1034

FIELD BOOK.

No. 403

Southern County Bldg DEFLECTION

Fourth Truss from West End		CEN	NE
12th " " "		1 1/2	1 3/4
3rd Truss from East	Top	5 1/4	
	Bot	4 3/4	
4th Truss. "	Top	4 1/4	
	Bot	3 3/4	
5th Truss	Top	4"	
	Bot	3 1/2	
6th Truss	Top	6 1/4	
	Bot	5 7/8	

San Joaquin Bldg

Foundation —

N. E. Corner Trussed up.

Roof O.K.

Exterior in good preservation

except front Ent.

Kern & Tulare Bldg

Foundation O.K. dry.

Roof unable to examine but

from observation O.K

Roof leaks in panels

Truss pilasters 6 x 6

Exterior fair state of pres.

Top of base cracked

11.41 439.85 B.M. 428.44

1.55 438.30 Top Reservoir

7.14 432.71 bottom "

Alameda County Bldg.

Roof O.K. 

Cement Tile Roof

Exterior O.K.

Kansas Bldg

Inside & Outside O.K.

except Band at Foundation

Fire Station

Inside Beams de Stacked

Outside Staff bad.

Utah Bldg

Cannot See Trusses
Interior Showing bad leaks

Montana

Trusses good
Exterior Fair

New Mexico

Foundation Ok
Exterior Fair

Washington Bldg
Palace of Mines

Exterior Fair Condition

Transportation Bldg

Oregon.

Exterior bad.

Thursday Feb 15

Indian Arts.

Roof O.K.
Roof needs entire Composition Covering
Foundation showing Signs of
Cor. West portion
No ventilation

Foundation Footings Show
insufficient Dipping

Exterior Staff work needs
attention

Science of Man. (36)
- Education
Foundation O.K. French
Lack of Ventilation

Roof Trusses O.K.
Roof need repairs
Exterior Fair Staff work needs
repairing

Sacramento or Government Bldg.

Roof need Repairs
Plaster Good.
Staff need repair
Cornice "
Foundation O.K. except
no ventilation dry rot starting

Home Economy Bldg (36)

Foundation Deplorable

EW Ditch 4 wide 27 Rain
NS " " 17 "
Roof need Repairs

Agricultural Bldg.

W. N & NW Foundations in
water 4" in places

NE Corner OK
Roof needs repairs
Staff work in bad Condition
Fire wall & parapet broken &
cracked on top

Commerce & Industry
Canadian Exhibit

5 Pr. Covers of Main Driving
Rigging due to leaking from
Exhibit
Foundation Generally Good
" Ventilated Thoroughly

Truss Good

Roof needs repairing

Staff need repair

Exterior Good Condition

Foreign Arts Bld.

Foundation
Underpinning 35 Max. length
posts 6×6 Studs 2×6 · 24"
Posts 8 ft Centers

Foundation lower than ground
Shows dampness

Outside OK
Roof Trusses good
Roofing bad
Stairs "

Calif. Bldg

Roof leaks.

Fishmens Bldg

OK
Roof need Coating.

Nevada State Building

Foundation damp & Sagg y
No ventilation
Roof Trusses good
Roof Comp. needs Repairs

Standard Oil Bldg

Inside Good
Exterior need repair
No ventilation to foundation

Harvester Bldg

Foundation Good no ventilation
Outside Fair
Parapets & Staff bad.
Roof needs repair

Ottawa Apt. Feb 20.17

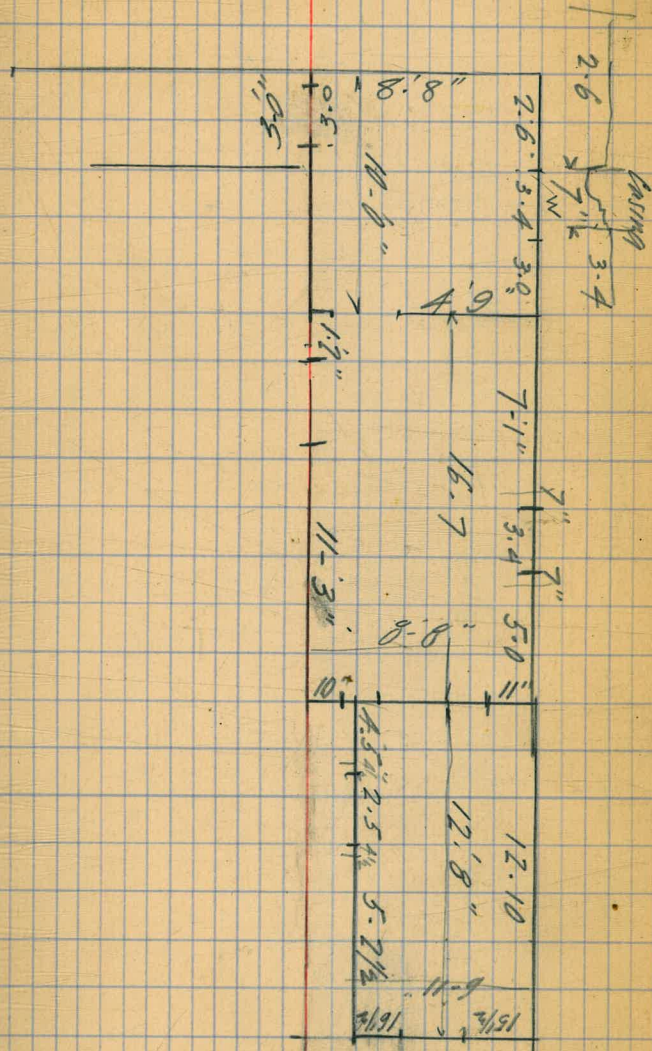
Minor patching
No bracing
No Ridge board.

Mr Sarcotti The owner.

SW Corner Roof

Mr Margaret Westfall
4438 Campus.
SW Corner Roof
Chimney down.

Rivers Playground Commission



GLASS
16
CASE
5'-9"
16
CASE
5'-9"
3 MIRRORS
4 MIRRORS
WALL CASE
8'-0"
COUNTER
SAFE
4'-2"
DOOR
2 FT.
6

2/4/18

Gregory
Moore
Miller

Survey of Ridge Road
Xrom Pueblo Farm.

SEE PAGE 17
THIS BOOK

64+47.82 E.C.

64+15 P.I. 7°32' L

R = 500
St = 32.92
Lc = 65.47

54+82.08 P.C.

SEE PAGE 17

24+97.5 ℄ P.O.T.

35+00 ⊙ POT.

69+00 @ P.O.T.

76+00 ⊙ P.O.T.

80+29.61 E.C.

79+00 Δ 25°10'L

R=600
St=133.93
Lc=263.54

77+66.07 P.C.

103+00.71 = 121+32.64 E.C. Book 1010 page 7

102+90.35 E.C.

99+97.27 34°41' L R = 1000 St = 312.26 LC = 605.34

96+85.01 P.C.

3/25/18 Gregory Moore Miller

Survey of Ridge Road from Pueblo Farm Bldgs to Top of Torrey Pines

51+00 ⊙ P.O.T.

45+65.68

43+50 Δ 3°27' L.

37+50

33+50

32+00 ⊙ P.O.T.

22+00 ⊙ P.O.T.

19+26.12 = Pueblo Line

17+50

15+10.52 = 26+30.83 E.C.

14+00 ⊙ P.O.T.

12+48

6+00 ⊙ P.O.T. N 13°30'W.

0+00 = 109+13.34
Desc. 19 Book 1010

SEE PAGE 53 FOR FINAL LOCATION HERE

32+00
15+10.52
16+89.48

42+00
15+10.52
26+89.48

17

70.20

BM 419.92 ○ 25.08' ⊞ BM 420.98

Granite Mon
N.W. Cor
P.L. 1314

89°07'30"

1027.9'

P.L. 1323

P.L. 1311

10"x10" post

90°00'

25' ○ 25' ⊞ BM 442.06

14" pipe reeled

438.30 Elev Top of Reservoir
432.71 " Bottom "

Reservoir 58'

89°05'

116.9'

25' ○ 25' ⊞ BM 428.44

25' ○ 25' ⊞ BM 413.11

Granite Mon
N.W. Cor
P.L. 1311

P.L. 1314

10x10 post

1012.60

90°28'00"

P.L. 1311

14" pipe reeled

25' ○ 25' ⊞ BM 402.06

To Linda Vista Road

40'

40'

Linda Vista Road

Appr. 8% Gr.

To San Diego

98+91.00 = Pueblo Line

98+00 ⊙ P.O.T.

95+00 ⊙ P.O.T.

80+00 ⊙ P.O.T.

73+38.5 E.C.

73+05.90 Δ 7°29' L

72+73.2 P.C.

R = 500
St = 32.70
Lc = 65.30

58+00 ⊙ P.O.T.

18

NW. Cor. P.L. 1326

Granite Mon.

425.25

49°31' → P.L. 1330

P.L. 1326

30' 30' B.M. 442.65

30' 30' B.M. 431.50

35' 35' B.M. 430.19

30' 35'

35' 35' B.M. 439.63

40°00'

25' 25' B.M. 424.56

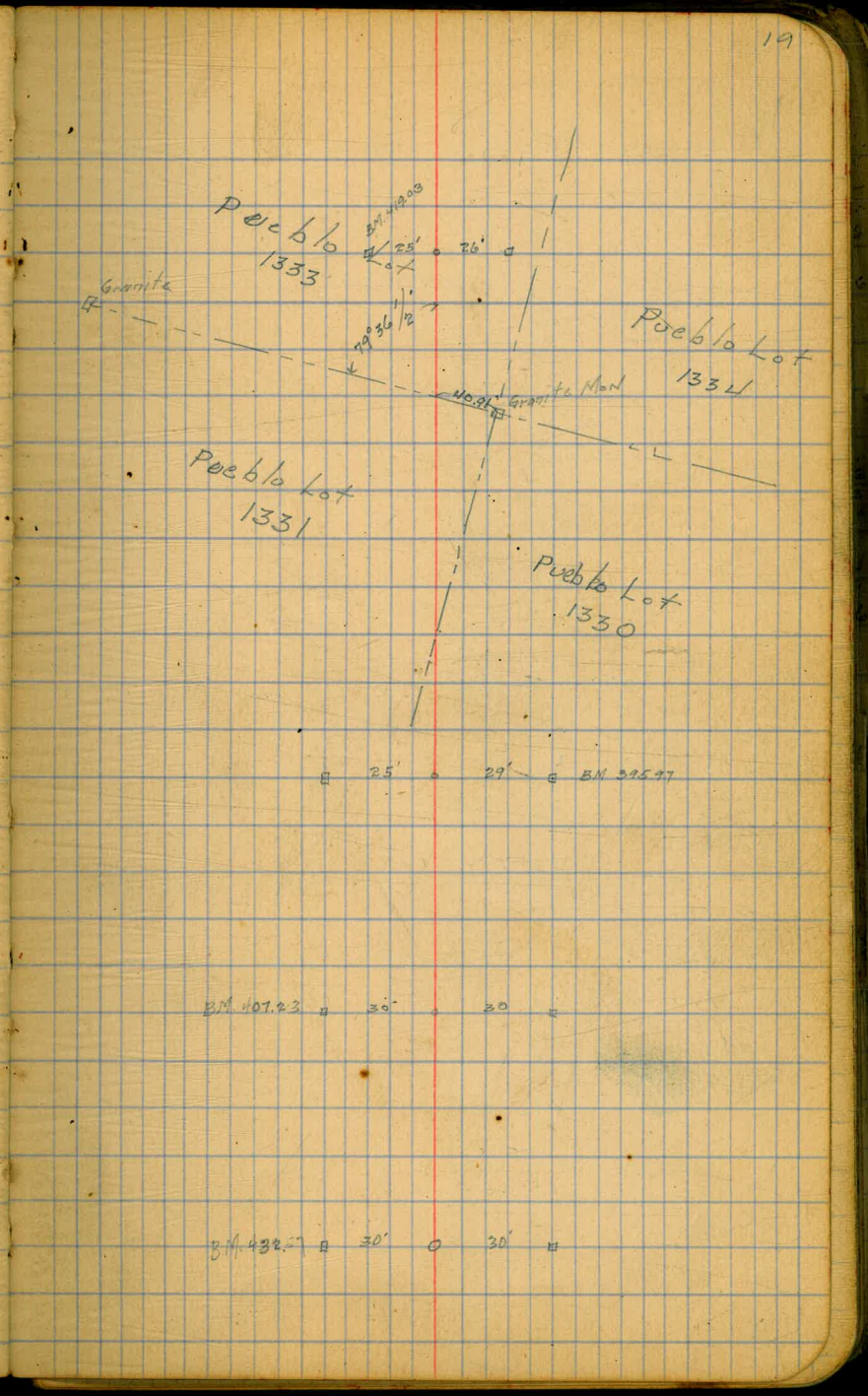
128+00 ⊙ P.O.T. Mag. N 21° 30 W

124+73.95 Pueblo Line

120+00 ⊙ P.O.T.

112+00 ⊙ P.O.T.

102+50 ⊙ P.O.T.



169+92.27 = 121+32.64 EC. Book 1010 Page 7

169+80.17 EC.

166+86.16 Δ 34°42' L

163+74.54 P.C.

For change of alignment see page 48 this book

R = 1000
St = 312.42
Lc = 605.63

1st dex from PC	1°43'46"	= 2586
2nd " " PC	2°89'41"	58
3rd	Sta 165	8 35 28
4th	+50	5 01 35
5th	166	6 27 32
6th	+50	7 53 29
7°	167	9 19 25
8	+50	10 45 22
	168	12 11 19
	+50	13 37 15
	169	15 03 11
	+50	16 29 07
169+80.17		17°-1

158+00 ⊙ POT. N49°35'W

152+00 ⊙ POT.

1st dex	2°05'57"	= 4380
2nd "	4°28'54"	4945
3rd "	6°52'07"	4945
4th "	9°15'22"	
5th "	11°38'37"	

147+19.69 E.C.

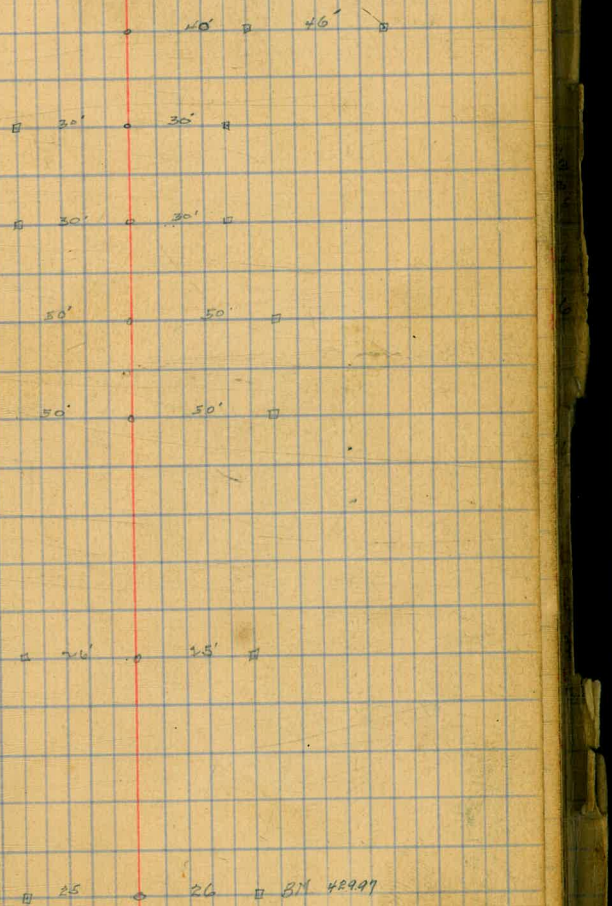
145+90.08 Δ 25°10' L

R = 600
St = 133.93
Lc = 263.54

144+56.15 P.C.

