

1036

EVILY BOOK

373

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

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MICROFILMED

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

47.57 on Arista W
45.00
16.58 on La Jolla
103.26
15.02
44.03
12.14 on 5 Tanglo E = 6.7
PI

N 20° N 50' 0.695
Palca 10 H 0.58
H 20 N 0.70
H 28 H 0.60
Lytton NE Tallend brace 1.75

0711.40 3 E Bolt
1+28 ✓
2+01 ✓



3/13/18
Gregory
Moore
Miller

CROSS SECTION OF
MAPLE ST, ARROYA DRIVE and DOVE ST.
from Reynard Way to Notmeq
10' walks on all widths

BM	0.13	111.72	111.59	spt 511 Union Notmeq
T.P.	0.51	99.44	12.79	98.93
T.P.	0.97	87.61	1280	86.64
T.P.	0.77	75.71	1267	74.94
T.P.	2.11	64.93	1289	62.82

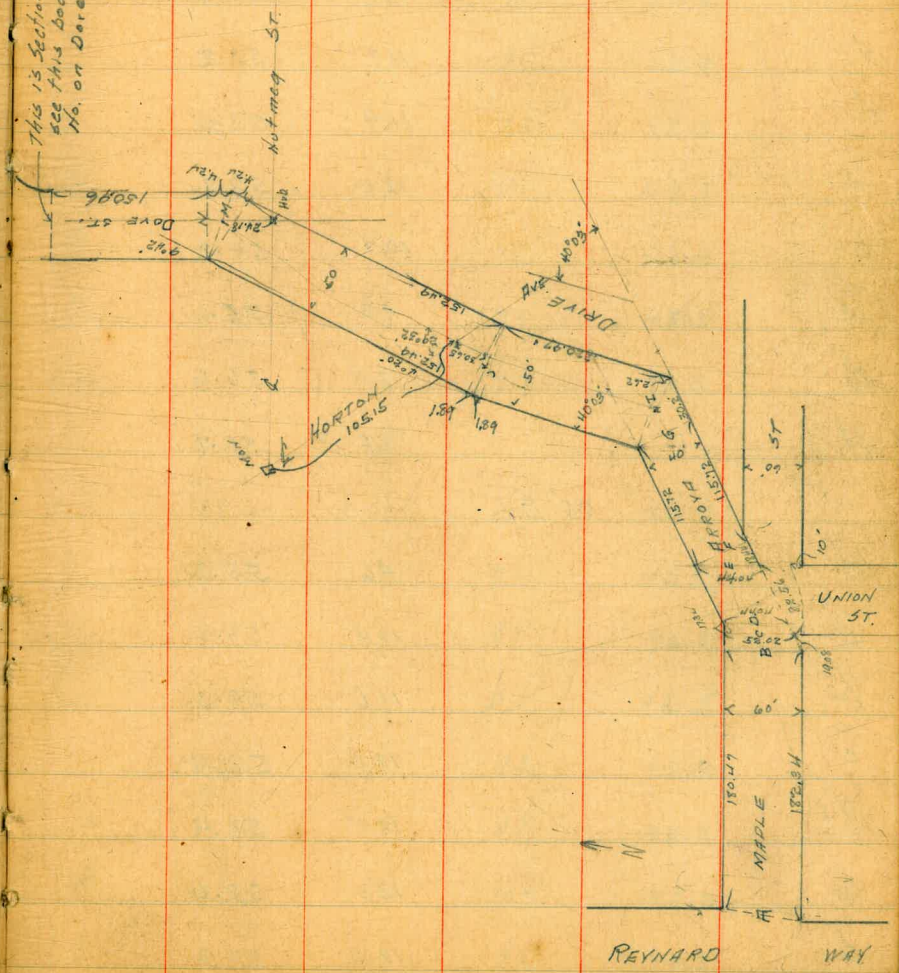
E.L. Reynard Way Sec. A.

3		6.4	58.5
cb		6.7	58.2
1/4		68	58.1
c		70	57.9
1/4		73	57.6
cb		7.5	57.4
H		7.6	57.3

6' E of A on No.

H		7.4	57.5
cb		82	56.7
1/4		85	56.4
c		82	56.7
1/4		89	56.0

This is Section B page 30 Book 66A
see this book for levels etc further
No. on Dove St.



64.93

cb		10.7	54.2
S		10.9	54.0
+5		11.1	53.8
	19' E		
-5		11.8	53.1
S		11.7	53.2
cb		11.9	53.0
1/4		12.0	52.9
C		10.7	54.2
1/4		9.3	55.6
cb		8.3	56.6
N		8.2	56.7
	23' E		
N		9.6	55.3
cb		10.4	54.5
1/4		11.6	53.3
C		12.0	52.9
1/4		12.5	52.4
cb		12.3	52.6
S		12.3	52.6
+5		12.3	52.6

MAPLE

V 2

T.P.	3.36	56.01	12.28	52.65
		31' E		
-20			7.8	48.2
S			7.0	49.0
cb			8.1	47.9
1/4			8.1	47.9
C			7.7	48.3
1/4			8.1	47.9
cb			8.6	47.4
N			7.7	48.3
+10			7.7	48.3
		35' E		
-10			9.3	46.7
N			9.2	46.8
cb			9.7	46.3
1/4			9.5	46.5
C			9.3	46.7
1/4			9.8	46.2
cb			10.0	46.0
S			9.2	46.8
+10			9.3	46.7

56.01

45' E

-15	11.6	44.4
S	11.4	44.6
cb	11.3	44.7
1/4	11.1	44.9
C	10.9	45.1
1/4	10.6	45.4
cb	10.4	45.6
N	9.4	46.6
+15	8.8	47.2

65' E

-15	8.4	47.6
N	8.9	47.1
cb	9.3	46.7
1/4	10.4	45.6
C	10.5	45.5
1/4	10.6	45.4
cb	11.0	45.0
S	11.2	44.8
+15	11.6	44.4

MAPLE

3

3

80' E

-15	4.6	51.4
S	4.8	51.2
cb	5.9	50.1
1/4	9.0	47.0
C	9.5	46.5
1/4	9.5	46.5
cb	9.4	46.6
N	9.4	46.6
+15	8.8	47.2

100' E

-15	5.4	50.6
N	1.7	54.3
cb	1.8	54.2
1/4	4.3	51.7
C	2.5	53.5
1/4	1.8	54.2
cb	1.7	54.3
S	1.7	54.3
+10	2.0	54.0

T.P.

12.68

67.49

120

54.81

120° E

-10		133	54.2
S		126	54.9
cb		12.5	55.0
1/4		11.5	56.0
C		10.7	56.8
1/4		10.1	57.4
cb		10.2	57.3
N		10.3	57.2
+10		10.5	57.0

143° E

-10		85	59.0
N		83	59.2
cb		83	59.2
1/4		72	60.3
+6		6.9	60.6
C		9.4	58.1
1/4		10.4	57.1
cb		10.9	56.6
S		11.4	56.1
+10		11.9	55.6

MAPLE

cb

160° E

-10		113	56.2
S		10.8	56.7
cb		10.4	57.1
1/4		9.9	57.6
+5		9.0	58.5
C		6.6	60.9
+2		3.4	64.1
1/4		3.4	64.1
cb		3.9	63.6
N		5.4	62.1
+10		6.6	60.9

175° E

-10		3.4	64.1
N		0.5	67.0
cb		+1.1	68.6
1/4		+1.3	68.8
C		+1.3	68.8
1/4		7.5	60.0
+6		9.4	58.1

67.49

cb			9.7	57.8
S			10.2	57.3
+10			10.8	56.4
	180.47, E. of No.	} = SECT. "B"		
	182.34 - 2.50			
-10			9.9	57.6
S			8.4	59.1
cb			7.1	60.4
+8			4.1	63.4
1/4			1.7	65.8
T.P.	9.67	76.96	0.20	67.29
+6			6.5	70.5
C			6.8	70.2
1/4			6.4	70.6
cb			6.7	70.3
N			8.7	68.3
+10			11.9	65.1
	9' E of "B" + parallel to same			
N			7.0	70.0
cb			6.2	70.8
1/4			5.8	71.2

MAPLE 5

C	5.2	71.6
1/4	5.4	71.6
cb	4.1	72.9
S	3.8	73.2
	17.34' E of "B" on No. = SEC. C = W.L. Union.	
	Sections are taken on lines which are parallel to W.L. Union.	
S	3.7	73.3
cb	4.7	72.3
1/4	4.6	72.4
C	5.1	71.9
1/4	5.7	71.3
cb	6.2	70.8
N	6.9	70.1
	12' E. of "C" on No. = W. C. b	
N	8.1	68.9
cb	6.7	70.3
1/4	5.0	72.0
C	4.5	72.5
1/4	4.6	72.4
cb	3.8	73.2
S	2.2	74.8

76.96

17.34 E. of "C" = Sect "D" = 44.04 wide

S	2.8	74.2
cb	3.3	73.7
1/4	2.9	74.1
C	2.3	74.7
1/4	2.9	74.1
cb	4.9	72.1
+4	5.7	71.3
+8	7.7	69.3
N	8.1	68.9
8.17 E of D = W. 1/4		
N	8.9	68.1
+2	8.7	68.3
+4	6.5	70.5
cb	4.8	72.2
1/4	3.4	73.6
C	2.7	74.3
1/4	2.1	74.9
cb	1.6	75.4
S	2.2	74.8

ARROYA 6

14.03 E of W. 1/4 = Ctr.

S	0.0	77.0
BM	0.42	76.52
cb	0.2	76.6
1/4	0.9	76.1
C	2.5	74.5
1/4	4.0	73.0
cb	5.9	71.1
+5	7.1	69.9
+7	9.3	67.7
N	9.6	67.4
T.P.	0.91	77.45
		76.54

ctr. Max
Union + Maple

14.03 E of Ctr = E. 1/4

N	10.8	66.7
+5	10.5	67.0
cb	8.6	68.9
1/4	6.5	71.0
C	5.1	72.4
1/4	3.7	74.8
cb	2.0	75.5
S	1.1	76.4

14.03 E of E 1/4 = Ecb

S	23	75.2
cb	5.3	72.2
1/4	6.3	71.2
C	7.7	69.8
1/4	9.0	68.5
cb	10.7	66.8
+2	11.2	66.3
N	11.0	66.5

13.27' E of Cb = E.L. UNION = SECT E

N	12.2	65.3
cb	11.5	66.0
+3	11.3	66.5
1/4	10.8	66.7
C	9.6	67.9
1/4	8.4	69.1
cb	6.9	70.6
S	3.7	73.8

15.44' E of SECT E on S. }
00 - - - - - } = SECT E

S	7.0	70.5
cb	9.0	68.5
1/4	9.9	67.6
C	11.1	66.4
1/4	11.5	66.0
cb	11.7	65.8
N	12.1	65.4
+10	13.3	64.2

18' E.

-15	16.6	60.9
-10	16.4	61.1
N	12.7	64.8
cb	12.1	65.4
1/4	12.1	65.4
C	12.2	65.3
1/4	12.2	65.3
cb	12.3	65.2
S	10.2	67.3

7745

25' E

-5		11.6	65.9	
3		12.8	64.9	
cb		12.8	64.7	
1/4		12.5	65.0	
C		12.2	65.3	
1/4		12.2	65.3	
cb		12.1	65.1	
T.P.	2.19	67.14	12.50	64.95
+5		2.6	64.5	
N		4.6	62.5	
+15		8.0	59.1	

38' E

-20		10.3	56.8
N		7.8	59.3
cb		2.6	64.5
1/4		1.8	65.3
C		2.1	65.0
1/4		2.1	65.0
cb		2.1	65.0

+7

5

+8.5

+10

-13

-12

5

cb

1/4

C

1/4

cb

+3

N

+10

+20

+22

-20

4.0

3.6

3.6

2.2

3.0

4.2

4.1

3.3

2.0

2.1

2.6

5.2

9.0

9.9

10.8

16.6

11.7

10.4

63.1

63.3

63.5

64.9

64.1

62.9

63.0

63.8

65.1

65.0

64.5

61.9

58.1

59.2

56.3

50.5

55.4

56.7

APPOY 8

46 E

54 E

6714

APPROX 9

-15		10.4	56.7	cb		6.8	60.3
-10		15.5	57.6	1/4		6.8	60.3
-3		15.5	51.6	c		8.1	59.0
N		10.9	56.2	1/4		9.3	57.8
+6		9.3	57.8	cb		10.3	56.8
cb		6.6	60.5	+6		11.4	55.7
1/4		3.2	63.9	+7		15.3	51.8
c		2.4	64.7	N		15.8	51.3 bottom
1/4		2.7	64.4	+5		10.5	56.6
cb		4.0	63.1	+15		10.2	56.9
+5		6.6	60.5		61' E		
5		6.6	60.5	-20		4.8	62.3
+5		5.6	61.5	-15		8.9	58.2
+15		6.0	61.1	-5		8.6	58.5
+17		5.5	61.6	N		10.9	56.2
	58' E			+1		13.0	54.1
-20		6.5	60.6	cb		12.7	54.4
-7		6.4	60.7	1/4		12.1	55.0
5		7.6	59.5	c		11.7	55.4
+6		7.7	59.4	1/4		11.5	55.6

67.14

16	8.5	58.6
5	7.6	59.5
+8	6.5	60.3
+20	7.3	59.8
	64' E	
-20	8.1	59.0
5	8.2	58.9
+7	8.7	58.4
cb	10.7	56.4
+2	11.4	55.7
1/4	11.6	55.5
c	11.6	55.5
1/2	12.5	54.6
cb	12.3	54.8
+3	10.1	57.0
N	10.0	57.1
+3	6.7	60.4
+10	4.4	62.7
	69' E	
-10	3.8	63.3

