

1031

LEVEL BOOK.

No. 410 T

MICROFILMED

DEC 17 1964

Paradis

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EUGENE DIETZGEN CO.

Drawing Materials and Surveying Instruments
NEW YORK. CHICAGO. SAN FRANCISCO.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.
DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 20 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

Copyright, 1902. No. 39340.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	0
1	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	1
2	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	2
3	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	3
4	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	4
5	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	5
6	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	6
7	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	7
8	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	8
9	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	9
10	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	10
11	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	11
12	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	12
13	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	13
14	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	14
15	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	15
16	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	16
17	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	17
18	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	18
19	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	19
20	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	20
21	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	21
22	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	22
23	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	23
24	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	24
25	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	25
26	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	26
27	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	27
28	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	28
29	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	29
30	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	30
31	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	31
32	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	32
33	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	33
34	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	34
35	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	35
36	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	36
37	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	37
38	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	38
39	49.0	49.1	49.2	49.3	49.4	49.5	49.6	49.7	49.8	49.9	39
40	50.0	50.1	50.2	50.3	50.4	50.5	50.6	50.7	50.8	50.9	40

Calculated by F. E. Paradis, C. E.

"A" Line Levels
Upper to Lower Otay Pipe Line

Sta.	+	H.I.	-	Elev.
55+00	11.55	149.87		138.32
56+00			6.90	142.97
57+00			2.10	147.77
57+47'			1.20	148.67
58+00			2.53	147.34
58+25			3.55	146.39
59+00			14.00	135.87
Top of stake Sta. 59+00 T.P.	0.31	137.24	14.94	136.93
60+00			16.40	120.84
60+20			20.50	116.74
60+30			23.50	113.74
61+00			14.90	122.34
62+00			2.50	134.74
Rock on line 62+45 T.P.	9.60	146.94	0.90	136.34
63+00			8.33	137.61
64+00			6.35	139.59
65+00			2.20	143.74
T.P. Rock on line 65+60	9.55	154.81	0.68	145.26
66+00			7.92	146.89
67+00			7.24	147.57

Continued from Book BA.P.58

Crowell
Bellamy
Grant.

Sta	+	H.I.	-	Elev
67+30			7.00	149.81
68+00			7.86	146.95
69+00			12.35	142.46
70+00			18.20	136.61
71+00			14.75	140.06
72+00			6.10	148.71
73+00			4.10	150.71
T.P. Top of Stake Sta. 70-70. old line	3.73	153.79	4.75	150.06
74+00			7.62	146.17
75+00			10.60	143.19
76+00			4.73	149.06
77+00			2.73	151.06
77+39'			5.20	148.59
78+00			9.65	144.14
T.P. Rock on line 78+25	0.55	141.84	12.50	141.29
79+00			7.10	134.74
80+00			11.80	130.04
80+45			14.90	126.94
81+00			7.74	134.10

Sta.	+	H.I	-	ELEV	Sta.	+	H.I	-	ELEV
82+00			6.63	135.21	T.P. TOP. of stake old LINE 88+50	2.57	152.66	5.75	150.15
83+00			0.83	141.01	96+00			5.00	147.66
T.P. Rock at Sta 83	10.14	151.24	0.74	141.10	97+00			10.15	142.51
84+00			13.60	147.64	98+00			3.40	149.26
84+65			3.15	148.09	99+00			4.00	148.66
85+00			3.15	148.09	100+00			1.90	150.76
86+00			3.80	147.44	100+43			5.00	147.66
86+48			5.35	145.89	TP-Rock to R 48' 100+75	1.18	143.40	10.44	142.22
87+00			2.30	148.94	101+00			6.05	137.35
T.P. Rock on Line 87+45	6.50	155.90	1.84	149.40	102+00			11.50	131.90
88+00			4.57	151.33	103+00			11.05	132.35
89+00			5.15	150.75	104+00			17.10	126.30
90+00			4.32	151.58	104+65			22.50	120.90
91+00			6.55	149.35	105+00			18.00	125.40
92+00			4.27	151.63	106+00			14.25	129.15
93+00			3.55	152.35	107+00			6.70	136.70
94+00			3.60	152.30	108+00			6.07	137.33
94+60			4.90	151.00	T.P. on Rock 108+50	12.75	155.95	0.20	143.20
95+00			5.15	150.75	109+00			7.20	148.75

Sta	+	HI	-	ELEV
B.M. on P19-				
109+70			3.86	152.09
110+00			3.40	152.55
111+00			5.00	150.95
TP on Rock 111+40	16.0	144.94	12.61	143.34
112+00			19.50	125.44
112+25			21.50	123.44
113+00			6.60	138.34
TP. Rock on Line 113+20	10.41	154.42	0.93	144.01
113+40			5.55	148.87
114+00			4.00	150.42
114+68			4.44	149.98
115+00			4.70	149.72
116+00			6.76	147.66
117+00			6.75	147.67
118+00			5.80	148.62
119+00			5.80	148.62
120+00			6.40	148.02
121+00			8.16	146.26
TP on HUB 121	0.86	147.12	8.16	146.26

Sta.	+	HI	-	ELEV.
122+00			8.01	139.11
122+25			11.09	136.03
122+75			22.50	124.62
123+00			21.60	125.12
124+00			4.40	142.72
125+00			3.06	144.06
126+00			1.59	145.53
TP on top of stake sta 126	8.20	154.36	0.96	146.16
127+00			6.80	147.56
128+00			5.70	149.26
129+00			5.31	149.05
130+00			4.84	149.52
131+00			6.75	147.61
132+00			7.23	147.13
133+00			8.04	146.32
134+00			11.05	143.31
135+00			11.70	142.66
TP. on top of stake 135	5.70	149.16	10.90	143.46
136+00			4.00	145.16

Sta.	+	H I	-	ELPV.	Sta.	+	H I	-	ELCV
137+00			4.19	144.97	149+00			15.60	122.23
138-00			10.85	138.31	150+00			-1.80	139.62
139+00			15.50	133.66	150+31			-3.00	140.83
139+30			17.70	131.46	150+72			-2.40	140.23
140+00			13.20	135.96	151+20			21.50	116.33
141+00			9.73	139.43	151+72			7.75	130.08
142+00			8.10	141.06	152+10			16.00	121.83
143+00			6.03	143.13	152+59			4.34	133.49
144+00			5.55	143.61	153+59			3.75	134.08
TP on Hub. sta. 144+35	0.56	144.02	5.70	143.46	TP on Rock 153+85	11.72	145.10	4.45	133.38
145+00			11.49	132.53	154+59			10.65	134.45
145+60			24.50	119.52	155+59			12.00	133.10
146+00			16.20	127.82	High. Water 156+59			9.94	135.16
146+50			9.36	134.66	157+59			11.25	133.85
147+00			14.40	129.62	158+59			11.00	134.10
147+40			16.40	127.62	TP on Rock 158+20	3.40	136.40	12.10	133.00
148+00			10.83	133.19	159+59			5.35	131.05
TP 148+25	4.86	137.83	11.05	132.97	160+59			5.84	130.56
148+80			17.25	120.58	161+59			9.02	127.38

Feb. 18th 1916.Levels at Lower Otay
Dam SiteCrowell
Bellevue

Sta.	+	H. I.	-	ELEV.
162			13.03	123.37
TP, Sta. Rock 162+8	0.08	124.27	12.21	124.19
TP, On Rock 162+60	1.05	119.49	12.83	111.44
163			9.10	103.39
TP On Rock 163+22	0.61	100.21	12.89	99.60
164+00			10.06	90.15
TP	0.25	88.05	12.41	87.80
165+00			11.25	76.80
TP	0.65	76.50	12.20	75.85
166+00			9.00	67.50
Hub 166+15			10.94	65.56
166+45				49.40
166+77.5				57.40

Sta.	+	H. I.	-	ELEV.	U.S. GOV. B.M.
	1.28	487.28		486.00	486.57'
Top of Dam East Side			5.62	481.66	
Top of core Wall E. Side			8.68	478.60	
T.P.	1.76	476.79	12.25	475.03	
T.P.	0.61	464.39	13.01	463.78	
T.P.	0.03	451.65	12.77	451.62	
T.P.	1.23	440.44	12.44	439.21	
T.P.	0.00	427.79	12.65	427.79	
T.P.	0.23	415.36	12.66	415.13	
T.P.	0.36	402.71	13.01	402.35	
T.P.	1.00	391.21	12.50	390.21	
T.P.	0.33	378.94	12.60	378.61	
River bot.			13.40	365.54	
T.P.	12.01	390.51	0.44	378.50	
T.P.	12.84	402.99	0.36	390.15	
T.P.	12.22	415.16	0.05	402.94	
T.P.	12.78	427.69	0.25	414.91	
T.P.	12.41	440.07	0.03	427.66	
T.P.	12.54	452.49	0.13	439.94	
	80.35		14.285		

Feb. 19th 1916.

Check Levels bet. Bench Marks
Lower Otay Dam.

Crowell,
Bellamy.

Sta.	+	H.I.	-	Elev.
T.P.	12.72	465.09	0.11	462.37
T.P.	12.71	477.66	0.14	464.95
T.P.	9.41	486.73	0.34	477.32
Top Roadway N. Side			5.08	481.65
Top Concrete			8.34	478.39
T.P.	12.69	498.45	0.88	485.85
	0.80	494.59	4.66	493.79
T.P.	1.50	483.14	12.95	481.64
T.P.	0.15	470.26	13.03	470.11
T.P.	0.06	457.56	12.76	467.50
T.P.	0.60	445.19	12.97	444.59
T.P.	0.25	432.44	13.00	432.19
T.P.	0.81	420.72	12.53	419.91
70' on Tower G			3.71	417.01
Top Concrete base of tower.			4.84	415.83
T.P.	0.15	408.21	12.66	408.06
Invert of Pipe at intake.			13.65	394.56

Sta.	+	H.I.	-	Elev.
	1.60	149.31		147.71 = B.M.
Top Concrete N. side Dam.	5.64	143.47	11.48	137.83
			11.40	132.07
	12.93	160.64		147.71 B.M.
T.P.	12.85	173.04	0.45	160.19
T.P.	12.73	185.42	0.35	172.69
T.P.	12.79	197.67	0.53	184.89
T.P.	12.20	209.74	0.13	197.54
T.P.	13.09	222.44	0.38	209.36
T.P.	2.72	224.94	0.22	222.22
			0.17	224.77 = Water Tank
	1.76	199.30	12.57	197.54
T.P.	0.45	187.147	12.603	186.697
T.P.	0.705	174.962	12.89	174.257
			11.40	163.562
				224.80 B.M. on Barn. 163.52

Feb. 24-1914

Levels for Main pipe across Sweetwater
River at Boneta.

