1043

LEVEL BOOK
373

KEUFFEL & ESSER CO.

DRAWING MATERIALS
AND
SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

22+00		G=5.8
6	7.5	
+50	77	
5	72	
+50	74	
4	70	
+50	64	
3	60	
1+50	48	
+60	68	
2+00	150	
+15	15.0	
+~~55~~	20.0	
+50	9.0	

Sept 10-11, 1918

22+00		G=5.8	
6	7.5		- 1.7
+50	7.7		- 1.9
5	7.2		- 1.4
+50	7.4		- 1.6
4	7.0		- 1.2
+50	6.4		- 0.6
3	6.0		- 0.2
+50	9.0		- 3.2
+45	20.0		- 14.2
+15	15.0		- 9.2
2	15.0		- 9.2
1 +60	6.8		- 1.0
1 +50	4.8	G=5.8	+ 10

Copied into Book 1046

21+50		G=4.2	
6+50	6.0		- 1.8
6	5.8		- 1.6
+50	5.9		- 1.7
5	6.0		- 1.8
+50	5.9		- 1.7
4	6.5		- 2.3
+75	6.0		- 1.8
+65	7.8		- 3.6
+50	11.0		- 6.8
3	20.0		- 15.8
+50	21.0		- 16.8
2	21.3		- 17.1
+50	22.8		- 18.6
+35	21.0		- 16.8
+20	11.5		- 7.3
+05	3.5		+ 0.7
1	3.5		+ 0.7

21+00		G=5.1	
4+50	6.5		-1.4
4	7.0		-1.9
+50	10.7		-5.6
3	17.5		-12.4
+50	21.7		-16.6
2	23.0		-17.9
+50	23.5		-18.4
+25	10.0		-4.9
1	3.0		+2.1

second page for 20+50

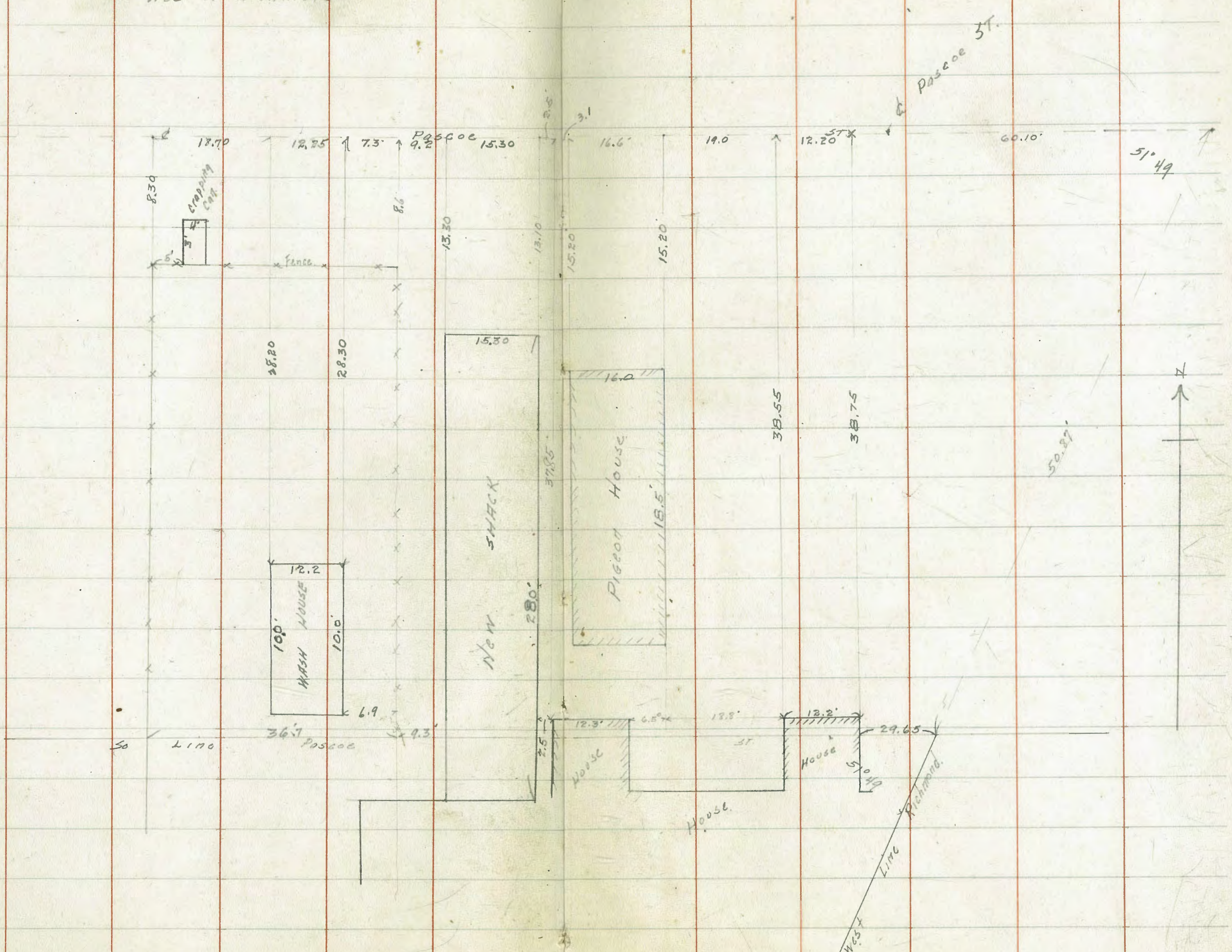
20+00		G=4.3	
1+00	2.5		+1.8
+35	3.5		+0.8
+50	18.0		-13.7
2	23.0		-18.7
+50	22.0		-17.7
3	19.0		-14.7
+50	14.0		-9.7
4	9.0		-4.7

19+50		G=3.8	
1+50	3.0		+0.8
+95	4.0		-0.2
2+00	19.2		-15.4
+08	20.5		-16.7
+25	20.0		-16.2
+50	14.5		-10.7
3+00	17.5		-13.7
+50	19.0		-15.2
4+00	22.0		-18.2
+25	21.0		-17.2
+50	6.0		-2.2
19+00		G=4.6	
4+50	7.7		-3.1
4	7.0		-2.4
3+75	19.0		-14.4
+50	20.0		-15.4
+25	23.0		-18.4
3+00	16.0		-11.4
2+75	5.0		-0.4
2+50	4.8		-0.2

20+50		G=5.2	
1+20	6.7		- 1.5
+25	20.5		- 15.3
+50	24.0		- 18.8
2	23.8		- 18.6
+50	21.7		- 16.5
3	21.0		- 15.8
+50	13.0		- 7.8
4	9.0		- 3.8
+50	7.0		- 1.8

9/26/15 Gregory Miller Shaw

Survey to Locate Improvements in Pascoe St West of Richmond St.



9/26/18 Gregory. CROSS-SECTION OF CALHOUN ST from N.L. Mason St on E To N.L. Taylor St — 40' wide, 10' cbs, 5' 1/4's

B.M	0.55	23.88		23.33	spit pole S.W. Mason + Calhoun p44, book 1042
		N.L. Mason St			
W			1.5	22.4	
cb			1.4	22.5	
1/4			1.2	22.7	
c			1.2	22.7	
1/4			1.1	22.8	
cb			1.0	22.9	
E			0.8	23.1	
		30' No.			
E			1.3	22.6	
cb			1.8	22.1	
1/4			2.1	21.8	
c			2.2	21.7	
1/4			2.4	21.5	
cb			2.7	21.2	
W			2.7	21.2	
		80' No			
W			4.0	19.9	

		23.88		
cb			4.2	19.7
1/4			4.4	19.5
c			4.2	19.7
1/4			4.2	19.7
cb			4.2	19.7
E			3.4	20.5
		130' No		
E			4.5	19.4
+2			4.6	19.3
+4			5.6	18.3
cb			6.0	17.9
1/4			6.1	17.8
c			5.9	18.0
1/4			5.8	18.1
cb			5.7	18.2
W			5.6	18.3
		170' No.		
W			6.5	17.4
cb			6.8	17.1
1/4			7.1	16.8

		2388						2388				
C			7.0	16.9		E			7.8	16.1		
1/4			6.9	17.0				300' No.				
cl			6.5	17.4		E			8.8	15.1		
+5			6.0	17.9		cl			9.3	14.6		
E			5.4	18.5		1/4			9.8	14.1		
		200' No				C			9.8	14.1		
E			6.5	17.4		1/4			9.6	14.3		
cl			7.3	16.6		cl			9.3	14.6		
1/4			7.7	16.2		W			9.8	14.1		
C			7.8	16.1				330' No.				
1/4			7.7	16.2		W			10.6	13.3		
cl			7.6	16.3		cl			10.5	13.4		
W			7.5	16.4		1/4			10.2	13.7		
		250 No.				C			9.9	14.0		
W			8.6	15.3		1/4			10.1	13.8		
cl			8.5	15.4		cl			9.7	14.2		
1/4			8.7	15.2		E			9.6	14.3		
C			8.8	15.1				356.5 No. = N.L Plaza				
1/4			9.0	14.9		E			9.8	14.1		
cl			8.6	15.3		cl			10.2	13.7		

		2388					2388				
1/4			10.4	13.5		1/4			11.7	12.2	
c			10.5	13.4		cb			11.5	12.4	
1/4			10.6	13.3		W			11.4	12.5	
cb			11.0	12.9				So. Curb			
+7			11.0	12.9		W			11.4	12.5	
W			10.4	13.5		+3			11.7	12.2	
		400' No.				cb			11.7	12.2	
W			10.8	13.1		1/4			11.6	12.3	
+3			11.3	12.6		c			11.8	12.1	
cb			11.5	12.4		1/4			12.0	11.9	
1/4			11.3	12.6		cb			11.9	12.0	
c			11.3	12.6		E			11.5	12.4	
1/4			11.2	12.7				So. Quarter			
cb			11.0	12.9		E			11.5	12.4	
E			10.6	13.3		+2			12.0	11.9	
		#25' No. = So. Line Wallace St			50 wide 10 abs 7 1/2 1/25 on E side only	cb			11.9	12.0	
E			11.3	12.6		1/4			12.0	11.9	
cb			11.7	12.2		c			11.9	12.0	
1/4			11.8	12.1		1/4			11.9	12.0	
c			11.9	12.0		cb			12.1	11.8	

		2388			
W			11.4	12.5	
		Center Wallace St			
W			11.5	12.4	
+5			12.4	11.5	
cb			12.3	11.6	
1/4			12.0	11.9	
C			12.1	11.8	
1/4			12.1	11.8	
cb			11.9	12.0	
E			12.1	11.8	
		No. Quarter			
E			11.8	12.1	
cb			12.0	11.9	
1/4			12.3	11.6	
C			12.2	11.7	
1/4			12.2	11.7	
cb			12.6	11.3	
+7			12.5	11.4	
W			11.4	12.5	

		2388	CALHOUN		
		No Curb			
W			11.6	12.3	
+3			12.6	11.3	
cb			12.7	11.2	
1/4			12.3	11.6	
C			12.5	11.4	
1/4			12.4	11.5	
cb			12.2	11.7	
E			12.1	11.8	
		No Line Wallace St			
E			12.2	11.7	
cb			12.7	11.2	
1/4			13.0	10.9	
C			12.7	11.2	
1/4			12.5	11.4	
cb			12.7	11.2	
+7			12.8	11.1	
W			11.8	12.1	
T.P.	2.56	13.47	12.99	10.91	

1347

50' No

W			3.0	10.5	
cl			3.5	10.0	
1/4			3.4	10.1	
c			3.3	10.2	
1/4			3.8	9.7	
cl			3.6	9.9	
+6			3.3	10.2	
E			2.4	11.1	

100' No

E			3.4	10.1	
cl			4.2	9.3	
1/4			4.3	9.2	
c			4.5	9.0	
1/4			4.6	8.9	
cl			4.5	9.0	
W			3.7	7.8	

150' No

W			5.0	8.5	
cl			5.2	8.3	

1347

1/4			5.2	8.3	
c			5.3	8.2	
1/4			5.1	8.4	
cl			4.8	8.7	
E			4.4	9.1	

185' No

E			7.7	5.8	
+8			6.8	6.7	
cl			5.3	8.2	
1/4			6.0	7.5	
c			6.0	7.5	
1/4			6.1	7.4	
cl			6.8	6.7	
W			7.5	6.0	

190' No

W			7.8	5.7	
cl			7.3	6.2	
1/4			6.3	7.2	
c			6.1	7.4	
1/4			5.9	7.6	

		1347			
ch			5.6	7.9	
E			5.1	8.4	
		100' No.			
E			5.0	8.5	
ch			5.5	8.0	
1/4			6.2	7.3	
c			6.3	7.2	
1/4			6.6	6.9	
ch			7.9	5.6	
W			8.6	4.9	
		205' No.			
W			9.0	4.5	
ch			7.6	5.9	
1/4			6.8	6.7	
c			6.4	7.1	
1/4			6.5	7.0	
ch			6.8	6.7	
E			8.9	4.6	
T.P.	V.68	9.00	7.15	6.32	