142+00 ⊙ P.O.T.

134+00 ⊙ POT.



3/25/13

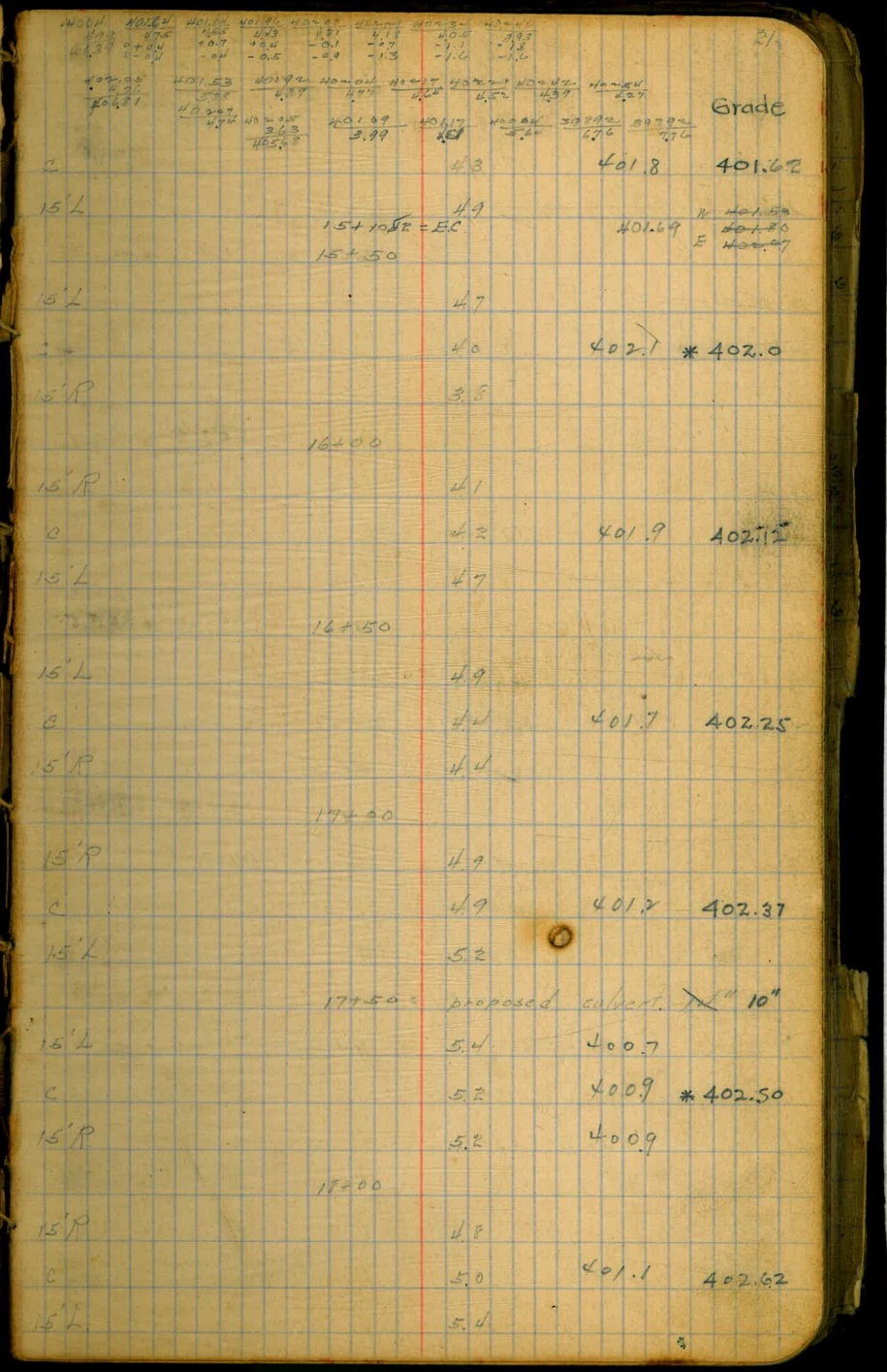
Gregory
Moore
Miller

CROSS SECTION OF
30' Road from
Sta 12+48 page 17 this book
to connect with Road at
Top Torrey Pines

					Grade
B.M.	12.79	394.97		382.18	RP Page 2 book 1011
	5.62	400.28	0.31	394.66	Mailing pole Lt. of Road
	12.53	406.14	6.67	393.61	
	Sta 12+48 = Approx* ctr Linda Vista Road				
15' L			9.6	396.6	
C			9.2	396.9	397
15' R			9.1		
"	13+00				
15' R			9.0		
C			8.5	397.6	398.0 398.12
15' L			8.4		
	13+50				
15' L			7.5		
C			7.3	398.8	399.0 399.25
15' R			7.5		
	14+00				
15' R			6.2		400.12 400.37
C			5.70	400.4	on 400
15' L			6.3		
	14+50				
15' L			5.2		
C			4.9	401.2	401.45 * 401.5
15' R			5.2		
	15+00				
15' R			4.5		

SEE PAGE 59 FOR LEVELS HERE

SEE PAGE 59
FOR LEVELS BACK
OF STA 15+10 ←



		Grade
C	401.8	401.62
15' L		
15+10.52 = EC	401.69	N 401.50 E 401.87
15+50		
15' L		
C	402.1	* 402.0
15' R		
16+00		
15' R		
C	401.9	402.12
15' L		
16+50		
15' L		
C	401.7	402.25
15' R		
17+00		
15' R		
C	401.7	402.37
15' L		
17+50 = proposed culvert. 74" 10"		
15' L	400.7	
C	400.9	* 402.50
15' R	400.9	
18+00		
15' R		
C	401.1	402.62
15' L		

	18+50		Grade
15' L		4.5	
C		4.1	402.0 *402.75
15' R		4.0	
	19+00		
15' R		2.3	
C		2.6	403.5 *403.75
15' L		3.2	
	19+50		
15' L		1.2	
C		0.9	405.2 *405.25
15' R		0.8	
T.P.	11.25 H17.11	0.27 H05.87	
	20+00		
15' R		9.7	
C		9.9	407.2 407.0
15' L		10.3	
	20+50		
15' L		8.1	
C		7.9	409.2 * 408.75
15' R		7.7	
	21+00		
15' R		6.2	
C		6.1	411.0 * 410.25
15' L		6.8	

Ridge 22

	21+50		Grade
15' L		5.9	
C		5.3	411.8 *411.50 ~~412.10~~
15' R		4.8	
	22+00		
15' R		4.0	*412.50 ~~412.95~~
C		4.20	412.94 07 406
15' L		5.1	
	22+50		
15' L		4.2	
C		3.5	413.6 H13.37 ~~413.8~~
15' R		3.5	
	23+00		
15' R		2.9	
C		3.0	414.1 XH14.25 ~~414.65~~
15' L		3.5	
	23+50		
15' L		2.6	
C		1.8	415.3 H15.13 ~~415.5~~
15' R		1.7	
	24+00		
15' R		1.3	H15.52
C		0.9	416.2 *~~416.00~~ 416.38
15' L		1.2	
T.P.	3.98 H20.51	0.58	416.53

420.55 | 417.09 346 -0.1 -0.1 416.09 4.86 +0.1 4.96 | 417.34 3.71 -0.3 -0.1 415.09 5.76 -0.8 +0.6 | 417.09 346 -0.5 +0.2 416.54 5.91 -1.2 -0.2 | 420.51

24+50

15'L
C
15'R

25+00

15'R
C
15'L

25+50

15'L
C
15'R

26+00

15'R
C
15'L

26+50

15'L
C
15'R

27+00

15'R
C
15'L

416.32 2.55 414.77 4.29 415.03 3.63 414.74 1.03 411.89 4.83 414.83 5.56 | 416.72 2.13 414.67 2.3

Grade

3.8
3.6 416.9 * 417.28 (415.91 416.40)
3.9
3.7
3.4 417.1 * 417.5 (416.30 416.80)
3.6
3.6
3.6 416.9 * 417.25 (416.20)
4.0
4.5
4.3 416.7 416.25 (416.0)
4.3
5.2
5.3 415.7 * 415.25 (415.30)
6.0
6.8
6.3 414.7 * 415.0
6.2

420.65 | 417.09 -0.5 -0.4 | 416.34 4.21 -1.3 +0.2 416.34 4.96 -1.2 -0.2 | 417.28 3.97 -1.1 +0.5 415.17 4.75 | 420.26 0.33 -0.9 -0.7 +0.9 419.39 1.24 418.15 3.65 | 422.66 9.83 -0.7 +0.8 422.74 1.21 | 425.09 7.45 -1.1 +1.1 418.89 6.07 422.96 9.57 422.82 8.92

Ridge #3

27+50 = X' culvert proposed

Grade

6.5 414.0
6.8 413.7 ~ 415.25
7.1 413.4
6.2
5.5 415.0 * 415.5
5.1
2.6
3.0 417.5 417.8 417.94
3.8
1.3
0.8 420.3 420.1 420.38
0.25 420.26
11.7
9.4
9.8 422.6 422.4 * 422.82
10.4
8.4
7.4 425.0 424.1 * 425.25
6.7

T.P. 12.17 432.43

27+00
28+00
28+50
29+00
29+50
30+00

		30+50		
15' L				
C				
15' R				
		31+00		
15' R				
C				
15' L				
		31+50		
15' L				
C				
15' R				
		32+00		
15' R				
C				
15' L				
		32+50		
15' L				
C				
15' R				
		33+00		
15' R				
C				
15' L				

		Grade	
4.8			
5.4	427.0	* 427.25	
6.4			
5.2			
3.9	428.5	* 428.75	
3.1			
2.1			
2.9	429.5	* 429.75	
4.0			
3.6			
2.41	430.02	on hub	
1.4			
1.2			
2.1	430.3	* 430.5	
3.2			
2.8			
1.8	430.6	430.75	
0.9			

		33+50	
15' L			
C			
15' R			
		34+00	
15' R			
C			
15' L			
T.P.	3.06	434.39	
		34+50	
15' L			
C			
15' R			
		35+00	
15' R			
C			
15' L			
		35+50	
15' L			
C			
15' R			
		36+00	
15' R			
C			
15' L			

		Grade	
0.9			
1.6	430.8	* 431.0	
2.8			
2.9			
1.8	430.6	430.75	
0.9			
2.00	430.43		
3.6			
4.0	430.4	* 430.5	
5.2			
6.0			
5.0	429.4	* 429.5	
4.3			
5.8			
6.1	428.3	* 428.5	
7.1			
8.5			
7.7	426.7	* 427.0	
7.0			

Ridge 25

Grade

36+50			
15' L	8.5		
C	9.1	425.3	* 425.5
15' R	10.0		
37+00			
15' R	10.9		
C	10.3	424.2	* 425.75
15' L	9.6		
37+50	10" CMP, proposed.		
15' L	9.5	424.9	
C	10.2	424.7	* 426.0
15' R	11.0	423.4	
38+00			
15' R	9.8		
C	9.2	425.2	* 426.25
15' L	8.5		
38+50			
15' L	6.9		
C	7.8	426.6	* 426.75
15' R	8.3		
39+00			
15' R	6.6		
C	5.8	428.6	* 428.75
15' L	5.1		

39+50			
15' L	2.6		
C	3.6	430.8	430.75
15' R	4.2		
40+00			
15' R	1.8		
C	1.1	432.3	* 432.75
15' L	0.4		
T.P.	0.23	434.16	
40+50			
15' L	9.6		
C	10.4	435.7	435.75
15' R	11.2		
41+00			
15' R	8.3		
C	7.7	438.4	* 438.75
15' L	6.9		
41+50			
15' L	4.9		
C	5.5	440.6	* 440.75
15' R	6.3		
42+00			
15' R	4.7		
C	4.1	442.0	* 441.25
15' L	3.6		

15' L		3.0	
C		3.5	442.6 * 442.75
15' R		3.9	
	43+00		
15' R		3.5	
C		3.5	442.6
15' L		3.6	
	43+50 A		
15' L		4.2	
C	4.95	445.17 3.87	442.22 .30
15' R		3.6	
	44+00		
R		3.3	441.1
C		4.5	440.7 * 441.0
L		4.8	439.6
	44+50		
L		6.6	437.8
C		6.8	438.4 * 438.75
R		5.7	438.7
	45+00		
R		8.3	436.1
C		9.7	435.5
L		9.8	434.6
	45+50		
L		13.6	430.8

C			
R			
	46+00		
TP	0.62	433.00	
R			
C			
L			
	46+50		
L			
C			
R			
	47+00		
R			
C			
L			
	47+50		
L			
C			
R			
TP	5.63	435.54	
		429.91	
	48+00		
R			
C			
L			
	48+50		
L			

Ridge

Grade

13.2	432.0	* ~~432.25~~ 432.0 431.13
11.9	432.5	
12.79	432.38	
13	428.8	
5.2	427.8	428.25
5.5	426.6	
9.3	422.8	425.39 424.50
8.9	424.1	* ~~424.25~~
7.4	426.7	
10.1	421.7	~~422.75~~ ~~422.50~~ ~~428.00~~
11.7	421.3	* ~~421.50~~
11.6	420.5	
12.0	419.1	
13.1	419.9	421.0 * ~~420.75~~
11.7	420.4	
13.09	419.91 ~~420.91~~	
	NO CULVERT.	
7.1	418.9	
6.2	419.3	420.50 ~~419.9~~
7.7	418.6	
9.1	419.2	

H26.25 H=0 H20.25 H419 H=5.54 H=1.34 H21.59 H21.58 H21.34
2.34 2.90 5.45 5.0 4.76 4.33 5.01
0.0 +0.1 -.00 -0.1 -0.3 +0.3 -0.4
-1.0 -1.0 -1.0 -0.3 -0.4 +0.3 -0.2
H=6.35 Xerotapes

H37.60 H20.17 H20.17 TP. H20.24 H20.47 H20.92 H20.67 H21.17 H20.92
1.45 6.08 H26.25 5.63 5.58 5.93 5.58 5.08 5.35

H24.75 H20.17 H20.24 H20.54 H20.67 H20.8 H20.92 H20.67 Grade
4.58 4.38 4.21 4.08 2.95 3.83 4.68 *H20.25
H20.13

C 5.5 H20.0

R 49+00 6.7 419.6

R 5.9 420.4 ✓ H20.50

C 5.1 H20.4 ~~H20.60~~

L 6.8 419.5

49+50

L 6.3 420.0

C 4.7 H20.8 H20.07 H20.75

R 5.8 420.5

50+00

R 5.3 421.0 H20.75 H21.0

C 4.3 H21.2 *~~421.50~~

L 5.7 420.6

50+50

L 5.1 421.2 H20.87 H21.18

C 3.9 H21.6 *~~421.75~~

R 5.1 421.2

51+00

R 5.1 421.2 × H21.0 H21.08

C 4.1 H21.4 ~~421.68~~

4.56 H20.98 Tie 406

L 5.1 421.2

517.50

L 5.2 421.1 × H20.75 × H21.0 H20.96

C 4.2 H21.3 *~~421.50~~

R 5.6 420.7

H24.25 H20.54 H20.34 H17.24 H16.34 H14.84 H16.34 H18.58
-0.4 2.01 5.51 10.01 11.51 3.178 7.18
-0.5 +0.9 +0.3 +0.6 +0.8 H14.57 -0.8
-0.8 -0.8 -0.7 -0.7 10.46 -0.8
8.60

H24.24 H20.08 H19.24 H17.94 H16.00 H16.44 H16.14
4.89 3.85 6.39 7.38 6.55 7.02 7.35
H24.75
479.41

R
C
L
L
C
R
R
C
L
T.P. 2.49 H20.38 H24.35
L
C
R
L
C
L
L
C
R.

