1038

LEVEL BOOK

373

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

Levels over Property lines of Belt St. Broadway & Davis to Laurel. Hanover & McElwaine

					BM Top Hyat S.E. At. & Ivy.
	2.80	11.60		8.80	
		No line Hawthorn			
E.			5.7	5.9	
W.			6.9	4.7	
		50' N.			
W.			7.3	4.3	
E			6.5	5.1	
		100' N.			
E			7.2	4.4	
W			7.2	4.4	
		150' N.			
W			7.6	4.0	
E			7.2	4.2	
		200' N.			
E			6.5	5.1	
W.			6.8	4.8	
		250 N.			
W.			6.4	5.2	
E			6.4	5.2	

	300' N.	
E	6.2	5.4
W	6.1	5.5
	350' N.	
W	5.7	5.9
E	6.4	5.2
	390' N.	
E	5.0	6.6
	400' N.	
E	6.1	5.5
W.	5.9	5.7
	450' N.	
W.	6.3	5.3
E	5.8	5.8
	500' N.	
E	5.9	5.7
W	6.6	5.0
	550' N.	
W	5.4	6.2
E	5.1	6.5

H1
1160

T.P.	4.05	11.05	4.60	7.00
		570 N.		
E			4.3	6.7
		600' N.		
E			5.6	5.4
W.			5.2	5.8
		680.38' N. = Saline Juniper		
W.			4.7	6.3
E.			6.0	5.0
		No. line Juniper		
E			5.3	5.7
W.			4.5	6.5
		100' No		
W.			5.2	5.8
E			4.7	6.3
		200' No		
E			6.5	4.5
W.			5.3	5.7

		300' No		
W.			5.6	5.4
E			6.8	4.2
T.P	2.99	7.61	6.43	4.62
		400' No		
E.			4.2	3.4
W.			3.3	4.3
		457.4 No = P.C		
W.			4.1	3.5
E			5.0	2.6
		500' N.		
E			6.2	2.4
W			4.7	2.9
		550' No		
W.			5.2	2.2
E			6.0	1.6
		600' No		
E			6.2	1.2
W			5.9	1.7

		M1 7.61		
		650' No		
W.			6.4	1.7
E			6.8	0.8
	680.76 No = So line Laurel.			
E			7.0	0.6
W			6.8	0.8
Hub SW Bolt & Laurel			6.68	0.93
	1.77	10.57		8.80 BM. SW Ivy & At. Top Hill
		So line Hawthorn		
E			6.0	
W.			5.6	
	82.09 on W	82.12 on E	So Hawthorn PC 0+00	
W.			5.7	
E			6.0	
T.P.	5.38	9.92	6.03	4.54
		50' So P.C		
E			5.0	
W			4.6	
		100' So P.C		
W			4.8	
E			5.0	
		150' So P.C		
E			4.4	
W.			4.7	
		200' So P.C		
W			5.0	
E			5.3	
		219' So PC = No line Grape on E.		
E			5.1	
		West Line Belt.		
250' So PC.			5.1	
300' "			5.5	
350' "			5.1	
400' "			4.1	
450"			4.4	
500 "			4.7	
550 "			4.8	
600' "			5.0	
617 "			4.7	
613 "			9.7	
606			9.6	

9.9 x 141

West Line Belt St

630 So.			4.5	
634 "			5.4	
650 "			5.0	
680 "			5.1	
688 "			4.2	
700.58 "	No line Date		7.4	

E Line Belt

So line Grape			4.8	
50' So "			5.5	
100' " "			5.2	
150 " "			4.6	
200 " "			5.3	
250 " "			4.9	
300 "			4.8	
T.P.	x60	8.92	3.60	6.32
350 "			3.3	
400 "			3.9	
405 "			3.3	
x408 "			4.5	

x408 So Grape	7.5	
418 "	7.2	
418 "	4.7	
422 "	3.2	
445 "	4.2	
450	5.8	
454.5 N.L. Date	6.3	
℄ Date St		
E	7.2	
W	9.0	
So Line Date		
W	4.0	
E	4.32	on hub
100' So Date		
E	3.7	
W	3.6	
200' So Date		
W	3.1	
E	3.2	

8.9 W H1

T.P.	5.60	11.51	3.01	5.91

300' So. Date

E	5.1
W.	5.0

400' So. Date

W.	4.5
E.	5.0

500' So. Date

E.	4.4
W.	4.9

600' So. Date

W.	4.9
E.	5.2

6590.6' So. Date. N. Line Beech

E	5.3
W.	4.6

So Line Beech

W.	3.8
E	5.4

100' So. Beech

E	5.1
W.	3.8

T.P.	4.36	11.29	3.57	7.94

200' So. Beech

W	5.0
E.	5.8

300 So. Beech

E	5.8
W	4.7

400 So. Beech

W	4.1
E.	5.1

500' So. Beech

E.	4.9
W.	4.9

600' So. Beech

W.	4.6
E.	4.8

12.79 M

679.62 So Beach - No Line "A" St

E			5.1		
T.P W.	4.07	12.20	4.16	8.13	on hub.

So Line "A" St

W			4.3		
E			5.5		

100' So A

E			5.7		
W			4.1		

150' So A

W.			4.1		

200' So A

W.			4.4		
E			5.1		

300' So A

E			6.0		
W.			4.7		

400' So A

W			4.6		
E			6.0		

500' So A

E			6.1		
W.			5.2		
T.P.	4.61	11.99	4.87	7.38	

600 So A

W.			4.9		
E			5.2		

700 S. A

E			4.7		
W.			5.6		

800' So A

W.			5.3		
E			5.5		

900' So A

E			6.0		
W			5.9		

1000' So A

W			5.8		
E			6.0		

11.99 PM.

10.19.66 So A = Top rail

E. 6.17

10.14.66 So. A. Top rail

E. 5.85

10.18.66 So A. N. Line Broadway

E 5.7

TP W = Top No rail 5.65 6.84

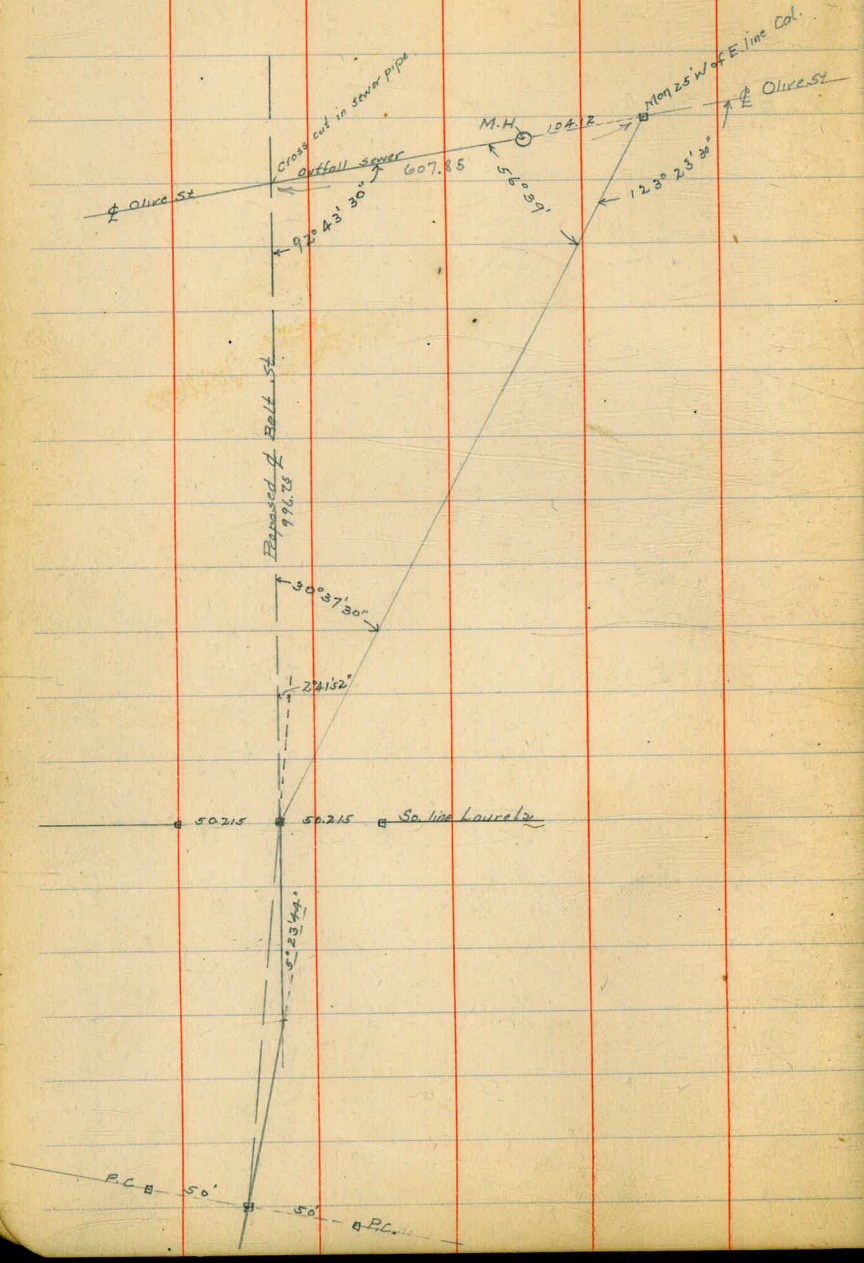
4/26/18 Gregory Moody Miller — Levels on Sewer pipe etc. at Neptune, Steele, and Arrow Packing Plants

B.M.	2.05	10.85	8.	8.80	BM. Top H-d. N/E of Atlantic
T.P.	2.51	10.63	2.73	8.12	
			4.94	5.69	on floor of Toilet room
			6.15	4.48	= on elbow of floor drain. below floor.

Toilets + Drain is 223' from W.L. of Belt St.

B.M.	2.22	11.02		8.80	Top H-d. N/E of Atlantic
			7.89	3.13	= Top of Soil Pipe 67' No. of Junction on W.L. Belt St.
T.P.	3.47	8.92	5.57	5.45	
			8.33	+0.59	Top 6"x6" soil pipe = 422' No. of Junction on W.L. Belt St.

Ties from Proposed ℄ Belt St to Olive St Outfall Sewer



Levels over proposed center line of Belt St from So. line Laurel to Olive St outfall sewer.

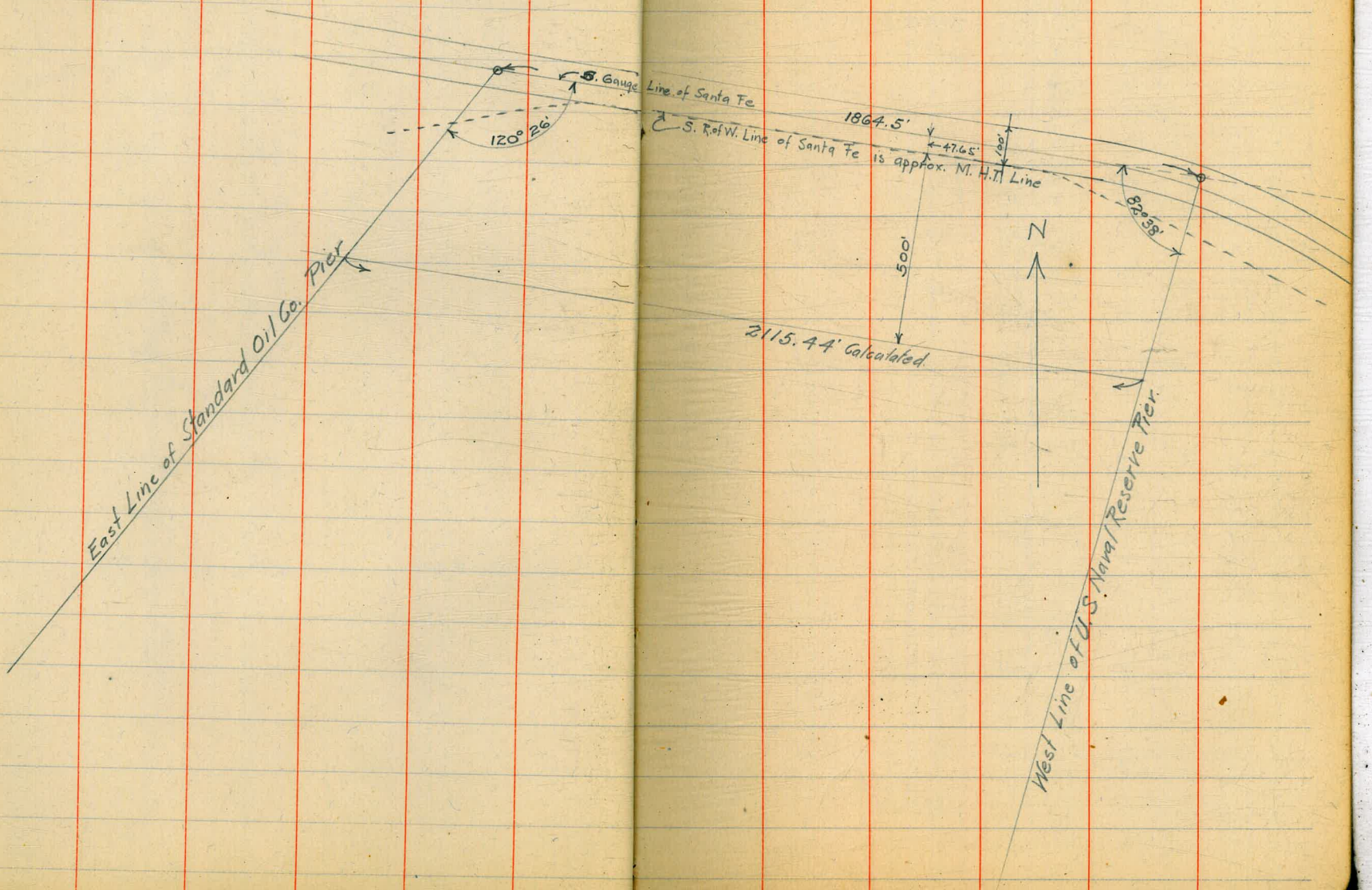
Doris Hancock
Mc Elwaine.

3.43 H.I. 4.36 0.93 B.M. Hub S.W. Belt & Laurel

0+00 So. Line Laurel	3.7	0.7
1	4.0	0.4
2	4.7	-0.3
3	5.3	-0.9
4	8.6	-4.2
5	9.4	-5.0
6	9.6	-5.2
7	10.2	-5.8
8	10.6	-6.2
9	10.9	-6.5
+96.75	11.8	-7.4
+96.75 Top Olive St outfall	5.5	-1.1

{Hayler
Bartlett
Brooks.

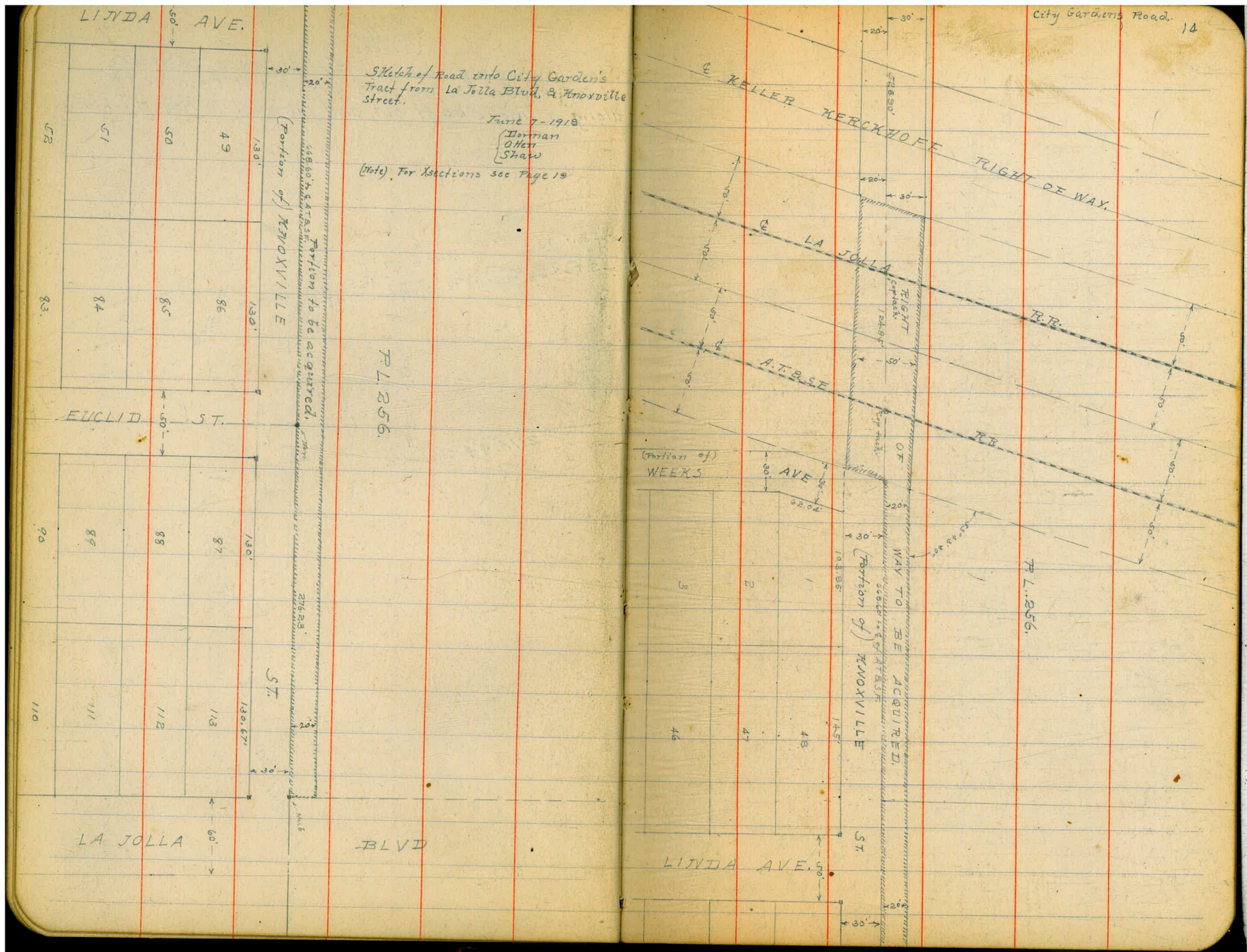
Sketch showing approximate distance between Standard Oil Co. Pier and U.S. Naval Reserve Pier along a line 500 ft out and parallel to Mean H.T. Line.

