

1044

DIETZEN
4



ENGINEERS
FIELD BOOK

No. 403



EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

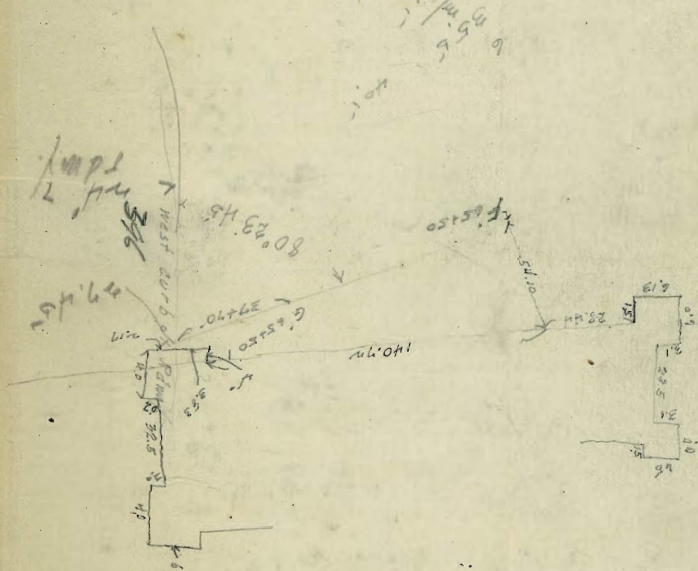
H	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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00029

00010
2000
20000



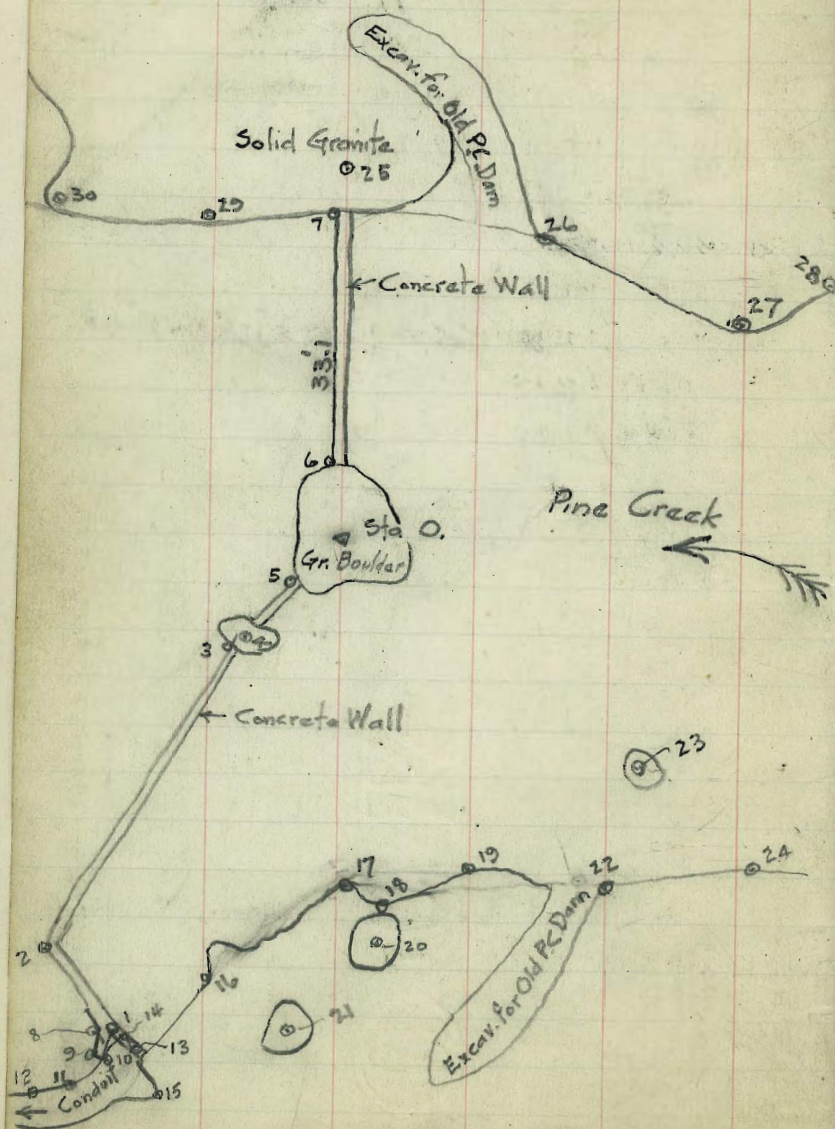
Handwritten notes and calculations, including '22.6', '30.6', and '32.6'.

Page

Survey Old Town Gov. Dilke

21-24

SURVEY OF PINE CREEK INTAKE



Note - See page 3 for details of Intake

Sept 17-1918

{ Lockwood
Cromwell
Jorgensen
Schwartz

— Distances —

Sta 4-5 = 5.0

" 6-7 = 33.1

" 7-13 = 7.85 (Clear opening at intake 6.45)

" 13-14 = 6.45

" 27-28 = 73.2

" 29-30 = 101.0

" 1-2 = 7.45

Note - Conduit has about same direction (11-12) for 80' beyond sta 12.

2.

Sta - Sta	Dist.	Azm.	
OA-1	37.65	164°50'	S 15°10' E
2	31.50	175°00'	S 5°00' E
3	14.37	184°00'	S 4°00' W
4	11.81	184°50'	S 4°50' W
5	6.82	184°50'	S 4°50' W
6	6.86	352°50'	N 7°10' W
7	37.3	304°40'	N 53°20' W
8	37.35	166°25'	S 13°35' E
9	42.31	167°00'	S 13°00' E
10	41.65	161°35'	
11	69.56	173°45'	
12	99.20	182°10'	
13	34.62	153°10'	
14			
15	34.86	145°05'	
16	29.15	153°00'	
17	20.56	128°45'	
18	25.63	124°40'	
19	29.04	98°50'	
20	39.04	110°10'	
21	36.18	130°35'	
22	72.2	74°25'	
23	71.4	44°05'	
24	143.7	46°55'	
25	48.9	302.50	

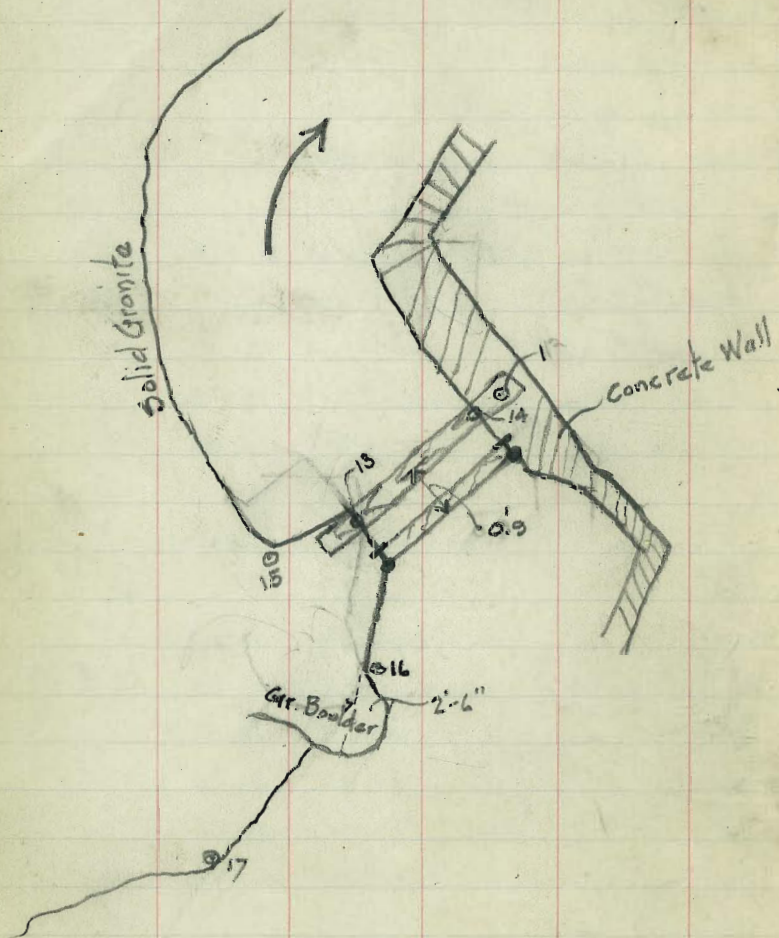
(Cont. on page 4)

Sta. O Δ = Pt. on top large Gr. Boulder

Zero Azm = N. by needle (var = 14°20' E)

1. Cen. Abut. W. Side of Intake Gate (Nail in wooden beam.)
2. Angle in old Intake dam
3. Junct wall & rock
4. Cen sm. gr boulder
5. Junct of wall & large gr. boulder
6. " " " on W. & " " "
7. " " " & Solid rock on W. abut.
8. Angle in E. Abut.
9. E. end of Abut.
10. Junct. Conduit with abut.
11. Pt on W. wall conduit
12. " " " " "
13. Pt. on E. side of Intake at edge of concrete
14. " " W. " " " " " "
15. " on gr. wall E. side of Intake
16. Junct. Conc. with gr rock in place.
17. Gr. bedrock at water surface
18. " " " " "
19. " " " " "
20. Top of Gr. rock in place
21. " " " " "
22. Nail in Gr. rock
23. Gr. Boulder in Gr. bed
24. Gr. rock in place on E. bank of Cr.
25. Pt. on Gr. rock in place on ext. of line of conc. wall

Detail of Intake at Pine Cr.



Sta - Sta	Dist	Azm.
0A - 26	58.37	337°40'
27	70.12	9°40'
28		18°40'
29	55.64	247°30'
30		222°00'

26. Gr. bedrock on N. side of excav. for W. abutment.

27. " " near water surf. on W. bank of Cr.

28. " " " " " " " " " "

29. " " " " " " " " " "

30. " " " " " " " " " "

LEVELS AT PINE CREEK INTAKE

Sta.	+	H.I.	-	Elev
B.M.	4.83	104.83		100.00
1			6.75	98.08
2			8.81	96.02
"			10.55	94.28
3			10.58	94.25
4			7.65	97.18
5			8.12	96.71
Cr bed app.			9.95	94.88
6			10.58	94.25
7			10.73	94.10
Cr bed			10.83	94.0
Bot. Conduit			14.93	89.90
Top W. Wall "			9.15	95.68
" " "			9.30	95.53
Water Level			12.15	92.68
" "			12.42	92.41
Top of W. Wall			8.71	96.12
13			6.69	98.14
15			8.40	96.43
16			6.95	97.88
17			10.15	94.68
18			Same	
19			10.90	94.83
20			(+ 0.20)	105.03

Sept 17, 1918. {Cramwell
Jorgensen}

Top of Gr. Boulder Sta 0. Assumed elev = 100.00

Conc. Abut. opp Sta 2 (top)

" Wall near Sta 2

Top of Conc. wall opp. Sta 3

Top sm. boulder

" Conc. wall opp Sta 5

Cr. bed opp. 2.

Top of conc. wall opp 6

Top of " " " 7

Opp Sta 7 (above & below the same)

Opp. Sta. 12

" " "

" " 11

" " "

100' below Sta. 11.

" " "

Top of Conc.

Junct of Conc. & Bedrock

Top of conc.

Cr. bed

" "

" "

Top Gr. rock

Levels

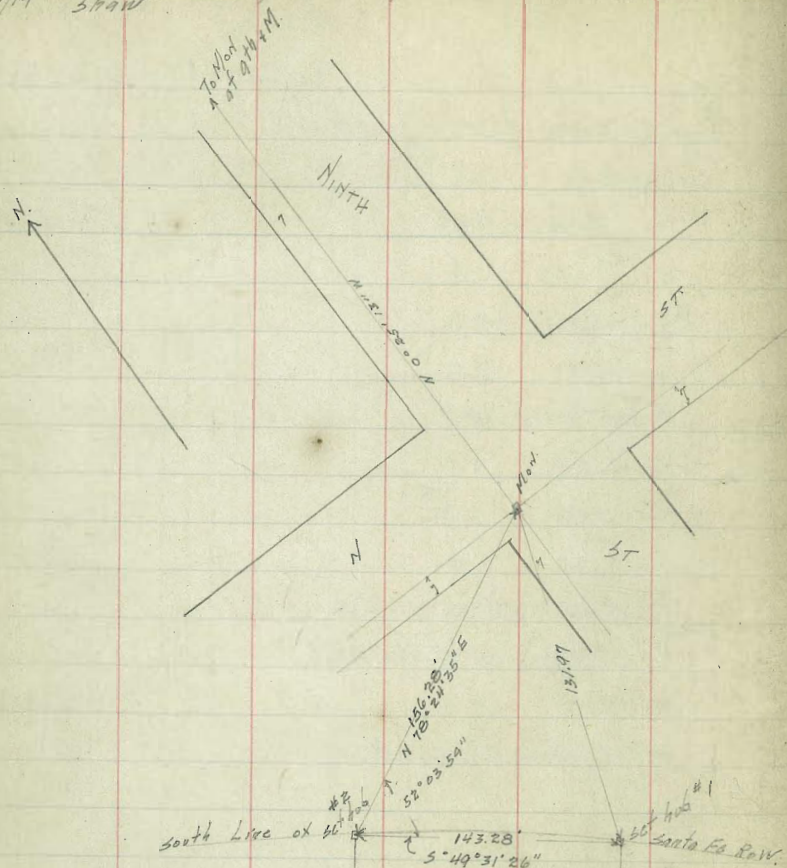
Sta	+	H1	-	Elev.
21		104.83	(+0.7)	105.53
22			7.1	97.7
23			8.9	95.9
24			3.1	101.7
25			4.83	100.00
26			8.7	96.1
27			9.75	95.08
28			9.2	95.6
29			11.2	93.6
30			12.1	92.7
Cr. Bed			10.7	94.1
Floor Intake			11.32	93.51
Water Surf.			10.20	94.63
" "			12.06	92.77

Sept 17-1918, 46.

Top Gr. rock
 Ground
 " stream bed
 "
 Bed rock
 "
 Water Surf.
 Ground
 Cr. bed
 " "
 At Intake upstream side
 Pt. just below intake weir
 At weir
 At beginning of conduit

5/17/19 Gregory Survey at City Incinerator Plant

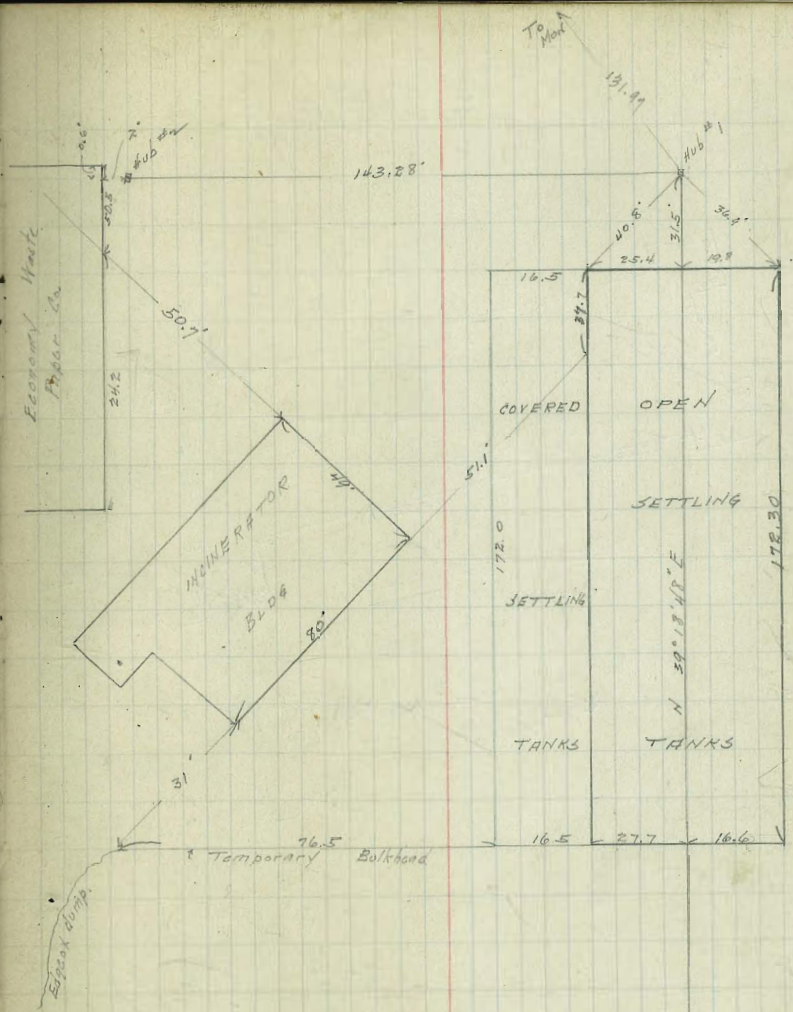
7



FOR Location of
Improvements see next
page.

