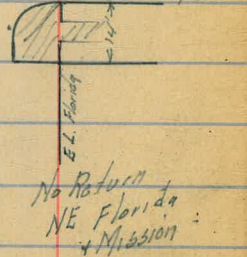
Returns  
like  
No Walk

N.L. Mission

3 Curb Monroe



3 Curb Monroe



5/30/25

Sewer Construction  
 Fern Glen  
 from La Jolla Blvd to Ocean  
 For Location & Profile see sheets 1541L  
 & 221.D.  
 See book 1000-50 for preliminary.

28

Station	Notes	Station	Station	Station	Grade	Elevation
5	5' W. & X W Edge paving 40' W of ex 3L of Fern Glen road	5.53	75.16	70.15	GRADE	+4.65
		0.15	79.16	71.15	66.50	+9.15
			4.51	79.01	62.0	
+50			203	70.13	61.19	+8.94
1			11.12	68.64	60.38	+7.66
	TP	0.72	68.05	11.83	67.33	
+50			1.04	67.01	59.57	+7.44
2			4.50	63.55	58.76	+4.79
					58.0	+2.59
+47.1 = 6' Olivetas = Drop MH			7.46	60.39	50.70	+9.89
3			7.25	60.80	50.05	+10.75
+50			11.81	56.24	49.43	+6.81
	T.P.	3.83	60.13	11.75	54.30	
4			7.26	52.87	48.79	+4.08
+50			4.15	55.38	48.16	+7.22
		12.55	52.38	39.38		
5+02.1 MH @ Monte Vista			0.48	51.90	47.50	+5.40
			2.40	50.53		
+50			1.84	50.54	45.05	+5.49
6. break			5.98	46.40	42.5	3.90
+30			10.08	42.30	38.67	3.63
		11.97	42.01	30.04		
+90 break			5.31	36.70	31.0	+5.70
7+35 MH Δ 31°46' L			6.45	35.56	30.0	+5.56
+68			5.90	36.11	29.49	+6.62
8 break			6.77	35.24	29.0	+6.24
+32.5				24.5		

Stub 8+65

	1923	1926				
4.09	33.46		29.37	on d stub 8+65		
8 + 65 M.H. Δ	11'06" L.	3.42	30.04	20.0		+10.04
9		12.05	21.41	19.22		+2.19
+ 50		3.20	30.26	18.11		+12.15
10		8.91	24.55	17.00		+7.55
+ 50		14.15	19.31	15.89		+3.42
11		13.82	19.64	14.78		+4.86
+ 50		12.77	20.69	13.67		+7.02
12		11.22	22.24	12.56		+9.68
0.02	21.23	12.45	21.21	12.0		+2.74
+ 25 Drop M.H.		6.49	14.74	4.50		+10.24
+ 50		15.20	6.03	4.27		+1.76
13		12.00	9.23	3.81		+5.42
+ 50		9.67	11.56	3.35		+8.21
0.11	8.46	12.88	3.35			
+ 74.5 M.H. at Tank.		1.88	6.78	3.10		+3.68

Sewer Construction from Sta 7+35 Fern Glenn Line

	To Monte Vista and North					
00 = 7+35.0 DMH Fern Glenn	11.97	42.101	30.04			on d stub sta 8+65
0 + 63.65			6.45	35.56	23.00	+2.56
12.58	52.38	1.79	40.22	36.50		+3.72
1 + 27.3 M.H. Monte Vista	3.03	50.57	2.14	39.83		
1 + 81.17			4.84	47.54	40.00	+7.54
2 + 35.05			3.42	47.56	40.97	+6.78
2 + 88.92			3.90	47.15	40.75	+5.92
3 + 42.8 DE. 40' set Arched			4.38	46.67	41.17	+5.07
			4.71	46.19	41.50	+4.36

FERN GLEN

29

255  
591

27  
10  
10

93

4/30/25 Sewer Construction  
NEPTUNE PL.

27.32

5.8

650  
177  
4781  
3715

55  
177  
2970  
2490  
319

50  
211  
570  
232  
261

30

8.46 from page 29

M.H. at Tank #2  
= 8+21.19

		1.68	6.78	3.5	+3.28
	(no. 11)	0.85	7.61	3.72	+3.89
7+56.65	M.H. Δ 8°10' L	10.53	9.58	3.94	+5.64
7		2.43	6.03	4.33	+1.70
6+60	M.H. Δ 81°04' R 12.50 20.11	3.07	+5.39	4.60	+0.79
6		0.85	7.61		
		7.07	13.04	8.08	+4.96
5+50		5.44	14.67	10.98	+3.69
5		3.10	17.01	13.88	+3.13
				16.50	+5.01
4+55	Drop M.H. 71°0' L 0.94 33.65	12.14	21.51	19.50	+2.01
			32.71		
4		5.02	28.63	20.16	+7.47
3+50				20.76	
3+30	M.H. Δ 31°30' R	4.84	28.81	21.00	+7.81
3		4.89	28.76	21.15	+7.61
2+50		4.75	29.90	21.40	+7.50
2		4.25	29.40	21.65	+7.75
1+50					
1+40	Cl. Belvedere. Δ 2°06' R Drop M.H. from Belvedere 464		28.97	21.95	+7.02
1+00		4.76	28.89	22.15	+6.74
0+50		5.18	28.47	22.40	+6.07
0.0				22.65	+5.24

BM Book 1000 P 49



Neptune Place

book 1000 page 56  
33.65

0+00	5.76	27.89	22.65	+ 5.24
+ 50	5.60	28.05	22.90	+ 5.15
1	5.14	28.51	23.15	+ 5.36
+ 34	4.84	28.81	23.32	+ 5.49

Sewer Construction

12 Alley bet Benjamin & Nantuxis

52.73

00-MH. & Cross Alley	2.56	50.17	42.00	+ 8.17
TP 10.96	61.73	2.56	50.17	
+ 50	9.66	51.47	43.33	+ 8.14
1+00	9.16	51.97	44.66	+ 7.31
+ 50	8.65	52.48	46.99	+ 6.49 ✓
2+00	10.14	50.99	47.32	+ 3.67
+ 50	6.74	54.39	48.65	+ 5.74
3+00	4.88	56.25	49.98	+ 6.27
3+60 MH=00	3.47	57.66	51.56	+ 6.10
+ 50	2.04	59.09	52.89	+ 6.20
1+00	0.61	60.52	54.22	+ 6.30
TP 11.76	72.28	0.61	60.52	
+ 50	10.63	61.65	55.55	+ 6.10
2+00	9.45	62.83	56.88	+ 5.95
+ 50	8.25	64.03	58.21	+ 5.82

7228

3+00			7.10	65.18	59.54	+5.64
3+60 M.H. = 00			5.44	66.84	61.13	+5.71
750			4.18	68.10	62.47	+5.63
1+00			3.00	69.28	63.81	+5.47
450			2.02	70.26	65.16	+5.10
2+00			0.48	71.80	66.50	+5.30
+P	8.70	80.50	0.48	71.80		
450			7.30	73.20	67.84	+5.36
3+00			5.94	74.56	69.18	+5.38
3+62.5 D.F.			4.31	76.19	70.80	+5.39
T.P.	4.98	83.31	2.17	78.33		
4+KombM			4.25	79.06		
					79.06	
						SE West Bench L. J. 11-13-14
T.P.			6.80	76.51		

# # 2 OUTFALL

8.46 H 2 from page 29

1181  
999  
1180

33

0+00 = Tank End.

-2.5

+41.37

9.50

-1.04

-4.0

+2.96

+82.74

10.02

-1.56

-5.5

+3.94

1+24.11

13.08

-4.62

-7.0

+2.38

1+65.5 = break

15.80

-7.34

-8.50

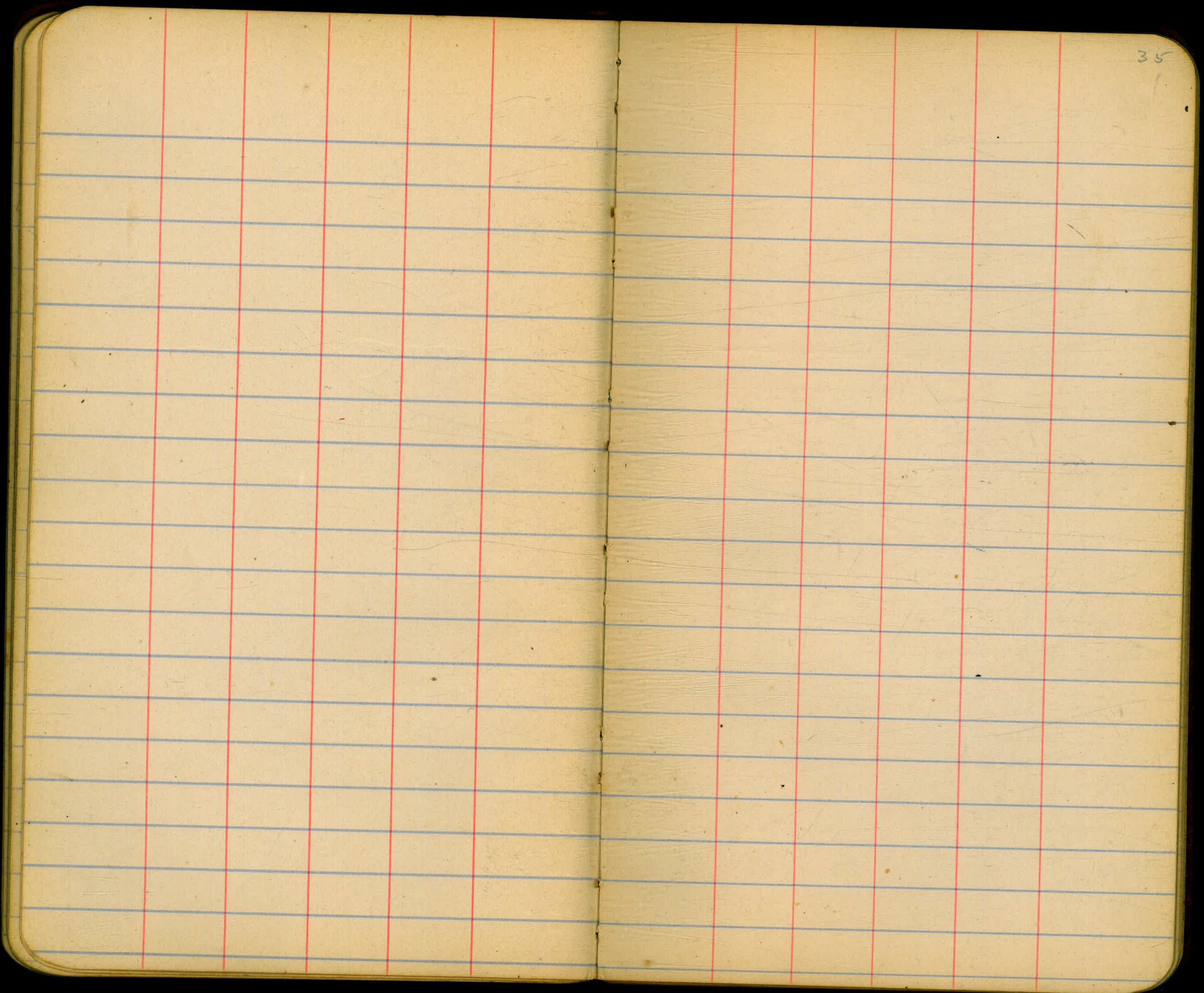
+1.16

Sewer Construction in Sutton Place  
from D.M.H. sta H+55 Neptune Line E. to DE

H+55 Neptune Line = 00				16.50		
M.H. 0+50				20.00		
BrK 1+0.2, 5				29.00		
1+55				31.25		
↳ Vista Del Mar						
M.H. 2+07.5	12.78	51.27	38.49	33.50	+4.99	
4+87						
2+57.37		10.31	40.96	35.62	+5.34	
3+07.25		8.73	42.54	37.75	+4.79	
3+57.12		6.65	44.62	39.87	+4.75	
4+07.0 BrK		4.24	47.03	42.00	+5.03	
4+56.33		2.56	48.71	43.16	+5.55	
5+05.67		1.56	49.71	44.33	+5.38	
5+55.0 = DE		1.48	49.79	45.50	+4.29	

Olivetias from Prop. M.H. in Fern Glen No DE  
48.05

Prop. D.M.H. in Fern Glen				50.70	+2.57	
+50		8.90	59.15	51.00	+9.15	
1+00		6.43	61.62	51.30	+10.32	
1+50		7.12	60.93	51.60	+7.33	
2+00		7.92	60.13	51.90	+8.23	
2+50		8.73	59.32	52.20	+7.12	
3+00		9.52	58.53	52.51	+6.02	
3+50		10.33	57.72	52.82	+4.90	
3+80		10.73	57.32	53.00	+4.32	



Sewer Construction  
in Alley bet Nautilus & Westbourne Sts.