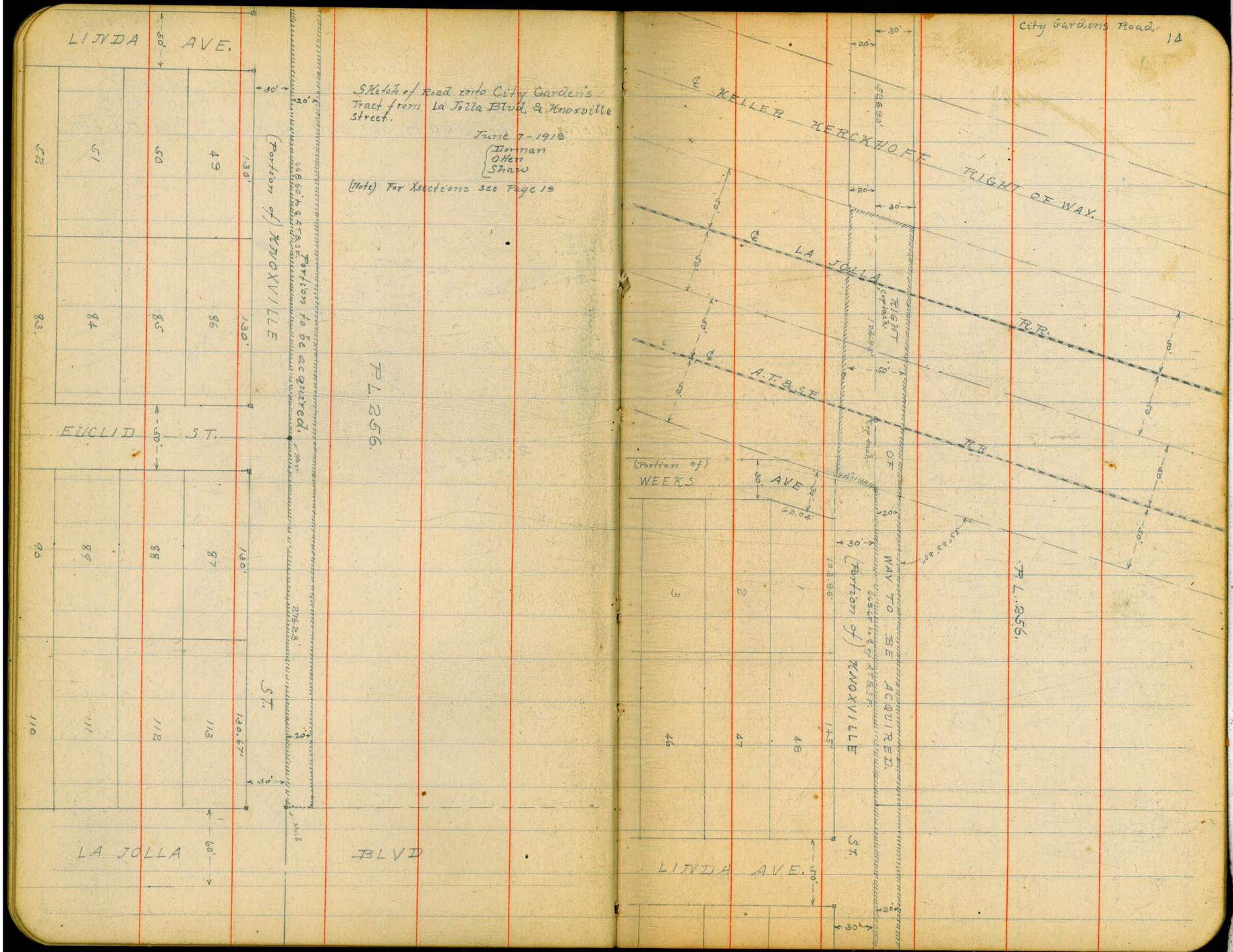


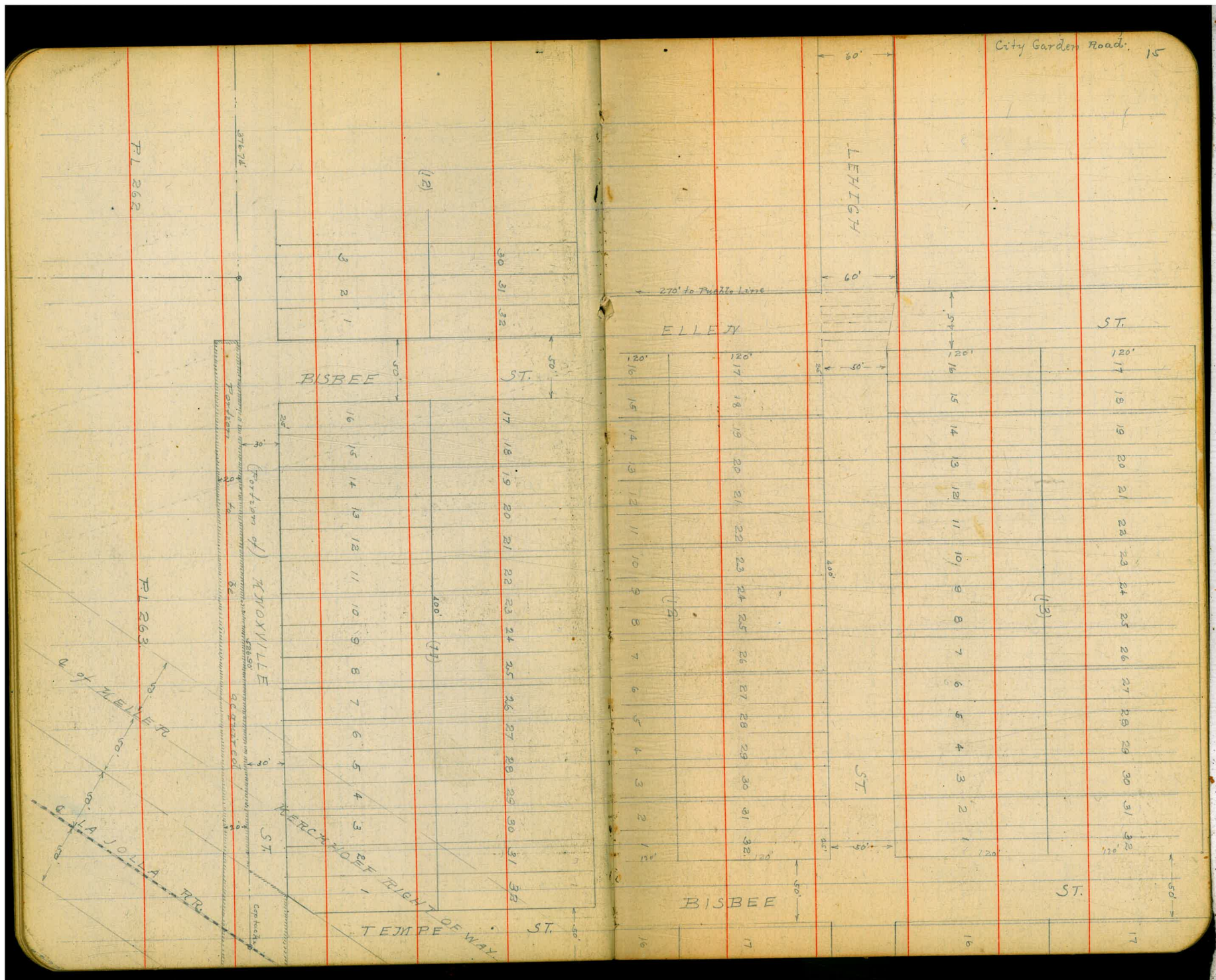
Sketch of Road into City Gardens Tract from La Jolla Blvd. & Knoxville Street.