CITY
INCINERATOR
PLANT

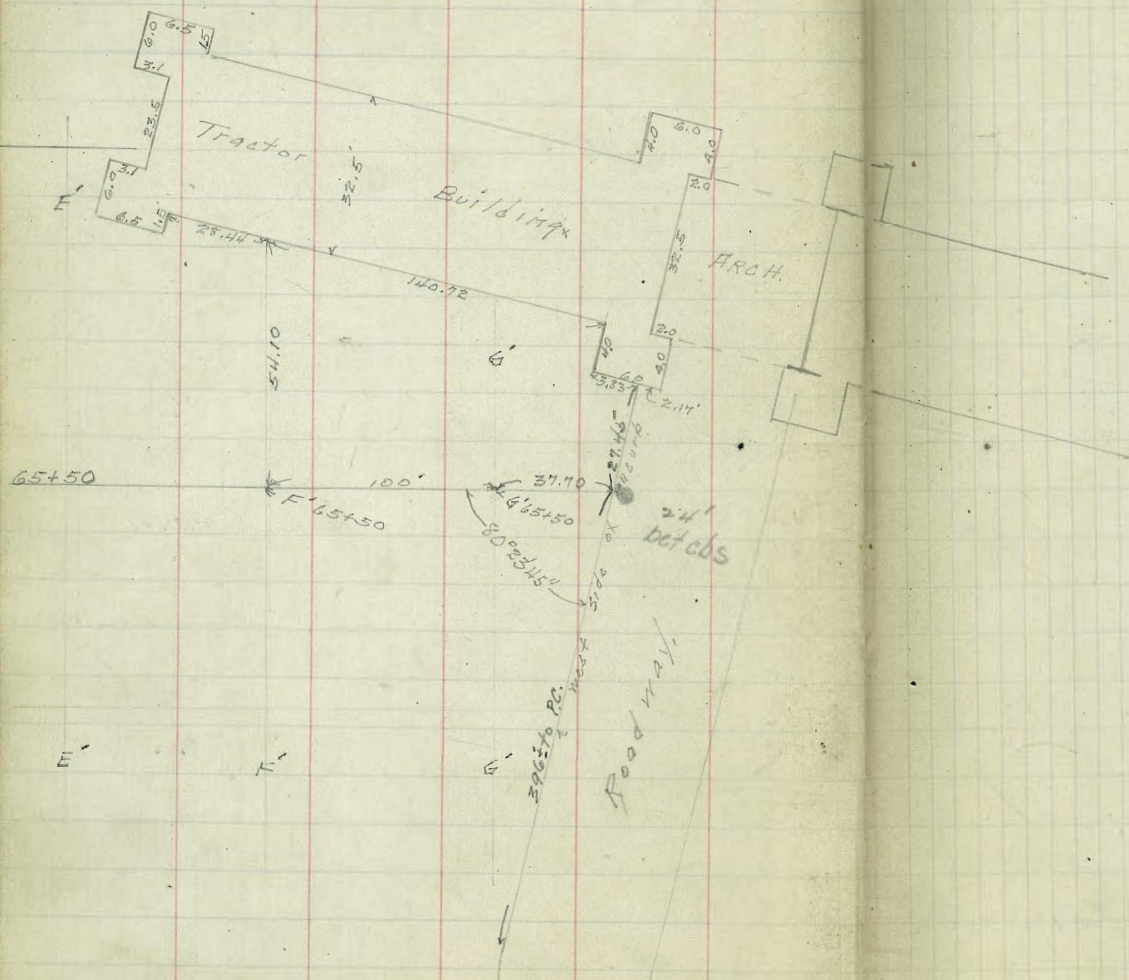
Set stakes of
Copper tanks on
railings over
Gas Co's. settling
Tanks.



Temporary Bulkhead

8/9/19 Gregory
Miller
Shaw

Survey To Locate
Tractor Bldg +
Road at new site
of 100 Balboa PK.



SEE TOPO. MAP OF BALBOA PARK FOR LOCATION
OF LINES E-F-G + STATION 65+50.

11/4/19
 9
 6000
 5000

Cross Section of
 WILLOW STREET
 EL. India to EL. of State

80' wide
 14' 205
 13' 1/2

94.94

9

on B.M. 12.48 82.54 70.06

EL INDIA

N 9.7 72.8

cb 9.6

1/4 9.8

c 9.8 72.7

1/4 9.8

cb 9.1 73.4

S 9.7 72.7

2' E

S 6.7 75.8

H 3.8 78.1

1/4 7.4

c 7.9 74.6

1/4 7.8 74.9

cb 0.4

+7 0.2

N 2.2 80.3

T.P. 12.91 94.94 0.51 82.03

7' E

N 11.4 83.5

cb 11.2

1/4 17.7

c 17.4 77.5

1/4 17.3

cb 140 80.9

S 10.4 84.5

15' E

S 8.6 86.3

cb 11.8 83.1

1/4 12.0

c 10.2 84.5

1/4 10.3

+10 10.1

cb 8.7

N 9.3 85.6

25' E

N 6.2 88.7

+11 5.6

cb 7.1

1/4 7.0

c 7.3 87.6

1/4 7.9

cb 8.1 86.8

+7 7.6 87.5

S 6.0 88.7

T.P. 12.71 107.64 2.01 94.93

50' E

S 11.4 96.2

+5 11.3 96.3

cb 14.1 93.5

		109.64		
9	1/4		13.9	
	c		13.7	93.9
	1/2		12.8	
	cb		12.9	
	+7		12.1	
	N		14.6	95.2
		75'E		
	N		5.4	102.2
	+7		5.5	
	cb		7.2	
	1/2		7.6	
	c		7.0	100.6
	1/4		7.7	
	cb		7.6	100.0
	+3		7.0	100.6
	+8		4.6	103.0
	S		4.9	102.7
+7	T.P.	1286	120.22	0.28
				107.36
		100'E		
T.	S		12.1	108.1
	cb		12.1	108.1
	1/4		11.8	
	c		11.9	108.3
	1/4		11.9	
	cb		12.1	
	+7		11.7	

		120.22	WILLOW	
	N		11.7	108.5
		125'E		
	N		6.0	114.2
	cb		5.6	
	1/4		5.7	
	c		5.3	114.9
	1/4		5.7	
	cb		6.1	114.1
	S		6.7	113.5
		150'E		
	S		1.6	118.6
	cb		0.7	119.5
	1/2		0.5	
	c		0.1	120.1
	1/4		0.1	
	cb		0.3	
	N		0.5	119.7
	T.P.	1298	133.17	0.03
				120.19
		175'E		
	N		8.2	125.0
	cb		7.9	
	1/4		7.9	
	c		8.2	125.0
	1/4		8.5	
	cb		9.4	123.8
	S		10.3	122.9

9
11.

133.17

200' E = N = W.L. Columbia St

75 m. do
12' 0.25

S		5.9	127.3
cb		4.6	128.6
1/4		3.8	129.4
C		3.2	130.0
1/2		3.0	130.2
cb		3.2	130.0
N.		3.4	129.8
N. Cb.			
N.		1.0	132.2
cb		0.6	
1/4		0.8	
C		0.7	132.5
1/4		1.4	
cb		2.4	130.8
S		3.8	129.4
T.P.	122.85	145.36	0.66 132.51
W 1/4			
S		14.1	131.3
cb		12.7	132.7
1/4		11.7	
C		11.1	134.3
1/4		10.6	
cb		10.5	
N		10.7	134.7

WILLOW

11

145.36

Center Columbia

N		8.5	136.9
cb		8.3	
1/4		8.6	
C		8.81	136.55 or Mon.
1/4		9.6	
cb		10.5	134.9
S		12.2	133.2
E. 1/4			
S		10.4	135.0
cb		8.9	136.5
1/4		7.7	
C		7.0	138.4
1/4		6.4	
cb		6.1	
N		6.0	139.4
E. Cb.			
N		4.1	141.3
cb		4.0	
1/4		4.5	
C		4.8	140.6
1/4		5.6	
cb		6.8	138.6
S		8.6	136.8

E.L. Columbia

S		6.9	138.5
cb		5.2	140.2
1/4		3.8	141.6
C		3.0	142.4
1/4		2.3	143.1
cb		2.3	143.1
N		1.9	143.5
T.P.	142.77	158.12	0.01 145.35
		25' E	
N		11.4	146.7
cb		11.7	
1/4		12.1	
C		12.9	145.2
1/4		13.7	
cb		14.7	
S		17.1	141.0
		50' E	
S		15.0	143.1
cb		12.6	
1/4		11.1	
C		10.0	148.1
1/4		8.9	
cb		8.2	
N		7.9	150.2

75' E

N		4.8	153.3
cb		5.4	
1/4		6.1	
C		7.6	150.5
1/4		9.0	
cb		10.9	
S		13.5	144.6

100' E

S		13.3	144.8
cb		9.6	
1/4		7.2	
C		5.4	152.7
1/4		4.6	
cb		2.9	
N		2.5	155.6

125' E

N		0.4	157.2
cb		1.0	
1/4		2.6	
C		4.2	153.9
1/4		6.6	
cb		9.7	
S		14.1	144.0

150' E

S			16.9	141.2
cb			11.5	
1/4			6.8	
C			4.0	154.1
TP	8.28	161.75	46.5	153.17
1/4			5.2	
cb			4.0	
N			2.9	158.9

175' E

N			2.4	159.4
cb			4.3	
1/4			5.8	
C			8.3	153.5
1/4			11.1	
cb			15.9	
S			20.9	140.9

200' E = WL STATE 75' wide 12' obs

S			22.9	138.9
cb		18.0		
1/4			13.7	
C			10.6	151.2
1/4			7.4	
cb			6.3	
N			3.3	158.5

N' cb

N		4.0	157.8
cb		6.4	
1/4		8.7	
C		12.4	149.4
1/4		16.7	
cb		20.6	
S		25.2	136.6

7'E of N' cb

S		26.9	134.9
cb		21.3	
1/4		17.6	
C		13.0	148.8
1/4		9.5	
cb		7.1	
N		4.7	157.1

W 1/4

N		5.5	156.2
cb		7.9	
1/4		10.1	
C		13.9	149.9
1/4		17.9	
cb		21.8	
+3		25.5	
+5		30.0	
S		33.5	128.3

17

161.75

Center

S	36.7	125.1
cb	31.3	
+6	22.8	
1/4	20.1	
C	16.21	145.54 = Nord.
1/4	12.1	
cb	9.9	
N	6.9	154.9
E 1/4		
N	8.8	153.0
cb	11.3	
1/4	14.3	
C	18.5	143.3
+7	21.3	
1/4	29.3	
cb	36.1	
+	40.3	
S	43.2	118.6
E. Cb		
S	42.2	119.6
cb		121.0
1/4		124.6
C		133.9
+2	20.8	
1/4	16.7	
cb	13.3	
N	10.1	151.7

145.54

WILLOW

14

7'E of ECB

So. Cb		121.5
So.		120.0
E. L. STATE		
N		12.3 149.5
T.P.	0.31 149.11	12.95 148.80
cb		2.5
1/4		6.9
T.P.	0.32 136.72	12.71 136.10
+5		128.3
C		126.2
1/4		122.8
cb		121.7
+9		121.2
S		124.3

11/1/19
15 bridge

CROSS SECTION OF
STATE ST. 75' wide 12' db's
from S.L. Willow to S.L. Glanwood Dr
136.72 from last page.
S.L. WILLOW

E				124.3
+5				120.0
cl				119.6
1/4				118.6
C				125.1
1/4				128.3
+5		1.8		134.9
cl		0.1		136.6
W		+2.2		138.9
		25' S.		
W			6.9	
cl			12.2	
T.P.	4.39	131.75	9.36	127.36
1/4			13.3	
+8			16.0	
C			15.8	
1/4			15.2	
+5			11.0	
cl			10.2	
+4			10.0	
E			13.4	
		50' So.		
E			18.0	
cl			13.3	

STATE 103 15

1/4				14.4
+6				16.6
+7				19.0
C				19.1
1/4				19.2
+4				19.3
+7				16.8
cl				14.6
W				8.3
T.P.	1.28	120.14		12.89
			75' So.	118.86
W				6.0
+7				8.0
cl				10.7
1/4				10.8
C				10.4
+2				7.5
1/4				5.9
+6				4.9
cl				7.5
+7				9.8
E				9.1
			100' So.	
E				12.3
+10				12.2
cl				11.2

+8			8.9	
1/4			9.6	
c			11.6	
+3			13.5	
1/4			13.7	
cb.			13.7	
+6			14.3	
+7			12.2	
W			12.0	
T.P.	0.72	109.17	11.69	108.45
		125' So.		
W			4.7	
+7			5.8	
cb			5.4	
1/4			5.1	
+5			5.0	
c			3.3	
1/4			1.4	
+7			2.4	
cb			1.1	
+7			2.4	
F			2.3	
		150' So		
F			+1.5	110.7
cb.			1.6	
1/4			3.8	

c	4.9
1/4	6.6
cb	7.5
+6	8.1
W	7.1

164.89' So. = N.L. Glenwood Drive

W	8.4			
+1	9.9			
cb	7.9			
1/4	6.7			
c	5.2			
1/4	0.8			
T.P.	11.83	120.72	0.28	108.89
cb	8.7			
E	5.9			

20.7' So = Center Glenwood.

E	+1.6	122.3
cb	2.0	
1/4	5.4	
c	9.8	
1/4	13.8	
+4	15.1	
cb	19.9	
W	20.8	
	10.5' So. of Ctr	
W	22.1	

+9

18.4

cb

14.8

10.2 502 S.L. Glenwood Drive

W

17.9

+5

130

cb

86

1/4

56

c

1.8

TP

1237

132.14

0.95

119.77

1/4

97

cb

7.0

E

36

11/4/19
18

X SECTION OF
Columbia Sp 75' Sp
N.L. Willow & SL Chalmers

on BM.	6.39	14294	136.55	Col. Will Mon Ctr
		N.L. Willow		
W			129.8	
cb			132.2	
1/4			134.7	
C			136.9	
1/2			139.4	
cb			141.3	
E			143.5	

		75' No.		
E		0.3	142.6	
cb		2.8		
1/4		4.3		
C		6.1	136.5	
1/2		8.8		
cb		11.3		
W		13.4	129.5	

		75' No.		
W		17.3	125.6	
cb		14.7		
1/4		12.5		
C		10.2	132.7	
1/2		8.2		
cb		6.5		
E		4.5	138.4	

142.94

100' No.

E			7.4	135.5
cb			9.0	
1/4			11.2	
C			12.5	130.4
1/2			15.1	
T.P.	0.23	130.41	12.76	130.18
cb			4.7	
W			6.8	123.6

150' No.

W			12.8	117.6
cb			10.8	
1/4			8.3	
C			7.0	123.4
1/2			5.1	
cb			3.3	
E			2.2	128.2

200' No.