36

T.P.	124	77.75	76.51	Page 32	
00=DE 25' w/ft to Jolla Blvd		0.10	77.65	72.00	+5.65
+50		1.67	76.08	70.95	+5.23
100		2.67	75.04	69.71	+5.37
150		4.31	73.44	68.57	+4.87
200		5.62	72.13	67.42	+4.70
250		6.55	71.20	66.29	+4.91
300		7.70	70.05	65.15	+4.90
3+6 2.5# MH=00		9.10	68.65	63.72	+4.93
+50		10.13	67.62	62.57	+5.05
1+00		11.22	66.53	61.43	+5.10
T.P. 1.00	67.53	11.22	66.53		
+50		2.10	65.43	60.29	+5.14
2+00		3.35	64.18	59.15	+5.03
+50		4.24	63.29	58.01	+5.28
3+00		4.81	62.72	56.87	+5.85
3+60=MH=00		6.23	61.30	55.50	+5.80
+55		7.20	60.23	54.50	+5.73
1+10		8.29	59.24	53.50	+5.74
1+65		9.56	57.97	52.50	+5.47
B+K 2+20		11.03	56.50	51.50	+5.00
T.P. 0.83	57.33	11.03	56.50		
2+60		1.83	55.50	49.93	+5.57

57.33

3+10		4.04	53.29	47.97	+5.32
3+60 M.H. of Cross Alley = 00 T.P. 1.25 5031		8.27	49.06	46.00	+3.06
+50		1.00	49.31	43.78	+5.53
1+00		2.34	47.97	41.55	+6.42
1+50		3.66	46.65	39.33	+7.32
40.75					
1+70.75 M.H. in Westbourne St		4.51	45.80	37.51	+8.29

Sewer Construction

16 N of E of Westbourne St Neptune Place East

T.P.	0.37	38.73	11.95	38.36	
00 = M.H. Neptune Place		9.75	28.99	23.32	+5.66
+55.83		6.37	32.36	28.05	+4.31
1+11.67		0.37	38.36	32.78	+5.58
1+47.50 M.H. of Cross Alley	50.31			37.52	+8.29
55 T.P.	12.43	62.74	200	50.31	
2+22.50		12.21	50.53	42.26	+8.27
2+77.50 B.K.		10.29	52.45	47.00	+5.45
50.13					
3+28.33		8.03	54.71	48.33	+6.38
3+79.16		6.32	56.42	49.67	+6.75
4+30.00 M.H.		5.20	57.54	51.00	+6.54
4+80		4.14	58.56	52.35	+6.21

		62.74				
5+30			2.73	60.01	53.71	+6.30
5+80			1.68	61.06	55.06	+6.00
T.P.	5.60	67.80	0.54	62.20		
6+30			4.96	62.84	56.42	+6.42
6+80			4.33	63.47	57.78	+5.69
7+25 = D.E. now of Monte Vista			3.15	64.65	59.00	+5.65

## Sewer Construction

of Belvedere St from D.M.H. Neptune Place to M.H. of Monte Vista

Then S. & E. to D.E. in BIK 6

	12.37	41.35		28.99	stn B. Neptune & west pour in Page 37	
00 = D.M.H. in Neptune Place			11.98	29.37	25.50	+3.87
54.4			8.51	32.84	28.70	+4.14
1+08.8			3.57	37.78	31.90	+5.88
T.P.	12.98	53.82	0.51	40.84		
1+63.2			11.21	42.61	35.10	+7.51
2+17.6			7.61	46.21	38.30	+7.91
2+72 = M.H. of Vista Do/Max = 00 H5:42			7.17	46.65	41.50	+5.15
+45.42			5.13	48.69	43.08	+5.61
+90.84			33.3	50.49	44.66	+5.83
1+36.26			1.44	52.38	46.25	+6.13



		53.82					
T.P.	12.24	66.06	0.00	53.82			
1+81.68			12.24	53.82	47.83		+5.99
2+27.10			11.07	54.99	49.41		+5.58
2+72.5 = M.H. = 00			9.76	56.30	51.00		+5.30
+50			8.80	57.26	51.73		+5.53
1+00			8.16	57.90	52.46		+5.44
1+50			7.96	58.10	53.19		+4.91
2+00			7.62	58.44	53.92		+4.52
2+40 = M.H. & Monte Vista = 00			7.27	58.79	54.50		+4.29
+50			5.42	60.64	55.75		+4.89
1+00			3.92	62.14	57.00		+5.14
1+40 = M.H. & BIKG = 00			3.04	63.02	58.00		+5.02
+50			1.32	64.74	58.98		+5.76
1+00			0.70	65.36	59.97		+5.39
T.P.	12.78	78.14	0.70	65.26			
+50			12.40	65.74	60.96		+4.78
2+02.5 = M.H. = 00			11.42	66.72	62.00		+4.72
+50			8.90	69.24	63.61		+5.63
1+00			7.98	70.16	65.22		+4.94
1+50			5.69	72.45	66.83		+5.62
2+00			3.63	74.51	68.45		+6.06
2+32.5 = D.F.			2.78	75.36	69.50		+5.86

Sewer Construction  
Alley Bet Center & Arenas

40

RM.	12.86	80.60		27.74	N.W. Arreaga & La Jolla Blvd	
00=4' W of Pavmg			12.47	68.13	65.00	+3.13
+27			11.30	69.30	65.50	+3.80
0+74B <sup>H</sup>			9.37	71.23	66.00	+5.23
1+25.67			6.80	73.80	68.67	+5.13
1+77.34			3.53	77.07	71.34	+5.73
2+29.0			1.25	79.35	74.00	+5.35
TP	12.18	92.04	0.74	79.86		
2+80.67			10.73	81.31	76.67	+4.64
3+32.34			7.26	84.78	79.34	+5.44
3+84.00 MH			4.07	87.97	82.00	+5.97
4+34.52			0.93	91.11	84.25	+6.86
TP	11.60	103.35	0.29	91.75		
4+85.05			9.03	94.32	87.50	+6.82
5+35.57			6.51	96.84	90.25	+6.59
5+86.10			4.02	99.33	92.00	+7.33
6+36.62			1.08	102.27	95.75	+6.52
TP	12.55	115.68	0.22	103.13		
6+87.15			10.55	105.13	96.50	+8.63
7+37.67			8.31	107.37	101.25	+6.12
7+88.70 M.H. & Drive			5.90	109.78	104.00	+5.78
8+39.87			3.28	112.40	106.25	+6.15
8+91.54			1.48	114.20	108.50	+5.70
TP	10.94	126.08	0.54	115.14		
9+43.20			9.19	116.89	110.75	+6.14

124.08

9+94.87		7.06	119.02	113.00	+6.02
10+46.54		5.01	121.07	115.25	+5.82
10+89.20 D.M.H. & X Alley		2.89	123.19	117.50	+5.69

Sewer Construction

in Rushville St

10.08

81.23

71.15 Page 28

00=D.M.H. W of Paving		11.92	69.31	65.00	+4.31
+50		7.56	73.67	67.31	+6.36
1+00		4.87	76.36	69.61	+6.75
+50		3.34	77.89	71.92	+5.97
2+00 TP 12.81	93.60	0.44	80.79	74.23	+6.56
+50		10.07	83.53	76.53	+7.00
3+00		8.06	85.54	78.84	+6.70
+50		6.38	87.22	81.15	+6.07
3+90 M.H.=00		4.46	88.94	83.00	+5.94
+50		1.94	91.66	85.50	+6.16
TP 12.80	106.06	0.34	93.26		
1+00		12.12	93.94	88.00	+5.94

	106.06					
1450		8.91	97.15	90.50	+6.65	
2400		6.45	99.61	93.00	+6.61	
+50		3.82	102.24	95.50	+6.74	
3400 Brk		1.72	104.34	98.00	+6.34	
+50 TP	1238	117.89	0.55	105.51	99.00	+6.51
4400 M.H. & Draper		11.22	106.67	100.00	+6.67	
+55		11.00	106.89	101.00	+5.89	
1410 Brk		9.50	108.39	102.00	+6.39	
1460		5.01	112.88	106.00	+6.88	
2410		1.46	116.43	110.00	+6.43	
TP	11.03	128.83	0.09	117.80		
2460 DE		7.75	121.08	114.00	+7.08	

Sewer Construction  
 14 hrs Alley Bet Draper & Eads

	5.90	129.09	123.19	Page 41	
00 = DE S. of Center	6.91	122.18	118.50		+3.68
+55	6.57	122.52	118.00		+4.52
1+10 = D.M.H. # 8 W Alley	5.90	123.19	117.50		+5.69
" " " " " " " " = 00	5.90	123.19	118.50		+4.69
+51.66	5.87	123.22	219.00		+4.22
1+03.33	5.56	123.53	219.50		+4.03
1+54.99	5.34	123.75	220.00		+3.75
2+06.66	4.76	124.33	220.50		+3.83
2+58.33	3.74	125.35	221.00		+4.35
3+10.00 = DE 40' N. of Rushville	3.31	125.74	221.50		+4.28
TP. 3.05 128.83	3.31	125.78			
00 = DE 4222 S. of Rushville	6.45	122.38	118.50		+3.88
0+56.67	7.45	121.38	117.66		+3.72
1+13.34	6.34	122.47	116.82		+5.64
1+70.00 BTK	7.67	121.16	116.00		+5.16
2+20	10.91	117.92	113.50		+4.42
TP 0.52 117.03	12.22	116.51			
2+70	2.45	114.58	111.00		+3.58
3+20 M.H. # 1 + Westbourne	3.11	113.92	108.50		+5.42

Sewer Co  
11th Alley bet Fern Glen & West Bourne

44

117.03

00 = M.H. & NeSA 11.11			3.11	113.92	108.50	+5.42
+51.67			5.26	111.77	106.42	+5.35
1+63.33			7.46	109.57	104.23	+5.24
1+55.00			8.68	108.35	102.25	+6.10
2+06.66			10.32	106.71	100.17	+6.54
2+58.33			12.71	104.32	98.08	+6.24
T.P. 00.8	104.20		12.91	104.12		
3+10 M.H. & Draper 200			2.50	101.76	96.00	+5.76
+50			5.27	98.93	94.23	+4.70
1+00			7.03	97.17	92.46	+4.71
+50			8.97	95.13	90.69	+4.44
2+00			11.06	93.14	88.92	+4.22
T.P. 0.49	92.01		12.68	91.52		
+50			1.12	90.89	87.15	+3.74
3+00			2.41	89.60	85.38	+4.22
2+50			3.63	88.38	83.61	+4.77
1			3.85	88.16	82.50	+5.66
3+80.8 = M.H. = 20			3.49	88.52	81.00	+7.52
+50.75			5.76	86.25	79.50	+6.75
1+01.50			6.50	85.51	78.00	+7.51
1+52.25			8.31	83.70	76.50	+7.20
2+03.00						

92.01

2+53.75		70.03	81.98	75.00	+6.98
3+54.50		11.72	80.29	73.50	+6.79
T.P. 0.18	79.53	12.66	79.35		
3+58.25		0.88	78.65	72.00	+6.65
4+61-M.H. into La Jolla Blvd		4.90	74.63	70.50	+4.13