52+00

60 420.3

45 H20.7 H=0.0 *~~421.00~~

60 420.3

52+50

76 418.7

62 419.3 419.0 ~~419.50~~

66 419.7

53+00

82 417.9

76 417.9 ~~418.00~~

92 417.1

77.5 417.79

53+50

10.5 415.9

3.8 416.5 417.0 ~~416.50~~

9.7 416.7

54+00

10.9 415.5 416.5 ~~416.0~~

5.2 415.1 × ~~415.20~~

12.0 414.9

H=5.0 Xerotapes 54+50

12.1 412.9

6.8 413.5 H16.85 H15.0 *~~413.75~~

12.3 412.7

54+80 NO CULVERT NEEDED

R.		12.6	412.4	Grade
C		7.2	413.1	*+75 ~~413.5~~
L		11.9	413.1	
	55+00			
L		10.4	414.6	* 416.5 ~~416.0~~
C		6.2	414.1	* ~~414.0~~
R		11.9	413.1	
	55+50			
R.		7.4	417.6	
C		2.7	417.6	417.0
L.		7.4	417.6	
	56+00			
L		5 ±	419.8	
C		0.3	420.0	419.0 * ~~420.0~~
R		4.8	420.2	
T.P.	6.41	426.69	0.0	420.28
	slopes +N50n			
	56+50			
R		3 ±	421.8	
C		5.3	421.4	421.0 * ~~421.75~~
L		3.7	421.3	
	57+00			
L		2.5	422.5	
C		4.1	422.6	422.0 ~~422.75~~
R		2 ±	422.8	

58+00

L		6.1	423.7	423.90 424.0
C		2.3	424.4	* ~~424.75~~
R		5.0	424.8	
T.P.	2.13		424.56	To 405
	58+50			
R		6.4	424.8	
C		4.9	424.4	424.33
L		7.3	423.9	
	59+00			
L		6.7	423.5	
C		4.7	424.6	424.67
R		6.6	424.6	
	59+50			
R		6.7	424.5	
C		4.3	425.0	425.0
L		6.1	425.1	
	60+00			
L		5 ±	426.0	
C		3.8	425.5	425.33
R		6.4	424.8	

431.43 | 425.60 | 425.74 | 425.59 | H29.28
-0.2 | -0.4 | -0.5 | 431.43 for slope
+0.9 | +0.8 | +1.6
424.96 | 424.51 | 424.03
6.27 | 6.42 | 7.15
+0.7 | -1.0 | -1.0
+1.5 | +1.6 | +1.4

425.53 | 425.66 | 425.82
3.07 | 2.93 | 2.61
425.51 | 2.15 | 425.52 | 3.01
427.69

425.37 | 425.80 | 425.85
2.37 | 2.49 | 2.61
424.60 | 424.16
3.09 | 3.53

60+50

R	6.0	425.2	
C	3.3	426.0	425.67
L	4.8	426.4	

61+00

L	4.8	426.4	
C	3.2	426.1	425.60 426.0
R	5.7	425.5	

61+50

R	6.2	425.0	
C	3.4	425.9	425.40 425.58
L	4.7	426.5	

62+00

L	5.1	426.1	
C	4.0	425.3	425.12
R	6.6	424.6	

62+50

R	7.2	424.0	
C	4.7	424.6	424.67
L	5.3	425.9	

63+00

L	6.0	425.2	
C	5.2	424.1	424.24
R	8.0	423.2	

431.43 | 423.64 | 423.21 | 424.77 | 424.34 | 424.44 | 424.54
7.30 | 2.57 | 8.02 | 8.46 | 8.89 | 7.24 | 7.24
422.73 | -1.2 | -1.6 | -1.9 | -2.3 | -2.1 | -1.2
2.70 | +1.0 | +0.8 | +0.4 | +0.6 | +0.7 | +0.8
429.8

427.64 | 423.72 | 423.30 | 424.26 | 424.41 | 424.57 | 424.64
3.77 | 4.99 | 4.54 | 5.24 | 5.17 | 5.07

63+50

R	8.5	422.7	
C	6.0	423.3	423.40
L	6.7	424.5	

64+00

L	7.5	423.7	
C	6.7	424.6	423.37
R	9.2	422.0	

64+50

R	10.2	421.0	
C	7.6	421.7	422.43
L	8.2	423.0	

65+00 culvert needed.

L	8.6	422.6	
C	8.1	421.2	422.5
R	10.7	420.5	

H29.78 for slope

65+50

R	9.2	422.6	
C	7.3	422.0	422.6
L	6.9	422.9	

66+00

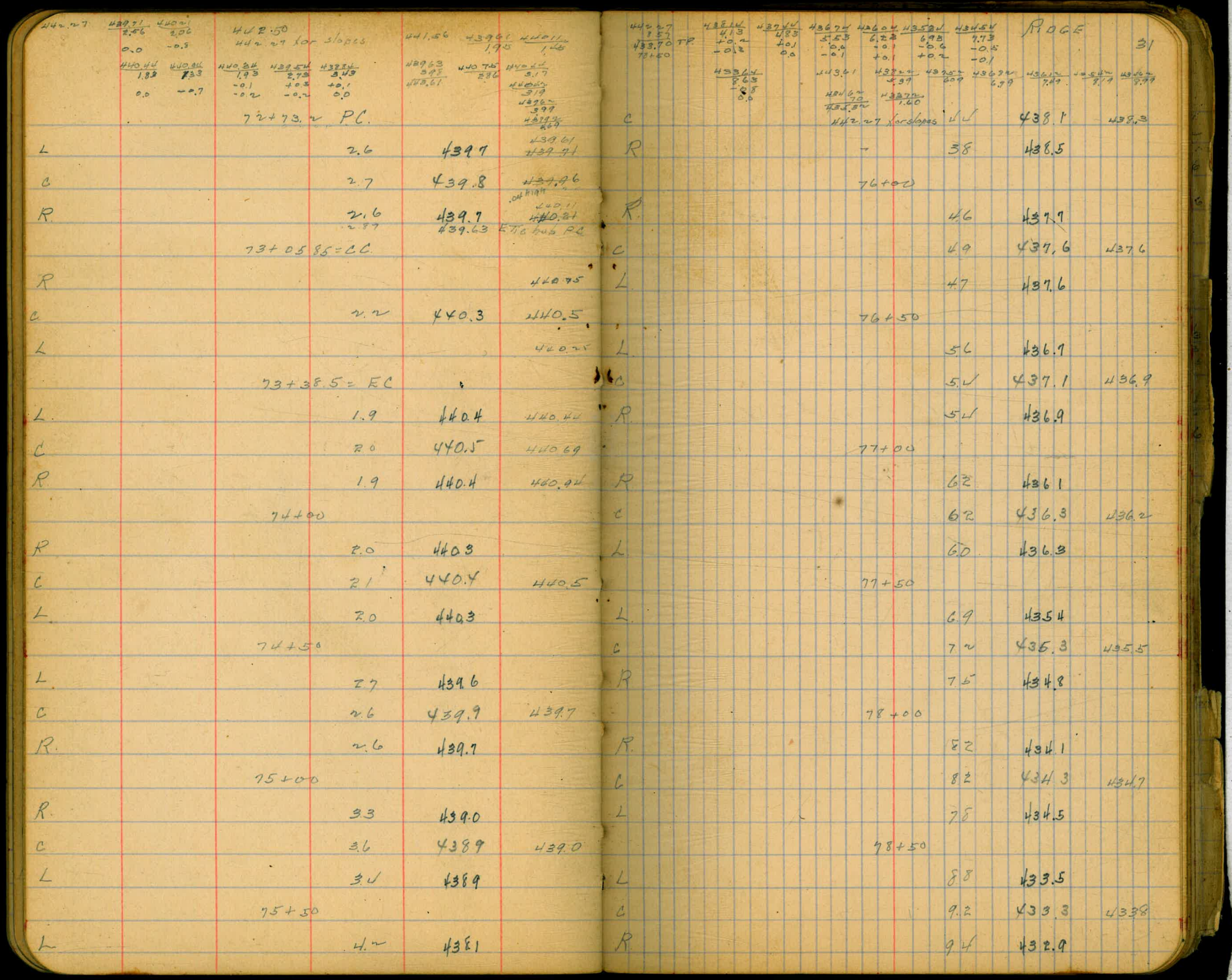
L	6.9	422.9	
C	7.0	422.3	422.7
R	8.1	421.7	

66+50

R	8.3	421.5	

			6.8	422.5	422.8
T.P.	12.49	435.81	5.96	423.32	
		429.78 for slope	6.6		
L		67+00 = Edge of brush			
L			6.4	429.4	
C			13.2	422.6	422.9
R			7.8	422.0	
		67+50			
R			6.8	423.0	
C			12.8	423.0	423.0
L			6.1	423.7	
		68+00			
L			5.5	424.3	
C			11.7	424.1	424.1 424.3
R			6.5	423.3	
		68+50			
R			4.3	425.5	
C			10.4	425.4	425.2 425.6
L			4.2	425.6	
		69+00			
L			2.8	427.0	
C			8.9	426.9	426.8 426.9
R			2.9	426.9	
		69+50			
R			1.3	428.5	
C			7.3	428.5	428.6 428.7
L			1.1	428.7	

					RIDGE 30
L			12.0	430.3	
C			5.5	430.3	430.4 430.5
R			12.0	430.3	
		70+50			
R			10.3	432.0	
C			3.8	432.0	432.2 432.3
L			10.4	431.9	
		71+00			
L			8.5	433.8	
C			2.0	433.6	433.7 433.9
R			8.5	433.8	
T.P.	6.71	442.50 442.27 for slopes	0.02		435.79
		71+50			
R			6.7	435.6	
C			6.8	435.7	435.5 435.9
L			6.7	435.6	
		72+00			
L			4.8	437.5	
C			4.8	437.7	437.6 437.7
R			4.7	437.6	
		72+50			
R			2.8	439.5	
C			3.2	439.3	439.4 439.5
L			2.0	439.3	



442.27 439.71 2.56 0.0 440.2 2.06 -0.5 440.44 1.83 0.0 440.84 1.33 -0.7

442.50 442.27 for slopes 440.34 1.93 -0.1 -0.2 439.54 2.73 +0.3 -0.2 438.24 3.43 +0.1 0.0

72+73.2 P.C.

L		2.6	439.7	439.71
C		2.7	439.8	439.96
R		2.6 2.97	439.7 439.63	440.11 440.21

441.56 439.96 1.95 439.63 393 438.61 440.75 396 440.11 1.45 440.45 3.17 440.45 319 439.61 397 439.71 439.61

ETC hub PC

73+05.85 = CC.

R			440.75
C	2.2	440.3	440.5
L			440.25

73+38.5 = EC

L	1.9	440.4	440.44
C	2.0	440.5	440.69
R	1.9	440.4	440.94

74+00

R	2.0	440.3	
C	2.1	440.4	440.5
L	2.0	440.3	

74+50

L	2.7	439.6	
C	2.6	439.9	439.7
R	2.6	439.7	

75+00

R	3.3	439.0	
C	3.6	439.9	439.0
L	3.2	439	

75+50

L	4.2	438.1	

442.27 1.57 433.70 TR. 78+50 438.44 4.13 +0.2 -0.2 438.44 5.63 -5.8 0.0 437.44 4.83 +0.1 0.0 436.74 3.53 -0.0 -0.1 436.04 6.24 +0.1 +0.1 435.34 6.98 -0.4 +0.2 434.64 9.73 -0.5 -0.1

443.41 437.27 4.39 436.07 6.79 435.37 9.49 434.67 9.79 433.97 9.99 433.27 10.29 432.57 10.59 431.87 10.89

434.67 70 433.97 1.60 434.52 for slopes

ROCE 31

C	44	438.1	438.3
R	38	438.5	

76+02

R	46	437.7	
C	49	437.6	437.6
L	47	437.6	

76+50

L	56	436.7	
C	57	437.1	436.9
R	57	436.9	

77+00

R	62	436.1	
C	62	436.3	436.2
L	60	436.3	

77+50

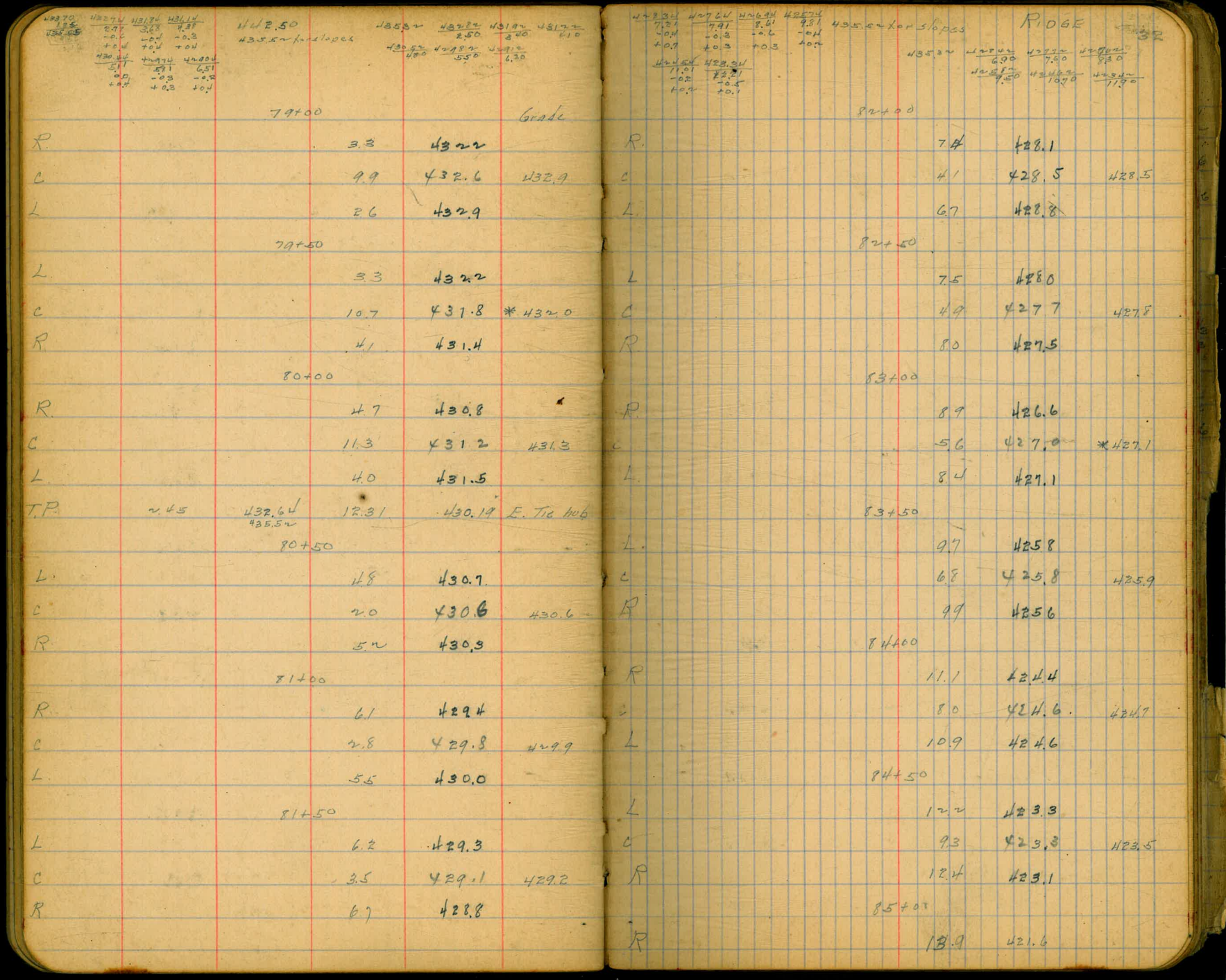
L	69	435.4	
C	72	435.3	435.5
R	75	434.8	

78+00

R	82	434.1	
C	82	434.3	434.7
L	78	434.5	

78+50

L	88	433.5	
C	92	433.3	433.8
R	94	432.9	



			79+00		Grade
R.			3.3	432.2	
C			9.9	432.6	432.9
L			2.6	432.9	
			79+50		
L			3.3	432.2	
C			10.7	431.8	* 432.0
R			4.1	431.4	
			80+00		
R.			4.7	430.8	
C			11.3	431.2	431.3
L			4.0	431.5	
T.P.	2.45	432.6 ℄ 435.5 ≈	12.31	430.19	E. Tie Inv.
			80+50		
L.			4.8	430.7	
C			2.0	430.6	430.6
R			5.2	430.3	
			81+00		
R.			6.1	429.4	
C			2.8	429.8	429.9
L			5.5	430.0	
			81+50		
L			6.2	429.3	
C			3.5	429.1	429.2
R			6.7	428.8	