E			9.9	120.5
cb			11.1	
1/4			13.0	
T.P.	0.13	117.57	12.97	117.44
C			1.9	115.6
1/4			3.7	
cb			5.0	
W			6.6	111.0

11757

225' No

W	9.8	107.8
cb	8.4	
1/4	7.1	
C	6.0	111.6
1/4	5.2	
cb	4.4	
E	3.2	114.4

237' No

E	5.6	112.0
cb	6.4	
1/4	6.2	
C	7.6	110.0
1/4	9.1	
cb	11.1	
W	12.8	104.8

255' No

W	20.2	97.4
+7	19.2	
cb	14.9	
1/4	14.1	
C	13.2	104.2
1/4	12.0	
cb	11.7	
E	10.8	8.901
T.P.	0.41	105.21
		17.77
		104.80

COLUMBIA

11707

270' No

105.21

E	3.8	101.4
cb	4.2	
1/4	4.6	
C	6.0	99.2
1/4	6.9	
cb	8.4	
W	10.2	95.0

285' No

W	12.4	92.8
cb	11.0	
1/4	10.0	
C	9.2	96.0
1/4	8.0	
cb	6.5	
E	5.9	199.3

300' No = S.L. Chalmers

E	11.3	93.9
cb	13.1	
T.P.	0.68	92.96
1/4	12.93	92.28
1/4	2.2	90.8
C	2.9	
1/4	0.7	
+5	0.6	
+8	8.3	
cb	9.6	
W	9.9	83.1

T.P.

-0.51

80.61

1286

80.10

350

77.11

77.01

B.P. SW.
Winder
1914

Jan 4-6-1920

Survey of Gov. Dike Near Old Town

8+05 Int of 15' Gov Dike

Δ 37° 19' Lt

3+75 Int of Scott St

0+00 Int of Taylor & Hickory

0+

Williams
Dunkle
Moore
Moore

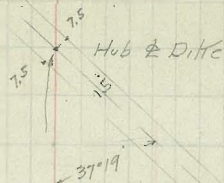
141.96
246.61

37° 19' Lt

375
430
805

21

E DIKE



430

50

Scott

Con. Mon.

50

street

Chestnut

375

Taylor

100

street

ST

Con. Mon.
Smith & Hickory

24

20+49.0

$\Delta 7^{\circ}46'30''$ Lt

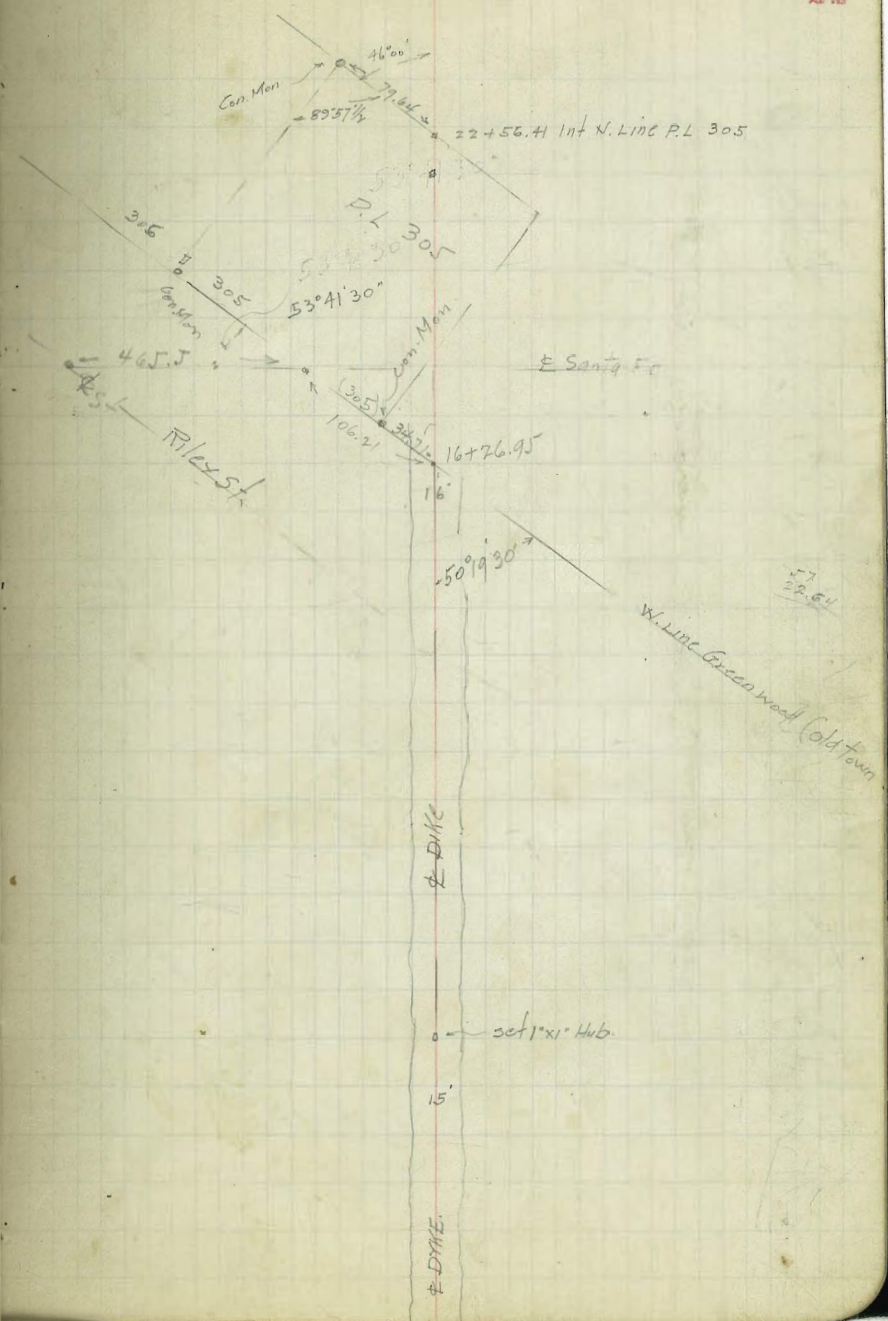
16+26.95 Int N. Line Greenwood 1933 Lt

13+00

$2^{\circ}19'30''$ Lt

22+56.41

22

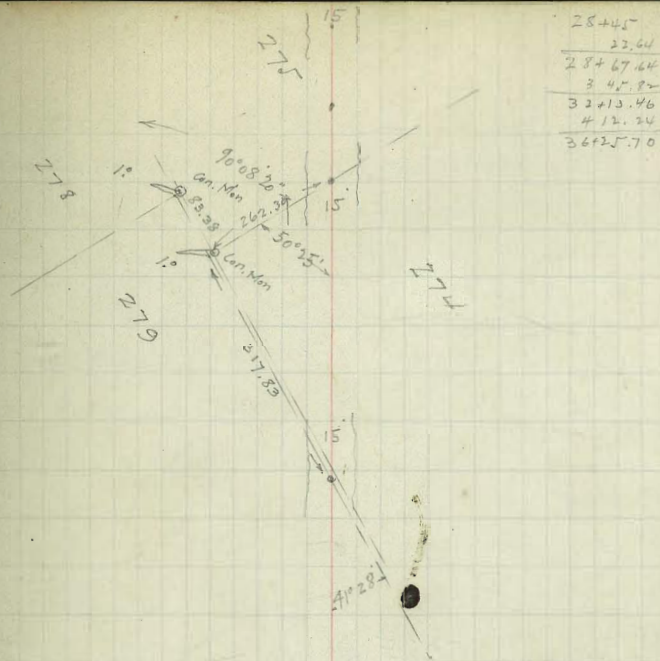


23
 42+25.7 Point in & DIKE
 39+25.9 Point 5' south of & of DIKE
 36+25.7 Int Line between 275-274 $\Delta 2^{\circ}51' Lt$

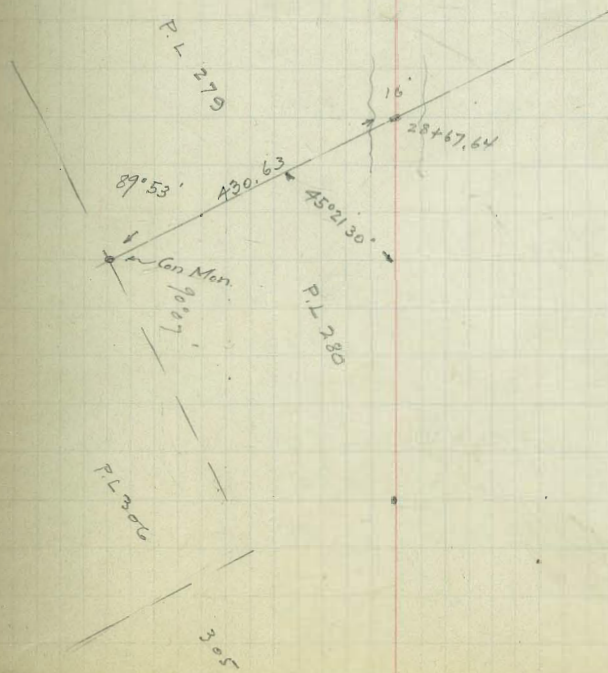
32+13.46 Int. Line 1' south of P.L. line. $\Delta 1^{\circ}45' 30" Lt$

28+67.64 $\Delta 3^{\circ}04' Lt$

23+67.0 $\Delta 1^{\circ}28' 30" Lt$



28+41
 22.64
 28+67.64
 345.82
 32+13.46
 412.24
 36+25.70



Levels of Walnut St
East West of Columbia
for Contours

	122.90	149.45	136.55
	25' E. of Columbia		
N.L. Walnut			2.7
25' N			3.1
50' N			4.6
75' N			7.4
100' N			10.6
3. L. Walnut			8.4
15' S. of -			11.3
25' - - - -			14.7
	50' E. of Columbia		
25' S. of S.L. Walnut			13.3
10' - - - -			8.2
25' N - N.L. -			40.3
50' - - - -			1.5
75' - - - -			4.0
	0.26	136.81	136.55
	E.L. Columbia		
20' S. of S.L. Walnut			1.8
35' - - - -			6.4
	Ctr. of Columbia		
10' - - - -			4.8
35' - - - -			9.3
49' - - - -			12.4

W.L. Columbia

	122.90	149.45	136.55	Mon Ctr Walnut & Col
50' S. of S.L. Walnut				16.9
30' - - - -				13.1
10' - - - -				10.3
	25' W. of Columbia			
25' N. of N.L. of Walnut				12.4
T.P. 2.08	122.48			12.41
				124.40
50' N. of N.L. Walnut				4.0
75' - - - -				5.0
100' - - - -				7.9
25' S. - S.L. -				5.8
50' - - - -				10.2
	50' W. of W.L. Columbia			
50' S. of S.L. Walnut				14.4
25' - - - -				10.5
25' N. - N.L. -				7.8
50' - - - -				9.3
75' - - - -				11.2
T.P. 0.51	115.00			11.99
				114.49
	75' W. of			
25' N. of N.L. Walnut				1.9
50' - - - -				3.5
75' - - - -				5.1
75' S. of S.L. -				12.3
50' - - - -				6.6
25' - - - -				2.9

100' W. of W. L. Columbia

75' N. of N. L. Walnut.	11.4
50' ✓ ✓ ✓ ✓ ✓	9.5
25' ✓ ✓ ✓ ✓ ✓	7.7
25' S. ✓ S. L. ✓	8.4
50' - - - - -	11.1
75' - - - - -	15.9

3/3/20

Measurements of rail
La Jolla Ry Track

26

on C	W.L. of India to 30' E. of W.L. of State double track = 580' =	1160' of Single Tr	on 6 th	N.L. F to 56' S. of K.	
on C	30' W. of E.L. of State to 70' W. of W.L. of 1 st double track = 710' =	1420' Single Tr		Single Tr	2031'
on C	70' of W.L. 1 st to 70' E. of E.L. 3 rd St minus 25' at 3 rd =	755' ✓ ✓ ✓		56' S. of K to L 244' Double =	488' single
	Curves at 4 th + C	88' ✓ ✓ ✓			
	C to Broadway on 4 th				
	300' of Double =	600' ✓ ✓ ✓			
on C	70' E. of E.L. 3 rd St to W.L. of 6 th St Double Tr = 665'	1330' ✓ ✓ ✓			
	curves at 6 th + C 41.7				
	62.7 =	104' ✓ ✓ ✓			
on 6 th	S.L. C St to 83' N. of Broadway Double = 217' =	434' ✓ ✓ ✓			
on 4 th	N.L. Broadway to N.L. F St East Track =	760' ✓ ✓ ✓			
on 6 th	83' N. of Broadway to 10 th N. of F Single Tr	741' ✓ ✓ ✓			
on 6 th	10 th Double Tr to F	204' ✓ ✓ ✓			
	Curves at 6 th + F	114' ✓ ✓ ✓			

Platted J.W. 4/22/20

5/20/00 Gregory Miller Shan

CROSS SECTION OF VERMONT ST 80' wide from S.L. of Lincoln to 160' So. No returns S.L. of Lincoln + VT.

	5.03	497.09	292.06	3pk SW Lincoln + VT.
		S.L. Lincoln		
W		4.5	292.6	
+15		4.5	92.6	
+20		5.1	92.0	
+40		4.7	92.5	
+55		5.1	92.0	
+70		4.2	92.9	
E		4.0	93.1	
		10' S.		
E		88	88.3	
+25		5.5	91.6	
+40		4.7	92.5	
+60		4.5	92.6	
W		4.4	92.7	
		35' S		
W		4.7	92.6	
+40		4.2	92.9	
+50		5.2	91.9	
+65.0		6.0	91.1	
E		7.6	89.5	
		60' S		
E		7.0	90.7	
+15		5.8	91.3	
+35		4.9	92.2	

Platted
5/10/00
Shan

+40	4.3	292.8
W	4.8	92.3
	100' S	
W	5.7	91.4
+40	4.4	92.7
+60	5.6	91.7
E	6.6	90.5
	150' S	
-2.5 = Sewer Pipe.	7.5	89.6
E	5.3	91.8
+20	4.6	92.5
+40	4.8	92.3
+60	6.1	91.0
W	6.0	90.5
	209.5' S. = N. End of Br.	
W	7.6	89.5
+153 = E. of Foot Bridge	8.15	88.94/1000
+40	6.7	90.4
+60	6.2	90.9
E	5.9	91.2
	180' S on E = walk to house	
E	5.45	91.84
	214.5' S = Edge of Canon	
E	6.3	90.8
+40	6.5	90.6
+40	6.9	90.2

297.09

+60 8.5 88 6

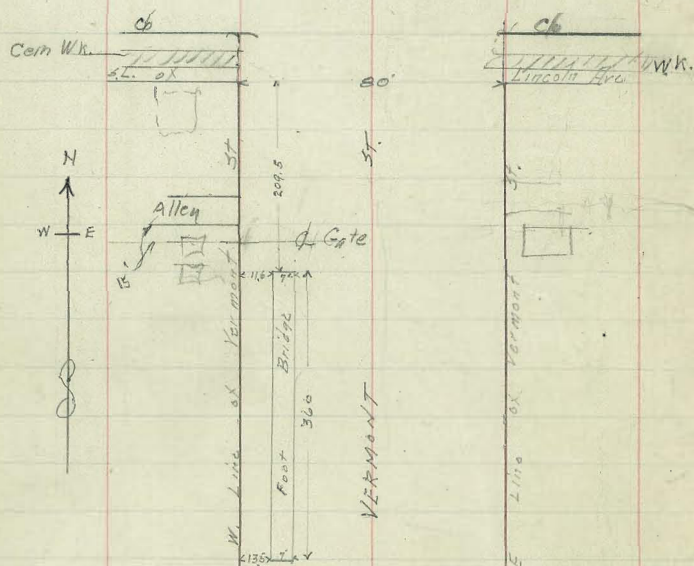
W 7.8 89 3

425' 3

d = Sewer Pipe 8.0 89 1

198' 3 on W Prop Line

W.L. = 4" Sewer Pipe to house 7.2 89.9



28

10/13/20

Gregory
Miller
ShawTraverse on roads west of
High School.

Forest plot on ledge at South chimney - X3

13+49.91 \odot P.O.T.

13+41

762

12+94

12+68 Δ $138^{\circ}52' L$

268

③
10+00 Δ $13^{\circ}02'30'' R$.

300

②
7+00 Δ $21^{\circ}37' R$.

375

①
3+25 Δ $29^{\circ}04' R$.

