1037

FIELD BOOK

1878

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

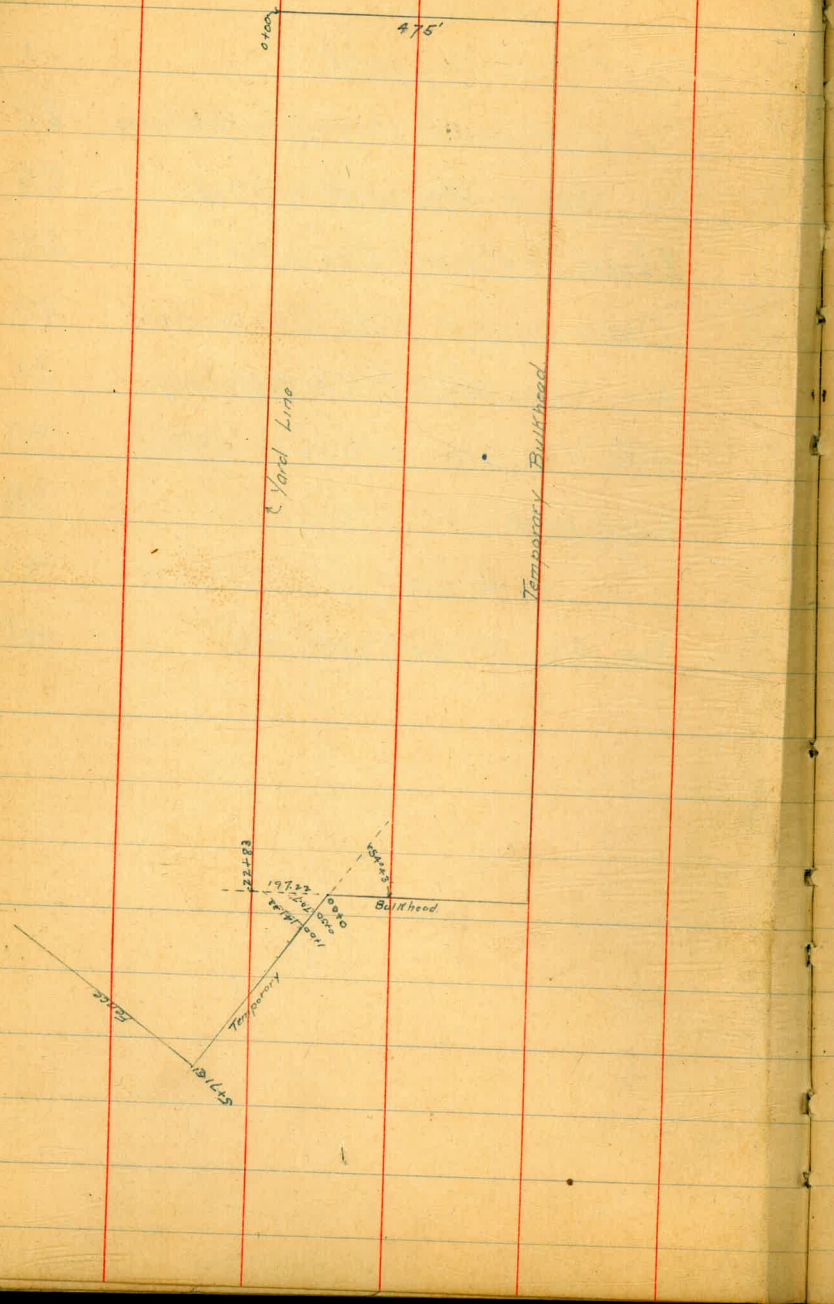
Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

INDEX



Cross Sections of Pacific Marine & Construction Co's Ship Yard Site { Dario Mancock Byers

Yard grade 9.67

	0.17	11.11		10.94 BM. Top MH - Foot 32d St
	6.50	16.28	1.33	9.78 C I.S.E Cor. out house platform Sta 4+50
	4.02	14.71	5.59	10.69
		5+71.5 = Fence Line		
0+00 = bl'k hd			7.2	7.5
+50			7.3	7.4
1+00			7.0	7.7
+50			6.7	8.0
2+00			5.8	8.9
+50			5.6	9.1
+79			5.0	9.7
3+00			4.8	9.9
+50			4.2	10.5
	5+50			
0+00 = bl'k hd			7.5	7.2
+50			6.6	8.1
1+00			7.1	7.6
+50			6.1	8.6
2+00			5.6	9.1
+03			5.0	9.7

14.71

5+50

2+06	5.8	8.9 ✓
+50	6.2	8.5 ✓
3+00	5.6	9.1 ✓
+27	5.0	9.7 ✓

5+00

0+00 - 61K hd	8.6	6.1 ✓
+07	8.2	6.5 ✓
+10	7.3	7.4 ✓
+50	7.0	7.7 ✓
1+00	6.2	8.5 ✓
+50	5.6	9.1 ✓
+80	6.2	8.5 ✓
2+00	3.8	10.9 ✓
+26	3.9	10.8 ✓
+40	5.1	9.6 ✓
+50	5.1	10.6 ✓
+80	5.0	9.7 ✓

4+50

0+00 - 61K hd	9.1	5.6 ✓
+14	8.7	6.0 ✓
+25	6.3	8.4 ✓
+37	7.7	7.0 ✓
+50	7.7	7.0 ✓
1+00	6.8	7.9 ✓
+50	6.3	8.4 ✓
+56	4.0	10.7 ✓
2+00	3.2	11.5 ✓
+12	5.5	9.2 ✓
+16	5.0	9.7 ✓

4+38

1+50	6.3	8.4 ✓
2+00	5.4	9.3 ✓
+16	5.0	9.7 ✓

4+00

0+00 - 61K hd	10.2	4.5 ✓
+36	8.1	6.6 ✓
+50	7.3	7.4 ✓

1.47

4+00

1+00	6.4	8.3 ✓
+50	5.3	9.4 ✓
+60	5.0	9.7 ✓

3+50

0+00 = 61Khd	10.8	3.9 ✓
+50	8.7	6.0 ✓
+67	7.0	7.7 ✓
1+00	5.6	9.1 ✓
+38	5.0	9.7 ✓

3+00

0+00 = 61Khd	11.2	3.5 ✓
+50	9.6	5.1 ✓
+82	7.8	6.9 ✓
+89	5.8	8.9 ✓
1+00	5.8	8.9 ✓
+50	5.0	9.7 ✓

2+50

0+00 = 61Khd	11.6	3.2 ✓
+50	10.6	4.1 ✓
1+00	8.7	6.5 ✓
+12	7.8	6.9 ✓
+15	5.7	9.0 ✓
+50	5.4	9.3 ✓
+62	5.0	9.7 ✓
T.P 1.47	12.16	4.0 ✓ 10.69

2+00

0+00 = 61Khd	9.7	3.0 ✓
+50	8.9	3.3 ✓
1+00	7.8	4.4 ✓
+49	4.7	7.5 ✓
+53	3.1	10.1 ✓
+75	1.5	10.7 ✓

12.16

1+50

0+00 = 61Khd		9.6	2.6	✓
+50		9.5	2.7	✓
1+00		8.8	3.4	✓
+50		7.2	5.0	✓
+74		5.2	7.0	✓
+80		4.0	8.2	✓
+87		1.5	10.7	✓
	1+00			
0+00 = 61Khd		9.7	2.5	✓
+50		9.6	2.6	✓
1+00		9.5	2.7	✓
+41.33 = Int with Sta 22+83 on Yard Line		8.7	3.5	✓
	0+50			
0+00 = 61Khd		9.7	2.5	✓
+50		9.6	2.6	✓
+70.2 = Int with Sta 22+83 on Yard Line		9.6	2.6	✓

	0.56	10.34	2.38	9.78
		22+83		
31'N.			0.7	9.6 ✓
25'.			3.3	7.0 ✓
0+00 = Yard Line			5.6	4.7 ✓
+50			7.3	3.0 ✓
1+00			7.8	2.5 ✓
+50			8.0	2.3 ✓
+97.22			8.0	2.3 ✓
2+00			8.0	2.3 ✓
+50			8.2	2.1 ✓
3+00			8.4	1.9 ✓
+50			8.5	1.8 ✓
4+00			8.6	1.7 ✓
+75 = 61Khd			8.7	1.6 ✓

10.34

22+50

4+75=61K Hd	8.8	1.5 ✓
4+00	8.6	1.7 ✓
+50	8.6	1.7 ✓
3+00	8.3	2.0 ✓
+50	8.3	2.0 ✓
2+00	8.2	2.1 ✓
+50	8.2	2.1 ✓
1+00	7.8	2.5 ✓
+50	7.3	3.0 ✓
0+00 Yard Line	5.1	5.2 ✓
+15	3.2	7.1 ✓
+19.5	0.7	9.6 ✓

22+00

+36	0.7	9.6 ✓
+31	3.3	7.0 ✓
0+00 Yard Line	5.7	4.6 ✓
+50	7.4	2.9 ✓
1+00	7.8	2.5 ✓
+50	8.7	2.1 ✓

22+00

2+00	8.2	2.1 ✓
+50	8.4	1.9 ✓
3+00	8.4	1.9 ✓
+50	8.5	1.8 ✓
4+00	8.7	1.6 ✓
+75=61K Hd	9.0	1.3 ✓

21+50

4+75=61K Hd	8.8	1.5 ✓
4+00	8.7	1.6 ✓
+50	8.6	1.7 ✓
3+00	8.4	1.9 ✓
+50	8.4	1.9 ✓
2+00	8.2	2.1 ✓
+50	8.2	2.1 ✓
1+00	5.0	2.3 ✓
+50	7.5	2.8 ✓
0+00=Yard Line	5.9	4.4 ✓
+40	3.3	7.0 ✓
+43	2.6	7.7 ✓
+45.5	0.7	9.6 ✓

10-3-W

2+00

+56	0.7	9.6 ✓
+47	2.9	7.4 ✓
0+00 = Yard Line	5.9	4.4 ✓
+50	7.4	2.9 ✓
1+00	7.9	2.4 ✓
+50	8.1	2.2 ✓
2+00	8.2	2.1 ✓
+50	8.4	1.9 ✓
3+00	8.5	1.8 ✓
+50	8.6	1.7 ✓
4+00	8.8	1.5 ✓
+75= blind	9.0	1.3 ✓

20+50

4+75 blind	8.9	1.4 ✓
4+00	8.8	1.5 ✓
+50	8.7	1.6 ✓
3+00	8.5	1.8 ✓
+50	8.3	2.0 ✓
2+00	8.2	2.1 ✓

20+50

+50	8.1	2.2 ✓
1+00	8.0	2.3 ✓
+50	7.5	2.8 ✓
0+00 = Yard Line	6.0	4.3 ✓
+50	7.7	7.6 ✓
+56	2.0	8.3 ✓
+58.5	0.7	9.6 ✓

20+00

+58	0.7	9.6 ✓
+55	2.5	7.8 ✓
+50	3.2	7.1 ✓
0+00	6.1	4.2 ✓
+50	7.5	2.8 ✓
1+00	8.1	2.2 ✓
+50	8.2	2.1 ✓
2+00	8.3	2.0 ✓
+50	8.4	2.1 ✓
3+00	8.7	1.6 ✓
+50	8.8	1.5 ✓

		10.3V			
		20+00			
4+00			8.9	1.4	✓
+75 = 61K hd			8.8	1.5	✓
		19+50			
4+75 = 61K hd			9.0	1.3	✓
4+00			9.0	1.3	✓
+50			8.8	1.5	✓
3+00			8.6	1.7	✓
+50			8.4	1.9	✓
2+00			8.2	2.1	✓
+50			8.2	2.1	✓
1+00			8.0	2.3	✓
+50			7.6	2.7	✓
0+00 = Yard Line			6.2	4.1	✓
+50			3.3	7.0	✓
+56			2.5	7.8	✓
+58.5			0.7	9.6	✓
T.P	16Y	11.4 0	0.56	9.78	✓

		11.4 0 ✓			
		19+00			
+57.5			1.7	9.7	✓
+53			4.2	7.2	✓
+50			4.3	7.1	✓
0+00 = Yard Line			7.2	4.2	✓
+50			8.8	2.6	✓
1+00			9.1	2.3	✓
+50			9.3	2.1	✓
2+00			9.3	2.1	✓
+50			9.6	1.8	✓
3+00			9.7	1.7	✓
+50			9.9	1.5	✓
4+00			10.0	1.4	✓
+75 = 61K hd.			10.0	1.4	✓
		18+50			
4+75 = 61K hd.			10.1	1.3	✓
4+00			10.0	1.4	✓
+50			9.9	1.5	✓
3+00			9.7	1.7	✓
+50			9.6	1.8	✓