			82+00		
R.			7.4	428.1	
C			4.1	428.5	428.5
L.			6.7	428.8	
			82+50		
L			7.5	428.0	
C			4.9	427.7	427.8
R.			8.0	427.5	
			83+00		
R.			8.9	426.6	
C			5.6	427.0	* 427.1
L.			8.4	427.1	
			83+50		
L.			9.7	425.8	
C			6.8	425.8	425.9
R			9.9	425.6	
			84+00		
R			11.1	424.4	
C			8.0	424.6	424.7
L			10.9	424.6	
			84+50		
L			12.2	423.3	
C			9.3	423.3	423.5
R			12.4	423.1	
			85+00		
R			13.9	421.6	

C			10.9	421.7	421.75
L			4.2	421.9	
C T.P.	5.01	426.51	11.14	421.50	E Tichnor
		426.10 for slopes			
L		85+50			
L			6.2	419.9	
C			6.6	419.9	420
R			6.3	419.8	
		86+00			
R			8.1	418.0	
C			8.3	418.2	418.25
L			7.9	418.2	
		86+50			
L			9.7	416.4	
C			10.0	416.5	*416.5
R			9.7	416.4	
		87+00			
R			11.4	414.7	
C			11.6	414.9	*415.5
L			11.1	415.0	
		87+50	culvert needed.		
L			12.2	413.9	
C			12.9	413.6	*415.0
R			12.6	413.5	
		88+00			
R			12.7	413.4	
C			12.9	413.6	*415.0

		426.10 for slopes			
L		88+50			
L			10.0	416.1	
C			11.0	415.5	*415.5
R			11.3	414.8	
		89+00			
R			9.8	416.3	
C			9.7	416.8	417.0
L			8.7	417.4	
		89+50			
L			7.0	419.1	
C			8.2	418.3	418.5
R			8.5	417.6	
		90+00			
R			7.3	418.8	
C			6.5	420.3	*420
L			5.6	420.5	
		90+50			
L			4.3	421.8	
C			5.5	421.0	421
R			6.1	420.0	
		91+00			
R			4.8	421.3	
C			4.4	421.1	422.0
L			3.1	423.0	

426.10 426.24 426.36 426.48 426.60 426.51
426.10 for slopes

427.10 427.22 427.34 427.46 427.58 427.70

451.29 451.41 451.53 451.65 451.77 451.89
-5.84 -5.72 -5.60 -5.48 -5.36 -5.24
427.13 427.25 427.37 427.49 427.61 427.73

423.24 423.36 423.48 423.60 423.72
-2.76 -2.64 -2.52 -2.40 -2.28
-1.3 -1.0 -0.8
+0.6 +0.6 +0.4

421.74 421.86 421.98
-1.0 -0.8
+0.6 +0.4

420.14
?

427.09 427.21 427.33 427.45 427.57
4.12 3.97 3.97 3.82 3.82

427.18 427.30 427.42 427.54
5.22 5.07 5.07 4.92

420.22 420.34 420.46 420.58
6.82 6.67 6.67 6.52

Grades

		91+50		
L.	2.2	423.9		
C	3.2	423.3	*423.3	
R	3.5	422.6		
		92+00		
R	3.1	423.0		
C	2.5 (3.91)	424.0 (422.60 ℄ tie hub)	*424.4	423.8
L	1.5	424.6		
		92+50		
L	1.6	424.5		
C	2.6	423.9	*424.0	423.75 425.7
R	3.0	423.1		
		93+00		
R	3.7	422.4		
C	3.3	423.2	*423.0	
L	2.4	423.1		
		93+50		
L	3.9	422.2		
C	4.7	421.8	421.9	
R	4.9	421.2		
		94+00		
		427.13 for slopes		
R	7.6	419.5		
C	6.4	420.1	420.3	
L	6.8	420.3		
		94+50		
L	8.2			

418.54 418.66 418.78 418.90 419.02 419.14 419.26
3.59 10.2 10.7 11.2 11.3 10.3 9.3
-0.6 +0.4 -1.2 -1.4 -1.4 -1.1 -0.8
+0.3 +0.5 -0.1 -0.6 -0.3 0.0 +0.4
427.0 418.62 417.92 416.47 415.92 416.22 417.72
8.42 11.20 10.27 11.12 10.14 9.1

427.13 for slopes

C	7.9	418.6	418.7	
R	9.0	418.1		
	95+00			
R	10.6	416.5		
C	9.6	416.9	*417.1	
L	9.9	417.2		
	95+50			
L	11.0	416.1		
C	10.5	416.0	416.55	
R	11.7	415.4		
T.P.	11.35	428.36	9.50	417.01
	427.12 for slopes			
	96+00	50' ditch here will take a culvert		
R	12.5	414.6		
C	13.3	415.1	*416.0	
L	11.8	415.3		
	96+50			
L	11.7	415.4		
C	13.2	415.2	*416.0	
R	12.6	414.6		
	97+00			
R	11.3	415.8		
C	12.0	416.4	417.0	
L	10.6	416.6		
	97+50			
L	9.0	418.1		
C	10.6	417.8	*418.0	

			98+00			
R				8.3	419.1	
C				9.0	419.4	419.8
L				7.2	419.9	
			98+50			
L				5.6	421.5	
C				7.1	421.3	421.6
R				6.3	420.8	
			99+00			
R				4.2	422.9	
C				5.4	423.0	423.4
L				3.7	423.4	
			99+50			
L				1.8	425.3	
C				3.2	425.2	425.2
R				2.4	424.7	
			100+00			
R				0.4	426.7	
C				1.2	427.2	427.0
L					427.5	
T.P.	834	436.49		0.21	428.15	
		436.23				
			100+50			
L				1.4	428.9	
C				1.5	429.0	428.8

428.36
427.13 for slopes

			101+00			
R				5.8		
C				5.8	430.7	430.6
L				5.6		
			101+50			
L				4.1		
C				4.2	432.3	*432.5
R				4.2		
			102+00			
R				2.9		
C				3.1	433.4	*433.5
L				3.1		
			102+50			
L				3.2		
C				2.9	433.6	*433.25
R				2.6		
			103+00			
R				3.3		
C				3.7	432.8	432.3 *432.5
L				3.8		
			103+50			
L				5.6		
C				5.4	431.1	430.5
R				4.6		

RIDGE

35

RIDGE 36

436.49
436.25 for slopes

		104+00			
R			6.5		
C			7.1	429.4	428.5
L			7.4		
		104+50			
L			9.6		
C			9.2	427.3	426.5
R			8.8		
		105+00			
R			10.9		
C			11.6	426.9	424.5
L			11.9		
TP	0.48	424.96	12.01	424.48	
		424.78 slopes			
		105+50			
L			2.9		
C			2.5	422.6	422.5
R			1.7		
		106+00			
R			4.1		
C			4.8	420.2	420.5
L			5.5		
		106+50			
L			7.8		
C			7.1	417.9	418.5
R			6.4		

		107+00			
R			8.7		
C			9.8	415.2	416.5
L			10.6		
		107+50			
L			12.9		
C			12.1	412.9	414.5
R			11.1		
TP	0.76	413.16	12.56		412.40
		108+00			
R			13.3		
C			2.5	410.7	412.5
L				409.7	
		411.86 for slopes			
		108+50			
L			4.4		
C			3.9	409.3	410.5
R			2.9		
		109+00			
R			3.5		
C			4.6	408.6	409.5
L			4.9		
		109+50			
L			5.3		
C			4.9	408.3	409.1
R			4.0		

4/12/86 — 413.16 — 412.86 slopes

		110+00	
R		4.5	
C		5.1	408.1 — 408.7
L		5.4	
		110+50	
L		5.4	
C		5.1	408.1 — 408.3
R		4.6	
		111+00	
R		4.5	
		5.1	408.1 — 407.8
C		~~5.0~~	
L		00	
		111+50	
L		5.1	
C		5.0	408.2 — 407.4
R		4.5	
		112+00	
R		4.7	
C	3.90	5.25	407.91 — 407.0 on hub
	411.81 412.86	4.58	407.23 Tie hub W.
L		5.4	
		112+50	
L		6.2	
C		4.8	407.0 — 406.0
R		5.7	

4/12/86 — 4/12/86 slopes — P.106E — 37

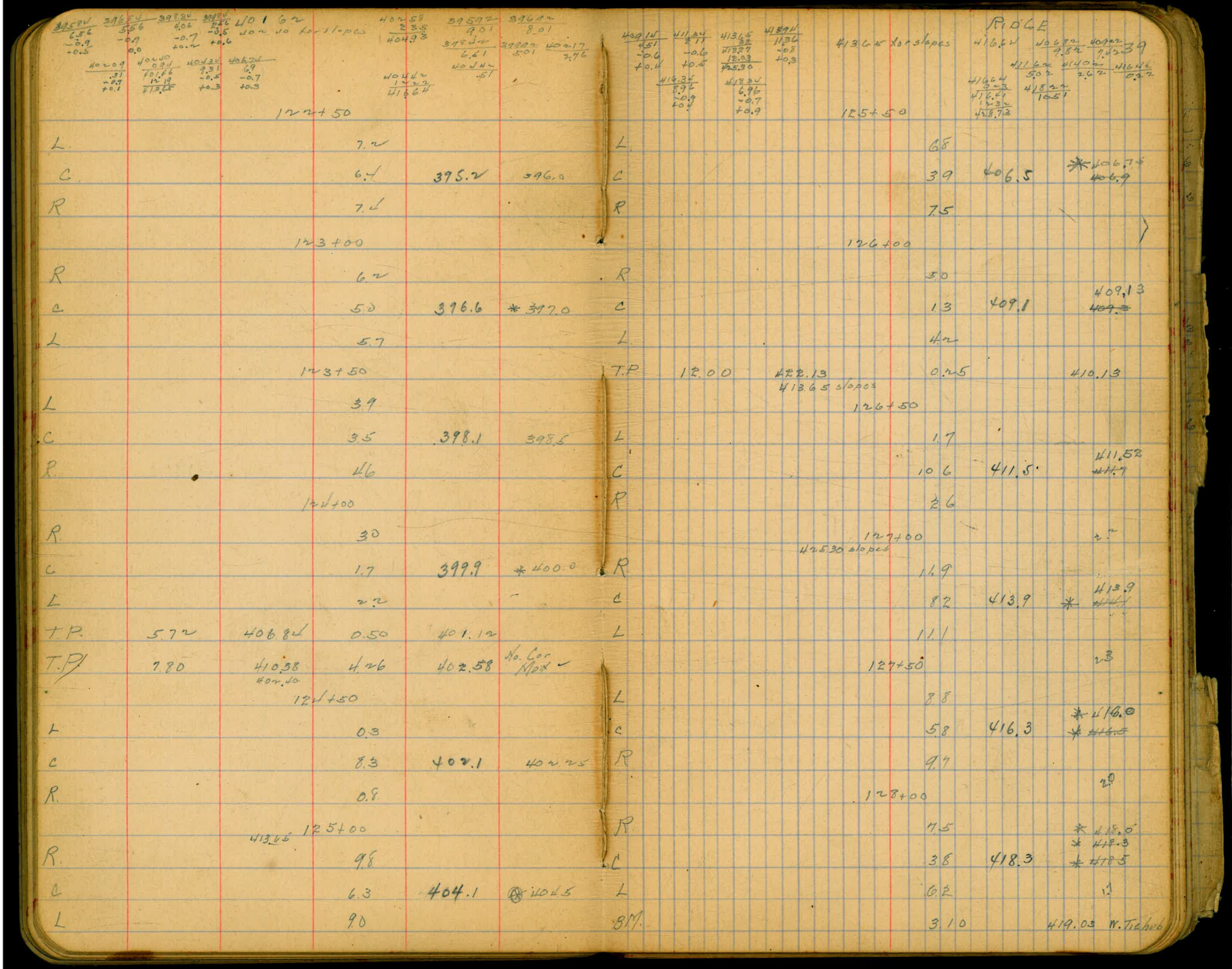
		113+00	
R		7.1	
C		6.3	405.5 — 405.0
L		7.8	
		113+50	
L		9.5	
C		7.8	404.0 — 404.0
R		8.7	
		114+00	
R		9.8	
C		9.2	402.6 — 403.0
L		10.9	
		114+50	
L		12.3	
C		10.3	401.5 — 402.0
R		10.8	
		115+00	
R		11.6	
C		11.2	400.6 — 401.0
L		13.1	
		115+50	
		402.2 Joyce 47.20	
L		3.1	
C		11.7	400.1 — 400.5
R		1.9	
		116+00	
R		E.S	

C	12.3	399.8	400.0
L	3.6		
	116+50		
L	3.9		
C	12.8	399.0	399.5
R	3.2		
	117+00		
R	3.4		
C	13.1	398.7	399.0
L	4.1		
	117+50		
L	4.2		
C	13.0	398.8	398.5
R	3.6		
	118+00		
R	3.8		
C	13.3	398.5	398.0
L	4.3		
T.P.	2.88	401.62	13.07	398.74
	Hor. to slopes		
	118+50		
L	4.9		
C	3.8	398.8	397.5
R	4.5		
	119+00		
R	5.2		
C	4.6	398.0	397.0

L	5.7		
	119+50		
L	6.4		
C	5.2	396.4	396.5
R	5.9		
	120+00		
R	6.4		
C	5.8	395.8	396.0
L	6.9		
	120+50		
L	7.5		
C	6.6	395.0	395.9
R	7.4		
	121+00		
R	7.9		
C	7.1	394.5	395.8
L	8.0		
	121+50	culvert needed	
L	8.2	393.1	
C	7.3	394.3	395.7
R	8.1	393.5	
	122+00		
R	8.0		
C	7.1	394.5	395.85
L	7.9		

RIDGE

38



H25.80

H19.84 −1.2 +1.0 | H21.34 3.96 −1.1 +1.0 | H22.34 3.46 −1.1 +1.2 | H22.13 H25.30 slope

H24.34 3.96 −1.1 +0.6 | H25.30 0.81 H26.99 3.20 H30.19 | H25.19 7.7 −1.0 +0.7 | H26.04 6.85 −1.1 +0.7

128+50

L		4.8		
C		2.2	419.9	* H19.9 H20.0
R		6.2		

129+00

R		4.9		
C		0.9	421.2	H21.2 H21.5
L		3.2		
T.P.	108.2	H32.91 H25.30	0.41	H21.72

129+50

L		1.5		
C		9.6	422.9	* H22.9 H23.0
R		3.4		

130+00

R		2.1		* H24.0 H24.3
C		8.5	424.0	* H24.5
L		0.6		

130+50
H32.89 for slopes

L		7.3		
C		7.2	425.3	H25.05 H25.35
R		8.6		

131+00

R		7.7		
C		6.4	426.1	H26.10
L		6.3		

H25.78

H19.92 8.81 H21.42 7.31 | H22.92 5.91 H24.20 4.81 | H25.27 5.46 H26.12 2.61

H26.89 6.82 −0.8 +0.6 | H27.74 5.15 −0.4 +0.3 | H28.58 4.3 −0.5 +0.1 | H29.44 3.45 −0.5 5.0 | H30.20 2.59 −0.3 −0.1 | H30.44 1.46 −0.1 −0.1