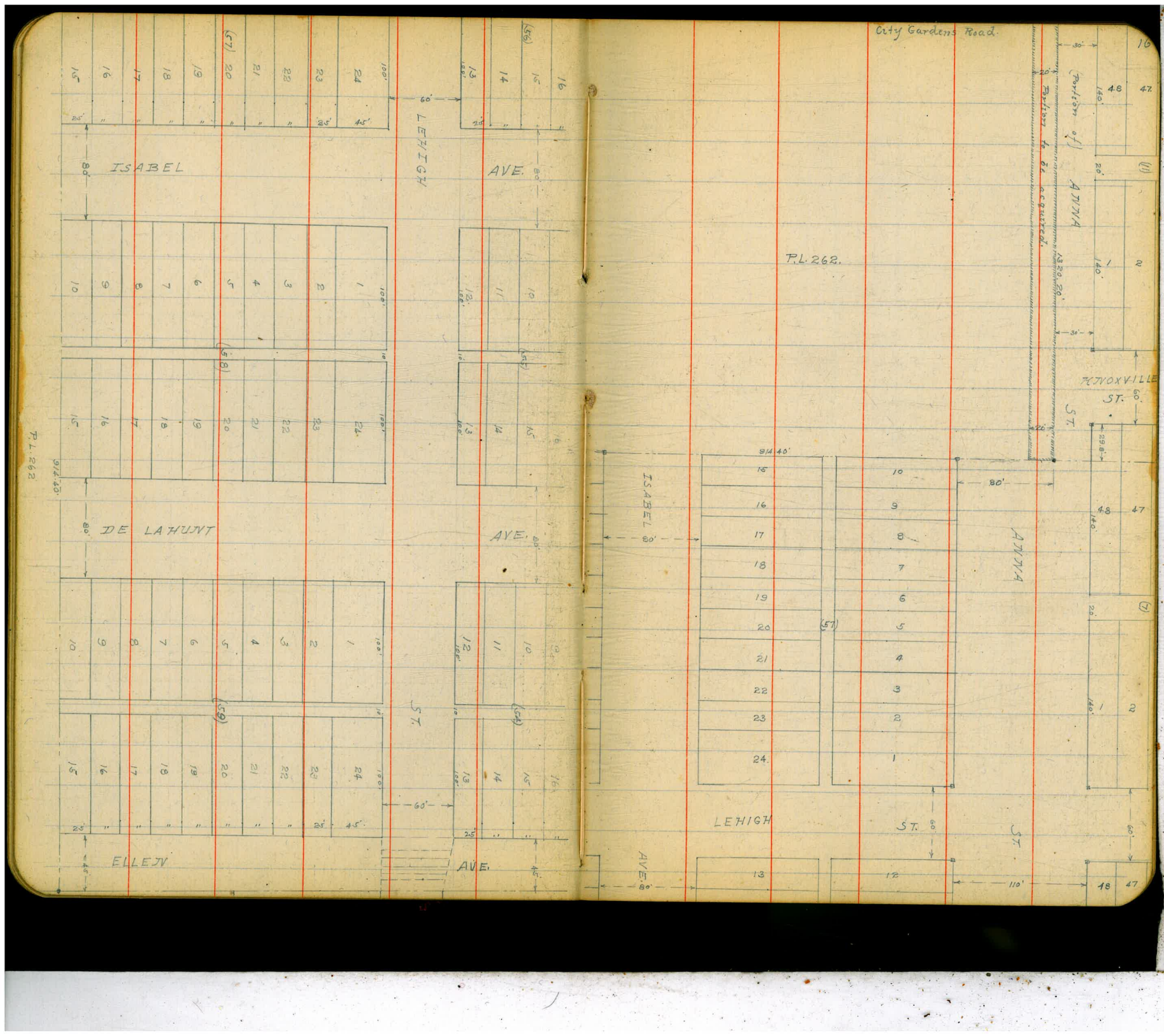
June 7-1918
(Dorman
Olsen
Shaw

(Note) For Xsections see Page 19

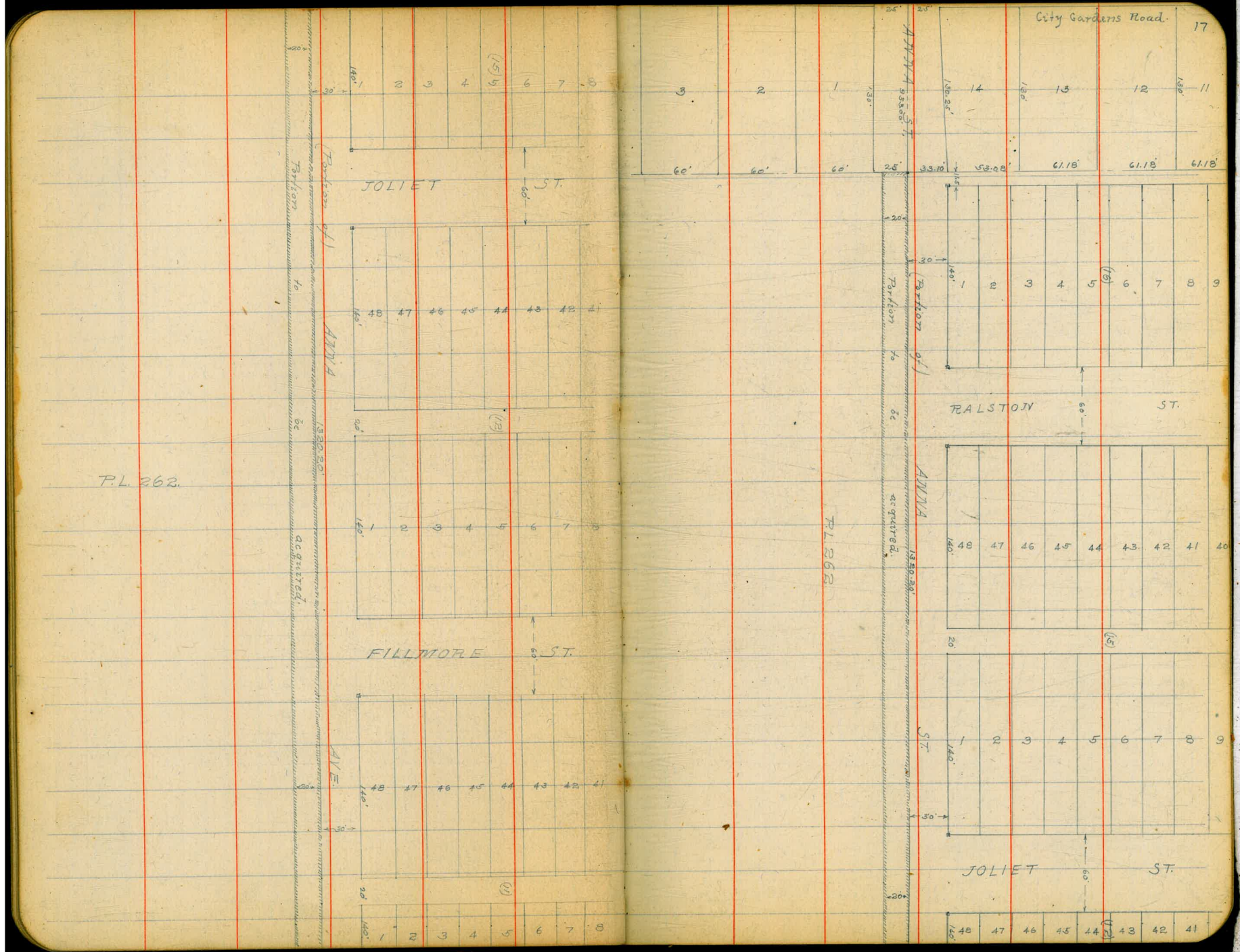


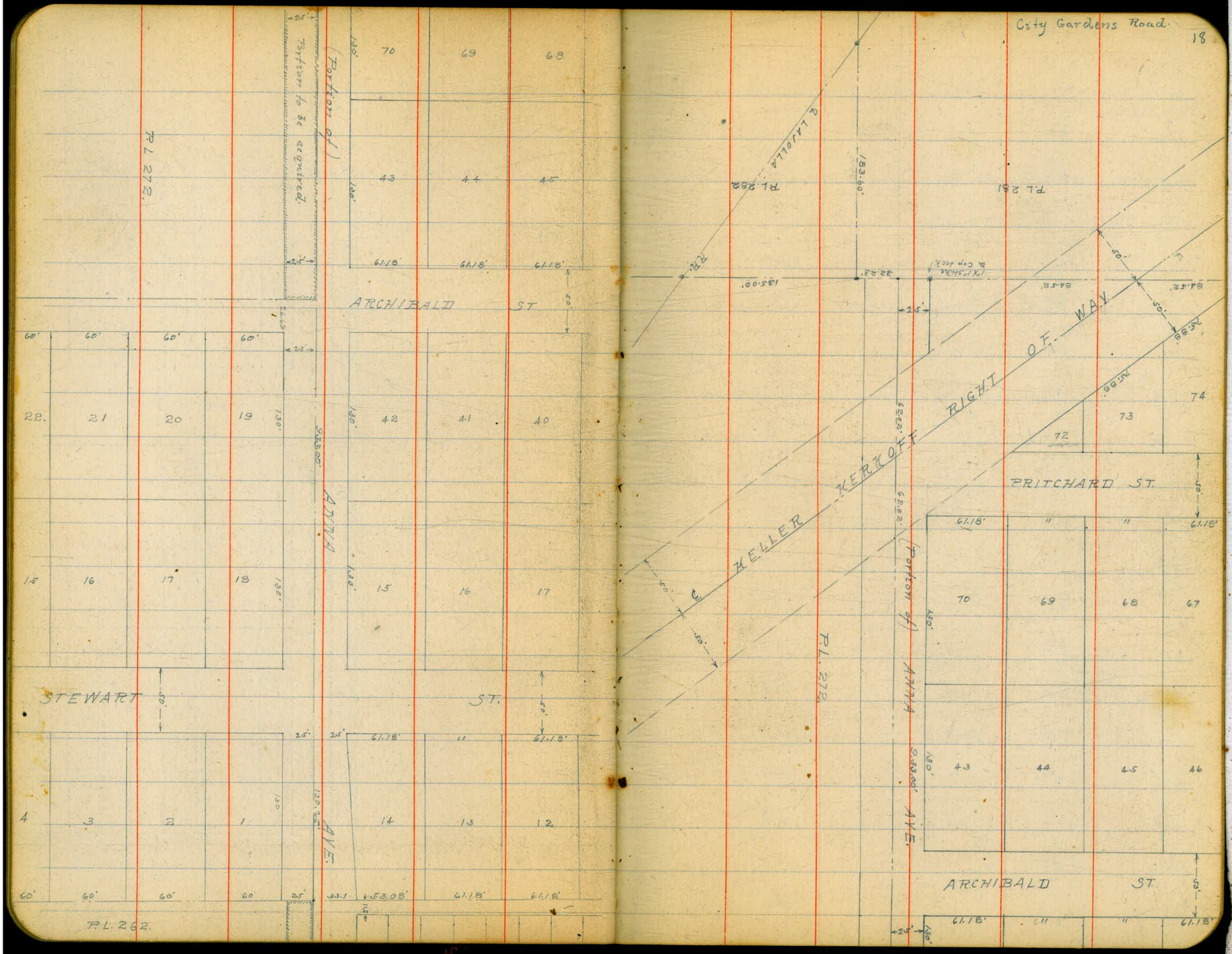

LINDA AVE.
EUCLID ST.
LA JOLLA BLVD
(Portion of) KNOXVILLE ST.
Portion to be acquired.
Portion of KNOXVILLE ST.
WEEKS AVE
LINDA AVE.
℄ KELLER KERCKHOFF RIGHT OF WAY.
℄ LA JOLLA R.R. RIGHT
A.T.&S.F. R.R.
(Portion of) WAY TO BE ACQUIRED.
(Portion of) KNOXVILLE ST.
PL. 256.
PL. 256.
Sketch of Road into City Gardens Tract from La Jolla Blvd. & Knoxville Street.
June 7-1918
Norman
Olsen
Shaw
(Note) For Xsections see Page 19


LEHIGH
ELLEN
BISBEE
ST.
TEMPE
WAY
(12)
(13)
(17)
(18)
(19)
(20)
(21)
(22)
(23)
(24)
(25)
(26)
(27)
(28)
(29)
(30)
(31)
(32)
120'
50'
60'
400'
270' to Public Lane
PL 262
PL 263
Portion of KNOXVILLE
Portion
Q of ALLEY
Q of STREET
SO. LA JOLLA RR.
Cap for Ch
TEMPE WAY
ST.


City Gardens Road.
P.L. 262.
ISABEL
LEHIGH
AVE.
DE LAHUNT
ELLEN
ST.
ANNA
KENSINGTON
Portion of
Portion to be acquired.
P.L. 262

City Gardens Road.




City Gardens Road.
18
PL 272.
(Portion of) ATTILA AVE.
ARCHIBALD ST
STEWART ST.
PRITCHARD ST.
KELLER
KERKOFF
RIGHT OF WAY
PL. 272.
PL. 261
PL. 262
70
69
68
67
74
73
72
43
44
45
46
42
41
40
22.
21
20
19
16
17
18
15
14
13
12
4
3
2
1
61.18'
60'
25'
50'
130'
183.60'
185.00'
84.55'
32.23'
33.1
53.08'

Sections for Road from La Jolla Blvd & Knoxville St to the E.L of the City Gardens Tract.

(Norman
Olsen
Sharo June 7-1918.

B.M. Horn, Tecolote Bridge (new) 1st curve S.E. North side La Jolla Blvd, 309' East of City Hydrant, Brass Plug 22.34

	+	H.I.	−	Ele
	0.90	23.24		22.34
	1.12	12.19	12.17	11.07 on Hydrant.

Commenceing on the Cen of La Jolla Blvd.

W.L.			3.7	8.5
cl			3.7	8.5
1/4			3.7	8.5
c			3.9	8.1
1/4			3.8	8.4
cl			3.9	8.3
E.L.			3.9	8.3

S 1/4 La Jolla Blvd.

E.L.			3.9	8.3
cl			3.9	8.3
1/4			4.0	8.2
c			4.0	8.2

	+	H.I. 12.19	−	
1/4			4.0	8.2
cl			3.9	8.3
W.L			3.9	8.3

1/2 + 4

W.L			4.0	8.2
cl			4.0	8.2
1/4			4.1	8.1
c			4.2	8.0
1/4			4.0	8.2
cl			4.1	8.1
E.L			4.2	8.0

South Curb.

E.L.			6.9	5.3
cl			7.2	5.0
1/4			7.4	4.8
c			7.5	4.7
1/4			7.2	5.0
cl			7.2	5.0
W.L			7.2	5.0
cl				

	+	⊼ 12.19	−	
	00=S. L. La Jolla Blvd.			
W.L			7.9	4.3
cl			7.8	4.4
½			7.8	4.4
c			8.0	4.2
½			7.9	4.3
cl.			7.8	4.4
E.L. +50			8.1	4.1
E.L.			7.5	4.7
cl.			7.3	4.9
½			7.0	5.2
c			6.8	5.4
½			7.0	5.2
cl.			7.3	4.9
W.L 1+00			7.1	5.1
W.L			7.5	4.7
cl			7.6	4.6
½			7.2	5.0
c			7.1	5.1
½			7.3	4.9
cl			7.7	4.5
E.L. 1+50			7.9	4.3
E.L			8.2	4.0
cl			8.0	4.2
½			7.8	4.4
c			7.0	5.2
½			7.6	4.6
cl			8.0	4.2
W.L 2+00			8.1	4.1
W.L			8.6	3.6
cl			8.4	3.8
¼			8.0	4.2
c			7.5	4.7
½			8.3	3.9
cl			8.7	3.5
E.L. 2+50			8.7	3.5
E.L			9.2	3.0
cl			9.2	3.0
¼			9.1	3.1
c			8.5	3.7

	+	℄ 12.19	−		
⅛					
¼			8.6	3.6	
cl			9.0	3.2	
W. L. 2+60.67 = North L. of Euclid St.			9.2	3.0	
W. L.			9.2	3.0	
cl			9.0	3.2	
⅛			8.7	3.5	
c			8.4	3.8	
⅛			8.9	3.3	
cl			9.1	3.1	
E. L.			9.1	3.1	
#	3.29	6.33	9.15	3.04 Mon. in E. Cor Euclid.	
	North Curb Euclid St.				
E. L.			3.6	2.7	
cl			3.4	2.9	
¼			3.3	3.0	
c			2.8	3.5	
¼			2.9	3.0	
cl			3.1	3.2	
W. L.			3.4	2.9	

	+	℄ 6.33	−		
	N ½ Euclid St.				
W. L.			3.4	2.9	
cl			3.3	3.0	
⅛			2.6	3.7	
c			2.7	3.6	
⅛			3.1	3.2	
cl			3.3	3.0	
E. L.			3.6	2.7	
	Cen Euclid St.				
E. L.			3.4	2.9	
cl			3.3	3.0	
⅛			3.1	3.2	
c			2.7	3.6	
⅛			2.9	3.0	
cl			3.2	3.1	
W. L.			3.4	2.9	
	S ¼ Euclid St.				
W. L.			3.6	2.7	
cl			3.2	3.1	
⅛			2.8	3.5	

	+	T 6.33	−	
c			2.8	3.5
½			3.3	3.0
cl			3.5	2.8
E.L.			3.4	2.9
	S. Curb Euclid St.			
E.L.			3.6	2.7
cl			3.4	2.9
½			3.3	3.0
c			3.1	3.2
½			2.9	3.4
cl			3.2	3.1
W.L.			3.6	2.7
	00= S.L Euclid St.			
W.L.			3.3	3.0
cl			3.3	3.0
½			3.1	3.2
c			2.9	3.4
½			3.5	2.8
cl			3.6	2.7
E.L.			3.6	2.7

	+	T 6.33	−	
+50 E.L.			4.0	2.3
cl			3.8	2.5
½			3.9	2.4
c			3.6	2.7
½			3.1	3.2
cl			3.7	2.6
W.L. 1+00			3.7	2.7
W.L.			4.0	2.3
cl			4.1	2.2
½			4.0	2.3
c			3.7	2.6
½			3.9	2.4
cl			4.1	2.2
E.L. 1+50			4.2	2.1
E.L.			4.7	1.6
cl			4.6	1.7
½			4.6	1.7
c			4.4	1.9
½			4.2	2.1
cl			4.2	2.1

	+	⊼ 6.33	—	
W. L 2+00			4.3	2.0
W. L.			4.8	1.5
cl			4.6	1.7
½			4.6	1.7
c			4.6	1.7
½			4.7	1.6
cl			4.7	1.6
E. L. 2+50			4.6	1.7
E. L			5.3	1.0
cl			5.2	1.1
½			5.1	1.2
c			4.6	1.7
½			4.6	1.7
cl.			5.0	1.3
W. L 2+60 = North L. Linda Ave.			4.8	1.5
W. L			5.0	1.3
cl			4.8	1.5
½			4.6	1.7
c			4.3	2.0
½			4.8	1.5

	+	⊼ 6.33	—	
cl			5.0	1.3
E. L.			5.4	0.9
N. Cē Linda Ave.				
E. L			5.2	1.1
cl			5.0	1.3
½			4.7	1.6
c			4.4	1.9
½			4.1	2.2
cl			4.3	2.0
W. L			4.5	1.8
N ¼ Linda Ave.				
W. L.			4.4	1.9
cl			4.2	2.1
½			4.1	2.2
c			4.2	2.1
½			4.5	1.8
cl			4.8	1.5
E. L.			5.1	1.2
Cen. Linda Ave.				
E. L.			5.1	1.2

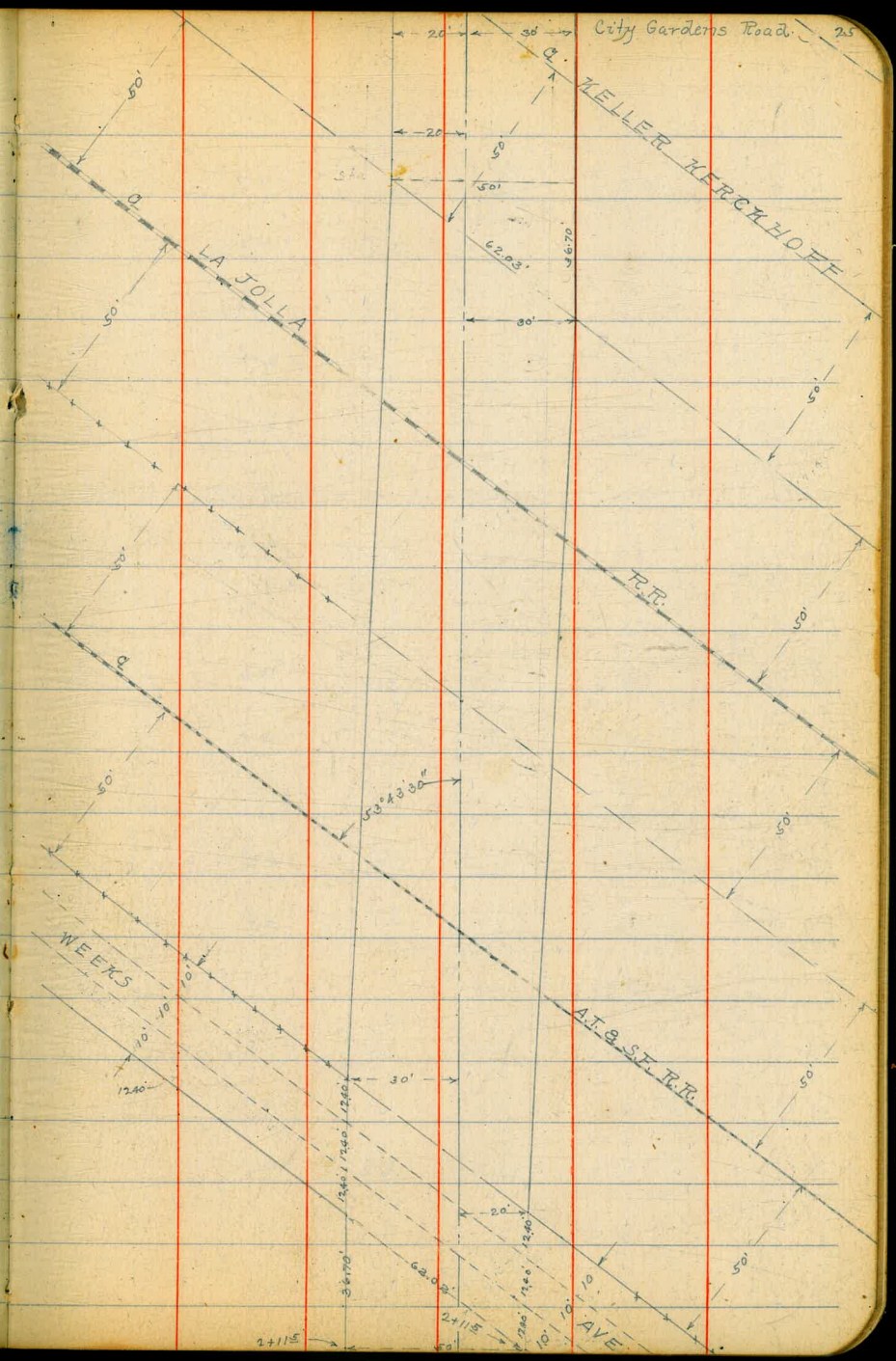
	+	⊼ 6.33	−	
cl			4.7	1.6
½			4.4	1.9
c			4.1	2.2
½			4.1	2.2
cl			4.3	2.0
W.L.			4.5	1.8
	S ½ Linda Ave.			
W.L.			4.5	1.8
cl			4.3	2.0
½			4.1	2.2
c			4.1	2.2
½			4.3	2.0
cl			4.6	1.7
E.L.			4.8	1.5
	S.C. Linda Ave.			
E.L.			4.5	1.8
cl			4.6	1.7
½			4.3	2.0
c			4.3	2.0
½			4.1	2.2