	11.40		
	18+50		
2+00	9.4	2.0	✓
+50	9.3	2.1	✓
1+00	9.1	2.3	✓
+50	8.8	2.6	✓
0+00 = Yard Line	7.4	4.0	✓
+50	4.3	7.1	✓
+54	3.6	7.8	✓
+56	3.3	8.1	✓
+56	1.7	9.7	✓
	18+00		
+54.5	1.7	9.7	✓
+50	4.0	7.4	✓
0+00: Yard Line	7.5	3.9	✓
+50	8.7	2.7	✓
1+00	9.3	2.1	✓
+50	9.3	2.1	✓
2+00	9.4	2.0	✓
+50	9.7	1.7	✓
3+00	9.8	1.6	✓

+50	9.9	1.5	✓
4+00	10.1	1.3	✓
+75 blkhd.	10.1	1.3	✓
	17+50		
A+75 blkhd.	10.2	1.2	✓
4+00	10.0	1.4	✓
+50	9.9	1.5	✓
3+00	9.8	1.6	✓
+50	9.6	1.8	✓
2+00	9.4	2.0	✓
+50	9.3	2.1	✓
1+00	9.2	2.2	✓
+50	8.8	2.6	✓
0+00 = Yard Line	7.6	3.8	✓
+50	4.2	7.2	✓
+57	1.7	9.7	✓

11:40 ✓

17+00

+59	1.7	9.7	✓
+55	4.2	7.2	✓
+50	4.6	6.8	✓
0+00 - Yard Line	7.7	3.7	✓
+50	8.8	2.6	✓
1+00	9.1	2.3	✓
+50	9.3	2.1	✓
2+00	9.4	2.0	✓
+50	9.7	1.7	✓
3+00	9.8	1.6	✓
+50	10.0	1.4	✓
4+00	10.1	1.3	✓
+75 - 4 WKhd	10.2	1.2	✓

16+50

4+75 - 6 WKhd	10.2	1.2	✓
4+00	10.2	1.2	✓
+50	10.0	1.4	✓
3+00	9.8	1.6	✓
+50	9.7	1.7	✓

2+00	9.4	2.0	✓
+50	9.3	2.1	✓
1+00	9.1	2.3	✓
+50	8.7	2.7	✓
0+00 - Yard Line	7.3	4.1	✓
+50	4.9	6.5	✓
+60	4.2	7.2	✓
+62	1.7	9.7	✓

16+00

+74	1.7	9.7	✓
+73	3.7	7.7	✓
+64	4.7	6.7	✓
+50	5.4	6.0	✓
0+00 - Yard Line	7.3	4.1	✓
+50	8.7	2.7	✓
1+00	9.2	2.2	✓
+50	9.3	2.1	✓
2+00	9.4	2.0	✓
+50	9.6	1.8	✓

		11.40			
		16+00			
3+00			9.7	1.7	✓
+50			9.9	1.5	✓
4+00			10.2	1.2	✓
+75 - 61K hd			10.2	1.2	✓
		15+50			
4+75 - 61K hd			10.4	1.0	✓
4+00			10.0	1.4	✓
+50			9.8	1.6	✓
3+00			9.7	1.7	✓
+50			9.5	1.9	✓
2+00			9.4	2.0	✓
+50			9.2	2.2	✓
1+00			9.1	2.3	✓
+50			8.8	2.6	✓
0+00 - Yard Line			7.6	3.8	✓
+50			5.1	6.3	✓
+60			4.1	7.3	✓
+67			1.7	9.7	✓
			0.46	10.9+ ✓	1094 BM. M.H.
	1.77	9.80 ✓	3.37	8.03 on test 16 Su M.H.	

		9.80 ✓			
		15+00			
+64.5			01	9.7	✓
+62			1.6	8.2	✓
+50			3.6	6.2	✓
0+00 - Yard Line			6.2	3.6	✓
+50			7.2	2.6	✓
1+00			7.5	2.3	✓
+50			7.5	2.3	✓
2+00			7.6	2.2	✓
+50			7.8	2.0	✓
3+00			8.1	1.7	✓
+50			8.4	1.4	✓
4+00			8.7	1.1	✓
+75 - 61K hd			9.2	0.6	✓
		14+50			
1+75 - 61K hd			9.5	0.3	✓
4+00			8.9	0.9	✓
+50			8.2	1.6	✓
3+00			8.0	1.8	✓
+50			7.9	1.9	✓

	980 ✓		
	14+50		
2+00	7.7	2.1	✓
+50	7.6	2.2	✓
1+00	7.5	2.3	✓
+50	7.1	2.7	✓
0+00 Yard Line	6.4	3.4	✓
+50	3.7	6.1	✓
+65	3.0	7.4	✓
+69	0.1	9.7	✓
	14+00		
+60	0.1	9.7	✓
+59	3.2	6.6	✓
+50	3.8	6.0	✓
0+00 Yard Line	6.1	3.7	✓
+50	7.2	2.6	✓
1+00	7.4	2.4	✓
+50	7.5	2.3	✓
2+00	7.7	2.1	✓
+50	7.9	1.9	✓
3+00	8.1	1.7	✓

+50	8.6	1.7	✓
4+00	9.0	0.8	✓
+75=61 Kbd.	9.6	0.7	✓
	13+50		
4+75=61 Kbd	9.7	0.1	✓
4+00	9.0	0.8	✓
+50	8.5	1.3	✓
3+00	8.2	1.6	✓
+50	8.1	1.7	✓
2+00	7.8	2.0	✓
+50	7.6	2.2	✓
1+00	7.5	2.3	✓
+50	7.2	2.6	✓
0+00 Yard Line	6.1	3.7	✓
+50	3.9	5.9	✓
+68	2.6	7.2	✓
+72.5	0.1	9.7	✓

9.80 V

13+00

+67		0.1	9.7
+67		2.8	7.0
+50		4.0	5.8
0+00 = Yard Line		6.4	3.4
+50		7.1	2.7
1+00		7.5	2.3
+50		7.7	2.1
2+00		7.9	1.9
+50		8.1	1.7
3+00		8.3	1.5
+50		8.7	1.1
4+00		8.9	0.9
+75 = 61Khd		9.8	0.0
	12+50		
4+75 61Khd		9.7	0.1
4+00		9.0	0.8
+50		8.7	1.1
3+00		8.3	1.5
+50		8.1	1.7
2+00		7.9	1.9
+50		7.6	2.2
1+00		7.4	2.4
+50		7.1	2.7
0+00 = Yard Line		6.1	3.7
+50		3.8	6.0
+57		3.6	6.2
+57		0.1	9.7
	12+00		
+30		0.1	9.7
+30		4.8	5.0
0+00		6.3	3.5
+50		7.3	2.5
1		7.7	2.1
+50		7.7	2.1
2+00		7.9	1.9
+50		8.1	1.7
3+00		8.4	1.4
+50		8.5	1.3
4+00		9.3	0.5
+75 = 61Khd		9.7	0.1

9.80 ✓

11+50

4+75 = 61 Kind	9.7	0.1
4+00	9.5	0.3
+50	8.8	1.0
3+00	8.0	1.8
+50	8.1	1.7
2+00	7.9	1.9
+50	7.7	2.1
1+00	7.4	2.4
+50	7.2	2.5
0+00 = Yard Line	6.2	3.6
+50	4.2	5.6
+58.5	3.5	6.3
+60	0.1	9.7

11+00

+68.5	0.1	9.7
+64.5	3.4	6.4
+50	4.2	5.6
0+00 = Yard Line	6.3	3.5
+50	7.2	2.5

1+00	7.6	2.2
+50	7.8	2.0
2+00	7.9	1.9
+50	8.0	1.8
3+00	8.3	1.5
+50	8.9	0.9
4+00	9.4	0.4
+75 = 61 Kind	9.5	0.3

10+50

4+75	9.8	0.0
4+00	9.1	0.7
+50	8.6	1.2
3+00	8.4	1.4
+50	8.0	1.8
2+00	7.9	1.9
+50	7.7	2.1
1+00	7.6	2.2
+50	7.2	2.6
0+00	6.3	3.5
+50	4.2	5.6
+54	4.1	5.7
+59.5	0.1	9.7

9.80 ✓

10+00

+70	0.1	9.7
+70	3.2	6.6
+50	4.2	5.6
0+00: Yard Line	6.3	3.5
+50	7.3	2.5
1	7.5	2.3
+50	7.7	2.1
2	8.0	1.8
+50	8.0	1.8
3	8.3	1.5
+50	8.9	0.9
4	9.2	0.6
+78: billhd	9.7	0.1

9+50

4+75: billhd	9.6	0.2
4	9.2	0.6
+50	8.7	1.1
3	8.0	1.8
+50	8.2	1.6

2	8.0	1.8
+50	7.7	2.1
1	7.6	2.2
+50	7.4	2.4
0+00: Yard Line	6.4	3.4
+50	4.4	5.4
+72.5	2.4	7.4
+76	0.1	9.7

9+00

+66.5	0.1	9.7
+61	3.7	6.1
+50	4.4	5.4
0+00: Yard Line	6.6	3.3
+50	7.4	2.4
1	7.6	2.2
+50	8.0	1.8
2	8.0	1.8
+50	8.2	1.6
3	8.4	1.4

		9.80 ✓		
3+50			8.8	1.0
4			9.1	0.7
+75 = 61 Khd.			9.7	0.1
		8+50		
4+75			9.8	0.0
4			9.3	0.5
+50			8.7	1.1
3			8.3	1.5
+50			8.2	1.6
2			8.1	1.7
+50			7.8	2.0
1			7.5	2.3
+50			7.3	2.5
0+00			6.1	3.7
+50			4.4	5.4
+71			3.2	6.6
+71			0.1	9.7
T.P.	4.00	9.89 ✓	3.91	5.89 ✓

		9.89 ✓		
		8+00		
+81			0.2	9.7
+77			2.8	7.1
+50			4.6	5.3
0+00 = Yard Line			6.5	3.4
+50			7.4	2.5
1			7.6	2.3
+50			8.0	1.9
2			8.2	1.7
+50			8.3	1.6
3			8.5	1.4
+50			9.0	0.9
4			9.6	0.3
+75 = 61 Khd			10.2	-0.3
		7+50		
4+75 = 61 Khd.			10.2	-0.3
4			9.8	0.1
+50			9.3	0.6
3			8.8	1.1
+50			8.3	1.6

9.89

7+50

2+00	8.1	1.8
+50	7.9	2.0
1	7.6	2.3
+50	7.4	2.5
0+00 = Yard Line	6.4	3.5
+50	4.4	5.5
+67.5	3.4	6.5
+71	0.2	9.7
7+00		
+67	0.2	9.7
+64	3.3	6.6
+50	4.2	5.7
0+00 Yard Line	6.3	3.6
+50	7.5	2.4
1	7.6	2.3
+50	8.0	1.9
2	8.1	1.8
+50	8.0	1.9
3	8.1	1.7

3+50	9.6	0.3
4	10.0	-0.1
+75 = blkhd	10.1	-0.2
6+50		
4+75	10.3	-0.4
4	10.0	-0.1
+50	9.1	0.8
3	8.3	1.6
+50	8.2	1.7
2	8.0	1.9
+50	7.9	2.0
1	7.7	2.2
+50	7.2	2.7
0+00 Yard Line	6.3	3.6
+50	4.1	5.8
+52	0.2	9.7

9.89

6+00

+40	0.7	9.7
+40	3.9	6.0
0+00 = Yard Line	5.9	4.0
+50	7.2	2.7
1	7.5	2.4
+50	7.8	2.1
2	8.1	1.8
+50	8.2	1.6
3	8.3	1.6
+50	8.7	1.7
4	9.8	0.1
+75	10.1	-0.2

5+50

4+75	10.1	-0.2
5	9.7	0.2
+50	9.0	0.9
3	8.3	1.6
+50	8.3	1.6
2	8.1	1.8

+50	7.8	2.1
1	7.5	2.4
+50	7.1	2.8
0+00	5.8	4.1
+17.5	4.9	5.0
+22.5	0.2	9.7

5+00

+20	0.2	9.7
+27	4.1	5.8
0+00	5.5	4.4
+50	7.1	2.8
1	7.5	2.4
+50	7.8	2.1
2	7.9	2.0
+50	8.2	1.7
3	8.4	1.5
+50	8.9	1.0
4	9.1	0.8
+75	9.9	0.0

9.89 ✓

4+50

4+75 - 6 Kind	10.1	-0.2
4	9.2	0.7
+50	8.9	1.0
3	8.4	1.5
+50	8.2	1.7
2	7.9	2.0
+50	7.8	2.1
1	7.6	2.3
+50	7.1	2.8
0+00	5.6	4.3
+21	4.0	5.9
+26	0.2	9.7
4+00		
+48	0.2	9.7
+48.5	2.8	7.1
0+00	5.6	4.3
+50	7.1	2.8
1	7.6	2.3
+50	7.8	2.1

