

1051

DEEGEN
INC.

ENGINEER'S

FIELD BOOK

No. 408

1051

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide Side Slopes 1 on 1.
For Single Track Embankment.

H	0	1	2	3	4	5	6	7	8	9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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Cross Section of Road for proposed Paving from
Pacific Beach to La Jolla - Sections

12 } Davis
10 } Pulte
18 } Shannon

	8.25	26.05	17.80	B.M. Wm. N.E. Grand
T.P.	8.05	33.57	0.53	25.52
	0+00 = No Line Garnet			
W = 15		56		28.0
+5		54		28.2
C		51		28.5
+10		55		28.1
+15 E		6.0		27.6
	0+50			
E		58		27.8
+5		55		28.1
C		49		28.7
+10		49		28.7
W		49		28.7
	1+00			
W		40		29.2
+5		40		29.2
C		42		29.4
+10		48		28.8
E		48		28.8
	1+50			
E		43		29.3
+5		38		29.8
C		33		30.3
+10		36		30.0
W		38		29.8

	2+00	
W	32	30.4
+5	27	30.9
C	22	31.4
+10	28	30.8
E	35	30.1
	2+50	
E	31	30.5
+1	21	31.5
+5	19	31.7
C	14	32.2
+10	19	31.7
W	22	31.4
	2+70 S. Line Feldspar	
W	19	31.7
	14	32.2
C	11	32.5
	15	32.1
E	16	32.0
	4 Feldspar	
E	10	32.6
	08	32.8
C	04	33.2
	06	33.0
W	10	32.6
T.P.	800	41.10
	050	33.07

4.10
N. Line Feldspar

W	81	33.0
	78	33.2
C	72	33.9
	76	33.5
E	80	33.1

150

E	73	33.8
	71	34.0
C	65	34.6
	70	34.1
W	74	33.7

140

W	66	34.5
	61	35.0
C	57	35.4
	62	34.9
E	65	34.6

150

E	59	35.2
	57	35.7
C	50	36.1
	54	35.7
W	58	35.3

4.10

2

240

W	50	36.1
	46	36.5
C	43	36.8
	45	36.6
E	49	36.2

5450

E	40	37.1
	38	37.3
C	36	37.5
	40	37.1
W	41	37.0

2470 = 50 Line Emerald

W	38	37.3
	38	37.3
C	33	37.8
	36	37.6
E	39	37.2

Emerald

E	36	37.5
	30	38.1
C	29	38.2
	33	37.8
W	34	37.7

4410

No. Line Emerald

W		27	38.4
		28	38.3
C		24	38.7
		26	38.5
E		29	38.2

150

E		22	38.9
		20	39.1
C		19	39.4
		21	39.0
W		18	39.3

1400

W		10	40.1
		11	40.0
C		08	40.3
		09	40.2
E		12	39.8

T.P	9.48	49.85	0.73	40.37
-----	------	-------	------	-------

1450

E		91	40.8
		86	41.3
C		84	41.5
		91	40.8
W		91	40.8

4985

3

2400

W		85	41.4
		79	42.0
C		76	42.5
		77	42.2
E		81	41.8

2150

E		75	42.4
		68	43.1
C		66	43.3
		71	42.8
W		75	42.4

24700 S. Line Diamond

W		72	42.7
		68	43.1
C		64	43.5
		67	43.2
E		76	42.2

C Diamond

E		59	44.0
		55	44.4
C		55	44.4
		60	43.9
W		66	43.3 ✓

4985

No Line Diamond

W	56	44.3
	52	44.7
C	49	45.0
	47	45.2
E	52	44.7
	750	.
E	42	45.7
	38	46.1
C	37	46.2
	42	45.4
W	46	45.3
	1400	
W	37	46.2
	32	46.7
C	28	47.1
	27	47.2
E	30	46.9
	1450	
E	19	48.0
	16	48.3
C	15	48.4
	19	48.0
W	25	47.4

4985

4

2700

W	14	48.5
	07	49.2
C	03	49.6
	04	49.5
E	06	49.3
T.P.	10.33	59.84
	034	49.51
	2150	
E	93	50.5
	91	50.7
C	91	50.7
	91	50.4
W	103	49.5
	2470-S. Line Missouri	
W	94	50.4
	90	50.8
C	86	51.2
	86	51.2
E	84	51.0
	Missouri	
E	79	51.9
	78	52.0
C	79	51.9
	83	51.5
W	88	51.0