-5

N

+3

cb

1/4

c

1/4

cb

5

+2

+20

-20

-4

5

+5

cb

1/4

c

1/4

ARROYA

190

4.2

6.1

10.1

10.0

11.4

5.8

6.4

10.5

10.0

8.7

8.3

73' E

7.6

7.3

9.3

7.6

7.2

6.2

3.1

1.8

62.9

61.0

57.0

57.1

55.7

61.3

60.7

56.6

57.1

bottom

58.4

58.8

59.5

59.8

57.8

59.5

59.9

60.9

64.0

65.3

67.14

cb	1.9	65.2
H	1.9	65.2
	next	
	87' E	
H	1.5	65.6
cb	0.8	66.3
1/4	0.3	66.8
C	0.2	66.9
1/4	0.8	66.3
cb	2.5	64.6
+9	3.4	63.7
3	5.7	61.4
+4	8.5	58.6
+6	41	63.0
+20	49	62.2
	89' E	
-20	4.2	62.9
-6	37	63.4
-4	86	58.5
5	80	59.1
+2	7.8	59.3

ARROYA

IN

+5	3.3	63.8
cb	2.5	64.6
1/4	0.3	66.8
C	0.1	67.0
1/4	0.1	67.0
cb	0.7	66.4
H	1.0	66.1
+5	1.2	65.9
T.P.	10.31	75.85
		1.60
	100' E	
-5	9.8	66.1
H	9.9	66.0
cb	8.6	67.3
1/4	8.3	67.6
C	8.3	67.6
1/4	8.5	67.4
+3	8.9	67.0
	15.9	66.0
cb	15.9	60.0
+3	16.4	59.5
+6	8.7	67.2

7585

5	86	67.3
+10	87	67.2
115.72'E = SEC. G.		
-5	85	67.4
-3	87	67.2
-2	13.1	62.8
5	138	62.1
+1	153	60.6
13	158	60.1
#8	89	67.0
cb	85	67.4
1/4	83	67.6
c	77	68.2
1/4	79	68.0
cb	81	67.8
N	85	67.4
+5	97	66.2
302 E of G on So } = # 00 - - - - - No.		
N	85	67.4
+4	7.1	68.8

ARROYA

1/2

cb	7.5	68.4
1/4	7.6	68.3
c	7.2	68.7
1/4	7.9	68.0
cb	8.4	67.5
S. or E	8.6	67.3
+5	8.4	67.5
SEC I = 1 st 50' SECTION		
E	8.6	67.3
cb	8.5	67.4
1/4	8.0	67.9
c	7.2	68.7
1/4	7.6	68.3
cb	7.6	68.3
+6	7.1	68.8
W	8.5	67.4
30' No. of I		
W	5.7	70.2
cb	5.9	70.0
1/4	5.8	70.1

c	6.0	69.9
1/4	5.7	70.2
cb	6.2	69.7
E	7.5	68.4
-5	7.6	68.3
E	4.7	71.2
cb	4.7	71.2
1/4	5.1	70.8
c	5.2	70.7
1/4	5.4	70.5
cb	5.4	70.5
W	5.5	70.4
W	2.6	73.3
cb	2.2	73.7
1/4	2.2	73.7
c	1.9	74.0
1/4	1.9	74.0
+6	2.6	73.3

40' No. This is 1st complete section of ^{the st. as graded}

cb	1.0	74.9
E	1.0	74.9
TP	12.25	86.33
	1.77	74.08
	1.50	No.
E	7.9	78.4
cb	8.6	77.7
+1	9.9	76.4
1/4	9.1	77.2
c	9.3	77.0
1/4	9.5	76.8
cb	9.5	76.8
W	9.6	76.7
W	8.1	78.2
+5	7.3	79.0
cb	7.1	79.2
1/4	6.7	79.6
c	6.5	79.8
1/4	6.3	80.0
cb	7.3	79.0
	cb. 57	80.6

185' No.

E		5.3	81.0
	220.97 No. on E 222.86		
			SECT K.
E		2.3	84.0
cb		2.5	83.8
+1		4.2	82.1
1/4		3.0	83.3
C		3.5	82.8
1/4		3.9	82.4
cb		3.6	82.7
W		3.6	82.7
T.P.	12.59	98.22	0.70
			85.63
	50 No. on X		SEC L.
W		9.4	88.8
cb		9.6	88.6
+1		10.5	87.7
1/4		10.0	88.2
C		9.6	88.6
1/4		9.6	88.6
cb		10.8 } 9.4 }	87.4 88.8
E		9.5	88.7

			100' No	
E		3.6	94.6	
cb		3.7	94.5	
+1		4.6	93.6	
1/4		4.0	94.2	
C		3.9	94.3	
1/4		4.1	94.1	
+6.5		4.6	93.6	
cb		3.8	94.4	
W		3.7	94.5	
T.P.	12.25	109.81	0.66	
	152.44 No. on W			
	156.73 - - E			
			SEC. M.	
W		9.2	100.6	
cb		9.5	100.3	
+1		10.1	99.7	
1/4		9.6	100.2	
C		9.6	100.2	
1/4		9.7	100.1	
+6.5		10.4	99.4	
cb		9.5	100.3	
E		9.3	100.5	

109.81

50' No. of SECT. N

E			3.9	105.9
cb			4.1	105.7
+1			5.2	104.6
1/4			4.3	105.5
C			4.3	105.5
1/4			4.5	105.3
+6.5			4.7	105.1
cb			4.0	105.8
W			3.9	105.9
T.P.	12.83	12.40	0.24	109.57
	100' No.			
W			11.3	111.1
cb			11.5	110.9
+1			12.4	110.0
1/4			11.9	110.5
C			11.8	110.6
1/4			11.7	110.7
+6.5			12.1	110.3
cb			11.0	111.4
E			10.8	111.6

1515

150.96' No. of N. = SECT B on page 30 Book 966H

see map of Martha Heights

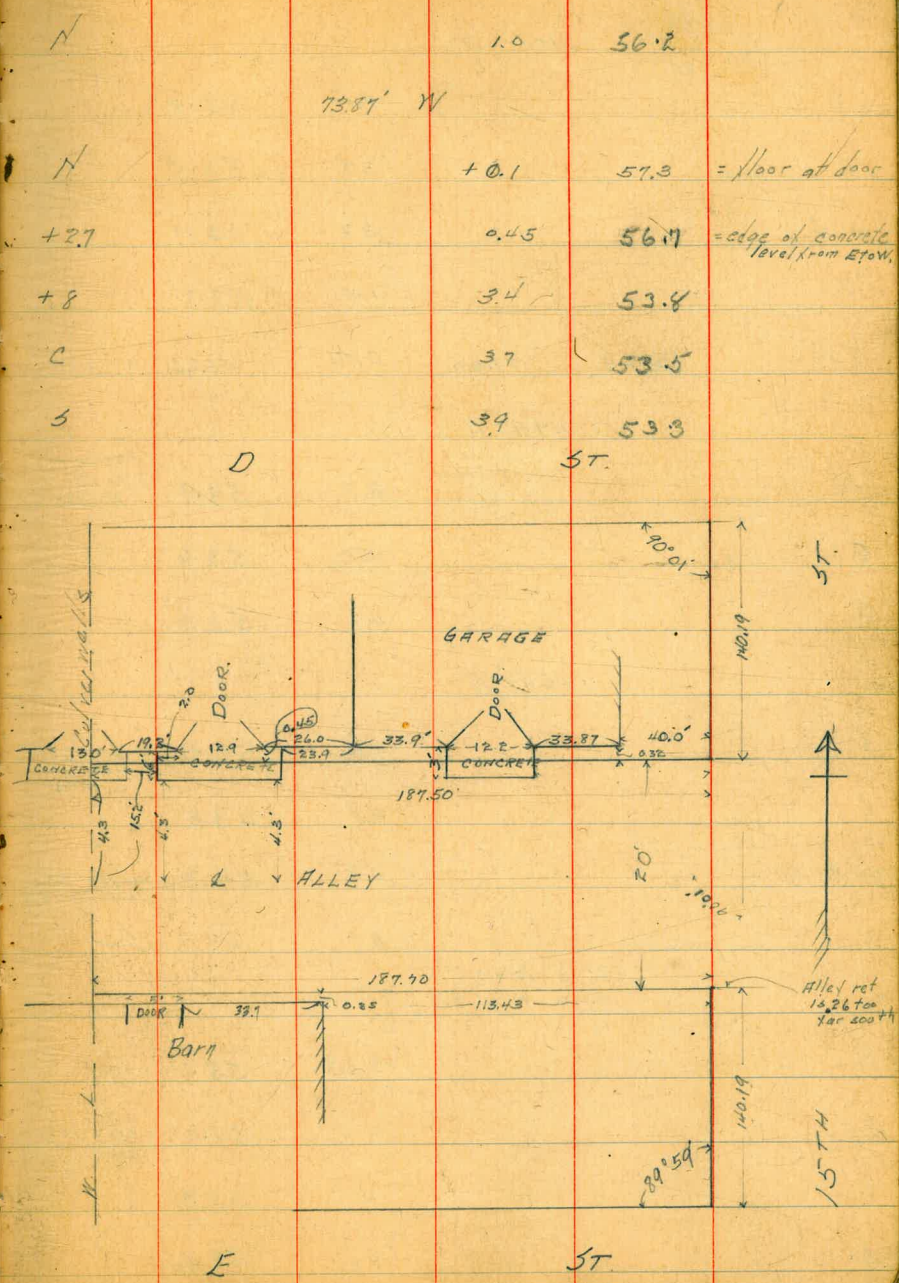
E			5.8	116.6
cb			6.3	116.1
+1			7.4	115.0
1/4			6.9	115.5
C			6.9	115.5
1/4			7.1	115.3
+6.5			7.2	115.2
cb			7.0	115.4
W			6.8	115.6
chk BM			5.56	116.84 = 90 page 28 book 966H

3/14/18 Gregory Moore Miller

CROSS SECTION and Improvements Alley bet D + E + 14th + 15

1616

BM	6.27	57.22	50.95	BP NW 14+E
N		14. L 15 TH		
N		3.7	53.5	
C		48	52.4	
S		41	53.1	on cement CB
		25' W		
S		41	53.1	
C		45	52.7	
+6		40	53.2	
N		27	54.5	
		40' W		
N		23	54.9	footings 6' 6 1/2" 13.15' higher
+5		37	53.5	
C		44	52.8	
S		41	53.1	
		50' W		
S		41	53.1	
C		41	53.1	
+4		38	53.4	



57.22

100' W

S		3.5	53.7	
C		37	53.5	
+4		33	53.9	
N		1.5	55.7	
T.P.	229	58.55	0.06	56.26 on pipe

119.97' W

N		3.7	54.9	footing of bldg 1.3 higher
E		5.0	53.6	
S		4.7	53.9	

145.97' W

S		4.6	54.0	= door dirt floor is 4" lower
C		4.8	53.8	
+4.3		4.3	54.3	= edge of conc. level from E to W.
N		3.7	54.9	= floor

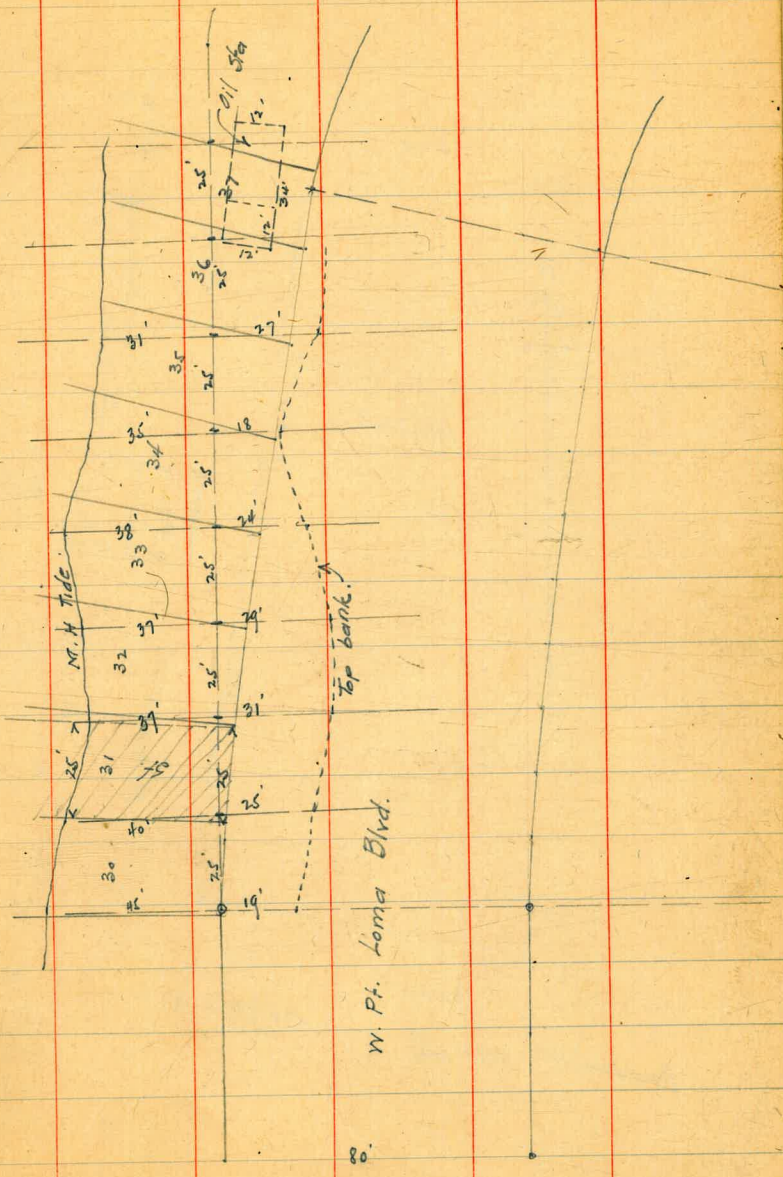
187.5' W on No. } = End.
187.7' v l 30

N		3.53	55.1	= floor
+5.7		4.4	54.2	= edge of conc. level from E to W.
C		4.7	53.9	
S		4.6	54.0	