Sewer Con

4' w of Paving on La Jolla Blvd  
79.56

00 = MH 200'S of Fern Glen				70.50	+4.13
+50		5.66	73.90	69.50	+4.40
1+00		6.81	72.75	68.50	+4.25
+50		7.95	71.61	67.50	+4.11
2+00 = DM.H. in Fern Glen		8.41	71.15	62.00	+9.15
				64.50	+4.65
3+00 = " " " " " "				62.00	
+50		8.79	70.77	62.25	+8.52
1+00		9.18	70.38	62.50	+7.88
+50		9.61	69.95	62.76	+7.19
2+00 DM.H. T.P. 3.09	72.40	10.25	69.31	63.03	+6.28
+50		3.18	69.22	63.29	+5.93
1+00		3.55	68.85	63.55	+5.30

69.31  
63.29  
63.55

72.40

1+50	3.90	68.50	63.81	+ 4.69
2+00	4.39	68.01	64.07	+ 3.94
+50	4.43	67.97	64.33	+ 3.64
3+00	4.27	68.13	64.59	+ 3.55
3+50	4.13	68.27	64.85	+ 3.42
3+80MH			65.00	



Sewer Construction  
 & ALLEY BLK 8 La Jolla Strand  
 SHEET 1#50 L 1540 L

1282  
 6.5  
 5128  
 7692  
 82048

47

56.92

101.5' E of EL Vista del Mar = 0+00 63.46	11.78	45.14	38.80	+6.34
0+63.9 = M.H.	11.61	51.95	47.00	+4.85
1+17.9	8.18	55.28	49.10	+6.18
1+71.9	5.72	57.74	51.20	+6.54
2+25.9	5.22	58.24	53.80	+4.94
2+79.9	3.28	60.18	55.40	+4.78
3+33.9 = M.H. 7.08 75.94	1.28	62.18	57.50	+4.68
3+87.9	10.1	65.84	59.60	+6.24
4+41.9	7.74	68.20	61.70	+6.50
4+95.9	6.42	69.52	63.80	+5.72
5+49.9	4.66	71.28	65.90	+5.38
6+03.9 = M.H. 15' west La Jolla Δ	3.20	72.44	68.00	+4.64
6+48.9	2.43	73.51	68.37	+5.14
6+93.9	1.50	74.44	68.75	+5.69
7+38.9	0.67	75.27	69.12	+6.15
7+83.9 D.E. 15' west La Jolla	0.06	75.84	69.50	+6.38

103.9  
 239.9  
 2700

103.9  
 693.9  
 1000

Sewer Construction  
 & ALLEY BLK 11  
 La Jolla Strand  
 SHEET ~~1450~~ 1540L

	T.P.	896	51.5	51.77			
120' EXCEL Vista Del Mar 100		60.73		12.81	47.92	43.07	+4.85
0+45				6.37	54.36	48.79	+5.57
0+90 M.H.				1.11	59.62	54.50	+5.12
	T.P.	12.94	73.47	0.20	60.53		
1+38.57				11.29	62.18	56.35	+5.83
1+77.14				10.02	63.45	58.23	+5.22
2+35.71				8.53	64.94	60.09	+4.85
2+84.28				6.39	67.08	61.94	+5.14
3+32.85				4.41	69.06	63.79	+5.27
3+81.42				2.24	71.23	65.65	+5.58
4+30.00 DE				0.30	73.17	67.50	+5.67

Sewer Construction  
 ALLEY BLK 13  
 La Jolla Strand.  
 SHEET 1450 L

14-

49

M.H. Vista Del Mar 50+00	42.89	40.67	32.22	26.00	+6.22
0+60		4.18	38.71	33.50	+5.21
1+20	54.76	9.25	45.51	41.00	+4.51
1+80		1.25	53.51	48.50	+5.01
2+40 M.H.	67.48	7.94	59.54	56.00	+3.54
3+00		4.30	63.18	58.14	+5.04
3+60		1.41	66.07	60.28	+5.79
4+20	80.27	11.79	68.48	62.43	+6.05
4+80		9.80	70.47	64.57	+5.90
5+40		7.64	72.63	66.72	+5.91
6+00		5.58	74.29	68.86	+5.83
6+60 M.H. 15' wide La Jolla Blvd		2.57	77.70	71.00	+6.70
+425 N		2.13	78.14	71.37	+6.77
+85:		1.79	78.49	71.75	+6.73
1+7.5		1.36	78.91	72.12	+6.79
+170 N of M.H. = DE		2.00	78.27	72.50	+5.77
+42.5 S of M.H.		3.26	77.01	71.30	+5.71
+85.5 - - - = DE		3.64	76.59	71.60	+4.99

73.47  
 0.76  
 72.71  
 7.56  
 80.27  
 12.83  
 67.44  
 0.24  
 67.48  
 12.81  
 54.67  
 0.09  
 54.76  
 12.74  
 42.02  
 0.87  
 42.89  
 30.42  
 12.47

4.52  
 78.85

Vista Del Mar  
 53.75 S of Alley 983 53.06 +6.66  
 107.5 - - - DE 899 34.90 +7.30  
 26.00  
 26.00

Sewer Construction in Alley 5/29/25  
bet Tave Girard & Pearl Line to Center

B.M. B.P. S.E. Pearl & Girard 115.05

50

BM	11.74	126.79		115.05	S.E. Pearl & Girard	
TP	10.60	137.12	0.27	124.52		
00= existing DE				112.77		
+24 D.M. Hon. PL			8.33	128.79		+7.79
50.77				121.00		+7.79
0+74.77			6.20	130.92		+7.86
1+25.54 $\Delta 10.00$			4.21	132.71		+7.78
54.25 T.P.	12.06	147.63	1.35	135.57		
1+79.79			12.94	137.79		+7.45
2+34.04			10.44	137.19		+7.63
2+88.29			9.30	138.32		+7.65
3+42.54 M.H.			7.39	140.24		+6.34
53.75				134.00		
3+96.29			5.00	142.63		+6.38
4+50.04			2.35	145.28		+6.78
TP	11.99	158.73	0.89	146.74		
5+03.79			11.24	147.49		+6.74
5+57.54 B.K.			8.83	149.90		+6.90
47.5				143.00		
6+5.04			7.01	151.72		+7.97
6+52.54			4.95	153.78		+9.28
TP	2.87	149.90	11.70	147.03		
chance N.E. Center & Fay			4.96	144.94		
T.P. for BM Top Hydrant			1.76	148.14	S.E. Center & Fay	

Sewer Box Structure  
In Keys 12-7-6-5.

	5.07	88.87	83.80 BM Rosemonts Electric			
00 = DE in Palmer			9.32	79.55	75.90	+ 3.65
+ 56.5			5.25	43.62	75.51	+ 8.11
1 + 13.0			4.24	44.63	75.13	+ 9.50
1 + 69.5			3.61	85.26	74.75	+ 10.51
2 + 260 R.M.H. Rosemont St. 00			6.10	82.77	74.37	+ 8.40
+ 46.25			3.94	84.93	74.06	+ 10.87
+ 92.56			4.92	83.95	73.74	+ 10.21
1 + 38.84			5.76	83.11	73.43	+ 9.68
1 + 85.12			4.36	82.51	73.12	+ 9.39
2 + 31.40			6.62	82.25	72.91	+ 9.44
2 + 77.65 M.H. 00			7.36	81.51	72.50	+ 9.01
+ 34.47			8.75	80.12	72.00	+ 8.12
1 + 08.94			9.91	78.96	71.50	+ 7.46
1 + 63.91 T.P. 0.14	77.67	11.38	77.49	71.00		+ 6.49
2 + 17.88			1.85	75.82	70.50	+ 5.32
2 + 72.35 M.H. & Gravel			4.48	73.19	70.00	+ 3.19
+ 49.75			5.56	72.11	68.25	+ 3.86
+ 99.50			7.45	70.22	66.50	+ 3.72
1 + 49.25			9.05	68.63	64.75	+ 3.87
TR	4.58	70.62	11.63	66.04		
1 + 99 DMH.					63.00	

	70.62				
1+99 DMH = 00		11.48	59.94	59.00	
+54.5 MH		4.13	66.49	58.56	+7.93
† 1+09 M.H = 00		7.98	62.64	58.13	+4.51
+44.75 P. 3.97	68.03	6.56	44.06	57.76	+6.30
+89.50		5.37	62.66	57.40	+5.26
1+34.25		6.71	61.32	57.04	+4.28
1+79 = M.H. = 00		8.43	59.60	56.68	+2.92
+42		6.19	61.84	56.34	+5.50
+84 = M.H. = 00		5.68	62.35	56.00	+6.35
+34.5		7.13	60.90	54.58	+6.32
+73 = connection existing sewer		8.14	59.89	53.17	+6.72
+66.50 = M.H. 0+84 above		3.57	64.46	58.00	+6.46
+126. = DE. & Gravel		2.85	65.18	60.00	+5.18

Sewer Construction  
 1<sup>st</sup> Rosemont & Electric Ave

	5.07	88.87	83.80 BM Elect Rosemont		
00 = DM.H & Alley Rosemont		6.10	82.77	77.00	+5.77
+41.67		5.66	83.21	77.33	+5.88
+83.34		5.60	83.27	77.67	+5.60
1+25 = MH & Rosemont & Electric Ave		5.51	83.34	78.00	+5.34
+42.5 No palove MH		5.55	83.32	78.50	+4.82
+85 DE		6.00	82.87	79.00	+3.87
+40 S. of MH & Rosemont & Electric		4.92	83.75	79.33	+5.62
+80		4.70	84.17	79.67	+5.50
	8.12	91.92	83.80 BM		
1+20 = DE		8.02	83.90	79.00	+4.90

Sewer Construction  
 1/2 Monte Vista & 1/2 Marine St

8/2/75  
 mll.

BM	12.91	49.17	36.26	M.W. Sea Lane + Vista Del Mar	
T.P.	7.46	56.82	0.21	48.76	
PT with Present Sewer 00 = 1/2 Monte Vista + Sealane			7.35	49.47	43.50 +5.97
0+64.82 = M.H.			5.07	51.75	43.82 +7.93
1+53.33			4.70	52.12	44.09 +8.03
1+06.66			4.65	52.17	44.35 +7.82
1+60.00			4.94	51.88	44.62 +7.26
2+13.33			5.08	51.74	44.89 +6.85
2+66.66			5.73	51.09	45.15 +5.94
3+20.00 M.H. & Marine			5.97	50.85	45.42 +5.43
+57.59			5.86	50.96	45.71 +5.25
1+15.18 D.E.			7.13	49.69	46.00 +3.69
		Marine St			
4 Marine	9.14	59.99	50.85		
00 = M.H. & Monte Vista			7.60	52.39	45.42 +5.43
0+46.25			7.60	52.39	47.44 +4.95
0+92.50			5.82	54.17	49.46 +4.71
1+38.75			3.70	56.29	51.48 +4.81
1+85 D.E.			1.76	58.23	53.50 +4.73



Sewer Construction  
From Existing Sewer in Sealane To M.H.  
1/4 Fern Glen

8/6/25  
mils.