		9.00			
		235' No.			
E			5.7	3.3	
+7			5.4	3.6	
ch			4.5	4.5	
1/4			2.5	6.5	
c			2.6	6.4	
1/4			2.8	6.2	
ch			4.1	4.9	
W			5.2	3.8	
		275' No.			
W			6.1	2.9	
ch			5.6	3.4	
1/4			3.8	5.2	
c			3.4	5.6	
1/4			3.5	5.5	
ch			5.6	3.4	
+5			7.3	1.7	
E			5.4	3.6	
		325' No.			
E			5.9	3.1	

		9.00			
+3			7.3	1.7	
+5			7.3	1.7	
cb			5.6	3.4	
1/4			4.2	4.8	
C			4.2	4.8	
1/4			4.6	4.4	
cb			6.3	2.7	
W			7.0	2.0	
		375' No.			
W			6.7	2.3	
cb			6.9	2.1	
1/4			4.9	4.1	
C			4.8	4.2	
1/4			4.9	4.1	
cb			6.7	2.3	
+5			8.1	0.9	
E			5.9	3.1	
		402' No.			
E			6.5	2.5	
cb			7.6	1.4	

		9.0			
cb			7.3	1.7	
+2			5.7	3.3	
1/4			5.1	3.9	
C			5.2	3.8	
1/4			5.3	3.7	
cb			7.0	2.0	
W			7.0	2.0	
		406' No.			
W			7.2	1.8	
cb			7.2	1.8	
1/4			5.5	3.5	
C			5.2	3.8	
1/4			4.9	4.1	
cb			4.8	4.2	
E			4.4	4.6	
		418' No.			
E			4.5	4.5	
cb			4.8	4.2	
1/4			5.3	3.7	
C			5.3	3.7	

1/4	9.00	5.4	3.6	
cb		7.1	1.9	
W		7.1	1.9	
	425' No. = 5th TAYLOR ST			100' wide 16' obs 17' 1/2's
W		7.1	1.9	
cb		7.0	2.0	
1/4		5.5	3.5	
C		5.3	3.7	
1/4		5.3	3.7	
cb		7.0	2.0	
+5		8.2	0.8	
+7		8.3	0.7	
E		8.1	0.9	
	So Cb.			
E		7.4	1.6	
+5		8.1	0.9	
+10.32=cb		8.3	0.7	
+6.04=1/4		6.1	2.9	
+6.04=C		5.5	3.5	
+6.04=1/4		5.4	3.6	

CALHOUN

	9.00		
+6.04=cb.		6.8	2.2
+10.32=W		7.2	1.6
	So. Quarter		
W.		6.7	2.3
+3		7.9	1.1
+10.66=cb		6.8	2.2
+7.14=1/4		5.6	3.4
+7.15=C		5.7	3.3
+7.14=1/4		7.3	1.7
+3.0		8.3	0.7
+7.15=cb		8.2	0.8
+10.66=E		6.8	2.2
	Center Taylor St.		
E		6.8	2.2
411 cb.		7.9	1.1
+5		8.5	0.5
+8.75=1/4		8.1	0.9
+8.75=C		6.0	3.0
+8.75=1/4		5.6	3.4
+4		5.7	3.3
+8.75=cb.		7.1	1.9

	9.00		
+11 = W		7.8	1.2
	No. Quarter		
W		8.3	0.7
+ 11.34 = cb		6.8	2.2
+4		6.0	3.0
+ 9.35 = ¼		5.7	3.3
+6		5.8	3.2
+ 9.36 = c		8.0	1.0
+ 9.35 = ¼		8.2	0.8
+ 9.36 = cb		7.3	1.7
+ 11.34 = E		6.7	2.3
	No. Curb		
E		6.9	2.1
+ 11.68 = cb.		7.4	1.6
+ 10.46 = ¼		7.8	1.2
		8.2	0.8
+8			
+ 10.46 = c		7.9	1.1
+6		5.7	3.3
+ 10.46 = ¼		5.8	3.2
+7		5.9	3.1
+ 10.46 = cb		7.1	1.9

	9.00		
+ 11.68 = W		7.7	1.3
	N.L. TAYLOR ~~St.~~		
W		8.0	1.0
		7.8	1.2
+7			
+12 = cb		6.6	2.4
+2		6.0	3.0
+ 11.5 = ¼		5.8	3.2
+ 11.5 = c		7.9	1.1
+ 11.5 = ¼		7.5	1.5
+ 11.5 = cb		7.2	1.8
+12 = E		6.7	2.3
T.P.		5.82	3.18

9/26/18 Gregory

CROSS SECTION OF TAYLOR ST Xfrom Calhoun To Joan St

100' ST 16 chs 17 1/43

TP from last page	4.33	7.51		3.18	
		E L. Calhoun St			
No.			5.2	2.3	
cb			5.4	2.1	
1/4			5.2	2.3	
c			5.3	2.2	
1/4			5.3	2.2	
cb			5.9	1.6	
So.			6.6	0.9	
		30' E on So 00 E on No } = E.L Calhoun on No.			
So			4.7	2.8	
+4			5.9	1.6	
+13			6.1	1.4	
cb			5.0	2.5	
1/4			5.0	2.5	
+7			5.2	2.3	
c			5.2	2.3	
+19			5.6	1.9	
1/4			5.4	2.1	
cb			5.0	2.5	

TAYLOR 14

		7.51		
No.			5.2	2.3
		50' E of Calhoun on No.		
No.			5.6	1.9
cb			5.5	2.0
+10			4.4	3.1
1/4			5.0	2.5
+7			5.0	2.5
c			5.4	2.1
+10			4.8	2.7
1/4			4.9	2.6
cb			4.8	2.7
+3			5.9	1.6
+12			5.3	2.2
So			3.7	3.8
		100' E		
So.			4.1	3.4
+4			5.2	2.3
+13			5.7	1.8
cb			4.9	2.6
1/4			4.7	2.8

		7.51						7.51				
+7			47	2.8				200	E			
C			50	2.5		50.				33	4.2	
+10			48	2.7		+5				49	2.6	
1/4			48	2.7		+13				51	2.4	
+6			42	3.3		dr				46	2.9	
dr			51	2.4		1/4				49	2.6	
No			50	2.5		+7				48	2.7	
		150' E				C				52	2.3	
No.			52	2.3		+10				53	2.2	
dr			50	2.5		1/4				52	2.3	
+10			39	3.6		+8				45	3.0	
1/4			46	2.9		dr				56	1.9	
+7			48	2.7		No.				57	1.8	
C			49	2.6				225' E = W.L. JUAN St				
+10			51	2.4		No.				50	2.5	
1/4			49	2.6		dr				50	2.5	
dr			45	3.0		1/4				41	3.4	
+3			54	2.1		+9				42	3.3	
+11			53	2.2		C				41	3.4	
50.			34	4.1		+10				37	3.8	

		7.51									
1/4			3.6	3.9							
cb			3.9	3.6							
+4			5.8	1.7							
5a			4.3	3.2							
chk			1.13	6.38	Hydrant Taylor + Juan						

Levels over Herman St - Ck Elevations

Note - Curb and Sidewalk in from Univ Ave to N. Line Dwight - Street graded except intersection of Dwight St

	+	H.I.	−	Elev.	
	5.38	354.27		348.89	SE. Herman & Wightman
SE Wightman			5.36	348.91	
N.E "			4.74	349.53	
N.W "			4.34	349.93	
S.W "			4.88	349.39	
	0.85	344.66		343.81	BM S.E Herman & Landis
SE Landis			0.84	343.82	
NE "			0.30	344.36	
NW "			0.20	344.41	
SW "			0.80	343.86	
375' So of So Line Landis W Ck/break			6.25	338.41	
" " " E Ck -			6.25	338.41	
NW Dwight			10.70	333.96	
N.E "			10.70	333.96	
T.P.	1.30	335.65	10.31	334.35	
S.E "			2.30	333.35	
SW "	on old grade stake		2.26	333.39	
T.P.	3.21	329.00	9.86	325.79	

N.W Myrtle	3.20	325.80
NE "	3.20	325.80
SE "	3.70	325.30
S.E "	3.70	325.30
N.W Upas	7.50	321.50
S.W "	8.10	320.90
SE "	8.00	321.00
N.E "	7.70	321.30

4/20/19 Gregory Miller Shaw

Levels on ℄ of Witherby St and Juan St from Mission Hills To Old Town

on B.M.	2.37	285.27		282.90	Mon NE Sunset + Ingleside
T.P.	0.75	273.19	12.83	272.44	
E.L. Witherby + ℄ of Sunset Blvd.			12.7	260.5	
30.95 W. of above = ℄ With. + ℄			12.2	261.0	
30' So of last on ℄ of Witherby			10.9	262.3	
49.52 " " ℄ Sunset = S.L. Sunset			7.3	265.9	
5' So of S.L. Sunset on ℄ With			6.7	266.5	
30' " " " " "			8.1	265.1	
60' " " " " "			8.7	264.5	
100' " " " " "			10.0	263.2	
135' " " " " "			10.8	262.4	
150' " " " " "			12.3	260.9	
T.R	1.99	262.10	13.08	260.11	
	9.47	258.72	12.85	249.25	on Mon
200' So of S.L. Sunset.			1.1	257.1	
225 " " "			2.6	255.6	
249.1 So. " " = W.L. Juan			5.2	253.0	
274.1 " " " = ℄ Juan			7.4	250.8	
W.L. Witherby + ℄ Juan.			9.5	248.7	
50' W. of W.L. Witherby on ℄ Juan			12.3	245.9	
100' " " " " "			12.8	245.4	
T.P.	0.20	246.12	12.80	245.92	
150' " " " " "			1.4	244.7	
185 " " " " "			2.5	242.6	
211 " " " " "			6.5	239.6	
227 " " " " "			10.5	236.6	
T.P.	1.38	234.42	13.08	233.04	
247' " " " " "			3.5	230.9	
285 " " " " "			7.0	227.4	
310' " " " " "			9.6	224.8	
T.P.	0.01	221.34	13.09	221.33	
350' " " " " "			2.2	219.1	
375' " " " " "			4.8	216.5	
400' " " " " "			6.4	214.9	
430' " " " " "			11.8	209.5	
T.P.	0.05	208.39	15.00	208.34	
443' " " " " "			3.0	206.4	
470' " " " " "			5.7	202.7	

		208.39			
480' W. of W. L. Witherby		on L. Juan	8.1	200.3	
500' " " " "		" "	10.1	198.3	
T.P.	0.42	196.15	12.66	195.73	
550' " " " " "		" "	2.0	194.2	
600' " " " " "		" "	4.9	191.3	
630' " " " " "		" "	5.7	190.5	
650' " " " " "		" "	7.9	188.3	
700' " " "			12.1	184.1	
730' " " "			14.5	181.7	
765' " " "			14.8	181.4	
810' " " "			12.6	183.6	
850' " " "			8.0	188.2	
875' " " "			6.8	189.4	
915' " " "			7.2	189.0	
950' " " "			6.4	189.8	
970' " " "			8.6	187.6	
1025' " " "			10.1	186.1	
T.P.	3.10	188.56	10.69	185.46	Mon of Amp.
1058' " " "			2.0	186.6	
1065' " " "			0.8	187.8	

1110' W. of W. L. Witherby			0.3	188.3	
1130' " " "			1.8	186.8	
1165' " " "			6.7	181.9	
1215' " " "			12.3	176.3	
T.P.	0.50	176.46	12.60	175.96	
1240' " " "			5.3	171.3	
1260' " " "			7.8	169.8	
1280' " " "			9.9	166.7	
T.P.	0.48	164.06	12.88	163.58	
1325' " " "			8.5	155.6	
1345' " " "			9.8	154.3	
T.P.	0.37	151.51	12.92	151.14	
1375' " " "			2.6	148.9	ctr Arista
			2.62		on Mon
1415' " " "			7.9	143.6	
1460' " " "			11.7	139.8	
T.P.	0.29	139.03	11.77	138.74	
1515' " " "			4.0	135.	
1570' " " "			6.5	132.5	
1595' " " "			9.3	129.7	

		139.03			
T.P.	0.19	126.39	12.83	126.20	
1635' W. of W.L. Witherby	on L. Joan		2.1	124.3	
1665' " " "	"		4.2	122.2	
1700 " " "	"		7.1	119.3	= E.L. Conde
1750 " " "	"		10.9	115.5	= W.L. "
T.P.	0.10	113.72	12.77	113.62	
1800' " " "	"		2.9	110.8	
1845' " " "	"		7.0	106.7	
1895' " " "	"		13.3	100.4	
T.P.	1.38	102.14	12.96	100.76	
1940' " " "	"		8.4	94.7	
1960' " " "	"		11.2	90.9	
T.P.	1.23	90.73	12.64	89.50	
1980' " " "	"		3.8	86.9	
2000' " " "	"		8.1	82.6	
2027' " " "	"		12.6	78.1	
T.P.	0.26	78.23	12.76	77.97	
T.P.	6.06	73.89	10.60	67.63	
2050' W. " "	"		1.7	72.2	= E.L. Harney
2065' " " "	"		3.8	70.1	

2067 W. of W.L. Witherby			6.7	67.2	
2075' " " "			11.2	62.7	
2100' " " "			11.7	62.2	= W.L. Harney.
			11.57	62.32	= bottom bolt Hydrant.
T.P.	0.05	60.87	13.07	60.82	
T.P.	0.52	48.56	12.83	48.04	
T.P.	3.37	39.65	12.28	36.28	
			6.29	33.36 = 27	M. on N.E. Harney & San Diego.