209
122
50
40
119.97
26
12
19
178
0.7

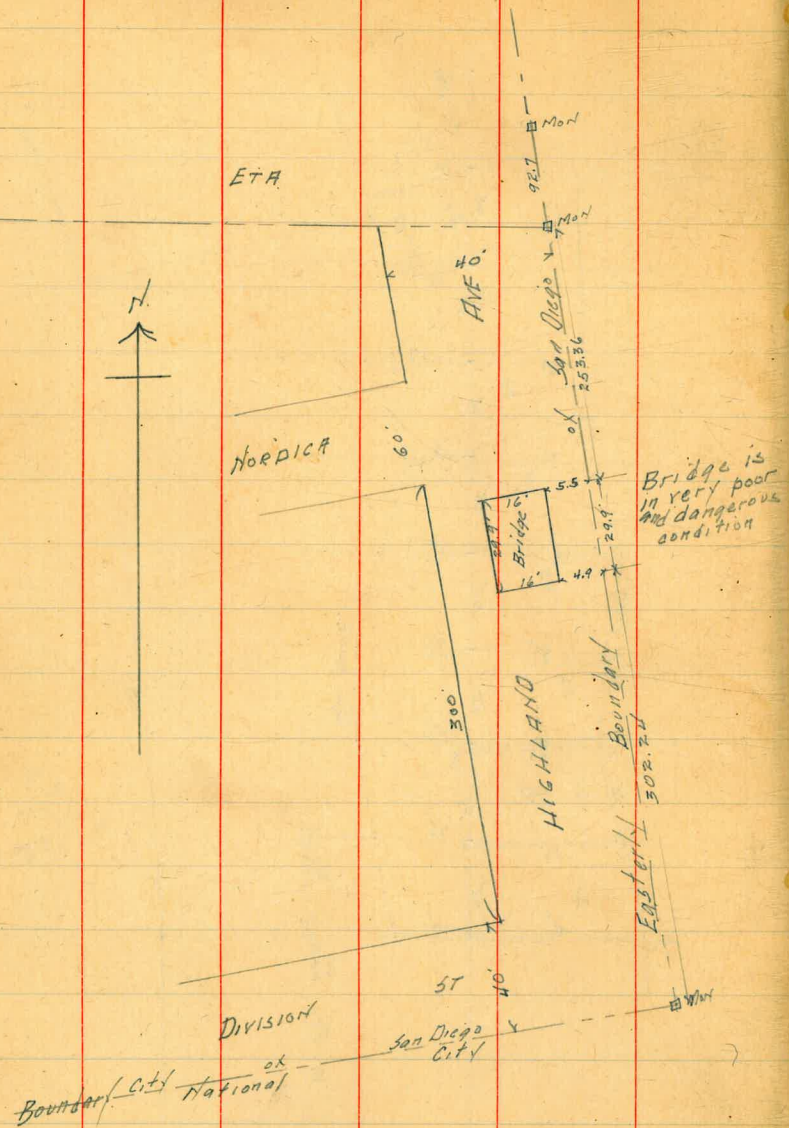
17

19.73
14.5
6
61.6
79



10/16/18 Grogan
Miller

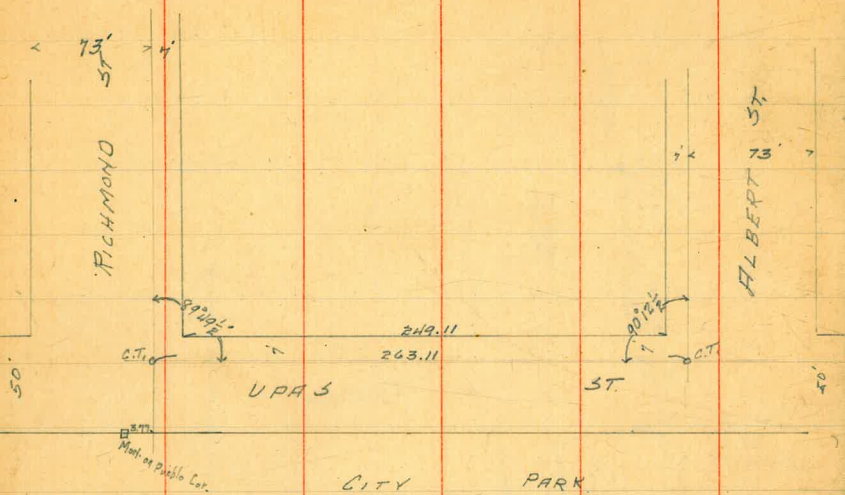
Location of
Bridge on Highland Ave
East Boundary of City



10/16/18 Gregory
Miller

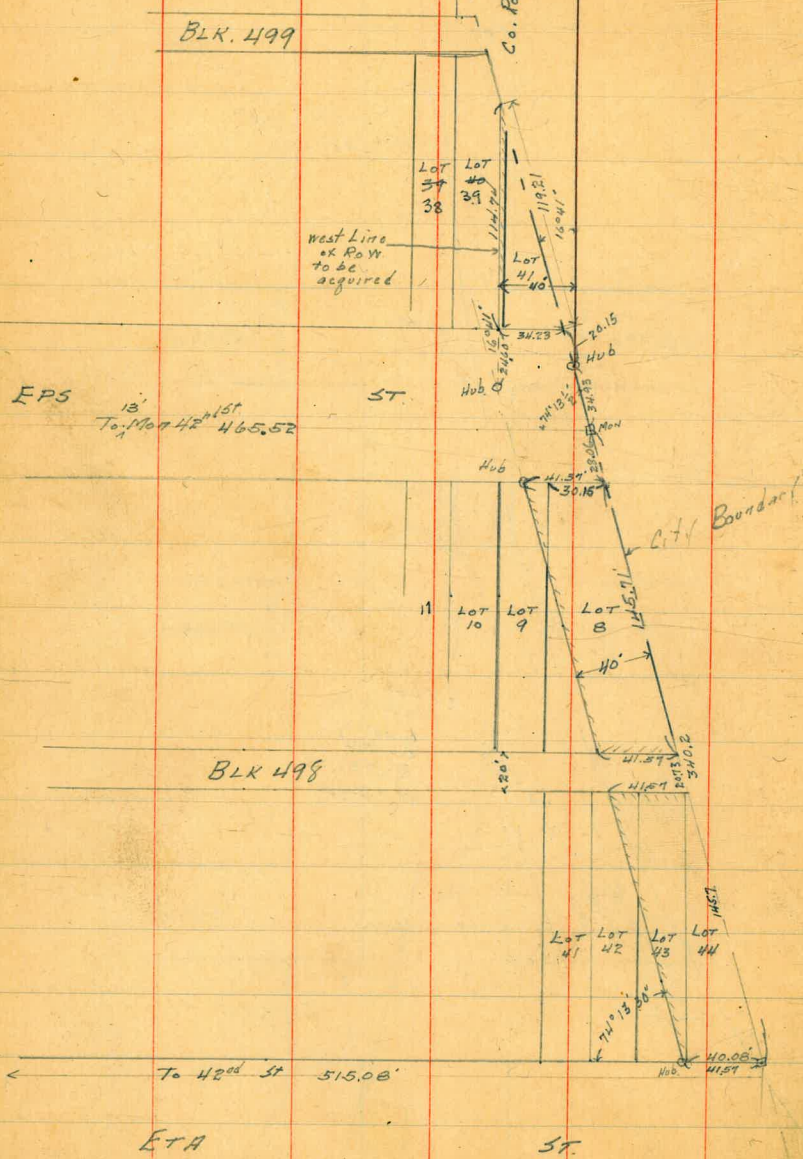
Survey between
Richmond + Albert
on
Upas St.

20



10/24/15
Gregory
Miller
Shank

Survey for the opening of
Highland Ave
through Blks 498 + 499
H.M. Dougherty's Subd.



Highland

1/2/19 Gregory

GRADES ON ALLEY
bet D+E, 14+15th

50 75
7.72
57.87

	So.		No
W.L. 15 th	53.25	53.00	53.72
25' W	53.38		53.82
40' W	53.44	53.21	53.89
50' W	53.51		53.93
70' W	53.62	53.39	54.01
75' W	53.65		54.03
100' W	53.78	53.53	54.14
125' W	53.92	53.69	54.24
150' W	54.05	53.80	54.35
175' W	54.19	53.94	54.45
187.6 W = End of Alley	54.25	54.0	54.5
200' W	54.33	54.08	54.56
225' W	54.45	54.20	54.66
250' W	54.58	54.33	54.77

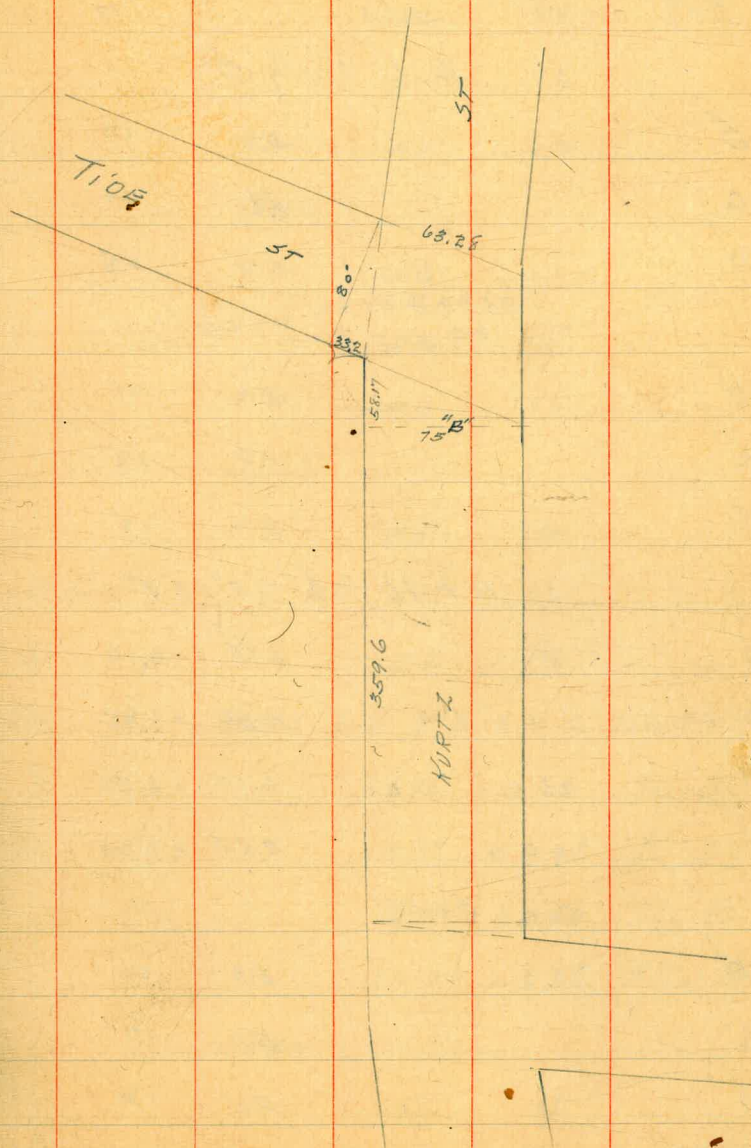
5095 NW 14+E	54.58	54.77	54.66	54.45	54.33	54.21	54.14	54.0
792	4.29	4.10	4.21	4.42	4.54	4.31	4.42	4.68
58.87								
	54.05	54.36	54.44	53.92	53.78	54.14	53.62	53.46
	4.29	4.50	4.53	4.95	5.09	4.93	4.25	5.41
53.16								
5.07	53.21	53.29	53.58	53.67	53.70	53.84	54.03	54.20
57.53	53.2	53.6	5.00	4.86	4.93	4.59	4.45	4.20

1/17/19		Levels on Kurtz St 75 wide from Witherby to Tide St.					
					C	3.1	3.3
W	B.M.	4.88	6.65	1.77	N.W. Kurtz + Tide E	2.6	4.1
		N.L. Witherby St.				250' No.	
	W		3.2	3.5	E	2.9	3.8
	C		2.1	4.3	C	3.7	3.0
	E		1.1	5.6	W	4.1	2.6
		50' No.				300' No.	
	E		1.2	5.5	W	4.3	2.4
	C		2.5	4.2	C	4.1	2.6
	W		3.1	3.3	E	3.2	3.5
		100' No.				359.6' No. = Rt Lst to SE Tide + Kurtz = "B"	
	W		3.6	3.1	E	3.8	2.9
	C		2.8	3.9	C	4.1	2.3
	E		1.7	5.0	W	4.7	2.0
		150' No.				3. L. Tide St.	
	E		2.2	4.5	W	5.0	1.7
	C		3.0	3.7	C	4.5	2.2
	W		3.7	3.0	E	3.8	2.9
		200' No.				6. Tide St.	
	W		3.9	2.8	E	4.1	2.6