335

0+00

29

80'

Edge of road

Edge of

strubs

Edge of

road

edge strubs

35'

edge road

17'

10'

edge road

edge strubs

35'

edge road

10'

10'

edge road

Edge strubs

35'

Edge road

11'

10'

edge road

 $83^{\circ}01'50'' \rightarrow$

Tack

25

24

23+65

600

22+00

21+00

③

20+50

△

93°15'30" L

20+38

②

7

18

782

17

16+54 app

①

P.O.T.

①

16

15

14+50



Edge of road

Edge of road

Edge of road

50'

50'

50'

50'

50'

34 + 73.36 = 107.36

289.18

31 + 93.18 Δ 88° 56' 30" L

545.18

27 + 100

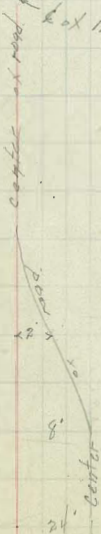
26 + 50 Δ 50° 41' L

26 + 100

600

2.0 x Twelfth St.

2.0 x 11th St + 52.0 x Park



10/13/20
Gregory Miller
Shaw

Traverse around Proposed
High School Site at
N. End Balboa Park

21+00 Δ 65°53' L

19+00 Δ 51°46'30" L

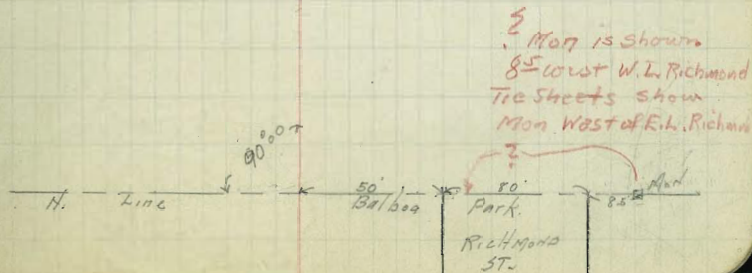
15+95 Δ 60°55'30" R

14+15 Δ 76°15'30" R

13+45 Δ 37°13' R

9+50 Δ 137°46' L

0+00 hds.



$$48+30.64 = 0+00$$

$$38+4.12 \triangle 91^{\circ}17'30''L$$

$$37+6.5 \triangle 36^{\circ}03'30''L$$

$$33+00 \triangle 35^{\circ}10' R.$$

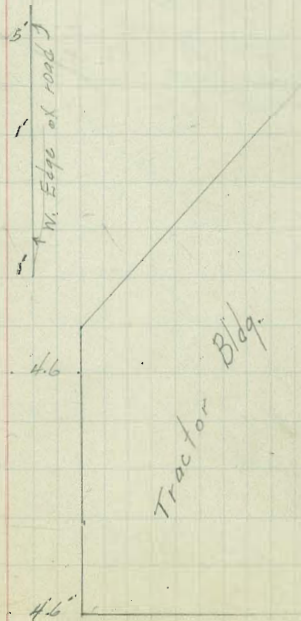
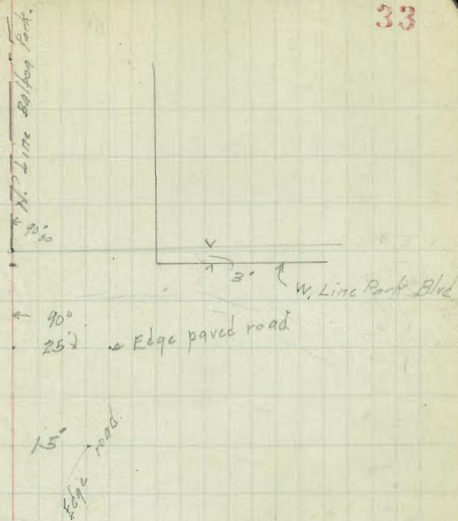
30+50

$$29+50 \triangle 6^{\circ}46'30''L$$

$$24+39 \triangle 90^{\circ}07' L$$

22+60

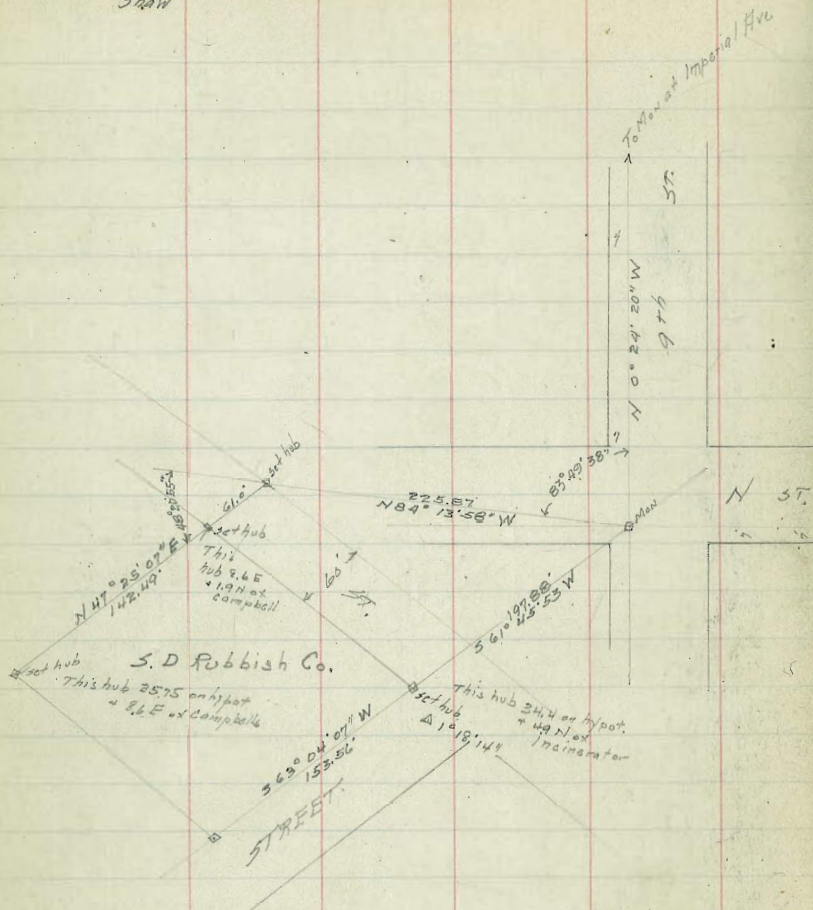
33



1st 2/20
Gregory
Miller
Shaw

Survey of Lease to S. D. Robbish, Co.

34



7/7/21 Gregory Levels on N. cb Line of Edgemont St
 from N. cb Line of Ash St To Beech ✓
 Web line is 12.5 from Prop

	240.56	238.31
N. cb Line Ash = 25' S. of N.L.	2.2	238.4
N. L. ✓	1.9	238.7
50' N. of N.L. Ash	1.9	238.7
100' ✓ ✓ ✓ ✓	2.1	238.5
140' ✓ ✓ ✓ ✓	3.2	237.4
170' ✓ ✓ ✓ ✓	5.1	235.5
180' ✓ ✓ ✓ ✓	6.9	233.7
192' ✓ ✓ ✓ ✓	7.0	233.6
215' ✓ ✓ ✓ ✓	10.9	229.7
T.P. 0.69 228.86	12.41	228.15
250' N. of N.L. Ash	6.8	222.0
270' ✓ ✓ ✓ ✓	11.9	216.9
280' ✓ ✓ ✓ ✓	13.5	215.3
T.P. 1.41 217.50	12.75	216.09
310.8 N. = 5 L. Beech	10.0	207.5
S. cb Line ✓ = 15' N. of 5 L. Beech	13.4	204.1
N. cb " Beech	22.4	195.1

Levels on E cb Line of Edgemont St
 from Ash to Beech
 Ecb Line is 10' from Prop

35

	240.56	238.31
N. cb Line Ash = 14' S. of N.L.	2.7	237.9
N.L. of ✓	3.5	238.1
15' ✓ of N.L. ✓	2.7	237.9
65' ✓ ✓ ✓ ✓	3.2	237.4
115' ✓ ✓ ✓ ✓	5.9	234.7
150' ✓ ✓ ✓ ✓	9.1	231.5
170' ✓ ✓ ✓ ✓	10.2	230.4
180' ✓ ✓ ✓ ✓	13.2	227.4
190' ✓ ✓ ✓ ✓	13.0	227.6
T.P. 0.69 228.86	12.41	228.15
195' N. of N.L. Ash	4.1	224.4
205' ✓ ✓ ✓ ✓	6.0	222.8
215' ✓ ✓ ✓ ✓	5.9	222.9
230' ✓ ✓ ✓ ✓	9.9	218.9
T.P. 1.41 217.50	12.75	216.09
255' ✓ ✓ ✓ ✓	4.4	213.1
280' ✓ ✓ ✓ ✓	11.2	206.3
310.8 ✓ ✓ ✓ ✓ = 5 L. Beech	18.7	198.8
325.8 ✓ ✓ ✓ ✓ = 500 ✓	22.1	195.4
355.8 ✓ ✓ ✓ ✓ = 11 ✓	29.7	187.8

7/2/21 Gregory Levels on N. Cb Line of
Beech St
from W.L. of Edgement
To E.L. of 31st

cb line is 15'
from Prop

	217.50		
W.L. Edgement		19.8	197.7
20' W.		12.2	205.3
40' ✓		5.1	212.4
T.P.	1232 229.71	0.11	217.39
60' W		11.2	218.5
75' ✓		6.8	222.9
	950 238.82	0.39	229.32
100' W		9.7	229.1
120' ✓		6.5	232.3
150' ✓		5.4	233.4
175' ✓		5.8	233.0
213.76 = EL 31 st		8.6	230.2
chk BM		8.22	230.60 = 230.57

Levels on S. Cb Line of
Beech St
from W.L. of Edgement
To E.L. of 31st

26

	217.50		
W.L. Edgement		10.5	207.0
20' W.		3.6	213.9
T.P.	1232 229.71	0.11	217.39
35' W		11.5	218.2
55' W		5.9	223.8
70' W - Drive		0.5	229.2
T.P.	950 238.82	0.39	229.32
110' W		4.4	234.4
160' ✓		3.7	235.1
209' ✓		5.4	233.4
213.76 = EL 31 st		7.4	231.4

8/12/21 Gregory
Hoard
Shaw

CROSS SECTION OF
ASH ST
from 31st to Edgemont

80' wide
25' CB
7.5' 1/4"

Station	Distance	Elevation	Notes
	5.03	243.34	238.31 ^{SPK SW} Edgemont Pk.
			E.L. 31 st
N	7.5	235.8 ✓	
cb	7.6	235.7 ✓	
1/4	7.6	235.7 ✓	
C	7.5	235.8 ✓	
1/4	7.4	235.9 ✓	
cb	7.7	235.6 ✓	
+10	8.2	235.1 ✓	
S	7.8	235.5 ✓	
			5' E
S	7.2	236.1 ✓	
+10	6.8	236.5 ✓	
cb	6.8	236.5 ✓	
1/4	6.5	236.8 ✓	
C	6.5	236.8 ✓	
1/4	6.2	237.1 ✓	
cb	6.1	237.2 ✓	
+15	5.8	237.5 ✓	
N	5.7	237.6 ✓	
			45' E
N	5.2	238.1 ✓	
+10	5.7	237.6 ✓	
cb	6.0	237.3 ✓	
1/4	6.0	237.3 ✓	
C	6.2	237.1 ✓	

Station	Distance	Elevation	Notes
1/4	6.4	236.9 ✓	
cb	6.5	236.8 ✓	
S	7.1	236.2 ✓	
			50' E
S	7.1	236.2 ✓	
cb	6.8	236.5 ✓	
1/4	6.7	236.6 ✓	
C	6.4	236.9 ✓	
1/4	6.2	237.1 ✓	
cb	6.0	237.3 ✓	
+10	5.2	238.1 ✓	
N	5.1	238.2 ✓	
			70' E
N	4.6	238.7 ✓	
+5	5.1	238.2 ✓	
cb	6.0	237.3 ✓	
1/4	6.3	237.0 ✓	
C	6.4	236.9 ✓	
1/4	6.4	236.9 ✓	
cb	6.5	236.5 ✓	
S	7.3	236.0 ✓ or limit	
			100' E
S	6.9	236.4 ✓	
cb	6.2	237.1 ✓	
1/4	5.7	237.6 ✓	
0	5.8	237.5 ✓	

243.34

1/4	5.5	237.8✓
cb	5.3	238.0✓
+10	4.4	238.9✓
N	4.2	239.1✓

150° E

N	4.0	239.3✓
+15	4.2	239.1✓
cb	4.5	238.8✓
1/4	4.7	238.6✓
c	4.8	238.5✓
1/4	4.9	238.4✓
cb	5.2	238.1✓
S	5.8	237.5✓

158.3 E

S = ^{N edge} end of walk parallel with St.

S	5.4	237.90✓
---	-----	---------

200° E

S = N edge of walk

S	5.4	237.90✓
cb	5.6	237.7✓
1/4	5.2	238.1✓
c	5.1	238.2✓
1/4	4.9	238.4✓
cb	4.4	238.9✓
+10	4.4	238.9✓
+20	4.7	238.6✓
N	4.4	238.9✓

4376

H3H

38

213.76 = N. L. Edgemont

N	4.7	238.6✓
cb	5.1	238.2✓
1/4	5.1	238.2✓
c	5.1	238.2✓
1/4	5.3	238.0✓
cb	5.5	237.8✓
S	5.5	237.8✓

8/12/21

Gregory
Moore
ShawCROSS SECTION OF
EDGEMONT ST.
From the HL of Ash
to the HL of BeechFrom A To S.L. Ash
From HL Ash To
HL Beech660' ST.
17.5' CASE
12.5' W
7.5' H52.5' ST.
10' CASE
12.5' W
7.5' H

39

	11.11	238.50	✓		227.39	BP SW
		HL A St.				
W		97	228.8	✓		
cb		96	229.9	✓		
1/4		98	228.7	✓		
C		93	229.2	✓		
1/4		94	229.1	✓		
cb		93	229.2	✓		
E		90	229.5	✓		
	3' N					
E		82	230.3	✓		
cb		82	230.3	✓		
1/4		85	230.0	✓		
C		91	229.4	✓		
1/4		95	229.0	✓		
cb		93	229.2	✓		
W		87	229.8	✓		
	50' N					
W		77	230.8	✓		
cb		76	230.9	✓		
1/4		77	230.8	✓		
C		74	231.1	✓		
1/4		73	231.2	✓		
cb		71	231.4	✓		
E		68	231.7	✓		

	100' N					
E		56	232.9	✓		
cb		59	232.6	✓		
1/4		62	232.3	✓		
C		63	232.2	✓		
1/4		65	232.0	✓		
cb		62	232.3	✓		
W		65	232.0	✓		
	150' N					
W		53	233.2	✓		
cb		52	233.3	✓		
1/4		53	233.2	✓		
C		49	233.6	✓		
1/4		52	233.3	✓		
cb		49	233.6	✓		
E		45	234.0	✓		
	192' N = center of 2.5' walk to house					
	W - 1.5'	40.4	234.46	✓		
	200' N					
E		31	235.1	✓		
cb		39	234.6	✓		
1/4		40	234.5	✓		
C		37	234.8	✓		
1/4		42	234.3	✓		
cb		43	234.2	✓		
W		41	234.4	✓		

228.30 = center of 4' walk to house.

W - 1.7

3.65 234.85 ✓

250' N

W

2.9 235.6 ✓

cb

3.1 235.4 ✓

1/2

3.0 235.5 ✓

C

2.6 235.9 ✓

1/2

2.7 235.8 ✓

cb

2.7 235.8 ✓

E

2.2 236.1 ✓

255' = center of drive to garage

5.3 E of E

2.10 236.40 ✓

273' = center of 4' walk

7.5 E of E

2.10 = 236.48 ✓

300' N

E

1.6 236.9 ✓

cb

1.5 237.0 ✓

1/2

1.3 237.2 ✓

C

1.5 237.0 ✓

1/2

1.8 236.7 ✓

cb

2.2 236.3 ✓

W

2.1 236.4 ✓

330' N = C

W = S. E. edge of 5.5' walk to house

1.0 237.5 ✓

cb

1.5 237.0 ✓

1/2

1.2 237.1 ✓

C

1.2

237.3 ✓

1/2

1.2

237.3 ✓

cb

1.2

237.3 ✓

E = center 35' walk to house.