N.W. Sealane  
Vista Del Mar

55

11.7

BM	0.01	26.27		36.26			0.13	36.39	36.26	
J.P.	0.22	23.87	12.92	23.35			0.44	24.73	12.10	24.29
with existing TP	4.44	17.58	10.43	13.14					8.45	16.28
00=Fl. 4" Pipe in Sealane										4.4
0+50		7.90	9.68	6.52	+3.16					11.68
1+00		8.95	8.63	6.14	+2.49					11.88
1+50		9.51	8.07	5.76	+2.31		24.73	10.61	14.12	M.H. 11.68
2+00		10.00	7.54	5.38	+2.20		0.45	14.57	8.91	5.66
2+50		10.42	7.16	5.00	+2.16			10.76	3.81	5.1-FL
3+00		9.77	8.36	4.62				11.47	3.10	Manhole at Tank
3+16 M.H. 17" 00 R		9.22	8.36	4.30	+3.86			9.93	4.64	Top of Tank
3+50		9.27	8.31	4.34	+3.97					
4+00		8.02	9.56	4.11	+5.45		4.40	18.52	14.12	F.L. Manhole 225' S. of Sealane
4+50		9.04	8.54	3.84	+4.66			10.79	7.73	
5+00		10.63	6.95	3.66	+3.30			12.05	6.47	Top of Pipe w. of Wall
5+50		5.83	11.75	3.42	+8.33					
6+00		14.45	3.13	3.19	-0.06					
Existing M.H. 6+30 = M. Fern Glen		14.52	3.06	3.06	Flow line					

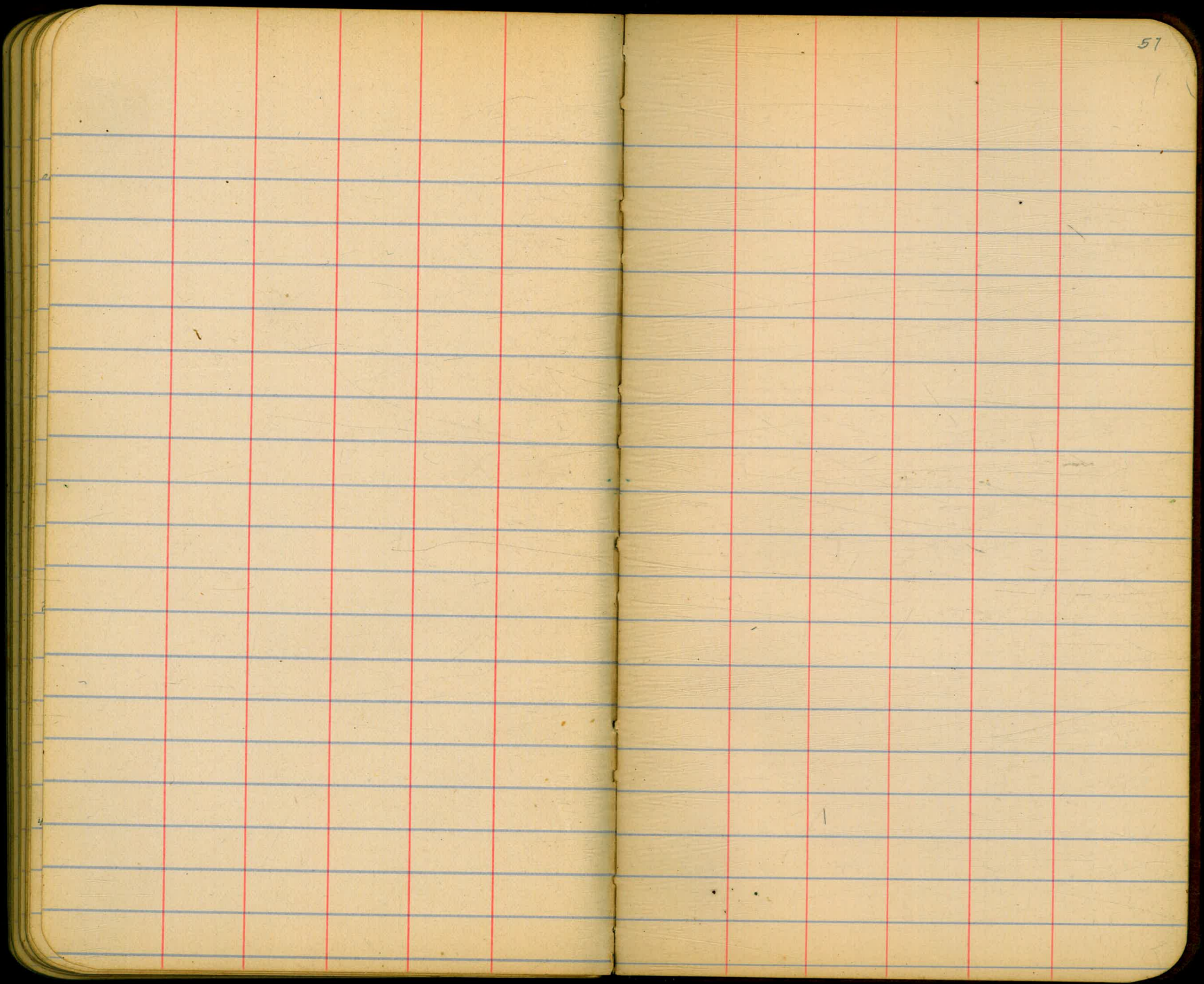
Sewer Construction  
 \$ Sea Lane from P.I. with Sewer Page 55  
 To M.H. & Monte Vista

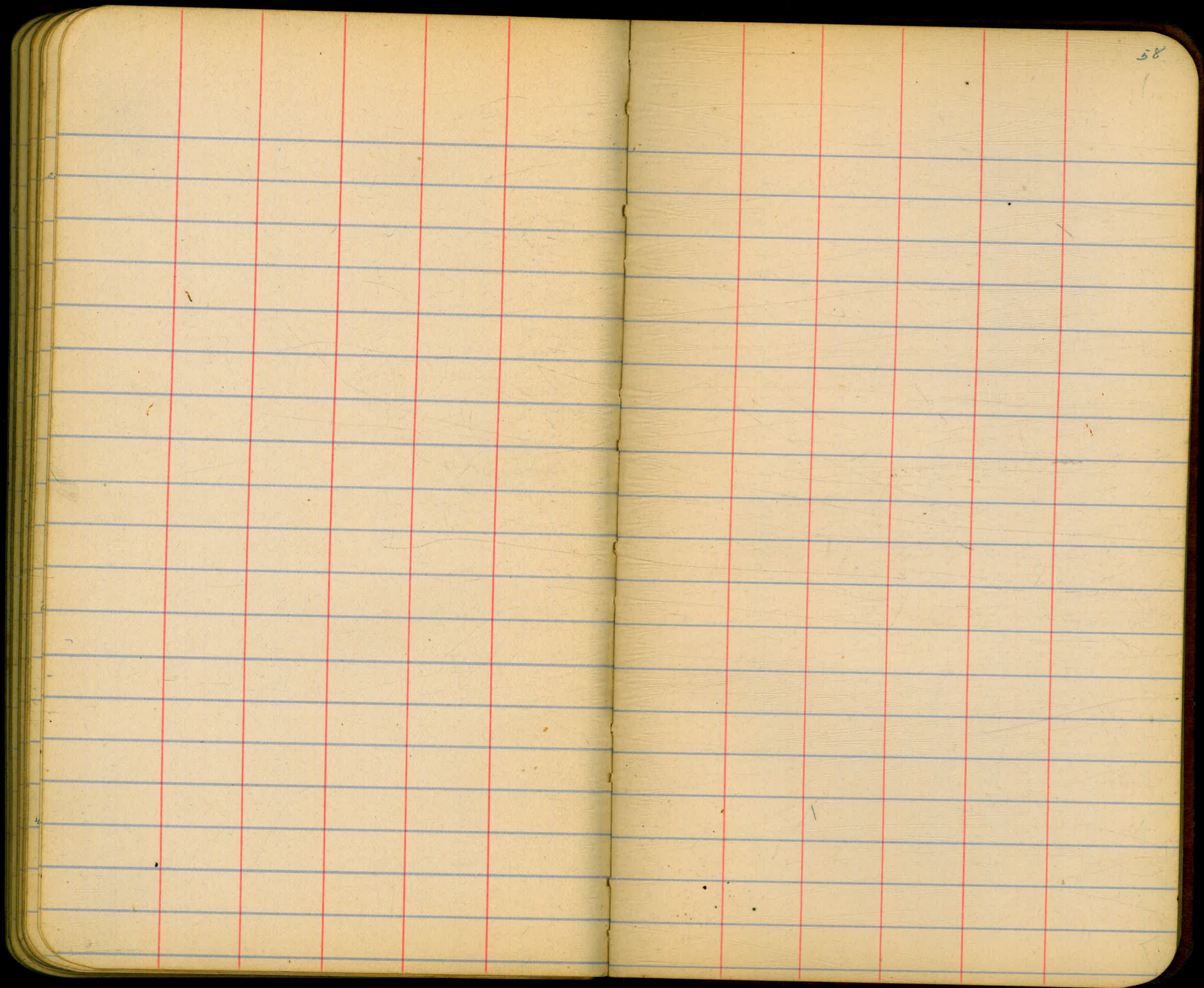
	T.P.	8.51	21.65	Ground & Sea Lane	13.14	Page 55
ea = New P.I. 8' 3" of Present Pipe in Sea Lane				11.9	10.75	
+15				9.2	12.45	
+20				7.2	14.45	
+35				5.5	16.15	
+50				3.8	17.85	
T.P.	12.25	33.88	0.12	21.53		
1+00				10.6	23.28	
1+50				5.3	28.58	
2+00				0.8	33.08	
T.P.	12.40	45.55	0.79	33.09		
2+54 = Vista Del Mar M.H.				8.3	37.25	
3+00				5.4	40.15	
3+50				2.1	43.45	
T.P.	7.65	53.14	2.06	43.49		
4+00				6.5	46.64	
4+62.8 Proposed M.H. & Monte Vista				3.7	49.44	

5' 11" b  
 3' 5" of Sea Lane

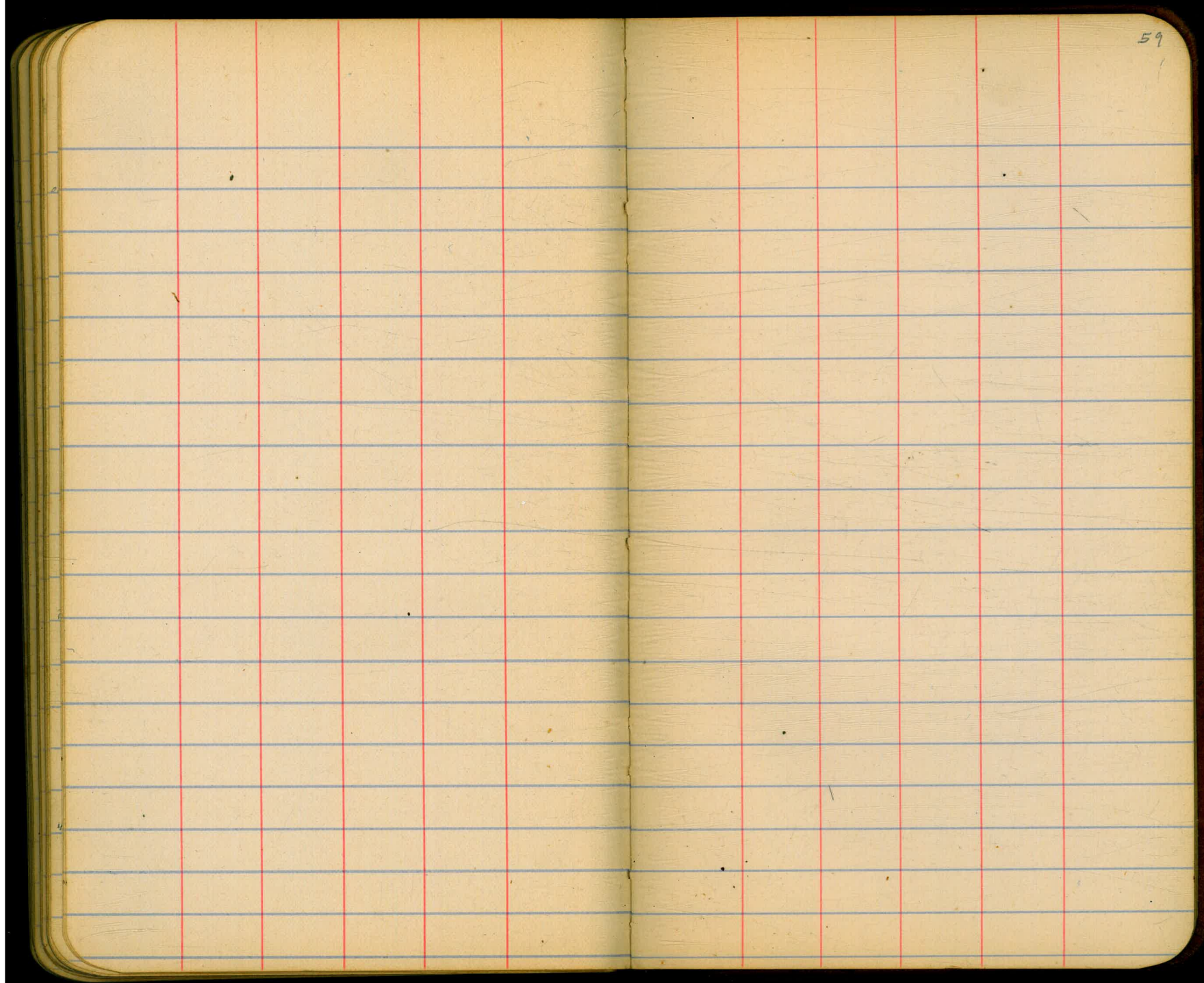
12.62	9.03	6.90	+2.13
3.74	17.87	11.90	+5.97
10.61	23.27	16.90	+6.37
5.31	28.57	21.90	+6.67
0.79	33.09	26.90	+6.19
8.41	37.14	32.30	+4.84
3.30	40.25	34.76	+5.49
2.06	43.49	37.43	+6.06
6.42	46.72	40.10	+6.62
3.67	49.77	43.50	+5.97