6.65

C	4.7	2.0
W	4.8	1.9
NL. Tide St		
W	5.2	1.5
C	5.9	0.8
E	5.9	0.8

25



1/9/19 Gregor

Levels on Tide St
from Kurty to Lytton

B.M.	4.88	6.65	1.77	NW Kurty + Tide
W. L. Kurty St.				
S		5.0	1.7	
C		4.8	1.9	
N		5.2	1.5	
33.22 W on So } = 0.0. 00 v v No }				
N		5.2	1.5	
C		4.9	1.8	
S		5.2	1.5	
0 + 11 = 2'3" x 3'9" concrete curb.				
S		6.75	-0.10	Top Capping
S		10.50	-3.85	Flow Line
N		6.10	+0.55	Top Capping
N		9.85	-3.20	Flow Line
0 + 50				
N		5.3	1.4	
C		5.0	1.7	
S		5.5	1.2	

			1400	
S		5.6	1.1	
C		5.1	1.6	
N		5.5	1.2	
			1450	
N		5.6	1.1	
C		5.2	1.5	
S		5.6	1.1	
			2400	
S		5.5	1.2	
C		5.4	1.3	
N		5.5	1.2	
			2401 = 2'3' x 4'0" concrete curb	
S		6.85	-0.20	Top Capping
S		10.60	-3.95	Flow Line
N		6.25	+0.40	Top Capping
N		10.00	-3.35	Flow Line
			2450	
N		5.6	1.1	
C		5.4	1.3	

6.65

So	58	0.9
3+00		
So	61	0.6
C	55	1.7
No.	56	1.1
3+50		
No.	59	0.8
C	56	1.1
So.	62	0.5
4+00		
So	60	0.7
C	57	1.0
No.	59	0.8
4+50		
No.	60	0.7
C	58	0.9
So.	63	0.4
5+00		
So	62	0.2
C	58	0.9

TIDE 27

N	6.2	0.5
5+29		
N	6.3	0.4
C	59	0.8
S	61	0.6
5+41		
S.	2.7	4.0
+9	6.1	0.6
C	5.9	0.8
N	6.2	0.5
~6+00		
N	6.1	0.6
C	6.1	0.6
+26	6.6	0.1
+32	3.1	3.6
+38	2.5	4.2
So.	5.31	2.97
T.P.	1.43	3.88
6+50		
S	1.6	3.7
+5	1.6	3.7

+13		4.8	0.5
c		4.8	0.5
N		4.8	0.5
	7+00		
N		4.8	0.5
c		4.9	0.4
+27		5.3	0.0
+33		1.2	4.1
So.		1.3	4.0
	7+50		
So+1		1.2	4.1
+8		1.5	3.8
+13		5.2	0.1
c		4.9	0.4
N		5.0	0.3
	8+00		
N		4.8	0.5
		4.8	0.5
c		5.0	0.3
+27		5.2	0.1
+33		1.5	3.8

+38		1.2	4.1
	8+50		
S		1.2	4.1
+7		1.4	3.9
+13		5.1	0.2
c		5.0	0.3
N		4.9	0.4
	9+00		
N		4.9	0.4
c		4.9	0.4
+27		5.2	0.1
+33		1.9	3.4
So.		1.4	3.9
	9+50		
So.		2.1	3.2
+3		1.4	3.9
+6		1.4	3.9
+13		4.9	0.4
c		4.8	0.5
N		5.0	0.1

5.31

10+00

N	5.3	0.0
C	4.7	0.6
+27	5.3	0.0
+33	1.6	3.7
+39	1.2	4.1
S ₀	2.1	3.2

10+50

S ₀	3.0	2.3
+3	1.6	3.7
+6	1.4	3.9
+13	5.1	0.2
C	4.7	0.6
N	5.2	0.1

11+00

N	5.0	0.3
C	4.5	0.8
+28	4.6	0.7
+33	1.0	4.3
+38	1.2	4.1

TIDE

29

S₀

3.1

2.2

11+50

S ₀	3.7	1.6
+2	1.2	4.1
+8	1.1	4.2
+13	4.7	0.6
C	4.4	0.9
N	4.8	0.5

12+00

N	4.8	0.5
C	4.3	1.0
+27	4.6	0.7
+32	1.2	4.1
+37	1.3	4.0
S	3.4	1.9

12+50

S	3.2	2.1
+3	1.3	4.0
+7	1.0	4.3
+13	4.6	0.7

5.31

C	4.2	1.1
N	4.8	0.5
	13+00	
N	4.9	0.4
C	4.1	1.2
+2.7	4.2	1.0
+3.2	1.0	4.3
+3.8	0.9	4.4
S	2.1	3.2
	13+50	
S	2.1	2.9
+1	1.3	4.0
+7	1.3	4.0
+13	4.2	1.1
C	4.1	1.2
N	4.6	0.7
	14+00	
N	4.4	0.9
C	4.0	1.3
+2.8	4.0	1.3

TIDE

30

+3.2	0.7	4.6
+3.8	0.9	4.4
S	2.3	3.0
	14+50	
S	2.4	2.9
+2	1.0	4.3
+8	1.1	4.2
+1.2	4.0	1.3
C	3.9	1.4
N	4.4	0.9
	15+00	
N	4.2	1.1
C	3.8	1.5
+2.9	3.8	1.5
+3.3	1.6	1.7
+3.8	1.8	1.5
S	2.8	2.5
	15+50	
S	2.0	2.3
+8	0.9	4.4

5.31

+8	0.8	4.5
+12	3.9	1.4
C	3.7	1.6
N	3.9	1.4

16+00

N	4.1	1.1
C	3.7	1.6
+27	3.9	1.4
+32	0.6	4.7
+38	0.5	4.8

S	1.6	3.7
---	-----	-----

16+50

S	0.6	4.7
+8	0.6	4.7
+12	3.6	1.7
C	3.7	1.6
N	4.1	1.2

17+00

N	4.2	1.1
C	3.7	1.6

+29	4.0	1.3
+31	1.4	3.9
S	1.2	4.1

17+69.8 =
Send to Culy is buried in mud.

S	1.4	3.9
+8	1.2	4.1
+12	4.1	1.2
C	3.8	1.5

N	4.1	1.2
N	5.45	-0.14
N	7.2	-3.9

18+00

N	4.6	0.8
C	3.9	1.4
+27	4.2	1.1
+31	1.5	3.8
S	1.4	3.9

18+50

S	3.6	1.7
+12	1.8	3.5
+8	1.4	3.9
+12	4.3	1.0

TIDE 31

4.0" concrete cul.

Top Coping
Flow Line

5.31

TIDE

32

C			41	1.2	+27	4.2	0.7
N			46	0.7	+33	0.4	0.5
	19400				+38	0.5	0.4
N			46	0.7	5	2.1	2.8
C			42	1.1			
+27			46	0.7	5	2.2	2.7
+32			1.4	3.9	+2	0.8	4.1
+38			1.3	4.0	+7	0.8	4.1
S			26	2.7	+12	3.9	1.0
T.P.	0.60	4.88	1.03	4.88	C	4.0	0.9
		19450			N	4.3	0.6
S.			1.7	3.2			
+4			0.6	4.3	N	4.2	0.7
+7			0.5	4.4	C	4.0	0.9
+13			4.0	0.9	+26	4.0	0.9
C			3.7	1.2	+34	0.8	4.1
N			4.1	0.8	+38	1.0	3.9
	20400				5	2.0	2.9
N			4.3	0.6			
C			3.8	1.1			

488

21+50

S	1.2	37
+5	0.4	45
+12	3.9	10
C	4.1	0.8
N	4.2	0.7

22+00

N	4.0	0.9
C	4.2	0.7
+28	4.1	0.8
+31	1.1	38
+35	0.4	45
S	1.2	37

22+50

S	1.0	39
+3	0.4	45
+8	1.1	38
+12	4.3	0.6
C	4.3	0.6
N	4.2	0.7

TIDE

33

23+00

N	4.2	0.7
C	4.4	0.5
+27	4.3	0.6
+33	0.4	4.5
S	0.6	4.3

23+50

S	0.9	4.0
+7	1.2	37
+12	4.4	0.5
+0	4.6	0.3
N	4.6	0.3

24+00

N	4.4	0.5
C	4.6	0.3
+29	4.3	0.6
+33	1.1	38
S	0.9	4.0

24+50

S	0.9	4.0
+6	1.0	3.9
+11	4.7	0.2
C	4.5	0.4
N	4.4	0.5

25+00

N	4.2	0.7
C	4.5	0.4
+28	4.6	0.3
+32	1.2	3.7
S	1.0	3.9

25+50

S	2.8	2.1
+3	1.1	3.8
+7	0.9	4.0
+12	4.5	0.4
C	4.5	0.4
N	4.1	0.8

TIDE 34

26+00

N	4.1	0.8
C	4.3	0.6
+28	4.8	0.1
+33	0.5	4.4
S	0.7	4.2

26+50

S	1.7	3.2
+1	0.6	4.3
+7	0.6	4.3
+10	4.4	0.5
C	4.3	0.6
N	4.3	0.6

27+00

N	4.3	0.6
C	4.2	0.7
+30	4.4	0.5
+35	0.3	4.4
S	1.1	3.8

4.88

27+50

S	0.6	43
+5	0.5	44
+10	4.4	05
C	4.1	08
N	4.0	09

28+0

N	4.3	06
C	4.0	09
+29	4.1	08
+35	0.3	46
+38	0.4	45
S	1.7	32

28+50

S	1.2	37
+1	0.2	47
+6	0.3	46
+11	3.9	10
C	4.0	09
N	4.3	06

TIDE 35

29+00

N	4.4	05
C	4.0	09
+29	4.1	08
+35	0.3	46
S	0.7	42

29+50

S	0.9	40
+7	0.3	46
+12	3.9	10
C	3.9	10
N	4.1	08

30+00

N	4.3	06
C	3.8	11
+29	4.0	09
+34	0.5	44
+39	0.7	42
S	1.4	35

485

30+50

S	1.2	3.7
+7	0.6	4.3
+12	4.0	0.9
C	3.8	1.1
N	4.2	0.7

31+00

N	4.2	0.7		
C	3.7	1.2		
+27	3.9	1.0		
+33	0.4	4.5		
+35	1.0	3.9		
S	2.3	2.6		
T.P.	5.06	6.13	3.81	1.07

31+50

S	3.0	3.1
+3	1.6	4.5
+7	1.7	4.4
+12	5.2	0.9
C	5.0	1.1

TIDE

36

N

5.6

0.5

32+0

N

5.5

0.6

C

4.9

1.2

+28

5.2

0.7

+33

2.0

4.1

+37

2.0

4.1

S

2.9

3.2

33+50

S

3.7

2.4

+3

1.9

4.2

+7

2.0

4.1

+12

5.2

0.9

C

4.8

1.3

N

5.3

0.8

33+0

N

5.2

0.9

C

4.7

1.4

+28

5.3

0.8

+33

2.1

4.0

+37		2.1	1.0			34+50	
S		3.0	3.1		N		5.0 1.1
	33+42.6 =	ctr 2'4" x 3.9" concrete coils			C		4.3 1.8
S		6.0	0.1		+38		1.7 1.4
+3		2.2	3.9		S		2.7 2.4
+7		2.2	3.9		+5		1.6 4.5
+11		4.6	1.5		-5	35+00	1.5 4.6
C		4.6	1.5		-5		4.4 1.7
N		5.1	0.7		C		4.3 1.8
N		6.8	-0.7		N		4.7 1.4
N	33+95	12.05	-5.92	Top Coping Flow Line		35+50	
N		5.4	0.7		N		4.8 1.3
C		4.5	1.6		C		4.4 1.7
+33		5.1	1.0		+38		4.5 1.6
+38		2.3	3.8		S		4.0 2.1
S		2.0	4.1		+5		1.6 4.5
	34+10					36+00	
S		2.3	3.8		-5		1.4 4.7
+3		5.0	1.1		S		3.8 2.3
C		4.5	1.6		+2		4.8 1.3
N		5.3	0.8		C		4.5 1.6

N		4.8	13
	36+50		
N		4.8	13
C		4.6	15
+38		5.0	11
S		4.4	17
+5		1.9	4.2
	37+0		
-5		2.0	4.1
S		4.4	17
+1		5.1	10
C		4.9	14
N		5.1	10
	37+50		
N		5.1	10
C		4.8	13
+39		5.3	0.8
S		4.9	12
+5		2.1	4.0

	38+00		
-5		2.0	4.1
S		5.4	0.7
C		4.8	1.3
N		5.1	1.0
	38+50		
N		5.1	1.0
C		4.9	1.2
S		5.0	1.1
+5		2.2	3.9
	39+0		
-5		2.2	3.9
S		4.5	1.6
+1		5.2	0.8
C		5.2	0.9
N		5.5	0.6
	39+50		
N		5.5	0.6
C		5.3	0.8
+39		5.0	1.1

613

S			4.3	1.8
+5			1.8	4.3
		40+00		
-5			1.7	4.7
S			4.6	1.5
+1			5.2	0.9
C			5.4	0.7
N			5.6	0.5
T.P.	4.98	5.53	5.58	0.55
		40+50		
N			5.0	0.5
C			4.9	0.6
S			4.5	1.0
+5			0.9	4.6
		41+0		
-6			0.8	4.7
S			4.7	0.8
C			4.9	0.6
N			5.3	0.2

TIDE

39

		41+50		
N			5.1	0.4
C			4.9	0.6
S			4.8	0.7
+6			1.3	4.2
		42+0		
-5			1.4	4.1
S			3.9	1.6
+1			5.0	0.5
C			5.1	0.4
N			5.2	0.3
		42+50		
N			5.4	0.1
C			5.1	0.4
+38			5.3	0.2
S			3.5	2.0
+3			1.7	3.8
		43+0		
-3			1.6	3.9
S			3.7	1.8

553

+2		5.3	0.2
C		5.2	0.3
N		5.4	0.1
	43+50		
N		5.4	0.1
C		5.0	0.5
+38		5.1	0.4
S		4.1	1.4
+4		1.6	3.9
	44+0		
-4		1.3	4.2
S		4.6	0.9
C		4.9	0.6
N		5.2	0.3
	44+50		
N		5.2	0.3
C		4.7	0.8
+38		4.8	0.7
S		3.4	1.1
+3		1.6	3.9

TIDE 40

	45+0		
-4		1.6	3.9
S		4.2	1.3
+2		5.1	0.4
C		4.6	0.9
N		4.9	0.6
	45+50		
N		5.1	0.4
C		4.5	1.0
+38		4.9	0.6
S		3.5	2.0
+3		1.3	4.2
	46+0		
S		5.5	0.0
C		4.4	1.1
N		4.9	0.6
	46+50		
N		4.6	0.9
C		4.3	1.2
S		4.9	0.6

5.53

47+0

S	48	0.7
C	41	1.4
N	43	1.2

47+50

N	42	1.3
C	40	1.5
S	45	1.0

48+00

S	43	1.2
C	38	1.7
N	43	1.2

48+50

N	40	1.5		
C	38	1.7		
S	41	1.4		
T.P.	5.28	6.78	4.03	1.50

So End 6' 50" of S.L. $48+68.8$ on No. $48+78.8$ - 50 = ctr 8' 0" x 4' 6" mo. adv.