2	8.1	1.8
+50	8.2	1.7
3	8.5	1.4
+50	8.7	1.2
4	9.2	0.7
+75	10.0	-0.1
3+50		
4+75	9.8	0.1
↓	8.9	1.0
+50	8.7	1.2
3	8.5	1.4
+50	8.3	1.6
2	8.0	1.9
+50	7.7	2.2
1	7.5	2.4
+50	7.0	2.9
0+00	5.8	4.1
+34	3.6	6.3
+37	0.2	9.7

		9.89 ✓								
		3+00								
{+47.5			0.2	9.7	+50			7.8	2.1	
{+47.5			2.4	7.5	1			7.6	2.3	
0+00			5.5	4.4	+50			7.3	2.6	
+50			7.2	2.7	0+00			5.8	4.1	
1			7.6	2.3	+24			4.1	5.8	
+50			7.8	2.1	+26			0.2	9.7	
✓			8.0	1.9	T.P	4.93	10.37 ✓	4.45	5.44 ✓ Con. Mon Sta 2+15 on high point.	
+50			8.2	1.7			2+00			
3			8.4	1.5	+51			0.7	9.7	
+50			8.7	1.2	+48			3.0	7.4	
4			8.8	1.1	0+00			6.0	4.4	
+75			9.6	0.3	+50			7.7	2.7	
		2+50			1			8.2	2.2	
4+75			9.5	0.4	+50			8.4	2.0	
4			9.0	0.9	✓			8.7	1.7	
+50			8.6	1.3	+50			8.9	1.5	
3			8.4	1.5	3			9.1	1.3	
+50			8.1	1.8	+50			9.4	1.0	
2			8.0	1.9	4			9.6	0.8	
					+75			10.1	0.3	

10:37

1+50

H+75	10.1	0.3
4	9.6	0.8
+50	9.2	1.2
3	9.0	1.4
+50	8.8	1.6
2	8.6	1.8
+50	8.2	2.2
1	8.2	2.2
+50	7.8	2.6
0+00	6.3	4.1
+50	4.4	6.0
+60	3.3	7.1
+65	0.7	9.7

1+00

+87	0.7	9.7
+87	1.4	9.0
+50	5.5	4.9
0+00	7.0	3.4
+50	8.0	2.4
1	8.2	2.2
+50	8.3	2.1
2	8.6	1.8
+50	8.8	1.6
3	8.9	1.5
+50	9.1	1.3
4	9.6	0.8
+75	9.7	0.7

0+50

H+75	9.7	0.7
4	9.6	0.8
+50	9.2	1.2
3	9.0	1.4
+50	8.8	1.6
2	8.7	1.7
+50	8.5	1.9
1	8.2	2.2
+50	8.1	2.3
0+00	7.4	3.0

10.37

0+50

+50	6.30	4.1
1+00	28	7.6
+03	0.7	9.7

0+00

1+26	0.7	9.7
1+21	29	7.5
1+00	4.3	6.1
+60	6.9	3.5
0+00 Yard Line	7.7	2.7
+50	7.9	2.5
1	8.3	2.1
+50	8.4	2.0
2	8.5	1.9
+50	8.8	1.6
3	9.0	1.4
+50	9.1	1.3
4	9.5	0.9
+75	9.7	0.7

1"/30/s Gregory Shaw

CROSS SECTION OF BANCROFT ST

from N.L. Grape St to S.L. Hawthorn St.

80' wide 14' walks

BM.	5.67	278.92		273.25	36k SW Grape + Bancroft
		N.L. Grape St.			
W.			4.8	274.1	
cb			4.3	274.6	
1/4			4.8	274.1	
C			4.6	274.3	
1/4			4.3	274.6	
cb			4.1	274.8	
E			3.8	275.1	
		25' No.			
E			3.0	275.9	
cb			3.2	275.7	
1/4			3.5	275.4	
C			3.4	275.0	
1/4			3.7	275.2	
cb			3.3	275.6	
W			3.9	275	
		50' No.			
W			2.5	276.4	
cb			2.5	276.4	
1/4			2.6	276.3	
C			3.3	275.6	
1/4			3.5	275.4	
cb			2.7	276.2	
E			2.7	276.2	
		75' No.			
E			3.3	275.6	
cb			3.0	275.9	
1/4			3.5	275.4	
C			3.3	275.6	
1/4			2.9	276.0	
cb			2.6	276.3	
W			2.4	276.5	
		100' No.			
W			2.9	276.0	
cb			3.3	275.6	
1/4			3.5	275.4	
C			3.8	275.1	
1/4			3.9	275.0	

		278.9								
cb			4.1	274.8		cb			17.0	261.9
E			4.4	274.5		1/4			15.9	263.0
		125' No.				c			14.3	264.6
E			6.8	272.1		1/4			10.8	268.1
cb			6.1	272.8		cb			9.3	269.6
1/4			5.8	273.1		W			8.0	270.9
c			4.9	274.0				200' No.		
1/4			4.6	274.3		W			9.6	269.3
cb			4.2	274.7		cb			11.5	267.4
W			3.8	275.1		T.P.	0.65	266.50	13.07	265.85
		165' No.				+10			1.7	264.8
W			6.1	272.8		1/4			2.9	263.6
cb			7.5	271.4		+4			4.5	262.0
1/4			8.7	270.2		c			9.6	256.9
c			9.7	269.2		+8			12.8	253.7
1/4			10.4	268.5		1/4			12.7	253.8
cb			10.9	268.0		cb			14.8	251.7
E			11.7	267.2		E			15.0	251.5
		180' No.						225' No.		
E			16.9	262.0		E			28.1	238.4

		266.50		
cb			28.1	238.4
1/4			34.6	241.9
c			19.1	247.4
1/4			13.7	252.8
cb			8.6	257.9
W			1.4	265.1
		255' No.		
W			6.3	260.3
cb			12.7	253.8
1/4			18.4	248.1
c			24.3	242.3
1/4			31.9	234.6
cb			37.9	228.6
47			41.8	214.7
E			42.0	224.5
		262' No.		
E			45.9	220.6
cb			39.0	227.5
1/4			33.3	233.2
c			26.6	239.9

1/4			20.3	246.2
cb			13.7	252.8
W			8.1	258.4
T.P.	0.34	261.19	126.5	253.85
		285' No.		
W			1.3	249.9
cb			10.4	243.8
1/4			15.0	239.2
c			19.1	235.1
1/4			24.6	229.2
cb			30.6	223.6
E			36.4	217.8
		Box' No. = SL. HAWTHORN		
E			39.6	214.6
cb			34.6	219.6
1/4			29.5	224.7
c			24.3	229.9
1/4			20.0	234.2
cb			15.8	238.4
			12.3	241.9

12/30/18 Gregory / Shaw

CROSS SECTION OF GRAPE ST.

from E.L. Bancroft St to E.L. 33rd St

80' wide

	5.1 ↓	278.39	273.25	SBK SW Grape & Bancroft

E. L. BANCROFT ST.

No.	3.3	275.1
cb	3.8	274.6
1/4	4.6	273.8
C	5.4	273.0
1/4	6.4	272.0
cb	7.5	270.9
So	13.3	265.1
25' E		
-15	15.6	263
So	11.8	266.6
cb	7.1	271.3
+ 4	6.1	272.3
1/4	5.7	272.7
C	4.7	273.7
1/4	4.0	274.4
cb	3.4	275.0
No	3.0	275.4
45' E		
No	2.9	275.5
cb	3.3	275.1
1/4	3.7	274.7
C	4.3	274.1
1/4	5.2	273.2
cb	5.9	272.5
So	7.1	271.3
75' E		
So	5.6	272.8
cb	4.9	273.5
1/4	4.2	274.2
C	3.9	274.5
1/4	3.5	274.9
cb	3.3	275.1
No	3.1	275.3
100' E		
No.	3.6	274.8
cb	3.5	274.9
1/4	3.5	274.9

		278.39			
c			3.9	274.5	
1/4			4.1	274.3	
cb			4.5	273.9	
So			4.9	273.5	
		140' E			
So			4.2	274.2	
cb			4.0	274.4	
1/4			4.2	274.2	
c			4.2	274.2	
1/4			4.5	273.9	
cb			5.2	273.2	
No.			5.8	272.6	
		170' E			
No.			10.5	267.9	
cb			9.4	269.0	
1/4			8.3	270.1	
c			7.4	272.0	
1/4			6.7	271.7	
cb			5.6	272.8	
So.			5.3	273.1	

		200' E = W.L. of 33rd St		80' St	
So.			7.1	271.3	
on BM.			6.54	271.85	Mon S.W.
cb			9.1	269.3	
1/4			10.4	268.0	
c			11.2	267.2	
1/4			12.7	265.7	
T.P.	5.31	270.83	12.87	265.52	
cb			6.1	264.7	
No			7.5	263.3	
		W. Curb			
No			9.9	260.9	
cb			8.0	262.8	
1/4			6.6	264.2	
c			5.1	265.7	
1/4			4.1	266.7	
cb			2.7	268.1	
So.			1.2	269.6	
		W. 1/4			
So			2.1	268.7	

270.83

cl	3.7	267.1
1/4	5.2	265.6
c	6.5	264.3
1/4	8.1	262.7
cl	10.3	260.5
No.	12.0	258.8
Center		
No.	14.1	256.7
cl	12.2	258.6
1/4	10.2	260.6
c	8.3	262.5
1/4	6.8	264.0
cl	5.3	265.5
So.	3.6	267.2
E 1/4		
So.	4.9	265.9
cl	6.4	264.4
1/4	8.0	262.8
c	9.9	260.9
1/4	11.6	259.2

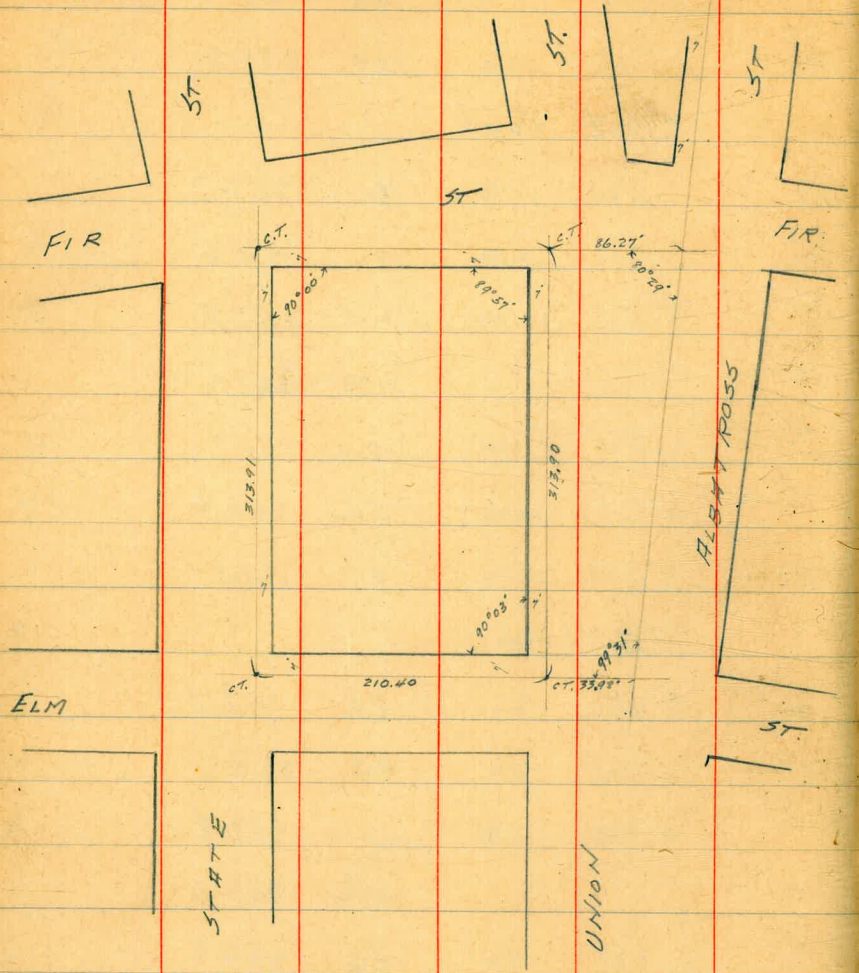
GRAPE 27

cl	13.5	257.3
No.	15.9	254.9
E. Cor.		
No.	19.1	251.7
cl	14.6	256.2
1/4	12.9	257.9
c	11.3	259.5
1/4	10.0	260.8
cl	8.2	262.6
So.	6.7	264.1
E. Line		
So.	8.5	262.3
cl	9.9	260.9
1/4	11.0	259.8
c	12.2	258.6
1/4	14.6	256.2
cl	17.9	252.9
No.	22.2	248.6