	+	⊼ 6.33	−	
cl.			4.5	1.8
W.L.			4.5	1.8
	00 = S.L. of Linda Ave.			
W.L.			4.7	1.6
cl			4.6	1.6
½			4.4	1.9
c			4.2	2.1
½			4.5	1.8
cl.			4.6	1.7
E.L. 0+50			4.3	2.0
E.L.			4.9	1.4
cl			5.1	1.2
½			5.1	1.2
c			5.2	1.1
½			5.2	1.1
cl			5.2	1.1
W.L. 1+00			5.2	1.1
W.L.			5.7	0.6
cl			6.1	0.2
½			6.0	0.3

	+	π 6.33	−	
c			5.1	1.2
1/8			5.1	1.2
cl.			5.2	1.1
E.L. 1+50			5.3	1.0
E.L			6.2	0.1
cl			6.2	0.1
1/8			6.3	0.0
c			5.6	0.7
1/8			5.6	0.7
cl			5.9	0.4
W.L. 2+00			5.9	0.4
W.L			5.8	+ 0.5
cl			7.0	− 0.7
1/8			6.8	− 0.5
c			6.4	− 0.1
1/8			6.7	− 0.4
cl			6.5	− 0.2
E.L.			6.1	+ 0.2

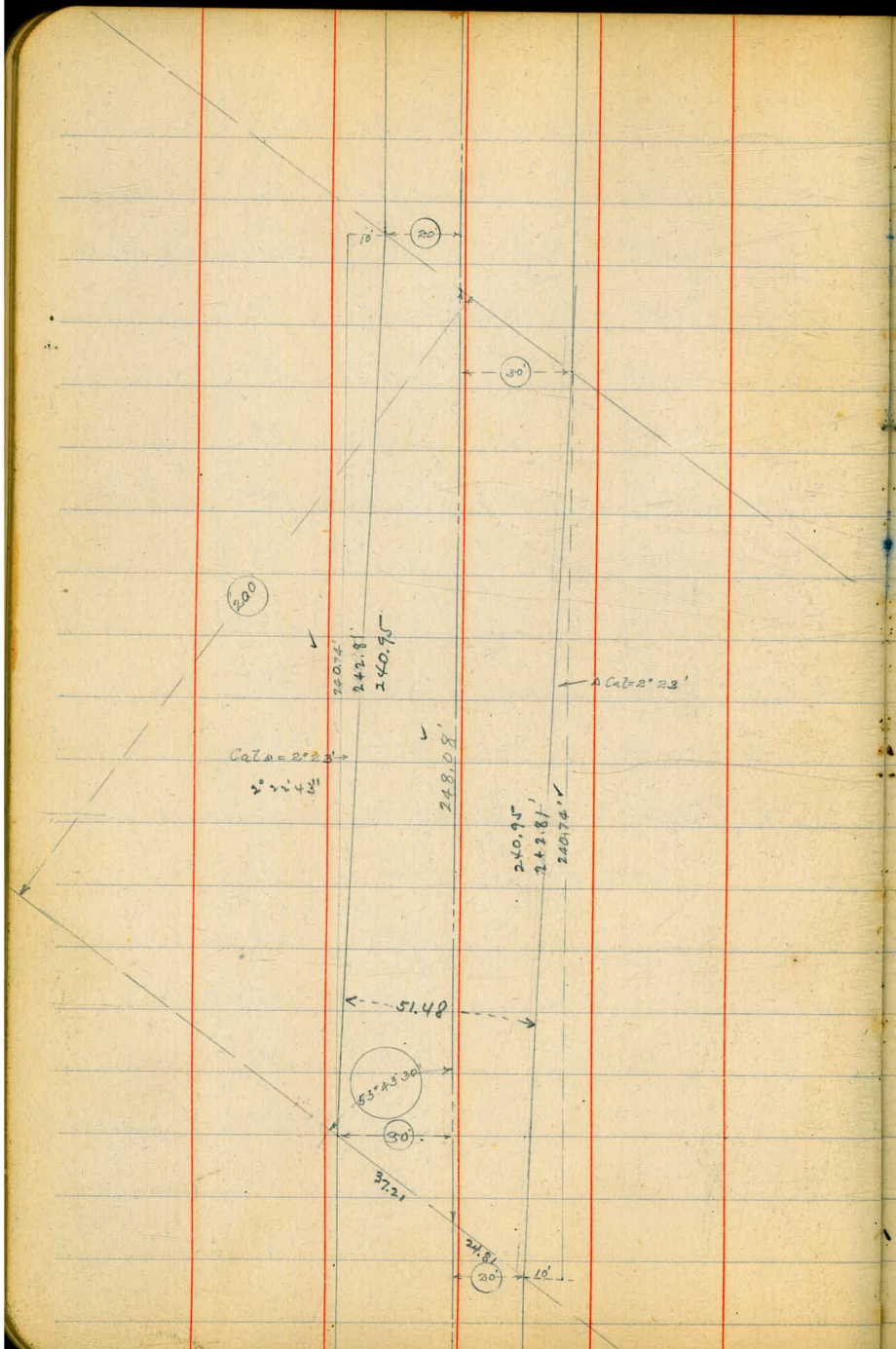
2+11.5 = Intersection of W.L. of Weeks Ave produced with W.L. of Knoxville St.

E.L			6.5	− 0.2



	+	π 6.33	−	37.+
cl			6.7	-0.4
½			7.0	-0.7
c			6.5	-0.2
½			6.3	0.0
cl			6.2	+0.1
W.L			5.8	+0.5
2+11.5 on W to 2+48.5 on E = along W.L. Weeks Ave produced across Knoxville St				
W.L			5.8	+0.5
cl			6.4	-0.1
½			6.3	0.0
c			6.4	-0.1
½			6.4	-0.1
cl			6.7	-0.4
E.L.			7.1	-0.8
		(Weeks Ave 30' wide)		
	W ½ of Weeks Ave.			
E.L.			7.3	-1.0
cl			7.0	-0.7
½			6.6	-0.3
c			6.4	-0.1
½			6.3	0.0

	+	π 6.33	−	
cl			6.0	+0.3
W.L.			6.0	0.3
#	4.60 ✓	7.70	3.23 ✓	3.10 Tipo Fence post.
S ½ of Weeks Ave.				
W.L			7.5	0.2
cl.			7.4	0.3
½			7.7	0.0
c			8.0	-0.3
½			8.3	-0.6
cl.			8.6	-0.9
E.L.			8.9	-1.2
S.L. of Weeks Ave = W.L. of A.T. & S.F. Right of way = 0.0				
E.L			7.7	0.0
cl			8.0	-0.3
½			8.7	-1.0
c			8.9	-1.2
½			8.9	-1.2
cl.			8.8	-1.1
W.L.			7.6	+0.1



+	⊼ 7.70	−	
00 + 38 = toe of Slope of R.R. Fill on the East.			
W.L.		8.8	- 1.1
cl		8.9	- 1.2
½		7.8	- 0.1
c		7.6	+ 0.1
½		7.6	+ 0.1
cl		7.4	+ 0.3
E.L.		8.0	- 0.3
00 + 57 = Shoulder of Fill on the East.			
E.L.		3.1	4.6
cl.		3.1	4.6
½		3.1	4.6
c		3.1	4.6
+7 = at Bulkhead		3.1	4.6
½		5.6	2.1
cl		6.9	0.8
+8		7.8	- 0.1
W.L.		10.0	- 2.3
0 + 60.5 = Apx Cen of A.T. & S.F. R.R.			
On Rails at W.L.		1.59	6.11

	+	H.I. 7.70	−	
E.L. on Rails.			1.68	6.02
0+70 = Shoulder of Fill on the East.				
E.L.			3.2	4.5
⅛			3.2	4.5
cl			3.2	4.5
⅛			3.2	4.5
Cen			3.2	4.5
¼			3.2	4.5
+8 = Bulkhead.			3.0	4.7
cl			5.7	2.0
+6			5.5	2.2
W.L			7.3	0.4
00+84 = Toe of A.T.&S.F. Fill.				
W.L.			6.9	0.8
cl			6.5	1.2
⅛			7.0	0.7
c			7.2	0.5
⅛			6.9	0.8
cl			7.2	0.5
E.L.			7.4	0.3

	+	7.70	−	
1+20 = Appx. S.L. A.T.&S.F. Right of way.				
E.L.			7.5	0.2
cl			7.6	0.1
⅛			7.6	0.1
c			7.6	0.1
⅛			7.5	0.2
cl			7.3	0.4
W.L.			7.6	+ 0.1
1+60 = Toe of Fill of La Jolla R.R.				
W.L.			8.1	− 0.4
cl			8.1	− 0.4
⅛			8.2	− 0.5
c			7.9	− 0.2
⅛			8.1	− 0.4
cl.			7.9	− 0.2
E.L.			7.5	+ 0.2
1+70 = Shoulder of La Jolla Fill.				
E.L.			4.1	3.6
cl			4.1	3.6
⅛			4.1	3.6

	+	℄ 7.70	−	
c			4.1	3.6
¼			4.2	3.5
cl			4.2	3.5
1+8 = Bulkhead			4.2	3.5
W.L.			7.5	0.2
1+78.5 = Appx Cen Line of La Jolla R.R.				
W.L.			2.92	4.78
E.L.			2.94	4.76
1+95 = Shoulder of La Jolla fill.				
E.L.			3.8	3.9
cl			3.9	3.9
¼			3.9	3.9
c			3.8	3.9
¼			3.8	3.9
cl.			3.8	3.9
W.L.			3.8	+ 3.9
2+10 Toe of La Jolla Fill.				
W.L.			10.6	- 2.9
cl			10.5	- 2.8
¼			11.1	- 3.4

	+	℄ 7.70	−	
c			11.4	- 3.7
¼			11.7	- 4.0
cl			11.9	- 4.2
E.L.			12.0	- 4.3
2+35 = Toe of La Jolla side ditch.				
E.L.			9.7	- 2.0
cl			9.9	- 2.2
¼			9.6	- 1.9
c			9.6	- 1.9
¼			9.5	- 1.8
cl			9.5	- 1.8
W.L.			9.1	- 1.4
2+42.5 Appx = on East = ℄ in line. See Plat. Last diagonal Xsection.				
W.L.			7.9	- 0.2
cl			7.6	+ 0.1
¼			7.4	+ 0.3
c			7.3	0.4
¼			7.2	0.5
cl.			7.1	0.6
E.L.			7.3	0.4

	+	ℸ 7.70	−		
#	5.30	6.72	6.28	1.42	
00 R.T.A					
E.L.			6.3	0.4	
cl			5.4	1.3	
½			5.4	1.3	
c			5.5	1.2	
½			5.5	1.2	
cl.			5.4	1.3	
W.L.			4.9	1.8	
0+08 W.L.			4.3	2.4	
cl			5.0	1.7	
½			5.4	1.3	
c			5.5	1.2	
½			5.6	1.1	
cl.			5.5	1.2	
E.L.			5.8	0.9	
0+15 E.L.			5.4	1.3	
cl			5.5	1.2	
½			5.2	1.5	
c			5.2	1.5	

	+	ℸ 6.72	−	
½			4.8	1.9
cl.			3.7	3.0
W.L.			1.5	5.2
0+35 W.L.			1.5	5.2
cl.			1.2	5.5
½			1.2	5.5
c			1.7	5.0
½			3.8	2.9
cl.			4.6	2.1
E.L.			4.8	1.9
0+42 E.L.			4.2	2.5
cl			2.6	4.2
½			1.4	5.3
c			1.2	5.5
½			1.2	5.5
cl.			1.5	5.2
W.L			3.7	3.0
0+51 W.L.			4.8	1.9
cl.			4.0	2.7
½			2.0	4.7

	+	ℸ 6.72	−	
c			1.5	5.2
½			1.2	5.5
cl.			1.2	5.5
E.L.			1.5	5.2
0+63 E.L.			1.2	5.5
cl.			1.4	5.3
½			2.7	4.0
c			4.2	2.5
½			5.4	1.3
cl.			6.1	+ 0.6
W.L.			7.3	− 0.6
0+72 W.L.			6.4	+ 0.3
cl.			7.2	− 0.5
¼			6.0	+ 0.7
c			5.8	0.9
½			5.0	1.7
cl.			4.1	2.6
E.L.			1.6	5.1
0+90 E.L.			3.8	2.9
cl.			5.6	1.1

	+	ℸ 6.72	−	
½			6.3	0.4
c			6.5	+ 0.2
½			7.0	− 0.3
cl.			6.5	+ 0.2
W.L.			5.3	1.4
0+90 W.L.			5.1	1.6
cl.			5.3	1.4
¼			6.1	0.6
c			6.6	+ 0.1
½			6.8	− 0.1
cl.			6.6	+ 0.1
E.L.			6.2	+ 0.5
1+00 E.L.			7.1	− 0.4
cl.			6.8	− 0.1
½			6.3	+ 0.4
c			5.6	1.1
¼			4.8	1.9
cl.			4.9	1.8
E.L.			4.8	1.9
1+20 E.L.			5.1	1.6

	+	⊼ 6.72	−				⊼ 6.72	−	City Gardens Road. 32
cb.			5.0	1.7	2+50 E.L.			5.0	1.7
½			4.9	18	cb			5.4	13
c			5.0	17	½			5.3	14
¼			5.1	16	c			5.6	11
cb.			4.8	1.9	½			5.9	08
E.L.			4.9	1.8	cb			6.2	05
1+50 E.L.			5.2	15	W.L.			6.1	06
cb			5.0	17	3 W.L.			5.9	08
½			5.4	13	cb			5.6	11
c			5.6	11	¼			5.7	10
½			5.1	16	c			5.5	12
cb.			5.2	15	¼			5.1	16
W.L			5.1	16	cb			5.4	13
2 W.L.			5.2	15	E.L.			5.3	14
cb			5.2	15	3+50 E.L.			5.6	11
½			5.3	14	cb			5.6	11
c			5.6	11	½			5.5	12
¼			5.5	12	c			5.7	10
cb.			5.1	16	½			5.9	08
E.L.			5.2	15	cb.			5.8	09

	+	H.I. 6.72	−	
W. L.			5.5	1.2
3+77 W. L. Bisbee St				
W. L.			5.9	0.8
cl			5.7	1.0
1/4			5.7	1.0
c			5.7	1.0
1/2			5.6	1.1
cl.			5.4	1.3
E. L.			5.5	1.2
N. Cl Bisbee St.				
E. L.			5.3	1.4
cl			5.6	1.1
1/2			5.6	1.1
c			5.5	1.2
1/2			5.6	1.1
cl			5.5	1.2
W. L			5.6	1.1
N 1/2 Bisbee S.T.				
W. L.			5.9	0.8
cl			5.6	1.1

	+	H.I. 6.72	−	
1/2			5.5	1.2
c			5.3	1.4
1/2			4.8	1.9
cl			5.1	1.6
E. L.			5.5	1.2
Cen Bisbee St.				
E. L.			5.5	1.2
cl			5.6	1.1
1/4			5.9	0.8
c			5.9	0.8
1/2			5.8	0.9
cl.			5.6	1.1
W. L.			5.8	0.9
S 1/2 Bisbee St.				
W. L.			5.6	1.1
cl.			5.7	1.0
1/2			5.8	0.9
c			5.8	0.9
1/2			5.8	0.9
cl.			5.7	1.0

	+	↑ 6.72	−	
E.L.			6.0	0.7
S. Curb Bisbee St.				
E.L.			5.9	0.8
cl			6.0	0.7
¼			5.8	0.8
c			5.7	1.0
¼			5.9	0.8
cl			5.8	0.9
W.L.			5.7	1.0
S.L. Bisbee St.				
W.L.			5.7	1.0
cl			5.7	1.0
¼			5.7	1.0
c			5.6	1.1
¼			5.6	1.1
cl			6.0	0.7
E.L			5.9	0.8
#	4.09	✓ 5.02	5.79	✓ 0.93
oo = W.L. of Knoxville St.				
S.L.			4.0	1.0

	+	↑ 5.02	−	
cl.			4.0	1.0
¼			3.9	1.1
c			4.1	0.9
¼			4.2	0.8
cl			3.9	1.1
W.L.			4.2	0.8
450 W.L.			3.9	1.1
cl			4.1	0.9
¼			4.3	0.7
c			4.0	1.0
¼			4.1	0.9
cl			4.1	0.9
S.L.			3.9	1.1
1400 S.L.			4.2	0.8
cl			4.5	0.5
¼			4.6	0.4
c			4.4	0.6
¼			4.4	0.6
cl.			4.7	0.3
W.L.			4.7	0.3

	+	⊼ 5.02	−	
1450 N.L.			4.4	0.6
cb.			4.6	0.4
¼			4.5	0.5
c			4.4	0.6
¼			4.0	1.0
cb			4.3	0.7
S.L.			4.1	0.9
2400 S.L.			4.3	0.7
cb			4.0	1.0
¼			4.2	0.8
c			4.3	0.7
¼			4.3	0.7
cb			4.5	0.5
N.L.			4.4	0.6
2+40 = E.L. of Lehigh St.				
N.L.			4.0	1.0
cb			4.2	0.8
¼			4.2	0.8
c			4.1	0.9
¼			4.3	0.7