Sta	+	H.I.	Elev.	Elev.	Sta.	+	H.I.	Elev.	Elev.
0+00	6.74	56.74			9+00	7.45	8.30	49.29	48.44
	9' 6" E. of Pipe Line on Pipe Line								
	7.01		49.73	50.00	9+50	7.55	8.19	49.19	48.55
0+34.6	7.10	7.00	49.64	49.74	10+00	7.50	8.45	49.24	48.29
2+02.5	7.09	6.70	49.65	50.04	11+06.3	3.55	4.38	53.19	52.36
2+50	6.00	6.73	50.74	50.01					
3+00	6.93	6.86	49.81	49.88					
3+50	7.23	9.73	49.51	47.01					
4+00	7.78	9.44	48.96	47.30					
4+50	7.77	9.30	48.97	47.44					
5+00	5.52	9.22	51.22	47.52					
5+50	4.96	7.89	51.78	48.85					
6+00	4.22	8.35	52.52	48.39					
6+50	4.38	8.31	52.36	48.43					
7+00	5.53	8.52	51.21	48.22					
7+50	7.44	8.84	49.30	47.90					
8+00	7.17	7.43	49.57	49.31					
8+50	6.62	7.88	50.12	48.86					

Crowell
Ballemy

B.M. TOP of
Pipe opp. Sta.
646. 50.00

Plug Line
Pipe Line

Elev. taken
where pipe
enters ground
under Road.

Top of Pipe

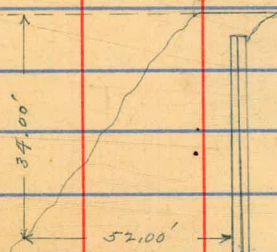
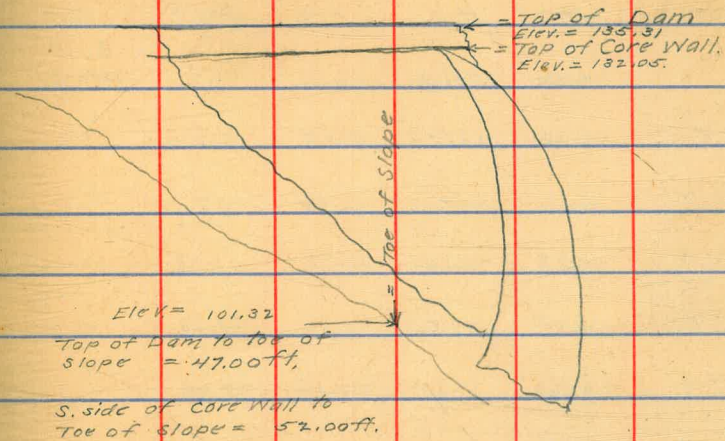
at bend in
pipe. on
top

Feb. 22nd 1916.

Crowell
Bellamy

Levels to determine Elev. of
Core Wall Lower Otay Dam.

Sta.	+	Ht.	-	Elev.
	2.18	149.89		B. M. 147.71
T.P.	1.62	140.74	10.77	139.12
Top of Concrete Core Wall W. Side			8.69	132.05
T.P.	0.22	128.32	12.20	128.54
T.P.	0.48	115.83	12.97	115.35
T.P.	2.81	106.52	12.12	103.71
92.0 ft. below (down stream) Core Wall.			9.07	97.45



Feb. 22nd 1916.

Crowell
Bellamy.

Levels to Determine Elevation of
Intake pipe and blowoff.

Sta.	+	H.I.	-	Elev.	Sta.	+	H.I.	-	Elev.
	1.41	149.12			B.M.				
				147.71	T.P.	0.47	76.96	12.62	76.49
T.P.	1.66	137.73	13.05	136.07	T.P.	0.08	64.42	12.62	64.34
T.P.	0.16	125.16	12.73	125.00	T.P.	0.27	51.66	13.03	51.39
T.P.	0.28	112.67	12.77	112.39	center of blowoff pipe			11.53	40.13
T.P.	0.57	100.20	13.04	99.63	set			3.84	47.82
T.P.	0.27	87.83	12.64	87.56	B.M.				
T.P.	0.52	75.89	12.46	75.37		11.77	59.59		47.82
B.M. on N.E. Cor. Concrete Base of Tower				5.95				9.30	50.29
				69.94					
7' on Gauge			4.89	71.00					
T.P.	0.26	63.14	13.01	62.88					
Top inside of inlet pipe.			10.14	53.00	size of Inlet 48" B.M. on BARN.				
	0.23	163.79			163.56				
T.P.	0.20	151.23	12.76	151.03					
T.P.	0.10	138.24	13.09	138.14					
T.P.	0.62	126.14	12.72	125.52					
T.P.	0.16	114.20	12.10	114.04					
T.P.	0.17	101.33	13.04	101.16					
T.P.	0.38	89.11	12.60	88.73					

on top of
concrete
blowoff
sewer outlet

center of
36" blowoff
Valve.

Grade-levels
 Otay-San Diego Pipe-Crossing

of Sweetwater River
 Feb 26 1916 Wueste-Lewis!

Sta	+ HI	- BM
11+06.3	1.17 5436	5319
10+60		509 49.27
9+00		515 49.21
7+50		510 49.26
	5.61 5487	
5+50		313 51.74
4+00		593 48.94
	4.91 5385	
2+025		420 49.65
0+00		383 50.02

On top pipe where same enters
 Ground under roadway from south
 at joint to which connection can be made.

= Mr. Crowell's Starting Point

Grades on Hub-line
9'6 $\frac{1}{2}$ " east from side of

Otay-San Diego Pipe-Line

Sta	Elev of Hub	Grade	Cut	Fill
0+00	49.73	49.25	0.48	
0+34.6	49.64		0.39	
2+02.5	49.65		0.90	
2+50	50.74		1.49	
3	49.81		0.56	
3+50	49.51		0.26	
4	48.96			0.29
4+50	48.97			0.28
5	51.22		1.97	
5+50	51.78		2.53	
6	52.52		3.27	
6+50	52.36		3.11	
7	51.21		1.96	
7+50	49.30		0.05	
8	49.57		0.32	
8+50	50.12		0.87	

2-26-16.
Wueste-Lewis

Crossing at Sweetwater River.

Sta	Elev Hub	Grade	Cut	Fill
9	49.29	49.25	0.04	
9+50	49.19			0.06
10	49.24			0.01
10+60	49.27		0.02	

Cross Section of Gorge below
Lower Otay Dam

Crowell
Bellamy
Carrall
Mansfield

Sta.	+	H.L.	-	Elev.	Sta.	+	H.L.	-	Elev.
		150.00	0.0	150.00	0+85			6.49	71.84
0+03			5.0	145.0	0+87			9.50	68.83
0+12			10.10	139.9	1+00			8.95	69.38
	0.29	137.38	12.90	137.10	T.P.	12.80	82.18	8.95	69.38
0+25			5.7	131.68	2+70			12.40	69.78
T.P.			12.35	125.03	2+82			5.35	76.83
Hand Level	0.80	119.38	6.45	118.58	T.P.	12.62	94.41	0.39	81.79
0+34			0.80	118.58	3+24			3.05	91.36
0+47			7.30	112.08	T.P.	11.41	105.79	0.03	94.38
T.P.	1.95	109.03	12.30	107.08	3+30			7.60	98.19
0+50			3.95	105.08	T.P.	11.29	117.41	0.37	105.42
0+58			9.65	99.38	3+49			10.72	106.69
T.P.	3.80	100.77	12.06	96.97	3+72			4.38	115.03
0+58			8.90	91.87	T.P.	12.07	129.16	0.32	117.09
T.P.	1.93	90.24	12.46	88.31	3+83			7.03	122.13
0+67			3.83	86.41	3+96			0.0	129.16
0+75			10.63	79.61	T.P.	12.08	141.14	0.10	129.06
T.P.	1.12	78.33	13.03	77.21	4+26			1.25	139.89
					4+30			-1.00	142.14

Assumed
Elev.
150+00
= 99.23
Otay
working
Elevation

River bot.

River bot.

Sta.	AR	AL	Mag
202.7 50+21 ⁸		127° 18'	S. 24° 05' E.
48+19 ⁶	45° 06'		N. 76° 25' W.
244.6 46+35	11° 43'		S. 58° 15' W.
0.535 40+50		16° 31'	S. 47° 15' W.
0.158 32+19	77° 36'		S. 63° 45' W.
0.141 27+04 ⁹	35° 28'		S. 13° 05' E.
0.160 16+45 ⁸	19° 51'		S. 50° 05' E.
0.508 11+37 ⁸	5° 48'		S. 69° 30' E.
0.778 5+70	10° 48'		S. 75° 10' E.
0.45 0+0 = Dam			S. 86° 00' E.

127° 18' 7
LINE OF SECTION

98° 04'
LINE OF SECTION

Levels connecting x sections
of Gorge below Dam
of Lower Otay-

sta.	+	H.I.	-	Elev.
2+70 of X sec. Line = 5+70 of connecting line	8.62	78.40		69.78
6+70			6.85	71.55
7+70			5.40	73.00
8+70			5.25	73.15
9+70			5.55	72.85
10+70			8.95	69.45
11+37 ⁸			9.70	68.70
12+00			12.75	65.65
13+00			11.25	67.15
14+00			13.60	64.80
T.P.	2.13	67.88	12.65	65.75
15+00			3.98	63.90
16+00			6.70	61.18
16+45 ⁸			7.80	60.08
17+00			8.95	58.93
18+00			18.30	49.58
19+00			18.00	49.88
20+00			15.70	52.48
21+00			17.20	50.68

Elev 150.00 = 99.53 Otay working Datum

Sta	+	H.I.	-	Elev
T.P.	1.86	58.72	11.02	56.86
22+00			8.90	49.82
22+86			16.90	41.82
24+00			13.10	45.62
25+00			10.60	48.12
26+00			11.05	47.67
27+00			12.90	45.82
27+04 ⁹			13.25	45.47
28+00			14.70	44.02
29+00			15.50	43.22
30+00			18.00	40.72
T.P.	1.03	46.76	12.99	45.73
31+00			8.63	38.13
32+00			12.90	33.86
32+19			13.30	33.46
33+00			11.05	35.71
34+00			10.95	35.81
T.P.	2.00	36.71	12.05	34.71

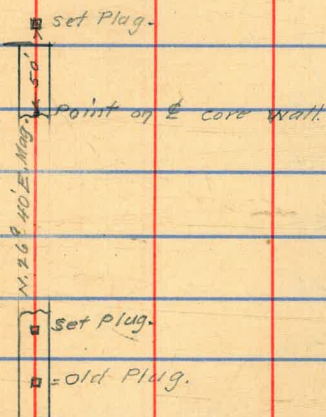
Sta.	+	H.I.	-	Elev
35+00			2.10	37.61
35+82			4.75	31.96
37+00			6.52	30.19
38+00			6.51	30.20
39+00			8.00	28.71
40+00			6.90	29.89
T.P.	4.54	36.04	5.21	31.50
40+50			4.56	31.48
T.P.	0.30	23.61	12.73	23.31
41+00			8.50	15.11
42+00			10.50	13.11
43+00			11.55	12.06
43+64			17.10	6.51 Water edge
44+64			15.70	7.91
T.P.	1.29	12.20	12.70	10.91
45+83			8.38	3.92
46+35			8.24	3.96
47+00			10.30	1.90