11/21/19 Gregor / Miller

UNION ST

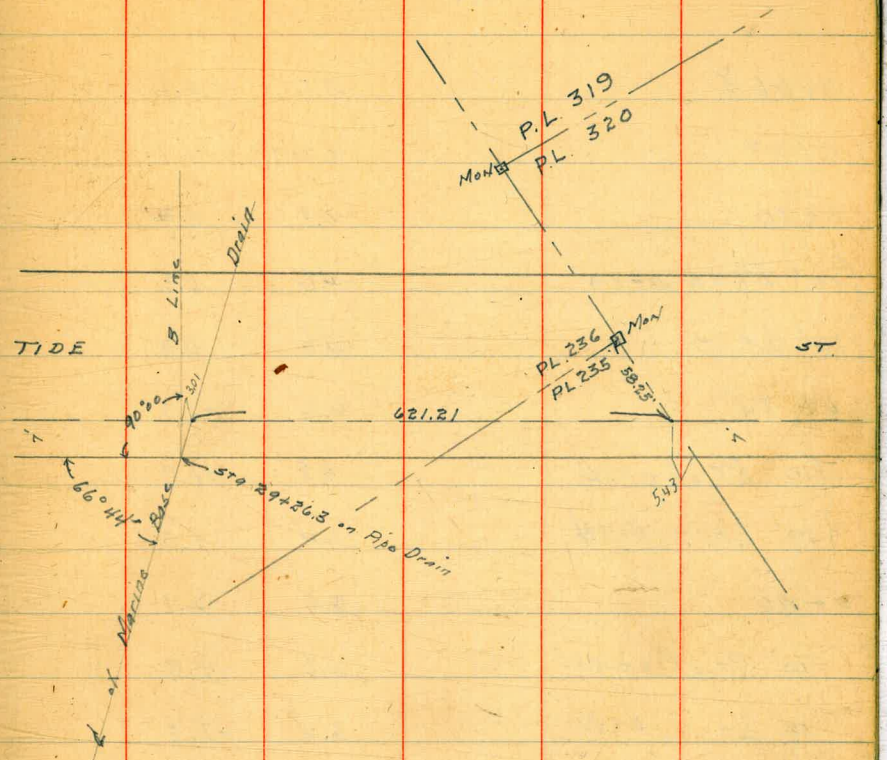
Survey of Proposed Closing from Elm to Fir



3/29/20 Gregory Moore Miller Shaw

Location of Drain to be Built across Tide St.

on B.M.	3.17	13.71		10.54	Mon Ctr of Manhole & El. Northerly 5ft N Curb & Tide
			12.08	1.63	
T.P.	3.44	4.66	12.49	1.22	
	5.16	5.65	4.17	0.49	
	4.63	4.94	5.34	0.31	
29+26.3 = St. Tide St = 0+00			4.47	0.47	on hub
0+19			4.2	0.7	
0+19.5			4.7	0.2	
0+32			4.2	0.7	
0+52.3			3.79	1.15	on N. rail
0+54			3.8	1.1	
0+					
0+72			5.1	-0.2	
0+73			4.1	0.8	
0+87			4.4	0.5	
10' Rt of 0+87 on N. L. of Tide			4.4	0.5	
" Lt " " " " " "			4.4	0.5	
0+93			7.0	-2.1	
10' Rt of 0+93 Parallel to Tide			7.1	-2.2	
10' Lt " " " "			7.0	-2.1	
1+00			7.1	-2.2	



Levels on ℄ Line = rt Ls to Tide

10' Lt of 1+00		6.9	-2.0
10' Rt " 1+00		7.2	-2.3
29+26.3 = St. Tide = 0+00		4.47	0.47 on hub
0+17		4.4	0.5
0+18		4.9	0.0
0+28		4.7	0.2
0+48		3.84	1.10 = N rail

		4.94		
0+66.5			5.1	-0.2
0+67			4.2	0.7
0+80			4.7	0.2
10' Rt of	0+80		4.6	0.3
10' Lt	"		4.6	0.3
0+84			6.6	-1.7
10' Rt of	0+84		6.8	-1.9
10' Lt	" 0+84		6.4	-1.5
0+90			7.0	-2.1
10' Rt of	0+90		6.8	-1.9
10' Lt	" 0+90		6.4	-1.5
1+00			6.3	-1.4
10' Rt of	1+00		6.3	-1.4
10' Lt	" 1+00		6.5	-1.6
	Tie to Marine Base B.M.			
T.P.		6.33	6.82	0.49
			3.31	3.51 =
				12.48 = Govt B.M.
				8.97

3.56
1.58

7/7/20 Gregory Miller Shaw

Levels on N. & of 24th to 25th bet C & Broadway

Block 41 Golden Hill

	10.53	189.96	179.43	B.P. SW 24th & C

E cb Line 24th

N.	11.99	177.97	on end of curb no return on N.
S	11.95	178.01	~ curb return

Present paving (in rather poor shape extends to 5' W of E curb line of 24th

E. L 24th = 0+00

S	11.7	178.3	on paving
C	11.9	178.1	~ ~
+W.5	11.6	178.4	N edge ~
N	10.7	179.3	

0+45

N	6.8	183.2	
+6.5	7.1	182.9	N. edge paving
C	7.3	182.7	on paving
S	6.9	183.1	~ ~

0+57.

paving extends from S.L. to 9' N. of center.

	5.7.	~~5.7~~ 184.3	N edge paving

0+62

S	5.3	184.7	on paving

195
99
18450
17830
60) 620 (10.33
60
200
515
309
3605
181.90

		189.96			
C			5.5	184.5	
+9			5.3	184.7	N edge paving
N			5.3	184.7	
		0+74			
0.4 S of SL.			4.8	185.2	= center of 8' garage door cement floor
		1+00			
0.4 S. of SL			4.1	185.9	= center of 3.5' cement walk to house
		1+08	= end of present paving		
4.7 N. of N.L.			3.6	186.4	= center of 8' garage door cement floor
N			4.1	185.9	= edge of cement apron and edge of present paving
C			4.3	185.7	on paving
S			4.0	186.0	" "
		1+08	= N. end of 2.4' walk (cement)		on S. S edge of walk = S.L of Alley at this point.
		1+27			
N			2.7	187.3	= center of 3' cement walk to house
		1+30			
S			2.3	187.7	= S edge of cement walk
+1.4			1.4	187.6	= N " " "
C			2.9	187.1	
N			2.4	187.6	

		189.96			
		1+70			
3.2' N. of N.L.			0.4	189.6	= center of 8' garage door cement floor
N			0.8	189.2	= edge of cement apron
		1+78			
N			0.3	189.7	
C			0.7	189.3	
+7.5			0.6	189.4	= N. edge cement walk
S			0.5	189.5	= S " " "
		1+89			
S			0.4	189.6	= center of 20' double garage door cement floor.
		1+99.5 = end of cement walk.			
S			0.4	189.6	S edge " cement walk
+7.5			0.4	189.6	N " " "
T.P.	8.93	198.58	0.31	189.65	
		2+28.5 = W. end cement apron			
S			7.5	191.1	= S. edge apron
+2.4			7.6	191.0	= N. " "
		2+40			
S			7.0	191.6	= center of 10' garage door cement floor
+2.4			7.4	191.2	= edge of apron

	198.58				
C		8.0	190.6		
+7.5		7.5	191.1	= S edge	cement apron
N		7.1	191.5	= center of	20' double garage cement floor
	2+62				
S		6.9	191.7	= center	of 10' garage door
+7.5		7.2	191.4	= N. edge	of apron
	2+71 = Sewer M.H.	7.2	191.4		
	2+73 = E end cement apron				
S		7.0	191.6	= S edge	of apron =
+7.5		7.1	191.5	= N "	" "
	2+82				
0.3 N. of N.L.		6.1	192.5	= center of	2.4' walk to house.
	2+93				
3.5' N. of N.L.		6.2	192.4	= center of	8' garage door cement floor
	3+15				
3.5' N. of N.L.		5.6	193.0	= center of	20' double garage cement floor
N		6.0	192.6	= S edge	cement apron
C		6.5	192.1		
S		6.5	192.1		
	3+33				
S		6.3	192.3	on cement	walk 20.0' wide extends 1.4' into alley.

	198.58			
	3+73	= east side of garage door	is on E side Apron is on E side 2.7' wide	
0.3' N. of N.L.		4.8	193.8	= floor
	3+75.7			
0.3 N of N.L.		4.9	193.7	= E edge of Apron
	4+00			
S		5.0	193.6	
C		5.1	193.5	
N		4.6	194.0	
	4+45			
4' N of N.L.		3.4	195.2	= center of 8' garage door cement floor
N		3.6	195.0	= S edge of cement apron
C		3.8	194.8	
S		3.8	194.8	
	4+63			
2' N. of N.L.		3.2	195.4	= center of 16' double garage door cement floor
N		3.4	195.2	= S edge cement apron
	5+04.5			
N		3.1	195.5	= center of 3.4 cement walk to house
	5+15			
.15 S. of N.L.		3.3	195.3	= center of 14' double garage door cement floor

		198.58			
		5+30			
S			3.8	194.8	
C			3.9	194.7	
N			3.5	195.1	
		5+50 = sewer M.H.			
C			4.5	194.1	
		5+65			
N			5.2	193.4	
C			5.5	193.1	
+3			5.4	193.2	
+6			4.4	194.2	
S			4.2	194.4	
		5+85			
S			5.2	193.4	
+4			5.5	193.1	
+8			6.8	191.8	
C			6.7	191.9	
N			6.5	192.1	

		6+00			
N			8.5	190.1	
C			8.8	189.8	
+2			8.6	190.0	
+6			6.9	191.7	
S			5.5	193.1	
		6+01.3 = W.L. 25th St			
S			9.0	189.6	on curb
C			9.15	189.43	on paving
N			8.7	189.9	on curb
CMP			11.57	187.01	=197.03 SW 25th St Bridge

5/13/21 Gregory Moore Miller Shaw.

Levels on Curb Lines of KITE ST. From the S.L. of Marine View To ~ NL. of Walnut

The curb Lines on Both sides are produced S. from The lines in Marine View, N.E. the cb line on E is 8' from E.L. of St. + W cb line is 52' W of E.L. of St.

	1.10	257.19	256.09	Bolt in Hydrant.
		S.L. Marine View		
E cb		1.75	255.44	on cement.
W cb		1.5	255.7	
		46.5' S		
W cb		1.9	255.3	
E cb		2.94	254.25	on cement
		53' S		
E cb		4.13	530	on cement.
W cb		3.2	540	
		60' S		
W cb				
E cb		5.5	51.7	
		100' S		
E cb		8.0	49.2	
W cb		5.5	51.7	

	57.19		
	150' S		
W cb		7.8	49.4
E cb		12.1	45.1
	200' S		
E cb		14.6	42.6
W cb		9.5	47.7
	254 ± S = NL Walnut.		
W cb		10.9	46.3
E cb		17.4	39.8

5/ 7/22 M. Moore
Miller
Shaw

Levels on Curb lines of J St
From W.L. of 27th West to P.C.

Note: { 10' Curbs on So. side of J St
{ Recomend 14' Curbs on N. side

BP S.E. 27th & I St

				142.11
T.P	10.43	152.54	9.54	143.0
	9.88	152.88		
		W.L. of 27th = 0+00		
N L			9.3	143.6
N 10' Cb			9.4	143.5
14' cb			9.6	143.3
S cb			10.95	141.93
		0+20 on S Curb		
S cb			9.28	143.60
		0+50		
S Cb			7.53	145.35
		0+74		
N L			6.31	146.57
N L			6.9	146.0
N 10' Cb			7.1	145.8
N 14' cb			7.4	145.5
		0+50		
N L			5.8	147.1

Foot of Cobblestone Wall

Cement Curb

" "

" "

Ely. on lower step of cement stairway, 5' wide on ground

Foot of cobblestone Wall

9 54

~~40~~ 38

		152.88		
N 10' ℄			6.0	146.9
N 14 ℄			6.2	146.7
		0+75		
N L			4.8	148.1
N 10' ℄			5.2	147.7
N 14' ℄			5.3	147.6
S ℄			6.4	146.5
		1+00		
S ℄			5.5	147.4
N 14 ℄			5.0	147.9
N 10 ℄			4.8	148.1
N			4.2	148.7
		1+50		
NL			2.8	150.1
N 10' ℄			3.4	149.5
N 14 ℄			3.6	149.3
S ℄			4.0	148.9
		7+10.8		
S ℄			2.1	150.8
N 14' ℄			1.5	151.4

End of cobblestone wall Elv. at foot of wall

Shade Trees 12' from prop line.