7+35.38 EC.

6+50 Δ 19°46' L

5+62.88 PC.

R= 500
st= 87.12
lc = 172.50

1+90.06 EC.

1+50 Δ 104°12' R.

0+53.66 PC.

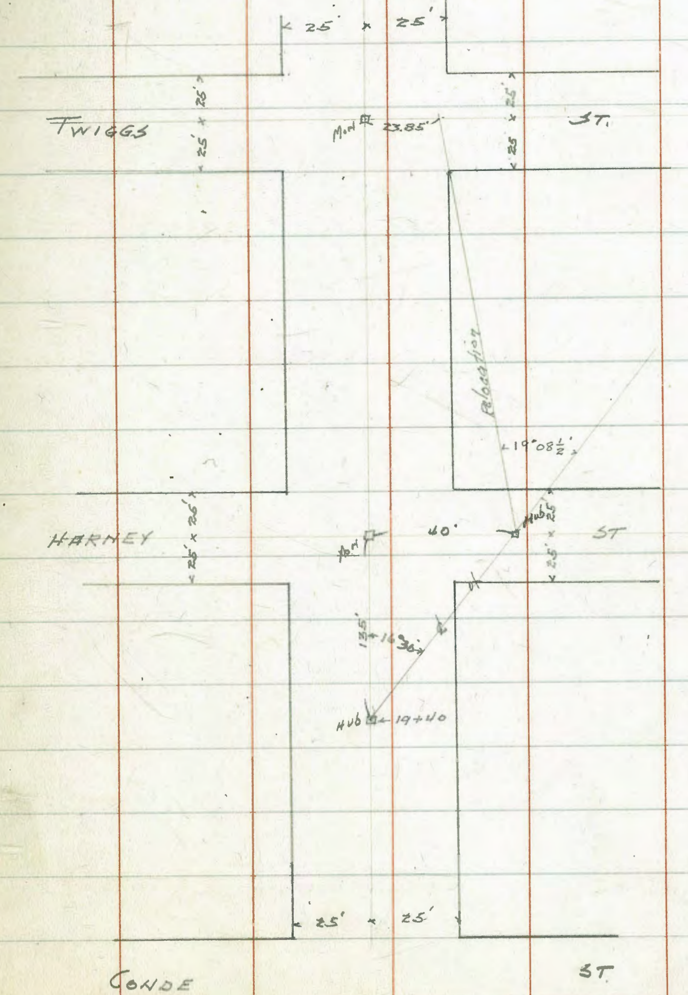
R= 75
st= 96.34
lc = 136.40

0+00

5/10/19 Levels on Relocation Juan St.

	0.14	94.04		93.90	on hub 19+40
19+40 page 20 = Δ pt 16°30'					
19+75			4.1	89.9	
20+00			7.0	84.0	
20+40			12.1	81.9	
T.P.	0.50	~~81.43~~	13.11	80.93	
20+65			4.6	76.8	
20+80.80 Δ pt 19°08'30"			6.9	74.5	
21+00			9.1	72.3	
21+40			12.5	68.9	
T.P.	0.43	69.07	12.79	68.64	
on BM	6.75	69.07	6.75	62.32	Hydrant Juan + Harney
22+00			1.5	67.6	
22+30			2.5	66.6	
22+65			4.7	64.4	
23+00			7.6	61.5	
23+50			10.0	59.1	
23+80			11.2	57.9	
T.P.	0.60	57.00	12.67	56.40	

24+00	2.0	55.0	
	6.7	51.0	
℄ Juan + N.L. Twiggs	9.8	47.2	
T.P.	8.51		Mon't ℄ Twiggs + ℄ Juan



5/5/19 Gregory Miller Shaw

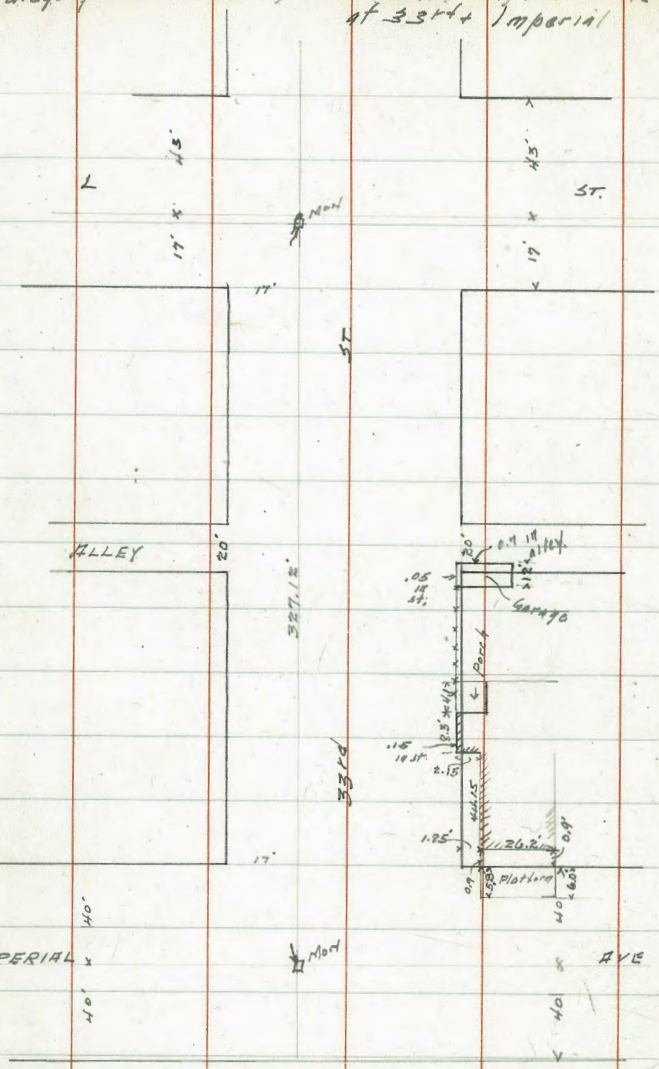
Levels on & of Juan St Relocation.

	1.62	250.87		249.25	Mon Juan + Witherby
0+00 = ℄ Juan + Witherby			0.1	250.8	
0+15			1.1	249.8	
0+25 = ℄ Juan St.			2.6	248.3	
0+53.66 = P.C.			4.9	246.0	
0+75			6.6	244.3	
1+00			8.8	242.1	
1+25			11.7	239.2	
T.P.	0.50	238.48	12.69	237.98	
1+50			12.1	236.4	
1+75			5.1	233.4	
1+90.06 = E.C.			6.6	231.9	
2+10			8.5	230.0	
2+50			9.5		
2+70			9.6		
2+90			10.7		
T.P.			12.49	225.99	

8/27/19 Gregory

Survey to Locate Improvements at 33rd & Imperial

24



x-section Orchard St from E.L. DeFoe To W.L. Ebers. Street 80' wide - 20' walks 10' 1/4 3/5

B.M. N.W. brass Ag curb. Delmar & DeFoe				36.12
B.M.	3.40	39.52		
		E.L. DeFoe		
N			8.1	31.4 ✓
Crb			8.6	30.9
1/4			9.2	30.3
Ctr			9.3	30.2 ✓
1/4			8.9	30.6
Crb			8.6	30.9
S			9.4	30.1
		0+25 East		
S			9.7	29.81
Crb			9.2	30.3
1/4			9.3	30.2
Ctr			9.2	30.3 ✓
1/4			8.7	30.8
Crb.			8.5	31.0
N			8.1	31.4 ✓

10/11/19 Dunkle
C. Moore
B. Moore

			39.52	
			0+50	
N			7.8	31.7 ✓
Crb			8.3	31.2
1/4			8.6	30.9
Ctr			8.3	30.7 ✓
1/4			9.1	30.4
Crb			8.9	30.6
S			9.3	30.2 ✓
			0+75	
S			8.0	31.51
Crb			8.3	31.2
1/4			8.5	31.0
Ctr			8.0	31.5 ✓
1/4			7.9	31.6
Crb			7.7	31.8
N			7.4	32.1 ✓

		39.52						39.52			
		1+00						1+50			
N			6.7	32.8 ✓		N			5.4	34.1 ✓	
crb			7.0	32.5		crb			5.3	34.2	
1/4			7.0	32.5		1/4			5.4	34.1	
ctr			7.2	32.3 ✓		ctr			5.9	34.6 ✓	
1/4			7.4	32.1		1/4			6.2	33.3	
crb			7.4	32.1		crb			6.0	33.5	
						+17			6.2	33.3	
S			7.5	32.0 ✓		S			7.6	31.9 ✓	
		1+25						1+75			
S			6.9	32.6 ✓		S			6.7	32.8 ✓	
crb			6.7	32.8		+3'			5.5	34.0	
1/4			6.7	32.8		crb			5.2	34.3	
ctr			6.5	33.0 ✓		1/4			5.2	34.3	
1/4			6.0	33.5		ctr			5.1	34.4 ✓	
crb			5.9	33.6		1/4			4.8	34.7	
N			6.1	33.4 ✓		crb			4.8	34.7	
						N			4.4	35.1 ✓	

		39.52			
		2+0			
N			4.0	35.51	
crb			3.9	35.6	
1/4			4.0	35.5	
ctr			4.1	35.4 ✓	
1/4			4.3	35.2	
crb			4.4	35.1	
S			4.5	35.0 ✓	
		2+25			
S			3.3	36.2 ✓	
crb			3.3	36.2	
1/4			3.2	36.3	
ctr			3.0	36.5 ✓	
1/4			2.8	36.7	
crb			2.6	36.9	
N			2.8	36.7 ✓	
T.P.	12.72	51.01	1.23	38.29	

		51.01			
		2+50			
N			12.7	38.3 ✓	
crb			13.0	38.0	
1/4			13.2	37.8	
ctr			13.3	37.7 ✓	
1/4			13.6	37.4	
crb			13.8	37.2	
S			14.2	36.8 ✓	
		2+75			
S			11.8	39.2 ✓	
crb			11.8	39.2	
1/4			11.7	39.3	
ctr			11.8	39.2 ✓	
1/4			11.4	39.6	
crb			11.3	39.7	
N			10.8	40.2 ✓	

		51.01 3+00			
N			8.8	42,2 ✓	
crb			9.4	41.6	
1/4			9.6	41.4	
ctr			9.5	41,5 ✓	
1/4			9.6	41.4	
Crb			9.8	41.2	
S			10.1	40,9 ✓	
		3+25			
S			8.0	43.0 ✓	
+3			9.1	41.9	
Crb			8.7	42,3	
1/4			8.8	42,2	
Ctr			8.0	43.0 ✓	
1/4			8.0	43.0	
Crb			7.5	43.4	
N			7.4	43,6 ✓	

		51.01 3+50			
N			5,3	45,7 ✓	
+5			6.6	44,4	
Crb			7.1	43,9	
1/4			7.2	43.8	
ctr			7.7	43.3 ✓	
1/4			7.9	43,1	
crb			8.1	42,9	
+16			8.1	42,9	
S			6.3	44,7 ✓	
		3+75			
S			5.1	45,9 ✓	
+4'			6.6	44,4	
Crb			6.7	44,3	
1/4			6.5	44,5	
ctr			6.3	44.7 ✓	
1/4			6.0	45.0	
Crb			5,8	45,2	
+16			5,1	45,9	
N			7.7	48,8 ✓	

		51.01			
		4+00			
N			0.6	50.4 ✓	
+5'			3.4	47.6	
CVL			4.3	46.7	
1/4			4.7	46.3	
CTR			4.9	46.1 ✓	
1/4			4.9	46.1	
CVL			4.9	46.1	
+17			4.7	46.3	
S			1.9	49.1 ✓	
T.P.	12.62	61.19	2.44	48.57	
		4+25			
S			10.2	51.0 ✓	
+3'			13.1	48.1	
CVL			13.3	47.9	
1/4			13.2	48.0	
CTR			13.2	48.0 ✓	
1/4			13.0	48.2	
CVL			12.7	48.5	
+16			12.2	49.0	
N			8.8	52.4 ✓	

		61.19			
		4+50			
N			6.1	55.1 ✓	
+4'			9.8	52.4	
CVL			10.9	50.3	
1/4			10.7	50.5	
CTR			11.1	50.1 ✓	
1/4			11.1	50.1	
CVL			11.6	49.6	
+16			11.2	50.0	
S			8.5	52.7 ✓	
		4+75			
S			6.9	54.3 ✓	
+4'			9.1	52.1	
CVL			9.2	52.0	
1/4			9.1	52.1	
CTL			8.9	52.3 ✓	
1/4			5.5	52.7	
CVL			8.7	52.5	
+15			7.8	53.4	
N			4.1	57.1 ✓	