S	7.60	- 0.82	Top opening
---	------	--------	-------------

S	13.7	- 6.9	Flow Line
---	------	-------	-----------

TIDE 41

N	6.50	0.28	Top opening
N	13.50	- 6.72	Flow Line
$49+15.8$ on No. $48+82.7$ - No.			
N	5.0	1.7	
C	4.7	2.0	
S	5.1	1.6	

1/8/19 Gregory

Levelson Lytton St
from Tide to Roscarans

LYTTON 42

7.08

858

1.50

T.P. on preceding page

West Line Tide St.

250' W

So.	6.7	1.9
c	6.8	1.8
No.	6.4	2.2

c	4.8	3.8
No.	4.5	4.1
No.	3.5	4.8
c	4.2	4.4
So.	4.0	4.6

50' W

300' W = E.L.

ST 90' wide

No.	6.0	2.6
c	6.4	2.2
So.	6.3	2.3

So.	3.5	5.1
c	3.6	5.0
No.	3.5	5.1

100' W

W.L.

So.	5.8	2.8
c	5.8	2.8
No.	5.5	3.1

No.	1.5	7.1
c	1.7	6.9
So.	1.4	7.2

150' W

T.P. 12.33 2089 0.02 856

No.	4.9	3.7
c	5.3	3.3
So.	5.2	3.4

50' W

So.	4.7	3.9
-----	-----	-----

So.	11.9	9.0
c	12.0	8.9
N	12.2	8.7

2059

100' W

N		
C	10.0	10.9
So	10.1	10.8
	10.3	10.6

150' W

S	8.3	12.6
C	8.0	12.9
N	7.8	13.1

200' W

N	6.0	14.9
C	6.0	14.9
S	6.1	14.8

250' W

S	4.1	16.8
C	4.0	16.9
N	3.8	17.1

300' W =

E.L.

5Y 70' mids

N	1.8	19.1
C	2.0	18.9
S	2.8	18.1

LYTTON 43

T.P. 12.02 32.30 0.61 20.28

W.L.

5T

So. 11.1 21.2

C 11.3 21.0

No. 10.9 21.4

50' W

No. 8.7 23.6

C 8.6 23.7

S 8.7 23.6

100' W

S 5.7 26.6

C 5.9 26.4

N 6.0 26.3

150' W

N 2.8 29.5

C 2.5 29.8

S 2.6 29.7

T.P. 11.42 43.30 0.42 31.88

200' W

S 10.3 33.0

4330

C		10.6	32.7	
N		10.9	32.9	
	250' W			
N		7.5	35.6	
C		7.3	36.0	
S		7.3	36.0	on walk
	300' W = E.L. Roscorans			
S		4.1	39.2	on walk
C		4.3	39.0	
N		4.7	38.6	
ohh BM		1.62	41.68	↓ S/L Roscorans + 1.75 = 41.75

2/14/19 Gregory

GRADES IN ALLEY
BLOCK 27 NEXT PAGE

44

	S	C	N	
1/1.26 th	193.51	193.48 193.95	193.98	188.98 SW 26 + 0 8.23 197.21 3.70 193.51 3.43 202.94
25' W +3.8	196.46 6.48	196.26	196.74	6.20 + 4.1
50' W +0.7	199.4 3.54	199.05 3.47 3.47 202	199.5	3.44 + 0.5
60' W +0.1	199.8 3.14	199.5	200.0	2.94 + 0.7
75' W +0.3	199.3 3.22	199	199.5	3.44 + 0.4
100' W -0.2	198.13 4.81	197.83	198.38	4.56 + 0.7
125' W -0.4	196.96 5.98	196.66	197.26	5.65 + 0.1
150' W 0.0	195.79 7.15	195.49	196.14	6.10 - 0.2
175'				
200				
220	192.5	192.85	193.0	
188.98	188.48 8.41 197.39	188.78 3.64 4.39	188.48 3.91 4.51	188.78 4.63 5.14
193.48	126.46 8.43	126.26 6.03	126.46 5.53	126.46 5.03
202.29	198.13 8.16	197.83 4.26	198.08 3.91	197.96 5.33
	196.96 8.43	196.66 6.03	196.96 5.03	196.66 6.15
	195.79 8.90	195.49 6.15	195.79 6.80	195.49 6.60

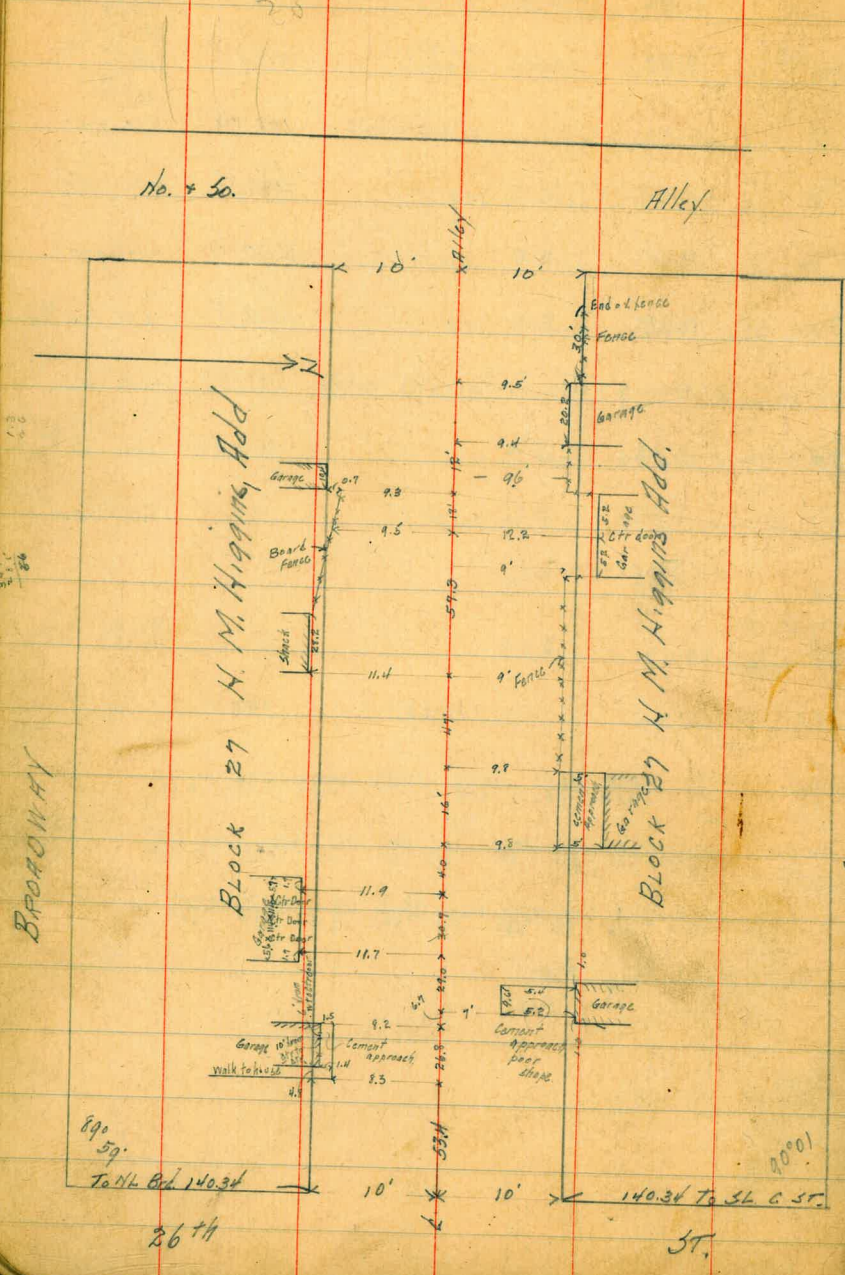
Paving stakes

2/20/19

Gregory
Miller
Shaw

1/29/19 Gregory Miller show.

Location of Improvements in Alley Blk 27 H. M. Higgins Add.



1/29/19

CROSS SECTION OF E+W. Alley Blk 27 Higgins Add

45

on BM	8.18	197.16	188.98	314.26 to 0
				N. L. 26th St. = 0.0
S			3.47	198.69 on cement curb
C			2.6	194.6
N			3.74	194.02 on cement curb
T.P.	18.47	202.74	2.89	194.27
				3' W.
N			4.1	198.6
+4			4.5	
+7			7.5	
C			7.8	194.9
+6			8.0	
+8			3.3	
S			3.0	199.7
				13.5' W.
S			2.6	200.1
+2			2.7	200.0
+4.5			6.1	
C			6.2	196.5
+3			6.1	

202.74

+5	4.6			
+5.1	2.6			S
N	2.3	200.4		+1.8
				+3
N	1.7	201.0		C
+4	1.9			N
+5	2.5			
+8	3.3			N
C	3.4	199.3		+3
+5	3.4			
+8	2.6			N
S	2.3	200.4		+3
				C
S	2.95	199.9	on cement	S
S	2.92	199.8	on cement floor ctr door	S
+1.7	3.07		=edge approach	C
				N
S	3.10	199.6	cement floor ctr door	
+1.7	3.25		edge app.	N

43' W

53.4 W

63' W

74.1' W

46

80.2' W

86.9' W

96.5' W

114.2' W

119.8' W

3.15	199.6	on cement foundation
3.40		edge approach
3.8		
3.5	199.2	
3.2	199.5	
3.18	199.5	cement app.
3.66		=edge - ✓
3.40	199.3	cement app
3.76		=edge ✓
4.43	198.3	
4.8	197.9	
5.3	197.4	
4.5	198.2	
4.9	197.8	

202.74

C		5.6	197.1		
S		6.03	196.7	= cement floor ctr door	
	131.2' W				
S		6.05	196.6	cement floor ctr door	
	142.6' W				
S		5.99	196.7	cement floor ctr door	
	150.6' W				
S		7.0	195.7		
C		7.1	195.6		
N		6.8	195.9	edges app.	
+4.8		6.51		= at door	
	166.6' W				
-4.8		6.62	196.1	= door	
N		6.96	195.98	edges app.	
	178.8' W				
TP	0.98	195.29	8.43	194.31	
N		0.2	195.1		
C		0.9	194.4		
S		1.1	194.2		

47

	223' W				
		1.95	193.0	= elev. of floor track	
		2.6	192.7		
		1.8	193.5		
	241' W				
		3.1	192.2		
		3.5	191.8	ctr man hole	
		3.7	191.6		
	270.9' W				
		5.8	189.5		
		6.0	189.3		
		5.9	189.4		
		4.1	191.2	wood = floor of garage	
	300.9' W				
		7.28	188.0	wood = floor garage	
		7.7	187.6		
		7.7	187.6		
	0.17	187.42	8.04	187.25	

187.42

323' W

S	0.7	186.7
C	0.7	186.7
N	0.1	187.3

350' W

N	3.7	183.7
C	4.0	183.4
	0.9	186.5
	do not use for Top of 6" Xiguring yardage sewer pipe	
+2	5.2	182.2
S	5.6	181.8

372' W

S	8.0	179.4
C	6.5	180.9
+3	4.9	
N	4.8	182.6

393' W

N	5.3	182.1
+5	6.6	
C	6.9	180.5
S	8.1	179.0

48

400 W = E.L. of N+S alley

S	8.7	178.7
C	7.3	180.1
N	6.3	181.1

420' W = W.L. N+S alley

N	5.9	181.5
+5	5.4	
C	6.7	180.7
+7	6.9	
S	8.7	178.7

21' No of No Line of E+W Alley + on W.L. of N+S Alley

	5.2						Floor of garage.
T.P.	10.41	192.94	5.49	182.13			
adj BM.			5.50	187.04	516.25 th D		

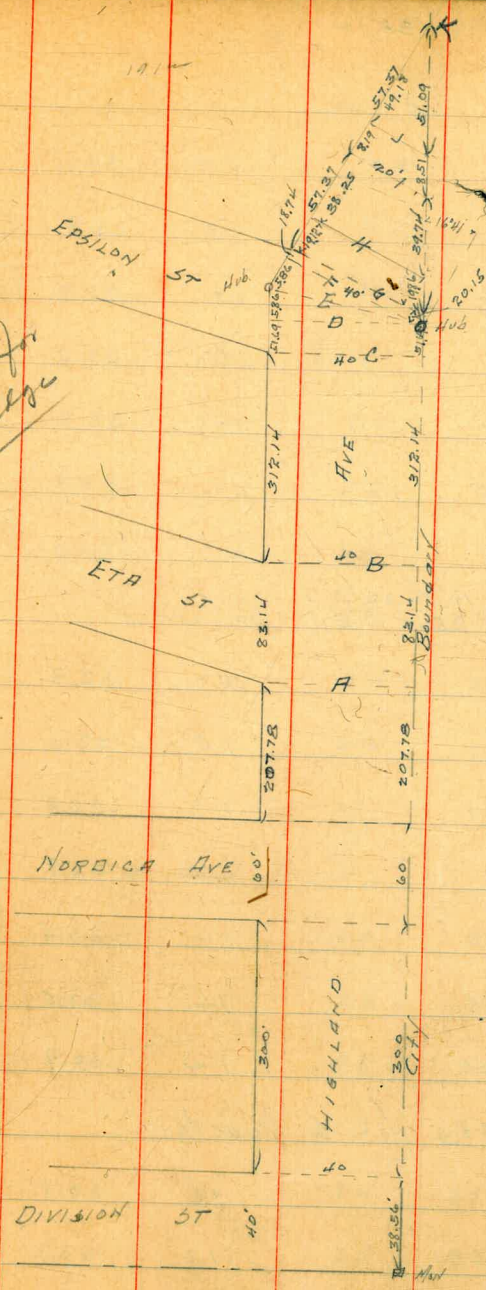
1/30/19 *Gregory Miller Strawn* CROSS SECTION OF
 Highland Avenue 40' wide 10' obs
 End to End.

on B.M	13.05	26.12		13.07	Mon. NW Main + Division
T.P.	13.00	38.73	0.39	25.73	
T.P.	12.66	51.07	0.32	38.41	
T.P.	13.00	63.78	0.29	50.78	
T.P.	11.61	75.37	0.02	63.76	
T.P.	0.48	63.08	12.77	62.60	
T.P.	0.39	50.53	12.94	50.14	
T.P.	0.85	38.54	12.86	37.69	
T.P.	3.05	35.12	6.47	32.07	

SL DIVISION ST.