" " " " " "

		152.88		
N 10' ∧			1.5	151.4
N L			0.9	152.0
T.P	3.79	154.87	1.80	151.08
		2+45		
N L			1.7	153.2
N 10' ∧			2.3	152.6
N 14 ∧			2.4	152.5

Shade Trees 12' from prop't

Note:- 5 Fine Camphor Trees about 25' high 20" in diam. at base (Try to save)

7/28/11 Moore Miller

Curb Levels on Hmpudia from NL Pine to SL Cherry

10' Curb 50' wide

				B.R NE Trip Post Stockton
			267.06	
	8.06	275.12	8.22	266.90
	0.77	267.67 ✓	1.71	265.96
		NL Pine = 0+00		
W cb			1.9	265.8
C			1.6	266.1
		0+50		
C			5.2	262.5
W cb			5.8	261.9
		1+00		
W cb			9.6	258.1
C			9.5	258.2
		1+50		
C			13.3	254.4
W cb			13.5	254.2
T.P.	1.30	256.04 ✓	12.93	254.74 ✓
		1+75		
W cb			3.4	252.6
C			3.3	252.7

B.M. on Hub N.W. Hmpudia + Pine

Cocos Plumosas Palms planted from Sta 1+50 to 3+00 8' from prop. Line

		256.04		
		2+00		
E			4.6	251.4
W ch			4.9	251.1
		2+15.5		
W L			6.09	249.95
		2+44.0		
W L			7.85	248.19
		2+50		
W ch			7.5	248.5
C			7.2	248.8
		3+00 = SL Cherry		
C			9.7	246.3
W ch			9.8	246.2
T.P	11.72	266.57	1.19	254.85
	9.0	274.96	0.61	265.96
			7.91	267.05

Elv so. side of Cement Drive

" No. " " " "

ckd BM. Trias + Fort Stockton 267.06

11/16/21 Gregory Moore Miller Shaw

CROSS SECTION OF ALLEY BLOCK 84 Univ Hgts 20' wide.
S. side University Ave. bet Park Blvd and Georgia

	1.83	338.24	336.41	SW Georgia + Univ.
	S. L. of Univ = 0+00			
E. on curb		6.78	331.52	
E - gutter (on paving)		7.37	330.87	
C		7.3	330.9	
W on curb and paving		8.32	329.92	
	0+02.0			
W		5.7	332.5	
+4		7.3	330.9	
C		7.0	331.2	
+6		6.9	331.3	
E		5.8	332.4	
	0+10			
E		5.0	333.2	
+6		6.0	332.2	
C		5.9	332.3	
+6		6.0	332.2	
W		5.4	332.8	
	0+25			
W		5.3	332.9	

C		5.2	333.0
+5		5.2	333.0
E		4.4	333.8
	0+50		
E		3.9	334.3
+5		5.0	333.2
C		5.1	333.1
+4		5.2	333.0
W		4.8	333.2
	1+00		
W		5.2	333.0
C		5.3	332.9
+4		5.3	332.9
E		4.3	333.9
	1+50		
E		4.4	333.8
C		5.6	332.6
W		6.1	332.1
	2+00		
W		6.7	331.5

		338.24		
C			6.0	332.2
+4			6.0	332.2
+9.5 = fence			4.6	333.6
		2+50		
E			6.9	331.3
C			7.9	330.3
W			8.8	329.4
		3+00		
W			12.4	325.8
+8			10.1	328.1
C			10.1	328.1
+7			10.1	328.1
+9.4 = concrete walk (foot bk)			9.1	329.1
		3+50		
T.P.	1.62	327.24	12.62	325.62
E			1.1	326.1
+5			2.2	325.6
C			2.6	324.7
+4			2.5	324.7
W			4.2	323.0

3+89 = center garage on W			
-1 = front of garage dirt	5.9	321.3	
W	5.9	321.3	
C	5.1	322.1	
E	4.0	323.2	
4+00			
E	4.0	323.2	
C	5.0	322.2	
+5	4.8	322.4	
+7	6.1	321.1	
W	5.6	321.6	
4+20			
W	6.4	320.8	
+6	4.4	322.8	
C	4.2	323.0	
+6	4.1	323.1	
E	2.2	325.0	
4+30			
E	1.6	324.6	
+2	3.0	324.2	

		327.24		
+3			4.2	323.0
C			4.4	322.8
W			5.2	322.0
		4+78 = center garage on W		
-1 = front of garage			6.0	321.2
W			6.0	321.2
C			5.4	321.8
+7			5.0	322.2
E			3.3	323.9
		5+00		
E			2.8	324.4
+3			5.1	322.1
C			5.6	321.6
W			5.6	321.6
		5+35		
W			6.5	320.7
+1.4 = fence			6.5	320.7
C			6.7	320.5
+6			6.4	320.8
E			4.9	322.3

		5+70		
E			8.0	319.2
+4			9.3	317.9
C			9.4	317.8
+8 = fence			9.2	318.0
W			9.2	318.0
		5+85		
W			9.9	317.3
+2			11.0	316.2
C			11.4	315.8
+4			11.4	315.8
+5			10.1	317.1
E			9.0	318.2
		6+00		
E			9.7	317.5
+5			10.1	317.1
TP	1.87	317.58	11.53	315.71
+7			4.6	313.1
C			4.7	312.9
W			4.2	313.4

317.58

6+15

W		7.0	310.6
C		7.4	310.2
+3		7.2	310.4
+5		2.3	315.3
E		1.2	316.4

6+17

E		1.7	315.9
+3		7.5	310.1
C		7.6	310.0
W		7.7	309.9

6+19 = N.L. Robinson Ave

W	no curb	9.0	308.6
+1		8.2	309.4
C		7.8	309.8
E	on cement curb.	7.79	309.79

7/10/[illegible] Longfellow Moore 12/13

CROSS SECTION OF KITE ST

from S.L. of Marine View to N.L. of Horton's Add.

60' wide 8' cbs 11' 1/4's } From S.L. of Marine View S. to N.L. Walnut

50' wide 10' cbs } From S.L. Walnut to N.L. Horton's Add.

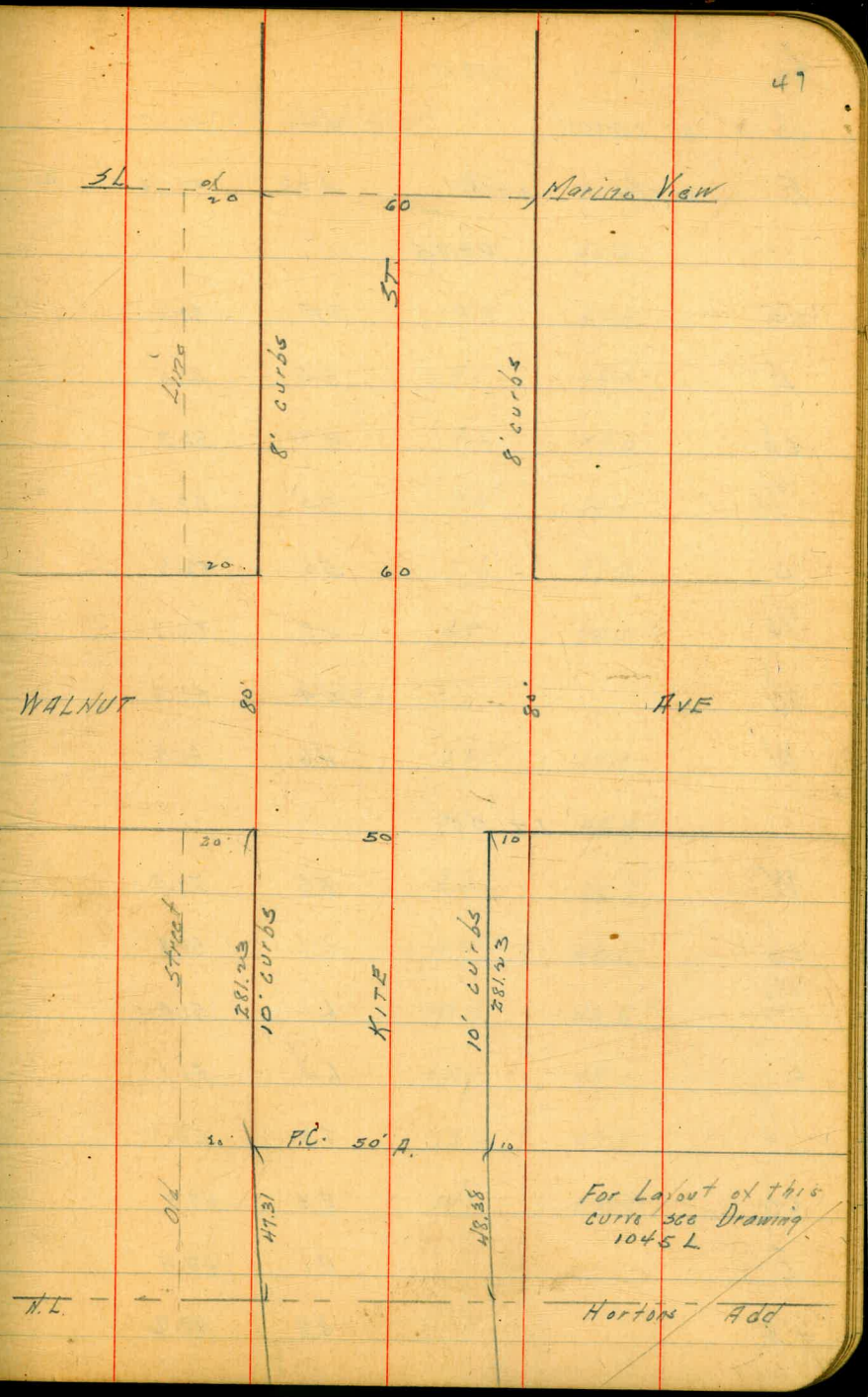
	1.38	257.47	256.09	Bolt bot. of H/d. Kite & Brook

S.L. Marine View = 0+00

E.	edge cement walk	1.77	55.77
cb.	on cement	2.01	55.46
✓	in gutter	2.8	54.7
1/4		2.4	55.1
C		1.9	55.6
1/4		1.7	55.8
cb	in gutter	2.0	55.5
✓	on cement	1.43	56.04
W =	edge cement walk	1.25	56.22

52.5' S on W
54.0 ✓ - E } = S end of Curb & Walk both sides

W =	edge cement walk	3.45	54.02
cb	on cement	3.67	53.80
✓	in gutter	4.2	53.3
1/4		3.7	53.8
C		4.2	53.3
1/4		4.6	52.9
cb	in gutter	4.9	52.6



		259.47		
cb	on cement		4.40	53.07
E	on edge of walk		4.23	53.24
		0+75		
-5			7.5	50.0
E			6.5	51.0
cb			6.2	51.3
1/4			5.5	52.0
C			5.0	52.5
1/4			4.8	52.7
cb			4.9	52.6
W			4.6	52.9
		1+00		
W			5.6	51.9
cb			6.1	51.4
1/4			6.1	51.4
C			6.4	51.1
1/4			7.3	50.2
cb			8.3	49.2
E			9.1	48.4
+5			9.3	48.2

		1+25		
-5			11.6	45.9
E			10.9	46.6
cb			9.9	47.6
1/4			9.1	48.4
C			8.5	49.0
1/4			7.4	50.1
cb			7.6	49.9
W			6.8	50.7
		1+50		
W			7.7	49.8
cb			8.1	49.4
1/4			8.8	48.7
C			9.4	48.1
1/4			10.9	46.6
cb			11.4	45.1
E			13.6	43.9
+5			14.1	43.4

		2+57.47			
		1+75			
-5			15.1	42.4	
E			14.9	42.6	
cb			13 ✓	44.1	
1/4			12.1	45.4	
C			10.8	46.7	
1/4			9 ✓	48.1	
cb			8.9	48.6	
W			8 ✓	49.1	
		2+00 ✓			
W			9.5	48.0	
cb			10.0	47.5	
1/4			10.7	46.8	
C			11.7	45.8	
1/4			13.3	44.2	
cb			14.7	42.8	
E			16.2	41.3	
+10			18.2	39.3	

		57.5			
		2+25 ✓			
-10			19.2	38.2	
E			17.6	39.9	
cb			17.0	40.5	
1/4			14.6	42.9	
C			12.9	44.6	
1/4			11.4	46.1	
cb			10.7	46.8	
W			10.3	47.2	
		2+54 ± on W. 2+52.5 ± " E } =		N.L Walnut 80' St 14' cbs	
W			11.1	46.4	
cb			11.4	46.1	
1/4			12.5	45.0	
T.P.	2.49	248.48 ✓	11.48	245.99 ✓	
C			5.2	49.3	
1/4			7.4	41.1	
cb			8.7	39.8	
E			10.3	38.2	
+10			14.3	36.2	

24&48		
N. Curb ✓		
-10	13.4	35.1
E	10.5	38.0
+8.35 = cb.	9.3	39.2
+10.39 = 1/4	7.9	40.6
+10.39 = c	6.1	42.4
+10.38 = 1/4	4.2	44.3
+10.39 = cb	2.8	45.7
+8.35 = W.	2.8	45.7
N. 1/4 ✓		
W	3.1	45.4
+8.67 = cb	3.3	45.2
+9.82 = 1/4	4.5	44.0
+9.82 = c	6.3	42.2
+9.82 = 1/4	7.8	40.7
+9.82 = cb	9.2	39.3
+8.67 = E	10.8	37.7
+10	12.8	35.7
Center Walnut		
-10	13.0	35.5