		61.19		
		5+0		
N			2.0	59.2 ✓
+4'			5.6	55.6
Crk			6.5	54.7
1/4			6.4	54.8
Ctr			6.5	54.7 ✓
1/4			7.1	54.1
Crk			7.1	54.1
+16			7.6	53.6
S			4.5	56.7 ✓
		5+25		
S			2.5	58.7 ✓
+4'			5.0	56.2
Crk			5.3	55.9
1/4			4.7	56.5
Ctr			4.1	57.1 ✓
1/4			3.8	57.4
Crk			3.8	57.4
+16			2.9	58.3
N			+0.4	61.6 ✓
T.P.	12.37	72.34	1.22	59.97

		72.34		
		5+50		
N			8.2	64.1 ✓
+4'			12.0	60.3
Crk			12.7	59.6
1/4			13.0	59.3
Ctr			13.3	59.01
1/4			13.9	58.4
Crk			13.9	58.4
+17			13.7	58.6
S			10.9	61.4 ✓
		5+75		
S			8.7	63.6 ✓
+3'			11.5	60.8
Crk			11.4	60.9
1/4			11.5	60.8
Ctr			11.0	61.3 ✓
1/4			10.7	61.6
Crk			10.7	61.6
+18			9.9	62.4
N			5.8	66.5

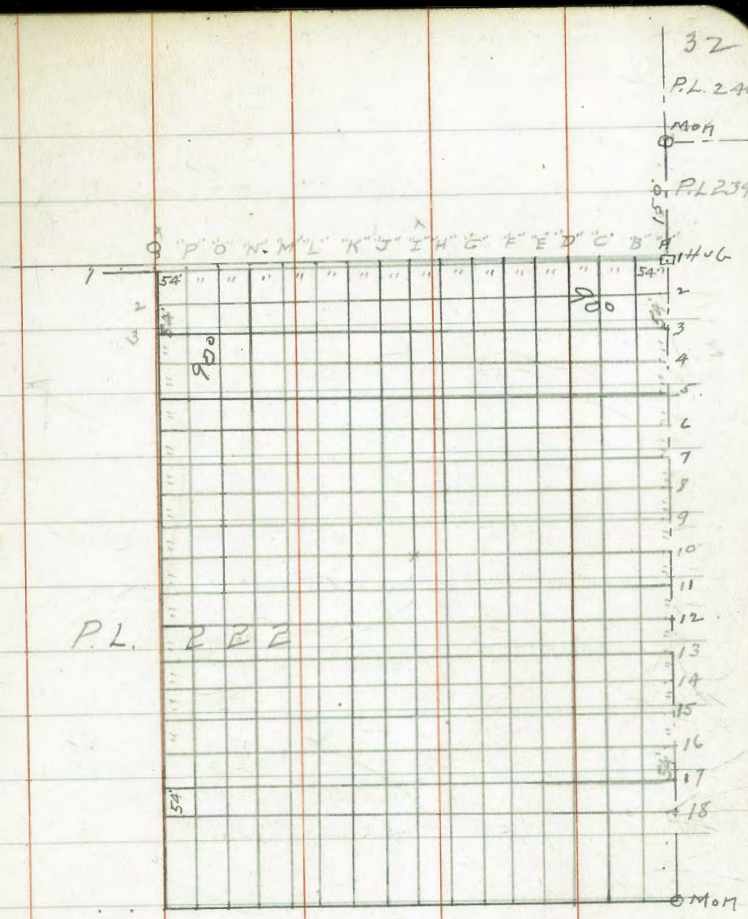
72.34

5+98 = W.L. Ebers 5+

N	3.6	68.7
+2	7.3	65.0
cr &	8.3	64.0
1/4	8.4	63.9
c/l	8.3	64.0
1/4	8.4	63.9
cr &	9.2	63.1
+18	9.4	62.9
S	6.5	65.8
9.74	79.20	2.88	69.46
B.M. N.E. Mrn Orchard & Ebers		5.22	73.98

x-section portion of P.L. 222 12/15/19 Dunkle C. Moore B. Moore

B.M. brass p/g N.W. Cor Rosecrans & Lytton				41.75
	6.60	48.35		
T.P.	12.28	47.81	12.82	35.53
		"Q"		
1			6.9	
2			10.7	
3			13.8	
4			15.8	
T.P.	2.80	37.80	12.81	35.00
5			5.6	
6			6.0	
T.P.	3.25	29.70	11.35	26.45
7			3.3	
8			18.0	
T.P.	2.08	21.63	10.15	19.55
9			2.3	
18' E of 10 = bottom granite p/f			8.7	
13 " " 10 = Top "		"	5.0	
10			4.6	
11			6.4	
T.P.	4.37	16.87	9.13	12.50
12			1.7	
13			1.9	
14			4.9	



		47.81 "P"			
1			7.3		
2			9.3		
3			13.8		
4			18.2		
	2.80	37.80	12.81	35.00	
5			12.6		
6			15.1		
T.P.	3.25	29.70	11.35	26.45	
7			10.5		
8			12.8		
T.P.	2.08	21.63	10.15	19.55	
9			5.0		
+ 9' to granite pit top			4.8		
+ 14" " pit bottom			18.5		
10			19.9		
11 = S.L. granite pit bottom			19.0		
+ 1' " " top,			8.0		
T.P.	4.37	16.87	9.13	12.50	
12			3.3		
13			4.8		
14			8.1		

		47.81 "O"			
1			5.0		
2			5.4		
3			7.4		
4			11.5		
T.P.	2.80	37.80	12.81	35.00	
5			7.4		
6			13.3		
T.P	3.25	29.70	11.35	26.45	
7			11.1		
8			17.7		
	2.08	21.63	10.15	19.55	
9			9.8		
+ 6' to granite pit top			10.1		
+10 " " " bottom			18.8		
10			19.5		
T.P.	4.37	16.87	9.13	12.50	
11 S.L. pit bottom					
" " " top			13.4		
			7.9		
E end of pit 25 E of "O"-11					
12			6.8		
13			9.2		
14			12.8		

		47.81 "N"						47.81 "M"			
1			2.5			1			2.22	45.59	
2			2.3			2			3.3		
3			4.5			3			4.3		
4			7.4			4			6.7		
T.P.	2.80	37.80	12.81	35.00		T.P.	2.80	37.80	12.81	35.00	
5			2.3			5			1.6		
6			8.4			6			8.6		
T.P.	3.25	29.70	11.35	26.45		T.P.	3.25	29.70	11.35	26.45	
7			6.5			7			7.1		
8			16.0			8 = N.L. granite pit top			14.7		
T.P.	2.08	21.63	10.15	19.55		T.P. +10'± "	2.08	21.63	10.15	19.55	
9 = N.L. pit top			16.8			9	"	" bottom	13.4		
+105 = " " " bottom			19.5				~~4.04~~	16.	19.3		
10			19.6			10			19.7		
T.P.	4.37	16.87	9.13	12.5							
11			14.4								
12			14.3								
13			16.1								
14			16.1								

"L"

B.M.	1.55	47.14		45.59	
1			3.1		
2			4.8		
3			6.3		
4			7.5		
5			12.2		
T.P.	1.18	35.77	12.55	34.59	
6			8.4		
T.P.	0.67	23.45	12.99	22.78	
7			2.5		
+35' = N.L. granite Pit top			7.7		
T.P.	1.68	12.49	12.64	10.81	
+38' = " " Pit bottom			7.6		
9			11.3		

"K"

47.14

1			7.2		
2			8.3		
3			9.2		
4			10.9		
5			16.0		
	1.18	35.77	12.55	34.59	
6			11.5		
T.P.	0.67	23.45	12.99	22.78	
7			5.4		
8' = N.L. granite Pit			11.2		
T.P.	1.68	12.49	12.64	10.81	
+05'			10.2		
9			11.4		
S.L. Pit ends 15' E of 9					

		47.14			
		"J"			
1			T.P. 11.11	36.03	Hub
	0.48	36.51			
2			2.9		
3			3.1		
4			5.7		
5			10.0		
T.P.	1.76	25.51	12.76	23.75	
6			3.8		
7			10.3		
	1.18	13.64	13.05	12.46	
8			6.1		
9			12.7		
10			12.1		
		"H"			
B.M.	0.34	36.37		36.03	
1			9.3		
T.P.	1.89	26.20	12.06	24.31	
2			0.9		
3			3.5		
4			5.7		
5			8.4		
T.P.	2.05	15.31	12.94	13.26	
6			0.4		
7			4.4		
8			10.6		
9			15.3		

		"I"			
		36.51			
1			5.1		
2			7.3		
3			9.3		
4			10.5		
5			14.1		
T.P.	1.76	25.51	12.76	23.75	
6			7.0		
7			12.0		
T.P.	1.18	13.64	13.05	12.46	
8			7.5		
9			13.3		
10			12.2		
		"G"			
B.M.	0.34	36.37		36.03	
1			12.8		
T.P.	1.89	26.20	12.06	24.31	
2			4.1		
3			6.5		
4			9.5		
5			12.8		
T.P.	2.05	15.31	12.94	13.26	
6			6.3		
7			10.1		
8			14.6		
9			14.8		

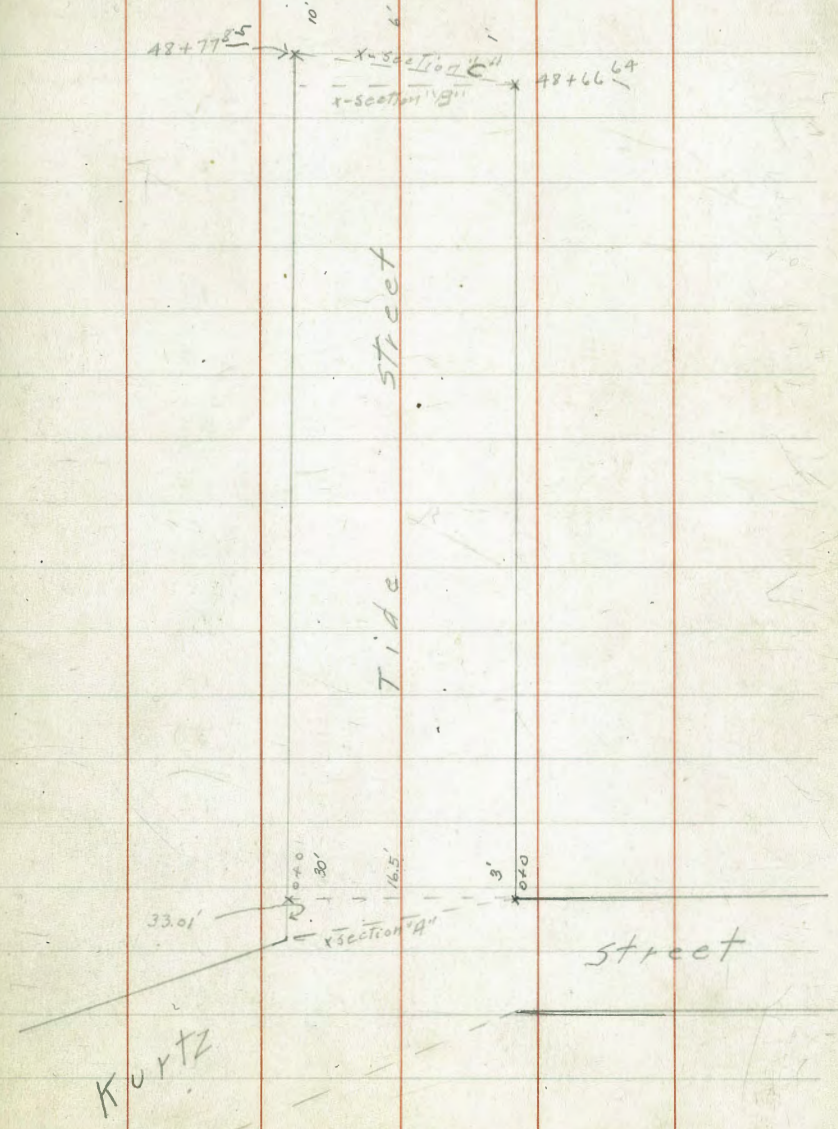
B.M.	1.18	25.49		24.31				25.49		
		"F"						"E"		
									6.02	B.M. 19.47
1			4.4			1			6.7	
2			6.5			2			8.4	
3			8.7			3			10.9	
4			12.2			4			14.9	
T.P.	1.26	14.26	12.49	13.00		T.P.	1.26	14.26	12.49	13.00
5			6.4			5			9.6	
6			10.7			6			13.9	
7			13.8							
B.M.	1.08	20.55		19.47		B.M.	1.08	20.55		19.47
		"D"						"C"		
1			3.2			1			4.84	15.71
2			5.5			2			7.3	
3			7.7			+27			8.5	
T.P.	2.24	10.35	12.44	8.11		3			12.4	
						T.P.	2.24	10.35	12.44	8.11
4			5.2			+27			6.3	
5			7.9			4			7.9	
6			10.3			5			10.3	