Sta	+	H.I.	-	Elev.
47+90			14.10	-1.90
48+19 ⁶		1.73	14.50	-2.30
T.P.	2.24	1.73	12.71	-0.51
49+00			10.22	-8.49
50+00			9.23	-7.50
50+21 ⁸			4.15	-2.42
T.P.			4.15	-2.42
Left of sta. 50+21 ⁸				
Right of sta. 50+21 ⁸				
Sta.		Elev.	Sta.	Elev.
0+16	-9.18 = River bot.		0+25	3.08
0+36	-9.00 = River bot.		0+38	10.18
0+55	-7.40		0+48	15.48
0+65	-2.00		0+56	23.80
0+83	13.98		0+61	29.20
0+89 ⁷	18.65		0+68	35.60
0+90	33.85		0+77	41.80
1+20	40.65		0+86	48.70
1+23	45.95		0+95	55.40
1+30	50.45		1+00	60.40
1+40	74.45		1+11	69.24
1+63	82.75		1+19	75.30
1+70	90.75		1+32	80.50
			1+43	89.90
			1+59	90.60
			1+61	104.60
			1+62	108.30
			1+64	112.60

x Sections Lower Otay Dam site

3-23-16

	3.72	151.43		147.71
	12.61	159.02	5.02	146.41
A ₁ 0+00			8.4	50.6
A ₁ 0+11			12.2	46.8
A ₂ 0+00			9.0	50.0
A ₂ 0+15			13.1	45.9
A ₃ 0+00			8.4	50.6
A ₄ 0+00			8.6	50.4
A ₄ 0+15			12.1	46.9
A ₅ 0+00			8.0	51.0
A ₅ 0+15			12.2	46.8
A ₆ 0+00			9.5	49.5
A ₇ 0+00			9.3	49.8
	12.96	170.86	1.12	157.20
A ₈ 0+00			9.0	70.9
A ₈ 0+20			10.5	60.4
	12.32	182.91	0.27	170.59
A ₉ 0+00			7.0	75.9
	41.61	182.91		
	6.41	147.71	6.41	
	35.20	35.20		



$$\begin{array}{r} 1346 \\ 210 \\ \hline 1136 \end{array}$$

$$\begin{array}{r} 19427 \\ 18291 \\ \hline 1136 \\ 18291 \end{array}$$

210

A ₉ -0+11			124	170.5
A ₁₀ -0+00			24	80.5
A ₁₀ 0+08			58	77.1
	8.95	19032	1.54	18137
A ₁₁ -0+00			12	89.1
A ₁₁ -0+03			58	84.5
A ₁₁ -0+13			92	81.1
A ₁₁ -0+34			163	74.0
A ₁₂ -0+23			76	82.7
A ₁₂ -0+44			173	73.0
	4.51	194.27	0.56	189.76
A ₁₂ -0+00			36	90.7
A ₁₂ -0+16			44	89.9
	12.92	159.33		146.41
A ₂ ' 0+00			125	46.8
A ₂ ' 0+08			123	47.0
A ₃ ' 0+00			98	49.5
A ₃ ' 0+15			96	49.7

159.33

A'_{40+00}	7.0	152.3
A'_{40+13}	7.2	52.1
A'_{50+00}	5.5	53.8
A'_{50+11}	6.0	53.3
A'_{60+00}	3.6	55.7
A'_{60+14}	4.7	53.6
A'_{70+00}	2.9	56.4
A'_{70+12}	4.3	55.0
A'_{80+00}	3.9	55.4
A'_{80+12}	4.7	53.6
A'_{90+00}	5.1	54.2
A'_{90+13}	6.2	53.1
A'_{100+00}	7.2	52.1
A'_{100+14}	8.8	50.5
A'_{110+00}	9.5	49.8
A'_{110+13}	12.2	47.1
A'_{120+00}	9.3	50.0
A'_{120+16}	13.2	46.1

152.33

A'_3 1+00	12.5	146.8
A'_3 1+50	12.9	46.4
A'_4 1+00	11.3	48.0
A'_4 1+03	2.5	49.8
A'_4 1+50	11.2	48.1
A'_5 1+00	8.3	50.0
A'_5 1+50	10.2	49.1
A'_5 2+00	12.7	46.6
A'_6 1+00	8.0	51.3
A'_6 1+50	9.8	49.5
A'_6 2+00	12.6	46.7
A'_7 1+00	7.3	52.0
A'_7 1+50	10.0	49.3
A'_7 2+00	12.5	46.8
A'_8 1+00	8.3	51.0
A'_8 1+50	10.3	49.0
A'_8 2+00	13.7	45.7
A'_9 1+00	10.1	49.2

+

15933

A ₉ 1+50		108	148.5
A ₁₀ 1+00		182	46.1
A ₁₀ 1+50		128	46.5
	846	155.09	1270
A ₁₀ -2+00		136	41.5
A ₁ 0+15 ✓		193	153.8
A ₂ 0+18 ✓		127	42.4
A ₁₁ 0+86		140	45.1
A ₁₁ 1+00		130	42.1
A ₁₁ 1+50		113	43.8
A ₃ 0+25 ✓		111	44.0
A ₄ 0+25 ✓		128	42.3
A ₄ 20' Down 0+25 ✓		109	44.7
A ₂ 0+88		110	44.1
A ₂ 1+00		112	43.9
A ₂ 1+50		114	43.7
A ₂ 2+00		133	41.8
	225	144.92	1302
	10.71	15933 14432	25.72 10.71
		√15.01	√15.01

+

+

X

144.32

A ₁ 0+50 ✓	77	1366
A ₁ 0+75	35	408
A ₁ 0+85 ✓	88	355
A ₁ 1+00	33	410
A ₁ 1+50	46	397
A ₂ 0+40 ✓	40	403
A ₁ 2+00	61	382
A ₂ 0+58 ✓	80	363
A ₁ 2+50	110	333
A ₁ 2+54	108	335
A ₃ 0+57 ✓	87	366
A ₂ 1+50	15	428
A ₃ 0+65 ✓	124	319
A ₂ 2+00	25	418
A ₂ 2+50	58	385
A ₂ 2+55	63	380
A ₄ 0+38 ✓	54	389
A ₂ 3+00	114	329

144.32

A ₂ 3+17	11.7	132.6
A ₄ 0+35	4.1	40.2
A ₄ 12' Down 0+35	3.2	41.1
A ₃ 2+00	0.0	44.3
A ₃ 2+50	2.2	42.1
A ₃ 3+00	8.2	36.1
A ₃ 3+28	11.2	33.1
A ₄ 2+50	1.6	42.7
A ₄ 3+00	7.0	37.3
A ₄ 3+28	11.3	33.0
A ₅ 2+50	0.6	43.7
A ₅ 3+00	6.7	37.6
A ₅ 3+25	11.5	32.8
A ₆ 2+50	1.2	43.1
A ₆ 3+00	9.5	34.8
A _L 3+03	12.2	32.1
A _L 3+11	12.1	32.2

14432

$A_7 - 2 + 50$	20	142.3
$A_7 - 2 + 70$	50	39.3
$A_4 0 + 40 \checkmark$	120	32.3
$A_7 - 2 + 96$	128	31.5
A_3 ^{8 Down} $0 + 65 \checkmark$	128	31.5
$A_8 - 2 + 00$	00	44.3
$A_8 - 2 + 40$	31	41.2
$A_2 2 + 84$	132	31.1
$A_9 2 + 00$	06	43.7
$A_9 2 + 50$	84	35.9
$A_9 2 + 75$	133	31.0
$A_5 0 + 27 \checkmark$	54	38.9
$A_{10} 2 + 00$	28	41.5
$A_6 0 + 11 \checkmark$	20	42.3
$A_{10} 2 + 62$	140	30.3
$A_7 0 + 11 \checkmark$	23	42.0
$A_{11} 1 + 50$	05	43.8
$A_{11} 2 + 00$	60	38.3

+

+

+

144.32

A' 2+25

12.2 132.1

A' 1+00

25 34.8

A' 1+50

42 40.1

A' 1+60

54 34.9

0.56 132.58 1230 132.02

A 1+00 ✓

42 28.4

A 1+10 ✓

108 218

A 1+22 ✓

107 21.9

A' 2+56

49 27.7

A' 2+93

44 28.2

A 1+44 ✓

126 20.0

A' 3+18

10.1 22.5

~~A 1+00~~~~86 24.0~~

A' 3+85

11.1 21.5

A 3 0+90 ✓

70 25.6

A' 2 3+30

72 25.4

A' 2 3+50

106 22.0

A 3 10' Down
0+90 ✓

72 25.4

144.32	12.30
132.58	56
11.74	11.74

13257

A'3	3+50	6.1	126.5	
A3	10' Down 1+00	128	19.6	
A'3	3+65	10.1	225	
A'4	3+50	57	269	
A'4	3+67	132	19.4	
A'5	3+50	116	21.0	
A'6	3+11	04	322	*
A'7	3+00	44	282	
A'8	-2+84	15	31.1	*
A'9	-2+80	46	28.0	
A'9	-3+00	122	20.4	
A'10	-2+62	25	30.1	*
A'11	-2+40	31	29.5	1
A'12	-2+25	35	29.1	
	0.30	120.24	1263	119.94
A2	1+21 ✓	27	17.5	
A2	1+37 ✓	90	11.2	
A'1	4+00	90	11.2	

132.57
120.24

1263
0.30

12.33

112.33

116
3

120.24

A ₃ 1+29 ✓			94	110.8
A ₂ 3+79			4.1	16.1
A ₃ 10' Down 1+30 ✓			108	09.4
A ₂ 3+84			113	08.9
A ₄ 3+67			0.8	19.4
A ₆ -3+35			42	16.0
A ₉ -3+20			104	09.8
A ₁₀ -2+90			5.0	15.2
A ₁₁ 2+72			58	14.4
A ₁₂ 2+77			146	05.6
	0.40	107.87	1277	107.47
A ₁ 1+60 ✓			76	00.2
A ₂ 1+64 ✓			6.5	01.4
A ₃ 1+52 ✓			5.0	10.29
A ₃ 1+57 ✓			8.5	99.4
A ₃ 20' Down 1+57 ✓			9.5	98.4
A ₃ 20' Down 1+65 ✓			13.6	94.3
A ₃ 4+0			64	101.5

$$\begin{array}{r} 120.24 \\ 107.87 \\ \hline 12.37 \end{array}$$

$$\begin{array}{r} 1277 \\ 40 \\ \hline 1237 \end{array}$$

1237

3-30-16

$$\begin{array}{r} 189.76 \\ 1.00 \\ \hline 190.76 \end{array}$$

$$\begin{array}{r} 190.76 \\ 12.88 \\ \hline 177.88 \\ 0.35 \\ \hline 178.23 \end{array}$$

$$\begin{array}{r} 178.23 \\ 12.52 \\ \hline 165.71 \\ 0.22 \\ \hline 165.93 \end{array}$$

$$\begin{array}{r} 165.93 \\ 12.99 \\ \hline 152.94 \\ 0.36 \\ \hline 153.30 \end{array}$$

107.87

sta.

+

H.I.

- Elev.

A'5 3+75

72 100.7

1.00 190.76

189.76 = B.M.

A'6 3+55

76 00.3

A13-0+0

1.00 189.76

A'6 3+60

142 93.7

A13-0+12

2.50 189.26

A'7 3+50

96 98.3

A14-0+0

4.20 186.56

1220 95.67

A14-0+07

4.40 186.36

A14-0+21

13.40 177.36

A13-0+33

18.80 171.96

A15-0+0

9.30 181.46

T.P.

0.35

12.88 177.88

A16 0+0

178.23

6.40 171.8

T.P.