50 & 51 ✓		
E	10.9	37.6
+9 = cb	9.2	39.3
+9.25 = 1/4	7.8	40.7
+9.25 = c	6.6	41.9
+9.25 = 1/4	5.3	43.2
+9.25 = cb	3.6	44.9
+9 = W	3.3	45.2
5. 1/4 ✓		
W	3.6	44.9
+9.32 = cb	4.0	44.5
+8.68 = 1/4	5.6	42.9
+8.68 = c	6.7	41.8
+8.68 = 1/4	8.1	40.4
+8.68 = cb	9.2	39.3
+9.32 = E	11.0	37.5
+10	12.7	35.8
S. Curb		
-10	12.2	36.3 ✓
E	10.5	38.0
+9.65 = cb	8.9	39.8
+8.11 = 1/4	7.8	40.7

	248.48		
+8.11 = C		6.8	41.7
+8.12 = 1/4		5.6	42.9
+8.11 = cb		4.3	44.2
+9.65 = W		3.8	44.7
	SL Walnut 50 10	ST cbs	from here south
W		4.0	44.5
cb		4.4	44.1
1/4		6.1	42.4
C		6.9	41.6
1/4		8.1	40.4
cb		8.6	39.9
E		10.1	38.4
+10		12.2	36.3
	25' S ✓		
-10		11.8	36.7
E		10.2	38.3
cb		8.7	39.8
1/4		8.1	40.4
C		7.1	41.4
1/4		6.0	42.5

cb		4.5	244.0
W		4.2	44.3
	50' S ✓		
W		4.4	44.1
cb		4.5	44.0
1/4		6.1	42.4
C		6.9	41.6
1/4		7.6	40.9
cb		8.9	39.6
E		10.3	38.2
+10		11.4	37.1
	75' S		
-10		11.5	37.0
E		9.8	38.7
cb		8.7	39.8
1/4		7.8	40.7
C		6.9	41.6
1/4		6.1	42.4
cb		4.7	43.8
W		4.6	43.9

24848

100' S

W	4.9	43.6
cb	5.2	43.3
1/4	6.2	42.3
C	6.8	41.7
1/4	7.8	40.7
cb	8.8	39.7
E	9.9	38.6
+10	11.3	37.2

125' S

-10	11.5	37.0
E	10.3	38.2
cb	9.1	39.4
1/4	8.1	40.4
C	7.1	41.4
1/4	6.4	42.1
cb	5.6	42.9
W	5.3	43.2

150' S

W	5.8	42.7
cb	6.2	42.3
1/4	6.6	41.9
C	7.4	41.1
1/4	8.0	40.5
cb	9.2	39.3
E	10.2	38.3
+10	11.8	36.7

175' S

-10	12.0	36.5
E	10.5	38.0
cb	9.2	39.3
1/4	8.3	40.2
C	8.0	40.5
1/4	7.0	41.5
cb	6.9	41.6
W	6.8	41.7

200' S

W	8.0	40.5

		N48.48			
cb			8.1	48.4	
1/4			8.1	40.4	
C			8.4	40.1	
1/4			8.6	39.9	
cb			9.8	38.7	
E			10.9	37.6	
+10			11.8	36.7	
		N75 S			
E			11.1	37.4	
cb			10.2	38.3	
1/4			9.7	38.8	
C			9.3	39.2	
1/4			9.2	39.3	
cb			9.3	39.2	
W			9.2	39.3	
		N50 S			
W			10.5	38.0	
cb			10.7	37.8	
1/4			10.4	38.1	
C			10.5	38.0	

1/4			10.4	38.1	
cb			10.8	37.7	
E			11.5	37.0	
		N81.23 S = SECT. A PC.			
E			12.0	36.5	
cb			11.7	36.8	
1/4			12.0	36.5	
C			11.8	36.7	
1/4			11.8	36.7	
cb			12.1	36.4	
W			12.3	36.2	
		N47.31 S ox P.C. on W 48.38 " " " E } = N.L Horton's Add.			
W			14.5	34.0	
cb			14.1	34.4	
1/4			14.0	34.5	
C			13.9	34.6	
1/4			13.6	34.9	
cb			13.6	34.9	
E			13.7	34.8	
T.P.	11.86	N58.04	N30	N4678	
chk BM			1.98	25606	= N56.09

3/3/25 Moore Preston Walker

Cross Section at Mission Ave
Georgia to Madison Middle 70' 15' 2 lns 10' 1/4S

3.93 348.13 344.20

EL Georgia = Section A

S		3.0	345.1
Ch	1X85	2.2	45.7
+7	11.9	2.5	45.6
1/4		4.4	43.7
C		4.0	44.1
1/4		3.8	44.3
Ch		3.9	44.2
N		4.3	43.8

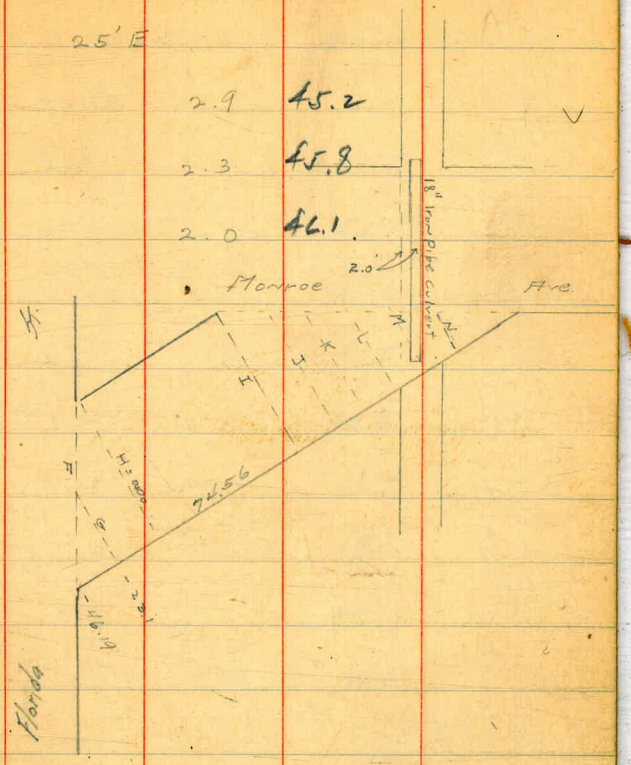
H916 E on SL = Section B = 0+00

N		4.3	43.8
Ch		4.1	44.0
1/4		4.0	44.1
C		4.3	43.8
1/4		4.5	43.6
+H		2.5	45.6
Ch		1.9	46.2
S		2.1	46.0

348.13

25' E

S	2.9	45.2
Ch	2.3	45.8
+5	2.0	46.1



1/4	4.9	43.2
C	4.6	43.5
1/4	4.5	43.6
Ch	4.1	43.7
+11	4.7	43.4
N	2.9	45.3

50' E

N	3.1	45.0

+7	3.3	44.8	
+10	5.4	42.7	
cb	5.5	42.6	
1/2	5.2	42.9	
c	5.4	42.7	
1/4	5.6	42.5	
+2	4.9	43.2	
+5	2.7	45.4	
cb	2.5	45.6	
S	3.2	44.9	
75° E			
S	3.3	344.8	
cb	3.5	44.6	
+6	3.9	44.2	
1/3	6.3	41.8	
c	6.2	41.9	
1/2	6.1	42.0	
+8	6.0	42.1	
cb	5.0	43.1	
+2	3.3	44.8	

N	3.1	45.0
100° E		
N	3.6	344.5
cb	3.4	44.7
+5	6.5	41.6
1/4	7.6	40.5
c	7.3	40.8
1/3	7.4	40.7
+5	5.1	43.0
cb	4.0	44.1
S	3.8	44.3
125° E		
S	5.0	343.1
+10	5.0	43.1
+12	5.8	42.3
cb	6.9	41.2
+2	7.9	40.2
1/4	8.6	39.5
c	8.3	39.7
1/3	8.1	340.0

		348.13		
+3			7.0	341.1
+4			4.5	43.6
cb			4.1	44.0
N			3.8	44.3
		147° E		
N			4.4	343.7
cb			4.6	43.5
+8			5.3	42.8
+9			8.7	39.4
1/4			9.4	38.7
C			9.7	38.4
1/4			9.6	38.5
cb			7.8	40.3
+8			6.6	41.5
+12			5.7	42.4
S			5.8	42.3
		167° E		
S			14.5	333.6
+10			13.0	35.1
cb			11.2	36.9

		348.13		
1/4			10.8	37.9
C			11.0	37.1
1/4			10.4	37.7
cb			8.5	39.6
N			4.8	43.3
		175° E		
N			11.4	336.7
cb			10.7	37.4
1/4			11.1	37.0
C			11.4	36.7
1/4			11.3	36.8
cb			12.0	36.1
+5			13.5	94.6
S			14.5	33.6
T.P.	.160	337.19	12.5	335.59
S		185° E	4.3	332.9
+10			3.5	33.7
cb			1.8	35.4
+5			1.1	36.1
1/4			1.2	36.0

337.19

C	1.2	36.0	
1/4	0.7	36.5	
Cb	1.1	36.1	
+2	0.5	36.7	
N	1.4	35.8	
	210° E		
N	2.7	334.5	
+3	3.5	33.7	
Cb	3.2	34.0	
+5	3.2	34.0	
+6	2.6	34.6	
1/4	2.5	34.7	
C	2.6	34.6	
1/4	3.0	34.2	
+5	2.4	34.8	
+6	4.2	33.0	
Cb	4.5	32.7	
S	4.9	32.2	
	225° E		
S	5.7	331.5	

Cb	5.1	332.1	
1/4	4.1	33.1	
C	3.7	32.4	
1/4	3.8	33.3	
Cb	4.1	33.1	
N	4.1	33.1	
	241° E		
N	4.5	332.7	
Cb	5.0	32.2	
1/4	5.1	32.1	
C	5.0	32.2	
1/4	5.4	31.8	
Cb	5.6	31.6	
S	6.3	30.9	
	245° E		
S	4.7	332.5	
+5	5.9	31.3	
Cb	5.8	31.4	
1/4	5.8	31.4	
C	5.3	31.9	

337.19

1/4		5.4	31.8
cb		5.4	31.8
+8		5.1	32.1
N		4.5	32.7
	260° E		
N		5.8	331.4
cb		5.6	31.6
1/4		6.8	30.4
C		6.9	30.3
1/4		7.1	30.1
+4		6.6	30.6
cb		6.7	30.5
S		7.6	29.6
	270° E		
S		9.1	328.1
cb		7.9	29.3
+6		7.6	29.6
1/4		8.3	28.9
C		8.0	29.2
1/4		7.7	29.5

337.19

cb		6.8	30.4
+7		5.5	31.7
N		5.1	32.1
	285° E		
N		7.6	329.6
cb		8.8	28.4
1/4		9.2	28.0
C		9.9	27.3
1/4		10.0	27.2
+5		9.6	27.6
cb		9.3	27.9
S		10.4	26.8
	315° E		
S		12.3	324.9
+10		12.4	24.8
+11		13.1	24.1
cb		13.1	24.1
+5		12.8	24.4
1/4		13.3	23.9
C		13.3	23.9

		337.19		
1/4			12.7	24.5
+5			10.8	26.4
Cb			10.6	26.6
N			10.2	27.0
T.P.	0.40	327.37	10.22	326.97
				on South
	324.19 E = W/L FLORIDA = Section C			
N			1.1	326.3
Cb			1.7	25.7
+7			2.2	25.2
1/4			3.3	24.1
+5			4.5	22.9
C			4.5	22.9
1/4			4.9	22.5
+4			4.1	23.3
Cb			3.9	23.5
+10			4.5	22.9
S			7.5	319.9
		1/last Section		
	23.1 E on N/L		= Section D	
C			7.3	320.1
+5			6.6	20.8

		327.37		
N 1/4			6.8	20.6
+5			3.5	23.9
Cb			3.9	23.5
N			2.6	24.8
	46.19 E = W/L FLORIDA = Section E			
N			4.8	322.6
Cb			5.6	21.8
+5			6.2	21.2
1/4			7.4	20.0
C			7.0	20.4
1/4			6.5	20.9
Cb			5.6	21.8
S			7.5	19.9
	E.L. FLORIDA = Section F = - 46.19			
S			9.1	318.3
Cb			8.9	18.5
1/4			8.8	18.6
C			8.6	18.8
1/4			8.3	19.1
Cb			8.0	19.1
N			7.8	19.6