B.M.	0.16	15.87		15.71	
		"B"			
1			2.8		
2			7.5		
+27			11.9		
3			13.3		
4			14.9		
		"A"			
1			7.7		
2			13.6		
3			15.00		

x-section Tide St 14 sdwks 13 1/4's St 80' wide

11/16/19 Dunkle
C. Moore
B. Moore

B.M. curb stk Cor	4.47	Kurtz & Tide 5.90	1.43	
		x-Section A		
Sou			4.4	15
crb			5.3	06
11A			4.3	16
crb			4.2	17
11A			4.6	13
+11			5.4	05
crb			4.7	17
N			4.6	13
		0+0		
N			4.6	13
crb			4.7	17
+7			5.4	05
11A			4.5	14
crb			4.3	16
11A			5.0	09
+10			5.5	04
crb			4.8	11
S			4.7	17



		5.90						5.90				
		1+0						3+0				
S			5.3	0.6		S			5.6	0.3		
crk			5.5	0.4		crk			5.3	0.6		
+3			6.2	-0.3		+3			6.2	-0.3		
1/4			5.1	0.8		1/4			5.7	0.2		
c/r			4.6	1.3		c/r			4.8	1.1		
1/4			4.8	1.1		1/4			5.3	0.6		
+11			5.6	0.3		+11			6.0	-0.1		
crk			5.2	0.7		+11			5.0	0.9		
N			4.9	1.0		crk			5.0	0.9		
						N			4.9	1.0		
		2+0						4+0				
N			4.9	1.0		N			5.4	0.5		
crk			4.9	1.0		crk			5.4	0.5		
+2			5.6	0.3		+2			6.2	-0.3		
1/4			4.8	1.1		+2			6.2	-0.3		
c/r			4.6	1.3		1/4			5.5	0.4		
1/4			5.4	0.5		c/r			5.0	0.9		
+10			5.6	0.3		1/4			5.9	0.0		
crk			4.9	1.0		+10			6.2	-0.3		
S			5.1	0.8		+10			5.4	0.5		
						crk			5.4	0.5		
						S			5.5	0.4		
						T.P.	4.76	4.84	5.32	0.58		

		4.84			
		5+0			
S			5.1	-0.3	
+5			4.4	0.4	
Crb			4.3	0.5	
+3			5.4	-0.6	
+3			5.4	-0.6	
1/4			5.0	-0.2	
Ctr			4.1	0.7	
1/4			4.6	0.2	
+11			5.1	-0.3	
+11			4.5	0.3	
Crb			4.5	0.3	
N			4.5	0.3	
		6+0			
N			4.4	0.4	
Crb			4.4	0.4	
+1			5.0	-0.2	
1/4			4.5	0.3	
Ctr			4.3	0.5	
1/4			5.0	-0.2	
+10			5.6	-0.8	
+10			4.6	0.2	
Crb			4.6	0.2	
S			4.7	-0.1	

		4.84			
		7+0			
S			4.8	0.0	
Crb			4.7	0.1	
+4			4.7	0.1	
+5			5.6	-0.8	
1/4			5.1	-0.3	
Ctr			4.5	0.3	
1/4			4.7	0.1	
+12			5.1	-0.3	
Crb			4.5	0.3	
N			4.7	0.1	
		8+0			
N			4.6	0.2	
Crb			4.5	0.3	
+1			5.0	-0.2	
1/4			4.6	0.2	
Ctr			4.5	0.3	
1/4			5.1	-0.3	
+8			5.5	-0.7	
+9			4.7	0.1	
Crb			4.6	0.2	
S			4.5	0.3	

		4.84			
		9+0			
S			4.7	0.1	
crk			4.1	0.7	
+4			5.0	-0.2	
+5			5.4	-0.6	
1/4			5.1	-0.3	
ctr			4.5	0.3	
1/4			4.7	0.1	
+12			5.1	-0.3	
crk			4.4	0.4	
N			4.9	-0.1	
T.P.	4.47	4.96	4.35	0.49	
		10+0			
N			5.3	-0.3	
crk			5.0	00	
+1			5.6	-0.6	
1/4			4.9	0.1	
ctr			4.4	0.6	
1/4			5.3	-0.3	
+9			5.6	-0.6	
+10			4.7	0.3	
crk			4.7	0.3	
S			5.0	0.0	

		4.96			
		11+0			
S			4.7	0.3	
crk			4.4	0.6	
+3			4.7	0.3	
+4			5.3	-0.3	
1/4			5.0	00	
ctr			4.2	0.8	
1/4			4.8	0.2	
+11			5.5	-0.5	
+12			4.8	0.2	
crk			4.8	0.2	
N			4.9	0.1	
		12+0			
N			5.0	00	
crk			4.4	0.6	
+2			4.4	0.6	
+2			5.3	-0.3	
1/4			4.6	0.4	
ctr			4.0	1.0	
1/4			4.9	01	
+10			5.3	-0.3	
+11			4.3	0.7	
crk			4.3	0.7	
S			4.8	0.2	
T.P	5.89	6.00	4.85	0.11	on x-sec splinter

		6.00			
		13+0			
S			5.4	0.6	
Crk			5.2	0.8	
+2			5.2	0.8	
+2			6.2	-0.2	
1/4			5.8	0.2	
CTr			5.0	1.0	
1/4			5.4	0.6	
+11			6.2	-0.2	
+11			5.5	0.5	
Crk			5.5	0.5	
N			5.8	0.2	
		14+0			
N			5.5	0.5	
Crk			5.3	0.7	
+2			5.3	0.7	
+2			6.1	-0.1	
1/4			5.2	0.8	
CTr			4.7	1.3	
1/4			5.4	0.6	
+11			5.8	0.2	
+11			5.1	0.9	
Crk			5.1	0.9	
S			5.2	0.8	

		6.00			
		15+0			
S			5.2	0.8	
Crk			4.6	1.4	
+2			4.6	1.4	
+2			5.8	0.2	
1/4			5.2	0.8	
CTr			4.5	1.5	
1/4			5.2	0.8	
+11			5.8	0.2	
+11			5.2	0.8	
Crk			5.0	1.0	
N			5.1	0.9	
		16+0			
N			4.8	1.2	
Crk			4.9	1.1	
+2			5.0	1.0	
+2			5.8	0.2	
1/4			5.1	0.9	
CTr			4.5	1.5	
1/4			5.1	0.9	
+2			5.6	0.4	
+2			4.9	1.1	
Crk			4.9	1.1	
S			5.1	0.9	

		6.00			
		17+0			
S			5.2	0.8	
crb			4.9	1.1	
+2			4.9	1.1	
+2			5.6	0.4	
¼			4.8	1.2	
ctr			4.4	1.6	
¼			5.1	0.9	
+11			5.5	0.5	
+11			4.8	1.2	
crb			4.7	1.3	
N			4.9	1.1	
		18+0			
N			5.3	0.7	
crb			5.3	0.7	
+2			5.4	0.6	
+2			6.3	−0.3	
¼			5.2	0.8	
ctr			4.6	1.4	
¼			5.2	0.8	
+11			5.9	0.1	
+11			5.0	1.0	
crb			5.0	1.0	
S			5.4	0.6	
T.P.	4.82	5.57	5.25	0.75	

5.57

Note— readings from N.L. to S.L. changed here account reading Sta 18+0 Twice

	19+0		
N		4.8	0.8
crb		4.6	1.0
+2		4.6	1.0
+2		5.4	0.2
¼		4.9	0.7
ctr		4.3	1.3
¼		4.9	0.7
+11		5.6	0.0
+11		5.0	0.6
crb		4.8	0.8
S		5.4	0.2

		5.57			
		20+0			
S			5.1	0.5	
CVL			4.9	0.7	
+3			5.0	0.6	
+3			5.6	00	
1/4			4.9	0.7	
CTR			4.4	1.2	
1/4			5.0	0.6	
+11			5.6	00	
+11			5.0	0.6	
CVL			5.0	0.6	
N			5.0	0.6	
		21+0			
N			5.0	0.6	
CVL			5.4	0.4	
1/4			5.2	0.4	
CTR			4.7	0.9	
1/4			5.3	0.3	
+10			5.7	-0.1	
+10			4.8	0.8	
CVL			4.8	0.8	
S			5.0	0.6	

		5.57			
		22+0			
S			5.1	0.5	
CVL			5.1	0.6	
+3			5.3	0.3	
+3			6.0	-0.4	
1/4			5.5	0.1	
CTR			4.9	0.7	
1/4			5.2	0.4	
+1			5.7	-0.1	
+11			5.2	0.4	
CVL			5.2	0.4	
N.			4.7	0.9	
		23+0			
N			5.1	0.5	
CVL			5.1	0.5	
+2			5.1	0.5	
+2			5.8	-0.2	
1/4			5.5	0.1	
CTR			5.2	0.4	
1/4			5.6	00	
+9			6.2	-0.6	
+9			5.3	0.3	
CVL			5.1	0.5	
S			5.5	0.1	

		5.57			
		24+0			
S			5.2	0.4	
crb			5.4	0.2	
+ 4			5.5	0.1	
+ 4			6.2	- 0.6	
1/4			6.1	-0.5	
ctr			5.3	0.3	
1/4			5.5	0.1	
+ 11			5.9	-0.3	
+ 11			5.3	0.3	
Crb			5.3	0.3	
N			5.3	0.3	
T.P.	6.34	6.65	5.26	0.31	
		25+0			
N			5.9	0.8	
Crb			6.2	0.5	
+ 2			6.2	0.5	
+ 2			7.1	- 0.4	
1/4			6.5	0.2	
ctr			6.3	0.4	
1/4			6.7	0.0	
+ 8			7.2	- 0.5	
+ 8			6.7	0.0	
Crb			6.7	0.0	
S			6.4	0.3	

		6.65			
		26+0			
S			6.5	0.2	
Crb			6.3	0.4	
+5			6.3	0.4	
+5			7.3	- 0.6	
1/4			6.7	0.0	
ctr			6.1	0.6	
1/4			6.6	0.1	
+11			6.8	- 0.1	
+11			6.0	0.7	
Crb			5.9	0.8	
N			6.1	0.6	
		27+0			
N			6.2	0.5	
Crb			6.0	0.7	
+2			6.0	0.7	
+2			6.9	- 0.2	
1/4			6.5	0.2	
ctr			6.0	0.7	
1/4			6.6	0.1	
+8			6.6	0.1	
+8			5.7	1.0	
Crb			5.5	1.2	
S			5.6	1.1	

		6.65					6.65				
		28+0					30+0				
S			5.0	1.7		S			4.5	2.2	
crk			5.1	1.6		crk			4.5	2.2	
+3			5.1	1.6		+2			4.7	2.0	
+3			6.6	1.1		+3			6.6	0.1	
1/4			6.4	1.3		1/4			6.0	0.7	
ctr			5.8	0.9		ctr			5.5	1.2	
1/4			6.4	0.3		1/4			6.2	0.5	
+11			6.7	0.0		+11			6.6	0.1	
+11			5.8	0.9		+12			5.9	0.8	
crk			5.8	0.9		crk			5.9	0.8	
N			6.6	0.1		N			6.3	0.1	
		29+0					31+0				
N			6.2	0.5		N			6.2	0.5	
crk			5.9	0.8		crk			5.8	0.9	
+2			5.9	0.8		+2			5.9	0.8	
+3			6.7	0.0		+3			6.6	0.1	
1/4			6.1	0.6		1/4			5.8	0.9	
ctr			5.7	1.0		ctr			5.3	1.4	
1/4			6.3	0.4		1/4			6.2	0.5	
+10			6.5	0.2		+10			6.3	0.4	
+11			4.7	2.0		+11			4.3	2.4	
crk			4.7	2.0		crk			4.3	2.4	
S			4.7	2.0		S			4.4	2.3	
						T.P.	5.17	7.40	4.42	2.23	

	7.40		
	32+0		
S		4.8	2.6
crb		4.9	2.5
+3		7.1	0.3
1/4		6.6	0.8
ctr		6.0	1.4
1/4		6.6	0.8
+11		7.2	0.2
+12		6.5	0.9
crb		* 6.4	1.0
N		7.1	0.3
	33+0		
N		6.6	0.8
crb		6.5	0.9
+1		6.6	0.8
+2		7.3	0.1
1/4		6.4	1.0
ctr		5.8	1.6
1/4		6.5	0.9
+10		7.0	0.4
crb		5.1	2.3
S		5.0	2.4

	7.4		
	34+0		
S		4.5	2.9
+7		5.8	1.6
crb		6.2	1.2
+3		6.7	0.7
1/4		6.3	1.1
ctr		5.6	1.8
1/4		6.3	1.1
+11		6.9	0.5
+12		6.3	1.1
crb		6.2	1.2
N		6.7	0.7
	34+05		
N		6.6	0.8
crb		6.2	1.2
+1		6.2	1.2
+2		6.9	0.5
1/4		6.3	1.1
ctr		5.6	1.8
1/4		6.3	1.1
+10		6.8	0.6
crb		6.1	1.3
S		6.0	1.4