1.2

237.3 ✓

355' N on E }
355.7' W } = S. L. Ash St. 80 ft.14' Cobson E
25' W
13' W
7.5' W

E

1.0

237.5 ✓

cb

0.9

237.6 ✓

1/2

0.9

237.6 ✓

C

0.7

237.8 ✓

1/2

0.8

237.7 ✓

cb

1.0

237.5 ✓

W

0.7

237.8 ✓

ch. B.M. 5.59

243.90 ✓

0.23

238.27 = 21' x 6' SW of Ash St.

25' N on W }
14' W } = 5' cb.

W

6.1

237.8 ✓

cb

6.0

237.9 ✓

1/2

6.0

237.9 ✓

C

6.0

237.9 ✓

1/2

6.0

237.9 ✓

cb

6.1

237.8 ✓

+ 16.19 = E

6.3

237.6 ✓

7.5' N. of Sec on W }
13' W } = 5' quarter.

E

6.2

227.7 ✓

+ 14.97 = cb

6.1

237.8 ✓

+ 17.5 = 1/2

5.9

238.0 ✓

ditto = C

6.0

237.9 ✓

24390

1/4	5.9	238.0 ✓
cb	5.9	238.0 ✓
W	5.9	238.0 ✓
W	5.6	238.3 ✓
cb	5.6	238.3 ✓
1/4	5.8	238.1 ✓
C	5.8	238.1 ✓
1/4	6.0	237.9 ✓
cb	6.0	237.9 ✓
+ 13.75 = E	6.4	237.5 ✓
E	6.7	237.2 ✓
+ 17.53 = cb	6.2	237.7 ✓
+ 7.5 = 1/4	6.8	237.9 ✓
ditto = C	6.0	237.9 ✓
1/4	5.9	238.0 ✓
cb	5.5	238.4 ✓
W	5.6	238.3 ✓
W	5.6	238.3 ✓
cb	5.5	238.4 ✓
1/4	5.7	238.2 ✓
C	5.9	238.0 ✓
1/4	6.0	237.9 ✓
cb	6.1	237.8 ✓

7.5' N on W }
13' v E } = Center of Ash7.5' N on W }
13' v E } = N. Quarter7.5' N on W }
13' v E } = N. curb

Edgemont 41

+ 11.31 = E	6.6	237.3 ✓
E	6.4	237.5 ✓
+ 10 = cb	5.9	238.0 ✓
1/4	5.7	238.2 ✓
C	5.6	238.3 ✓
1/4	5.5	238.4 ✓
cb	5.3	238.6 ✓
W	5.3	238.6 ✓
W	5.0	239.9 ✓
cb	5.2	238.7 ✓
1/4	5.3	238.6 ✓
C	5.6	238.3 ✓
1/4	6.1	237.8 ✓
cb	6.5	237.4 ✓
E	7.6	236.3 ✓
E	8.1	235.8 ✓
cb	6.6	237.3 ✓
E	8.7	235.2 ✓
cb	6.7	237.2 ✓
E	8.0	235.9 ✓
cb	6.7	237.2 ✓

25' N on W }
14' v E } = N. L. Ash St. Edgemont =
52.5' wide drain
here 10.
10' cbs on E
12.5' v W

50' N

53' N

59' N

64' N

24370

75' N

E	8.5	235.4 ✓
cb	7.0	236.9 ✓
1/4	5.8	238.1 ✓
C	5.6	238.3 ✓
1/4	5.3	238.6 ✓
cb	5.2	238.7 ✓
W	5.0	238.9 ✓

100' N

W	5.3	238.6 ✓
cb	5.4	238.5 ✓
1/4	5.6	238.3 ✓
C	5.8	238.1 ✓
1/4	7.0	236.9 ✓
cb	8.3	235.6 ✓
E	10.1	233.8 ✓
+5	10.9	233.0 ✓

125' N

-15 - 100'	16.4	227.5 ✓
E	11.8	232.1 ✓
cb	10.3	233.6 ✓
1/4	8.6	235.3 ✓
C	7.3	236.6 ✓
1/4	6.3	237.4 ✓
cb	6.0	237.9 ✓
W	5.6	238.3 ✓

Edgemont 42

150' N

W	6.0	237.9 ✓
cb	7.1	236.8 ✓
1/4	8.0	235.9 ✓
C	9.0	234.9 ✓
1/4	10.5	233.4 ✓
cb	12.5	231.4 ✓
+7	12.3	231.6 ✓
E	14.1	229.8 ✓
+5	14.5	229.4 ✓
+7	17.3	226.6 ✓
+15	17.9	226.0 ✓

165' N

-15	20.4	223.5 ✓
-5.0	19.7	224.2 ✓
E	15.7	228.2 ✓
cb	13.3	230.6 ✓

170' N

-15	21.0	224.9 ✓
E	19.4	224.5 ✓
+2	16.6	227.3 ✓
cb	13.7	230.2 ✓
1/4	13.4	230.5 ✓
C	12.6	231.3 ✓
1/4	9.6	234.3 ✓
cb	8.6	235.3 ✓
W	6.8	237.1 ✓

34390

180° N

Ecb	16.4	227.5 ✓
+4	17.8	226.1 ✓
E.L	18.6	225.3 ✓
+2	20.2	223.7 ✓
+15	22.1	221.8 ✓

190° N

W	8.5	235.4 ✓
cb	10.2	233.7 ✓
1/4	10.9	233.0 ✓
C	14.9	229.0 ✓
1/4	15.3	228.6 ✓
cb	16.6	227.3 ✓
+3	19.3	224.6 ✓
E	20.6	223.3 ✓
+15	23.5	220.4 ✓

193° N

-15	23.9	220.0 ✓
E	20.8	223.1 ✓
cb	19.3	224.6 ✓
+1	17.0	226.9 ✓
1/4	16.1	227.8 ✓
C	15.4	228.5 ✓

206° N

Ecb	20.8	223.1 ✓
+3	21.7	222.2 ✓

Edgemont 43

E	23.5	220.4 ✓
120	26.0	217.9 ✓

215° N

-20	28.4	215.5 ✓
E	23.1	220.8 ✓
cb	21.3	222.6 ✓
1/4	19.7	224.2 ✓
C	18.9	225.0 ✓
1/4	16.7	227.2 ✓
cb	14.3	229.6 ✓
W	11.9	232.0 ✓
T.P.	0.33	231.32 ✓
		121.91 ✓
		230.99 ✓

230° N

W	1.9	229.4 ✓
cb	4.9	226.6 ✓
1/4	5.9	225.4 ✓
C	8.3	223.0 ✓
1/4	9.4	221.9 ✓
cb	11.7	219.6 ✓
+2	12.9	218.4 ✓
E	14.0	217.3 ✓
+20	20.1	211.2 ✓

250° N

-15	46.8	204.5 ✓
E	19.7	211.6 ✓
cb	19.3	214.0 ✓

231.32

+3			15.3	216.0 ✓
1/4			14.4	216.9 ✓
C			13.0	218.3 ✓
on Manhole			(12.4)	218.9 ✓
1/4			10.6	220.7 ✓
Cb			9.3	222.0 ✓
W			6.2	225.1 ✓
+10			3.8	227.5 ✓
		275' N		
-10			9.0	222.3 ✓
W			11.8	219.5 ✓
TP	0.45	218.72 ✓	13.05	218.27 ✓
Cb			2.7	216.0 ✓
1/4			4.9	213.8 ✓
C			7.1	211.6 ✓
1/4			8.8	209.9 ✓
Cb			11.3	207.4 ✓
E			14.2	204.5 ✓
+10			15.5	203.2 ✓
		310' N = 5L Beech		
E			22.4	196.3 ✓
Cb			19.7	199.0 ✓
1/4			17.1	201.6 ✓
C			15.1	203.6 ✓
1/4			13.3	205.4 ✓
Cb			11.2	207.5 ✓

Edgemont

24

W			7.7	211.0 ✓
		S curb		
W			11.7	207.0 ✓
Cb			14.5	204.2 ✓
1/4			16.4	202.3 ✓
C			18.6	200.1 ✓
1/4			20.7	198.0 ✓
Cb			23.2	195.5 ✓
E			25.3	193.4 ✓
TP	0.20	206.08 ✓	12.84	205.88 ✓
		S. Quarter		
W			0.6	205.5 ✓
Cb			3.7	202.4 ✓
1/4			5.6	200.5 ✓
C			7.7	198.4 ✓
1/4			10.1	196.0 ✓
Cb			12.6	193.5 ✓
E			14.9	191.2 ✓
		Center Beech		
E			16.7	189.4 ✓
Cb			14.5	191.6 ✓
1/4			12.6	193.7 ✓
C			10.3	195.8 ✓
1/4			7.7	198.4 ✓
Cb			5.8	200.3 ✓
W			3.3	202.8 ✓

206.08

N. Quarter

W	4.8	201.3 ✓
cb	8.5	197.6 ✓
1/2	10.1	196.0 ✓
C	12.1	194.0 ✓
1/4	14.1	192.0 ✓
cb	16.1	190.0 ✓
E	18.6	187.5 ✓

N. Corb

E	20.6	185.5 ✓
cb	18.5	187.6 ✓
1/2	16.4	189.7 ✓
C	14.7	191.4 ✓
1/4	13.1	192.7 ✓
cb	11.2	194.9 ✓
W	9.0	197.1 ✓

N. Line Beech

W	14.6	191.5 ✓
cb	16.0	190.1 ✓
1/2	17.8	188.3 ✓
C	18.9	187.2 ✓
1/4	20.7	185.4 ✓
cb	21.8	184.3 ✓
E	24.1	182.0 ✓

Edgemont.

45

8/22/21
Gregory
11 bars
500W

CROSS SECTION OF
BEECH ST
from W.L. Edgemont to
E.L. 31st St

60' wide
15' 0.25'
7.5' 1/4's

W.L. Edgemont
R.D. from page 44
206.08

S			+ 4.9	211.0 ✓
cb			+ 0.9	207.0 ✓
1/4			0.6	205.5 ✓
c			3.3	202.8 ✓
1/4			4.8	201.3 ✓
cb			9.0	197.1 ✓
N			14.6	191.5 ✓
	12' W			
N			7.2	198.9 ✓
cb			2.7	203.2 ✓
1/4			0.4	205.7 ✓
TP	12' 80	218.50 ✓	0.08	206.0 ✓
c			10.6	208.2 ✓
1/4			8.7	210.1 ✓
cb			7.3	211.5 ✓
S			3.6	215.4 ✓
TP	12' 13	231.56 ✓	0.17	215.63 ✓
	30' W			
S			11.3	220.3 ✓
cb			14.6	217.0 ✓
1/4			16.6	215.0 ✓
c			18.4	213.2 ✓
1/4			20.2	211.4 ✓

26

cb	22.7	208.9 ✓
N	27.6	204.0 ✓
	170' R. of 31st = 43.76' W	
-20	28.0	203.6 ✓
N	22.3	209.3 ✓
cb	18.0	213.6 ✓
1/4	15.2	216.4 ✓
c	13.7	217.9 ✓
1/4	12.2	218.4 ✓
cb	10.5	221.1 ✓
S	4.8	226.8 ✓
	168.5 = 45.76' W	
S	3.3	228.3 ✓
cb	10.0	221.6 ✓
	54' E = 59.76' W	
S	2.7	228.9 ✓
19	2.9	228.7 ✓
cb	6.5	225.1 ✓
	145' E = 68.76' W	
S	1.2	230.4 ✓
13	2.3	229.3 ✓
cb	2.7	228.9 ✓
13	4.5	227.1 ✓
1/4	5.6	226.0 ✓
c	7.6	224.0 ✓
1/4	8.7	222.9 ✓

231.56

cb	10.9	220.7 ✓
N	14.8	216.8 ✓
+1	17.0	213.6 ✓
+15	17.2	214.4 ✓

135° E = 78.76° W

-15	13.3	218.3 ✓
N	11.3	220.3 ✓
cb	7.7	223.9 ✓
1/4	5.6	226.0 ✓

C	4.1	227.5 ✓
1/4	2.5	229.1 ✓

+3	1.4	230.2 ✓
----	-----	---------

cb	1.5	230.1 ✓
----	-----	---------

+8	1.6	230.0 ✓
----	-----	---------

TP	7.18	238.26 ✓
	0.48	231.88 ✓

+10	6.7	231.6 ✓
-----	-----	---------

S	6.0	232.3 ✓ on land
---	-----	-----------------

115° E = 98.76° W

S	3.3	235.0 ✓ on land
---	-----	-----------------

+13	4.1	234.2 ✓
-----	-----	---------

cb	5.2	233.1 ✓
----	-----	---------

1/4	5.3	233.0 ✓
-----	-----	---------

C	6.7	231.6 ✓
---	-----	---------

1/2	8.3	230.0 ✓
-----	-----	---------

cb	9.2	229.1 ✓
----	-----	---------

N	12.0	226.3 ✓
---	------	---------

+10	14.0	224.3 ✓
-----	------	---------

BEECH 47

100° E = 113.76° W

-10	11.1	237.2 ✓
-----	------	---------

N	9.3	229.0 ✓
---	-----	---------

cb	6.5	231.8 ✓
----	-----	---------

1/4	5.7	232.6 ✓
-----	-----	---------

C	4.8	233.5 ✓
---	-----	---------

1/4	4.1	234.2 ✓
-----	-----	---------

cb	3.7	234.6 ✓
----	-----	---------

S	2.8	235.5 ✓
---	-----	---------

88° E = 125.76° W

S	2.8	235.5 ✓
---	-----	---------

cb	3.5	234.8 ✓
----	-----	---------

1/4	4.0	234.3 ✓
-----	-----	---------

C	4.4	233.9 ✓
---	-----	---------

1/4	4.8	233.5 ✓
-----	-----	---------

cb	5.3	233.0 ✓
----	-----	---------

N	7.3	231.0 ✓
---	-----	---------

75° E = 138.76° W

N	5.8	232.5 ✓
---	-----	---------

cb	4.9	233.4 ✓
----	-----	---------

1/4	4.7	233.6 ✓
-----	-----	---------

C	4.1	234.2 ✓
---	-----	---------

1/4	3.6	234.7 ✓
-----	-----	---------

cb	3.3	235.0 ✓
----	-----	---------

S	2.6	235.7 ✓
---	-----	---------

338.26

-50' L = 163.76' W

S	2.7	235.6 ✓
cb	3.2	235.1 ✓
1/4	3.4	234.9 ✓
C	3.8	234.5 ✓
1/4	4.4	233.9 ✓
cb	4.9	233.4 ✓
+5	5.6	232.7 ✓
+9	6.6	231.7 ✓
N	7.3	231.0 ✓

25' E = 188.76' W

N	7.9	230.4 ✓
+5.9	7.6	230.7 ✓
+6.1	6.6	231.7 ✓
cb	6.0	232.3 ✓
1/4	5.4	232.9 ✓
C	4.9	233.4 ✓
1/4	4.6	233.7 ✓
cb	4.4	233.9 ✓
S	4.0	234.3 ✓

5' E = 208.76' W

S	4.2	234.1 ✓
cb	4.9	233.4 ✓
1/4	5.1	233.2 ✓
C	5.7	232.6 ✓
1/4	6.4	231.9 ✓

BEECH

48

cb	7.4	230.9 ✓
N	8.1	230.2 ✓

213.76' W = E. L. 31st St.