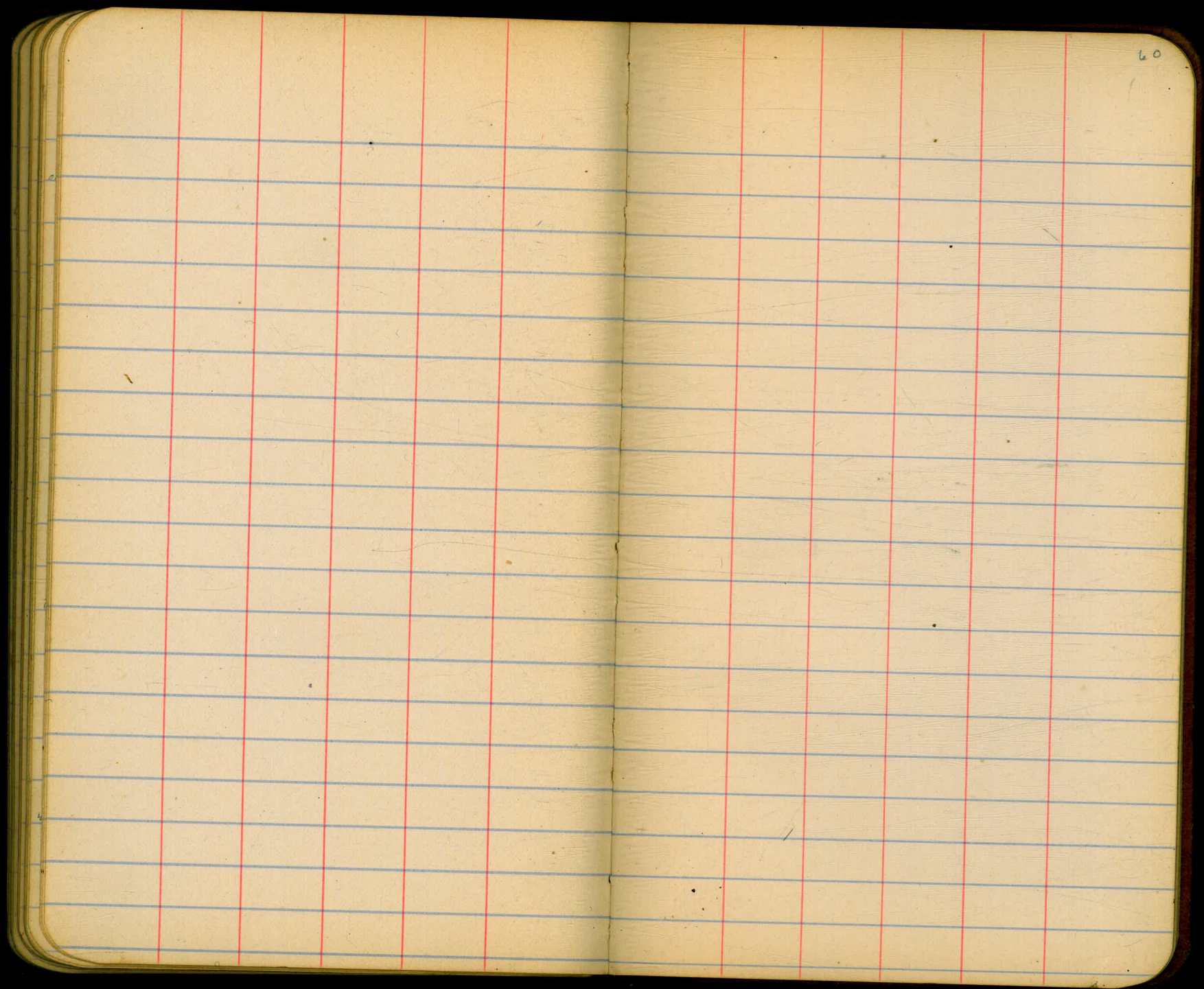
Monte Vista &  
 Marine Sewer  
 See Page 54