0.22

165.93

12.52 165.71

A15 0+32

7.00 159.93

A15 0+40

13.80 152.13

4 T.P.

0.36

153.30

12.99 152.94

A16 0+31

3.40 149.90

A16 0+46

12.90 140.40

A15 0+60

11.20 142.10 ✓

A'16 0+0

2.80 150.50

A'15 0+0

2.70 150.60

153.30
12.93
140.37
0.31
140.68

140.68
12.25
128.43
2.69
131.12

131.12
12.77
118.35
0.52
118.87

Sta.	+	H.I.	-	Elev.
A'14	0+0	153.30	1.00	152.30
A'13	0+0		2.20	151.10
A'13	0+20		6.80	146.50
A'14	0+20		7.10	146.20
A'15	0+20		8.40	144.60
A'16	0+22		10.80	142.50
A'13	0+35		12.60	140.70
T.P.	0.31	140.68	12.93	140.37
A'15	0+85		13.20	127.48
A'16	0+66		8.50	132.18
A'14	0+44		3.60	137.08
A'15	0+44		5.20	135.48
A'16	0+39		6.40	134.28
A'16	0+85		12.70	127.98
A'14	0+54		9.80	130.88
A'13	0+42		8.90	131.78
A'13	0+52		10.90	129.78
A'13	0+54		18.00	122.68
A'13	0+95		17.00	123.68

Top of concrete

Spillway Wall

Spillway Floor

Sta.	+	H.I.	-	Elev.
A'13	1+15	140.68	13.30	127.38
A'13	1+65		12.60	128.08
A'13	1+85		14.00	126.68
T.P.	2.69	131.12	12.25	128.43
A'15	0+95		11.60	119.52
A'16	0+68		11.01	120.11
A'15	0+67		11.30	119.82
A'14	0+64		11.60	119.52
T.P.	0.52	118.87	12.77	118.35
A'16	0+85		7.50	111.37
A'14	0+75		3.40	115.47
A'16	0+83		3.30	115.57
A'15	0+95		0.0	118.87
A'15	1+03		6.70	112.17
A'14	1+20		5.0	113.87
A'16	0+90		13.50	105.37
A'14	1+70		3.00	115.87
A'14	2+10		8.00	110.87
A'13	2+38		6.90	111.97

118.57
 11.72
 107.15
 1.68
 108.83

108.83
 11.99
 96.84
 2.70
 99.54

99.54
 11.48
 88.06
 1.14
 89.20

89.20
 12.93
 76.27
 0.57
 77.34

Sta.	+	H.I.	-	Elev.
T.P.	1.68	108.83	11.72	107.15
A'15	1+42		6.00	102.53
A'16	1+94		14.10	94.73
A'15	1+92		6.30	102.53
A'15	2+21		11.80	97.03
A'14	2+84		5.40	103.43
A'14	2+54		13.50	95.33
A'15	1+07		8.20	100.63
A'16	0+90		7.40	101.48
A'15	0+85		4.20	104.68
A'14	0+88		6.90	101.98
A'15	0+98		11.30	97.53
A'15	1+12		20.20	88.63
A'15	1+18		14.00	94.83
A'15	1+25		18.50	90.33
T.P.	2.70	99.54	11.99	96.84
A'16	1+12		12.60	86.94
A'16	1+20		28.00	71.54
A'16	1+40		29.10	70.44

Sta.	+	H.I.	-	Elev.
A'16	0+98	99.54	6.50	93.04
A'16	1+10		10.50	89.04
A'16	2+18		13.00	86.54
A'15	2+44		11.20	88.34
A'13	2+82		8.60	90.94
T.P.	1.14	89.20	11.48	88.06
A'16	2+40		9.70	79.50
A'14	2+64		4.80	84.40
A'14	2+79		10.60	78.60
A'13	3+00		14.80	74.40
A'15	1+39		12.70	76.50
A'14	5+76		9.90	79.30
A'14	5+95		5.15	84.05
T.P.	0.57	77.34	12.93	76.27
A'16	2+60		6.100	71.34
A'15	2+69		4.30	73.04
A'14	3+00		7.00	70.34
A'16	1+28		6.80	70.54
A'15	1+49		10.60	66.74

77.34	67.22
<u>12.65</u>	<u>12.49</u>
64.69	54.73
<u>2.53</u>	<u>0.14</u>
67.22	54.87

54.87	42.81	33.49
<u>12.83</u>	<u>12.39</u>	<u>9.01</u>
42.04	30.42	24.48
<u>0.77</u>	<u>3.07</u>	<u>4.05</u>
42.81	33.49	28.53

Sta.	+	H.I.	-	Elev.
T.P.	2.53	67.22	12.65	64.69
A'13	3+25		13.00	54.22
A'14	3+11		7.20	60.02
A'15	3+00		13.30	53.92
A'16	2+85		10.20	57.02
A'16	1+53		6.20	61.02
A'15	1+69		9.00	58.22
A'14	5+54		11.90	55.32
A'13	5+69		13.10	54.12
A'13	6+09		8.10	59.12
T.P.	0.14	54.87	12.49	54.73
A'15	3+05		11.70	43.17
A'15	3+14		9.40	45.47
A'14	3+13		3.50	51.37
A'14	3+28		7.40	47.47
A'13	3+46		9.30	45.57
A'15	1+80		5.70	49.17
A'14	5+33		9.70	45.17
A'13	5+49		7.90	46.97

Sta.	+	H.I.	-	Elev.	
T.P.	0.77	42.81	12.83	42.04	
A'13	3+55		10.80	32.01	
A'16	3+10		7.00	35.81	
A'16	1+63		3.80	39.01	
A'15	1+83		5.30	37.51	
A'14	5+12		7.10	35.71	
A'13	5+33		9.90	32.91	
T.P.	3.07	83.49	12.39	80.47	
A'16	3+41 ⁵		13.00	20.49	
A'15	3+47		12.40	21.09	
A'15	2+06		3.70	29.79	
A'16	1+88		5.70	29.79	
T.P.	4.05	28.53	9.01	24.48	
A'16	3+41 ⁵		10.00	18.53	Stream Bed
A'15	3+47		10.00	18.53	" "
A'14	3+65		10.00	18.53	" "
A'13	3+79		9.90	18.63	" "
A'16	2+03		9.80	18.93	" "
A'15	2+16 ⁵		9.40	19.13	" "

150.37
 3.40
 153.77
 11.21
 142.56
 6.46
 149.02

Sta.	+	H.I.	-	Elev.	
A'14	4+79		10.20	18.33	Stream Bed
A'13	5+09		8.80	19.73	" "
A'3A	0+50	3.40	153.77	4.10	149.67 <u>150.39 = B.M.</u> 139.40 = B.M.
A'3A	0+75		7.00	146.77	
A'3A	0+89		8.50	145.27	
A'3A	0+92		10.00	143.77	
A'3A	1+05		8.80	144.97	
A'2A	0+40		8.40	145.37	
A'2A	0+64		11.70	142.07	
A'2A	0+71		13.70	140.07	
A'2A	0+80		13.50	140.27	
A'1A	0+45		12.60	141.17	
T.P.	6.46	149.02	11.21	142.56	
A'1A	0+55		9.50	139.52	
A-A	0+45		13.80	135.22	
A'3A	2+55		-2.63	151.65	
A'3A	2+25		7.85	141.17	

A'2A 1+65

149.02
 12.33
 136.69
 0.76
 137.45

Sta.	+	H.I.	-	Elev.	
A'3A	2+00	149.02	13.40	135.62	
A'3A	1+65		8.93	140.09	
A'3A	1+40		8.70	140.32	
A'3A	1+25		6.30	142.72	
A'2A	2+55		-1.00	150.02	
A'2A	2+25		8.90	140.12	
A'2A	1+45		13.80	135.22	
A'2A	1+05		12.30	136.72	
A'1A	2+55		-2.10	151.12	
T.P.	0.76	137.45	12.33	136.69	
A'1A	2+10		0.40	137.15	
A'2A	1+65		8.80	128.75	
A'1A	1+60		17.30	120.25	
A'1A	1+35		12.80	124.75	
A'1A	1+05		6.70	130.85	
AA	1+45		23.00	114.55	
AA	1+05		13.90	123.65	

4/27/16 Continuation of Upper to Lower
Otay Pipeline.

Levels for Pipeline from Tower,
to Filter Plant.

Sta	+	H.I.	-	Elev.	Grade B.M.
	7.17	72.11			69.94
T.P.	12.78	88.94	0.95	76.16	
T.P.	11.11	99.05	1.00	87.94	
0+00			1.75	97.30	
0+50			11.63	87.42	87.0
T.P.	4.89	90.74	12.90	86.15	
0+75			8.33	82.41	
1+00			12.80	77.94	77.0
T.P.	6.21	84.07	12.88	77.86	
1+25			9.42	74.65	
1+50			12.18	71.89	71.0
1+75			14.80	69.27	69.5
1+97			17.90	66.17	
2+00			16.30	67.77	68.0
2+25			14.70	69.37	69.0
2+50			10.78	73.32	72.0
P.T. 2+80			5.80	78.27	76.5 2+75
3+00			4.45	79.62	79.0

Sta.	+	H.I.	-	Elev
3+50			0.30	83.77
T.P.	12.96	96.80	0.23	83.84
4+00			8.58	88.22
4+50			3.45	93.35
T.P.	13.05	109.69	0.16	96.64
5+00			10.00	99.69
5+50			4.25	105.44
6+00			0.0	109.69
T.P.	13.00	121.98	0.71	108.98
6+50			7.85	114.13
7+00			4.25	117.73
T.P.	12.41	133.78	0.61	121.37
7+50			11.00	122.78
P.C. 8+00			4.00	129.78
T.P.	12.70	146.12	0.36	133.42
8+25			12.10	134.02
8+50			8.55	137.57
8+75			4.90	141.22

Sta.	+	H.I.	-	Elev.	Grade
9+00			1.40	144.70	144.0
T.P.	12.84	158.59	0.37	145.75	
P.T. 9+24 ⁷			9.90	148.69	147.5
9+50			6.45	152.14	150.5
10+00			1.35	157.24	153.0
T.P.	5.08	163.35	0.32	158.77	
10+40			2.90	160.45	154.0
10+50			2.65	160.70	154.0
10+57			2.30	161.05	154.0
11+00			2.00	161.35	154.0
11+50			4.60	158.75	153.5
11+77			7.40	155.95	152.5
11+95			7.50	155.85	152.5
12+00			8.95	154.40	157.0
12+50			12.70	150.65	148.0
T.P.	0.21	150.96	12.60	150.75	148.0
13+00			6.50	144.16	139.5
13+21			9.70	141.76	138.0
13+82			13.50	137.16	137.0

Sta.	+	H.I.	-	Elev.	Grade
T.P.	0.57	138.71	12.82	138.14	
13+65			4.85	133.86	130.0
14+00			12.05	126.66	123.0
T.P.	0.23	126.11	12.83	125.88	
14+35			4.90	121.21	118.0
14+50			8.45	117.66	
T.P.	0.60	113.81	12.96	113.21	
15+00			8.78	105.03	103.5
T.P.	0.00	100.86	12.95	100.86	
15+26			3.00	97.86	97.5
15+30			6.20	94.66	
15+36			4.50	96.36	
15+50			7.25	93.61	
P.C. 15+80 ⁸⁷			12.65	88.21	87.0
T.P.	0.45	88.67	12.64	88.22	
16+00			3.10	85.57	
16+25			6.63	82.04	
16+50			10.00	78.67	
16+75			13.30	75.37	74.0