N	7.5	230.5 ✓
cb	7.9	230.4 ✓
1/4	7.3	231.0 ✓
C	7.0	231.3 ✓
1/4	7.1	231.2 ✓
cb	6.9	231.4 ✓
S	7.1	231.2 ✓

7.65 230.61 = 230.61 BPSE
31st Beech

11/21/41
Gregory
Moore
m/l/61
Shad

CROSS SECTION OF
FRANCIS ST
from N. L. Homestead Union 13 1/4's
To N.L. Imperial Ave

80' wide
11' CBS

B.M.	10.30	87.53	77.23	Mon N.L. Homestead
		N.L. Homestead Union = 0+00		
E		1.7	85.8	
+12		3.1	84.4	
cb		4.5	83.0	
1/4		5.1	82.4	
+6		6.4	81.1	
c		7.7	79.8	
1/4		9.8	77.7	
cb		10.9	76.6	
W		13.5	74.0	
+10		14.7	72.8	
	0+25			
-10		14.1	73.4	
W		12.5	75.0	
cb		10.8	76.7	
1/4		9.1	78.4	
c		6.9	80.6	
+10		5.2	82.3	
1/4		4.0	83.5	
cb		3.4	84.1	
+10		0.9	86.6	
E		0.7	86.8	
	0+50			
E		0.8	86.7	

+11	0.9	86.6
cb	2.2	85.3
1/4	2.5	85.0
+5	4.0	85.5
c	3.9	83.6
1/4	6.0	81.5
cb	8.5	79.0
W	11.3	76.2
+10	13.8	73.7
	0+75	
-10	15.0	72.5
W	11.8	75.7
cb	7.9	79.6
1/4	5.1	82.4
c	2.8	84.7
+7	2.1	85.4
1/4	2.7	84.8
cb	2.6	84.9
+6	1.2	86.3
E	1.7	85.8
	1+00	
E	2.4	85.1
+10	2.9	84.6
cb	3.8	83.7
1/4	3.9	83.6
c	5.1	82.4

1/4	7.2	80.3
cb	10.2	77.3
W	14.5	73.0
+10	16.7	70.8
	1+25	
-10	18.4	69.1
W	16.7	70.8
cb	12.4	75.1
1/4	9.8	79.7
C	8.1	79.4
+10	6.4	81.1
1/4	5.3	82.2
cb	4.6	82.9
+5	3.5	84.0
F	3.0	84.5
	1+44.46 on E 1+44.55 W	} = N.L. Shafter St 50' wide 1/4 cbs
E	3.4	84.3
cb	4.9	82.6
1/4	5.8	81.7
+3	6.8	80.7
C	8.7	78.8
1/4	11.7	75.8
cb	14.8	72.7
+12	17.2	70.3
W	18.5	69.0
+10	19.0	68.5

	N. cb.	
-10	20.7	66.8
W	18.7	68.8
cb	16.5	71.0
1/4	12.1	75.4
C	9.1	78.4
1/4	5.8	81.7
cb	5.0	82.5
F	3.4	84.1
	N. 1/4	
E	4.0	83.5
cb	5.3	82.2
+6	5.5	82.0
1/4	6.6	80.9
C	9.1	78.4
1/4	13.5	74.0
cb	17.2	70.3
W	19.6	67.9
+10	21.5	66.0
	center	
+10	44.4	65.3
W	40.3	67.2
cb	17.9	69.6
1/4	13.9	73.6
C	9.9	77.6
1/4	7.0	80.5

+7	5.5	82.0
cb	5.4	82.1
E	4.2	83.3
5 1/4		
E	4.7	82.8
cb	5.7	81.8
+8	5.9	81.6
1/4	7.5	80.0
C	10.4	77.1
1/4	15.3	72.2
cb	18.0	69.5
W	21.1	66.4
+10	23.0	64.5
5 Curb		
-10	23.7	63.8
W	21.7	65.8
cb	19.4	69.1
1/4	14.2	71.3
C	12.1	75.4
1/4	8.4	79.1
+6	6.7	80.8
cb	6.9	80.6
E	5.0	82.5
5L Shafter = 0+00		
T.P.	6.66	80.87 ^{HV}
E	6.7	80.8 ^{SE}

cb	9.2	78.2
+8	8.8	78.7
1/4	10.2	77.3
T.P.	0.24	75.08
12.69		74.84
C	1.4	73.7
1/4	5.3	69.8
cb	8.3	66.8
W	10.4	64.7
+10	11.8	62.3
0+50		
-10	16.3	58.8
W	14.9	60.2
cb	13.0	62.1
1/4	11.0	64.1
C	9.4	65.7
+10	7.6	67.5
1/4	5.9	69.4
cb	5.4	69.7
E	5.3	69.8
0+75		
E	6.8	68.3
cb	9.0	66.1
1/4	9.4	65.7
+4	10.7	64.4
C	11.7	63.4
1/4	13.0	62.1

75.08

cb		14.8	60.3
W		16.3	58.8
+10		17.2	57.9
	14.00		
-10		15.5	59.6
W		15.7	59.4
cb		14.8	60.3
1/4		13.8	61.3
c		13.1	62.0
1/4		12.4	62.7
cb		12.0	63.1
E		10.0	65.1
	14.02.0		
E		10.9	64.2
cb		12.2	62.9
	14.25		
E		12.9	62.4
T.P.	0.13	62.53	12.68 62.40
+5		1.1	61.4
cb		2.2	60.3
1/4		2.0	60.5
c		1.7	60.8
1/4		1.9	60.6
cb		2.1	60.4
W		2.8	59.7

This is under
steps to house

62.53

FRANCIS 52

	14.40		
E		1.0	61.5
+8		3.7	58.8
cb		3.5	59.0
	14.41		
W		2.4	60.1
cb		2.4	60.1
1/4		2.2	60.3
c		2.3	60.2
1/4		2.5	60.0
+4		3.5	59.0
cb		3.5	59.0
+6		3.7	58.8
E		4.0	58.5
+10		4.6	57.9
	14.70		
-10		4.8	57.7
E		5.6	56.9
cb		5.7	56.8
1/4		5.9	56.6
c		4.9	57.6
1/4		4.2	58.3
cb		3.8	58.7
W		3.5	59.0
	2+00		
W		5.9	56.6

Adjustment
to garage

6253

cb	7.0	55.5
1/4	8.5	54.0
c	11.0	51.5
+10	9.4	53.1
1/4	8.1	54.4
+4	6.8	55.7
cb	6.7	55.8
E	6.5	56.0
+10	5.6	56.9

2+05

E	4.2	58.3
+8	6.2	56.3
cb	6.7	55.8

2+25

E	4.3	58.2
+4	4.7	57.8
+8	6.2	56.3
cb	7.0	55.5
+9	7.2	55.3
1/4	8.1	54.4
c	10.7	51.8
1/4	12.7	49.8
cb	11.3	51.2
W	10.1	52.4
+10	8.9	53.6

173
66
173

6253

FRANCIS

53

2+50

-10	11.7	50.8
W	12.6	49.9
cb	14.5	48.0
1/4	12.6	49.9
c	8.6	53.9
1/4	7.1	55.4
cb	6.7	55.8
E	5.0	57.5

2+75

E	6.1	56.4
cb	7.3	55.2
1/4	7.3	55.2
+4	7.5	55.0
c	9.0	53.5
1/4	12.0	50.5
cb	14.2	48.3
+10	15.8	46.7
W	15.8	46.7
+10	14.0	48.5

3400 = N.L. TOMPKINS ST ^{80' wide} _{14' cbs}

-10	15.7	46.8
W	17.3	45.2
cb	14.8	47.7
1/4	11.6	50.9
c	9.5	53.0

6253

1/4			8.7	53.8	
cb			8.5	54.0	
E			7.1	55.4	
T.P.	4.54	55.63	11.44	51.09	noibs 19 pp N. of Tompkins
	10.5				
E			0.5	55.1	
+10			2.1	53.5	
cb			2.4	53.2	
		N. curb			
E			2.8	52.8	
cb			2.5	53.1	
1/4			2.4	53.2	
c			3.3	52.3	
1/4			6.0	49.6	
cb			9.0	46.6	
W			11.1	44.5	
		N. 1/4			
W			11.9	43.7	
cb			9.9	45.7	
1/4			8.1	47.5	
c			4.2	51.4	
1/4			2.9	52.7	
cb			3.0	52.6	
E			3.5	52.1	
		Center			
E			3.7	51.9	

55,63

FRANCIS 54

cb			3.7	51.9	
1/4			3.9	51.7	
c			6.1	49.5	
1/4			9.8	45.8	
cb			10.9	44.7	
W			12.4	43.2	
		3 1/4			
W			12.1	43.5	
+5			13.0	42.6	
cb			12.1	43.5	
1/4			10.85	44.78	on Mar
c			8.4	47.2	
1/4			5.1	50.5	
cb			4.7	50.9	
E			4.3	51.3	
		S. Curb			
E			5.3	50.3	
cb			5.9	49.7	
1/4			6.2	49.4	
c			9.6	46.0	
+7			11.7	43.9	
1/4			12.0	43.6	
cb			13.3	42.3	
W			12.4	43.2	
		S.L. Tompkins = 0400			
W			12.7	42.9	

55,63

cb	14.6	41.0
+7	14.7	40.9
1/4	13.7	41.9
c	11.0	44.6
1/4	7.8	47.8
cb	7.2	48.4
E	6.7	48.9

+ 0.3 = House Line

0+25

E	10.0	45.6
cb	10.0	45.6
1/4	10.7	44.9
c	13.4	42.7
T.P.	0.59	44.0
1/4		12.20
1/4	3.1	40.9
cb	4.8	39.2
+7	5.0	39.0
W	3.5	40.5

0+50

W	6.7	37.3
cb	5.4	38.6
1/4	3.7	40.3
c	2.7	41.3
1/4	2.2	41.8
cb	0.8	43.2
+7	2.0	44.0

FRANCIS

55

440v

E	3.0	41.0
	0+80	
E	7.0	37.0
cb	6.0	38.0
1/4	5.6	38.4
c	6.3	37.7
1/4	5.7	38.3
cb	6.0	38.0
W	7.0	37.0

0+90

W	6.3	37.7
cb	6.4	37.6
1/4	6.8	37.2
c	7.4	36.6
1/4	7.7	36.3
cb	7.4	36.6
E	8.8	35.2

0+90.90 on W = 1 rail

W on rail 6.15 37.87

0+96.52 on W = 5 rail

W on rail

1+00

E	9.5	34.5
cb	8.2	35.8
1/4	7.7	36.3
c	7.6	36.4

44.02

1/4	7.0	37.0
cb = center of Track	6.3	37.7
W.	6.0	38.0
1+14.9 on E = N rail		
W	8.3	35.7
cb	8.0	36.0
1/2	7.3	36.7
c	6.8	37.2
1/4	6.5	37.5
cb = center of Track	6.2	37.8
E	6.7	37.3
N rail	6.35	37.67
1+20.1 on E = S rail		
S rail	5.99	38.03
1+26		
E	7.2	36.8
cb	8.0	36.0
1/4	8.8	35.2
c	8.4	35.9
1/2	8.2	35.8
cb	8.9	35.1
W	10.1	33.9
1+30		
W	10.5	33.5
cb	9.3	34.7
1/4	8.7	35.3

44.02

FRANCIS

56

c	11.9	32.1
1/4	9.2	34.8
cb	9.5	34.5
E	10.0	34.0
1+38		
E	9.8	34.2
+10	10.6	33.4
cb	13.8	30.2
1/4	13.8	30.2
c	16.3	27.7
1/4	15.5	28.5
cb	12.0	32.0
+3	10.3	33.7
W	11.1	32.9
1+40		
W	11.2	32.8
+8	10.5	33.5
T.P. 1488	32.95	12.89
cb	2.7	30.3
1/4	5.4	27.6
c	5.8	27.2
1/4	4.6	28.4
+11	3.9	29.1
cb	1.9	31.1
+8	0.0	33.0
E	2.3	30.7

32.95

1+50

E	8.5	245
cb	7.8	252
1/4	8.6	244
c	8.8	242
1/4	9.4	236
cb	7.2	258
+9	0.2	328
W	0.2	328

1+54

W	2.3	307
cb	7.8	252
1/4	9.9	231
c	9.7	233
1/4	8.7	243
+5	10.1	229
cb	10.7	223
+8	11.8	212
E	11.6	214

1+65

E	9.9	231
cb	10.9	221
+6	11.5	215
1/4	12.3	207
+3	11.2	218
c	10.1	229

32.95

FRANCIS

57

1/4	10.1	229
cb	11.0	220
W	7.2	258

1+75

W	11.1	219
cb	9.8	232
1/4	11.1	219
c	11.4	216
+2	12.6	204
+8	12.2	208
1/4	10.4	226
cb	9.3	237
E	8.3	247

1+90

E	7.5	255
cb	7.6	254
1/4	7.6	254
c	9.5	235
+2	9.7	233
+8	12.8	202
1/4	11.8	212
cb	11.5	215
+9	9.8	232
W	10.4	226
W	10.6	224

2+00.35 = 1/4 Imperial on W

32.95

+5	11.6	21.4
cb	11.7	21.3
+3	12.8	20.2
+7	12.8	20.2
+10	10.4	22.6
1/4	10.4	22.6
c	7.9	25.1
1/4	7.5	25.5
cb	7.0	26.0
E	7.3	25.7

2+43.17 on E at L's to E. Line

E	6.7	26.3
cb	7.3	25.7
1/4	7.6	25.4
c	7.6	25.4

2+00.35 on W
2+85.09 on E = N.H. Imperial Ave.

E	6.3	26.7
cb	6.8	26.5
1/4	7.2	25.8
c	7.6	25.4
1/4	8.1	24.9
cb	9.5	23.5
+6	12.7	20.3
+12	12.8	20.2
W	10.6	22.4
T.P.	0.31	32.40
	0.86	32.09

32.95
1.43
33.38
33.38
33.38
33.38

58

6.59

25.81

N. on SE

33rd + L.

3.55

28.85

Top N. on

33rd + M.

See notes on X section of Imperial Ave
for location of Big pipe. (Book 1040 plot)

14 1/2
Gregory
Pierce
Miller
Shaw

CROSS SECTION OF
TOMPKINS ST
from W. of Francis to
W.L. of 36th ST

80' wide to
W.L. Parke 14' obs.
60' wide E.L. Parke
to W.L. 36th

5775

59

6.66 57.75 51.09

nails in place
109L 54

178' W. of Francis

N 10.4 47.4

176' W. of Francis

N 6.4 51.4

150' W. of Francis

N 0.8 57.0

(Not practical to Grade)
(before this section)
unless on the diagonal

118' W. of Francis

123' W. of Francis
is 10' lower on S side
than 118' W.