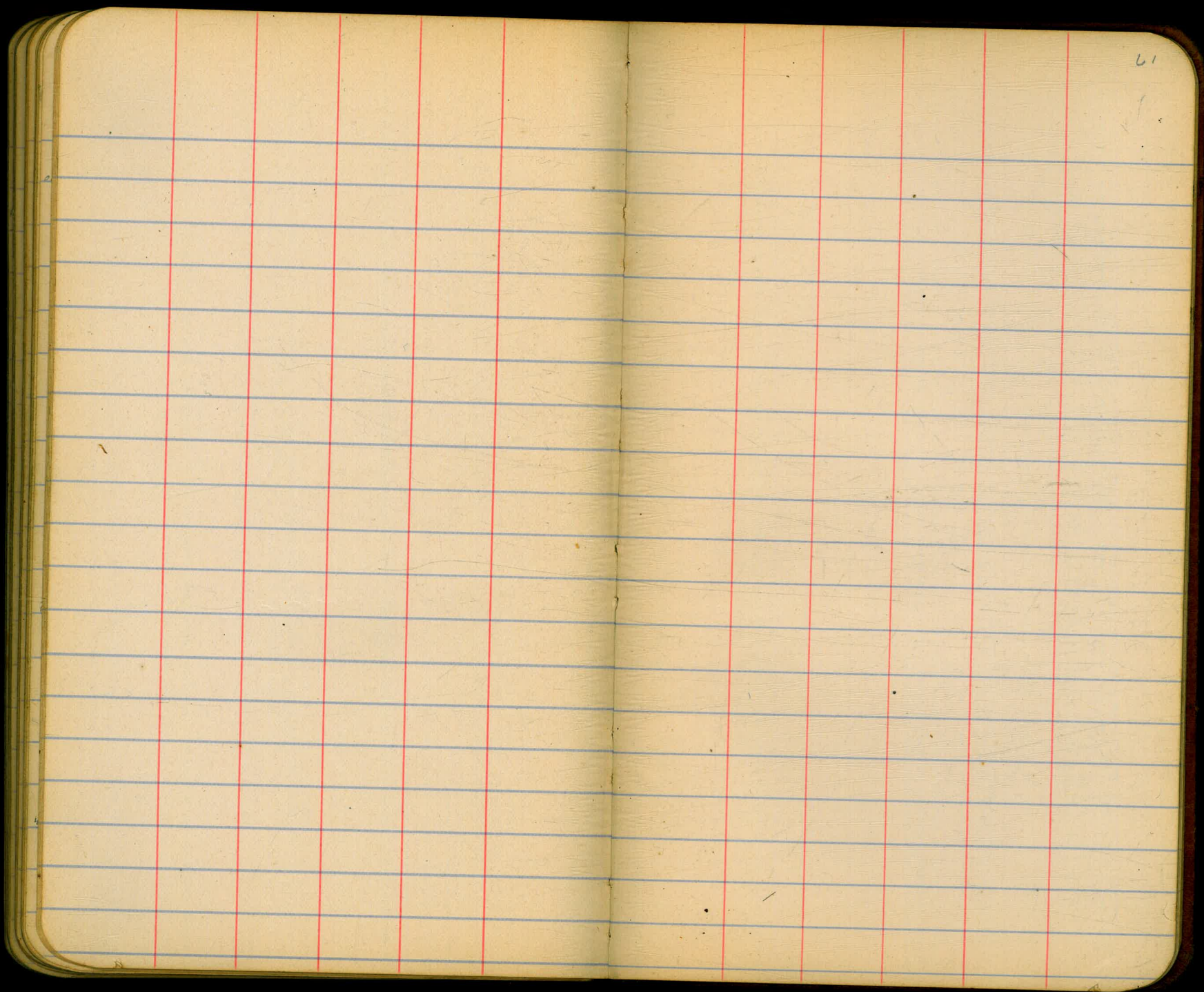


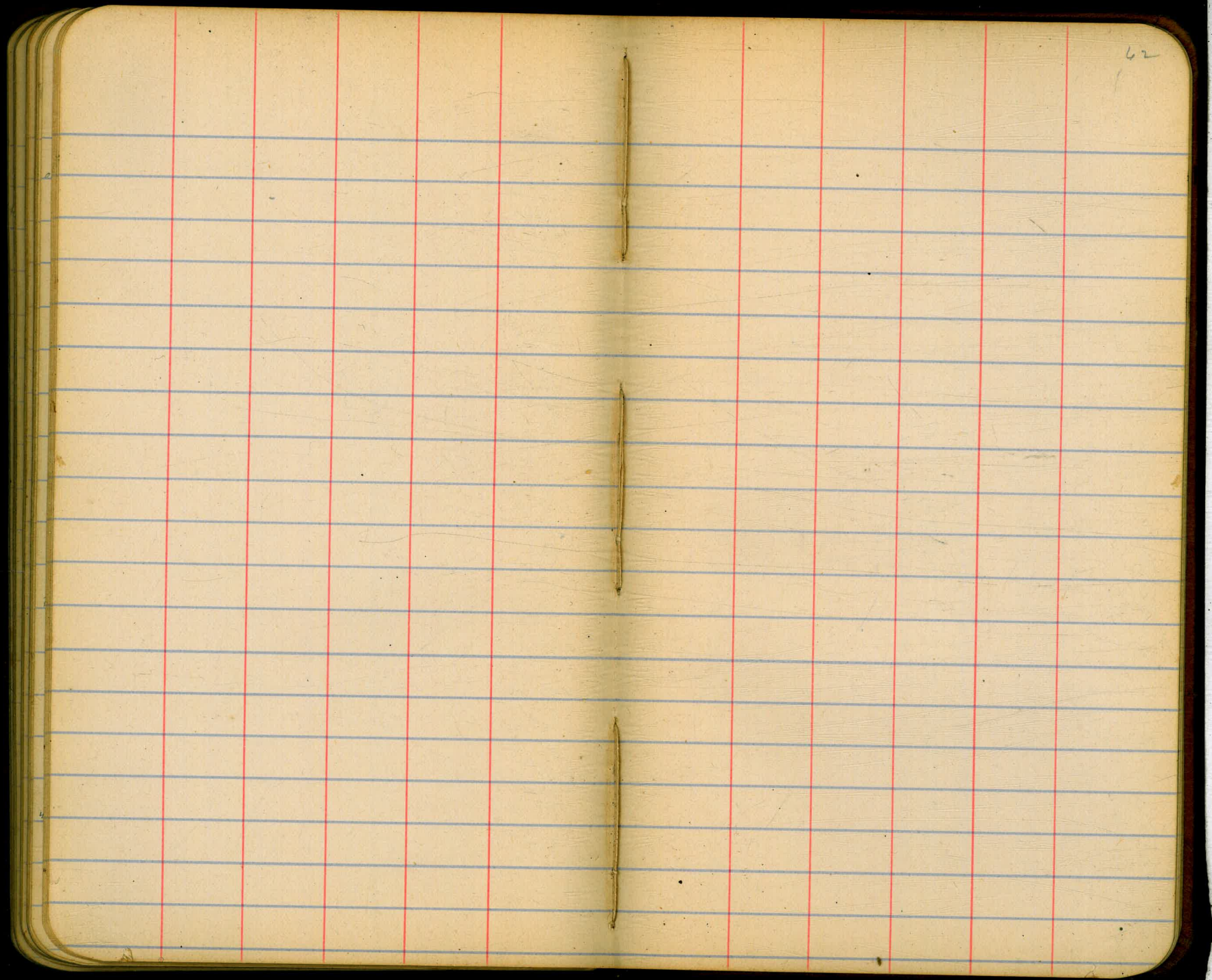
58





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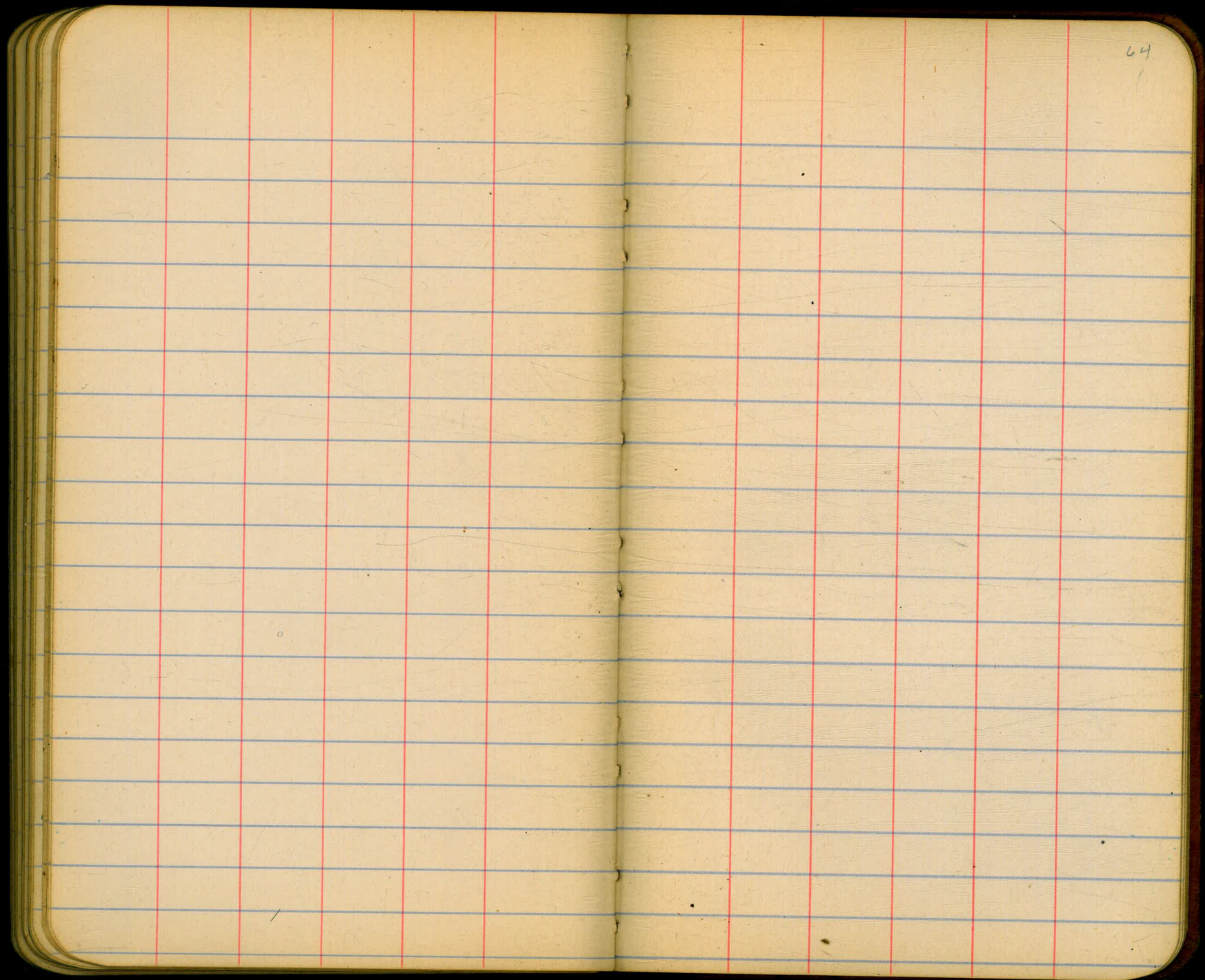




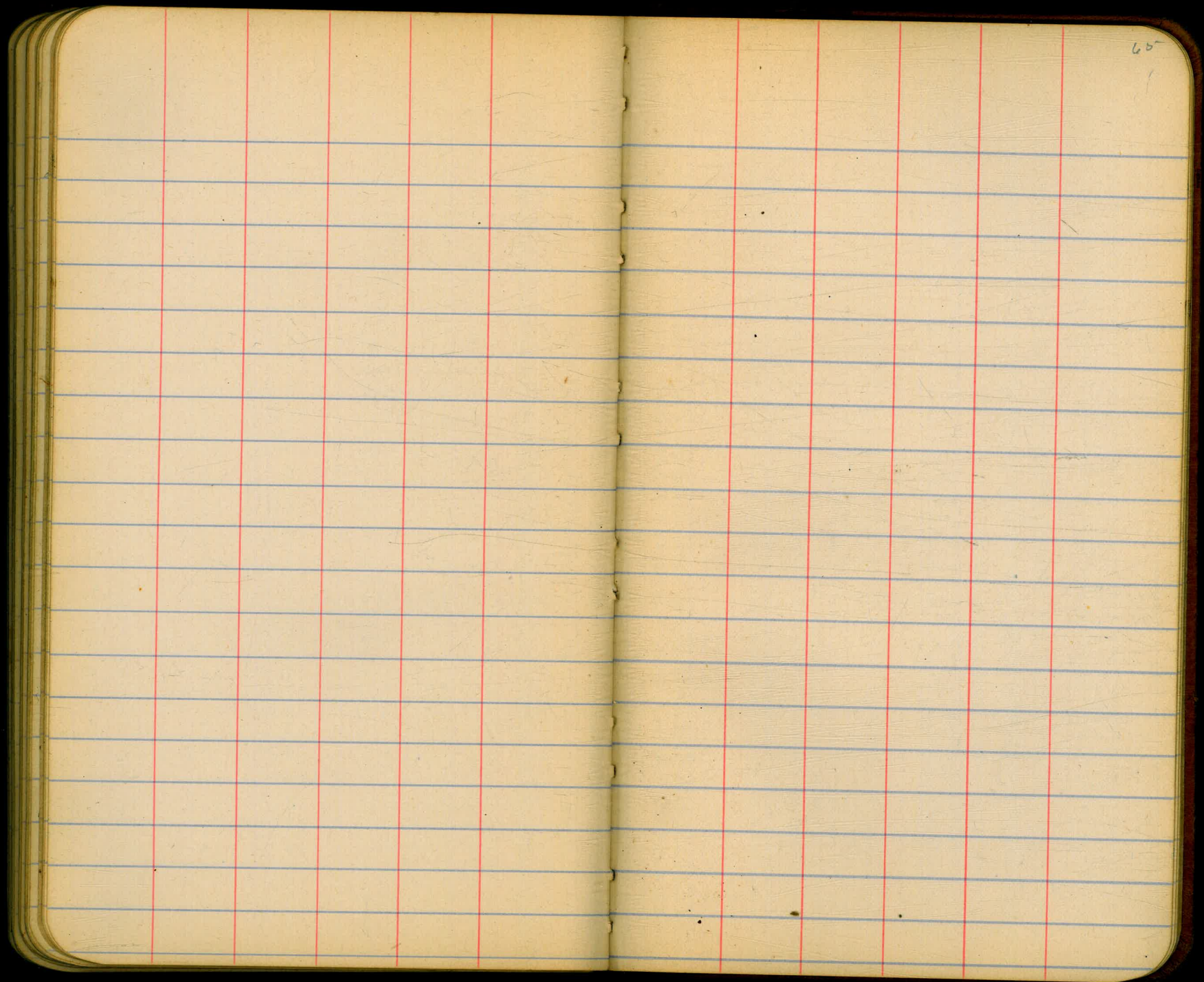
62



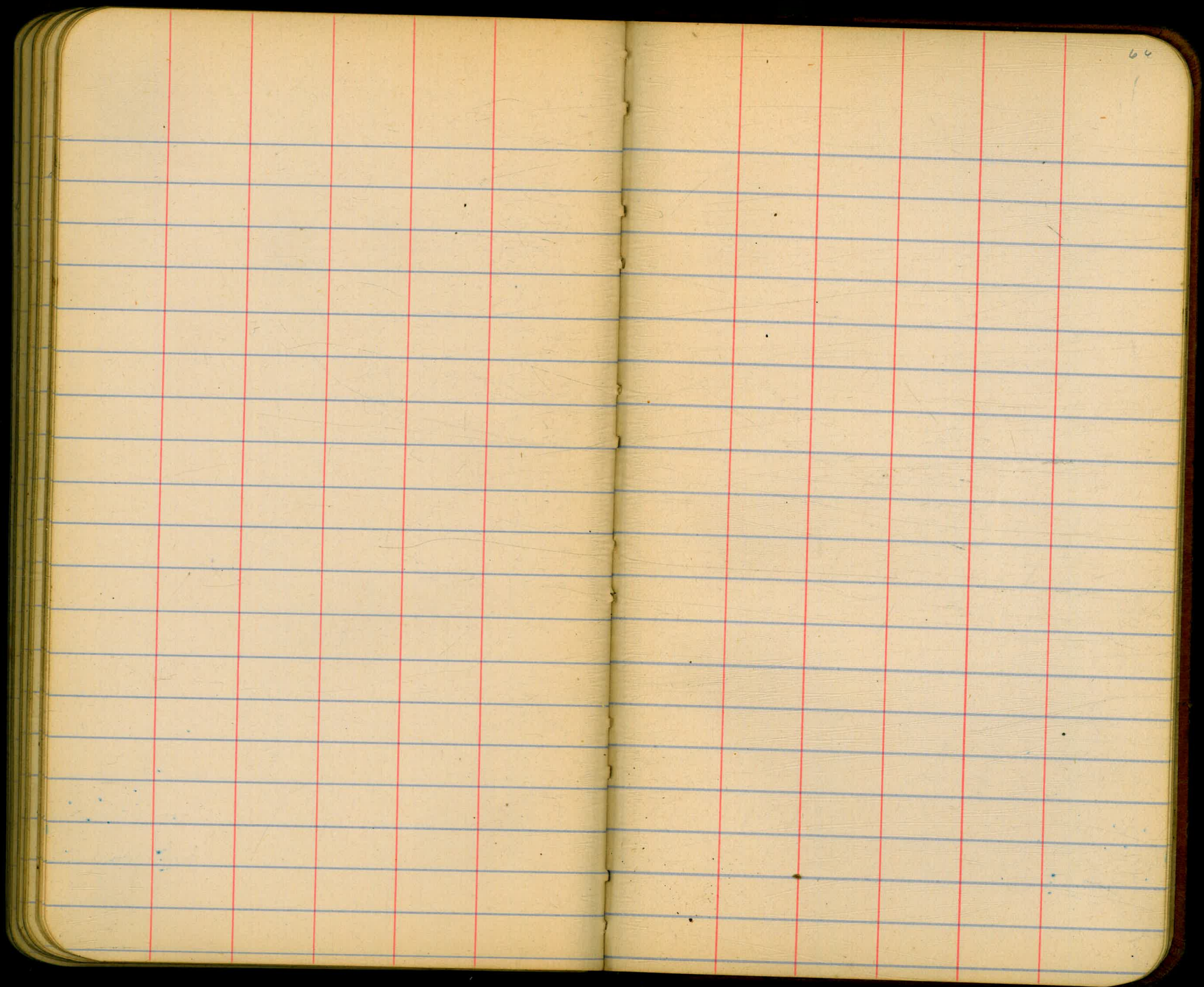
The image shows an open notebook with two facing pages. The pages are cream-colored and feature a grid of blue horizontal lines and red vertical lines, creating a ledger-style layout. There are four red vertical lines on each page, dividing the space into five columns. The notebook is bound in the center, and the dark brown cover is visible at the edges. The pages are otherwise blank, with only the number '63' written in the top right corner of the right page.