59.84
No Line Missouri

W	78	52.0
	7.1	52.7
C	68	53.0
	6.7	53.1
E	69	52.9
	1.50	
E	56	54.2
	5.4	54.4
C	56	54.2
	5.9	53.9
W	6.6	53.2
	1.40	
W	5.4	54.4
	4.7	55.1
C	4.4	53.4
	4.4	53.4
E	4.4	55.4
	1.40	
E	3.6	56.2
	3.3	56.5
C	3.3	56.5
	3.6	56.2
W	4.5	55.3

59.84
2+00

W	3.1	56.7	
	2.4	57.2	
C	2.3	57.5	
	2.1	57.7	
E	2.5	57.2	
	2+50		
E	1.2	58.6	
	0.9	58.9	
C	0.9	58.9	
	1.2	58.6	
W	2.0	57.8	
	2+70 S. Line Chalcedony		
W	1.7	58.1	
	0.9	58.9	
C	0.4	59.4	
	0.4	59.4	
E	0.6	59.2	
T.P. 9.50	68.88	64.6	59.88 ✓
	Chalcedony		
E	9.1	59.8	
	8.7	60.2	
C	8.6	60.3	
	8.8	60.1	
W	9.4	59.5	

68.88

No line Chalcedony

W	8.7	60.2
	8.0	60.9
C	7.9	61.2
	7.6	61.3
E	8.2	60.7

+50.

E	7.0	61.9
	6.6	62.3
C	6.6	62.3
	7.0	61.9
W	7.4	61.5

1400

W	6.5	62.4
	6.0	62.9
C	5.7	63.2
	5.8	63.1
E	6.0	62.9

1450

E	5.1	63.8
	4.8	64.1
C	4.7	64.2
	4.8	64.1
W	5.6	63.3

68.88

6

2+00

W	4.5	64.4
	3.9	65.0
C	3.7	65.2
	3.8	65.1
E	4.1	64.8

2450

E	3.2	65.7
	2.9	66.0
C	2.7	66.2
	3.0	65.9
W	3.4	65.5

2470 = S. line Low

W	3.1	65.8
	2.7	66.2
C	2.4	66.5
	2.6	66.3
E	3.0	65.9

ϕ Low

E	2.1	66.8
	1.8	67.1
C	1.7	67.2
	1.9	67.0
W	2.5	66.4

68.88

1/2 line Low

W			1.7	67.2
			1.3	67.6
C			1.1	67.8
			1.1	67.8
F			1.4	67.5
		+50		
E			0.8	68.1
			0.4	68.5
C			0.2	68.7
			0.5	68.4
W			1.0	67.9
T.P	8.72	77.39	0.21	68.67
		1400		
W			8.2	68.6
			8.5	68.9
C			8.1	69.3
			8.2	69.2
E			8.5	68.9
		1450		
E			8.2	69.2
			7.6	69.8
C			7.4	70.0
			7.7	69.7
W			8.0	69.4

7

2700

W			7.1	70.3
			6.8	70.6
C			6.5	70.9
			6.8	70.6
E			7.3	70.1
		2450		
E			6.5	70.9
			5.8	71.6
C			5.7	71.7
			6.0	71.4
W			6.1	71.0

2700 5/8 line Beryl

W			6.0	71.4
			5.6	71.8
C			5.2	72.2
			5.5	71.9
E			6.1	71.3
		2700 5/8 Beryl		
E			6.2	72.2
			4.8	72.6
C			4.5	72.9
			4.8	72.6
W			5.2	72.2

77.39
No Line Beryl

W			45	72.9
			41	73.3
C			37	73.7
			38	73.6
E			40	73.4
		+50		
E			31	74.3
			28	74.6
C			25	74.9
			30	74.4
W			34	74.0
Bm	10.82	86.60	161	75.78 Hub W side Sta 2200
		1400		
W			11.2	75.4
			11.0	75.6
C			10.5	76.1
			10.7	75.9
E			10.8	75.8
		+50		
E			9.8	76.8
			9.4	77.2
C			9.2	77.4
			9.4	77.2
W			9.6	77.0

86.60

8

2700

W			8.1	78.5
			8.0	78.6
C			7.8	78.8
			7.9	78.7
E			8.4	78.2
		+50		
E			7.0	79.3
			6.8	79.8
C			6.7	79.9
			6.8	79.8
W			6.8	79.8
		2700 S Line Millur		
W			6.3	80.3
			6.3	80.3
C			6.1	80.5
			6.2	80.4
E			6.4	80.2
		Wiltur		
E			5.6	81.0
			5.7	81.4
C			5.2	81.4
			5.3	81.3
W			5.3	81.3