H29.21 H29.97

43.89 slopes

131+50

L		5.5		
C		5.7	426.8	* H27.0.5
R		6.7		

132+00

R		5.4		
C		4.7	427.8	H27.9
L		4.9		

132+50

L		4.3		
C		4.0	428.5	H28.75
R		4.8		

133+00

R		3.9		
C		3.2	429.3	* H29.6
L		3.6		

133+50

L		2.6		
C		2.3	430.2	* H30.20
R		2.5		

134+00

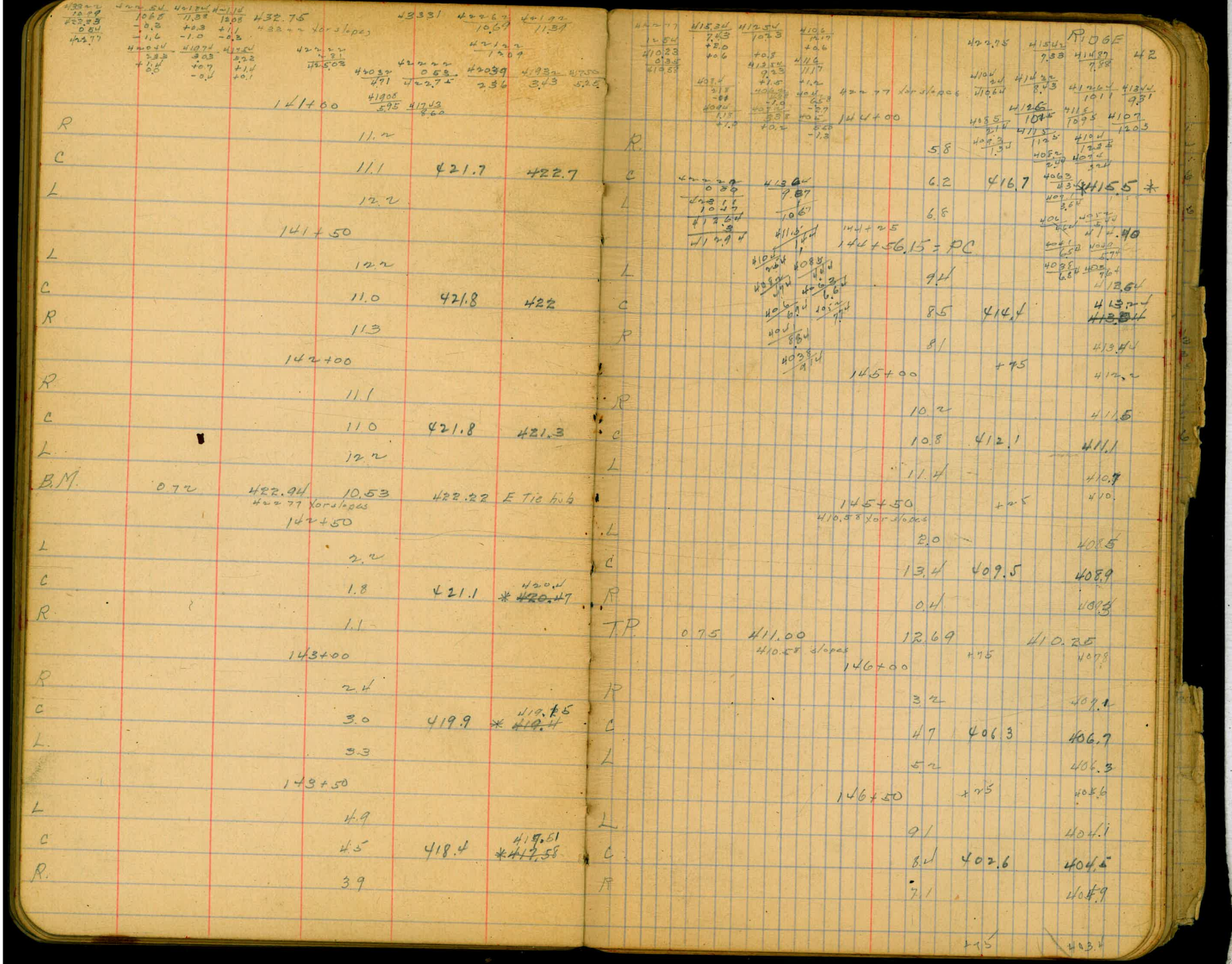
R		2.5		
C		2.0	430.5	* H30.4
L		2.4		
B.M.	2.78	432.75	2.57	H29.97 √E tie

H25.73 | H26.97 1.76 | H27.82 0.91 | 40

H27.82 6.54 H34.36 | H28.67 5.69 | H29.57 4.84 | H30.12 H29.46 | H30.54 3.84

		134+50		
L			2.7	
C			2.2	430.6
R			2.9	
		135+00		
R			2.6	
C			2.1	430.7
L			2.9	
		135+50		
L			3.3	
C			2.3	430.8
R			2.5	
		136+00		
R			2.9	
C			2.7	430.1
L			3.8	
		136+50		
L			4.5	
C			3.4	429.4
R			3.6	
		137+00		
R			3.6	
C			3.8	429.0
L			5.0	
		137+50		
L			5.4	

C		4.5	428.3	427.6
R		4.3		
	138+00			
R		5.2		
C		5.3	427.5	426.9
L		6.3		
	138+50			
L		7.1		
C		5.9	426.9	426.2
R		6.0		
	139+00			
R		7.2		
C		7.3	425.5	425.5
L		8.3		
	139+50			
L		9.8		
C		8.5	424.3	424.8
R		8.5		
	140+00			
R		9.5		
C		9.5	423.3	424.1
L		10.6		
	140+50			
L		11.9		
C		10.6	422.2	423.4
R		10.5		



			147+00		
R	403.6	400.0	10.0		402.9
C	394.20		11.1	399.9	402.3
L			11.6		401.9
			147+19.69 = EC		
L			12.5		401.0
C			12.2	398.8	401.4
R			11.0		401.8
B.M.			9.85	401.15	E Tie Hub
			147+50		
R			12.4		
C			13.4	397.6	400.1
L			13.7		
T.P.	0.37	398.35	13.02	397.98	
		~398.0m slopes			
			148+00		
L			3.3		
C			3.0	395.4	*397.9
R			2.2		
			148+50		
R			3.2		
C			4.0	394.4	*396.0 ~~395.7~~
L			4.3		
			149+00		
L			5.3		394.28
C			5.0	393.4	~~398.5~~
R			4.1		1.31

			149+50		
R	403.6	402.6	9.2		402.4
C	392.45	390.4	11.6	392.4	402.0
L			12.3		401.3
			150+00		
L			7.1		
C			6.8	391.6	390.84 ~~391.5~~
R			6.2		
			150+50		
R			7.4		
C			8.1	390.3	389.12 ~~390.6~~
L			8.4		
			151+00		
L			10.5		
C			10.0	388.4	387.4 ~~388.4~~
R			9.2		
			151+50		
R			10.8		
C			11.7	386.7	385.68 ~~386.3~~
L			12.5		
			152+00		
			~396.1m slopes		
L			2.8		
C			13.6	384.8	83.96 ~~384.2~~
			0.6		
B.M.			12.13		386.22 E. Tie
T.P.	0.18	386.26	12.27		386.08

386.26

152+50

R		3.4		
C		4.4	381.9	382.24 ~~381.1~~
L		5.5		

153+00

L		8.6		
C		7.2	379.1	380.52 ~~380.0~~
R		6.2		

153+50

R		8.7		* 378.83
C		9.5	376.8	* ~~377.9~~
L		10.4		

154+00

L		11.8		* 377.20
C		11.2	375.1	~~375.8~~
R		10.8		

154+50

R		11.2		375.62 ~~376.3~~
C		12.6	373.7	* ~~374.~~
L		3.0		

375.41 3 laps

TP	0.96	374.99 375.41	12.23	374.03

155+00

L		4.1		374.10 ~~374.3~~
C		2.3	372.7	373.0
R		2.6		

R1065 44

155+50

R		3.3		
C		3.1	371.9	~~372.6~~ ~~372.16~~
L		5.2		

156+00

L		6.0		371.12 ~~370.75~~
C		4.0	371.0	~~371.~~
R		3.9		

156+50

R		5.0		~~369.63~~ ~~369.71~~
C		5.0	370.0	~~370.~~
L		7.6		

157+00

L		8.7		~~368.14~~ ~~369.5~~
C		6.3	368.7	~~369.~~
R		6.5		

157+50

R		7.7		~~366.65~~ * ~~367.31~~
C		7.5	367.5	~~368.0~~
L		9.5		

+75 ~~367.5~~

158+00

L		9.7		~~365.16~~ * ~~366.0~~
C		8.4	366.6	~~366.6~~
R		8.8		

158+50

R		9.4		* ~~363.69~~ ~~364.4~~ ~~364.5~~
C		9.0	366.0	~~363.5~~
L		10.8		

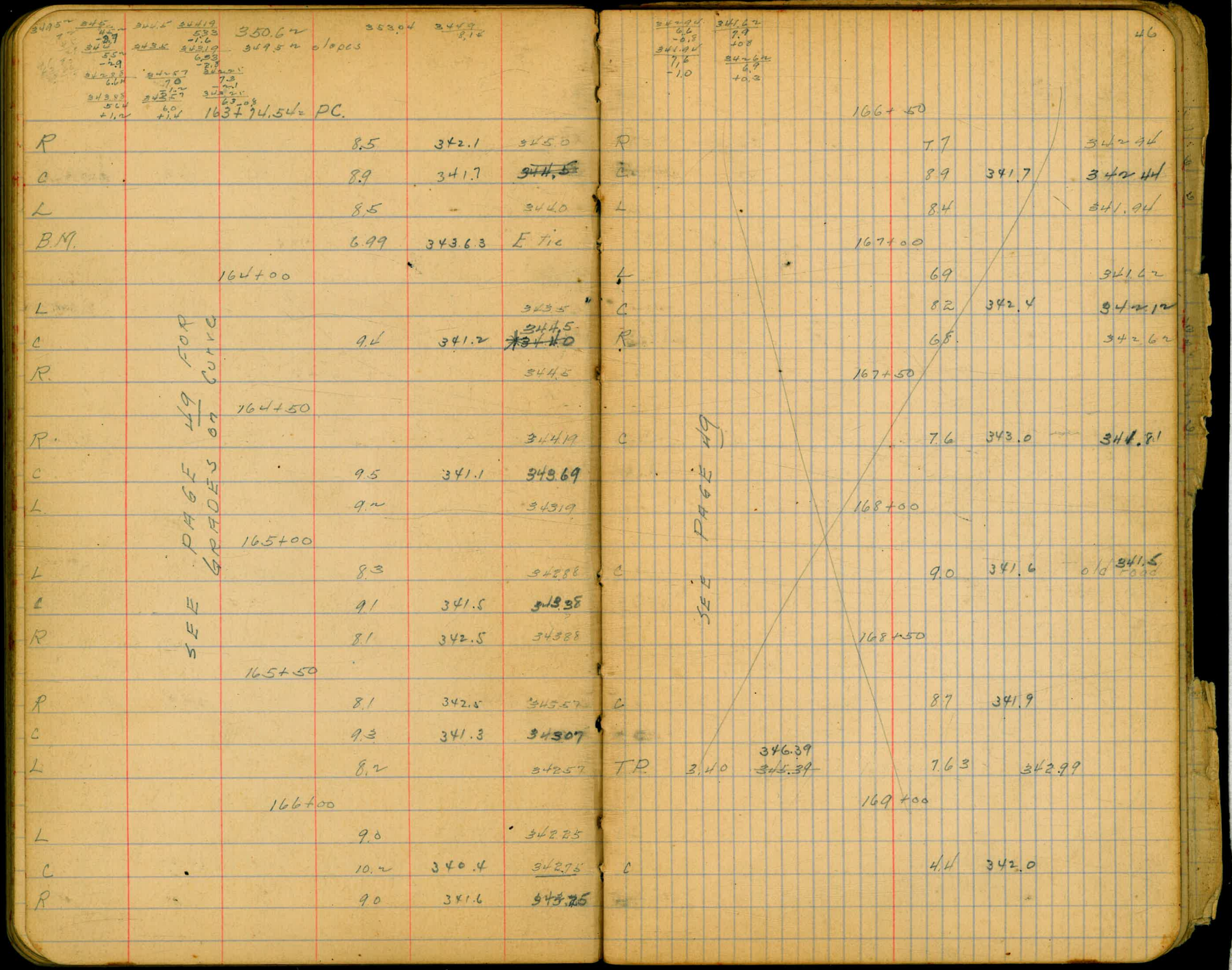
			159+00		
L			12.1		362.1 / 362.1
C			10.3	364.7	~~362.5~~ 361.6
R			10.4		
B.M.			9.08	365.91	E Tie hob
T.P. CAT	0.81	363.28 364.11	12.52 5.87	362.47 357.41 = 357.44 book roll 37A 111+81	
			159+50 (Hardpan from here to end)		
R			3.5		
C			2.9	360.4	360.5 ~~359.6~~
L			5.6		
			160+00		
L			7.4		
C			6.0	356.3	358.5 ~~357.6~~
R			6.4		
OK			160+50		
L			9.0		
C			7.4	355.9	356.5 ~~355.5~~
R			7.1	356.2	
			161+00		
R			8.7	354.6	
C			9.1	354.2	354.5 ~~353.6~~
L			10.7		
			161+50		
L			12.3		
C			10.4	352.9	352.5 ~~351.5~~
R			9.9	353.4	

P 062

45

354.90 for slopes

			162+00		
R			11.5	351.8	+1.6 * ~~349.5~~ 350.5
C			12.2	351.1	
L			4.8		
T.P.	0.16	350.62	12.82	350.46	
		354.90 slopes			
			162+20		
L			-		
C			1.6	349.0	
R			+ 0.7	351.3	
			162+50 = ctr of traveled road		
R			7.5		-1.2
C			3.2	347.4	* 349.15
L			3.2	347.4	
			163+00		
L			11.1		
C			6.5	344.1	348.0
R			9.8		346.0
			163+30		
R					
C			8.4	342.2	
L					
			163+50		
L					
C			8.4	342.2	347.13
R					



350.6 ± 349.5 ± slopes

1637 + 14.54 = PC.

R		8.5	342.1	345.0
C		8.9	341.7	~~344.5~~
L		8.5	-	344.0
B.M.		6.99	343.6.3	E Tic
	164+00			
L				343.5
C		9.4	341.2	344.5 ~~344.0~~
R				344.5
	164+50			
R				344.19
C		9.5	341.1	349.69
L		9.2		343.19
	165+00			
L		8.3		343.86
C		9.1	341.5	343.38
R		8.1	342.5	343.88
	165+50			
R		8.1	342.5	345.57
C		9.3	341.3	343.07
L		8.2		342.57
	166+00			
L		9.0		342.25
C		10.2	340.4	342.75
R		9.0	341.6	~~343.25~~

SEE PAGE 49 FOR GRADES OF CURVE

	166+50			
R		7.7		342.46
C		8.9	341.7	342.44
L		8.4		341.94
	167+00			
L		6.9		341.62
C		8.2	342.4	342.12
R		6.8		342.62
	167+50			
C		7.6	343.0	344.81
	168+00			
C		9.0	341.6	old 341.5
	168+50			
C		8.7	341.9	
T.P.	3.40	346.39 ~~345.39~~	7.63	342.99
	169+00			
C		4.4	342.0	

SEE PAGE 49

46

346.39 169+50

C 4.2 342.2

169+80.17 = EC

C 4.0 342.4

169+92.27 = 121+32.64 book 1010-7

C 3.7 342.7

B.M. 3.88 342.51 1st tie

173+81.34 EC = 125+23.35

~~173+81.04 = 125+18.50~~ EC. Book 1010 Page 8

~~173+83.44~~ Δ ~~28°53'20"~~ 28°47'30" R. ~~R=190.~~ R=190. ~~st=44.77~~ st=48.77 ~~lc=47.42~~ lc=95.48

172+85.86

~~173+83.69~~ P.C.