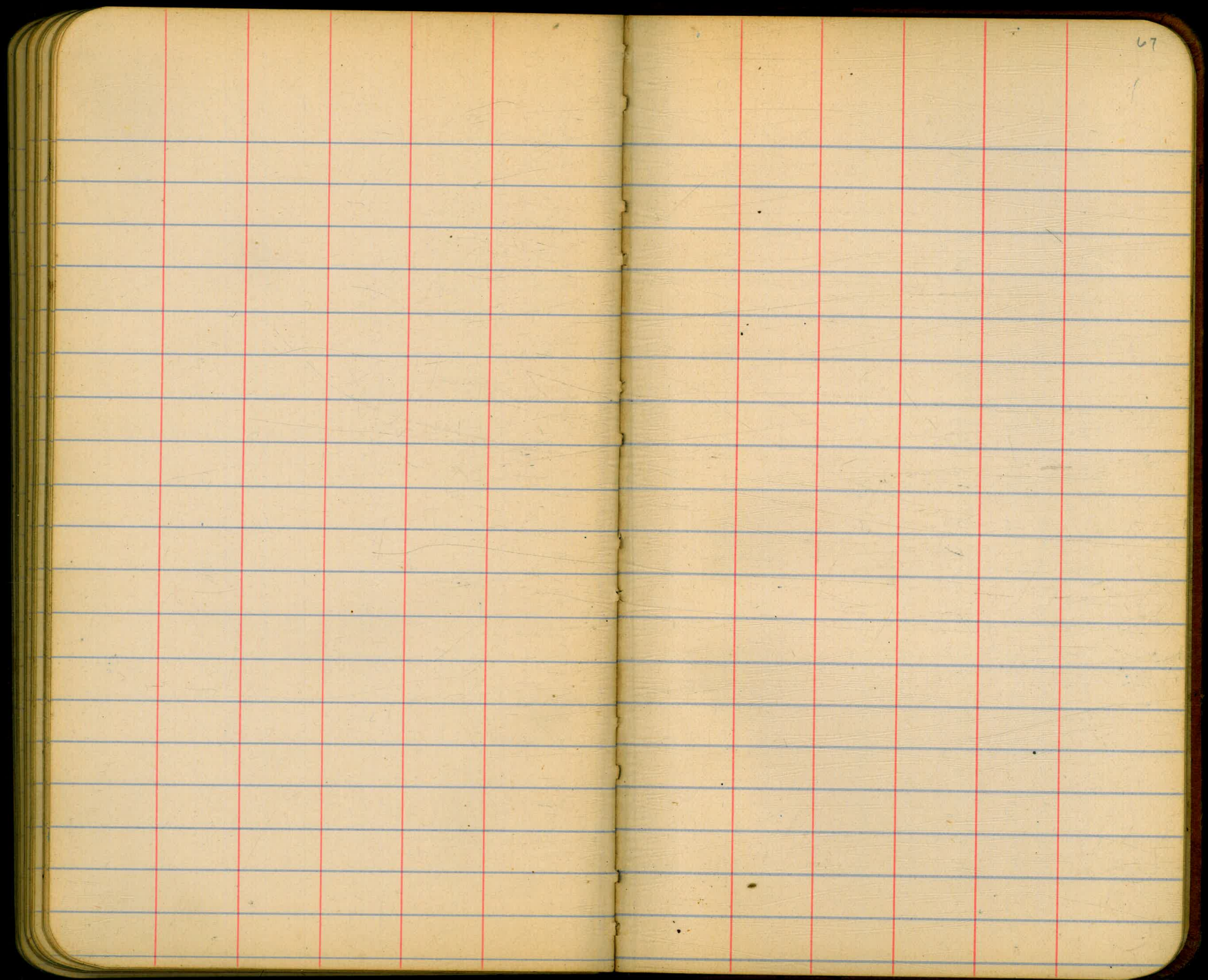


64

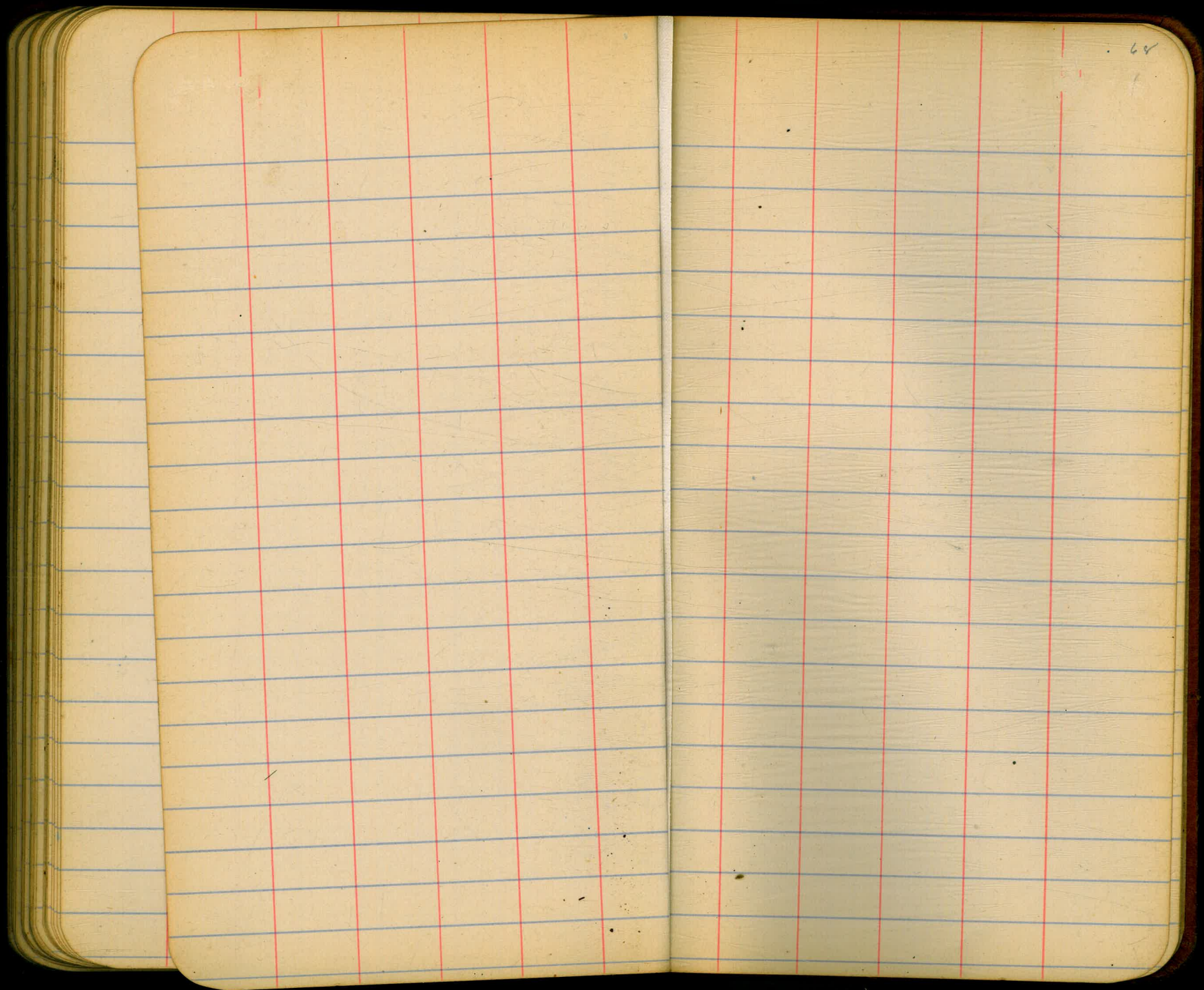


65

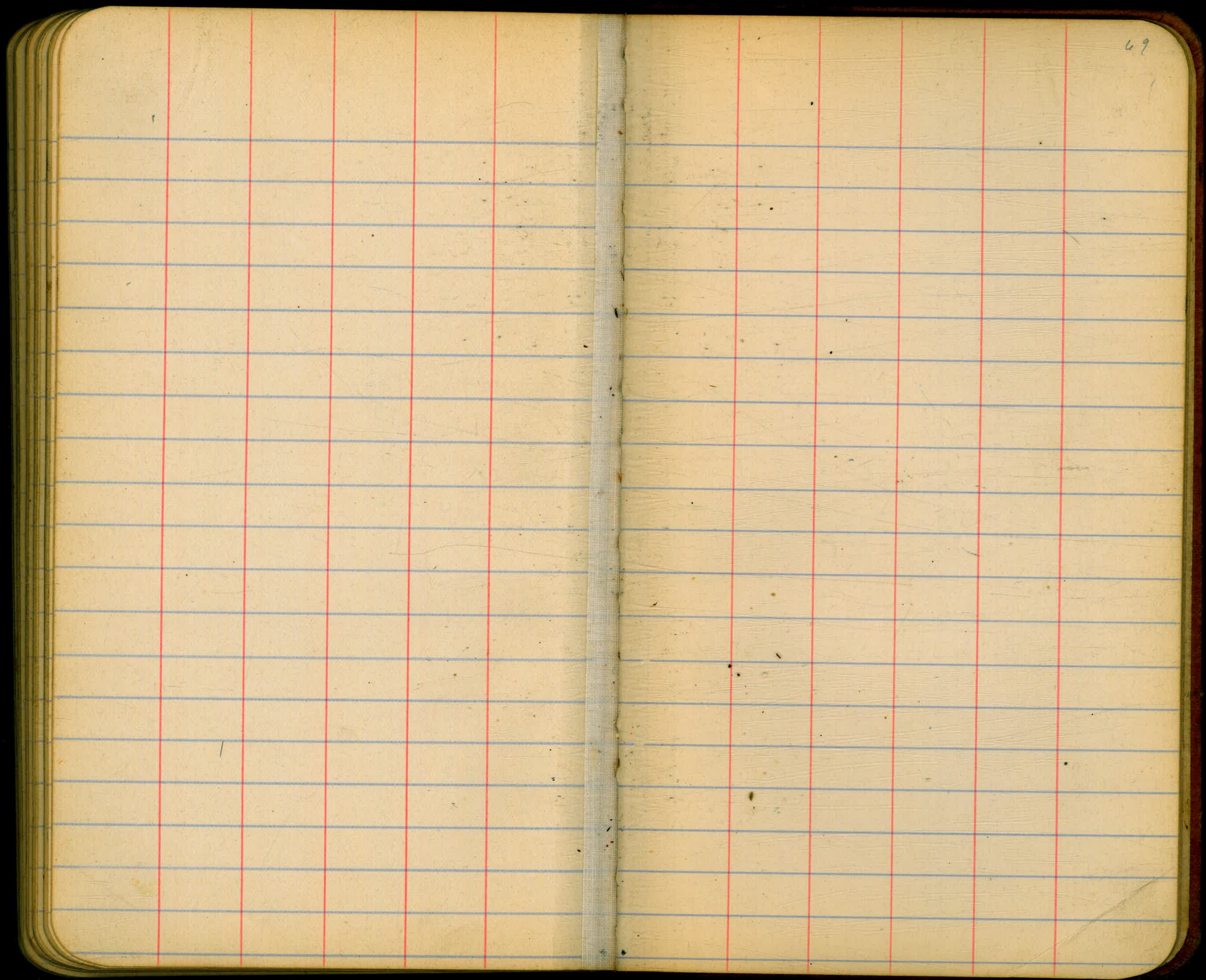




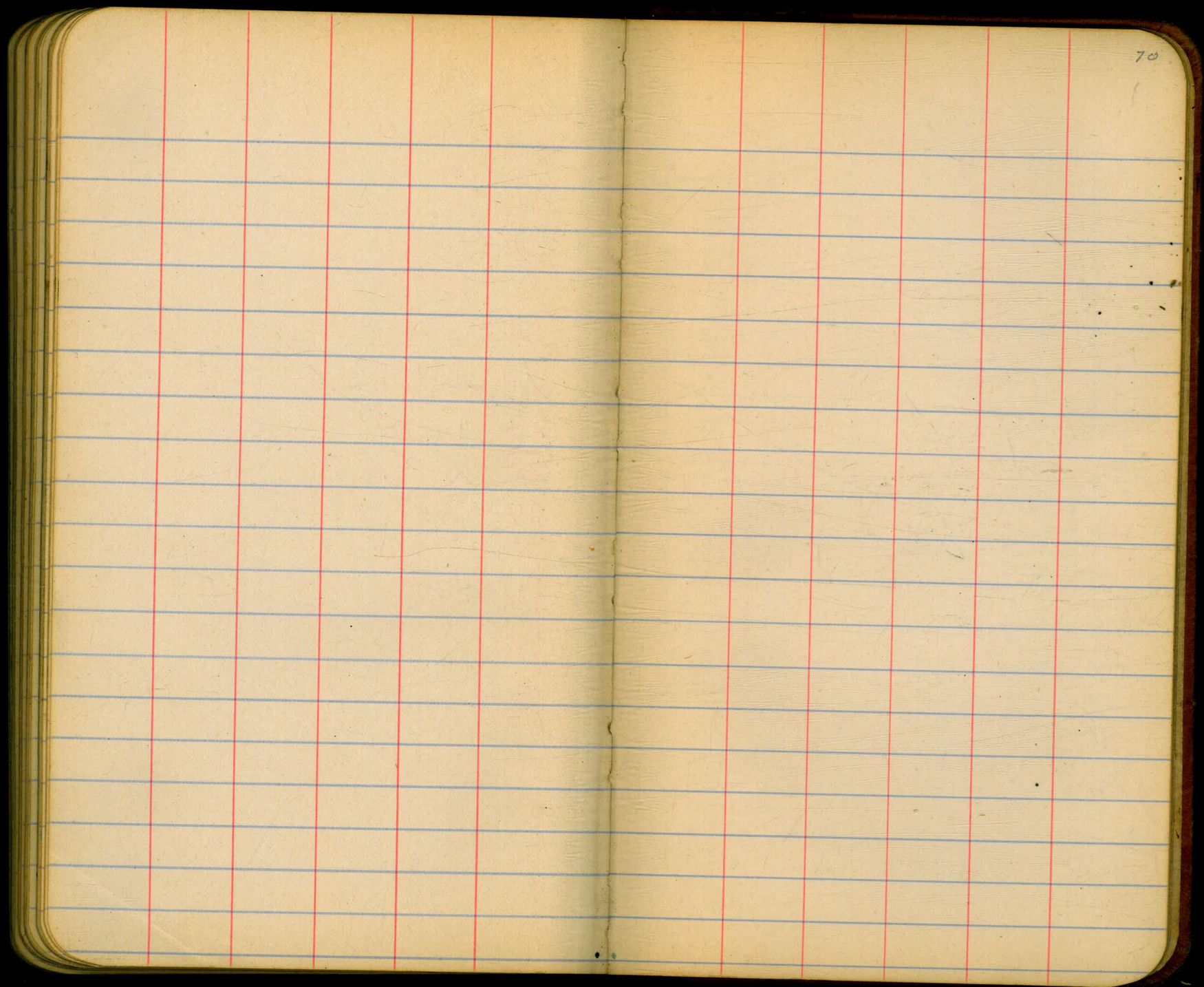
67



68



69



70





20' wide X Sec Alley BIK 57 City HTs 5/25/25  
 University to Klauker Bet Cherokee Reed

7.2

BM B.P. 104

N.W. University  
 & Cherokee

12' S. = 3 Garages on W 4' Back Garage on E end floor 5' out

00 = S. Line University Ave.

W 4.28

on Paving  
 curb same

- 4

6.2

C 4.76

on Paving

W

6.2

E 4.70

on Paving  
 curb same

C

6.4

+ 5

6.77

on end apron

15' S

E 4.5

E

7.1

C 4.7

C

7.4

W 4.6

W

7.3

33' S. = Garage E. Dirt Floor 02 out of Alley

W 4.9

W-11

7.7

C 5.0

W

8.0

E 5.0

C

8.0

70' S

E 5.7

E

8.0

C 5.7

C

8.9

W 5.3

C

8.4

245' S

93' S. Garage E. Dirt 1.0 out

E 6.5

W

8.6

C 6.3

284' S. Garage W end floor 11' out Garage E. dirt floor 11' out

W 5.8

W

9.3

E		9.3	
E		9.5	
+4		9.6	floor
T.P.	2.08	9.52	
		325' S	
E		2.4	
C		2.3	
W		2.4	
		366' S Garage on West floor 2.0 Back	
+2		1.9	
W		2.1	
C		2.3	
E		2.6	
		400' S	
E		3.0	
C		2.8	
W		2.9	
		445' S	
W		3.0	
C		2.8	

E		3.1	
		490' S. Garage on E 2nd floor 1.04 OUT	
E		4.1	
C		3.9	
W		3.6	
		From 502 S. to 535' S 4 Garages on E. dirt floor 11.00 OUT	
		540' S	
W		4.3	
E		4.7	
E		4.6	
		560' S.	
E		4.9	
C		5.2	
+5		5.2	
W		4.5	
		596' S	
W		6.3	
+5		7.4	
E		7.8	
+4		7.6	

TS 6.0

E 5.9

600' S. = N. Line Klawber

E 7.8

LS 8.2

C 8.3

W 8.0

602' S. = N. edge emt walk

W 8.21

emt walk

E 8.80

" " "





JAN. FEB. 1915

FEBRUARY 1915.

NAME.	No.	S	M	T	W	T	F	S	S	M	T	W	T	F	S
		31	1	2	3	4	5	6	7	8	9	10	11	12	13
E.W. Jewell	205	8	8	8	8	8	8	8	8	X	X	X	X	X	X
J.M. Suss	43	8	8	8	8	8	8	8	8	8	8	8	8	8	8
C.W. Brown	281	8	8							8	8	8	8	8	8
J.F. Malpin	199	8	8	8	8	8	8	8	8	8	8	8	8	8	8
H.A. Clark	257	8	8	8	8	8	8	8	8	8	8	8	8	8	8
A.C. Douglas	150	8	8	8	8	8	8	8	8	8	8	8	8	8	8
H.S. Hayes	23		8	8	8	8	8	8	8	8	8	8	8	8	8

NAME.	No.	S	M	T	W	T	F	S	S	M	T	W	T	F	S
		14	15	16	17	18	19	20	21	22	23	24	25	26	27
E.W. Jewell	205	X	X	X	X	X	X	X	X	X	X	X	X	X	X
J.M. Suss	43	8	8	8	8	8	8	8	8	M	8	8	8	8	8
C.W. Brown	281	8	8	8	8	8	8	8	8	8	8	8	8	8	8
J.F. Malpin	199	8	8	8	8	8	8	8	8	8	8	8	8	8	8
H.A. Clark	257	8	8	8	8	8	8	8	8	8	8	8	8	8	8
A.C. Douglas	150	8	8	8	8	8	8	8	8	8	8	8	8	8	8
H.S. Hayes	23	8	8	8	8	8	8	8	8	8	8	8	8	8	8

March.

NAME.	No.	S	M	T	W	T	F	S	S	M	T	W	T	F	S				
		14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