		7.40					7.40				
		35+0					37+00				
S			5.4	2.0		S			5.7	1.7	
+3			5.8	1.6							
CrL			6.1	1.3		+3			6.5	0.9	
+3			6.4	1.0		CrL			5.8	1.6	
1/4			6.1	1.3		+3			6.6	0.8	
Ctr			5.6	1.8		1/4			6.4	1.0	
1/4			6.1	1.3		Ctr			5.9	1.5	
+11			6.4	1.0							
+11			5.9	1.5		1/4			6.5	0.9	
						+11			6.9	0.5	
CrL			5.9	1.5		+12			6.1	1.3	
N			6.3	1.1		CrL			6.0	1.4	
		36+0				N			6.5	0.9	
N			6.4	1.0		T.P.	4.41	5.91	5.90	1.50	
CrL			6.0	1.4				38+0			
+1			6.0	1.4							
+2			6.6	0.8		N			5.1	0.8	
1/4			6.2	1.2		CrL			4.9	1.0	
						+1			4.9	1.0	
Ctr			5.7	1.7		+2			5.6	0.3	
1/4			6.3	1.1		1/4			5.1	0.8	
+10			6.5	0.9							
+11			5.6	1.8		Ctr			4.6	1.3	
CrL			5.6	1.8		1/4			5.3	0.6	
						+10			5.6	0.3	
+11			6.2	1.2		+11			4.8	1.1	
						CrL			4.7	1.2	
S			5.2	2.2		+12			5.2	0.7	
						S			4.7	1.2	

		5.91			
		39+0			
5			4.0	1.9	
+2			4.9	1.0	
crb			5.0	0.9	
+2			5.1	0.8	
+3			5.8	0.1	
1/4			5.4	0.5	
ctr			4.9	1.0	
1/4			5.3	0.6	
+11			5.8	0.1	
+12			5.1	0.8	
crb			5.0	0.9	
N			5.2	0.7	
		40+0			
N			5.2	0.7	
crb			5.3	0.6	
+1			5.3	0.6	
+2			6.1	-0.2	
1/4			5.5	0.4	
ctr			5.0	0.9	
1/4			5.5	0.4	
+10			5.8	0.1	
+11			5.0	0.9	
crb			4.9	1.0	
+11			5.1	0.8	
5			4.3	1.6	

		5.91			
		41+0			
5			4.9	1.0	
+2			5.5	0.4	
crb			5.1	0.8	
+2			5.2	0.7	
+3			5.9	0.0	
1/4			5.7	0.2	
ctr			5.2	0.7	
1/4			5.7	0.2	
+11			6.0	-0.1	
+12			5.3	0.6	
crb			5.3	0.6	
N			5.7	0.2	
		42+0			
N			5.7	0.2	
crb			5.8	0.1	
+1			5.8	0.1	
+1			6.3	-0.4	
1/4			5.7	0.2	
ctr			5.4	0.5	
1/4			5.9	0.0	
+10			6.1	-0.2	
+11			5.3	0.6	
crb			5.2	0.7	
+11			5.6	0.3	
5			4.2	1.7	
T.P.	3.73	5.69	3.95	1.96	

		5.69			
		43+0			
S			4.0	1.7	
+3			5.5	0.2	
CrLn			5.2	0.5	
+3			5.2	0.5	
+3			5.9	-0.2	
1/4			5.6	0.1	
Ctr			5.3	0.4	
1/4			5.5	0.2	
+11			6.2	-0.5	
+11			5.3	0.4	
CrLn			5.3	0.4	
N			5.4	0.3	
		44+0			
N			5.4	0.3	
CrLn			5.0	0.7	
+3			5.0	0.7	
+3			5.5	0.2	
1/4			5.2	0.5	
Ctr			5.1	0.6	
1/4			5.4	0.3	
+9			6.0	-0.3	
+9			5.0	0.7	
CrLn			5.0	0.7	
+11			5.3	0.4	
S			4.4	1.3	

		5.69			
		45+0			
S			5.0	0.7	
+3			5.3	0.4	
CrLn			4.8	0.9	
+3			4.9	0.8	
+4			5.8	-0.1	
1/4			5.2	0.5	
Ctr			4.8	0.9	
1/4			4.8	0.9	
+11			5.1	0.6	
+11			4.7	1.0	
CrLn			4.7	1.0	
N			5.2	0.5	
		46+0			
N			5.5	0.2	
CrLn			4.7	1.0	
+1			5.2	0.5	
1/4			4.5	1.2	
Ctr			4.5	1.2	
1/4			5.0	0.7	
+10			5.5	0.2	
+11			4.7	1.0	
CrLn			4.7	1.0	
S			5.2	0.5	

5.69

47+00

5	4.7	1.0
crl	4.5	1.2
+2	4.5	1.2
+2	5.4	0.3
1/4	4.9	0.8
ctr	4.2	1.5
1/4	4.5	1.2
+10	5.1	0.6
+11	4.4	1.3
crl	4.3	1.3
+12	4.8	0.9
N	5.4	0.3

48+00

N	4.6	1.1
crl	4.1	1.6
+2	4.1	1.6
+3	4.8	0.9
1/4	4.3	1.4
ctr	4.0	1.7
1/4	4.5	1.2
+11	4.9	0.8
+12	4.3	1.4
crl	4.3	1.4
5	4.4	1.3

48+66.64 – x-section "B"

5	4.0	1.7
crl	4.2	1.5
+3	4.6	1.1
1/4	3.8	1.9
ctr	3.9	1.8
1/4	4.2	1.5
+11	4.5	1.2
+12	3.8	1.9
crl	3.8	1.9
N	4.1	1.6

x-section "C"

N	4.1	1.6
crl	3.8	1.9
+4	4.4	1.3
1/4	4.3	1.4
ctr	3.8	1.9
1/4	4.1	1.6
+12	4.4	1.3
crl	4.0	1.7
+10	4.2	1.5
5	6.0	-0.3

12/17/19 Dunkle
C. Moore
B. Moore

	West curb	gutter	Center	gutter	E. curb
0+0 = St. National	3.50	2.50	3.75	3.00	4.00
+50	3.25	2.25	3.45	2.67	3.67
1+0	3.00	2.00	3.16	2.33	3.83
+50	2.75	1.75	2.87	2.00	3.00
2+0	2.50	1.50	2.58	1.67	2.67
+50	2.25	1.25	2.29	1.33	2.33
3+0 = N.L. Newton	2.00	1.00	2.00	1.00	2.00

Cut & fill for gutters & Center

53

3.80 B.M. brass plg N. Cor 16th & National

3.73
7.53 H.I.

7.53
4.24 National
3.29 west curb

7.53
3.93
3.60 center pavement

7.53
3.66
3.87 E. curb - National

7.53
5.71
1.8 = curb

E 0+50	W 1+0	E 1+50	W 2+0	E 2+50	W 3+0 = N.L. Newton
7.53	7.53	7.53	7.53	7.53	7.53
4.43	4.89	4.86	6.27	4.76	5.12
3.10	2.64	2.67	1.26	2.57	2.41
2.67	2.00	2.00	1.50	1.33	1.00
+0.43	+0.64	+0.67	-0.24	+1.24	+1.41
7.53	7.53	7.53	7.53	7.53	7.53
4.37	5.15	5.66	5.07	6.05	5.07
3.16	2.38	1.87	2.46	1.78	2.46
2.25	2.33	1.75	1.67	1.25	1.00
+0.91	+0.05	+0.12	+0.79	+0.23	+1.46
W	E	W	E	W	E

4/10/00 Gregori Moore Miller Shaw

CROSS SECTION OF Alley BLK 2 Cullen's Arlington Heights 20' wide

on B.M.	4.21	279.47		276.96	BP SW 32nd & Grape
		So. Cb line Grape St.			
E.			3.97		on cement
W			4.40		" "
		S.L. Grape.			
W			3.1		
C			3.4		
E			3.2		
		8' S.			
E			1.6		
C			4.4		
W			4.4		
		25.0' So			
W			4.1		
C			4.2		
E			1.9		
		55' S.			
E			4.6		
C			4.9		

W			3.0		22' wide cement apt. gar.
		100' S.			
W			4.0		
C			3.7		
E			3.7		Apt.
		140' S.			
E			4.5		
C			3.0		
W			5.7		
		182' S.			
W			7.9		
C			7.1		
E			6.6		
		200' S.			
E			7.4		
C			8.4		
W			10.4		
		435' S.			
W			15.5		
C			14.4		

		279.47			
E			10.1		
T.P.	0.30	266.98	12.79	266.68	
		270° S.			
E			3.3		
C			7.7		
W			7.5		
		295° S			
W			6.8		
C			11.4		
E			9.7		
		320° S			
E			13.7		
C			11.1		
W			6.3		
		337° S			
W			6.1		
C			11.1		
E			14.2		

		366.6	S = N.L. Fir St.		
E			15.8		
C			12.9		
W			8.3		

7/19/21 Moore, Miller, Shaw

Cross Section of 20' Alley
24th to 25th
betw. Broadway & E sts.

				BP SW 25th & D st
	4.65	191.67	187.02	
		W.L. 25th - 0+00		
N		5.51	86.2	
S		5.70	86.0	
		WL 25th 0+00		
N		4.5	87.2	
+5		5.2	86.5	
C		5.3	86.4	
S		5.2	86.5	
		0+12		
S		3.7	88.0	
C		4.2	87.5	
+3		4.1	87.6	
+8		1.8	189.9	
N		0.1	191.6	
		0+35		
N		0.4	191.3	
+3		1.9	189.8	
C		2.5	189.2	

Elv. cement alley return 9.7 from center

" " " " 10.3 " "

Cement Block Wall Elv. foot of wall 10.0 from ctr

" " " " " " " 10.7 " "

Wall ends at 0+30

		191.67			
S			1.8	89.9	Fence 10.7 from ctr
		0+56			
S			1.4	90.3	" 10.6 " "
C			1.27	90.4	Elv Sewer M.H.
N.			1.0	90.7	
		0+90			
N			1.7	90.0	
C			1.7	90.0	
+8			1.64	90.1	12' cement apron 8' from ctr
S			1.46	90.2	Elv cement floor
		1+00			
S			2.1	89.6	Fence 9.9 from ctr
C			2.1	89.6	
N			1.8	89.9	
		1+40			
N			2.8	88.9	
C			2.8	88.9	
S			2.6	89.1	Fence 9.8 from ctr
T.P.	1.95	190.80	2.87	188.85	

		190.80					
		1+51					
S			2.1	88.7	8' Garage door	Dirt floor	10.8 from ctr
C			2.3	88.5			
N			2.0	88.8			
		2+05					
N			3.1	87.7			
C			3.4	87.4			
S			3.6	87.2	8' Garage door	same elv cement floor	13.7 from ctr
		2+50					
S			4.3	86.5	Fence 9.9 from ctr		
C			4.1	86.7			
N			3.8	87.0			
		2+75					
N			4.2	86.6			
C			4.7	86.1			
S			4.6	86.2	" 9.9 "	"	
		3+10					
S			5.2	85.6			
C			5.2	85.6			
N			4.8	86.0	9.9 from ctr to 8' apron 5.5 back to Garage cement floor		

		190.80							
		3+57							
N			6.1	84.7		14' Garage door	cement floor	11.1	from ctr
Floor Elv			5.9	84.9					
C			6.4	84.4					
S			6.2	84.6					
		4+00							
S			7.7	83.1		Fence	103	from ctr	
C			7.9	82.9					
N			7.3	83.5					
		4+50							
N			9.6	81.2					
C			9.7	81.1					
+2			10.0	80.8					
S			9.5	81.3		"	99	"	"
		4+75							
S			10.2	80.6		"	10.0	"	"
+1			10.1	80.7					
C			10.9	79.9					
N			10.5	80.3					

		190.80								
		5+00								
N			11.2	79.6						
+6			11.8	79.0						
C			11.3	79.5						
S			11.0	79.8						
		5+25								
S										
			12.5	78.3						
+6			12.8	78.0						
N			12.3	78.5						
T.P.	5.19	183.57	12.42	178.38						
		5+34								
N			5.6	78.0						
+5			6.0	77.6						
C			5.5	78.1						
S			4.7	78.9						
Floor Elv.			3.76	79.8		8' Barn door		wooden floor		10.0 from ctr
		5+50								
S			6.1	77.5		End of cement wall				10' from ctr
C			6.4	77.2						