N 1.1 56.7

cb 1.8 56.0

1/2 2.5 55.3

c 3.1 54.7

1/2 4.1 53.7

cb 5.3 52.5

S 6.7 51.1

+2 13.0 44.8

100' W. of Francis

S 6.2 51.6

cb 5.5 52.3

1/2 4.5 53.3

c 3.6 54.2

1/2 3.0 54.8

cb 2.5 55.3

N 1.8 56.0

75' W. of Francis

N 2.9 54.9

cb 3.4 54.4

1/2 4.3 53.5

c 4.7 53.1

1/2 5.3 52.5

cb 6.2 51.6

S 6.8 51.0

50' W. of Francis

S 7.5 50.3

cb 7.0 50.8

1/2 6.7 51.1

c 6.2 51.6

1/2 5.7 52.1

cb 5.1 52.7

N 4.6 53.2

30' W. of Francis

N 7.5 50.3

cb 8.0 49.8

1/2 8.5 49.3

c 9.0 48.8

1/2 9.6 48.2

cb 9.1 48.7

S 9.2 48.6

W. L. Francis

S 14.8 43.0

57.75

cb	14.5	43.3
1/4	14.2	43.6
c	14.5	43.3
1/4	14.0	43.8
cb	13.2	44.6
N	12.5	45.3
E. L. Francis = 0400		
N	2.3	55.5
+10	2.6	55.2
cb	4.9	52.9
1/4	5.6	52.2
c	5.8	52.0
1/4	6.4	51.4
cb	7.4	50.4
S	8.8	49.0
0+25		
S = Under House.	9.8	48.0
+9.8 = Edge of - } House ends at 0+30	8.7	49.1
cb	7.8	50.0
1/4	7.0	50.8
c	6.2	51.6
1/4	5.5	52.3
cb	3.8	54.0
+4	2.3	55.5
N	1.3	56.5

57.75

TOMPKINS

60

0+55		
N	0.6	57.2
cb	1.4	56.4
1/4	6.5	51.3
+5	7.6	50.2
c	7.9	49.9
+7	8.4	49.4
1/4	11.5	46.3
cb	14.8	43.0
S	18.1	39.7
0+80		
S	15.2	42.6
cb	14.9	42.9
1/4	13.8	44.0
+4	12.6	45.2
+10	8.5	49.3
c	8.1	49.7
1/4	8.0	49.8
cb	3.8	54.0
N	0.6	57.2
0+86		
N	0.9	56.9
cb	4.2	53.6
1/4	8.0	49.8
c	7.9	49.9
+2	8.3	49.5

57.75

1/4		14.5	43.3
cb		15.7	42.1
S		17.2	40.6
	1+00		
S		12.0	45.8
cb		14.8	43.0
1/4		15.7	42.1
+11		11.4	46.4
C		11.4	46.4
1/4		11.5	46.3
+2		8.6	49.2
cb		5.2	52.6
N		1.8	56.0
	1+25		
N		6.8	51.0
cb		11.7	46.1
+9		11.6	46.2
1/4		8.9	48.9
+4		6.0	51.8
C		6.1	51.7
+6		5.8	52.0
+10		8.3	49.5
1/4		8.6	49.2
cb		6.2	51.6
S		1.3	56.5

57.75

TOMKINS

61

	1+35		
S		0.7	57.1
cb		2.5	55.3
1/4		5.3	52.5
C		4.8	53.0
+7		4.9	52.9
1/4		8.8	49.0
+3		10.9	46.9
+7		11.8	46.0
cb		11.8	46.0
N		9.8	48.0
	1+43		
N		11.5	46.3
cb		11.5	46.3
+8		10.9	46.9
1/4		7.8	50.0
+6		3.6	54.2
C		3.8	54.0
1/4		3.6	54.2
cb		1.2	56.6
S		0.0	57.8
	1+55		
S		+0.6	58.4
cb		0.1	57.7
1/4		2.0	55.8
C		2.4	55.4

For Culvert Notes
see page 79

57.75

+7		2.9	54.9
1/4		5.1	52.7
+w		6.1	51.7
cb		8.1	49.7
N		10.7	47.1

1+75

N		3.7	54.1	
cb		1.1	56.7	
T.P.	11.66	69.24	0.17	57.58
1/4		11.1	58.1	
c		11.3	57.9	
1/4		10.6	58.6	
cb		9.7	59.5	
s		9.7	59.5	

1+95

N		8.4	60.8
cb		9.0	60.2
	200' = W.L. 35' 1/2		70' wide 74' cbs
s		8.8	60.4
cb		8.7	60.5
1/4		8.8	60.4
c		8.9	60.3
1/4		8.7	60.5
cb		8.5	60.7
N		7.6	61.6
set B.M.		7.40	61.84

69.24

TAMPKINS

62

W. curb

N	6.3	62.9
cb	7.0	62.2
1/4	7.5	61.7
c	8.0	61.2
1/4	8.0	61.2
cb	7.9	61.3
s	7.9	61.3

W. 1/4

s	7.3	61.9
cb	7.6	61.6
1/4	7.1	62.1
c	6.9	62.3
1/4	6.4	62.8
cb	5.9	63.3
N	5.0	64.2

center 35' 1/2

N	3.9	65.3
cb	4.6	64.6
1/4	5.5	63.7
c	6.1	63.1
1/4	6.3	62.9
cb	7.0	62.2
s	7.3	61.9

6924

E 1/4

S	7.1	62.1
cb	6.8	62.4
1/4	5.6	63.6
C	5.4	63.8
1/4	4.9	64.3
cb	4.6	64.6
+4	3.5	65.7
N	3.0	66.2

E Curb.

N	2.9	66.3
+9	3.3	65.9
cb	4.5	64.7
1/4	4.7	64.5
C	5.1	64.1
1/4	5.3	63.9
cb	6.3	62.9
S	6.8	62.4

E.L. 35th ST = 0+00

S	6.5	62.7
+10 = fence	6.2	63.0
cb	6.1	63.1
1/4	5.0	64.2
C	4.7	64.5
1/4	4.3	64.7
cb	4.4	64.8

6924

TOMKINS

63

+5 = fence	3.3	65.9
N	2.4	66.8

0+50

N	1.6	67.6
+9.5 = fence	2.2	67.0
cb	3.0	66.2
+7	3.9	65.3
1/4	3.6	65.6
C	3.7	65.5
1/4	4.8	64.4
cb	5.8	63.4

+35 = fence

S	6.1	63.1
S	6.6	62.6

1+00

S	6.6	62.6
+7 = fence	5.6	63.6
cb	5.2	64.0
1/4	3.8	65.4
C	2.8	66.4
1/4	2.4	66.8
cb	1.4	67.8
N	0.6	68.6

T.P.	4.98	73.28
------	------	-------

1+50

N	3.4	69.9
cb	4.0	69.3

73.28

1/4	5.4	67.9
c	5.5	67.8
1/4	6.1	67.2
cb	7.1	66.2
+3.5 = fence	7.6	65.7
S	8.8	64.5
1+75		
S	8.4	64.9
+11	7.1	66.2
cb	6.4	66.9
1/4	5.5	67.8
c	5.0	68.3
1/4	4.4	68.9
cb	2.8	70.5
N	1.9	71.4
2+100 on S } = 1/4 L. Pardee 60' wide on N 2+10 - N } = 80' - S		
N	2.8	70.5
cb	2.8	70.5
1/4	4.6	68.7
c	5.0	68.3
1/4	5.2	68.1
cb	6.9	66.4
S	8.4	64.9
14' E on S } = 1/4 cb x = 76.5 wide 10' - - N }		
S	8.7	64.6
cb	7.4	65.9

73.28

TOMPKINS

64

1/4	6.1	67.2
c	5.3	68.0
1/4	4.8	68.5
cb	4.5	68.8
N	4.0	69.3
13' E on S } = 1/4 1/4 73.3 wide section 10' - - N }		
N	4.0	69.3
cb	4.8	68.5
1/4	5.1	68.2
c	5.7	67.6
+4	6.7	66.6
1/4	7.3	66.0
cb	7.7	65.6
S	8.8	64.5
set B.M.		
N	7.64	65.64
13' E on S } = Center 70' section 10' - - N }		
S	9.6	63.7
cb	9.1	64.2
1/4	8.4	64.9
+9	7.0	66.3
c	6.1	67.2
1/4	5.5	67.8
cb	4.6	68.7
N	3.9	69.4
13' E on S } = E 1/4 66.7' section 10' - - N }		
N	3.9	69.4

7328

cb	47	68.6
1/4	55	67.8
c	6.1	67.3
1/2	8.6	64.7
cb	10.3	63.0
S	11.6	61.7

13' E on S }
10' - - N } = E Curb

S	11.7	61.6
cb	11.0	62.3
1/2	8.7	64.6
c	6.4	66.9
1/2	5.5	67.8
cb	4.8	68.5
N	3.4	69.9

14' E on S }
10' - - N } = E.L. Pordec. on Diagonal

N	2.2	71.1
cb	4.5	68.8
1/2	5.4	67.9
c	6.3	67.0
1/2	8.2	65.1
cb	10.2	63.1
+2	11.0	62.3
S	11.8	61.5

25' E on S }
35' - - N }

Regular 60' section

S	10.1	63.2
cb	9.0	64.3

7328

TOMPKINS

65

1/2	7.0	66.3
c	6.3	67.0
1/2	5.1	68.2
cb	4.3	69.0
+9	3.6	69.7
N	2.9	70.4

50' E on S }
60' - - N }

N	4.1	69.2
cb	5.0	68.3
1/2	6.3	67.0
c	6.9	66.4
1/2	7.4	65.9
cb	8.1	65.2
S	8.7	64.6

100' E on S }
110' - - N }

S	7.1	66.2
cb	7.4	65.9
1/2	7.3	66.0
c	6.9	66.4
1/2	6.1	67.2
cb	5.6	67.7
N	5.0	68.3

407.6 E on S =
center of 3' walk on S. extends 6' in ST.

on walk

N	7.0	66.3
N	5.0	68.3

150' E on S }
160' - - N }

cb	5.5	67.8
1/4	5.9	67.4
c	6.2	67.1
1/4	6.4	66.9
cb	7.2	66.1
s	7.3	66.0
$\left. \begin{array}{l} 200' \text{ E } 075 \\ 220' \text{ } \end{array} \right\} N = 14.1, 36^{\text{th}} \text{ ST.}$		
s	7.7	65.6
cb	7.2	66.1
1/4	6.4	66.9
c	5.9	67.4
1/4	5.5	67.8
cb	4.9	68.4
N	4.4	68.9
set B.M.	4.51	68.77

12521

Gregory
Thompson
Miller
Starr

CROSS SECTION OF
35th St
from N.L. Tompkins to
N.L. Homestead Union

80' wide
14' cbs
13' 1/2

71.50

67

9.66

71.50

61.84

58th SW
35th Temp.

N.L. TOMPKINS +0100

0+55

W	11.1	60.4
cb	8.6	62.9
1/4	7.3	64.2
C	6.2	65.3
1/4	5.3	66.2
cb +3 = fence	5.2	66.3
E	4.7	66.8
0+25		
E +11 = fence	3.7	67.2
CO	4.4	67.1
1/4	4.9	66.6
C	5.4	66.1
1/4	6.7	64.8
cb	7.8	63.7
W	9.7	61.8
0+45		
W	11.8	59.7
+2	10.4	61.1
+8	9.1	62.4
cb	7.5	64.0
1/4	5.9	65.6
C	4.9	66.6
1/4	4.4	67.1

cb
+3 = fence
E

E	2.5	69.0
cb	3.2	68.3
+9	4.2	67.3
1/4	4.1	67.4
C	4.6	66.9
1/4	5.7	65.8
cb	7.3	64.2
+4	8.4	63.1
+6	12.1	59.4
W	12.3	59.2
0+80		
W	12.3	59.2
+8	11.5	60.0
+10	8.5	63.0
cb	6.7	64.8
+5	5.0	66.5
1/4	4.8	66.7
C	4.3	67.2
1/4	3.9	67.6
+5	3.8	67.7
+10	2.9	68.6
cb	2.8	68.7
E	2.0	69.5

71.50

0+99

W	11.7	59.8
+10	11.0	60.5
+11	9.5	62.0
cb	9.5	62.0

1+00

E	2.1	69.4
cb	2.8	68.7
+7	4.0	67.5
1/4	4.2	67.3
c	4.4	67.1
1/4	5.3	66.2
cb	8.7	62.8
W	11.4	60.1

1+25

W	11.0	60.5
cb	8.3	63.2
1/4	6.6	64.9
c	5.3	66.2
1/4	5.0	66.5
cb	4.3	67.2
E	3.6	67.9

1+42

E	3.5	68.0
+9.9	4.1	67.4
+10.1	6.5	65.0

71.50

35+4

68

cb	6.7	64.8
1/4	7.1	64.4
c	7.4	64.1
1/4	9.1	62.4
cb	10.2	61.3
W	11.6	59.9

1+49

E	3.6	67.9
+9.9	4.0	67.5
+10.1	7.0	64.5
cb	7.9	63.6

1+50

W	15.1	56.4
cb	14.3	57.2
+8	12.8	58.7
1/4	11.0	60.5
+5	8.7	62.8
c	8.0	63.5
+9	7.8	63.7
1/4	9.4	62.1
+4	10.1	61.4
cb	7.9	63.6
E	5.7	65.8

1+62

E	7.0	64.5
+9	8.9	62.6

71.50

cb	11.7	59.8
+6	11.5	60.0
1/4	10.3	61.2
+8	8.0	63.5
c	8.1	62.4
+4	8.2	63.3
+8	11.7	59.8
1/4	12.6	58.9
cb	14.0	57.5
W	14.9	56.6
1+72		
W	12.3	58.2
+8	13.7	57.8
cb	12.0	59.5
1/4	9.5	62.0
+7	7.8	63.7
c	7.8	63.7
1/4	8.8	62.7
+7	11.0	60.5
cb	11.5	60.0
E	11.0	60.5

see page 73 for culvert notes

1+82

E	11.1	60.4
cb	9.0	62.5
+8	7.5	64.0

71.50

3574

69

1/4	7.4	64.1
c	7.3	64.2
1/4	7.6	63.9
cb	10.1	61.4
+10	11.0	60.5
W	10.6	60.9
1+92		
W	9.3	62.2
cb	8.7	62.8
1/4	6.9	64.6
c	6.3	65.2
1/4	6.4	65.1
cb	6.6	64.9
E	6.7	64.8
2+00		
E	4.9	66.6
cb	4.9	66.6
1/4	5.1	66.4
c	5.4	66.1
1/4	6.1	65.4
cb	7.8	63.7
W	8.2	63.3
2+25		
W	2.8	68.7
cb	2.3	69.2
1/4	2.6	68.9

71.50

c		1.9	69.6	
1/4		1.0	70.5	
+5		1.3	70.2	
+8		0.2	71.3	
T.P.	12.83	84.03	0.30	71.20
cb		12.6	71.4	
E		12.0	72.0	
2+50				
E		9.0	75.0	
cb		9.3	74.7	
+6		9.6	74.4	
+7		10.5	73.5	
1/4		10.5	73.5	
c		11.4	72.6	
1/4		11.8	72.2	
cb		11.6	72.4	
W		11.3	72.7	
2+75				
W		9.1	74.9	
cb		9.1	74.9	
1/4		8.9	75.1	
c		8.5	75.5	
1/4		8.0	76.0	
+4		8.0	76.0	
+7		7.0	77.0	
cb		6.8	77.2	

84.03

35TH

70

F		6.3	77.7	
3400 = 3 L Shafter St 80 wide 14 cbs				
E		4.2	79.8	
cb		4.6	79.4	
+10		5.4	78.6	
1/4		5.4	78.6	
c		5.6	78.4	
1/4		5.8	78.2	
cb		5.7	78.3	
W		6.5	77.5	
S. Curb				
W		4.4	79.6	
cb		4.5	79.5	
set B.M.				
1/4		3.46	80.57	SW 13.12
1/4		4.5	79.5	
c		4.0	80.0	
1/4		4.0	80.0	
cb		3.0	81.0	
E		2.7	81.3	
S. Quarter				
E		1.3	82.7	
cb		1.7	82.3	
1/4		2.1	81.9	
c		2.8	81.2	
1/4		3.1	80.9	
cb		3.5	80.5	
W		3.9	80.1	

84.03

Center Shalter

W	2.9	81.1
cb	2.0	82.0
1/4	1.6	82.4
c	1.3	82.7
1/4	0.6	83.4
cb	0.1	83.9
E	0.0	84.0
T.P.	11.39	95.30
	0.12	83.91

N. Quarter

E	10.6	84.7
cb	10.8	84.5
1/4	11.3	84.0
c	11.7	83.6
1/4	12.0	83.3
cb	12.7	82.6
W	13.3	82.0

N. Curb

W	11.0	84.3
cb	10.9	84.4
1/4	10.8	84.5
c	10.4	84.9
1/4	10.2	85.1
cb	9.9	85.4
E	9.0	86.3

95.30

35.19

71

N. L. Shalter

= 0+00

E on lawn	7.5	87.8
cb	8.7	86.6
1/4	8.9	86.4
c	8.8	86.5
1/4	9.1	86.2
cb	9.8	85.5
W	10.4	84.9

0+15

W	10.1	85.2
cb	8.4	86.9
1/4	7.6	87.7
c	7.3	88.0
1/4	7.6	87.7
cb	7.4	87.9
E on lawn	6.0	89.3

0+35

E on lawn	4.7	90.6
cb	5.8	89.5
1/4	6.1	89.2
c	5.7	89.6
1/4	6.4	88.9
+9	7.2	88.1
cb	7.5	87.8
W	7.4	87.9

95.30

0+60

W	on lawn front wall of House	6.6	88.7
cb		6.3	89.0
1/4		5.1	90.2
+6		4.0	91.3
c		3.8	91.5
1/4		3.9	91.4
cb		3.8	91.5
+6 = fence		3.6	91.7
E		3.3	92.0

0+85

E		1.5	93.8
+8 = fence			
cb		1.7	93.6
1/4		1.7	93.6
c		2.2	93.1
1/4		3.2	92.1
cb		4.2	91.1
W = front wall of House		5.4	89.9