H.A. Clark	257	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
C.W. Brown	281	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
H.S. Hayes	23	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
J.M. Suss	43	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
J.F. Malpin	199	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
A.C. Douglas	150	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
J.M. Suss	357	X	9	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
A.C. Douglas	150	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
J.M. Suss	357	X	9	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8

NAME.	No.	S	M	T	W	T	F	S	S	M	T	W	T	F	S				
		14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31
E.W. Jewell	205	X	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
J.M. Suss	43	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
C.W. Brown	281	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
J.F. Malpin	199	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
H.A. Clark	257	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
A.C. Douglas	150	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8
H.S. Hayes	23	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8	8

Grant 283





Work order #417  
Work order #1394  
Paint

McDouglan #30

Geo McAlpine #199

John Seuss

DEC #150

Geo McAlpine #199

John Seuss #43

W. L. Brown #150

M. L. Mann

L. W. Brown

Nov. 1914

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H. A. Clark #437

Ed. W. Jewell #205

DEC. 1914

Ed. W. Jewell #205

McDouglan #150

J. S. McAlpine #199

John Seuss #43

H. A. Clark #437

M. L. Mann #26

L. W. Brown #434

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Extra Shifts

Address and Phone Numbers  
of Pump Employees.

John Suss  
Room No. 22

Sunset M. 4630

Hotel White House

A. C. Douglas  
1052 - 11<sup>th</sup> St.

Home Phone 4423  
(See below)

J. M. Alpine  
2406 A. St.

Phone / Main 5687 Home 1421

C. W. Brown  
Main 1142

3049 E. St.

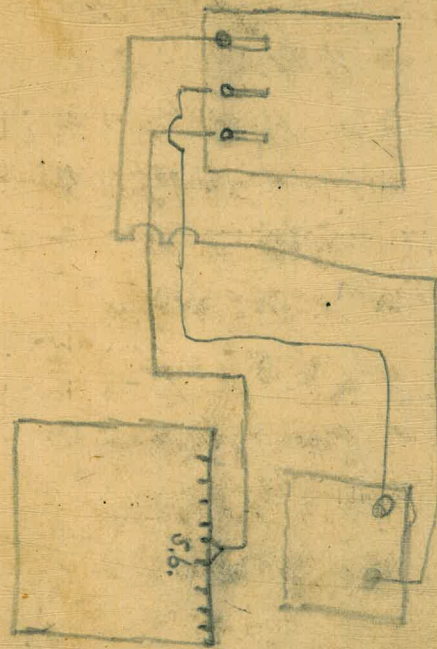
H. A. Clark  
1820 Mead Ave

Hillcrest 2181-J.

Fr. A. C. Douglas -

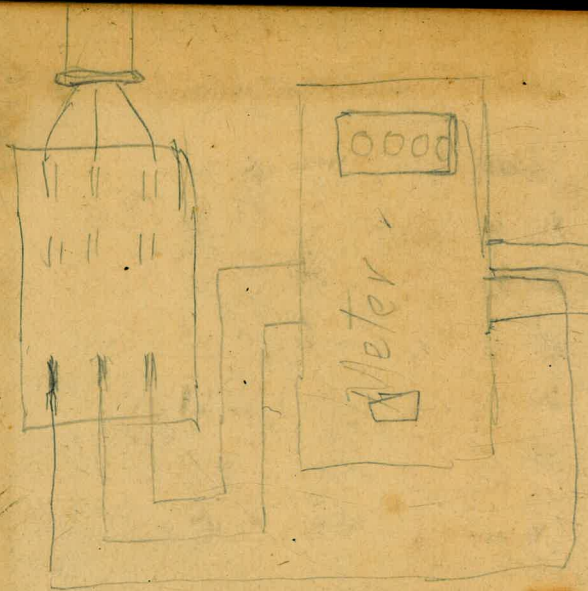
call - Main 1233 - R. D. Vernon

They will call him. 1042. 11<sup>th</sup> St.

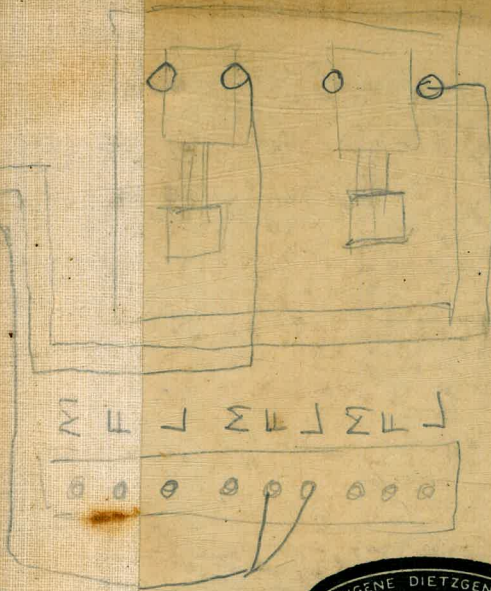
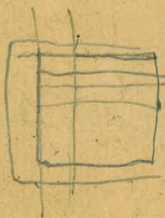


H. S. Haynes  
#2972 Woolman Ave.

Main 3480



#191  
9<sup>15</sup> pm.



1076



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12.