W		0.5	34.6
cb.		0.7	34.4
1/4		0.9	34.2
+3		1.3	33.8
C		1.3	33.8
1/4		1.0	34.1
d		1.0	34.1
E		0.7	34.4

*See pg 19 for
 the bridge*



35.12

5' No.

E 0.9 34.2

db 1.3 33.8

 $\frac{1}{4}$ 1.3 33.8

C 1.6 33.5

 $\frac{1}{4}$ 1.4 33.7

db 1.2 33.9

W 2.1 33.0

10' No. on W }
8.56 - - E } = So Curb

W 2.2 32.9

db 1.5 33.6

 $\frac{1}{4}$ 1.6 33.5

C 2.2 32.9

1.6 33.5

1.6 33.5

E 1.2 33.9

5' No. = So Quarter

E 1.6 33.5

1.8 33.3

2.0 33.1

35.12

Highland

50 ✓

C

2.2 32.9

2.3 32.8

2.1 33.0

W

2.5 32.6

5' No. = Center

W

2.6 32.5

2.2 32.9

2.2 32.9

C

2.2 32.9

2.4 32.7

2.2 32.9

E

1.8 33.3

5' No. = No. $\frac{1}{4}$

E

2.0 33.1

2.5 32.6

2.7 32.4

C

2.3 32.8

2.4 32.7

2.5 32.6

W

2.7 32.4

3512

5' No. = No Carb

W	3.0	32.1
	2.7	32.4
	2.5	32.6
C	2.5	32.6
	3.0	32.1
	2.9	32.2
E	2.2	32.9

10' No. = N.L. Division St

E	2.6	32.5
	3.3	31.8
	3.3	31.8
C	3.1	32.0
	3.2	31.9
	3.1	32.0
IV	3.4	31.7

20' No. of Division St

W	4.6	30.5
	4.3	30.8
	3.9	31.2

35.12

Highland

51

C	3.9	31.2
	4.0	31.1
cb	4.4	30.7
+5	3.4	31.7
E	3.2	31.9
	50' No.	

E	5.3	29.8
B.M.	5.57	29.55
cb	5.2	29.9
1/4	5.2	29.9
C	5.3	29.8
1/4	5.1	29.7
cb	5.9	29.2
W	6.0	29.1

100' No.

W	7.5	27.6
	7.0	28.1
	6.6	28.5
C	6.7	28.4
	6.5	28.6

 set in Tel. Pole
 E. Side Highland
 60' No. of Division

35.12

		6.5	28.6
E		6.6	28.5
	150' No.		
E		7.3	27.8
		7.3	27.8
		7.4	27.7
C		7.6	27.5
		7.7	27.4
		8.1	27.0
W		8.1	27.0
	200' No.		
W		8.6	26.5
		8.4	26.7
		8.3	26.8
C		8.0	27.1
		7.9	27.2
		7.9	27.2
E		7.8	27.3
	225' No.		
E		7.5	27.3

35.12

Highland

52

		7.9	27.2
		7.9	27.2
C		8.4	26.7
		8.7	26.4
		8.8	26.3
W		9.1	26.0
	253' No.		
W		9.4	25.7
		9.5	25.6
		8.8	26.3
C		6.5	28.6
		6.4	28.7
d		6.3	28.8
+7		6.1	29.0
E		7.7	27.4
	263' No. =		
-10	30. End Bridge Opening	9.6	25.5
-5	or Location of Bridge	9.6	25.5
E		10.7	24.4
+4		9.8	25.3

see page 19
for Location
of Bridge

	35.12		
+5		6.1	29.0
cb		6.0	29.1
1/4		6.0	29.1
C		6.1	29.0
+1		6.1	29.0
+1.2		10.2	24.9
1/4		9.9	25.2
cb		9.9	25.2
W		9.8	25.3
	263.1 No.		
W		9.8	25.3
cb		9.9	25.2
1/4		9.9	25.2
C		10.1	25.0
1/4		10.3	24.8
cb		10.5	24.6
E		10.7	24.4
+10		9.6	25.5
	275' No.		
-10		10.5	24.6

	35.12	Highland	53
E		11.6	23.5
cb		12.6	22.5
1/4		13.0	22.1
C		12.1	23.0
1/4		11.8	23.3
cb		11.8	23.3
W		11.5	23.6
+10		11.6	23.5
	281' No.		
-10		10.5	24.6
W		10.4	24.7
cb		10.2	24.9
1/4		10.3	24.8
C		10.4	24.7
1/4		10.6	24.5
cb		10.8	24.3
E		11.1	24.0
NO		10.4	24.7
	293.0 No.		
-10		11.0	24.1

35.12

ab	6.1	29.0
+6	6.7	28.4
E	8.6	26.5
+5	9.7	25.4
+10	10.3	24.8
	So. 1/6	
-10	10.2	24.9
E	8.7	26.4
+8	6.0	29.1
	6.0	29.1
	6.3	28.8
C	6.4	28.7
	7.2	27.9
	7.5	27.6
W	7.8	27.3
+10	7.7	27.4
	Center Nordica	
-10	7.3	27.8
W	7.3	27.8
	7.1	28.0

35.12

55

	6.6	28.5
C	6.4	28.7
	6.3	28.8
	5.9	29.2
+7	8.6	26.5
E	9.1	26.0
+10	9.9	25.2
	No. Quarter	
-10	9.7	25.4
E	8.9	26.2
+3	8.5	26.6
U	5.8	29.3
	6.1	29.0
C	6.2	28.9
	6.2	28.9
	6.9	28.2
W	6.8	28.3
	No. Curb	
W	6.5	28.6
	6.1	29.0

35.12

	5.9	29.2
C	6.0	29.1
	5.9	29.2
	5.8	29.3
E	8.8	26.3
+10	9.5	25.6

No. Line Nordicq

-10	9.6	25.5
E	9.0	26.1
+4	8.3	26.8
	5.6	29.5
	5.6	29.5
C	5.6	29.5
	5.6	29.5
	5.9	29.2
W	6.1	29.0

24' No.

W	5.2	29.9
	4.9	30.2
	4.9	30.2

35.12

High land

56

C	4.8	30.3
	4.7	30.4
	5.5	29.6
+5	7.1	28.0
E	8.1	27.0
+10	9.4	25.7

59' No.

-15	9.6	25.5
E	7.4	27.7
+2	6.8	28.3
C	3.9	31.2
+3	2.6	32.5
	2.5	32.6
C	2.4	32.7
	2.5	32.6
	2.4	32.7
W	2.1	33.0

91' No.

W	+0.3	35.4
	0.0	35.1

35.12

0.0 35.1

C 0.2 34.9

0.3 34.8

cb 2.7 32.4

+8 6.3 28.8

E 7.0 28.1

+4 9.5 25.6

+15 8.7 26.4

101' No.

-15 8.5 26.6

E 8.2 26.9

2.3 32.8

0.1 35.0

T.P. 11.72 46.81 0.03 35.09 ✓

C 11.4 35.4

10.9 35.9

11.0 35.8

W 10.8 36.0

129' No.

W 9.3 37.5

46.81

Highland 57

9.2 37.6

9.6 37.2

C 9.7 37.1

12.7 34.1

16.4 30.4

+5 19.7 27.1

E 21.2 25.6 ctr wash

+5 19.6 27.2

+15 19.9 26.9

139' No.

-15 19.8 27.0

-6 19.5 27.3

E 21.3 25.5 ctr wash

16.2 30.6

13.0 33.8

C 9.8 37.0

9.0 37.8

8.8 38.0

W 8.9 38.1

46.81

164' No.

W	7.8	39.0	
	8.0	38.8	
	7.9	38.9	
+2	7.7	38.9	
C	9.2	37.6	
	12.6	34.2	
	15.3	31.5	
E	18.7	28.1	
+9	20.9	25.9	ctr wash
+15	19.4	27.7	see sketch p49
	207.78' No. = S.L. ETA ST = Sec. A		
-15	17.2	29.6	
E	14.8	32.0	
+5	13.9	32.9	
	11.4	35.4	
	8.3	38.5	
C	5.6	41.2	
	5.3	41.5	
	5.3	41.5	✓

46.81

Highland Ave 58

W	5.4	41.4	
	1454' No. = So. Curb		
W	4.5	42.3	
	4.4	42.4	
	4.4	42.4	
C	4.3	42.5	
	6.6	40.2	
	9.3	37.5	
+5	11.8	35.0	
E	12.9	33.9	
+15	15.2	31.6	
	13.51' No. of Curb = 1/4		
-15	13.6	33.2	
E	11.2	35.6	
+5	9.9	36.9	
	9.6	39.2	
	4.3	42.5	
+2	3.3	43.5	
C	3.4	43.4	
	3.6	43.2	✓

46.81

3.6 43.2

W

3.0 43.2

13.52 No. of $\frac{1}{4}$ = Ctr

W

2.9 43.9

2.6 44.2

2.4 44.4

C

2.5 44.3

2.2 44.6

4.9 41.9

+4

7.0 39.8

E

8.4 38.4

+15

11.3 35.5

13.51 No. of Ctr. = No. $\frac{1}{4}$

-10

7.3 39.5

E

5.1 41.7

1.5 45.3

1.2 45.6

C

1.2 45.6

1.5 45.3

1.7 45.1

46.81

Highland

59

+5

2.0 44.8

W

1.9 44.9

13.52 No. of $\frac{1}{4}$ = No. Corb.

W

0.8 46.0

0.9 45.9

0.3 46.5

C

0.3 46.5

0.4 46.4

0.6 46.2

E

1.7 45.1

+10

4.1 42.7

13.54 No. of Ctr. = NL. E + A 5T = Sec B

-10

3.1 43.7

E

1.5 45.3

T.P.

12.67

58.07

1.41

NW. cor. of Man

NL E + A

11.5 46.6

10.8 47.3

C

10.6 47.5

10.7 47.4

11.0 47.1

58.07

W 11.3 46.8

25' No. of Sec. B

W 9.5 48.6

9.4 48.7

9.4 48.7

C 9.3 48.8

8.8 49.3

9.4 48.7

E 9.4 48.7

65' No.

E 7.1 51.0

7.3 50.8

6.5 51.6

C 6.7 51.4

6.9 51.2

6.9 51.2

W 7.0 51.1

90' No.

W 5.5 52.6

5.5 52.6 ✓

58.07

Highland

60

54 52.7

54 52.7

56 52.5

6.2 51.9

6.5 51.6

125' No.

4.4 53.7

3.9 54.2

4.1 54.0

3.9 54.2

4.1 54.0

4.2 53.9

W 4.8 53.3

145' No.

4.5 53.6

3.8 54.3

3.8 54.3

3.6 54.5

3.6 54.5

3.9 54.4 ✓

58.07

E 3.5 54.6

180' No

E 3.8 54.3

3.5 54.6

3.7 54.4

C 3.8 54.3

3.9 54.2

4.2 53.9

W 5.3 52.8

200' No

W 4.9 53.2

4.1 54.0

3.8 54.3

C 3.8 54.3

3.7 54.4

3.6 54.5

E 3.8 54.3

250' No

E 3.7 54.4

3.5 54.6

58.07

Highland

61

3.7 54.4

3.7 54.4

3.9 54.2

4.3 53.8

4.7 53.4

312.14' No. = S.L. Epsolon St Sec C

3.4 54.7

4.5 53.6

4.5 53.6

3.9 54.2

3.4 54.7

3.5 54.6

3.3 54.8

2.6 55.5

14.54' No of "C" = 30 Corb.