	+	⊼ 5.02	−	
cb.			4.6	0.4
S.L.			4.3	0.7
E. Curb Lehigh St.				
S.L.			4.2	0.8
cb			4.2	0.8
¼			4.2	0.8
c			4.1	0.9
¼			4.2	0.8
cb			3.9	1.1
N.L.			4.0	1.0
E/2 Lehigh St.				
N.L.			4.1	0.9
cb			3.8	1.2
¼			4.3	0.7
c			4.2	0.8
¼			4.1	0.9
cb			4.3	0.7
S.L.			4.4	0.6
Center Lehigh St.				
S.L.			4.2	0.8

	+	℄ 5.02	−	
cl			4.3	0.7
¼			4.3	0.7
c			4.2	0.8
¼			4.0	1.0
cl			3.9	1.1
N.L.			4.1	0.9
W ½ Lehigh St.				
N.L.			4.0	1.0
cl			3.7	1.3
¼			4.1	0.9
c			4.3	0.7
¼			4.5	0.5
cl			4.4	0.6
S.L.			4.4	0.6
W. Curb Lehigh St.				
S.L.			4.2	0.8
cl			4.4	0.6
¼			4.4	0.6
c			4.3	0.7
¼			4.1	0.9

	+	℄ 5.02	−	
cl			4.1	0.9
N.L.			4.5	0.5
W. Line Lehigh St.				
N.L.			4.5	0.5
cl			3.8	1.2
¼			4.0	1.0
c			4.3	0.7
¼			4.3	0.7
cl			4.2	0.8
S.L.			4.2	0.8
00 = South Line Bisbee St.				
W.L			4.2	0.8
cl			4.3	0.7
¼			4.4	0.6
c			4.1	0.9
¼			4.3	0.7
cl			4.2	0.8
E.L.			4.2	0.8
0+50 E.L.			4.7	0.3
cl			4.5	0.5

	+	⊼ 5.02	−		
¼			4.4	0.6	
c			4.3	0.7	
¼			4.3	0.7	
cl			4.0	1.0	
W.L			4.0	1.0	
1+00 W.L			4.0	1.0	
cl			3.9	1.1	
¼			4.3	0.7	
c			4.2	0.8	
¼			4.1	0.9	
cl			4.0	1.0	
E.L.			3.9	1.1	
1+50 E.L.			4.2	0.8	
cl			4.2	0.8	
¼			4.1	0.9	
c			4.1	0.9	
¼			4.2	0.8	
cl.			4.2	0.8	
W.L.			4.2	0.8	
2+00 W.L.			4.5	0.5	

	+	⊼ 5.02	−		
cl			4.2	0.8	
¼			4.1	0.9	
c			4.3	0.7	
¼			4.2	0.8	
cl			4.4	0.6	
E.L.			3.9	1.1	
2+50 E.L.			4.0	1.0	
cl			4.1	0.9	
¼			4.0	1.0	
c			4.0	1.0	
¼			4.0	1.0	
cl			3.9	1.1	
W.L.			3.9	1.1	
3+00 W.L.			4.0	1.0	
cl			4.0	1.0	
¼			4.0	1.0	
c			4.0	1.0	
¼			4.1	0.9	
cl			4.1	0.9	
E.L.			4.2	0.8	

	+	↑ 5.02	−	
3+50 E.L.			3.7	1.3
cl			3.7	1.3
¼			3.7	1.3
c			3.8	1.2
¼			3.8	1.2
cl			3.8	1.2
W.L.			3.9	1.1
4+00 = N.L. of ELLEN ST. (for intersection see plat)				
W.L.			4.2	0.8
cl			4.3	0.7
¼			4.5	0.5
c			4.4	0.6
¼			4.5	0.5
cl			4.6	0.4
E.L.			4.5	0.5
N. Curb Ellen St.				
E.L.			4.7	0.3
cl			4.7	0.3
¼			4.7	0.3
c			4.7	0.3

	+	↑ 5.02	−	
¼			4.7	0.3
cl			4.8	0.2
W.L			4.7	0.3
N ½ ELLEN St.				
W.L.			6.1	−1.1
cl.			6.1	−1.1
¼			5.1	−0.1
c			4.9	+0.1
¼			4.9	0.1
cl			4.7	0.3
E.L.			4.7	0.3
Cen Ellen St.				
E.L.			4.9	0.2
cl			4.8	0.2
¼			4.9	0.1
c			5.0	0.0
¼			5.7	−0.7
cl.			6.0	−1.0
W.L.			5.4	−0.4
S ½ Ellen St.				

	+	ℸ 5.02	−	
W.L.			4.6	+0.4
cl			4.7	0.3
¼			5.0	0.0
c			5.5	−0.5
¼			5.2	−0.2
cl			5.2	−0.2
E.L.			5.3	−0.3
S. Curb of Ellen St.				
E.L.			4.0	+1.0
cl			3.5	1.5
¼			3.5	1.5
c			4.0	1.0
¼			4.6	0.4
cl			4.5	0.5
W.L.			4.4	0.6
0.0 = S.L. of Ellen St.				
W.L.			3.9	1.1
cl			3.8	1.2
¼			4.3	0.7
c			4.1	0.9

	+	ℸ 5.02	−	
¼			4.5	0.5
cl			3.6	1.4
E.L.			4.0	1.0
H	1.76	5.18 ✓	1.30 ✓	3.72 Post 3"X3" Near S.E. Cor. Ellen & Lehigh.
+50 E.L.			5.3	0.2
cl			5.1	+0.3
¼			5.9	−0.4
c			5.7	−0.2
¼			6.2	−0.7
cl			6.1	−0.6
W.L.			6.1	−0.6
1+00 W.L.			5.2	+0.3
cl			5.2	0.3
¼			5.2	0.3
c			5.1	0.4
¼			5.0	0.5
cl			5.2	0.3
E.L.			5.1	0.4
1+50 E.L.			4.6	0.9
cl			4.4	1.1

	+	⊼ 5.48	−		
¼			4.4	1.1	
c			4.4	1.1	
¼			4.6	0.9	
cb			4.6	0.9	
W.L.			4.6	0.9	
2+00 W.L.			4.8	0.7	
cb			4.8	0.7	
¼			4.8	0.7	
c			4.8	0.7	
¼			4.7	0.8	
cb			4.7	0.8	
E.L.			4.4	1.1	
2+10 = N.L. De La Hunt Ave.					
E.L.			4.9	0.6	
cb			5.1	0.4	
¼			5.1	0.4	
c			5.1	0.4	
¼			5.1	0.4	
cb			5.0	0.5	
W.L.			5.0	0.5	

	+	⊼ 5.48	−	
N. Curb De Lahunt Ave.				
W.L.			5.2	0.3
cb			5.3	0.2
¼			5.2	0.3
c			5.2	0.3
¼			5.2	0.3
cb			5.2	0.3
E.L.			5.1	0.4
N ½ De Lahunt Ave.				
E.L.			5.1	0.4
cb			5.1	0.4
¼			5.2	0.3
c			5.2	0.3
¼			5.2	0.3
cb			5.3	0.2
W.L.			5.3	0.2
Cen De Lahunt Ave.				
W.L.			5.5	0.0
cb			5.5	0.0
¼			5.4	0.1

	+	⊼ 5.48.	−		
c			5.2	03	
¼			5.2	03	
cl			5.3	07	
E.L.			5.2	03	
S¼ De Lahunt Ave.					
E.L.			5.3	07	
cl			5.4	01	
½			5.5	00	
c			5.5	00	
¼			5.6	-01	
cl			5.5	00	
W.L.			5.3	02	
S. Curb De Lahunt Ave.					
W.L.			4.7	08	
cl			4.7	08	
½			4.8	07	
c			4.9	06	
¼			5.0	05	
cl.			5.7	-07	
E.L.			6.1	-06	

	+	⊼ 5.48.	−	
00 = S.L. De Lahunt Ave.				
E.L.			4.0	15
cl			3.9	16
¼			3.8	17
c			4.0	15
¼			4.6	09
cl			4.4	11
W.L.			4.2	13
+50 W.L.			4.4	11
cl			4.3	12
¼			4.1	14
c			4.3	12
¼			4.2	13
cl			4.2	13
E.L.			4.3	12
1400 E.L.			4.6	09
cl			4.8	07
¼			4.8	07
c			4.9	06
½			4.8	07

	+	℄ 5.48	−	
cl			5.0	0.5
W.L.			4.8	0.7
1+50 W.L			4.8	0.7
cb			4.9	0.6
½			4.6	0.9
c			4.5	1.0
¼			4.3	1.2
cl			4.4	1.1
E.L.			4.4	1.1
2+00 E.L.			4.5	1.0
cl			4.6	0.9
½			4.8	0.7
c			4.5	1.0
½			4.6	0.9
cl			4.8	0.7
W.L.			4.8	0.7
2+10 = N.L. of Isabel Ave.				
W.L			4.9	0.6
cl			4.8	0.7
¼			4.8	0.7

	+	℄ 5.48	−	
c			4.8	0.7
¼			4.8	0.7
cl			4.6	0.9
E.L.			4.7	0.8
N. Curb Isabel Ave.				
E.L.			4.8	0.7
cl			4.8	0.7
½			4.8	0.7
c			4.8	0.7
½			4.8	0.7
cl			4.8	0.7
W.L.			5.0	0.5
N. ½ Isabel Ave.				
W.L.			5.5	0.0
cl			5.4	0.1
½			5.4	0.1
c			5.0	0.5
½			5.2	0.3
cl			5.1	0.4
E.L.			5.0	0.5

	+	⊼ 5.48	−	
	Cen Isabel Ave.			
E. L.			5.4	0.1
cl			5.5	0.0
¼			6.2	− 0.7
c			6.1	− 0.6
¼			6.1	− 0.6
cl			6.1	− 0.6
W. L.			6.2	− 0.7
	S ¼ Isabel Ave.			
W. L.			6.6	− 1.1
cl			6.6	− 1.1
¼			6.6	− 1.1
c			6.6	− 1.1
¼			6.5	− 1.0
cl			6.5	− 1.0
E. L.			6.5	− 1.0
	S Curb Isabel Ave.			
E. L.			6.4	− 0.9
cl			6.5	− 1.0
¼			6.5	− 1.0

	+	⊼ 5.49	−	
c			6.6	− 1.1
¼			6.5	− 1.0
cl			6.4	− 0.9
W. L.			6.4	− 0.9
00 = S. L. Isabel Ave.				
W. L.			6.1	− 0.6
cl			6.0	− 0.5
¼			5.8	− 0.3
c			5.8	− 0.3
¼			5.7	− 0.2
cl			5.9	− 0.4
E. L.			6.2	− 0.7
H	3.02	4.53 ✓	3.97	1.51 ✓
+.50 E. L.			2.9	1.6
cl			3.1	1.4
¼			3.4	1.1
c			3.3	1.2
¼			3.3	1.2
cl			3.2	1.3
W. L.			3.3	− 1.2

	+	↑ 4.53	−	
1+00 W.L.			3.2	1.3
cl			3.2	1.3
¼			3.1	1.4
c			3.0	1.5
¼			3.0	1.5
cl.			3.0	1.5
E.L.			3.0	1.5
1+40 W.L.			3.7	0.8
cl			3.4	1.1
¼			3.4	1.1
c			3.6	0.9
¼			4.0	0.5
cl.			4.4	01
W.L			4.8	-0.3
1+50 W.L.			4.8	-0.3
cl			6.3	-1.8
¼			7.0	-2.5
c			7.4	-2.9
¼			7.0	-2.5
cl.			4.9	-0.4

	+	↑ 4.53	−	
E.L.			4.0	0.5
1+60 E.L.			4.1	0.4
cl			4.7	-0.2
¼			4.9	-0.4
c			4.1	+0.4
¼			3.8	0.7
cl			3.5	1.0
W.L.			4.0	0.5
1+75 W.L			3.6	0.9
cl			3.4	1.1
¼			2.9	1.6
c			3.4	1.1
¼			3.6	0.9
cl			3.4	1.1
E.L.			4.2	0.3
2+10 = W.L. of Anna St.				
E.L.			4.3	0.2
cl			4.0	0.5
¼			4.1	0.4
c			4.3	0.2

	+	⊼ 4.53	−	
℄			4.0	0.5
cl			4.1	0.4
W.L.			3.9	0.6
#	3.41	4.35 ✓	3.59 ✓	0.94 on scarf stake S.E. Cor Lehigh & Anna St.
N. Curb of Anna St. (110' wide down to P.L.) 20' curbs.				
W.L.			4.0	0.4
cl			4.0	0.4
℄			4.0	0.4
c			4.0	0.4
℄			4.0	0.4
cl			3.9	0.5
E.L.			4.0	0.4
N ½ of Anna St.				
E.L.			4.0	0.4
cl			4.0	0.4
¼			4.0	0.4
c			4.1	0.3
¼			4.0	0.4
cl.			4.1	0.3
W.L.			4.1	0.3

	+	⊼ 4.35	− City Gardens Road.	45
Cen of Anna St.				
W.L.			4.1	0.3
cl			4.0	0.4
¼			4.0	0.4
c			4.0	0.4
¼			4.0	0.4
cl			4.0	0.4
E.L.			4.0	0.4
S ½ Anna St.				
E.L.			3.8	0.6
cl			3.8	0.6
½			3.7	0.7
c			3.8	0.6
¼			3.9	0.5
cl.			3.9	0.5
W.L.			4.0	0.4
S curb Anna St.				
W.L.			3.5	0.9
cl			3.4	1.0
¼			3.2	1.2

	+	℄ 4.35	−	
c			3.2	1.2
1/4			3.1	1.3
cl			3.1	1.3
E.L			2.9	1.5
	S.L. Anna St.			
E.L.			3.1	1.3
cl			3.0	1.4
1/4			3.2	1.2
c			2.9	1.5
1/4			3.0	1.4
cl			3.2	1.2
W.L.			3.1	1.3
00= E.L. of Lehigh St.				
S.L.			3.1	1.3
cl			2.9	1.5
1/4			3.8	0.6
c			4.0	0.4
1/4			4.1	0.3
cl.			3.9	0.5
N.L.			4.2	0.2

	+	℄ 4.35	−	
0+50 N.L.			4.1	0.3
cl			3.9	0.5
1/4			4.2	0.2
c			4.0	0.4
1/4			3.7	0.7
cl.			3.0	1.4
S.L.			3.1	1.3
1+00 S.L.			3.3	1.1
cl.			3.0	1.4
1/4			3.4	1.0
c			4.0	0.4
1/4			4.1	0.3
cl.			4.0	0.4
N.L.			4.0	0.4
1+50 N.L.			4.0	0.4
cl			3.9	0.6
1/4			4.4	0.0
c			3.9	0.5
1/4			2.8	1.6
cl.			3.1	1.3

	+	↑ 4.35	−				+	↑ 4.35	−	
S.L.			3.3	1.1		1/a			4.1	0.3
2+00 S.L.			4.4	0.0		cb.			4.0	0.4
cb.			3.4	1.0		W.L.			3.5	0.9
1/a			3.2	1.2		2+70± Along Pruett Line for 50' St.				
c			3.3	1.1		W.L.			3.1	1.3
1/a			4.1	0.0		cb.			3.8	0.6
cb.			3.9	0.5		1/a			3.9	0.5
W.L.			3.9	0.5		c			4.2	0.2
2+50 W.L.			3.7	0.7		1/a			4.2	0.2
cb.			4.3	0.1		cb.			4.2	0.2
1/a			4.4	0.0		S.L.			3.8	0.5
c			2.5	1.9		#	577	5.30	4.82	−0.47 on P.L. Cor Mon.
1/a			3.7	0.7		3+00 = W.L. Knoxville St.				
cb.			4.4	0.0		3+00				
S.L.			4.1	0.3		S.L.			5.1	0.2
2+70± Along Pruett Line for 110' St.						cb			5.2	0.1
S.L.			3.9	0.5		1/a			5.1	0.2
cb			4.4	0.0		c			5.1	0.2
1/a			3.9	0.5		1/a			5.0	0.3
c			3.1	1.3		cb.			5.3	0.0
						W.L.			4.9	0.5

	+	ℸ 5.30	−	
W. Curb Knoxville St.				
N. L.			5.4	−0.1
cl			5.0	+0.3
¼			4.8	0.5
c			5.1	0.2
¼			5.0	0.3
cl.			5.3	0.0
S. L.			5.0	0.3
W ½ Knoxville St.				
S. L.			5.0	+0.3
cl.			5.4	−0.1
¼			5.0	+0.3
c			5.1	0.2
¼			5.0	0.3
cl.			4.7	0.6
N. L.			5.3	0.0
Cen Knoxville St.				
N. L.			4.8	0.5
cl.			4.8	0.5
¼			4.8	0.5