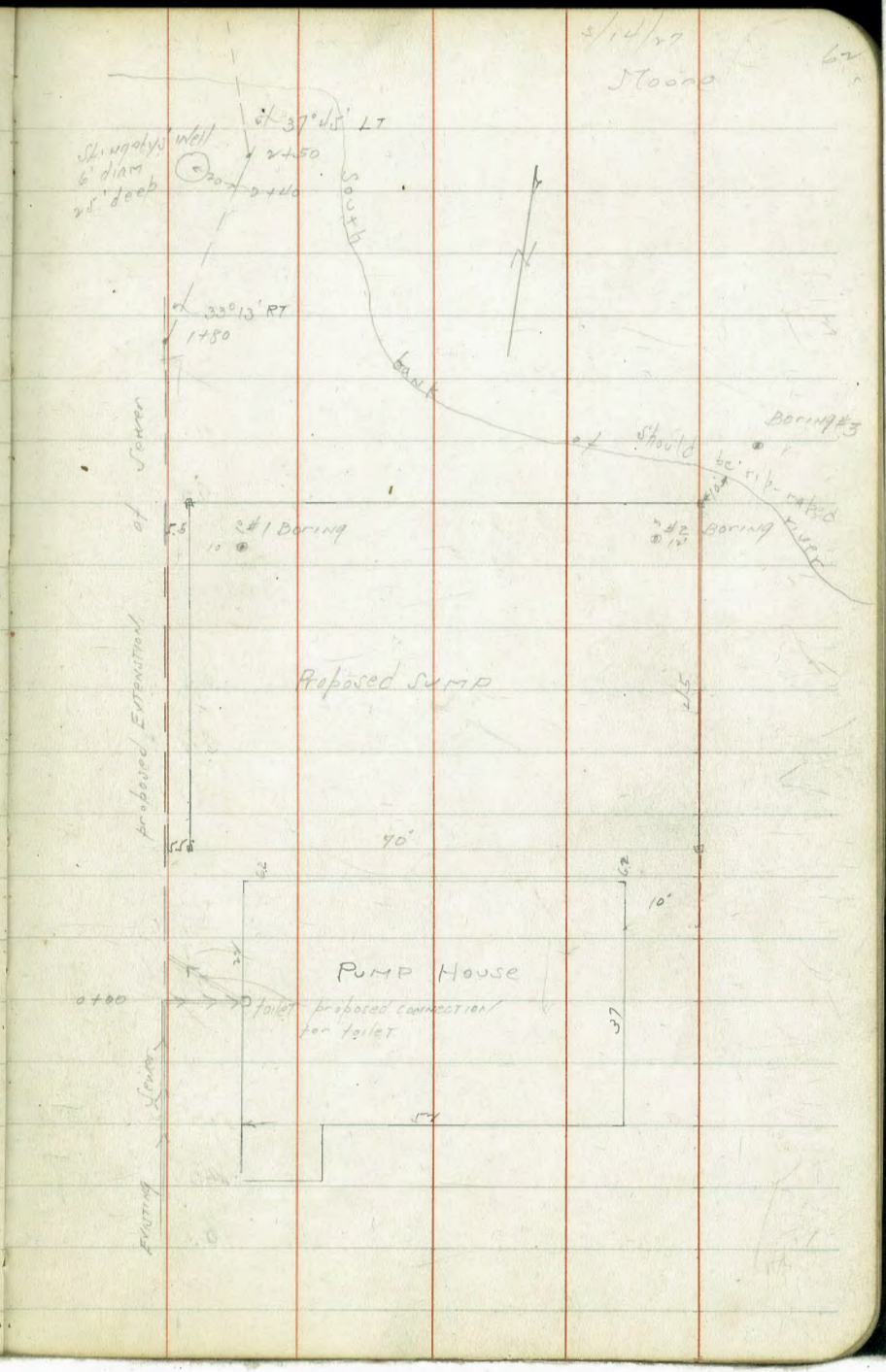
		183.57			
+1			6.8	76.8	
N			6.2	77.4	
		5+75			
N			7.3	76.3	
+3			7.5	76.1	
+5			8.5	75.1	
C			8.4	75.2	
S			7.8	75.8	Cement Wall 10.0 from ctr
		5+97			
S			9.0	74.6	" " " " "
C			9.8	73.8	
+3			9.8	73.8	
N			8.2	75.4	
		6+00.80 = Elv 24th			
N			9.4	74.2	
+7			10.0	73.6	
C			9.9	73.7	
S			10.3	73.3	Cement Wall 10.0 from ctr also Elv of sidewalk Elv
			9.63	173.94	B.P SW 24th & Dst BM 173.96

Levels for proposed Sump
at Mission Valley Pump Station
at City Line

Top retaining Wall South of Pump Plant	0.00	53.45		53.45	B.P. Eq.
T.P.	1.97	49.03	6.39	47.06	Floor of Pump House

El. Sump = Baseline

S		3.3	45.7
E		4.5	44.5
N		6.0	43.0
10' W			
N		7.5	41.5
C		5.4	43.6
S		2.9	46.1
20' W			
S		2.8	46.2
C		4.5	44.5
N		7.6	41.4
30' W			
N		7.5	41.5
C		5.1	43.9
S		2.8	46.2



		49.03					
40' W							
S			2.7	46.3			
C			4.8	44.2			
N			7.4	41.6			
50' W							
N			7.2	41.8			
C			4.8	44.2			
S			2.8	46.2			
60' W							
S			2.7	46.3			
C			5.0	44.0			
N			7.2	41.8			
70' W =							
N			7.0	42.0			
C			4.8	44.2			
T.P	4.09	47.30	5.8 W	43.21			
S			1.7	45.6			
approx. High water mark this year			2.4	44.9			
" " " " 1916			1.0	46.0			

Levels for proposed Sewer
Mission Valley Pump Plant

63

47.30 T

Flowline existing Sewer = 0.0	0.30	47.00	
0+50	3.6	43.7	
1	6.0	41.3	
+50	6.3	41.0	
1+50 = Δ 33°.3' RT	6.7	40.6	
2	6.9	40.4	
+40	7.7	39.6	
20' West of 2+40 = Shingoby's Well	6.0	41.3	on ground
2+50 = Δ 37°.5' LT	7.9	39.4	
2+66 = S edge river	11.7	35.6	Elev. of river water
+68	15.2	32.1	stream bed
River approx 150 wide			
Test Boring elev. 47.30 T			
#1 hole	12.0	35.3	= clay silt
#2 "	14.5	32.8	= Clay silt
#3 " 15' NE. of NE cor sump	15.0	32.3	= river sand

Levels in Pump House

	S.11	Sv.17	4706	at doorway Elev. Floor
Floor elev. 47	top of wall or pit	S.06	47.11	
elev of bottom of well or pit		N.05	31.12	
" " flowline of 30" Conc. pipe		17.19	34.98	

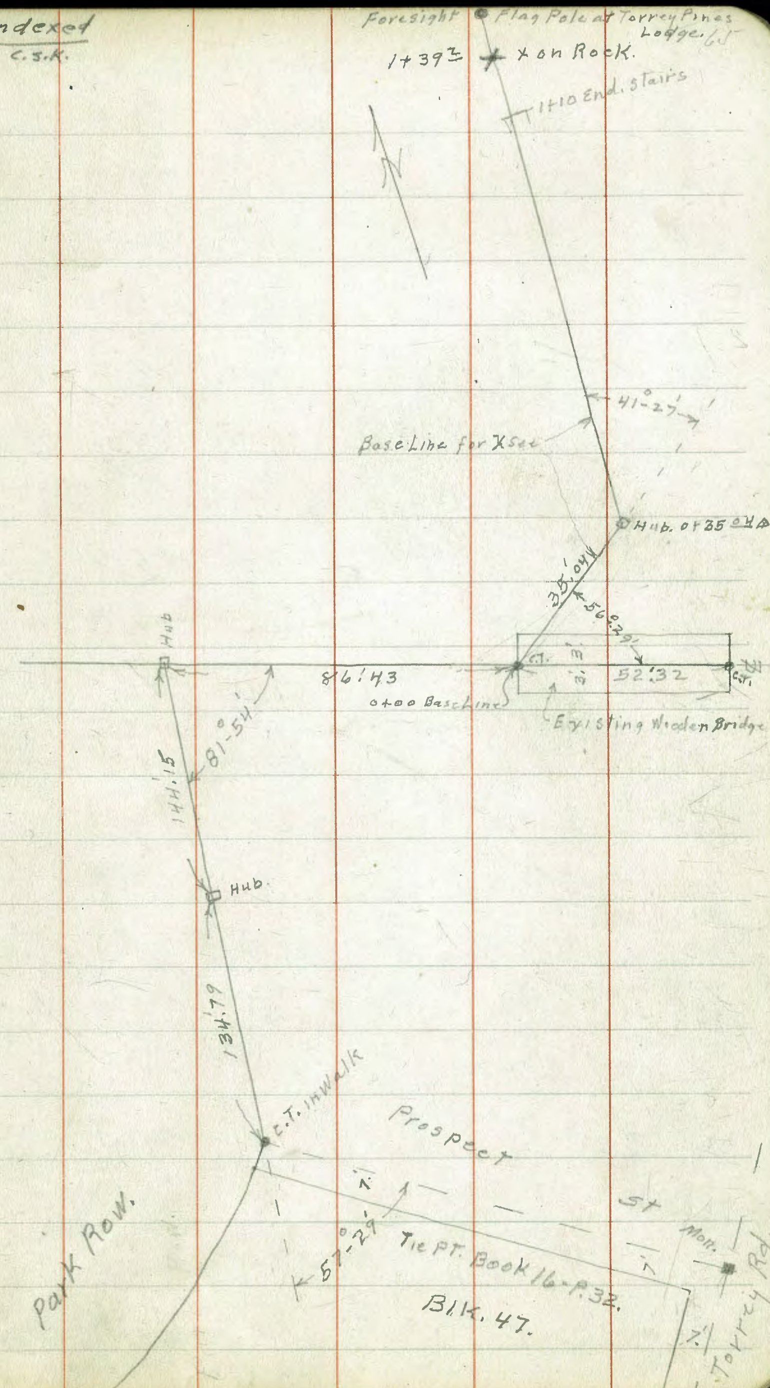
Clark says 12" pipe has been abandoned

Levels for Stairs at Devils Slide
At Termination of Park Row. LaJolla.

1-12-34
Miller
Walker
Bliss
sly cor. Park Row & Prospect.

B.M. B.P.	2.38	134.46		132.08	
T.P.	1.03	122.89	12.60	121.86	
T.P.	0.19	110.17	12.91	109.98	
T.P.	0.77	98.30	12.64	97.53	
T.P.	0.67	86.30	12.67	85.63	
0+00 - 10 on projection of B.L.					
20'. Lt			4.4	81.9	
16' "			6.6	79.7	
9			7.1	79.2	
B.L.			9.9	76.4	
10'. Rt.			12.3	74.0	
0+00 - C.T.					
10'. Rt.			16.2	70.1	
B.L. on C.T. end Bridge			10.09	76.21	
8'. Lt			9.5	76.8	
10 "			7.0	79.3	
20' "			6.3	80.0	
0+05					
20' Lt			7.8	78.5	
17' "			13.7	72.6	

indexed
C.S.K.



		86.30		
		0+05 (con)		
15 Lt			6.9	79.4
6 "			10.6	75.7
B.L			11.7	74.6
7' Rt			13.2	73.1
10' "			18.0	68.3
T.P	1.96	75.46	12.80	73.50
		0+20		
10' Rt			9.1	66.4
4			5.2	70.3
B.L.			4.6	70.9
5'3 Rt = Top. Existing Wood stairs			5.2	70.3
7' Lt.			5.1	70.4
10' "			3.3	72.2
20' "			9.4	67.1
23 "			8.0	67.5
26 "			5.5	70.0
		0+28		
28' Lt			10.4	65.1
20' "			10.7	64.8
14' "			14.7	60.8
5' "			9.5	66.0

		75.46		
B.L.			6.7	68.8
4' Rt.			8.8	66.7
10' "			15.0	60.5
		0+35.24 Δ 41°27' Lt. on split		
10' Rt			17.8	57.7
5' "			15.0	60.5
B.L. on Hub			11.39	64.07
4 Lt			12.1	63.4
13' Lt.			14.6	60.9
T.P.	4.55	68.62	11.39	64.07
		0+43		
25' Lt			3.8	64.8
20' "			3.3	65.3
11 "			10.0	58.6
8' "			11.2	57.4
B.L.			12.0	56.6
70' Rt.			16.0	52.6
		0+45		
4.7 Lt on Landing			12.0	56.6

		68.62			
		0+54			
25 Lt			4.0	64.6	
13' "			12.2	56.4	
5' "			15.0	53.6	
3' "			22.4	46.2	
B.L.			26.0	42.6	
7' Rt.			25.5	43.1	
		0+62			
12 Rt	In wash		36.5	32.1	
8 Rt.	edge "		36.0	32.6	
B.L.			26.0	42.6	
5 Lt			23.0	45.6	
16 "			15.7	52.9	
25' "			7.0	61.6	
H.L. T.P.	0.0	55.6	13.0	55.6	
H.L. T.P.	0.2	42.8	13.0	42.6	
0+66 - 4'	Rt. of B.L. =	on woodstake			on Platform
		0+72			
9' Lt			1.2	41.6	
4' "			7.5	35.3	
B L			7.3	35.5	
3' Rt			8.1	34.7	

		42.8			
9' Rt			20.8	22.0	
15' "			21.0	21.8	
		0+80			
13 Rt			21.0	21.8	
18' "			11.5	31.3	
B.L.			14.0	28.8	
6' Lt			9.7	33.1	
10' Lt			7.5	35.3	
H.L.T.P.	0.2	30.2	12.8	30.0	
		0+90			
10' Lt			3.9	26.3	
B.L.			8.9	21.3	
4' Rt			9.6	20.6	
6' Rt			6.8	23.4	
10' Rt			7.6	22.6	
H.L.T.P.	0.3	17.5	13.0	17.2	
13 Rt			12.9	4.6	
10'			1.9	15.6	
B.L			4.5	13.0	
5' Lt			2.5	13.0	
10' "			3.0	14.5	

		T 17.5			
H.L.T.P.	2.1	T 7.6	12.0	5.5	
		1+08			
35' Lt	Base cliff to W.		3.0	4.6	
13' Lt			1.8	5.8	
10' Lt	on Beach		3.8	3.8	
B.L.	" "		3.3	4.3	
10' Rt.	" "		4.0	3.6	
16' Rt.	on Beach In Wash from S.		3.5	4.1	
23' Rt	on Beach. Base cliff to E.		2.7	4.9	
		1+10.4			
1'.0 Rt. of B.L. = End. Existing stairs on N. end Platform.					
11'.0 Lt. = End of Existing Ramp.					
		1+15			
20 Rt	on Beach		4.2	3.4	
B.L.	" "		5.4	2.2	
35' Lt	" "		6.9	0.7	
		1+39½			
35' Lt			10.0	-2.4	
B.L.	X on Rock.		9.2	-1.6 = -1.8	computed from 0+35 ±4 Δ
20' Rt			7.8	-0.2	

H.I. 68.62
Vert ∠ = -34°-03'
Hor Dist. 104.12
Diff. Elev. 70.4

3/21/34.