2.7 55.4

3.4 54.7

3.6 54.5

3.3 54.6

4.2 53.9

58.07

4.9 53.4

4.2 53.9

13.51 No. of Corb = $\frac{50}{16}$

4.2 51.9

5.2 52.9

5.1 53.0

4.6 53.5

3.9 54.2

3.7 54.4

3.8 54.3

3.8 54.6

13.51 No. of $\frac{1}{4}$ = Ctr

4.0 54.1

4.4 53.7

4.4 53.7

4.9 53.2

5.3 52.8

6.1 52.0

8.6 49.5

58.07

62

10.12 No. of Ctr = Sec. D.

10.3 47.8

8.2 49.9

7.2 50.9

6.0 52.1

5.1 53.0

4.8 53.3

4.6 53.5

5.86 No. of "D" on W.
00 - - - - E } = Sec. E.

4.6 53.5

5.0 53.1

5.4 52.7

6.5 51.6

8.1 50.0

9.6 48.5

11.4 46.7

5.86 No. of E on W
00 - - - - E } = Sec. F.

12.0 46.1

10.2 47.9

8.8 49.3

58.07

C			7.1	51.0	
			5.6	52.5	
			5.0	53.1	
E			4.6	53.5	
		Sec G	sec sketch =	N.L. Eps.	
city Bdry			6.1	52.0	
+ 1/2 app. = cb.			6.0	52.1	
1/4			6.3	51.8	
C			9.4	48.7	
			11.9	46.2	
			12.7	45.4	
W			12.4	43.7	
T.P.	363	52.66.	9.04	49.03	spk E side city line tel pole at Dpt
	19.12 No =	Sec H.			
- 15			11.7	41.0	
W			10.8	41.9	
cb			9.4	43.3	
1/4			9.4	45.3	
C			4.9	47.8	
+ 1			2.4	50.3	
1/4			2.3	50.4	

52.66

63

+ 1/2 app = city Bdry		2.1	50.6	= ctr co. road
- 12				
W 1/4 = app. city Bdry	46.44 No. of H = 500.	3.9	48.8	ctr. co. road.
		4.6	48.1	edge - -
W ob		7.6	45.1	
+ 8		12.4	40.3	
W		12.5	40.2	
+ 15		12.7	40.0	
	Pt K.			
- 15		12.2	40.5	
W also city Bdry		12.0	40.7	
	50' No. of Sec. J. on			ctr. of co road
		4.7	48.0	ctr co. road.
	100' No. of J.			
		4.6	48.1	
	150' No. of J.			
		3.8	48.9	

v-section Essex Street from W.L. Park Blvd
 To E.L. of Good's Villa Tract
 Essex 50' wide 7.5' 1/4"

West
 Dunkle
 Evans
 Foleke

311.64

0+75

64

B.M. X Brasspigeon Univ Acad Univ Blvd 301.73

B.M. 6.18 307.91
 T.P. 8.99 316.24 0.66 307.25
 T.P. 2.39 311.64 6.99 309.25

0+0 = W.L. Park Blvd

S 2.14 309.50 ✓
 curb 2.39 309.25
 gutter 3.4 308.2

1/4 2.7 308.7

ctr 2.2 309.4 ✓

1/4 2.2 309.4
 gutter 2.5 309.1
 curb 1.34 310.30

N 1.10 310.54 ✓

0+04 West

N 1.2 310.4 ✓

curb 1.6 310.0

1/4 1.8 309.8

ctr 2.1 309.5 ✓

1/4 2.5 309.1

curb 3.1 308.5

S 3.7 307.9 ✓

S

+8

curb

1/4

ctr

1/4

curb

N

N

curb

1/4

ctr

1/4

curb

S

S

curb

1/4

ctr

1/4

curb

N

5.5

5.5

4.9

4.4

3.8

3.9

3.9

4.3

0+50

6.1

6.2

6.1

6.2

6.3

6.5

6.6

0+75

8.4

8.2

8.3

8.0

8.0

8.1

8.1

306.1

306.1

306.7

307.2

307.8

307.7

307.7

307.3

305.5

305.4

305.5

305.4

305.3

305.1

305.0

303.2

303.4

303.3

303.6

303.6

303.5

303.5

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

✓

		311.64			
		1+0			
N			9.4	302.4	✓
erb			9.9	301.7	
1/4			9.8	301.8	
ctr			10.0	301.6	✓
1/4			10.2	301.4	
erb			9.8	301.8	
S			9.5	302.1	✓
		1+25			
S			11.3	300.3	✓
erb			12.0	299.6	
1/4			12.2	299.4	
ctr			11.9	299.7	✓
1/4			11.9	299.7	
erb			11.9	299.7	
✓			11.9	299.7	✓
T.P.	1.35	300.23	12.76	298.88	

		300.23			65
		1+50			
N			3.3	296.9	✓
erb			2.9	297.3	
1/4			2.8	297.4	
ctr			2.5	297.7	✓
1/4			2.5	297.7	
erb			2.1	298.1	
S			1.0	299.2	✓
		1+75			
S			3.5	296.7	✓
erb			3.7	296.5	
1/4			4.2	296.0	
ctr			4.6	295.6	✓
1/4			4.6	295.6	
erb			4.8	295.4	
N			4.9	295.3	✓
		2+0			
N			6.3	293.9	✓
erb			6.5	293.7	
1/4			6.4	293.8	
ctr			6.3	293.9	✓
1/4			6.2	294.0	
erb			5.8	294.4	
S			5.1	295.1	✓

		300.23 2+25					293.10 3+0			66
S			8.8	291.4	✓	N		5.8	287.3	✓
crh			9.1	291.1		crh		6.1	287.0	
1/4			8.5	291.7		1/4		6.0	287.1	
ctr			9.1	291.1	✓	ctr		5.7	287.4	✓
1/4			8.9	291.3		1/4		5.8	287.3	
crh			8.9	291.3		crh		6.2	286.9	
N			8.5	291.7	✓	+8		6.2	286.9	
						5		7.0	286.1	✓
		2+50								
N			10.0	290.2	✓	5		7.5	285.6	✓
+1			11.0	289.2						
crh			11.3	288.9		crh		7.1	286.0	
1/4			11.3	288.9		1/4		6.8	286.3	
ctr			10.6	289.6	✓	ctr		6.6	286.5	✓
1/4			10.9	289.3		1/4		7.1	286.0	
crh			10.1	290.1		crh		7.1	286.0	
+8			10.4	289.8						
5			11.7	288.5	✓	N		7.1	286.0	✓
		2+75								
5			14.5	285.7	✓					
+3			12.1	288.1						
crh			11.8	288.4						
1/4			11.6	288.6						
ctr			12.3	287.9	✓					
1/4			12.4	287.8						
crh			12.0	288.2						
N			11.9	288.3	✓					
T.P.	4.92	293.10	12.05	288.18						

293.10

3750

N	6.5	286.6	✓
crh	6.6	286.5	
114	7.2	285.9	
CTV	7.5	285.6	✓
114	7.5	285.6	
crh	7.3	285.8	
S	7.4	285.7	✓

3756

S	8.1	285.0	✓
crh	5.9	287.2	
114	4.8	288.3	
CTV	4.6	288.5	✓
114	5.1	288.0	
crh	5.9	287.2	
N	6.1	287.0	✓

293.10

67

3771³⁰ = E.L. Good's Villa Tract

N	3.2	289.9	✓
crh	3.3	289.8	
114	2.8	290.3	
CTV	3.2	289.9	✓
114	3.4	289.7	
crh	4.7	288.4	
S	6.0	287.1	✓

12.85 305.41 0.54 292.56

3.10 307.23 1.28 304.13

B.M. 5.50 301.73

1/9/22

Gregory
Mason
Miller
S. H. W.CROSS SECTION OF
N. S. Alley
Blk 29 N. M. Higgins Add.
from B to A E. of 25thSee 1075-64 for
E & W alley

209.65

207

68

0+69

8.54

205.46

196.92

BP NW
25 + B

E on cement

2.60

207.1

6.69

209.65

7.50

202.96

C

3.2

206.5

S.C.B. Line A St

W = center of garage wood floor

3.5

206.2

E

4.13

205.52 on curb

0+79.5

W

4.79

204.86 ✓ ✓

E = S. End of Cement to Garage

2.37

207.28

S.L.A. ST. = 0+00

0+82

W

4.10

205.55 to Curb
on W. L. Alley

W = center of garage dirt floor

3.6

206.1

C

3.9

205.8

C

3.6

206.1

E

3.75

205.90 on curb

E

3.4

206.3

0+6'

1+07 = center of 17' door on W

E

2.7

207.0

E

4.0

205.7

C

2.9

206.8

C

4.2

205.5

W

3.0

206.7

+8.3 = edge cement apron

4.10

205.55

0+55'

W = garage floor

3.96

205.69

W

3.4

206.3

1+40 = N. L. E & W alley

C

3.1

206.6

W

4.5

205.2

E = N. End of Cement to Garage

2.62

207.03 on cement

C

4.6

205.1

E

4.0

205.7

{ 50' E end of E & W Alley
100' " " " " " " " " }

2.9

206.8

0.8

208.9

209.65

1+50

E	4.6	205.1	
C	5.0	204.7	
+8.6 = edge cement apron	4.96	204.69	on cement
W = center 7' door	4.90	204.75	✓✓

1+60

W = center 8' door dirt floor	5.5	204.2	
C	5.4	204.3	
E	4.7	205.0	
2+05			
E	5.7	204.0	
C	6.5	203.2	
W = center of 8' door dirt floor	6.4	203.3	

2+16

W = center of 8' door dirt floor	6.5	203.2	
----------------------------------	-----	-------	--

2+27

W = center of 8' door dirt floor	6.6	203.1	
C	7.0	202.7	
E	6.0	203.7	

69

2+50

E	6.1	203.6	
+2	6.9	202.8	
C	7.5	202.2	
W	7.3	202.4	

2+97

W	7.6	202.1	
+4	8.6	201.1	
+5	9.2	200.5	
C	9.1	200.6	
+3	9.1	200.6	
E	7.4	202.3	

3+00 = N.L. B 5+

E	8.90	200.75	on cement curb
C	9.25	200.40	✓ parking
W	9.15	200.50	on cement cb.

4/1/22 Gregory
Moore
Miller
Shaw

CROSS SECTION OF
ROSECRANS ST
from the N. Line of
Udal St
to the S. Line of
Russell St
13.67

80' St.

55
231
5368

70

160

7' Mod Udal

N.L. Udal St. 70' wide

W.L.

0.0 13.67

43' E

33 10.4

2' E

0.4 13.3

33'

31 10.6

14' E

0.6 13.1

23

29 10.8

16' E

1.6 12.1

18' E

25 11.2

18' E

2.6 11.1

16' E

26 11.1

23' E

2.6 11.1

W.L.

1.3 12.4

33' E

2.4 11.3

S.L. Udal

17 12.0

43' E

2.4 11.3

2' E

23 11.4

48'

2.5 11.2

14' E

24 11.3

55.65' - W Rail

2.93 10.74

16' E

31 10.6

70' E

2.9 10.8

18' E

41 9.6

80' E

4.0 9.7

23'

44 9.3

to Udal

80' E

4.7 9.0

26

38 9.9

70' E

3.9 9.8

33' E

40 9.7

55.65' - W rail

3.77 9.90

43' E

41 9.6

48' E

3.2 10.3

48' E

41 9.6

55.65

476 8.91

70' E

5.1 8.6

80' E

6.0 7.7

1367

50' S. of S.L. Udall

80' E of W.L.	7.2	6.5
55.65' E - - - = W rail	6.07	7.60
48' E	5.8	7.9
43' E	5.5	8.2
33' E	5.5	8.2
24' E	5.3	8.4
23' E	5.9	7.8
18' E	5.5	8.2
16' E	5.1	8.6
14' E	4.5	9.2
W.L.	4.1	9.6

100' S. of Udall

W.L.	5.5	8.2
1' E	5.9	7.8
14' E	6.3	7.4
16' E	6.8	6.9
18' E	6.8	6.9
22' E	7.5	6.2
23' E	6.8	6.9

33' E

43' E

48' E

55.65' E = W rail

80' E

150' S. of Udall

80' E of W.L. Rosecrans	10.6	3.1
60' E - - -	8.7	5.0
55.65' E - - - = W rail	8.67	5.00
48' E	8.4	5.3
43' E	8.3	5.4
33' E	8.2	5.5
23' E	8.0	5.7
21' E	9.0	4.7
18' E	8.5	5.2
16' E	8.4	5.3
14' E	7.6	6.1
3' E	7.8	5.9
W.L. Rosecrans	6.7	7.0

ROSECRANS

71

6.9 6.8

7.1 6.6

7.3 6.4

7.45 6.22

8.7 5.0

10.6 3.1

8.7 5.0

8.67 5.00

8.4 5.3

8.3 5.4

8.2 5.5

8.0 5.7

9.0 4.7

8.5 5.2

8.4 5.3

7.6 6.1

7.8 5.9

6.7 7.0

1367

200' S. = H.L. Tennyson 70' wide

W.L.	8.8	4.9
2' E	9.1	4.3
16' E	9.3	4.4
18' E	9.2	4.5
22' E	9.9	3.8
23' E	9.2	4.5
33' E	9.3	4.4
43' E	9.2	4.5
48' E	9.4	4.3
55.65' E = W. rail	9.80	3.87
60' E	9.8	3.9
80' E	12.0	1.7

E of Tennyson

80' E of W.L.	12.5	1.2
60'	10.5	3.7
55.65' E = W. rail	10.45	3.22
48' E	10.0	3.7
43' E	9.8	3.9
33' E	9.8	3.9

24' E

23' E

18' E

16' E

3' E

W.L.

set BM

W.L.