	+	ℸ 5.30	−	
c			5.1	0.2
¼			5.1	0.2
cl.			5.2	−0.1
S. L.			5.1	0.2
E ½ Knoxville St.				
S. L.			5.2	0.1
cl.			5.4	−0.1
¼			5.1	0.2
c			5.1	0.2
¼			4.8	0.5
cl.			4.7	0.6
N. L.			4.9	0.4
E. Curb Knoxville St.				
N. L.			4.8	0.5
cl.			4.7	0.6
¼			4.9	0.4
c			5.2	0.1
¼			5.3	0.0
cl.			5.5	−0.2
S. L.			5.4	−0.1

	+	ℸ 5.30	−	
00=S.L. Knoxville St				
S.L.			5.5	-0.2
cl.			5.6	-0.3
1/4			5.3	0.0
c			5.4	-0.1
1/4			5.1	0.2
cl.			4.7	0.6
N.L.			4.7	06
0+50 N.L.			4.8	0.5
cl			5.4	-0.1
1/4			5.8	-0.5
c			6.0	-0.7
1/4			6.0	-0.7
cl.			5.8	-0.5
S.L.			5.4	-0.1
1+00 S.L.			5.0	0.3
cl			5.8	-0.5
1/4			5.4	-0.1
c			5.5	-0.2
1/4			5.2	0.1

	+	ℸ 5.30	−	
cl.			5.6	-0.3
N.L.			5.0	0.3
1+50 N.L.			5.1	0.2
cl			5.0	0.3
1/4			5.0	0.3
c			5.0	0.3
1/4			5.0	0.3
cl.			5.0	0.3
S.L.			4.4	0.9
2+00 S.L.			4.0	1.3
cl			4.5	0.8
1/4			4.7	0.6
c			4.9	0.4
1/4			4.7	0.6
cl.			4.7	0.6
N.L.			4.6	0.7
2+50 N.L.			4.2	1.1
cl.			4.2	1.1
1/4			4.3	1.0
c			4.3	1.0

	+	℄ 5.30	−	
¼			4.2	1.1
cl.			4.5	0.8
S.L.			4.3	1.0
	3+00 = W.L. Fillmore St.			
S.L.			4.7	0.6
cl			4.5	0.8
¼			3.9	1.4
c			4.2	1.1
¼			4.0	1.3
cl.			4.1	1.2
N.L.			4.1	1.2
	W. Curb Fillmore St.			
N.L.			4.1	1.2
cl.			4.1	1.2
¼			4.1	1.2
c			4.1	1.2
¼			4.0	1.3
cl.			4.2	1.1
S.L			4.3	1.0
cl.				

	+	℄ 5.30	−	
	W. ¼ Fillmore St.			
S.L.			4.2	1.1
cl			4.2	1.1
¼			4.0	1.3
c			4.1	1.2
¼			4.0	1.3
cl.			4.1	1.2
N.L.			4.0	1.3
	Cen Fillmore St.			
N.L.			4.1	1.2
cl			4.1	1.2
¼			3.9	1.4
c			4.1	1.2
¼			4.1	1.2
cl.			4.3	1.0
S.L			4.2	1.1
	E. ¼ Fillmore St.			
S.L.			4.1	1.2
cl			4.2	1.1
¼			4.2	1.1

	+	↑ 5.30	−	
c			4.2	1.1
1/4			4.1	1.2
cl.			4.0	1.3
N.L.			4.1	1.2
E Curb Fillmore St.				
N.L.			4.1	1.2
cl.			4.1	1.2
1/4			3.9	1.4
c			3.9	1.4
1/4			4.0	1.3
cl.			4.2	1.1
S.L.			4.0	1.3
00 = E.L. Fillmore St.				
S.L.			4.2	11
cl			4.3	1.0
1/4			4.0	1.3
c			4.0	1.3
1/4			4.0	1.3
cl.			4.0	1.3
N.L.			4.1	1.2

	+	↑ 5.30	−	
0+50 N.L.			4.2	1.1
cl			4.0	1.3
1/4			3.9	1.4
c			3.8	1.5
1/4			3.7	1.6
cl.			3.9	1.4
S.L.			3.8	1.5
1+00 S.L.			3.6	1.7
cl.			3.9	1.4
1/4			3.8	1.5
c			3.8	1.5
1/4			3.9	1.4
cl.			3.9	1.4
N.L.			3.9	1.4
#	0.80	✓ 5.58	0.52	✓ 4.78 4"x4" Fence post G.S. Place.
1+50 N.L.			4.7	0.9
cl			4.4	1.2
1/4			4.2	1.4
c			4.2	1.4
1/4			4.0	1.6

	+	ℸ 5.58	−	
cl.			4.1	15
S.L.			4.1	15
2+00 S.L.			4.1	15
cl.			4.3	13
1/4			4.1	15
c			4.3	13
1/4			4.3	13
cl.			4.5	11
W.L.			4.3	13
2+50 W.L.			4.1	15
cl			4.1	15
1/4			4.1	15
c			4.4	12
1/4			4.0	16
cl.			4.4	12
S.L.			4.2	14
3+00 = W.L. Joliet St.				
S.L.			4.4	12
cl			4.4	12
1/4			4.4	12

	+	ℸ 5.58	−	
c			4.6	10
1/4			4.1	15
cl			4.3	13
W.L.			4.3	13
W. Curb Joliet St.				
W.L.			4.6	10
cl			4.7	09
1/4			4.5	11
c			4.5	11
1/4			4.5	11
cl.			4.4	12
S.L.			4.1	15
W. 1/4 Joliet St.				
S.L.			4.2	14
cl.			4.5	11
1/4			4.6	10
c			4.7	09
1/4			4.5	11
cl.			4.4	12
W.L.			4.4	12

	+	↑ 5.58	−	
	Cen Joliet St.			
N.L.			4.2	1.4
ck.			4.2	1.4
1/4			4.3	1.3
c			4.4	1.2
1/4			4.4	1.2
ck.			4.6	1.0
S.L.			4.6	1.0
	E 1/4 Joliet St.			
S.L.			4.6	1.0
ck.			4.5	1.1
1/4			4.3	1.3
c			4.4	1.2
1/4			4.1	1.5
ck.			4.1	1.5
N.L.			4.0	1.6
	E. Curb Joliet St.			
N.L.			3.7	1.9
ck.			3.9	1.7
1/4			3.9	1.7

	+	↑ 5.58	−	
a			4.2	1.4
1/4			4.2	1.4
ck.			4.3	1.3
S.L.			4.2	1.4
00= E.L. Joliet St.				
S.L.			4.0	1.6
ck.			4.1	1.5
1/4			4.0	1.5
c			4.0	1.5
1/4			3.6	2.0
ck.			3.5	2.1
N.L.			3.7	1.9
0+50 N.L.			3.6	2.0
ck			3.6	2.0
1/4			3.6	2.0
c			3.8	1.8
1/4			3.6	2.0
ck			3.6	2.0
S.L.			3.4	2.2

	+	+ 5.58	−	
1400 S.L.			3.6	2.0
cl.			3.9	1.7
1/4			3.7	1.9
c			3.8	1.8
1/4			3.8	1.8
cl.			3.8	1.8
N.L.			3.7	1.9
#	4.31	6.82 ✓	3.07	2.15 ✓
1450 N.L.			4.6	2.2
cl			4.6	2.2
1/4			4.4	2.4
c			4.6	2.2
1/4			4.4	2.4
cl.			4.5	2.3
S.L.			4.3	2.5
2+00 S.L.			3.9	2.9
cl.			4.3	2.5
1/4			4.3	2.5
c			4.3	2.5
1/4			4.3	2.5

	+	+ 6.82	−	
cl.			4.2	2.6
N.L.			4.5	2.3
2+50 N.L.			4.7	2.1
cl			4.5	2.3
1/4			4.3	2.5
c			4.2	2.6
1/4			4.2	2.6
cl.			4.4	2.4
S.L.			3.9	2.9
3+00 = W.L. Ralston St.				
S.L.			4.4	2.4
cl.			4.4	2.4
1/4			4.8	2.0
c			5.0	1.8
1/4			4.7	2.1
cl.			4.9	1.9
N.L.			4.9	1.9
W. Curb Ralston St.				
N.L.			4.5	2.3
cl.			4.4	2.4

	+	℄ 6.82	−	
½			4.4	2.4
c			4.8	2.0
½			4.8	2.0
cb.			4.8	2.0
S.L.			4.7	2.1
W. ½ Ralston St.				
S.L.			4.5	2.3
cb			4.5	2.3
½			4.4	2.4
c			4.3	2.5
½			4.1	2.7
cb.			4.4	2.4
N. L.			4.4	2.4
Cen Ralston St.				
N. L.			4.5	2.3
cb.			4.4	2.4
½			4.0	2.8
c			4.4	2.4
½			4.1	2.7
cb.			4.1	2.7

	+	℄ 6.82	−	
S.L.			3.9	2.9
E ½ Ralston St.				
S.L.			4.0	2.8
cb			4.1	2.7
½			4.2	2.6
c			4.4	2.4
½			4.1	2.7
cb.			4.4	2.4
N. L.			4.5	2.3
E. Curb Ralston St.				
N. L.			4.4	2.4
cb			4.5	2.3
½			4.2	2.6
c			4.3	2.5
½			4.1	2.7
cb.			4.2	2.6
S.L.			4.0	2.8
00 = E.L. Ralston St.				
S.L.			4.0	2.8
cb.			4.1	2.7

	+	ℸ 6.82	−		
1/4			4.1	2.7	
c			4.4	2.4	
1/4			4.4	2.4	
cl.			4.4	2.4	
N.L.			4.4	2.4	
0+50 N.L.			4.4	2.4	
cl.			4.5	2.3	
1/4			4.3	2.5	
c			4.4	2.4	
1/4			4.0	2.8	
cl.			4.2	2.6	
S.L.			4.0	2.8	
1+00 S.L.			4.4	2.4	
cl			4.7	2.1	
1/4			4.7	2.1	
c			4.7	2.1	
1/4			5.0	1.8	
cl.			4.9	1.9	
N.L.			5.1	1.7	

City Gardens Road. 56

	+	ℸ 6.82	−	
1+51.5 = Pueblo Line. (Xsections for 50' St.)				
N.L.			4.8	2.0
cl.			4.9	1.9
1/4			5.0	1.8
c			4.4	2.4
1/4			4.3	2.5
cl.			4.2	2.6
S.L.			4.2	2.6
1+51.5 = Pueblo Line (Xsectioned for 58.10' St.)				
S.L.			4.2	2.6
cl.			4.1	2.7
1/4			4.3	2.5
c			4.6	2.2
X			5.1	1.7
cl.			5.1	1.7
N.L.			4.5	2.3
#	5.98	7.70 ✓	5.10	1.72 on Pueblo Cor Mon. ✓
00 = Pueblo Line (Note: Street narrows from 58.10' at P.L. to 50' at W.L. of Stewart St.)				
N.L.			4.9	2.8
cl			5.6	2.1

	+	± 7.70	−	
¼			5.6	2.1
c			5.5	2.2
¼			5.6	2.1
cl			5.2	2.5
S.L.			5.3	2.4
1+00 S.L.			5.1	2.6
cl			5.3	2.4
¼			5.5	2.2
c			5.1	2.6
¼			4.2	3.4
cl			4.4	3.3
W.L.			4.6	3.1
1+30 = W.L. of Stewart St.				
W.L.			4.3	3.4
cl			4.4	3.3
¼			4.3	3.4
c			4.9	2.8
¼			5.4	2.3
cl			5.3	2.4
S.L.			5.0	2.7

	+	± 7.70	−	
W. Curb Stewart St.				
S.L.			5.1	2.6
cl			5.3	2.4
¼			5.3	2.4
c			4.7	3.0
¼			4.1	3.6
cl			4.4	3.3
W.L.			4.5	3.2
W ½ Stewart St.				
W.L.			4.3	3.4
cl			4.4	3.3
¼			4.1	3.6
c			4.6	3.1
¼			5.5	2.2
cl			4.9	2.8
S.L.			5.1	2.6
Cen Stewart St.				
S.L.			5.1	2.6
cl			5.1	2.6
¼			5.6	2.1

	+	↑ 7.70	−	
c			4.6	3.1
¼			4.3	3.4
cl			4.3	3.4
N. L.			4.2	3.5
E. ¼ Stewart St.				
N. L.			4.3	3.4
cl.			4.3	3.4
¼			4.3	3.4
c			4.6	3.1
¼			5.3	2.4
cl			5.2	2.5
S. L.			5.0	2.7
E. Curb Stewart St.				
S. L.			5.0	2.7
cl			5.4	2.3
¼			5.3	2.4
c			4.4	3.3
¼			4.1	3.6
cl			4.4	3.3
N. L.			4.4	3.3

	+	↑ 7.70	−	
00 = E. L. Stewart St.				
N. L.			4.6	3.1
cl			4.5	3.2
¼			4.3	3.4
c			4.6	3.1
¼			5.3	2.4
cl			5.1	2.6
S. L.			5.1	2.6
+50 S. L.			4.7	3.0
cl			5.0	2.7
¼			5.0	2.7
c			3.7	4.0
¼			4.1	3.6
cl.			4.3	3.4
N. L.			4.2	3.5
1+00 N. L.			4.7	3.0
cl			4.5	3.2
¼			4.0	3.7
c			4.4	3.3
¼			4.9	2.8

	+	⊼ 7.70	−	
cl			4.7	3.0
S. L.			4.4	3.3
1+50 S.L.			4.4	3.3
cl			4.5	3.2
½			4.6	3.1
c			4.8	2.9
½			4.4	3.3
cl			4.3	3.4
W.L.			4.1	3.6
2+00 W.L.			3.7	4.0
cl			3.5	4.2
½			3.9	3.8
c			4.6	3.1
¼			4.6	3.1
cl			4.4	3.3
S.L.			4.5	3.2
2+50 S.L.			4.4	3.3
cl			4.4	3.3
½			4.4	3.3
c			3.4	4.3

City Gardens Road. 59

	+	⊼ 7.70	−	
½			3.4	4.3
cl			3.2	4.5
W. L.			3.5	4.2
2+60 = W.L. Archibald St.				
W. L.			3.4	4.3
cl			3.3	4.4
¼			3.2	4.5
c			3.5	4.2
½			4.2	3.5
cl			4.2	3.5
S. L.			4.3	3.4
#	5.42	9.03 ✓	4.08	3.61 ✓
W. Curb Archibald St.				
S.L.			5.6	3.4
cl			5.6	3.4
½			5.6	3.4
c			4.8	4.2
½			4.8	4.2
cl			4.7	4.3
W. L.			4.9	4.1

	+	⊼ 9.03	−	
W ½ Archibald St				
N.L.			5.1	3.9
cl			4.6	4.4
½			4.4	4.6
c			4.6	4.4
½			5.4	3.6
cl			5.5	3.5
S.L.			5.7	3.3
Cen Archibald St.				
S.L.			5.7	3.3
cl			5.5	3.5
½			5.3	3.7
c			4.6	4.4
½			4.6	4.4
cl			4.9	4.2
N.L.			5.0	4.0
E ½ Archibald St.				
N.L.			5.0	4.0
cl			4.9	4.1
½			4.4	4.6

	+	⊼ 9.03	−	
c			4.8	4.2
½			5.3	3.7
cl			5.2	3.8
S.L.			5.7	3.3
E. Curb Archibald St.				
S.L.			5.5	3.5
cl			5.3	3.7
½			5.2	3.8
c			4.5	4.5
½			4.6	4.4
cl			4.8	4.2
N.L.			4.8	4.2
00=E.L. Archibald St.				
N.L.			4.9	4.1
cl			4.7	4.3
½			4.7	4.3
c			5.0	4.0
½			5.2	3.8
cl			5.1	3.9
S.L.			5.4	3.6

	+	↑ 19.03	−	
0+50 S.L.			5.2	3.8
cl			5.4	3.6
1/2			5.1	3.9
c			4.4	4.6
1/2			4.7	4.3
cl			4.7	4.3
N.L.			5.0	4.0
1+00 N.L.			5.0	4.0
cl			4.9	4.1
1/2			5.0	4.0
c			4.9	4.1
1/2			5.1	3.9
cl			5.1	3.9
S.L.			5.1	3.9
1+50 S.L.			4.6	4.4
cl			4.5	4.5
1/2			4.8	4.2
c			4.7	4.3
1/2			4.3	4.7
cl			4.4	4.6