	−23.1 = Section G		
C		8.6	18.8
S 1/2		8.4	19.0
cb		8.7	18.7
S		8.0	19.4
	0+00 = Section H		
S		7.8	319.6
cb		8.0	19.4
1/4		7.4	20.0
C		8.0	19.4
1/4		8.1	19.3
cb		7.9	19.5
N		7.8	19.6
	25' E		
N		8.0	319.4
cb		8.1	19.3
1/2		7.9	19.5
C		7.7	19.7
1/4		8.7	18.7
cb		9.7	17.7

S		9.6	17.8
+10		9.5	17.9
−15	50' E	11.4	316.0
S		10.0	17.4
cb		8.6	18.8
1/4		8.6	18.8
C		8.5	18.9
1/4		8.0	19.4
cb		7.4	20.2
N		6.9	20.5
	74.56 E = Section I		
N		6.8	20.6
cb		7.6	19.8
1/2		8.7	18.7
C		9.0	18.4
1/4		9.4	18.2
cb		9.0	18.4
S		10.7	16.7
+15		11.4	16.0
	97.32 E on SL = Section J		
−15		11.6	315.8
S		10.0	17.4

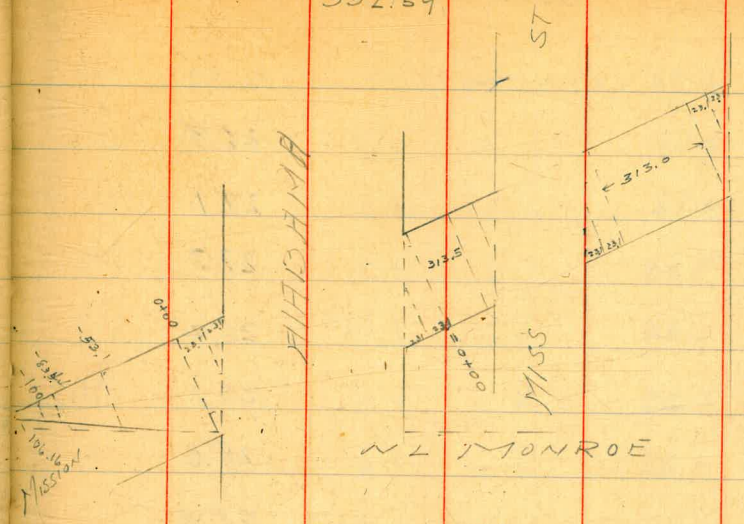
cb			9.8	17.6
1/4			8.7	18.7
c			8.5	18.9
1/4			7.7	19.7
cb = SL Monroe			7.4	20.0
	112.49' E on S = Section K			
N 1/4 = SL Monroe			7.2	320.2
c			7.6	19.8
1/4			8.5	18.9
cb			9.7	17.7
S			11.4	16.0
+15			11.5	15.9
	127.66' E on SL = Section L			
-12			11.6	315.8
S			11.6	15.8
cb			10.7	16.7
1/4			8.6	18.8
C = SL Monroe			7.2	19.2
	142.83' E on SL = Section M			
S 1/4 = SL ✓			7.0	320.4

cb			10.0	17.4
+5			10.8	16.6
+7 Flowline outlet			11.55	15.82 18" Iron pipe Culv.
+10			10.3	17.1
S			9.0	18.4
+5			9.1	18.3
	158' E on SL = Section N			
S			7.1	20.3
S cb = SL Monroe			6.7	20.7
	180.72' E = SL Mission & Monroe			
SL			5.8	21.6
T.P.	11.45	332.59	6.23	321.14
	-106.16 = NL Mission & Monroe			see sketch Page 62
NL			10.1	322.5
5' out			12.6	70.0
	-100'			
NL Monroe			10.4	322.2
" Mission			12.6	20.1
5' out			12.8	19.8

332.59

–	– 83.44		
– 5		12.5	19.1
N		12.5	19.1
+ 8		12.1	20.5
N cb + NL Monroe		10.2	22.4
	– 53.10		
C + . . ✓		9.5	323.1
+ 5		10.7	21.9
N 1/4 S		10.8	21.8
cb		11.0	21.6
N		11.5	21.1
+ 5		11.5	21.1
	0+00		
N		9.8	322.8
cb		9.5	23.1
1/4		9.4	23.2
C		9.6	23.0
1/4		9.4	23.2
cb		9.3	23.3
S		9.3	23.3

332.59



+ 23.10 on NL

C on WL Ala.	8.9	325.7
N 1/4	8.8	23.8
cb	8.9	23.7
N	8.8	23.8

+ 46.2 on NL - WL Ala

N	8.4	324.2
cb	8.6	24.0
1/4	8.8	23.8
C	8.9	23.7
1/4	9.1	23.5
cb	9.3	23.3
S	9.3	23.3

	332.59			
	-46.2 on SL Mission = EL Ah.			
S			5.7	26.9
db			5.5	27.1
+5			5.3	27.3
+7			6.4	26.2
1/4			6.5	26.1
C			7.0	25.6
1/4			6.7	25.9
db			6.5	26.1
N			6.5	26.1
	-23.10			
C			7.0	325.6
1/4			6.2	26.4
+5			5.9	26.7
+7			5.3	27.3
db			5.2	27.4
S			5.1	27.5
	0+00			
S			4.6	328.0
db			4.9	27.7

	332.59		Mission	
+4			5.0	27.6
+6			5.6	27.0
1/4			5.6	27.0
C			6.1	26.5
1/4			6.5	26.1
Cb			5.9	26.7
N			6.5	26.1
	25' E			
N			5.3	327.3
Cb			5.1	27.5
1/4			5.1	27.5
C			4.8	27.8
1/4			4.7	27.9
+4			5.0	27.6
+5			4.4	28.2
Cb			4.3	28.3
S			4.0	28.6
	50' E			
S			3.0	329.6
db			3.4	29.2

		332.59				332.59			Mission 64
1/4			4.2	28.6	cb			3.1	29.5
c			3.9	28.7	N			3.3	29.3
1/4			4.4	28.2			125'E		
cb			4.7	27.9	N			2.0	330.6
N			5.0	27.6	cb			2.3	30.3
		75'E			1/4			2.0	30.6
N			4.3	328.3	c			1.7	30.9
cb			4.0	28.6	1/4			1.8	30.8
1/4			3.8	28.8	+3			1.8	30.8
c			3.4	29.2	+5			1.1	31.5
1/4			3.3	29.3	cb			0.6	32.0
cb			2.5	30.1	S			0.3	32.3
S			2.1	30.5	T.P.	6.14	338.58	0.15	332.44
		100'E					150'E		
S			1.3	331.6	S			5.5	333.1
cb			1.8	30.8	cb			6.1	32.5
+5			2.1	30.5	1/4			6.7	31.9
1/4			2.8	29.8	c			6.7	31.9
c			2.6	30.0	1/4			6.9	31.7
1/4			2.9	29.7	cb			6.8	31.8

		338.58		
N			6.9	331.7
		175' E		
N			6.1	332.5
cb			6.0	32.6
1/4			6.0	32.6
c			5.8	32.8
1/4			5.8	32.8
+4			6.1	32.5
+7			5.4	33.2
cb			5.3	333.3
S			4.9	33.7
		200' E		
S			3.9	334.7
cb			4.3	34.3
1/4			5.0	33.6
C			4.9	33.7
1/4			4.9	33.7
cb			5.0	33.6
N			5.6	33.0

		338.58		
		225' E		
N			4.9	333.7
cb			4.4	34.2
1/4			4.3	34.3
c			4.1	34.5
1/4			4.3	34.3
cb			3.8	34.8
S			3.4	35.2
		250 E		
S			2.7	335.9
+7			2.7	35.9
cb			3.5	35.1
1/4			3.5	35.1
c			3.5	35.1
1/4			3.6	35.0
cb			3.3	35.3
+8			2.9	35.7
N			3.6	35.0
		275' E		
N			3.3	335.3

		338.58			
ob			3.3	35.3	
1/4			3.1	35.5	
c			2.9	35.7	
1/4			2.9	35.7	
ob			3.2	35.4	
+5			2.6	36.0	
S			2.1	36.5	
		313.4 E = WL Miss on South			
S			1.4	37.2	
+8			1.3	37.3	
ob			2.1	36.5	
1/4			2.1	36.5	
c			2.2	36.4	
1/4			2.4	36.2	
ob			2.7	35.9	
N			2.7	35.9	
		23.1 E of Last			
N			1.8	336.8	
ob			2.3	35.6	
1/4			1.8	36.8	

		338.58			Mission
C			1.6	37.0	
		46.2 E	of 313.4 = WL Miss.		
S			1.4	37.2	
+7			1.7	36.9	
ob			2.1	36.5	
1/4			1.6	37.0	
C			1.6	37.0	
1/4			1.7	36.9	
ob			2.3	36.3	
+7			2.1	36.5	
N			1.9	36.7	
T.P	10.06	346.68	1.96	336.62	on NW ob
		-46.2 EL. Miss. on angle			
N			8.5	338.2	
+8			8.6	38.1	
+9			9.2	37.5	
ob			9.2	37.5	
1/4			8.8	37.9	
C			8.7	38.0	
1/4			9.0	37.7	

cb		9.5	37.2
+8		9.3	37.4
S		8.9	37.8
	+23.1 on SL		
S		8.9	337.8
cb		9.0	37.7
+3		9.2	37.5
1/4		8.8	37.9
C		8.7	38.0
	0400		
N		8.5	338.2
+7		8.7	38.0
+9		9.2	37.5
cb		9.2	37.5
1/4		8.6	38.1
C		8.5	38.2
1/4		8.6	38.1
cb		9.0	37.7
S		8.6	38.1
	25' E		

S		8.5	338.2
cb		8.6	38.1
1/4		8.2	38.5
C		8.2	38.5
1/4		8.3	38.4
+7		8.8	37.9
cb		8.3	38.4
N		7.9	38.8
	50' E		
N		7.9	338,8
cb		7.9	38.8
+3		7.9	388
+5		8.2	38.5
1/4		7.8	38.9
C		7.7	39.0
1/4		8.0	38.7
+5		8.5	38.2
cb		8.5	38.2
S		8.0	38.7
	75' E		

346.68

S		7.3	339.4
cb		7.6	39.1
1/4		7.6	39.1
C		7.3	39.4
1/4		7.4	39.3
+5		7.7	39.0
cb		7.3	39.3
N		7.3	39.3
	100 E		
N		7.3	39.3
cb		6.7	40.0
+2		6.8	39.9
+5		7.3	39.3
1/2		6.9	39.8
C		6.8	39.9
1/4		7.0	39.7
cb		7.0	39.7
S		6.7	39.9
	125' E		
S		6.3	40.4

346.68 JMission 68

cb	6.3	40.4
+6	6.8	39.9
1/4	6.6	40.1
C	6.4	40.3
1/4	6.6	40.1
+5	7.0	39.7
+7	6.6	40.1
cb	6.6	40.1
N	6.5	40.2
	150' E	
N	6.2	340.5
cb	6.2	40.5
+3	6.2	40.5
+5	6.6	40.1
1/2	6.2	40.5
C	6.1	40.6
1/4	5.9	40.8
+4	6.2	40.5
+6	5.7	41.0
cb	5.5	41.2

346.68

S		5.6	41.1
200' E			
S		4.7	342.0
cb		5.0	41.7
+4		5.1	41.6
+6		5.5	41.2
1/4		5.3	41.4
C		5.2	41.5
1/4		5.3	41.4
+5		5.7	41.0
+8		5.3	41.4
cb		5.3	41.4
N		5.6	41.1
250' E			
N		4.6	342.1
cb		4.5	42.2
+4		4.7	42.0
+6		5.2	41.5
1/4		4.8	41.9
C		4.6	42.1

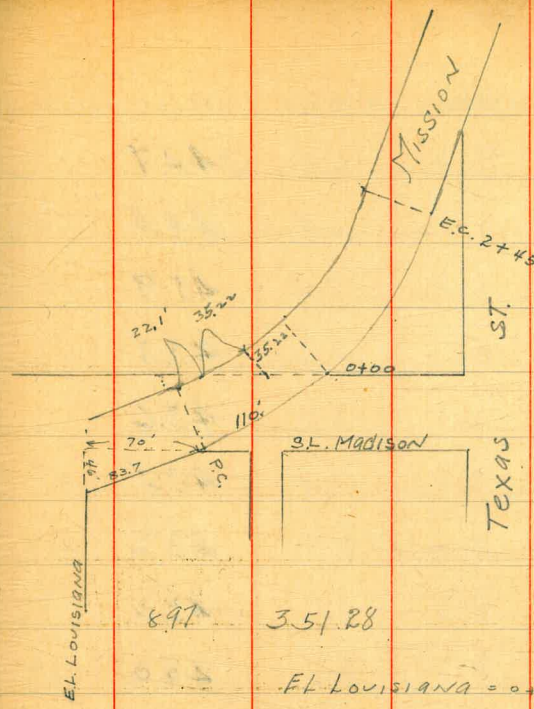
346.68 Mission 69

1/4		4.9	41.8
cb		4.8	41.9
S		4.2	42.5
275' E			
S		4.4	342.3
cb		4.6	42.1
1/4		4.8	41.9
C		4.4	42.3
1/4		4.6	42.1
+5		4.8	41.9
+6		4.2	42.4
cb		4.3	42.4
N		4.5	42.2
313' E = W.L. Louisiana on South			
N		4.5	42.2
cb		4.4	42.3
+6		4.8	41.9
1/4		4.6	42.1
C		4.4	42.3
1/4		5.0	41.7