1+00

W		3.3	92.0
cb		3.0	92.3
1/4		2.0	93.3
c		1.1	94.2
1/4		0.9	94.4
cb		0.4	94.9
+6 = fence			
E		0.0	95.3

95.30

35th

72

T.P. 6.02 100.50 0.82 94.48
1+25

E		3.7	96.8
cb		4.2	96.3
1/4		4.5	96.0
c		4.8	95.7
1/4		5.3	95.2
cb		6.4	94.1
W = 0.35 under House		7.3	93.2

1+44.23 on W
1+44.12 - E } = N.L. Homestead Union

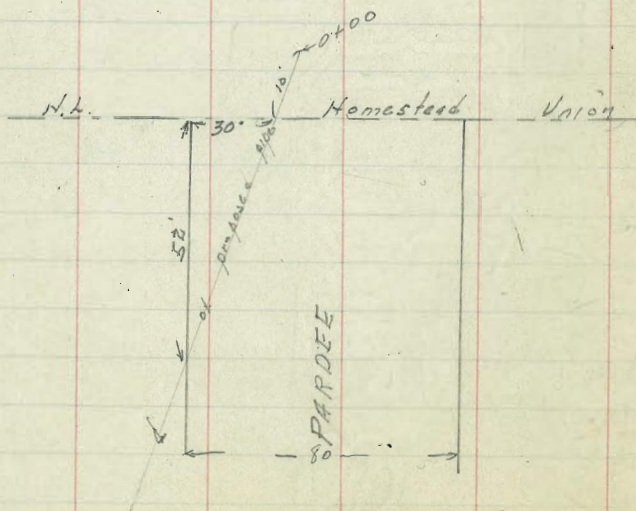
W		6.5	94.0
cb		5.1	95.4
1/4		4.3	96.2
c		3.9	96.6
set BM		4.04	96.46 ngils BM
1/4		3.4	97.1
cb		4.5	98.0
E		2.4	98.1

T.P. 6.98 94.68 12.30 87.70

Levels on proposed pipe shown below

Ad. 94.68

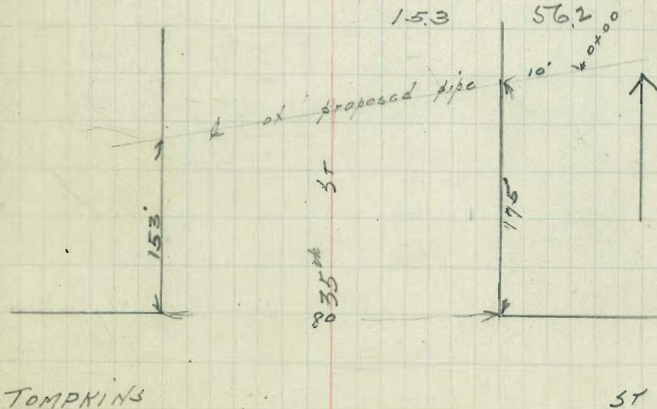
0+00	7.0	87.7
0+30	9.0	85.7
0+40	8.4	86.3
+61	8.9	85.8
+72	11.2	83.5
+92	12.6	82.1
1+00	13.0	81.7
1+10	13.8	80.9



73

Levels on pipe shown below
H.T. = 71.50

0+00	10.4	61.1
0+10 = EL. 35 th	11.2	60.3
0+30	11.2	60.3
0+40	9.8	61.7
0+46	8.0	63.5
0+56	8.3	63.2
0+60	11.8	59.7
0+80	14.3	57.2
1+04	15.3	56.2



12/5/21

Gregory
Moore
Miller
Shaw

CROSS SECTION OF
PARDEE ST
from N.L. Homestead Union
To N.L. Tompkins St

80' wide
14' cbs from
N. End To N.L. Shelter
60' wide
10' cbs
Shelter To Tompkins

94.68

74

94.68 from page 72
N.L. Homestead Union
For Culvert notes
see page 73

W	5.2	89.5
cb	7.0	87.7
+6	6.6	88.1
+9	7.6	87.1
1/4	7.6	87.1
set B.M.	8.09	86.59
+5	7.5	87.2
c	6.2	88.5
1/4	4.8	89.9
cb	3.3	91.4
E	0.3	94.4
E	0.7	94.0
cb	3.0	91.7
1/4	3.8	90.9
c	5.9	88.8
1/4	8.7	86.0
+5	8.7	86.0
+8	7.7	87.0
cb	7.6	87.1
W	6.6	88.1
W	8.9	85.8
cb	8.9	86.0

18.83 S on W
18.72 v - E

100 138.83 S on W
137.72 v - E

1/4	8.1	86.6
c	6.4	88.3
1/4	4.8	89.9
cb	3.5	91.2
E	1.7	93.0
E	2.3	92.4
cb	4.5	90.2
1/4	6.1	88.6
c	7.3	87.4
1/4	8.5	86.2
cb	9.5	85.2
+6	11.8	82.9
W	12.2	82.5
W	13.3	81.4
+7	10.6	84.1
cb	9.5	85.2
1/4	8.3	86.4
c	7.2	87.5
1/2	4.9	89.8
cb	2.7	92.0
E	0.6	94.1
E	1.2	93.5
cb	2.5	92.2

88.83 S on W
68.72 v - E

93.83 S on W
93.72 v - E

108.83 S on W
108.72 v - E

04.68

1/4		4.1	90.6
c		5.6	89.1
1/4		7.9	86.8
+4		9.3	85.4
cb		9.7	85.0
W		11.3	83.4
	128.83 S on W 128.72 - - E		
W		11.5	83.2
cb		8.8	85.9
+8		8.2	86.5
+10		7.0	87.7
1/4		6.4	88.3
e		5.1	89.6
1/4		3.5	91.2
cb		2.9	91.8
E		2.3	92.4
	143.83 S on W 153.83 - - E		
E		6.1	88.6
cb		5.9	88.8
1/4		5.4	89.3
c		6.3	88.4
1/4		8.0	86.7
+5		9.2	85.5
cb		9.6	85.1
W		12.2	82.5

60' wide on E
80' - - W

94.68

PARDEE

75

	14' S. on W 10' - - E		
W		13.0	81.7
cb		11.0	83.7
1/4		10.0	84.7
c		7.5	87.2
1/4		7.3	87.4
cb		7.4	87.3
E		7.4	87.3
	13' S. on W 10' - - E		
E		8.9	85.8
cb		9.0	85.7
1/4		8.7	85.0
c		9.0	85.7
1/4		10.8	83.9
+5		11.8	82.9
cb		12.6	82.1
W		13.6	81.1
	13' S. on W 10' - - E		
W		13.9	80.8
cb		12.9	81.8
1/4		12.0	82.7
c		10.5	84.2
1/4		10.1	84.6
cb		10.0	84.7
E		9.8	84.9

9468

$$\left. \begin{array}{l} 13' \text{ S. on W} \\ 10' \text{ - - E} \end{array} \right\} = \text{S. Quarter}$$

E	10.3	844
cb	10.7	840
$\frac{1}{4}$	11.0	837
c	11.5	832
$\frac{1}{4}$	12.2	825
cb	12.6	821
W	13.1	816

$$\left. \begin{array}{l} 13' \text{ S. on W} \\ 10' \text{ - - E} \end{array} \right\} = \text{S. Curb.}$$

W	12.2	825
cb	12.1	826
$\frac{1}{4}$	11.8	829
c	11.3	834
$\frac{1}{4}$	11.1	836
cb	10.9	838
E	10.5	842

$$\left. \begin{array}{l} 14' \text{ S. on W} \\ 10' \text{ - - E} \end{array} \right\} = \text{S. L. Shafter}$$

E	10.0	847
cb	10.4	843
$\frac{1}{4}$	10.4	843
c	10.8	839
$\frac{1}{4}$	11.0	837
cb	11.6	831
W	11.7	830

From HERE, St. 15 60' wide

9468

PARDEE

76

$$\left. \begin{array}{l} 15' \text{ S. on W} \\ 25' \text{ - - E} \end{array} \right\} = \text{O+00}$$

W	10.7	840
cb	10.7	840
$\frac{1}{4}$	10.2	845
c	9.6	851
$\frac{1}{4}$	9.2	853
cb	9.2	855
E	8.8	859

O+25

E	8.9	858
cb	9.1	856
$\frac{1}{4}$	9.2	855
c	9.0	857
$\frac{1}{4}$	9.2	855
$\frac{1}{4}$	9.6	851
cb	8.4	863
W	8.6	861

O+50

W	9.7	850
cb	9.9	848
$\frac{1}{4}$	9.9	848
c	8.9	858
$\frac{1}{4}$	9.2	855
cb	9.2	855
E	8.5	862

94.68

0+85

E	9.2	855
cb	9.4	853
1/4	9.5	852
c	9.4	853
1/4	10.1	846
cb	11.0	837
W	11.1	836

↓
1+10

W	12.5	822
cb	12.2	825
1/4	11.2	835
c	10.3	844
1/4	10.5	842
cb	10.1	846
E	9.6	851

1+35

E	10.8	829
cb	11.7	830
+2	12.2	825
1/4	12.1	826
c	11.9	828
1/4	12.6	821
T.P.	0.23	82.01
cb	1.1	80.9
W	1.2	80.8

82.01

PARDEE 77

1+60

W	2.9	79.1
cb	2.7	79.3
1/4	1.7	80.3
c	1.2	80.8
1/4	1.2	80.8
cb	1.0	81.0
E	0.0	82.0

↓
1+85

E	2.1	79.9
cb	3.1	78.9
+2	3.6	78.4
1/4	3.8	78.2
c	3.5	78.5
1/4	4.3	77.7
cb	5.1	76.9
W	5.2	76.8

↓
2+10

W	7.5	74.5
cb	7.5	74.5
1/4	6.6	75.4
c	5.8	76.2
1/4	5.7	76.3
cb	5.6	76.4
+2	4.9	77.1
E	4.3	77.7

82.01

2+35

E	64	75.6
+9	71	74.9
cb	7.7	74.3
1/4	7.9	74.1
c	8.1	73.9
1/4	8.8	73.2
cb	9.7	72.3
W	9.5	72.5

2+60

W	10.9	71.1
cb	10.7	71.3
1/4	10.5	71.5
c	10.2	71.8
1/4	9.9	72.1
cb	9.5	72.5
+1	8.7	73.3
E	8.2	73.8

2+85 on W }
 2+95 - E } = NL TOMPKINS

E	10.9	71.1
cb	12.1	69.9
1/4	12.6	69.4
c	12.6	69.4
1/4	12.7	69.3
cb	12.7	69.3
W	11.5	70.5

PARDEE 78

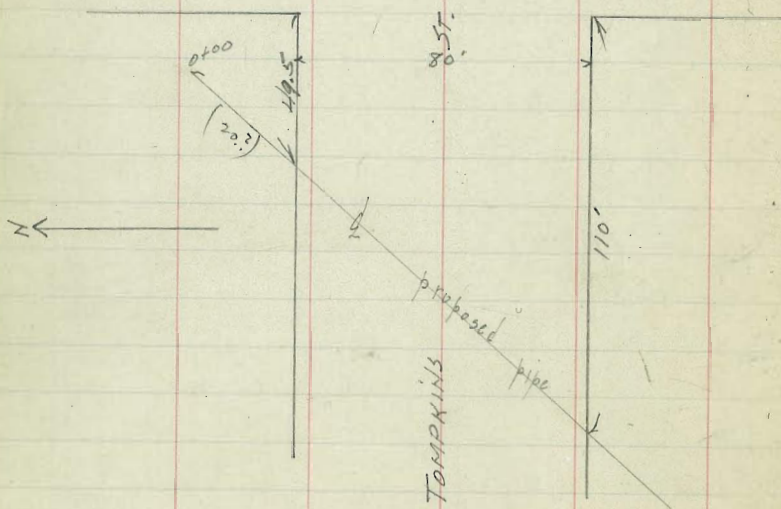
Levels on proposed pipe shown below

	0.86	62.70		61.84
	1.20	51.50	12.40	50.30
0+00			2.9	48.6
+13			3.3	48.2
+16			4.6	46.9
+20			4.8	46.7
+50			5.4	46.1
+60			+0.4	51.9
+77			0.5	51.0

continued next page.

35th St

St



51.50

79

spt SW Temp + Frm	+88	7.0	44.5
	1+00	8.2	43.3
	+25	10.9	40.6
	+45	10.6	40.9

Shaffer Turkey

E.L. Francois

+20
+40
+60
+70
+89
~~1+23~~ out out
1+23
1+45
1+60
1+85
2+00 = W.L. 35

E.L. 35

50
65
1+00
+10
+20
+30
+40
+55
+60

W.L. Pardac

35
E.L. Tompkins

45
55
80
1+00
+25
+40
+55
+62
+72
+82
+94

+45
+50
+75
3
+15
+35
+60
+85
+95
1+00
1+44.73

1+44.73

Pardac

150
175
150
175
235
260
285

W.L. Shaffer

0+10
0+30
0+50
0+70

+25
+43.53
+45.72

Francois St

N.L. Namastand Wing

+25
50
75
100
125
144.6 on E
144.55 W

W.L. Shaffer

31 Shaffer

+50
75
1+00
+25
+40
+41
+70
2+00
2+05
2+25
+150
+75

E 6.5 + 10 = 5.6

S.L. Tompkins

25
50
80
90
90.90 = Nail
96.52 = 5 -

+ 14.9 = Nail on E
+ 20 = 5
+ 30
+ 38
+ 40
+ 45
+ 75
+ 90
200.35 =

285.47

200.35

85.12

1.28

TOMIX

W.L. Fran

30
50
75

+16 Top on S

+50

+70 Top on N

E.L. Fran

25
55
80
85
140
125
+35
+45
+50
75
2

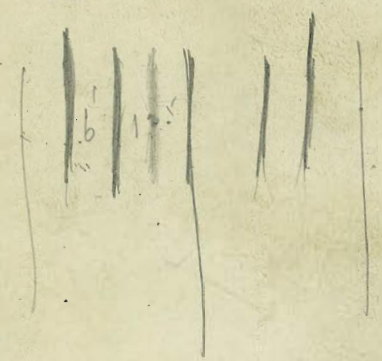
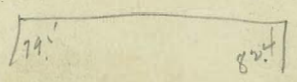
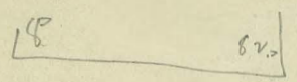
+55

150

30

180

400



18.5
21.5

00

21.5

27.5

40

52.5

58.5

80.0

33.75

46.25

137
 255
 270
 28
 21
 30' N 204.0
 12.5
 09375
 45
 09375
 14
 37500
 4375
 131250
 09375
 121875

80 F
 800 FG
 80 O
 300 GH
 75 H
 500 J
 80 K
 3000 L
 80 M
 300 J K
 80 K

118
 20
 80
 750
 385
 410
 300
 600
 300
 85.00
 21.21
 106.71
 1.67
 6/10.00
 20
 1st strad

1000
 475
 113
 6031
 3173.15
 250.15
 3493.36
 56
 1000
 150
 200
 150
 125
 125
 30
 164
 263
 12.468
 7921
 13+4781
 3427.5
 71
 163
 167
 330
 333
 338
 671
 200
 17900
 15612
 98952
 354112
 483060
 172
 180
 140
 26
 164
 26.64
 14
 175
 13.193
 48
 156
 15.6
 15
 200
 15
 406
 215
 40.8
 41.9
 43
 71.7
 44.4
 45
 21.3
 15
 43.9
 40
 46.2
 48.1
 49.8

179
 180
 185
 190
 195
 200
 205
 210
 215
 220
 225
 230
 235
 240
 245
 250
 255
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 265
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 275
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 285
 290
 295
 300

T F
 190
 195
 200
 205
 210
 215
 220
 225
 230
 235
 240
 245
 250
 255
 260
 265
 270
 275
 280
 285
 290
 295
 300

179
 270
 179
 137
 113
 43.76
 21376
 3876
**DISTANCES FROM CENTER OF ROADWAY FOR
 CROSS-SECTIONING.**
 Roadway 16 feet wide. Side Slopes 1 on 1 1/2.
 For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20-16)÷2 or 2 ft. added to 41.9=43.9. For slopes of 1 on 1 see inside of front cover.