Sta.	+	H.I.	-	Elev.	
A T.P.	0.04	76.10	12.61	76.06	
A 17+00			3.05	73.05	
17+25			5.73	70.37	69.0
A 17+50			7.30	68.80	67.0
A P.T. 17+55 ⁸⁷			8.10	68.00	
A T.P.	0.01	64.71	11.40	64.70	
A P.C. 17+82 ²²			3.05	61.66	
A 18+00			7.73	56.98	Top Concr. Grade Wall
A 18+25			7.55	57.16	
A 18+50			9.10	55.61	
A T.P.	5.72	60.00	10.43	54.28	
A Bot. of Gate			11.08	48.92	

Grades on Pipe Line Extension - L.O. Datum

Sta 0+00	97.0
+50	87.0
1+00	77.0
+50	71.0
2+00	68.0
+25	69.0
+50	72.0
+75	76.5
3+00	79.0
+50	83.0
4+00	87.5
+50	92.5
5+00	99.0
+50	104.5
6+00	109.0
+50	113.5
7+00	117.0
+50	122.0
8+00	128.5

Sta. Grades

8+50 137.0

9+00 144.0

+25 147.5

+50 150.5

+75 152.5

10+00 153.5

+25 154.0

+50 154.0

11+00 154.0

+25 154.0

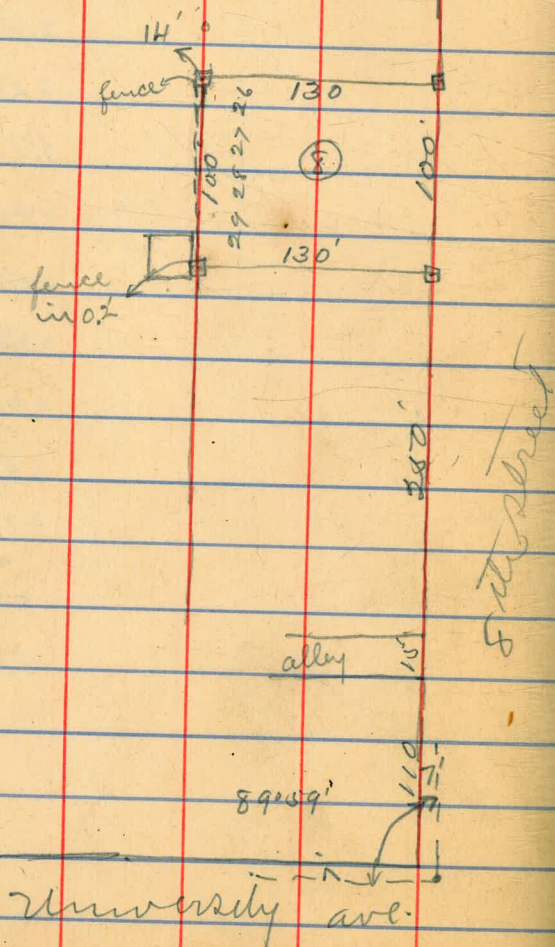
+50 153.5

+75 152.5

12+00 151.0

+50 148.0

Monterey Street



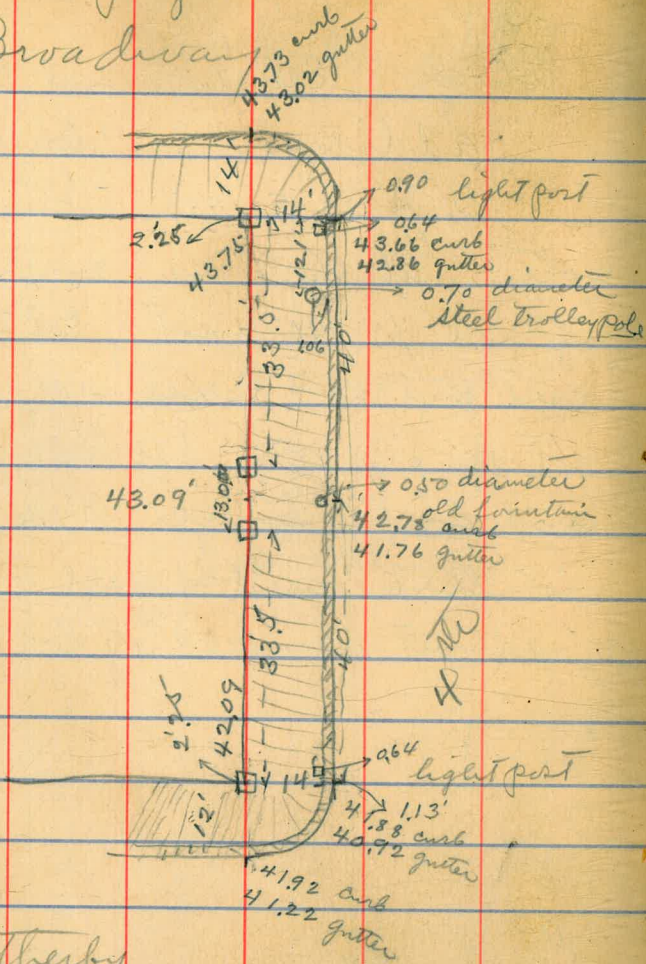
Survey of lots 26, 27, 28 & 29
Block 8 Estudillo and Capron's
addition

Jan 8, 1918

Behlde
Evans
more

note - at N.W. cor. north & south
fence is 14' west of lot line and
east and west fence is 07' north of
lot line. at S.W. cor. north
and south fence is 02' east of
lot line. and small building
is about 0.3 west of lot line.

Survey of sidewalk on 4th
Broadway



Weatherby

bet. Weatherby & Childs
Jan. 22/18 Evans

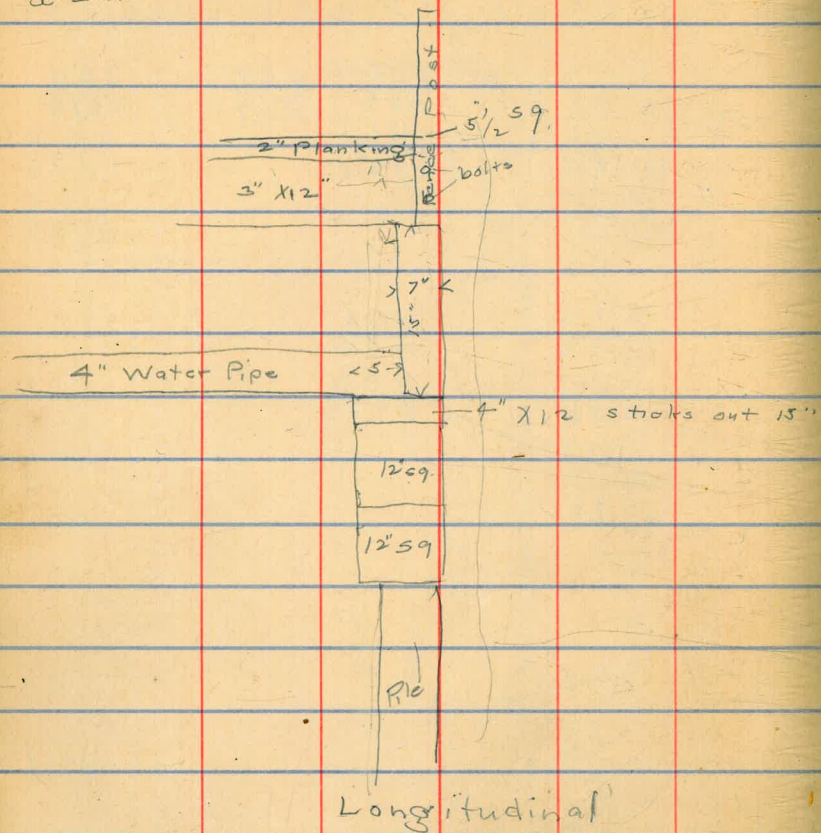
sw. cor. stone step, 44.31 B.M. S.E. cor. Broadway & North

2.07	4.50	4.29	3.60
<u>46.38</u>	H.I. 41.88	42.09	42.78
4.46	5.46		4.62
<u>41.92</u>	40.92		41.76
5.16			3.99
41.22			43.09

27.2	2.65
<u>43.66</u>	43.73
3.52	3.86
<u>42.86</u>	43.02
2.63	
43.75	

2/18/18
Dunkle
& Z.R.

Mission Bay Br.
S. End W. side

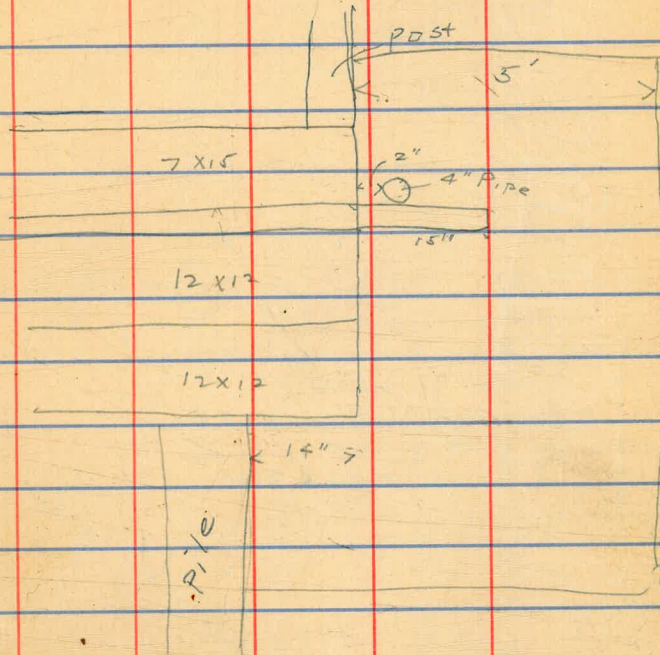


Longitudinal

5'-7" from floor level to outside
of 3" x 12"

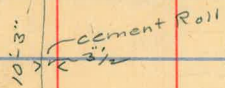
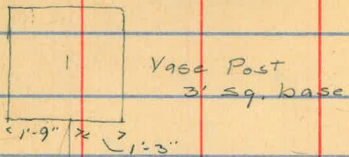
Proposed Toilets
Ocean Beach

Transverse



2/27/18
Z. Rungee

Proposed Comfort Sta. at Plaza.