Davis's EC.

169+58.11 EC

R = 1000'

166+71.81 Δ 33°39'30" L st=304.06

lc=590.36

163+67.75 P.C.

EC.

169+00 P.O.T.

1st dev. = d from PC = 0°55'26"

2nd " = 21

3 47

5 13

6 39

8 05

9 31

10 57

12 23

13 49

15 15

16 41

16 54 45

d at EC. = 3°35'56"

d = ~~2211~~ or L

25.11 on L

~~27.60~~ on R

60.86 26.73

63.34 approx 39.51

45.83

dev from EC. to 169+25 = 56' 54" || 37.79 for 1161.66

" " " to 169 = 1339.52 24.75

" " " to 168+75 = 40.60

50' 30'

168+50	74.05	3°05'48"
168+25	98.96	3°48'46"
168+00	123.84	
167+75	148.44	
167+50	172.80	
167+25	196.86	
167	220.56	
166+75	243.84	
+50	266.64	
+46	270.37	
166	289.15	
+75	310.58	
+50	331.41	
+25	351.62	
165	371.20	
+75	390.07	
+50	408.30	
+25	425.80	
164	442.54	
163+67.75	459.54	

40 28 46'

		163	1627+67.75 PC.		
	R		-3.2	6.2	42.3
	C			6.5	
	L		346.31	7.1	41.7
			-3.5		
	L			7.6	41.2
			164		
	L		-3.2		
			345.35	8.0	40.8
	C		G = 345.75	7.5	41.2
	R		-3.8	7.1	
				7.3	41.5
			343.31		
			1644+50		
	R		-2.0	6.1	
				7.0	41.8
	C		344.89	7.7	41.1
	L		-3.4		
				8.4	40.4
			44.44		
		165			
	L		-2.2		
			343.6	7.5	41.3
	C		* 344.0		
	R		+0.5	3.9	
			344.4	4.7	41.1
			1654+50		
	R		+0.8	3.9	
			344.15	5.0	41.8
	C		343.75		
	L		-2.0		
			343.35	7.5	41.3
			343.6		
		166+00			
	L		- 2.8	8.6	
			343.1	8.6	40.2
	C		343.5		
	R		-1.9		
			343.9	6.5	41.3
			1664+50		
	R		Grade = 343.65	6.7	
				7.0	41.8

	C				343.25
					-1.8
	L		7.8	41.0	342.35
					41.2
		167			
	L		6.7		F 0.4
			6.2	42.6	342.6
	C		6.2	42.6	343.0
	R		5.7		F 0.4
			6.0	42.8	343.4
					42.8
		1674+50			
	R		5.4		+0.1
			5.6	43.2	343.15
	C		6.1	42.7	342.75
	L		6.5		0.0
			6.6	42.2	342.35
					42.6
		168			
	L		6.6		F 0.2
			6.7	42.1	342.1
	C		6.9	41.9 *	342.5
	R		6.4	42.4	343.9
				✓	42.50
		1684+50			
	R		7.0	41.8	342.9
	O		7.5	41.3 ✓	342.5
	L		7.3		
			7.6	41.2	342.1
		169			
	L		7.7		F 0.6
			7.8	41.0	342.1
	C		7.3	41.5 ✓*	342.5
	R		7.2	41.6	342.90
		1694+58.11 EC.			342.62
	R	For grades from here to paving see page 61	6.9	41.9	343.52
	C		6.9	41.9	342.72
	L		7.7		F 0.6
			7.9	40.9	

48.84

50

BM.			341.11	on 30" fire hub
	170			
		6.1	42.7	343.00
	170+50			
		5.3	43.5	
	171			
		4.6	44.2	
	171+50			
		4.1	44.7	

H 26/8 Gregory Point Miller

LOCATION OF ROAD
from End of Paving at the Top of the Biological Grade to Summit of Ridge Road

dex for 25' ord ℄ = 1°35'30"

EQUATION (page 174)

26 + 30.78

26+30.83 E.C. = 15+10.52 R = 450

24+17.45 PI 60°44' L St 263.67

21+53.78 P.C. Lc = ~~477.13~~ 477.00

15+08.38 E.C. R = 870

11+65.50 PI 48°13½' R St = 389.39

7+76.11 P.C. Lc = 732.27

4+59.56 ℄ 5°40' L

0+00.

From P.C.

1st	1°21'43"
	2°57'13
	4°32'43"
	6°08'13
	7°43'43
	9°19'13
	10°54'43
	12°30'13
	14°05'43
	15°41'13
	17°16'43
	18°52'13
	20°27'43
	22°03'13
	23°38'43
	25°14'13
	26°49'43
	28°25'13
	30°00'43
	30° [illegible]

21+53.78
15+08.38
6 45.40
490.00
1 35.40

53

BM 402.05

25 25

321.57 21 25

[illegible] 5°

1st from P.C. 47' 12" 23.89

49' 23' = L for 25'

90°00'

36 25

BM 396.79

40 50

1st	1°	36' 35"
2	2	25 59
3	3	15 22
4	4	04 46
5	4	54 09
6	5	43 33
7	6	32 57
8	7	22 20
9	8	11 44
9	9	01 07
10	9	50 30
11	10	39 54
12	11	29 17
13	12	18 41
13	13	08 04
14	13	57 28
15	14	46 51
16	15	36 15
17	16	25 38
18	17	15 02
18	18	04 25
19	18	53 49
20	19	43 12
21	20	32 36
22	21	21 59
23	22	11 23
23	23	00 46
24	23	49 10
25	24	38 33

87°
20

32.84 App. 25

End of Present Paving

4/26/18 Gregory/Makoc/Miller — CROSS SECTION OF SURVEY OF ROAD ON PAGE 53 This book. Road is 30' wide

		0+00 = End of paving 17.5 wide			
B.M.	247	384.65		382.18	on tic hub at Sta 4+89
8.75 R.			9.1	375.6	on paving
c			9.5	375.2	~375.2
8.75 L			9.9	374.8	" "
		0+50			
15' L.			9.0	375.7	
14' L			9.2	375.8	c 0.1
13' L			9.7	375.0	375.73
c			9.1	375.6	F 0.6
15' R			9.7	375.0	
		1+00			
15' R			8.8	375.9	F 0.4
c			8.7	376.0	376.26
13' L.			9.1 / 8.2	375.6 / 376.5	c 0.2
15' L.			8.3	376.4	
		1+50			
15' L.			7.5	377.7	
11' L.			7.3	377.4	
9' L.			8.5	376.2	c 0.6
c			8.0	376.7	376.79
11' R			8.4 / 7.2	376.3 / 377.5	c 0.6
15' R.			7.4	377.3	

		2+00		
15' R	6.1	378.6		
12'	6.7 / 7.8	378.0 / 376.9	c 1.4	
C	7.4	377.3	377.52	
8' L	8.0	376.7	F 0.3	
10' L	7.0	377.7		
15' L	7.6	377.1		
		2+50		
15' L	7.6	377.1		
11' L	6.8	377.9		
9' L	7.5	377.2	F 1.0	
C	7.0	377.7	377.55	
11' R	7.4	377.3	c 0.0	
13' R	5.4	379.3		
15' R	5.3	379.4		
		3+00		
15' R	6.4	378.3		
12'	6.9	377.8	c 0.3	
C	6.6	378.1	377.38	
10'	7.0	377.7		
15' L	8.3	376.4	F 0.2	
		3+50		
15' L	6.7	378.0		
9' L	6.0	378.7		
7'	6.5	378.2	F 1.2	
C	6.0	378.7	378.91	

38819
38218 757 389.75
37894 / 4.25
7936 / 383
38042 / 9.33 38072 / 9.01
384.65
386.01
38074 / 5.27 38042 / 5.59 ~~37744~~ / 7.07 380 / 6.01 37486 / 6.65

11R		6.3	378.4	C 0.5
13'		5.5	379.2	
15'R		5.2	379.5	
	4+00			
15'R		3.8	380.9	
10'		5.6	379.1	C 1.5
C		5.4	379.3	379.44
10'L		5.9 4.5	378.8 380.2	C 0.1
15'L		4.7	380.0	
	4+59.56	△		
15'L		5.4	379.3	F 0.4
C'		4.8	379.9	C Elev = .6
9'		53	379.4	380.07
11'		4.2	380.5	C 1.5
15'R		3.9	380.8	
	5+00			
15'R		2.9	381.8	
10'		3.6	381.1	
8		4.7	380.0	C 2.2
C		4.4	380.3	*380.5
12'		5.0	379.7	F 0.2
15'L		4.0	380.7	
	5+50			
15'L		4.5	380.2	F 0.1
C		4.0	380.7	380.82
7'R		4.2	380.5	C 2.6

389.76
38218 / 383 / 386.01
38107 / 768 38139 / 836 38172 / 803 38232 / 7.43 38240 / 7.05
3827 / 3.31 3824 / 3.61 38172 / 4.29 38139 / 4.62 38107 / 4.94

15'R		2.5	382.2	
	6+0			
15'R		3.1	381.6	
6'		3.8	380.9	C 2.0
C		3.7	381.0	381.15
15'L		4.3	380.4	F 0.7
	6+50 = ctr of Road to Torrey			
15'L		3.9	380.8	F 0.9
C		3.5	381.2	381.47
15'R		3.3	381.4	C 1.4
	7+00			
15'R		3.0	381.7	C 1.4
C		3.3	381.4	381.8
15'L		3.6	381.1	F 1.0
	7+50			
15'L		3.2	381.5	F 1.4
C		2.8	381.9	382.2
5'R		2.8	381.9	C 2.6
15'R		0.4	384.3	
	7+76.11 PC.			
15'R		2.3	382.4	C 1.7
C		2.5	382.2	382.7
15'L		2.8	381.9	F 2.3
T.P.	12.43 394.90	2.18	382.47	

			8+00						
15'L				12.5	382.4				
C				12.4	382.5	388.0			
15'R				11.9	383.0	C 2.4			
			8+50						
15'R				10.3	384.6				
6'				10.9	384.0				
5'				11.7	383.2	C 3.4			
C				11.4	383.5	388.6			
15'L				11.6	383.3	F 1.5			
			9+00						
15'L				11.5	383.4				
11'				10.5	384.4	F 2.0			
C				10.7	384.2	384.2			
6'				11.1	383.8	C 2.9			
15'R				9.0	385.9				
			9+50						
15'R				7.8	387.1				
11				7.9	387.0				
7				10.4	384.5	C 2.9			
C				10.4	384.5	384.8			
10'				10.3	384.6	F 2.5			
15'L				11.2	383.7				
			10+0						
15'L				11.4	383.5				
7'				9.7	385.2	C 1.9			

C				9.5	385.4				
8'R				9.8	385.1				
11 R				8.4	386.5				
15'R				8.3	386.6				
			10+50						
15'R				7.3	387.6				
10'				7.8	387.1				
8'				8.7	386.2				
C				8.4	386.5				
8'L				8.6	386.3				
15'L				9.6	385.3				
			11+0						
15'L				6.6	388.3				
11'				6.1	388.8				
C				6.6	388.3				
9'R				7.4	387.5				
11				5.4	389.5				
15'R				4.8	390.1				
			11+50						
15'R				3.3	391.6				
10'				3.9	391.0				
8'				5.7	389.2				
C				5.1	389.8				
11'L				4.9	390.0				
15'L				5.6	389.3				

		12+00		390.65
15'L			4.5	390.4	
9			3.4	391.5	F1.8
0			3.4	391.5	391.4
11'R			3.8	391.1	C1.7
12			2.8	392.1	
15'R			2.5	392.4	
		12+50			392.15
15'R			1.1	393.8	
10'			1.3	393.6	
8'R			2.0	392.9	C1.6
C			1.6	393.3	392.9
15'L			1.7	393.2	F0.6
TP	7.10	401.76	0.24	394.66	
		13+0			93.65
15'L			7.8	394.0	F1.2
C			7.1	394.7	394.4
15'R			7.7	394.1	C1.6
		13+50			394.1
15'R			6.9	394.9	C1.9
C			6.1	395.7	395.45
10'			6.3	395.5	F0.6
15'L			6.3	395.5	
		14+00			15.97
15'L			5.3	396.5	
11'			4.8	397.0	

10'L		5.4	396.4	F0.8
C		5.3	396.5	396.5
15'R		6.1	395.7	C1.6
	14+50			96.77
15'R		5.6	396.3	C2.0
10		4.7	397.1	397.05
7'L		4.7	397.1	F0.8
8'		4.2	397.6	97.2
15'L		4.8	397.0	
	15+08.38 EC		15+00	397.6
15'L		4.4	397.4	
8'		3.8	398.0	
7'		4.7	397.1	F0.9
C		4.6	397.2	397.5
15'R		5.5	396.3	C1.1
	15+50			
15'R		5.8	396.0	
C		5.0	396.8	C1.3
7'L		5.1	396.7	397.12
8'		4.5	397.3	F0.3
15'L		4.9	396.9	
	16+00			
15'L		5.4	396.4	
9'		4.9	396.9	
7'		5.5	396.3	F0.4
C		5.3	396.5	396.67
15'R		6.0	395.8	C1.6

		401.76	401.73		
		16+50			
15'R			6.0	395.8	
14			6.8	395.0	0.0
C			5.8	396.0	
15'L			6.3	395.5	F 0.5
		17+0			
15'L			6.8	395.0	F 0.5
C			6.2	395.6	
15'R			7.0	394.8	C 0.1
		17+50			
15'R			7.2	394.6	C 0.3
C			6.5	395.3	
15'L			7.2	394.6	F 0.5
		18+0			
15'L			7.7	394.1	0.0
C			7.1	394.7	
15'R			8.0	393.8	C 0.2
		18+50			
15'R			8.5	393.3	F 0.1
C			7.5	394.3	
15'L			8.6	393.2	F 0.9
		19+0			
15'L			18.9	392.9	F 0.9
C			7.9	393.9	
15'R			8.9	392.9	0.0

		19+50		
15'R	8.9	392.9		0.0
C	8.1	393.7		
15'L	9.5	392.3		F 1.2
T.P. 4.17	8.13	393.63		
	20+0			
15'L	5.5	392.3		F 0.8
C	4.3	393.5		
15'R	4.9	392.9		C 0.1
	20+50			
15'R	5.0	392.8		C 0.3
C	4.3	393.5		
15'L	5.5	392.3		F 1.2
	21+00			
15'L	5.4	392.4		F 1.1
C	4.3	393.5		
15'R	5.0	392.8		C 0.3
	21+53.70 P.C.			
15'R	5.0	392.8		
C	4.2	393.6		
15'L	5.6	392.2		
	22+0			R F 0.3 39398 L F 1.0
15'L	5.2	392.6		F 1.0 393.1
C	4.1	393.7		
15'R	4.5	393.3		P 1.5 3941
			39387	R F 1.2
			39400	R F 1.1

404.27 398.7 5.57 398.2 6.07 398 5.77 397.80
398.5 5.77 398 6.27
39685 7.42 396 8.17 395.3 8.92
394.6 9.64 394.47 9.80 394.45 9.82 394.0 10.27

22+33 = present pipe culvert to be extended 10' Left. Elev. coping 394.10, which can be the same as grade elev. 12" corrugated

22+50

15' R	403.25	394 9.25	3.6	394.2	F0.5 394.25
C		9535 7.90 94.2 9.05	4.3	393.5	394.35
15' L		96 7.15 9655 6.40	4.8	393.0	F0.7 394.0 R F0.5 394.47 L F0.3
		22+0			
15' L		976 5.66 986 4.63	4.1	393.7	F0.5
C		981 5.15 991 4.13	3.8	394.0	394.6
15' R			3.3	394.5	394.8 F0.2 LF0.2 395.35 R F0.1
		23+50			
15' R			1.9	395.9	F0.4
C			1.9	395.9	396.1
15' L			2.1	395.7	F0.1
		24+0			396.85 R=0.65
15' L			0.7	397.1	397.2
C			0.6	397.2	397.6
15' R			0.6	397.2	F0.2 398.0
T.P.	6.52	404.25	0.07	397.73	R F0.2 398.1 L
		24+50			
15' R			5.6	398.7	F1.0 399.9
C			5.9	398.4	398.6
15' L			5.9	398.4	C D.1 398.2

L 398.7

401.4 11.70 404.27 401.4 2.87 400.2 3.47 400.2 3.97 397.75 4.52 398.2 6.07

99+ 404.5 399.15 3.60 400.3 2.47 401.4 1.85 400.55 2.40

25+00

15' L	4.2	400.1	399.2 F0.1
C	4.8	399.5	399.6
15' R	4.8	399.5	399.6 L C 0.2 399.75
25+50			
15' R	3.9	400.4	
C	3.9	400.4	
15' L	3.7	400.6	F0.1 400.2 L C 0.3 400.25
26+0			
15' L	3.2	401.1	401.4 F2.6
C	2.7	401.6	401.6
15' R	2.9	401.4	

EQUATION 26+30.83 E.C. = 15+10.52 on T

15' R	2.5	401.8	
C	2.5	401.8	
15' L	3.2	401.1	
T.P.	3.85	400.40	

1 NT ox Pairings Westenbourne = 94.6 — high side curve No side Tu

14' East 94.80

94.7 = 1176 Eof PC on So side

94.52 = 909 " " " "

94.80 1343 " " " "

95.6 1843 " " both sides

96.4 2343 " " " "

0+00 end of Biological pavement

4+59.56. Δ = 5°40' L

7+76.11 PC R=870. Δ=48°13'30" R T=389.39

5+08.38 EC

+53.70 PC R=450. Δ=60°45' L T=263.75

+30.83 EC = 15+10.52 EQUATION

3+50 Δ = 3°27' L

72+73.52 PC R=500. Δ=7°29' L T=32.70

73+38.5 EC

44+56.15 PC R=600 Δ=25°10' L T=133.93

47+19.69 EC

63+74.54 PC R=1000 Δ=34°42'2" L T=312.42

79+80.17 EC.