LA JOLLA PATHS.
(Devils slide.)

			Construction Notes.	Grade	Gr. Rod.
B.M.				76.21	
A 0+35	9.90	73.97		64.07	64.07
0+00					75.67
					9.4
0+7.5					
0+11.5					
0+24		✓	7.75	66.22	66.27 7.70
T.P	3.06	69.00	8.03	65.94	8.73
0+28					
0+38			10.30	58.70	57.54
T.P			9.11	59.89	Root
0+40.5					Sta 0+38
Check			5.00	64.00	
B.M # 2	12.70	73.88		61.18	
B.M. # 1	3.50	73.94		70.44	

3/24/34 — LA JOLLA PATHS — COAST WALK (Devils Slide) — W.M. McCarty, H.M. Huntington, J.E. Engert

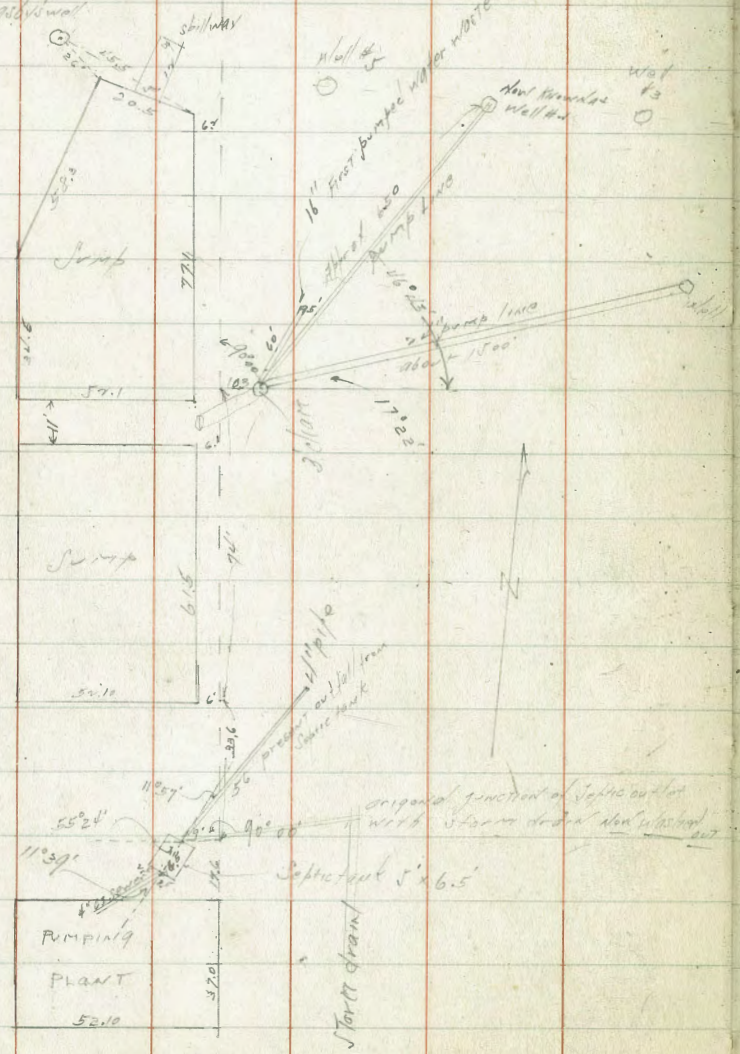
STA.	+	H.I.	−	Elev.	Grade	Gr. Rod.	C & F			
End of Bridge.										
B.M.	0.40			76.21						
		76.61								
Pier.										
0+7.5	1st.		1.00							
Pier	Plat.									
0+11.5			1.02	75.59	75.59					
16.5										
0+18.1			5.81	70.80	70.91		F 0.11			
0+24	2nd		10.50	66.11	66.22					
TACK	Plat									
0+28			10.55	66.06	66.22					
T.P., STAKE 4 R STA 0+33 +0.31		64.52	12.40	64.21						
Pier										
0+32.8 Edge Concrete			2.00	62.52						
0+38 Slab	3rd		5.88	58.64	58.72					
A Point										
0+40.5 Slab.	Plat		5.88		58.72		F 0.80	= 1"		
B.M. Roof			4.64	59.88	Check					
0+43.0 Slab			5.88	58.64	58.72		1.24	59.88	48.07	
T.P.	2.20	55.61		T.P.						
0+50.1			11.11	53.41	53.41	11.11				
0+57.2			7.50	48.11	48.09	7.52	1.24	51.65	1.18	42.84
T.P.	1.99	39.64	17.96	37.65						
0+61.2	44				48.09					
114					10.63					
0+					42.78					
0+75.4	5+1		1.50	38.14	37.46	2.18	C 0.7			
0+79.4			2.67	36.97	37.46	0.51	F 0.5			
0+										

Left. ∠ 37°-13' at last point

Sta	+	H.I	−	Elev	Grade		
0+86.5		39.64	6.60	33.04	32.64		C 0.4
0+93.6	T.P. 0.91	28.13	12.42	27.22	26.83	F 1.30	on nail E 0.40
0+97.6	6th ∠ pt 37°13' L.		1.60	26.53	26.83		
1+04.7			5.75	22.38	21.51		C. 0.90
1+11.8	7th		11.48	16.65	16.20	F 1.93	C. 0.45
1+15.8	T.P. 1.81	18.24	11.70	16.43	16.20		C. 0.23
1+22.9			6.85	11.39	10.88		C. 0.5
1+30.0	T.P. 0.48	6.52	12.20	6.04	5.57	0.95	
B.M. on rock near bank 50' right 1+05				1.47	5.10	B.M.	
			8.24	-1.72		X	
	0.37	60.26		59.89			
3rd Plat.			1.63	58.63	58.72		
			6.84	53.42			
			12.10	48.16			
Foot. 4th Plat.	+1.0 T.P.	49.19	12.17	48.09	48.09	Grade.	
Top up-side Left pier. Break			7.26	41.93	42.78	F 0.85	
Bottom. Break.	T.P. 1.34	39.00	11.53	37.66	37.46	C 0.20	
Break.			1.33	37.67			
			6.12	32.88			
			11.92	27.08	26.83	C. 0.25	C 3"
Break	.1.13	28.24	11.99	27.01			

		H.I 28-24										
			6.42	21.82	21.51	C O 31						
T.P	0.96	17.55	11.65	16.59	1620	C.O.39						
			6.33	14.22	10.88	CO. 34						
			11.62	5.93	5.57	CO. 36						
			12.11	5.44	Error 34	B.M.						
	-1.05	4.05		5.10								
	Ver ∠ 21-35'		0.5' Interval									
	16°05'		0.75' "									

Location of Septic tank, Sump, pump lines etc at City Pumping Plant in Mission Valley at City Boundary Line



Moore
Walker
aboard

10/31/26

Well #4 Well #2 abandoned

4/24/19 Gregory Miller — Levels to determine elev of High water marks at Old Town Pumping Plant.

on B.M.	1.60	21.28		19.68	B.M. on Concrete Coping of Bridge at Old Town.
T.P.	3.13	16.49	7.92	13.36	
T.P.	2.47	16.58	2.38	14.11	
			3.98	12.60	Elev of Red lead Marked High water on old Reservoir.
T.P.	4.78	16.16	5.20	11.38	
			3.01	13.15	High water mark inside pump house. Marked. High Water Mar 25 1906.
			0.78	15.38	Mark dated 1/27/16 Marked in pencil "High water 1/27/16" inside pump house.

598.4

De Foe

Orchard - S.W. Mon 28.92

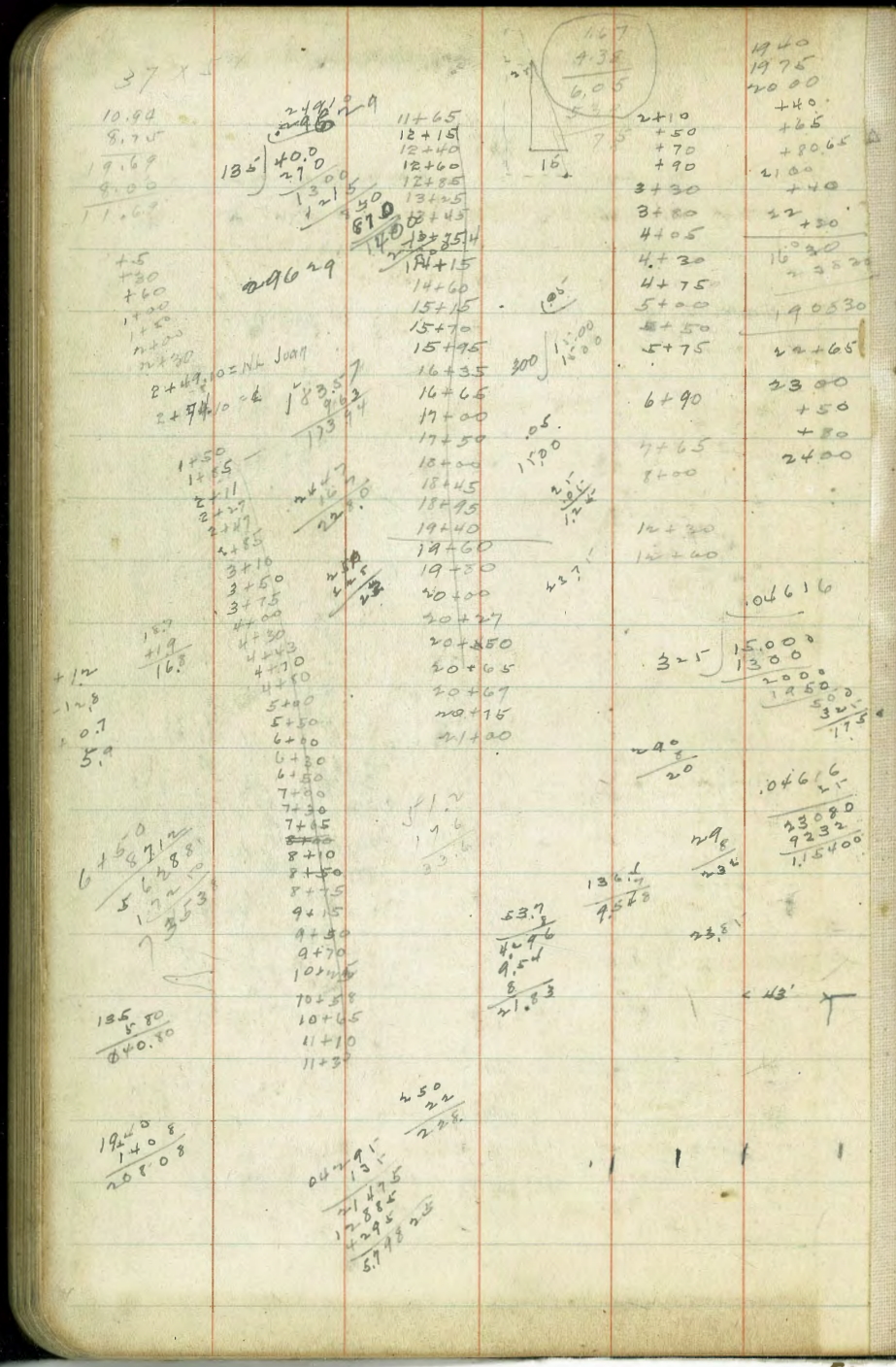
Del Mar N.W. Brass plg curb 36.117

Ebers

Orchard - N.E. Mon 73.98

C. 0.1
1.0

8
55
100
140
182
200
235
270 +
295
320
330
360
390



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18 9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.