12' 40"
(11' 11 1/2")



12' 0"



5' 8"



10 1/2"



11"



12"



10"



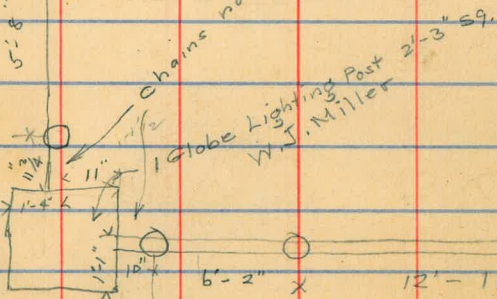
10"



10"

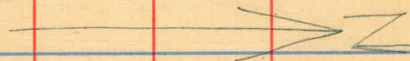
4 ^{old} Comfort Sta. Posts
same size (3' sq. base)

chains not fastened to Cor. Light Post



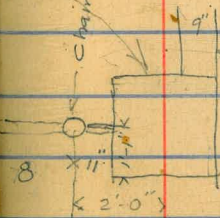
4th

Fence Posts & Cement Roll functionally symmetrical



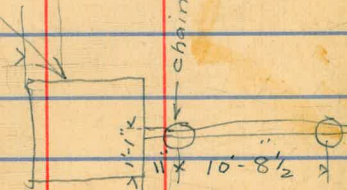
3/11/18 W. Bellon to Z.R.
57.67 from center of Ely Vase Post
to W. curb of 4th St.
43.55 center of Vase Post to
center of Lamp Post S.E. cor.
of Plaza.
14.15 sidewalk

Chain Ends at Fence Post

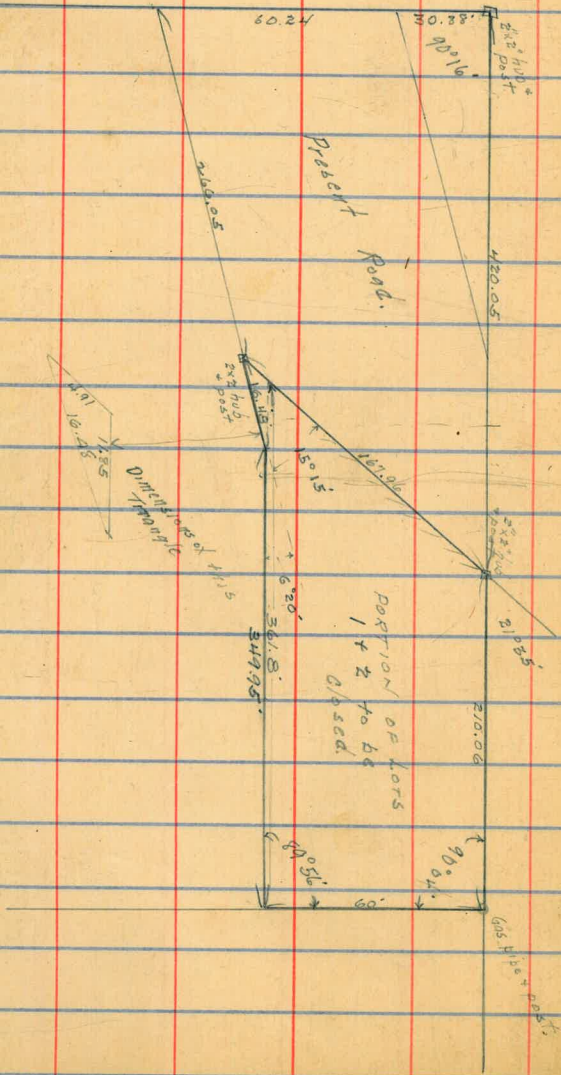


St

chain ends at Fence Post



9/25/15 Gregory Survey of Portion of
 Lots 1 & 2
 E.W. Morse's which was
 closed as st.



Cross-Section of Lookout Drive - La Jolla Hills.

10' (Ditch)
20' (Peds)
18' (Shoulder)

14' Sidewalks - Where no slopes are taken, continue slope of St. for toe of slope
Top Curb SW Cr

0+25

1284	111.48		9864	Primrose & Terry Rd	E	27.3	163.5
1292	124.20	0.20	111.48		Cl	42.4	168.4
1283	136.88	0.15	124.05		C	19.1	171.7
1295	149.71	0.12	132.76		Cl	15.1	175.7
1272	162.16	0.28	144.3		W	88	182.0
1285	174.92	0.09	162.07				

0+50

1288	187.69	0.11	174.81		W	78	183.0
1201	200.21	0.49	187.20		Cl	130	177.8
1064	210.75	0.10	200.11		C	15.7	175.1
Elbow of outlet pipe of shed near Keweenaw Sealed.				818	202.57		

379	214.08	0.46	210.29		E	23.1	167.7
0.52	201.72	1288	201.20				

0+75

185	190.77	1280	188.92	1	E	17.2	173.6
-----	--------	------	--------	---	---	------	-------

0+00 = End Lookout Drive

W		1140	179.4		C	111	179.7
Cl		17.4	173.4		Cl	86	182.2
Clr		211	169.7		W	49	185.9
Cl		250	165.8		T.P	4.58	189.90
E		294	161.4				

194.48

✓

19448

1+07 45 S Line Alley

W	356	190.92	on hub
ct	76	186.9	
C	102	184.3	
ct	129	181.6	
E	164	178.1	

1+25¹⁹ N₆ Line Alley

E	152	179.3	
d	114	183.1	
C	73	187.2	
+7	43	190.2	
ct	40	190.5	
W	84	191.1	

1+41

W	35	191.0	
ct	42	190.3	

1+50

W	10	193.5	
+9	25	192.0	
+11	46	189.9	
ct	46	189.9	

19448

1+75

E	12.1	182.4	
ct	84	186.1	
C	55	189.0	
ct	55	189.0	
+2	52	189.1	
+5	25	192.0	
W	03	194.2	

2+00 - PC - Curve #1 divided into 7 equal parts W = 17.87 - E = 26.77 on property

W	19	192.6	
+5	25	192.0	
+9	60	188.5	
ct	59	188.6	
C	57	188.8	
ct	78	186.7	
E	108	183.7	

194.48 ✓

1st Sta on Curve #1

NE	10.5	184.0
CL	7.9	186.6
C	6.2	188.3
CL	6.3	188.2
+5	6.7	187.8
+9	3.5	191.0
SW	3.0	191.5

2nd Sta on Curve #1

SW	38	190.7
+5	44	190.1
+9	73	187.2
CL	70	187.5
C	66	187.9
CL	79	186.6
NE	95	185.0

194.48

3rd Sta on Curve #1

NE	109	183.6
CL	89	185.6
C	74	187.1
CL	76	186.9
+5	76	186.9
+9	50	189.5
SW	49	189.8

4th Sta on Curve #1

SW	46	189.9
+7	56	188.9
+9	81	186.4
CL	81	186.4
C	81	186.4
CL	101	184.4
NE	124	182.1

194.48
5th Sta on Curve #1

NE	11.8	182.7
cl	9.6	184.9
C	8.7	185.8
cl	8.5	186.0
+5	8.7	185.8
+9	5.0	189.5
Sw.	4.0	190.5

6th Sta on Curve #1

Sw.	4.4	190.1
+3	5.0	189.5
+9	9.3	185.2
cl	8.9	185.6
C	8.6	185.9
cl	9.6	184.9
NE	11.6	183.9
T.P	8.30	186.18

190.23
7th Sta on Curve #1 - EC 0400

No.	10.3	179.9
cl	7.2	183.0
C	4.8	185.4
cl	5.2	185.0
+4	6.1	184.1
+8	1.7	188.5
So	0.4	189.8

0125

N	11.6	178.6
cl	8.6	181.6
C	6.3	183.9
cl	6.2	183.9
+2	6.9	183.3
+7	3.0	187.2
So	1.2	189.0

190.13

0150

So	23	187.9
tr	35	186.7
+11	70	183.2
cl	71	183.1
c	72	182.9
+5	95	180.7
cl	108	179.4
No	135	176.7

0175

No	173	172.9
+11	149	175.3
cl	142	176.0
c	80	182.2
cl	75	182.7
+4	74	182.8
S	50	185.2

190.23

1100

So	61	184.1
cl	80	182.2
c	81	182.1
+5	84	181.8
cl	119	178.3
+5	146	175.6
No	163	173.9
+20	200	170.2

1125

+20	216	168.6
No	148	175.4
cl	94	180.8
c	83	181.9
+8	79	182.3
cl	49	185.3
S	24	187.8

190.23

1st Sta on Curve #2

So	10	189.2
+11	20	188.2
cl	31	187.1
+2	38	186.4
+7	43	181.9
C	45	181.7
cl	91	181.1
+6	128	177.4
No	150	175.2
+20	260	164.2

1st Sta on Curve #2

+20	210	169.2
No	171	173.1
cl	95	180.7
C	87	181.5
cl	73	182.9
So	41	186.1

190.23

2nd Sta on Curve #2

So	8.5	181.7
+6	99	180.3
cl	8.5	181.7
C	9.0	181.2
+4	9.6	180.6
cl	14.6	175.6
+4	16.7	173.5
No	175	172.7
+15	200	170.2

3rd Sta on Curve #2 - 12" culvert needed on this Sta

+15	195	170.7
E	176	172.6
cl	160	174.2
C	111	179.1
+2	94	180.8
cl	87	181.5
W	114	178.8
+15	95	180.7

190.23

4th Sta on Curve #2

W	74	182.8
CL	82	182.0
T8	91	181.1
C	105	179.7
CL	135	176.7
E	172	173.0
T15	195	170.7

5th Sta on Curve #2

T15	195	170.7
E	163	173.9
CL	117	178.5
C	88	181.4
CL	87	181.5
T3	83	181.9
T12	39	186.3
W	35	186.7

190.23

6th Sta - FC#2 = 0400

W	44	185.8
T7	60	184.2
T11	101	180.1
CL	101	180.1
C	98	180.4
CL	119	178.3
E	157	174.5
T15	195	170.7

0425

T20	227	167.5
E	172	173.0
CL	139	176.3
T8	117	178.5
C	119	178.3
CL	120	178.2
T4	85	181.7
W	65	183.7

19043

0+50

w		7.1	183.1
t12		9.6	180.6
cl		12.5	177.7
t3		14.1	176.1
C		13.3	176.9
t7		13.2	177.0
cl		14.5	175.7
E		18.0	172.2
t20		23.6	166.6
T.P.	3.78	180.99	13.07 177.51 ✓

0+75

t20		15.5	165.5
E		10.8	170.2
cl		7.1	173.9
t3		6.0	175.0
0		5.8	175.2
t7		6.2	174.8
cl		1.9	179.1
N		t0.3	180.7

180.99

1+00

w		1.9	179.1
cl		4.2	176.8
t2		4.7	176.5
t5		7.9	173.1
0		7.7	173.3
t7		7.8	173.2
cl		8.7	172.3
E		11.4	169.6
t20		17.0	164.0

1+25

t20		20.0	161.0
E		14.0	167.0
cl		10.3	170.7
t3		9.5	171.5
0		9.5	171.6
t5		9.7	171.3
t8		6.7	174.3
cl		6.0	175.0
w		3.3	177.7

18099

1450

W	65	174.5
U	84	172.6
tr	88	172.2
TS	41	169.9
C	108	170.2
tr	109	170.1
Ch	118	169.2
E	155	165.5
tr	241	156.9

1475

tr	255	155.5
E	169	164.1
Ch	133	167.7
tr	121	168.9
C	121	168.9
tr	126	168.4
Ch	98	171.2
W	84	172.6

T.P.

108

17067

1140

169.59

PIPS at N Side on P.C.

17067

21025 = P.C. # 3

W	11	169.6
TS	60	164.7
tr	36	167.1
Ch	35	167.2
C	32	167.3
Ch	35	167.2
E	66	164.1
tr	103	160.4

1st Sta on Curve # 3

tr	85	162.2
E	56	165.1
Ch	36	167.1
C	39	166.8
Ch	44	166.3
W	46	166.1

17067

2nd Sta on Curve #3

W	56	165.1
Ch	54	165.3
C	48	165.9
Ch	57	165.0
C	79	162.8
+15	101	160.6

3rd Sta on Curve #3

+20	175	153.2
E	178	157.9
Ch	99	160.8
C	75	163.2
Ch	66	164.1
W	65	164.2

4th Sta on Curve #3 = P.R.C.