	+	↑ 9.03	−	
N.L.			4.4	4.6
2+00 N.L.			4.2	4.8
cl			4.2	4.8
1/2			4.0	5.0
c			4.2	4.8
1/2			4.7	4.3
cl			4.7	4.3
S.L.			4.2	4.8
#	7.26	12.16	4.13	4.90 8.28
2+50 S.L.			7.3	4.9
cl			7.6	4.6
1/2			7.6	4.6
c			7.6	4.6
1/2			7.7	4.5
cl			8.1	4.1
N.L.			8.1	4.1
2+60 = W.L Pritchard St.				
N.L.			7.9	4.3
cl			8.2	4.0
1/2			8.1	4.1

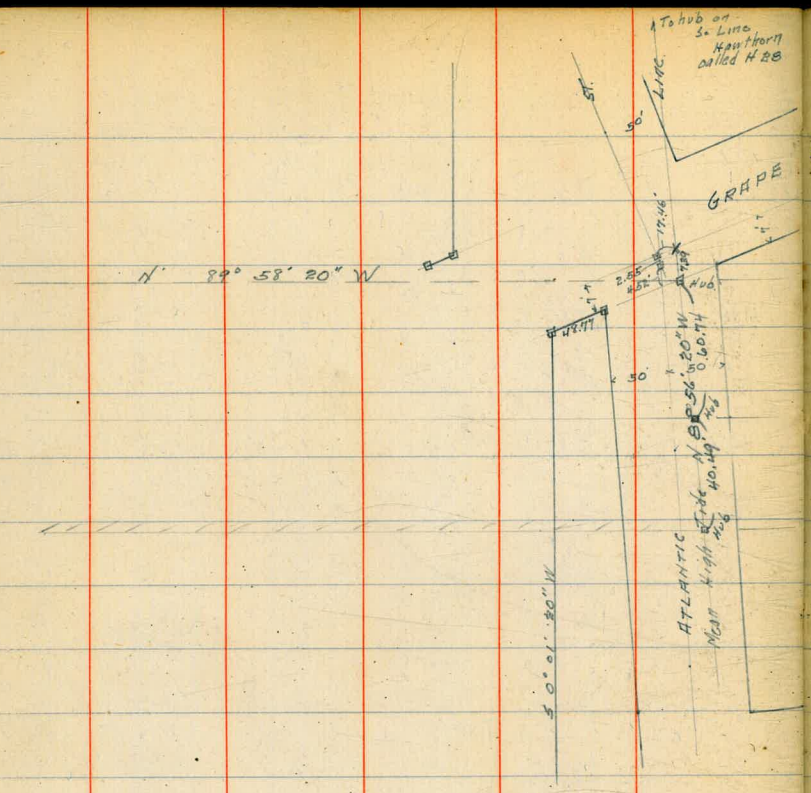
	+	✳ 12.16	−	
c			7.9	4.3
½			7.5	4.7
cb			7.5	4.7
S.L.			7.2	4.8
W. Curb Pritchard St.				
S.L.			7.6	4.6
cb			7.8	4.4
¼			7.9	4.3
c			8.0	4.2
¼			8.2	4.0
cb			7.8	4.4
N.L.			6.9	5.3
W. ½ Pritchard St.				
N.L.			5.9	6.3
cb			6.8	5.4
½			7.7	4.5
c			7.9	4.3
¼			8.0	4.2
cb			7.9	4.3
S.L.			8.0	4.2

	+	✳ 12.16	−	
Cen. Pritchard St.				
S.L.			8.0	4.2
cb			7.8	4.4
½			7.9	4.3
c			7.7	4.5
½			6.7	5.5
cb			5.6	6.6
N.L.			4.7	7.5
E ½ Pritchard St.				
N.L.			4.6	7.6
cb			4.7	7.5
¼			5.3	6.9
c			6.3	5.9
½			7.2	4.8
cb			7.7	4.5
S.L.			7.8	4.4
E. Curb Pritchard St.				
S.L.			7.8	4.4
cb			7.3	4.9
¼			6.3	5.9

	+	R.L. 12.16	−	
C			5.2	7.0
½			4.4	7.8
cb			4.5	7.7
N.L.			5.1	7.1
00 = E.L. Pritchard St.				
N.L.			7.0	5.2
cb			5.2	7.0
¼			4.5	7.7
C			4.5	7.7
½			4.4	7.8
cb			5.2	7.0
S.L.			6.8	5.4
0+12 S.L.			4.0	8.2
cb			4.3	7.9
½			4.2	8.0
C			5.1	7.1
¼			6.3	5.9
cl			7.6	4.6
N.L.			8.4	3.8
0+29 N.L.			8.2	4.0

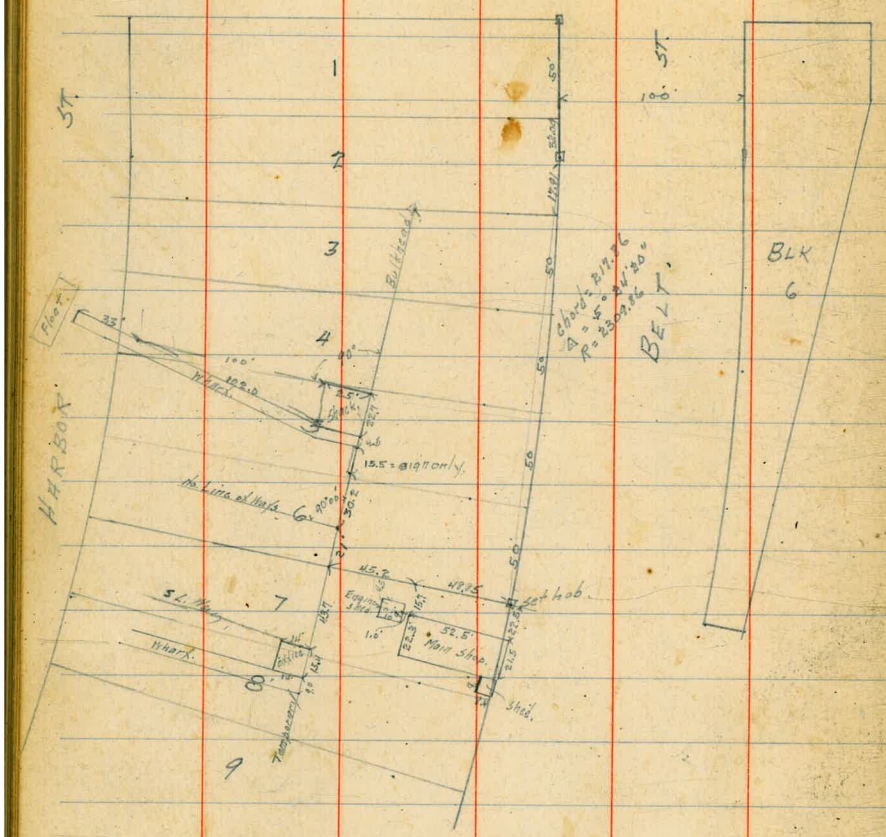
	+	R.L. 12.16	−	
cb			8.6	3.6
½			8.8	3.4
C			8.1	4.1
½			7.6	4.6
cb			6.5	5.7
S.L.			4.7	7.5
0+50 S.L.			8.6	3.6
cb			9.0	3.2
½			8.9	3.3
C			8.9	3.3
½			8.9	3.3
cb			8.1	4.1
N.L.			6.9	5.3
1+00 N.L.			6.4	5.8
cb			7.1	5.1
½			7.0	5.2
C			7.0	5.2
½			6.7	5.5
cb			6.8	5.4
S.L.			6.8	5.4

	+	ℸ 12.16	− City Gardens Road.		
1+33.5 Appx = Pueblo Lime.					
S.L.			6.9	5.3	
cl			6.6	5.6	
¼			6.6	5.6	
c			6.6	5.6	
½			6.7	5.5	
cl,			6.6	5.6	
N.L.			6.5	5.7	
#	10.60	14.55	8.21	3.95	= Mon Cor P.L.s 272,273, 281
#	8.27	10.65	12.17	2.38	Rock.
#	6.20	11.08	5.77	4.88	
#	4.03	10.52	4.59	6.49	
#	12.19	21.46	1.25	9.27	Rock loc dike.
#	4.55	24.79	1.22	20.24	Rock in Road.
#	3.67	25.69	2.77	22.02	Mon front Hardys
#	5.50	22.68	8.51	17.18	
#	6.36	25.27	3.77	18.91	
			3.36	21.91	


To hub on S. Line Hawthorn called H 28
ST.
LINE
ST.
GRAPE
N. 89° 58' 20" W
H.H.
H.H.
H.H.
H.H.
50.
50.
ATLANTIC
Near High Water
S 0° 01' 40" W
N 89° 58' 20" W
0.60 FT.
40.49'

1/20/19 Gregory

LOCATION OF BUILDINGS
ON LOTS 6-7-8
BLOCK 5 OF TIDE LAND SUBD.



7/30/19 Gregory Miller Shaw

Levels on Proposed Curb Lines of Bancroft St From Grape To Elm
see sketch Page 70

	0.17	273.42		273.25	Spk SW Bancroft & Grape
		St L of Grape St (80' wide)			
W Cb.			3.3	270.1	✓
+13			3.4	270.0	
E Cb			3.6	269.6	✓
		+25			
E Cb			5.1	268.3	✓
+13			4.7	268.7	
W Cb			4.5	268.9	✓
		+50			
W Cb			5.8	267.6	✓
+13			6.0	267.4	
E Cb			6.6	266.8	✓
		+75			
E Cb			7.6	265.8	✓
+13			7.0	266.4	
W Cb			6.9	266.5	✓
		+85			
E Cb.			11.1	262.3	✓

		1+00			
W Cb.			8.3	265.1	✓
+13			8.4	265.0	
E Cb			13.1	260.3	✓
		1+12			
E Cb			13.4	260.0	✓
		1+20			
E Cb			11.3	262.1	✓
		1+25			
E Cb			11.8	261.6	✓
+13			9.8	263.6	
W Cb			9.9	263.5	✓
		1+50			
W Cb.			11.6	261.8	✓
+13			11.4	262.0	
T.P.	0.87	261.18	13.11	260.31	
E Cb.			11.1	257.1	✓
		1+65			
E Cb			8.4	252.8	✓
+13			0.7	260.5	

	261.18			
W.Cb		0.3	260.9 ✓	
	1+90			
W.Cb		1.4	259.8 ✓	
+13		1.6	259.6	
E.Cb.		6.1	255.1 ✓	
	2+05			
E.Cb		4.9	256.3 ✓	
+13		2.2	259.0	
W Cb		2.1	259.1 ✓	
	2+25 = P.C.			
W.Cb		2.9	258.3 ✓	
+13		3.4	257.8	
E.Cb.		5.9	255.3 ✓	
	28.48 So. on E 30.26 ✓ ~ W } of P.C.			
E.Cb		6.7	254.5 ✓	
+13		4.8	256.4	
W.Cb		4.5	256.7 ✓	
	56.96 So on E 60.52 ✓ ~ W } of P.C.			
W.Cb		6.2	255.0 ✓	
+13		6.1	255.1	

E.Cb		8.9	252.3 ✓	
	85.44 So. of (PC on E) 90.78 So. of PC on W = P.R.C.			
E.Cb		12.9	248.3 ✓	
+13		9.6	251.6	
W Cb		7.9	253.3 ✓	
	28.48 So. of PRC on E 30.26 ✓ ~ PRC ~ W.			
W.Cb		10.1	251.1 ✓	
+13		11.8	249.4	
T.P.	1.44	249.82 ✓	12.78	248.40
			3.48	259.70
E Cb		4.7	245.1 ✓	
	56.96 So of PRC on E 60.52 ✓ ~ ~ ~ W			
E.Cb.		5.6	244.2 ✓	
+13		2.9	246.9	
W.Cb		1.0	248.8 ✓	
	85.44 So of PRC on E 90.78 ~ ✓ ~ ~ W } = E.C. = 20' So. of SL Fir.			
W.Cb		2.8	247.0 ✓	
+13		4.5	245.3	
E.Cb		6.3	243.5 ✓	

		249.84			
		50' So. of Fir			
E. Cb			7.0	242.8	✓
+13			5.0	244.8	
W. Cb			3.7	246.1	✓
		75' So. of Fir			
W. Cb			4.4	245.4	✓
+13			6.3	243.5	
E. Cb			8.0	241.8	✓
		100' So			
E. Cb			8.8	241.0	✓
+13			7.2	242.6	
W. Cb			5.7	244.1	✓
		125' So			
W. Cb			6.7	243.1	✓
+13			7.8	242.0	
E. Cb			8.9	240.9	✓
		150' So.			
E. Cb			9.6	240.2	✓
+13			8.4	241.4	
W. Cb			7.7	242.1	✓

		175' So			
W. Cb			9.5	240.3	✓
+13			9.6	240.2	
E. Cb			10.1	239.7	✓
		200' So			
E. Cb			11.9	237.9	✓
+13			11.6	238.2	
W. Cb			11.5	238.3	✓
		225' So			
T.P.	0.94	237.95	12.83	237.01	
W. Cb			1.5	236.4	✓
+13			1.6	236.3	
E. Cb			2.4	235.6	✓
		250' So			
E. Cb			6.1	231.9	✓
+13			4.8	233.2	
W. Cb			3.5	234.5	✓
		275' So.			
W. Cb			6.2	231.8	
+13			8.2	229.8	
E. Cb			10.5	227.5	✓

237.95

300.30 = HL. ELM

E.Cb		13.5	224.5
+13		11.5	226.5
W.Cb		9.1	228.9

11/24/20 Dunkle re-x-section according to dotted lines C. Moore
GRAPE B Moore See page 74

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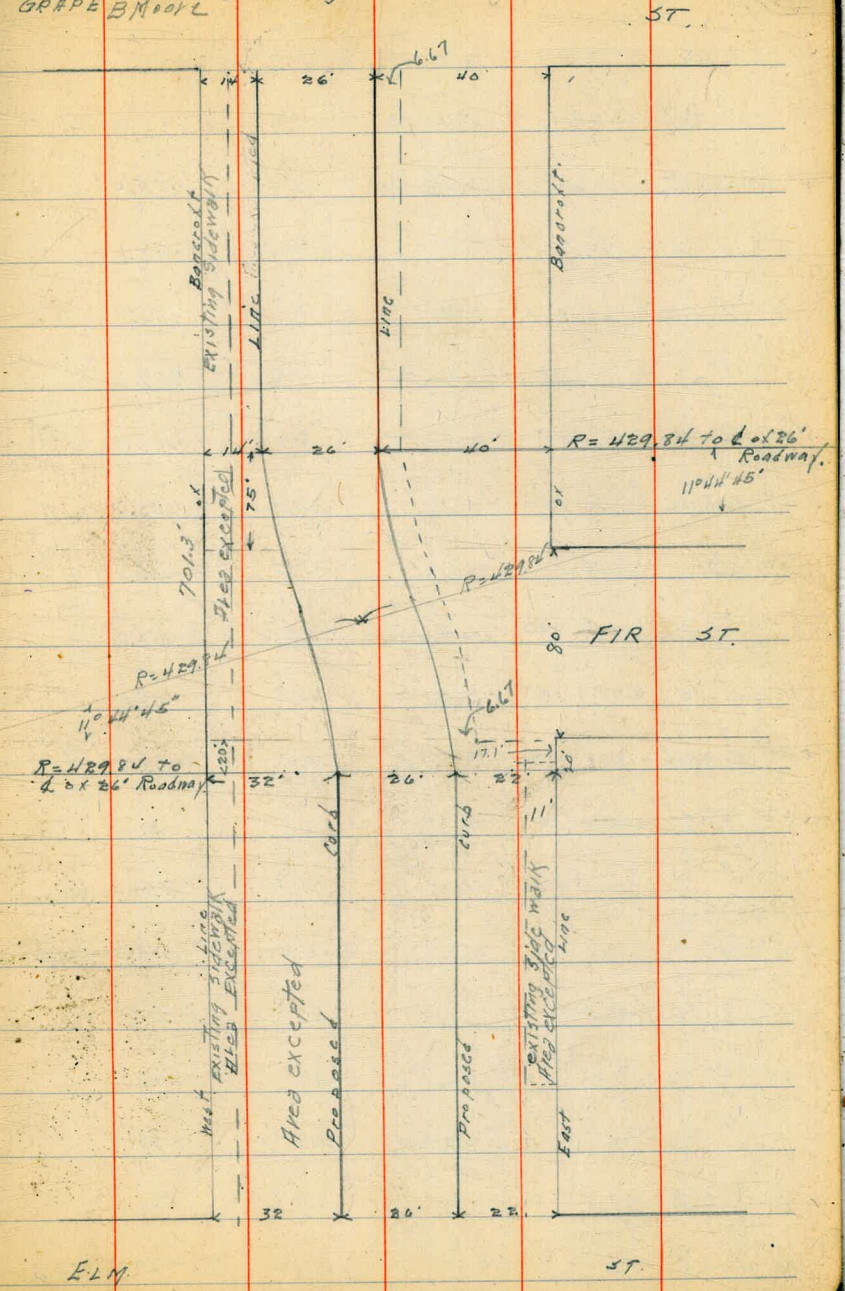