89+92.27 = 121+32.64 EQUATION

+25.30 PC R=180. Δ=29°40' R T=47.67

+18.50 EC

+77.60 PC R=500 Δ=47°37' L T=220.61

8+93.13 EC

9+21.73 PC R=170 Δ=32°26' R T=49.44

0+17.96 EC

40+56.58 end of Tommy Pinno pavement

Changed see opp. page

P.I. 3 R.1034

P.I. 13 R.1034

P.I. 17 R.1034

P.I. 7 R.1010

140+56.58
121+32.64
19+23.94
154+81.75
26+30.83
200+36.52 = length of line
Changed. see below

169+92.27
15+10.52
154+81.75

163+67.75 PC R=1000' Δ=33°49'30" T=304.06

169+58.11 EC

172+85.86 PC R=190 Δ=28°47'30" T=48.77

173+81.34 EC =

125+23.35 POT EQUATION

140+56.58
125+23.35
153328
15870.82
2630.83
20034.88 = length of line

173+81.34
15+10.52
158 7082

0+00 End of Biological pavement.

4+59.56. Δ = 5°40' L

7+76.11 PC

R=870. Δ=48°13'30" R T=389.39

5+08.38 EC

2+53.70 PC

R=450. Δ=60°45' L T=263.75

2+30.83 EC = 15+10.52 EQUATION

13+50 Δ= 3°27' L

12+73.2 PC

13+38.5 EC R=500. Δ=7°29' L T=32.70

44+56.15 PC

47+19.69 EC R=600 Δ=25°10' L T=133.93

43+74.54 PC

49+80.17 E.C. R=1000 Δ=34°42' L T=312.42

49+92.27 = 121+32.64 EQUATION

2+25.30 PC

18+50 EC R=180. Δ=29°40' R. T=47.67

4+77.60 PC

8+93.13 EC R=500 Δ=47°37' L T=220.61

9+21.73 PC

20+17.96 EC R=170 Δ=32°26' R T=49.44

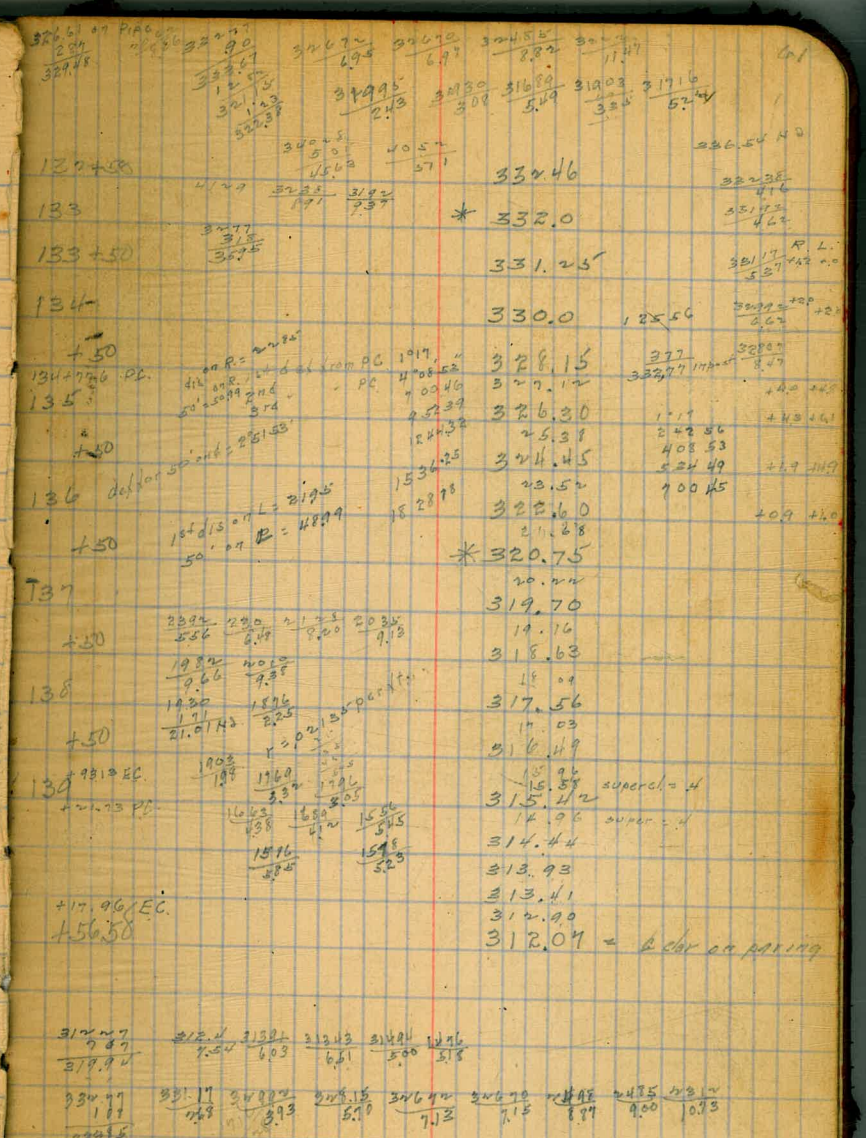
140+56.58 End of Tommy Pines pavement

Changed at upp. grade

P.J.3 R 1035'

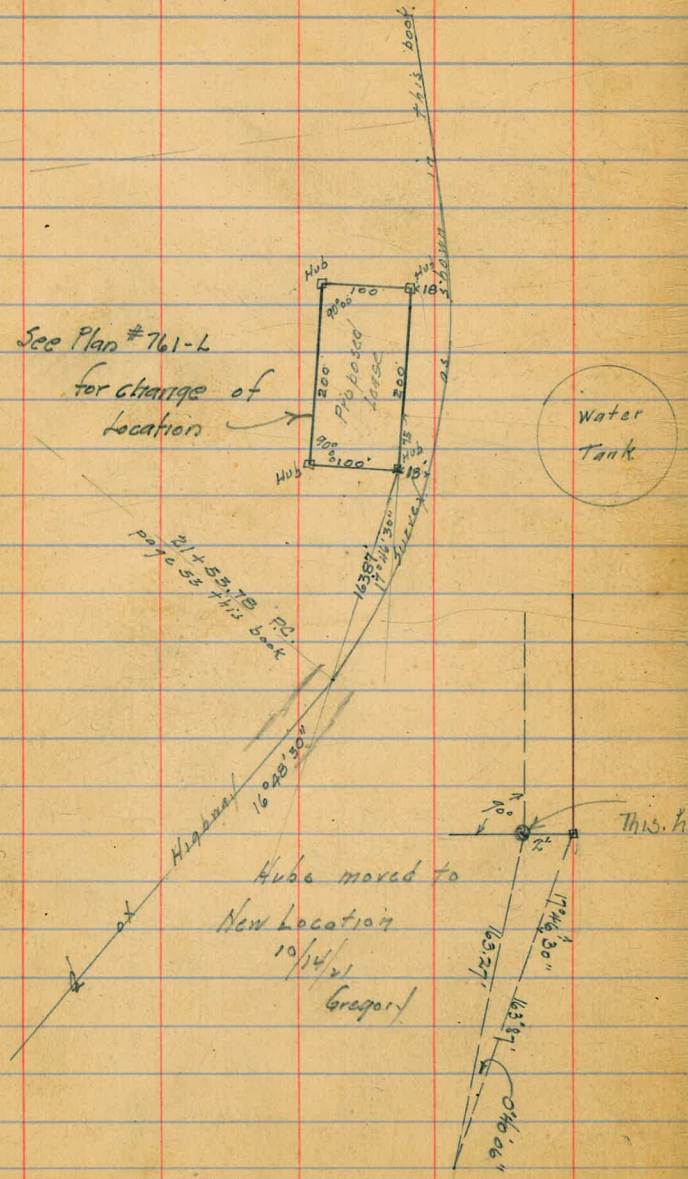
1+17 R 1035'

1.07 R 1010



10/10/21. Gregory Moore Miller Shaw

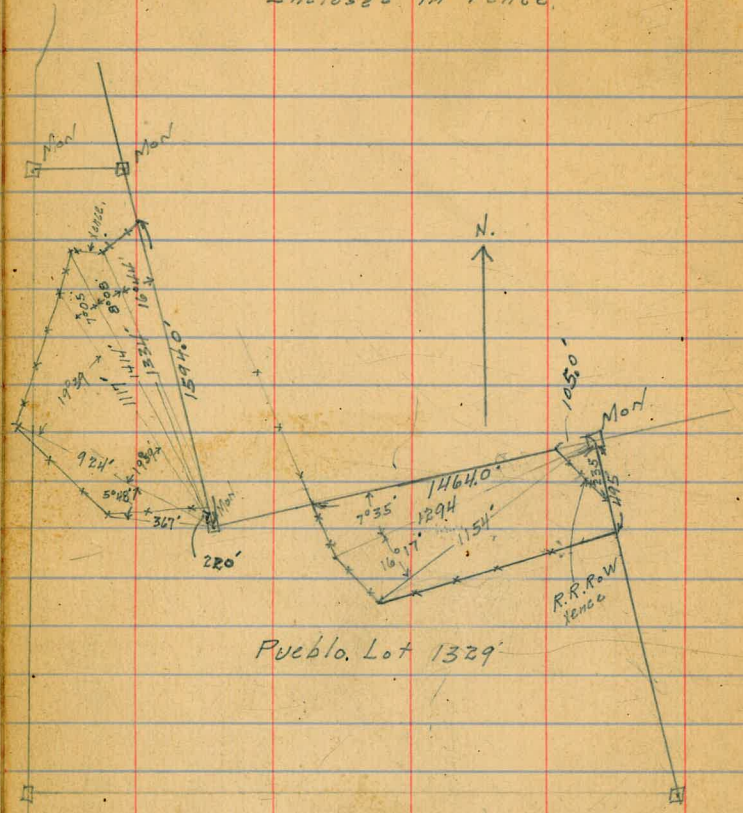
Survey of Lease at Water Tank on Paved Highway N. of Pueblo Farm House