S	71	163.6
Ch	82	162.5
C	99	160.8
Ch	129	157.8
A ₀	16.6	154.1
+20	232	147.5

T.P. 267 163.69 9.65 161.02 ✓

Curve #4
1st Sta beyond P.R.C. - Curved into 3 equal parts { 13.16 inside }
23.06 outside

W	15	162.2
Ch	22	161.3
+7	28	160.9
C	37	160.0
Ch	64	157.3
E	104	153.3
+20	168	146.9

2nd Sta from P.R.C. #4

+20	178	145.9
E	121	151.6
Ch	86	155.1
C	48	158.9
+3	40	159.7
Ch	37	160.0
W	28	160.9

163.69

#4

3d Sta from P.R.C. S. Line Blvd

Place

+10	5.2	158.47
W	6.0	157.7
+6	18	158.9
cl	19	158.8
+5	52	158.5
C	88	154.9
cl	119	151.8
E	149	148.8
+20	175	146.2

#5

+6.5 on E + 11.3 on W = ϕ proposed Culvert 12"

+20	17.2	146.5
E	15.2	148.5
cl	13.0	150.7
+8	11.3	152.4
C	9.8	153.9
+7	54	158.3
cl	52	158.5
W	62	157.5
+10	51	158.1

163.69

1st Sta from S. Line Blvd. Curve divided into 4 equal parts #5

W	55	158.2
cl	58	157.9
+5	64	157.3
C	94	154.3
cl	123	151.4
E	142	149.5
+20	171	146.6

2d Sta from S. Line Blvd #5

+20	156	148.1
E	109	152.8
cl	74	156.3
C	64	157.3
cl	57	158.0
W	48	158.9

2d Sta +5 on E side #5

E	87	155.0
cl	74	156.3

16369.

3^d Sta from Blvd Curve #5

E	91	154.6
cl	77	156.0
c	67	157.0
cl	63	157.4
+5	62	157.5
+11	3.0	160.7
W	2.2	161.5

#5

4th Sta from S.L. Blvd = P.R.C. 693 from Al. line on E

W	0.4	163.3
+10	1.5	162.2
cl	50	158.7
+2	6.4	157.3
c	68	156.9
cl	76	156.1
E	92	154.5

16369

L/G

+400.00 W +693 on E = N.L. Blvd Place on E

E	92	154.5
cl	77	156.3
c	67	157.0
+8	6.4	157.3
cl	44	159.3
+12	0.7	162.0
W	0.1	163.6

#6

Bet N. Line Blvd & Xsect "O" - Curve divided into 15 equal parts
+14 on E side14.09 inside
24.45 outside

E	79	155.8
cl	70	156.7
+17 on E side		
E	55	158.2
+3	77	156.0
cl	70	156.7

16369
#6
1st Sta from N. Line Blvd

E	51	158.6
+54	49	158.8
+6	68	156.9
Ch	67	157.0
C	66	157.1
+4	28	160.9
Ch	18	161.9
W	08	162.9

#6 2nd Sta from N. Line Blvd.

W	20	161.7
Ch	33	160.4
C	38	159.9
+3	38	159.9
+6	73	156.4
Ch	70	156.7
+9	70	156.7
+13	56	158.1
E	60	157.7

16369
3rd Sta from N. Line Blvd #6

E	84	155.3
Ch	84	155.3
+1	83	155.4
+7	61	157.6
Ch	58	157.9
Ch	52	158.5
W	35	160.2

4th Sta from N. Line Blvd #6

W	42	159.5
Ch	63	157.4
C	78	155.9
+2	81	155.6
+5	99	153.8
Ch	97	154.0
+12	99	153.8
E	105	153.2
+10	126	151.1

16369'

5th Sta from N.L. Blvd. #6

t15	148	148.9
NE	117	152.0
tY	111	152.6
ck	112	152.5
t5	112	152.5
t8	91	154.6
c	87	155.0
ck.	70	156.7
SW	47	159.0

6th Sta from N.L. Blvd #6

S	48	158.9
ck	70	156.4
U	10.2	153.5
t4	10.8	152.9
t5	118	151.9
ck	117	152.0
N	121	151.6
t10	145	149.2

16369

7th Sta from N.L. Blvd. #6

t20	18.3	145.4
N	14.3	151.4
ck	112	152.5
t9	11.3	152.4
C	10.3	153.4
ck	74	156.3
So	48	158.9

8th Sta from N.L. Blvd. #6

So	46	159.1
ck	74	156.3
t9	9.5	154.2
C	105	153.2
ck	106	153.1
t8	11.2	152.5
N	125	151.2
t10	187	145.0
t20	210	142.7

16369

9th Sta from N.L. Blvd #6

+20	205	143.2
+10	177	146.0
N.	139	149.8
+9	96	154.1
ck.	95	154.2
C	94	154.3
+3	95	154.2
+6	80	155.7
cl.	68	156.9
S.	42	159.5

10th from N.L. Blvd #6

S.	32	160.5
cl.	58	157.9
+5	68	156.9
+7	82	155.5
C	82	155.5
cl.	81	155.6
+6	81	155.6
+10	109	152.8
N.	121	151.6
+10	157	148.0
+20	198	144.7

16369

11th Sta from N.L. Blvd #6

+20	158	147.9		
N.	99	153.8		
+5	85	155.2		
+10	65	157.3		
ck.	65	157.3		
C	67	157.0		
H	66	157.1		
+6	53	158.4		
Cl.	41	159.6		
TP	1157	171.23	4.03	159.66
S.	92	162.0		

12th Sta from N.L. Blvd #6

S.	72	164.0
ck.	84	162.3
+3	97	161.5
+8	122	159.0
C	118	159.4
ck	118	159.4
+5	114	159.8
N	152	156.0
+10	164	154.8

171.23

12th Sta from N.L. Blvd. #6

NW	10.9	160.3
+17	91	162.1
Ch.	94	161.8
C	93	161.9
Ch	94	161.8
+4	57	165.5
SE	54	165.8

14th Sta from N.L. Blvd. #6

E	39	167.3
+7	39	167.3
+11	76	163.6
Ch.	73	163.9
C	72	164.0
+4	73	163.9
+7	43	166.9
Ch	43	166.9
W	53	165.9

171.23

15th Sta from N.L. Blvd. = X Sect "O" #6-7

W	23	168.9
Ch	26	168.6
+7	25	168.7
C	52	166.0
Ch	51	166.1
+4	55	165.7
+9	25	168.7
E	271	168.52 on pipe at POC

1st Sta from "O" #7

E	09	170.3
+8	1.0	170.2
+10	28	168.4
Ch.	26	168.6
C	30	168.2
+3	1.0	170.2
Ch	29	170.3
W	0.2	171.0
TP	10.99	181.64
	0.58	170.65 ✓

181.64

2nd Sta from "O" #7

41.5 W of EL = Car House	102	171.4
Ch	103	171.3
+8	103	171.3
C	11.5	170.1
Ch	11.3	170.3
+5	11.6	170.0
+7	103	171.3
E	10.0	171.6

3rd Sta from "O" #9

E	94	172.2
+5	89	172.7
+9	101	171.5
Ch	100	171.6
C	98	171.8
Ch	92	172.4
39.3 W of EL = Fence at gate	93	172.3
45' W of EL = Car House	93	172.3

181.64

4th Sta from "O" #7

W	89	172.7
+9.9 = Fence	86	173.0
Ch	86	173.0
O	85	173.1
Ch	87	172.9
E	82	173.4

5th Sta from "O" #7

E	71	174.5
Ch	76	174.0
C	75	174.1
Ch	75	174.1
+5.5 = fence	77	173.9
W	80	173.6

6th Sta from "O" #7

W	74	174.2
+6.2 = fence	67.1	174.5
Top Concrete wall - at fence	64	175.2
End of Wall is 9' N of this Sta - Top	66	175.0
A	63	175.3
C	63	175.3
Ch	64	175.2
E	65	175.1

181.64 ✓

7th Sta from "0" #7

E	51	176.5
Ch	52	176.4
C	53	176.3
Ch	55	176.1
+11 = fence - Top wall	58	175.8
bottom wall	66	175.0
W	67	174.9
Top Wall Ctr gate - 6' S of 7 th Sta	57	175.9
Top Step " " " " "	52	176.4
Top end Wall - 14' S of 7 th Sta	51	176.5

8th Sta from "0" #7

W on concrete entrance to garage	40	177.6
+9.4 - edge concrete	43	177.3
Ch	46	177.0
C	42	177.4
Ch	36	178.0
E	44	177.2

181.64

9th Sta from "0" #7

E	32	178.4
Ch	30	178.6
C	23	178.3
Ch	34	178.2
N	42	177.4

10th Sta from "0" #7

+10	52	176.2
W	42	177.4
Ch	31	178.5
C	28	178.8
Ch	27	178.9
E	26	179.1

11th Sta from "0" #7

E	31	178.5
Ch	29	178.7
W	21	179.5
C	23	179.3
Ch	20	178.6
+9	69	174.7
W	76	174.0
+15	76	172.0

181.64 ✓

12th Sta from "O" #7

E. 98	27	178.9
cl	21	179.2
12	22	179.4
+5	15	180.1
C	15	180.1
+8	19	179.7
cl	25	179.1
+6	69	174.7
W	75	174.1
+15	88	172.8

13th Sta from "O" #7

+15	46	177.0
W	41	177.5
+8	40	177.6
cl	15	180.1
12	09	180.7
C	07	180.9
+8	01	180.9
cl	18	179.8
E	09	180.7

181.64

T.P. 1198 192.93 069 180.95 ✓

14th Sta from "O" #7

E	120	180.9
cl	71.6	181.3
+3	110	181.9
d	108	182.1
cl	115	181.4
+5	127	180.2
W	132	179.7
+10	140	178.9

15th Sta from "O" #7

W	90	183.9
+2	90	183.9
14	102	182.7
cl	100	182.9
C	95	183.4
+9	100	182.9
d	95	183.4
E	96	183.2

19293

16th Sta from 'O' #7

E	71	185.8
cl	78	185.1
+1	88	184.1
c	81	184.8
cl	86	184.3
+10	85	184.4
W	79	185.0

17th Sta from 'O' #7

W	70	185.9
cl	71	185.8
c	67	186.2
+10	75	185.4
cl	65	186.4
E	62	186.7

19293

18th Sta from 'O' #7

E	42	188.7
cl	47	188.2
+1	58	187.1
e	54	187.5
cl	58	187.1
+1	40	188.9
W	53	187.6

19th Sta from 'O' #7

W	43	188.6
+11	33	189.6
cl	43	188.6
c	35	189.4
+1	41	188.8
+9	27	190.2
cl	27	190.2
E	25	190.4
T.P.	12.1	204.01
	163	191.30

204.01 ✓

20th Sta from "O" #7

E	114	192.6
ct.	117	192.3
+3	118	192.2
+4	132	190.8
C	130	191.0
ct.	132	190.8
+3	135	190.5
+5	118	192.2
W	123	191.7