7/30/19 Gregory / Miller / Shaw. Levels at 1st & Spruce.

on B.M.	2.30	257.30		255.00	NW 1st & Thorn
on cb. E side 200 No. of Spruce			2.3	255.0	
in gutter " " " " "			3.4	253.9	
on E rail " " " "			3.1	254.2	
" W " 150' " " "			3.7	253.6	
" E " 150' " " "			3.6	253.7	
in gutter E side 150' " "			3.8	253.5	
on cb " " " " "			2.7	254.6	
" " " " 100' " "			3.3	254.0	
in gutter " " 100' " "			4.3	253.0	
on E rail 100' " "			4.0	253.3	
" W " 100' " "			4.3	253.0	
" " " 50' " "			4.9	252.4	
" E " 50' " "			5.0	250.3	
in gutter E. side 50' " "			4.7	252.6	
on cb " " 50' " "			3.8	253.5	
" " " " N.L. Spruce			4.3	253.0	
in gutter " " " "			5.3	252.0	
on E rail N.L. Spruce			5.3	252.0	= 15.9 W. of E. Cb

257.30

on W. rail of E Track N.L. Spruce	5.0	252.3	= 21.7 W. of E Cb
" E " " W " " "	5.6	251.7	= 33.1 " " "
" W " " " " " "	5.4	251.9	= 38.5 " " "
in gutter W side " "	6.2	251.1	
on curb " " " "	5.8	251.5	
" Nail Spruce W.L. First	5.9	251.4	
in No. 1 cement gutter " "	7.7	249.6	= Outlet 1'x2' wood box.
" " " " 50' W. of First	11.0	246.3	= 3' cement gutter
" " cb " " "	10.6	247.3	
W rail W Track. No. Cb Line Spruce	5.4	251.9	46' W. of E.L. 1st
E. " " " " " "	5.6	251.7	40 " " "
W " E " " " "	5.1	252.2	26.3 " " "
E " " " " " "	5.3	252.0	19.9 " " "
No. Cb Spruce E.L. 1st.	4.2	253.1	
Cement Gutter N. side Spruce E.L. 1st	5.4	251.9	= 5' Cement Gutter Inlet 1'x2' box.
N. rail of N. Track E.L. 1st	4.5	252.8	16.1 So. of Ncb
S " " " " "	4.2	253.1	21.8 " " "
N " " S " " "	4.5	252.8	33.3 " " "
S " " " " "	4.2	253.1	38.6 " " "
T.P. 858	264.00	1.88	255.42

on outside 5' gutter N side Spruce 50' E. of 1st 6.4

on inside " " " " " " " 6.7

on cb " " " " " " 6.0

" " " " " 100' " " 0.9

" inside 5' gutter " " " " " 1.5

" outside " " " " " " " 1.3

8/4/19 Gregory. Proposed GRADES on BANCROFT ST Elm to Grape.

	W	E
Old S.L. GRAPE	269.0 ~~270.0~~	269.0 ~~270.0~~
+50	269.33	
1+00	268.67	
1+50	268.0	
2+00	267.33	
R=449.81 to ℄ Δ11°44'45"		
2+26=PC.	258.0	258.0
2+67.72 on E 2+70.39 on W	256.0	255.5
3+10.45 on E 3+15.78 on W } =PRC.	253.0	253.0
3+55.84 on E 3+58.50 on W	247.5	248.0
4+01.23 EC=20'So. of Fir	242.0	242.0
50' So. of Fir	241.23	241.23
100'	239.94	239.94

160' So. of Fir	238.39				238.39	
175 " "	237.6				237.6	
190 " "	236.84				236.44	236.44
250' So	232.30				232.3	230.2
300' So = M.L. Elm	228.5				228.5	

273.25 SW. Grape bpk.

270	267.33	264.67	262		259.33
3.27	5.94	8.60	11.27		1.07
W +0.1	+0.4	+0.2	-0.2		+0.1
E -0.2	-0.5	-0.4	-5.7		-3.0

258 2.40	256 4.40	255.5 4.90	253.0 7.4	247.5 12.90	248 12.40	
+0.2 -2.7	-0.2	-1.5	+0.2 -4.8	+1.1	-3.2	

242 6.61	241.23 7.38	239.94 8.67	238.39 10.22	236.44 12.17	230.2 6.13	
+5.1 +0.9	+11.8 +1.6	+4.2 +1.1	+3.0 +1.6	+4.7 +2.4 +1.4	+2.6 +4.3 +1.6 -0.5	

242	
+1.33	
+1.1	-4.1
+0.5	
+0.4	

X-section Bancroft from N.L. of Grape to S.L. Elm.
" " Taken on Lines shown on Paving Plans or see sketch Page 70

B.M. Spk S.W. Grape & Bancroft 273.25
3.37
276.62

N.L. Grape 60' wide 10' walks 10' 1/4's

W.L. Bancroft 80' wide	2.5	274.1	
Crb	2.0	274.6	
1/4	2.6	274.0	
C/L	2.4	274.2	
1/4	2.0	274.6	
Crb	1.9	274.7	
E.L.	1.4	275.2	
S. curb			
E.L.	1.8	274.8	
Crb	2.2	274.4	
1/4	2.5	274.1	
C/L	2.9	273.7	
1/4	3.1	273.5	
Crb	2.6	274.0	
W.L.	3.1	273.5	
S. 1/4			
W.L.	3.3	273.3	
Crb	3.3	273.3	
1/4	3.4	273.2	
C/L	3.4	273.2	
1/4	3.0	273.6	
Crb	2.9	273.7	
E.L.	2.5	274.1	
Center			
E.L.	3.1	273.5	
Crb	3.4	273.2	
1/4	3.6	273.0	
C/L	3.7	272.9	
1/4	4.0	272.6	
Crb	3.8	272.8	
W.L.	3.7	272.9	

1/13/20 Dunkle
C Moore
B Moore

276.67

Sou 1/4

W.L.	4.0	272.6
Crb	4.2	272.4
1/4	4.5	272.1
C/L	4.4	272.2
1/4	4.3	272.3
Crb	4.1	272.5
E.L.	3.7	272.9

Sou Curb

E.L.	4.6	272.0
Crb	4.8	271.8
1/4	4.9	271.7
C/L	5.1	271.5
1/4	5.1	271.5
Crb	5.1	271.5
W.L.	4.6	272.0

Sou. Line Grape

W.L.	5.0	271.6
Crb	5.5	271.1
1/4	5.7	270.9
C/L	6.2	270.4
1/4	5.7	270.9
Crb	6.0	270.6
E.L.	5.2	271.4

0+25 S. of Sou. Line of Grape as 60' wide

E.L.	7.5	269.1
+6.67 = E. curb Line	7.2	269.4
℄ between curbs	6.8	269.8
W. crb	6.7	269.9
+4	6.3	270.3
+7.8 W.L.	5.5	271.1

		276.62		
		0+50	500	
W.L.			6.6	270.0
+4			7.3	269.3
+7.9 W. Crk			7.9	268.7
CTr			8.1	268.5
E. Crk			8.6	268.0
+6.67 E.L.			8.4	268.2
		+75		
E.L.			11.3	265.3
Crk			10.1	266.5
CTr			9.5	267.1
Crk			9.2	267.4
+4			8.2	268.4
+7.8 W.L.			7.7	268.9
		1+0		
W.L.			8.9	267.7
+4			9.7	266.9
+7.8 Crk			10.3	266.3
CTr			10.5	266.1
Crk			12.5	264.1
E.L.			15.6	261 0
T.P.	1.63	266.18	12.07	264.55
		1+25		
E.L.			7.5	258.7
Crk			6.3	259.9
+8			1.6	264.6
CTr			1.5	264.7
Crk			1.4	264.7
+4			1.1	265.1
+7.8 W.L.			+ 0.3	266.5

		266.18		
		1+50		
W.L.			1.9	264.3
+4			2.7	263.5
+7.7 Crk			3.1	263.1
CTr			2.7	263.5
+4			2.9	263.3
Crk			4.8	261.4
E.L.			5.9	260.3
		1+75		
E.L.			13.3	252.9
Crk			10.3	255.9
+8			5.7	260.5
CTr			4.7	261.5
Crk			4.6	261.6
+7.7 = W.L.			3.0	263.2
		2+0		
W.L.			4.1	262.1
+6			5.7	260.5
Crk			6.9	259.3
CTr			6.3	259.9
Crk			12.8	253.4
E.L.			17.5	248.7
		2+25		
E.L.			12.4	253.8
Crk			10.2	256.0
+6			8.0	258.2
CTr			7.3	258.9
Crk			7.0	259.2
+7.6 W.L.			4.9	261.3

766.18

2+45 = P.C.

W.L.	5.6	260.6
+3	6.9	259.3
+7.5 crk	7.8	258.4
ctr	8.4	257.8
crk	10.9	255.3
E.L.	12.7	253.5

Note- 5°30' on curve arc on west curb Line and 6.67 E of E. curb Line

2+75 26 on W. curb Line 3+73 02 on E dotted Line

E.L.	13.1	253.1
crk	11.7	254.5
CTr	9.8	256.4
crk	9.42	257.0
+4	8.1	258.1
+8.3 W.L.	7.1	259.1

3+05 52 on W. crk 3+01 24 E.L.

W.L.	8.2	258.0
+5	10.5	255.7
+11.3 crk	11.1	255.1
CTr	11.3	254.9
crk	14.2	252.0
E.L.	15.2	251.0

3+35 78 on W. crk 3+29 06 on E.L. = P.R.C

E.L.	21.1	245.1
crk	17.6	248.6
CTr	14.5	251.7
+7	12.7	253.5
crk	12.9	253.3
+10	12.6	253.6
+16 W.L.	10.6	255.6
T.P. 0.09	12.88	253.20

258.39

3+64 26 W. crk 3+59 78 E.L.

W.L.	0.0	253.4
+8	1.7	251.7
+20.2 W. crk	2.1	251.3
CTr	3.8	249.6
crk	5.3	245.1
E.L.	10.7	242.7

3+92 74 W. crk 3+90 50 E.L.

E.L.	11.7	241.7
crk	9.0	244.4
CTr	6.3	247.1
crk	4.4	249.0
+23.1 = W.L.	2.1	251.3

S.L. Fir St

W.L.	1.9	251.5
+3	2.0	251.4
+4	3.4	250.0
+17	3.9	249.5
+24 W. crk	5.1	248.3
CTr	6.8	246.6
crk	9.0	244.4
+6.67	10.4	243.0
+9	11.8	241.6
E.L. Bancroft 2580' St	21.8	231.6

S.L. Fir St

E.L. Bancroft 2580' St	11.3	242.1
+16.5	11.8	241.6
+18.5	10.4	243.0
E. crk	9.0	244.4
CTr	6.8	246.6
W crk	5.1	248.3
+7	3.9	249.5
+20	3.4	250.0
+21	2.0	251.4
+24 W.L.	1.9	251.5

253.39

4+21.22 = P.T

W.L.	3.1	250.3
+3	3.2	250.2
+3	4.3	249.1
+18	4.5	248.9
+25.2 = W. crk	6.3	247.1
C Tr	8.1	245.3
crk	10.6	242.8
+11 E.L. = 11' W of E.L. Bancroft	11.5	241.9

4+50

E.L.	12.4	241.0
+11 crk	10.3	243.1
C Tr	8.5	244.9
crk	7.2	246.2
+7	6.2	247.2
+21	5.0	248.4
+25 W.L.	3.7	249.7

4+75

W.L.	4.5	48.9
+4	5.3	48.1
+5	6.3	47.1
crk	8.0	45.4
C Tr	9.5	43.9
crk	11.5	41.9
+11 E.L.	13.1	40.3

5+0

E.L	13.7	39.7
+11 = crk	12.3	41.1
C Tr	10.9	42.5
crk	9.2	44.2
+20	7.7	45.7
+25 W.L.	5.5	47.9

253.39

5+25

W.L.	7.1	46.3
+6	9.3	44.1
crk	10.2	43.2
C Tr	11.3	42.1
crk	12.6	40.8
+11 E.L.	14.0	39.4
5.47	12.58	240.81

5+50

E.L.	7.4	38.9
+11 crk	6.1	40.2
C Tr	4.9	41.4
crk	4.2	42.1
+19	3.1	43.2
+25 W.L.	1.3	45.0

5+75

W.L.	2.9	43.4
+3	4.2	42.1
+13	5.4	40.9
crk	5.9	40.4
C Tr	5.9	40.4
crk	6.5	39.8
+11 E.L.	7.8	38.5

6+0

E.L.	8.5	37.8
+11 = crk	8.2	38.1
C Tr	8.0	38.3
crk	7.8	38.5
+21	6.5	39.8
+25 W.L.	4.8	41.5

		246.28			
		6+25			
W.L.			6.8	39.5	
+5			9.1	37.2	
crb			9.7	36.6	
ctr			9.9	36.4	
crb			10.6	35.7	
+6			11.4	34.9	
+11 E.L.			10.7	35.6	
		6+57			
E.L.			13.7	32.6	
+3			15.2	31.1	
+11 E. Curb			15.2	31.1	
ctr			13.8	32.5	
crb			12.4	33.9	
+22			10.9	35.4	
+25 = W.L.			9.9	36.4	
		6+57			
W.L.			9.9	36.4	
+3			10.9	35.4	
+25 crb			12.4	33.9	
ctr			13.8	32.5	
+11 crb			15.2	31.1	
+11			16.2	30.1	
+22 = E.L. Bancroft			17.3	29.0	
	1.65	235.37	12.56	233.72	

	235.37		228.9
	6+75		
E.L. Bancroft		9.5	25.9
+11		9.6	25.8
+22 = crb		7.8	27.6
ctr		5.4	30.0
crb		3.3	32.1
+8		2.4	33.0
+22		1.5	33.9
+25 W.L.		0.7	34.7
7+01.30 = N.L. Elm 25 80' St			
W.L.		3.1	32.3
+3		4.0	31.4
+18		5.2	30.2
+25.6 crb		6.6	28.8
ctr		9.0	26.4
crb		11.0	24.4
+11		12.1	23.3
+22 E.L. Bancroft		13.7	21.7
N.L. Elm 25 60' St & Bancroft 80' 14' side walk 13'. 14's on Bancroft 10' walk 10 1/4's Elm			
E		14.5	20.9
crb		12.8	22.6
"		11.4	24.0
ctr		9.8	25.6
"		7.7	27.7
crb		6.7	28.7
W		5.4	30.0

N curb

W	6.0	29.4
crb	7.7	27.7
1/4	8.5	26.9
ctr	10.5	24.9
1/4	11.9	23.5
crb	13.2	22.2
E	14.8	20.6

N 1/4

E	15.2	20.2
crb	13.5	21.6
1/4	12.3	23.1
ctr	10.9	24.5
1/4	9.1	26.3
crb	8.1	27.3
W	6.9	28.5

Center

W	7.9	27.5
crb	8.8	26.6
1/4	9.7	25.7
ctr	11.6	23.8
1/4	13.0	22.4
crb	14.1	21.3
E	15.1	20.3

S 1/4

E	15.2	20.2
Crb	14.3	21.1
1/4	13.0	22.4
ctr	11.6	23.8
1/4	10.5	24.9
crb	9.5	25.9
W	8.6	26.8

	So. curb		
W		9.2	26.2
crb		10.1	25.3
1/4		10.9	24.5
ctr		11.8	23.6
1/4		13.0	22.4
crb		14.1	21.3
E.		15.1	20.3
	S. L. Elm		
E		15.0	20.4
crb		14.0	21.4
1/4		13.1	22.3
ctr		12.1	23.3
1/4		11.3	24.1
crb		10.7	24.7
W		10.2	25.2

61.7

17) 8.00 (.47
7 00
1000
875
1 25

5 | 11.7
2.34
2.35
4.7°

4 | 17.50
1.75
7.50
7.50
0

6 | 4.50
4.800

12.35
1.75
14.10
7.50
21.60°

21.60
9.25
30.85
9.25
40.10°
9.2

49.35
12.35
61.7°

P C 1/4 C 1/4 cl P
0 — 12.35 — 21.60 — 30.85 — 40.10 — 49.35 — 61.70

4.280

6 | 4.50
1.8270

4
12) 8.00

4 | 70
17½

20 - 375 - 55 - 775 - 9
110

55
17.5
7.25

28.5

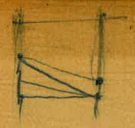
12) 3.10 (.108
2.80
1000
1000

.028
50
1400
1.12

238
28.5
12) 9.75 (.076
8.75
750

229.9
231.02

.076
50
3800
3.14



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.