346.68

⌀		5.4	41.3
S		5.8	40.9
	23.1 E of 313'		
C = WL Louisiana		5.4	341.3
N¼		5.2	41.5
⌀		4.5	42.2
N		4.5	42.2
	46.2 E = WL Louisiana on angle		
N		4.5	342.2
⌀		4.7	42.0
+8		4.7	42.0
+9		5.1	41.6
¼		5.2	41.5
C		5.4	41.3
¼		5.4	41.3
⌀		5.5	41.2
S		5.8	40.9
T.P. check B.M. S.E.B.P. Madison + La.		4.43	342.25 342.31

Mission 70'



	8.9	351.28	342.31 SEBP Madison + Louisiana
	EL Louisiana = 0+00		
S	8.6	342.7	
46' N	8.7	42.6	
	35' E		
23' N	8.5	42.8	
S	8.1	43.2	on Cem walk
	70' E = Intersection SL Mission + SL Madison		
on cem. walk	7.5	343.8	

351.28

NL Madison on Angle = 0+00 on SL Mission

S			6.9	344.4
+10			6.9	44.4
+13			7.1	43.9
Cb			7.6	43.7
1/4			7.7	43.6
C			7.8	43.5
1/4			8.1	43.2
+9			8.1	43.2
+11			7.3	44.0
Cb			7.1	44.2
N	= -70.44 Sta		7.1	44.2
		- 35.22		
N			6.3	345.0
+12			6.3	45.0
Cb			6.9	44.4
+12			7.5	43.8
1/4			7.8	43.5
C	ON NL Madison		7.8	43.5

351.28

0+00 Sta. on SL

Mission

71

S		6.9	344.4
Cb		7.0	44.3
+7		6.8	44.5
1/4		7.2	44.1
C		6.5	44.8
1/4		6.4	44.9
+5		6.5	448
Cb		6.9	44.4
+5		6.4	44.9
N		6.1	45.2
	+ 30.68		
N		6.1	345.2
+10		6.5	448
Cb		6.6	44.7
+3		6.3	45.0
1/4		6.1	45.2
C		6.3	45.0
1/4		6.7	44.6
Cb		6.3	45.0
S		6.3	45.0

351.28

+61.36

S	6.1	45.2
cb	5.8	45.5
1/4	6.3	45.0
e	5.8	45.5
1/4	5.8	45.5
+5	6.0	45.3
cb	6.4	44.9
+5	6.0	45.3
N	6.0	45.3

+92.04

N	5.6	345.7
+12	5.3	46.0
cb	5.7	45.6
+2	6.2	45.1
+6	5.6	45.7
1/4	5.4	45.9
c	5.4	459
+7	5.6	45.7
1/4	6.1	45.2

351.28

Mission 72

+3	5.9	45.4
+5	5.5	45.8
cb	5.4	45.9
S	5.2	46.1

+122.72

S	5.1	3462
cb	5.4	45.9
+2	5.4	45.9
+4	5.8	45.5
1/4	5.3	46.0
C	5.0	46.3
1/4	5.4	45.9
+3	5.7	45.6
+6	5.2	46.1
cb	5.2	46.1
N	5.4	45.9

+153.40

N	5.1	462
cb	5.0	46.3
1/4	5.1	46.2

		351.28		
+5			5.5	45.8
C			5.2	46.1
+5			4.9	46.4
1/4			4.9	46.4
cb			5.5	45.8
+3			5.7	45.6
+5			5.1	46.2
S			5.1	46.2
		+184.08		
S			5.1	346.2
+5			5.4	45.9
cb			4.8	46.5
1/4			4.8	46.5
C			5.1	46.2
1/4			5.0	46.3
cb			5.0	46.3
N			5.1	46.2
		+214.76		
N			4.8	48.5
cb			4.8	46.5

		351.28		Mission 73
1/4			5.0	46.3
C			5.0	46.3
1/4			5.2	46.1
cb			5.1	46.2
S			5.2	46.1
		+245.23	= E.C.	
S			6.3	45.0
+10			6.6	44.7
+13			5.8	45.5
cb			5.7	45.6
1/4			5.6	45.7
C			5.6	45.7
1/4			5.4	45.9
cb			5.3	46.0
N			5.0	46.3
		275		
N			5.5	45.8
cb			5.7	45.6
1/4			5.8	45.5
+3			5.9	45.4

		351.28		
+5			6.3	45.0
C			6.6	44.7
1/4			7.0	44.3
cb			7.3	44.0
S			7.8	43.5
		300'		
S			8.7	342.6
cb			7.9	43.4
1/4			7.7	43.6
C			7.3	44.0
1/4			6.1	45.2
cb			5.8	45.5
N			5.8	45.5
		315'		
N			5.8	345.5
cb			6.0	45.3
1/4			6.4	44.9
C			6.5	44.8
1/4			7.0	44.3
cb			7.7	43.6

		351.28		Mission 74
S			9.1	42.2
		335' N		
S			7.8	343.5
cb			6.6	44.7
1/4			6.1	45.2
C			5.8	45.5
1/4			5.4	45.9
+3			5.4	45.9
+7			6.0	45.1
cb			6.2	45.1
N			6.1	45.2
		369'		
N			7.1	344.2
cb			7.1	44.2
1/4			7.1	442
C			7.7	43.6
1/4			9.6	41.7
cb			10.7	40.6
S			12.8	38.5
+5			17.0	34.3

		351.28		
		371' N		
-5			18.2	333.3
S			18.0	33.3
+7			15.4	35.9
cb			12.4	38.9
+4			10.2	41.1
1/4			9.0	42.3
C			7.9	43.4
1/4			7.3	44.0
cb			7.1	44.2
N			7.3	44.0
		390' N		
N			8.4	342.9
cb			8.8	42.5
1/4			9.5	41.8
C			10.2	41.1
+6			11.1	40.2
1/4			14.4	36.9
T.P.	534	343.69	12.93	338.35
cb			12.7	31.0

		343.69		
S			14.0	29.7
+10			14.1	29.6
		400'		
-10			14.0	329.7
S			14.1	29.6
cb			13.2	30.5
+3			12.9	30.8
1/4			10.0	33.7
C			5.0	38.7
+3			3.0	40.7
1/4			1.9	41.8
cb			1.7	42.0
N			0.8	42.9
		415'		
N			0.3	343.4
+7			1.5	42.2
cb			1.6	42.1
1/4			2.1	41.6
+6			2.9	40.8
C			5.7	38.0

	343.69		
1/4		11.3	332.4
+5		13.1	30.6
cb		13.4	30.3
+6		14.3	29.4
S		14.4	29.3
+10		14.5	29.2
	440'		
-10		15.8	27.9
S		15.3	28.4
cb		15.0	28.7
+8		13.6	30.1
1/4		12.9	30.8
C		9.4	34.3
+2		8.7	35.0
+3		5.6	38.1
+8		1.5	42.2
1/4		1.2	42.5
cb		1.4	42.3
N		0.7	43.0
	469'		

	343.69		Mission	76
N		1.2	342.5	
cb		2.8	40.9	
1/4		4.0	39.7	
C		6.1	37.6	
+2		10.3	33.4	
1/4		12.4	31.3	
cb		14.1	29.6	
S		15.7	28.0	
+5		21.4	22.3	
+10		22.1	21.6	WL Texas St Grade
	472'			
-10		22.5	21.2	
S		21.5	22.2	
+8		21.3	22.4	
cb		19.6	24.1	
+4		18.5	25.2	
+7		14.2	29.5	
+8		13.2	30.5	
1/4		12.8	30.9	
+5		11.6	32.1	

		343.69			
C			9.6	34.9	
+2			6.4	37.3	
1/4			4.1	39.6	
cb			2.8	40.9	
N			1.2	42.5	
		488'			
N			1.1	342.6	
+10			2.4	41.3	
cb			3.5	40.2	
+5			4.2	39.5	
1/4			5.4	38.3	
+5			6.5	37.2	
C			7.9	35.8	
+2			8.6	35.1	
+3			11.2	32.5	
1/4			13.4	30.3	
+5			18.5	25.2	
cb			20.5	23.2	
+10			25.1	18.6	WL Texas St Grade
S			24.8	18.9	

		343.69		Mission	77
+2			22.6	21.1	EL Texas St Grade
		496'			
-17			23.5	320.2	✓ ✓ ✓
S			25.3	18.4	
+8			26.1	17.6	WL ✓
+9			25.2	18.5	
cb			23.0	20.7	
+3			20.7	23.0	
+5			12.1	31.6	
1/4			10.7	33.0	
C			8.2	35.5	
1/4			5.8	37.9	
cb			3.6	40.1	
N			1.0	42.7	
		506			
N			2.4	41.3	
cb			6.0	37.7	
1/4			8.6	35.1	
C			12.8	30.9	
+5			14.1	29.8	

		343.69			
1/4			19.3	24.4	
cb			26.0	17.7	
+3			26.5	17.2	WL Texas Gra
S			25.2	18.5	
+10			24.5	19.2	EL ✓ ✓
		519'			
S			26.0	317.7	✓ ✓ ✓ ✓
cb			28.3	15.4	
+5			29.2	14.5	
1/4			25.5	18.2	
C			21.0	22.7	
1/4			14.8	28.9	
cb			9.8	33.9	
+8			7.7	36.0	
+12			5.3	38.4	
N			4.3	39.4	
		537			
N			5.9	337.8	
cb			13.4	30.3	
+7			16.6	27.1	

		343.69			MISSION 78
1/4			19.5	24.2	
+3			25.8	17.9	
C			30.5	13.2	
+3			31.3	12.4	WL Grade
1/4			30.4	13.3	
cb			29.8	13.9	
+3			29.3	14.4	EL ✓
		550'			
cb +5			31.2	312.4	✓ ✓
1/4			31.9	11.8	
C			32.8	10.9	WL ✓
1/4			29.0	14.7	
+4			27.4	16.3	
cb			17.4	16.3	
N			12.1	31.6	
T.P.	0.64	331.66	12.67	331.02	
		580'			
N			9.5	322.2	
+4			21.9	309.8	
cb			24.8	306.9	WL ✓

		331.66			
1/4			23.5	308.2	
+7			22.6	309.1	EL Grade
		590'			
W 1/4			24.1	307.6	✓ ✓ ✓
⌀			25.5	306.2	
+5			25.9	305.8	NL ✓
N			19.0	312.7	
		609'			
N			28.0	303.7	✓ ✓ ✓
W Cb			26.1	305.6	EL ✓
		638'			
NL			29.8	301.9	EL ✓
TP	13.14	344.16	0.64	331.02	
TP	9.05	351.37	1.84	342.32	
check to BM.			9.05	342.32	342.31

Levels on 010 S.L. of Mission
Between Madison & Texas

MISSION 71

	8.53	350.84	342.31	Louisiana & SEBP Mission
0+00 = NL Madison & SL Mission'				
SL = Newline		6.5	44.3	
25' S = old SL of Mission		6.33	44.5	on SE M.Cb of Madison
	+ 3.068 N'			
SL		5.9	44.9	
+10 S		5.9	44.9	
+14		5.0	45.8	
+25 = 0 SL		5.1	45.7	
	+61.36 N			72' N & 25' S = NW Cor. of House under construction
SL		5.7	45.1	
+3 S		5.5	45.3	
+5		5.0	45.8	
+25 = 0 SL		4.4	46.4	
	+92.04 N			
SL		4.9	45.9	
+25 = 0 SL		3.8	47.0	
	+122.72 N			
SL		4.7	46.1	
+25 = 0 SL		4.0	46.8	

350.84

	153.40 N		
SL of Newline		4.7	46.1
+11 S		4.3	46.5
+25' S = 0 SL		3.5	47.3
	168' N		
SL		4.4	46.4
+1 N		4.1	46.7
+15		2.8	48.0
+25 S = 0 SL		2.6	48.2
	184.08' N		
SL		4.7	46.1
25' S = 0 SL		3.9	46.9
	214.76' N		
SL		4.8	46.0
25' S = 0 SL		5.3	44.5
	245.23 N = EC		
SL		6.0	44.8
25' S on Old Hub		6.60	44.2

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.