21st Sta from "O" = P.C.C. "A" #7

W	97	194.3
+8	90	195.0
+9	110	193.0
ct.	107	193.3
C	111	192.9
+5	113	192.7
+7	93	194.7
ct.	94	194.6
E	95	194.5

204.01

CC = "B" - 73' Wide

E	61	197.9
+17	66	197.4
+29	65	197.5
+34	88	195.2
+365-0	84	195.6
+57	87	195.3
+58	83	195.7
+73-W	90	195.0

EC = "C" 132.8' Wide

E	25	201.5
+45	46	199.4
+47	58	198.2
+664 C	62	197.8
+80	66	197.4
+100'	67	197.3
+15	73	196.7
+328-W	75	196.5
	143	202.58 ✓

ON Elbow outlet pipe at Shed

Cross-Section of Dwight St - 30th to Ray St

$\frac{12}{2}$ Doris
 $\frac{4}{2}$ Rocks
 $\frac{18}{2}$ Showin

+	HI	-	Elev	B.M. N.W. Cor		25' E	
314	341.09		337.95	30 th & Dwight	No	45	336.6
	E. Line 30 th St.				Ch	50	336.1
No - Sidewalk		4.50	336.6		4	51	336.0
Ch "		4.70	336.4		C	49	336.2
Quar paving		5.28	335.8		4	51	336.0
4		4.9	336.2		Ch	48	336.3
C		5.0	336.1		50	46	336.5
4 on paving		5.1	336.0				
Quar paving		5.30	335.8		50	47	336.4
Ch Sidewalk		4.74	336.4		Ch	54	335.7
So on Sidewalk		4.45	336.7		4	58	335.3
	14' E 30 th				C	57	335.4
50		4.5	336.6		4	56	335.6
Ch		4.7	336.2		Ch	49	336.2
4		4.9	336.2		No	47	336.4
C		4.8	336.3				
4		5.0	336.1				
Ch		4.4	336.7				
N.		4.5	336.8				

50' E

Dwight St.

341.69

75' E 30th

No	55	335.6
Ch	47	336.4
4	36	335.5
C	60	335.1
4	64	334.7
Ch	59	335.2
So	53	335.8

100' E

So	58	335.3
Ch	65	334.6
4	66	334.5
C	63	334.8
4	62	334.8
Ch	47	336.4
No	52	335.5

175' E

No	57	335.9
Ch	58	335.3
4	60	335.1
C	62	334.9
4	61	334.7
Ch	70	334.1
So	60	334.5

150' E

So	71	334.0
Ch	69	334.2
4	69	334.2
C	68	334.3
4	63	334.8
Ch	59	335.2
No	64	334.9

Dwight St.
341.09
175' E 30th

No	62	334.9
Cl	71	334.1
W	70	334.1
e	63	334.8
W	69	334.2
Cl	68	334.3
S.	75	333.6

200' E 30th - W. L. Ray

S.	71	334.0
Cl	68	334.3
W	67	334.4
c	71	334.0
W	70	334.1
Cl	66	334.5
N.	61	335.0

Cross Section of Gunn St - 30th to Ray

12/4 }
18/50

No	+	HT.	-	Elev.
	5.69	349.62		343.93
Ch	E Line 30th St			
1/4	No - on walk		4.5	345.1
c	Ch "		4.8	344.8
1/4	Gutr - parking		5.43	344.3
Ch	1/4 "		5.4	344.2
S _o	C "		5.5	344.1
1/4	" "		5.8	343.8
S _o	Gutr "		6.2	343.4
Ch	Curb		5.75	343.8
1/4	S _o on walk.		5.5	344.1
c	14' E 30th			
1/4	S _o		4.9	344.7
Ch	Ch		4.1	345.5
N _o	1/4		4.0	345.6
c			4.0	345.6
1/4			3.3	346.3
Ch			3.8	345.8
N _o			3.8	345.8

25' E 30th

H _o	4.0	345.6
Ch	3.7	345.9
1/4	3.2	346.4
c	3.8	345.8
1/4	3.9	345.7
Ch	3.7	345.9
S _o	4.1	345.0

50' E 30th

S _o	4.2	345.4
Ch	4.0	345.6
1/4	3.4	346.2
c	3.0	346.6
1/4	3.1	346.5
Ch	3.1	346.5
N _o	3.4	346.2

Gunn St.

349.62

75' E 30th

N	37	345.9
Ch	29	346.7
4	34	346.2
c	30	346.6
4	42	345.4
Ch	41	345.5
S ₀	44	345.2

100' E

S ₀	53	344.3
Ch	42	345.4
4	44	345.2
c	41	345.5
4	37	345.9
Ch	38	345.8
N	40	345.6

125' E 30th

N ₀	47	344.9
Ch	40	345.6
4	45	345.1
c	40	345.6
4	44	345.2
Ch	42	345.4
S ₀	48	344.8

150' E

S ₀	54	344.2
Ch	50	344.6
4	49	344.7
c	44	345.2
4	46	345.0
Ch	43	345.3
N ₀	40	345.6

Gunn St

349.62

175' E 30th

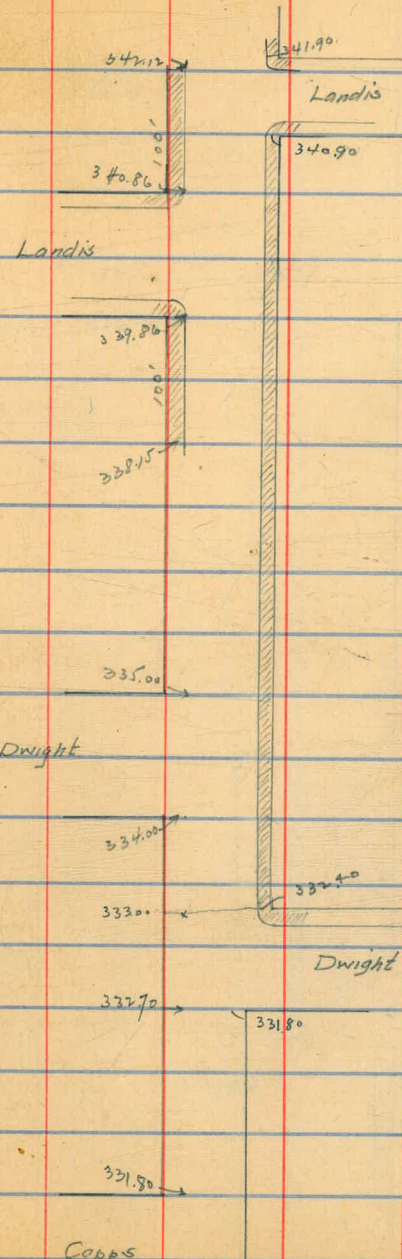
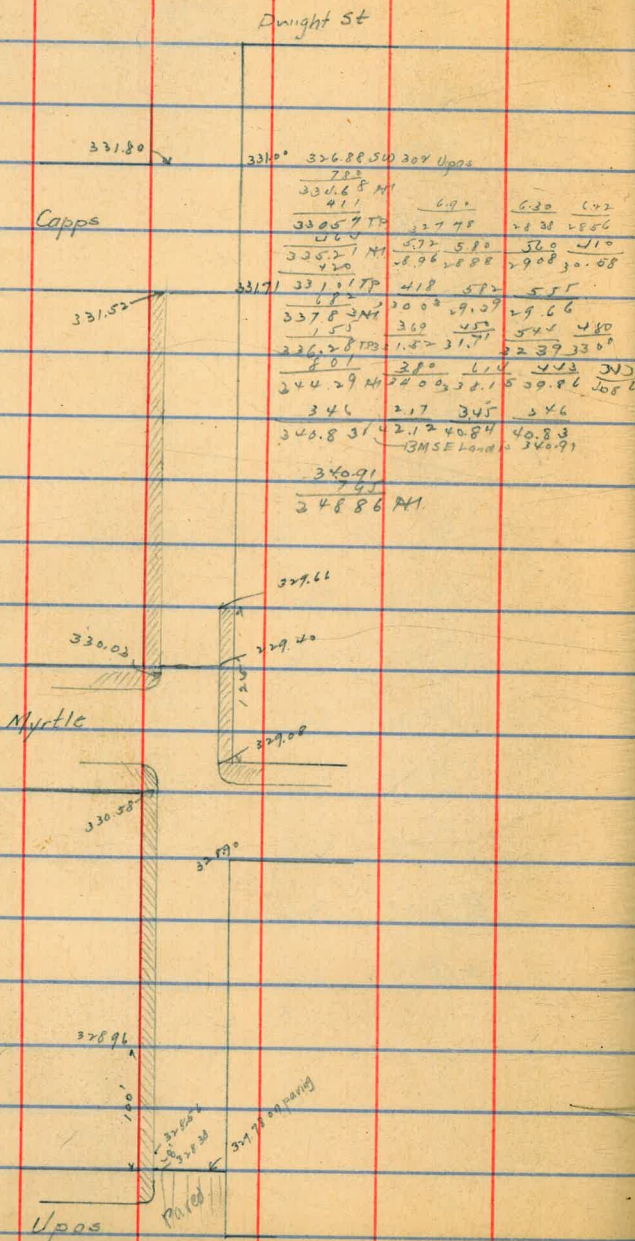
N	46	345.0
Ch	45	345.1
4	48	344.8
C	48	344.8
4	50	344.6
Ch	50	344.6
S	52	344.2

200' E 30th = W. L. Ray St

S	48	344.8
Ch	46	345.0
4	49	344.7
C	45	345.1
4	44	345.2
Ch	39	345.7
N.	36	346.0

Levels on Ray St. Over Ave to Upas St.

12 } Davis
 7 } Roche
 18 } Sherman



3524.1

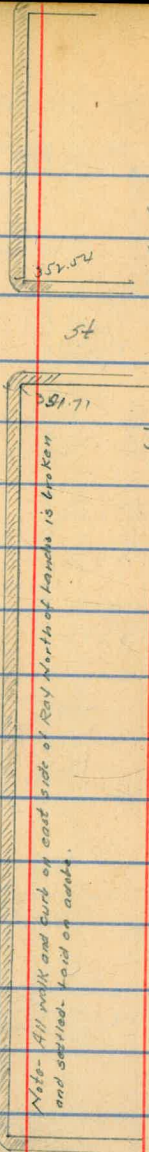
3512.0

346.00

345.00

342.2

340.86



352.00

351.71

Landis

348.86 AM
79.
346.92 TP
835
355.57.41

41.2 360
51.21 41.71

277 290
52.54 52.41

31.0
51.71 51.03 OMSE Right

Rightmap

St

Gunn

Note - All work and curb on east side of Ray North of Landis is broken and settled. Land on grade.

Landis

266
 .00029
 2394
 5344
 .0771

A9 6+19
 6274

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 16 FEET WIDE. SIDE SLOPES 1½ TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Calculated by F. E. Paradis, C. E.

3/11/11
 57.7 to 4th St. Creek
 43.55
 14.15

Handwritten calculations and notes on the right page, including various numerical values and a circular stamp.

Stamp: EUGENE DIETZGEN CO. MANUFACTURERS & IMPORTERS OF DRAWING MATERIALS AND SURVEYING INSTRUMENTS. NEW YORK, CHICAGO, NEW ORLEANS & SAN FRANCISCO.