3' E

16' E

18' E

23' E

33' E

43' E

48' E

55.65' E = W. rail

65' E

80' E

9.7

10.3

9.8

9.8

10.1

9.2

10.40

9.4

9.9

9.8

10.2

10.5

10.4

10.4

10.5

11.00

11.2

12.8

4.0

3.4

3.9

3.9

3.6

4.5

3.27 7' Non

4.3

3.8

3.9

3.5

3.2

3.3

3.3

3.2

2.7

2.5

0.9

Rosecrans

72

1367

50' S of S.L. Tennyson

80' E	12.7	1.0
60' E	11.7	2.0
55.65' E = W rail	11.65	2.02
48' E	11.2	2.5
43' E	10.9	2.8
33' E	10.9	2.8
23' E	10.9	2.8
18' E	10.8	2.9
16' E	10.6	3.1
11' E	9.7	3.0
W.L.	10.1	3.6

100' S of S.L. Tennyson

W.L.	10.5	3.2
14' E	10.7	3.0
16' E	11.1	2.6
18' E	11.4	2.3
23' E	11.2	2.5
33' E	11.3	2.4
43' E	11.3	2.4

48' E

55.65' E = W rail

60' E

80' E

80' E

60' E

55.65' E = W rail

48' E

43' E

33' E

23' E

18' E

16' E

8' E

W.L. Rosecrans

W.L.

16' E

18' E

Rosecrans

73

11.5 2.2

12.2 1.65

12.0 1.7

13.0 0.7

150' S of S.L. Tennyson

12.9 0.8

12.2 1.5

12.17 1.50

12.0 1.7

11.9 1.8

11.6 2.1

11.5 2.2

11.6 2.1

11.3 2.4

10.6 3.1

10.8 2.9

200' S. = N.L. Sterns St 70 wide

11.1 2.6

11.3 2.4

11.9 1.8

1367

23' E	11.3	2.4
33' E	11.3	2.4
43' E	11.4	2.3
48' E	11.4	2.3
55.65' E = W rail	11.95	1.72
60' E	11.9	1.8
80' E	13.0	0.7

Q Sterne St

80' E	12.9	0.8
60' E	11.6	2.1
55.65' E = W rail	11.66	2.01
48' E	11.4	2.3
43' E	11.1	2.6
33' E	11.0	2.7
23' E	11.4	2.3
18' E	11.9	1.8
16' E	11.1	2.6
2' E	10.7	3.0
W L	10.3	3.4
T.P.	5.88	8.98
	10.57	3.10

7' Non Stop

Rosecrans 74

5L Sterne

8.98

W L	5.22	3.8
14' E	5.6	3.4
16' E	6.2	2.8
18' E	6.4	2.6
22' E	6.8	2.2
23' E	6.1	2.9
33' E	6.0	3.0
43' E	6.0	3.0
48' E	6.2	2.8
55.65' E = W rail	6.63	2.35
69' E	6.9	2.1
73' E	8.0	1.0
80' E	8.0	1.0
	50' S of 5L Sterne	
80' E	7.5	1.5
75' E	7.5	1.5
71' E	6.4	2.6
55.65' E = W rail	6.13	2.85
48' E	5.5	3.5

898

43' E	54	3.6
33 E	54	3.6
45' E	56	3.4
23' E	66	2.4
20 E	55	3.5
18' E	52	3.8
16' E	52	3.8
W.L.	51	3.9
	100' S	
W.L.	35	5.5
2 E	42	4.8
15' E	46	4.4
16' E	52	3.8
18' E	51	3.9
23 E	58	3.2
24' E	51	3.9
33' E	50	4.0
43 E	50	4.0
48 E	53	3.7
55.65 E = W rail	560	3.38

898

Rosecrans 75

67' E	57	3.3
80' E	68	2.2
	150' S	
80' E	67	2.3
60 E	51	3.9
55.65 E = W rail	509	3.89
48' E	47	4.3
43' E	46	4.4
33' E	46	4.4
24' E	46	4.4
23' E	53	3.7
18' E	47	4.3
16' E	42	4.8
2' E	37	5.3
W.L.	31	5.9
	200' S = N.L. Russell 70' wide	
W.L.	25	6.5
2' E	31	5.9
16' E	41	4.9
18' E	45	4.5

23' E	4.8	4.2
25' E	4.4	4.6
33' E	4.3	4.7
43' E	4.2	4.8
48' E	4.4	4.6
55.65' E = W. Rail	4.77	4.21
60' E	4.8	4.2
67' E	4.6	4.4
80' E	6.6	2.4

L Russell

80' E	6.4	2.6
60' E	4.7	4.3
55.65' E = W. Rail	4.73	4.25
48' E	4.3	4.7
43' E	4.1	4.9
33' E	4.2	4.8
33' E	4.3	4.7
18' E	4.3	4.7
16' E	4.0	5.0
W.L.	3.1	5.9
	3.75	5.23 on Mon

S.L. Russell

W.L.	3.3	5.7
16' E	3.8	5.2
18' E	4.3	4.7
33' E	4.7	4.3
25' E	4.0	5.0
33' E	4.2	4.8
43' E	4.0	5.0
48' E	4.1	4.9
55.65' E = W. Rail	4.77	4.21
60' E	4.8	4.2
80' E	6.2	2.8
T.P.	7.33	12.30
	4.01	4.97
	3.81	8.49 = 853 4th SE W. Russell

3/30/25 Sewer Levels on Scott St.
Ingelow to Emerson

Moore
Preston
Walker

SE Rosecrans + Hawley	5.89	12.42	8.53	
T.P.	0.83	+ 4.48	10.77	3.65
0+00 = RW Hub			5.61	-1.13
+50			5.6	-1.12
1			5.6	-1.1
+50			5.7	-1.2
+90			5.7	-1.2
2			7.4	-2.9
+20			8.1	-3.6
+70 = E Hugo			8.91	-4.43
31' W on E Hugo			7.1	-2.6
32' ✓ ✓ ✓			5.1	-0.6
50' ✓ ✓ ✓			5.3	-0.8
100' ✓ ✓ ✓			5.4	-0.9
300' S of Ingelow. E of Scott			9.1	-4.9
350' ✓ ✓ ✓			9.9	-5.4
400' ✓ ✓ ✓			9.8	-5.3
450' ✓ ✓ ✓			9.9	-5.4
500' ✓ ✓ ✓			9.4	-4.9
524			9.6	-5.1

Store Line

on RW Hub

Shore line

+4.48

77

SE Spike	525 S of Ingelow. E of Scott	10.9	-6.4	Slough
	521 ✓ ✓ ✓	10.3	-5.9	✓
	530 ✓ ✓ ✓	9.7	-5.2	
	540 S = E of Goethe	9.5	-5.0	
	50' W of E Scott and Goethe	9.4	-4.9	
	71 ✓ ✓ ✓	9.2	-4.7	
	73 ✓ ✓ ✓	10.4	-5.9	
	79 ✓ ✓ ✓	10.3	-5.8	
	80 ✓ ✓ ✓	9.7	-5.2	
	88 ✓ ✓ ✓	8.5	-4.0	
	103 ✓ ✓ ✓	7.9	-3.4	
	117 ✓ ✓ ✓	6.0	-1.5	Shore line
	150 ✓ ✓ ✓	6.0	-1.5	
	200 ✓ ✓ ✓	5.9	-1.4	
	575' S of E of Ingelow and Scott	9.2	-4.7	
	615' ✓ ✓ ✓	9.8	-5.3	
	650' ✓ ✓ ✓	9.2	-4.7	
	700' ✓ ✓ ✓	8.5	-4.0	
	750' ✓ ✓ ✓	8.3	-3.8	
	810' ✓ = E of Fenelon	8.10	-3.6	on RW Hub

15'	W of E of Scott on Favelon	6.4	-1.9	Store line
50'	✓ ✓ ✓ ✓	6.3	-1.8	
100'	✓ ✓ ✓ ✓	5.7	-1.2	
842'	S of E of Ingham on E of Scott	6.8	-2.3	Store line
852'	✓ ✓ ✓ ✓	6.4	-1.9	
865'	✓ ✓ ✓ ✓	6.1	-1.6	
900'	✓ ✓ ✓ ✓	6.2	1.7	
950'	✓ ✓ ✓ ✓	5.7	1.2	
1000'	✓ ✓ ✓ ✓	5.1	0.6	
1050'	✓ ✓ ✓ ✓	4.5	0.0	
1080'	✓ = E of Emerson	4.03	+0.45	on Hub

Note - Below store line is all soft mud.

B.M. 288.95 NEBP
Lauralt
Park Blvd

9

UPAS



Park Blvd

Balboa Park

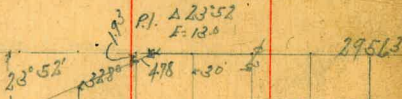


4.500
28
052

3.5150
28
052

Walker
Bliss
Dobert
5-19-31

SURVEY PARCEL LAND
IN BALBOA PARK
FOR PROPOSED LITTLE THEATRE.



Dirt Road

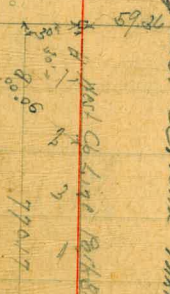
See next page

WEST 6th line Park Blvd.

Proposed site

Proposed
Large Rose Garden
Balboa Park

North Carb Call + Coloy



258.85

90° 00'

315.30

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

10'

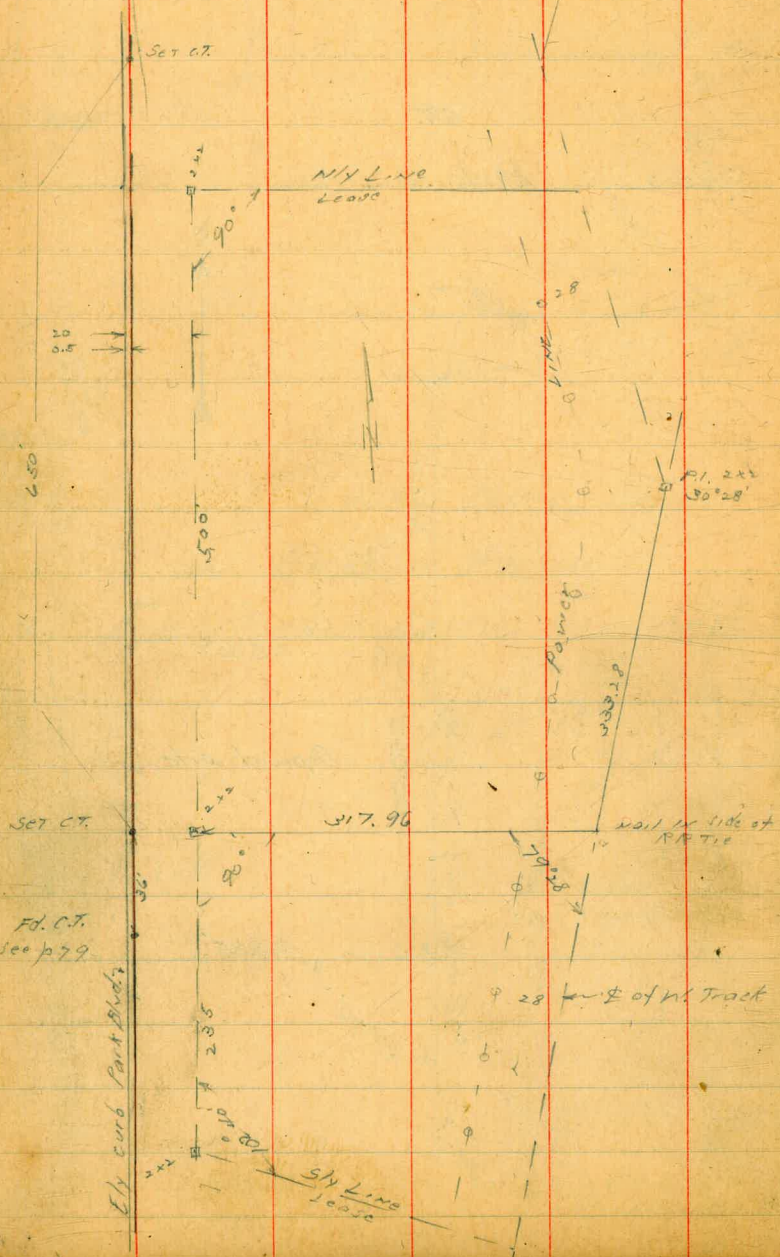
10'

10'

Prop. Site of Indexed
2151K.
FM. Legion Wm. T. 1, Bly
Moore
1-16-37

See Dwg. No
5442-L

Call Custodial
80



49 18
2 11 18
30°28'

317.96

24.00
 1+20 +64
 1+50 +39
 1+40 +49
 1+12 +01
 1+02 +01
 0+70 +59
 0+35 +44
 11
 0+20

5837
 430
 5467

CITY LIMITS NW MON
 13.07

3rd block

+25
 +65
 90
 1+21
 1+60
 1+80
 2+00
 2+50
 2+00

475
 168
 4007
 4168
 177
 39.91

0+20

Chk Levels

41.75 L. H. Ross
 +1.66
 43.41
 -11.46
 31.95
 + 37
 35.32
 -11.98
 20.34
 + 0.67
 21.01
 -12.92
 8.09
 + .41
 8.50
 - 4.96
 1.54
 + 3.75
 5.32
 - 2.82
 2.50
 + 2.23
 4.73
 - 3.27
 1.46
 + 3.27
 4.73
 3.08
 1.65

188.98
 76.2
 196.60
 208
 193.62
 18.79
 202.41

314.68
 294.68
 147.32

47.152
 47.00
 7

358 on rail
 HUGO
 Goethe
 Ferrelan

738
 113.43
 193.96
 121.21
 120.27
 80.07
 34.24
 193.75
 192.50
 192.2
 150
 221
 37.5
 67.1
 104.0
 219
 219
 6.602
 1.200
 200.311
 1.7
 107.11

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

T 53W 3 AM