See Plan #761-L for change of Location

10/10/21 Gregory Survey of Bottom Land in
Moore
Miller
Shaw

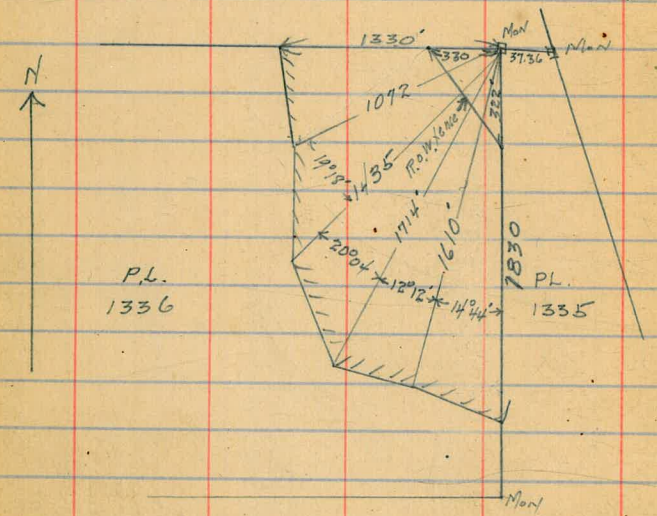
P.L. 1329
Enclosed in Fence



Pueblo. Lot 1329

10/10/21 Gregory Moore Miller Shaw

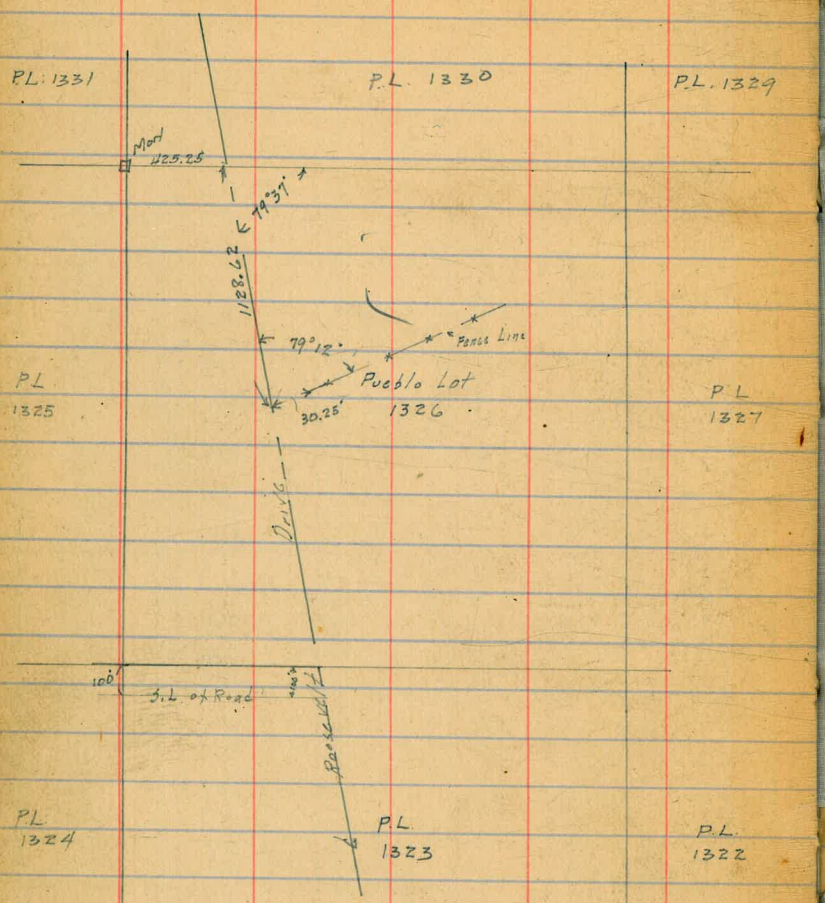
Survey of Bottom Land
P.L. 1336



5/15/73

Gregor
Moore
Miller
Shaw

Location of Fence Line East of Roosevelt Drive in P.L. 1326



73

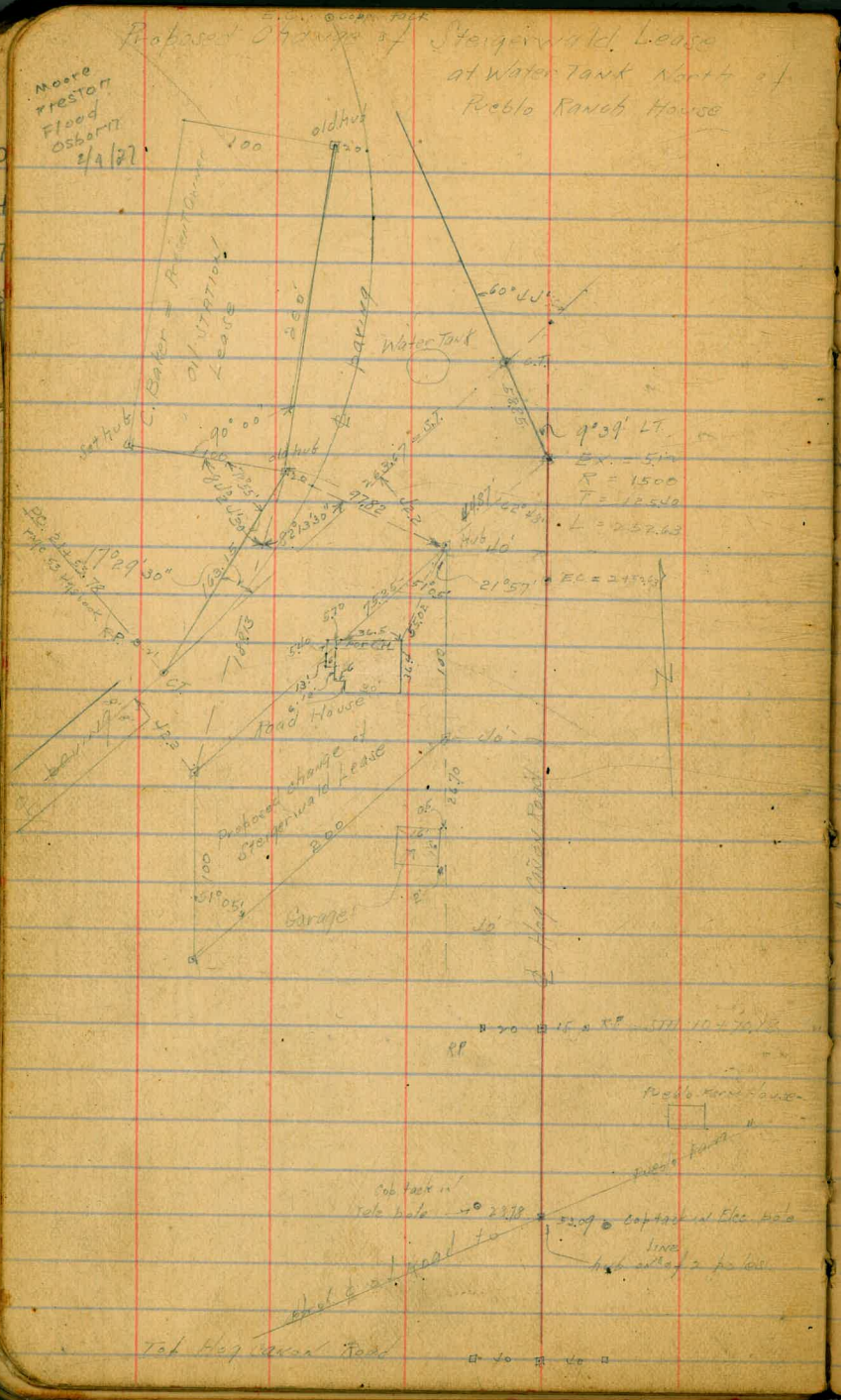
37.42
62.38
87

9891
8762.36
1128.62

65

Moore
Preston
Flood
Osborn
2/9/27

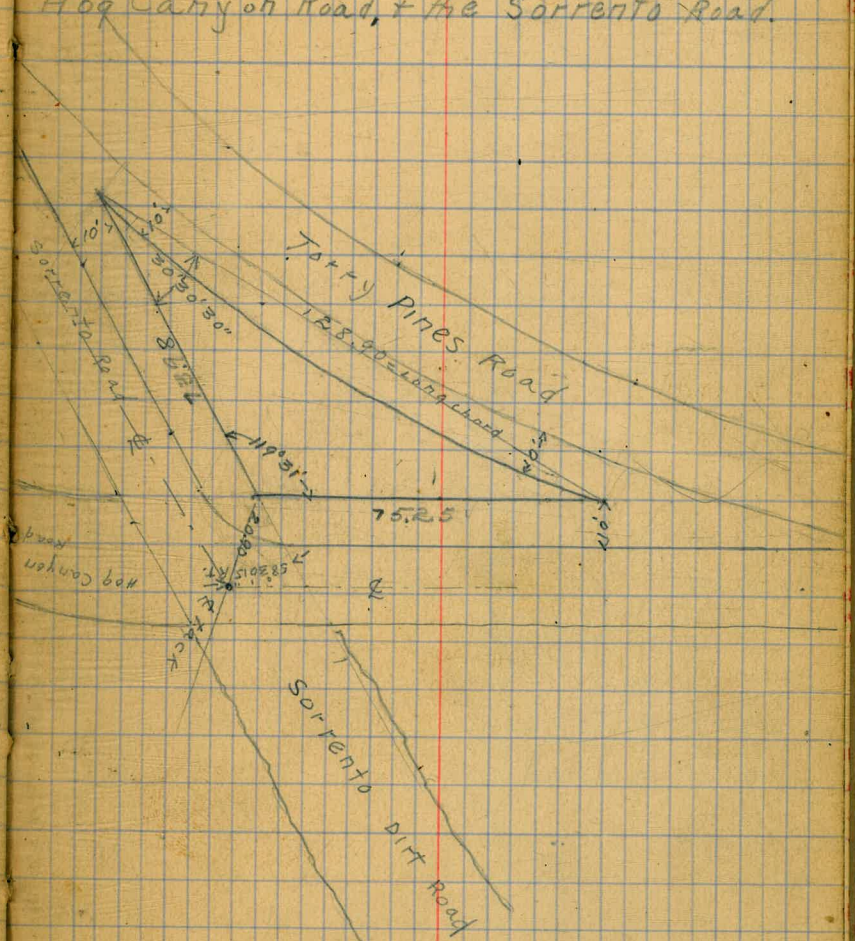
Proposed Extension of Steigerwald Lease at Water Tank North of Pueblo Ranch House



McHugh
Flood
Rauner

66

Measurements on triangular plot inclosed by the junction of Tarry Pines Road, Hog Canyon Road, & the Sorrento Road.

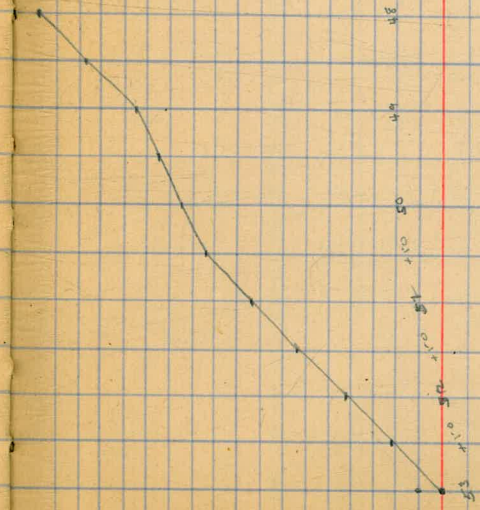


193.00
1.00
191.96

		11.67			
	4.19	370.10		365.91	
160			11.7	58.2	
+50			9.7	60.4	
159			8.0	362.1	
+50			6.5	63.6	
158			4.9	65.2	
+50			3.4	66.7	
157			2.1	68.0	
+50			0.6	69.5	
	12.63	382.36	0.37	369.73	
156			11.3	71.1	
+50			9.9	72.5	
155			8.3	74.1	
+50			6.7	75.7	
154			5.2	77.2	
+50			3.5	78.9	
153			1.9	80.5	✓
+50			0.25	82.11	
	17.69	394.93	0.1 N	384.04	
152			11.1	83.8	

9493

+50			94	85.5
151			7.56	87.38
+50			5.85	89.08
150			40	90.9
+50			2.25	92.68
149			0.6	94.3 ✓
	9.29	403.64 ✓	0.58	394.35
+50			7.6	96.0 ✓
148			5.6	98.0 ✓
+50			3.5	00.1 ✓
EC			2.3	01.3 ✓



Paving Estimate on Imperial Ave. between 8th & 9th Sts

Curb on No. Side = 99.2 lin. ft.
" " So. " = 100.2 " "

Paving

100 × 2.25 = 225
100 × 2.93 = 293

Average 294 □' − (5 × 2.98 C.B.) = 279.4 □'

13.5 × 3.5 = (INT OF 8th St) (47.25)
25.91 × 10 = 259.1
27.09 × 10 = 270.9
Average = 265 265.0 □'

27.09 × 10 = 270.9
28.08 × 10 = 280.8
Average = 275.85 275.85 □'

28.08 × 10 = 280.8
28.84 × 10 = 288.4
Ave 284.6 284.6 □'

28.84 × 10 = 288.4
29.39 × 10 = 293.9
Ave = 291.15 291.15 □'

29.39 × 10 = 293.9
29.77 × 10 = 297.7
Ave 295.8 295.8 □'

29.77 × 10 = 297.7
29.99 × 10 = 299.9
Ave 298.8 298.8 □'

carried for'd 1990.60 □'

brot for'd 1990.60

29.99 × 10 = 299.9
30.05 × 10 = 300.5
Ave 300.2 300.2 □'

30.05 × 30 = 901.5
30.02 × 30 = 900.6
Ave 901.05 901.05 □'

4.8 × 10 = 48.0
3.64 × 10 = 36.4
Ave 42.2 − (2.9 × 5.0 C.B.) = 27.7

3.64 × 10 = 36.4
2.64 × 10 = 26.4
Ave 31.4 31.4

2.64 × 10 = 26.4
1.84 × 10 = 18.4
Ave 22.4 22.4

1.84 × 10 = 18.4
1.27 × 10 = 12.7
Ave 15.55 15.55

1.27 × 10 = 12.7
.92 × 10 = 9.2
Ave 10.95 10.95

.92 × 10 = 9.2
.78 × 10 = 7.8
Ave 8.5 8.5

for'd 3308.35

Connection Diagram on Lots

	N	N2			
		100.00			
600	from 0.0		5.7	94.3	approx bot of lake
			3.6	96.4	apparent high water
00			4.7	95.3	
1			4.1	95.9	
2			3.0	97.0	
T.P	7.6	104.8	2.8	97.2	
3			6.1	98.7	
T.P.	5.7	106.6	3.9	100.9	
4			5.4	101.2	
5			2.9	103.9	←
TP	4.2	107.9	2.9	103.7	
6			4.8	103.1	
7			6.4	101.5	
8			7.7	100.2	
TP	4.1	104.3	7.7	100.2	
9			5.7	98.6	
10			7.8	96.5	
+50			10.7	93.6	

from Or Station to Big Corral - 15.8

L 2.60
4.9
4 2.1.4

30 1.06
4 2.9.6 2
74.44

629.6 2

3 2.78 to so. hub.

	card Yard.	3308.35
.78 x 10	7.8	
.75 x 10	7.5	
	7.65	7.65
.75 x 30	22.5	
.78 x 30	23.4	
	28.95	22.95
Total paving		3338.95 □
Total curb		199.4 lin ft

Paving in 8th St 47.25 □

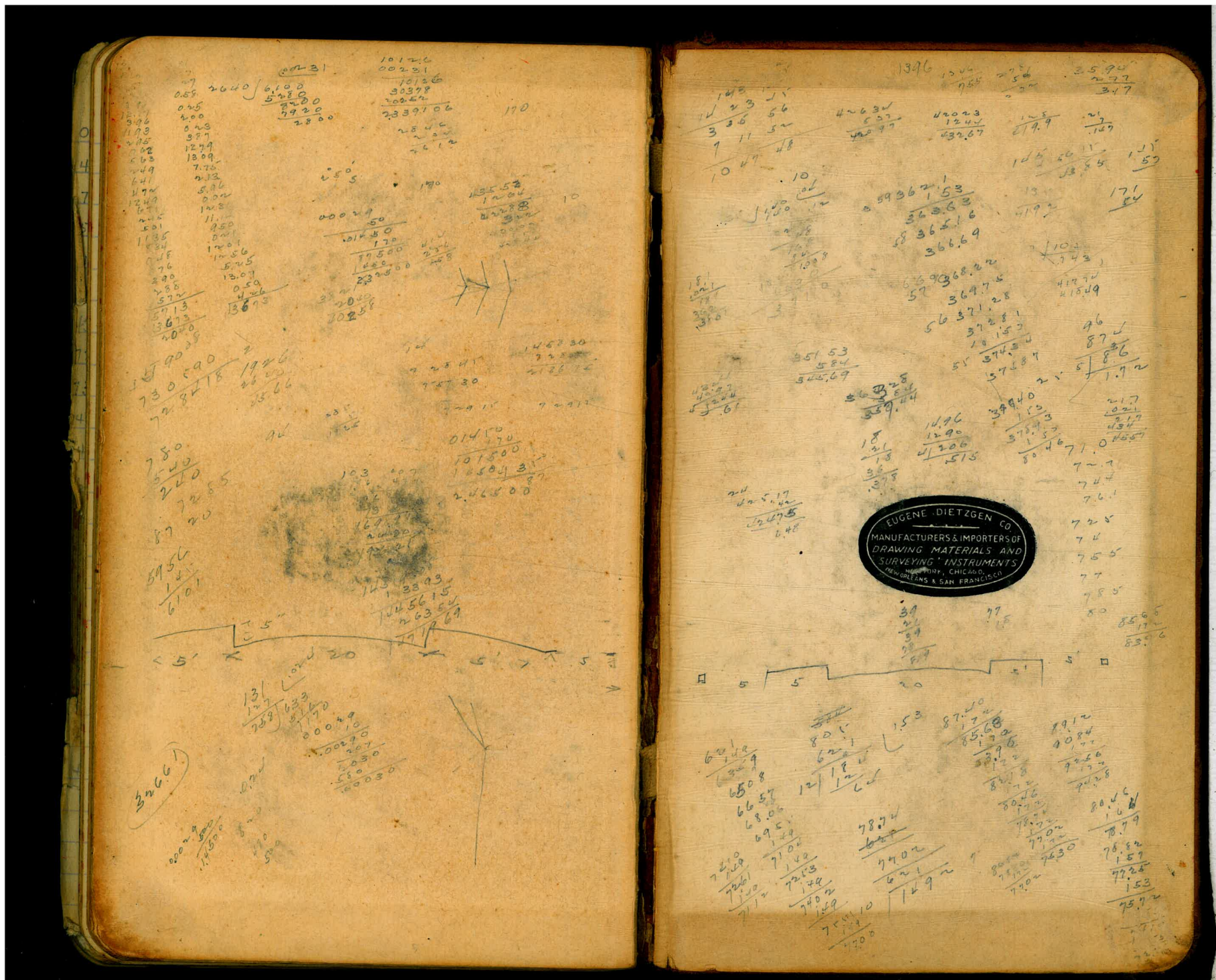
380.5 2
17 2 378.86
378.80
1.60

377.20
377.08

375.65
375.63
375.59

374.10

3.5 2
1.06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