86.60
N. Line Wilbur

W		4.2	87.2
		4.3	87.3
C		4.1	87.5
		4.2	87.4
E		4.5	87.1

+50

E		36	83.0
		30	83.6
C		30	83.6
		32	83.4
W		34	83.2

+100

W		2.2	84.4
		20	84.6
C		1.8	84.8
		1.8	84.8
E		2.3	84.3

+150

E		0.9	85.7	
		0.5	86.1	
C		0.5	86.1	
		0.7	85.9	
W		0.8	85.8	
T.P.	11.48	97.62	0.46	86.84

97.62

9

+100

W		10.2	87.2
		10.3	87.3
C		10.0	87.6
		10.1	87.5
E		10.3	87.3

+50

E		9.2	88.4
		8.8	88.8
C		8.5	89.1
		8.7	88.9
W		8.6	89.0

+170 = St. Loring

W		8.2	89.4
		8.2	89.4
C		8.0	89.6
		8.3	89.3
E		8.8	88.8

+64.08 =
(+64.07) St. Loring

E		6.7	90.9
		6.6	91.0
C		6.4	91.2
		6.5	91.1
W		6.6	91.0

97.62
N. Line Loring

W		50	926
		47	929
C		46	930
		48	928
		50	926
E		47	929
	+50		
E		35	941
		35	941
C		33	943
		35	941
W		38	938
	1700		
W		25	951
		23	951
C		21	955
		24	952
E		24	952
	1750		
E		13	963
		12	964
C		11	965
		13	963
W		14	962
T.P.	11.61	108.95	0.28
			97.34

10895

10

Σ100

W		11.2	97.7
		11.0	98.0
C		10.8	98.2
		11.1	97.9
E		11.1	97.9

Σ165 = S. Line Hyacinth

E		9.2	99.7
		9.1	99.9
C		8.7	100.3
		8.9	100.1
W		9.1	99.9

♀ Hyacinth - 70' st.

W		7.9	101.1
		7.6	101.4
C		7.5	101.5
		8.0	101.0
E		8.1	100.9

N. Line Hyacinth

E		6.5	102.5
		6.5	102.5
C		6.2	102.7
		6.4	102.6
W		6.6	102.4

10895

+50

W	51	103.9
	47	104.3
C	4.5	104.4
¹¹⁰ ₁₁₂	52	103.8
E	53	103.7
	43	104.7

1700

E	32	105.8
	34	105.6
C	3.0	106.0
	3.3	105.7
W	3.6	105.4

1750

W	19	107.1
	1.5	107.5
C	1.1	107.6
	1.8	107.2
E	1.9	107.1

2400

E	0.6	108.4
	0.6	108.6
C	0.0	109.0
	0.2	108.8
W	0.6	108.4
T.P.	110.6	119.80
	0.21	108.74

119.8

11

S46.5°S. Line Tourmaline

W	9.6	110.2
	9.2	110.6
C	9.0	110.8
¹¹⁶ ₁₁₃	9.6	110.2
E	9.4	110.4
	9.8	110.8

E Tourmaline - 70° St

E	7.0	112.8
	8.5	111.3
C	8.0	111.8
	8.2	111.6
W	8.8	111.0

N. Line Tourmaline

W	7.6	112.2
	7.3	112.5
C	7.1	112.7
	7.6	112.2
E	6.7	113.1

+50

E	5.5	114.3
	6.5	113.3
C	5.9	113.9
	6.1	113.7
W	6.5	113.3

119.80
1+00

N	5.1	114.7
	47	115.1
C	4.6	115.2
	51	114.7
F	4.2	115.4

1450

E	3.0	116.8
	34	116.4
C	2.9	116.9
	3.2	116.6
W	3.5	116.3

2+00

W	1.6	118.2
	1.4	118.4
C	1.2	118.6
	1.5	118.3
E	1.6	118.2

T.P.	11.66	<u>131.04</u> 2+50	0.42	119.38
E			10.8	120.2
			10.8	120.2
C			10.5	120.5
			10.7	120.3
W			10.8	120.2

131.04

2+65=8 Line Sapphire

W	10.4	120.6
	10.1	120.9
C	9.9	121.1
	10.2	120.8
E	10.4	120.6

♀ Sapphire - 70St

E	8.0	122.6
	8.8	122.2
C	8.0	122.6
	8.5	122.5
W	8.9	122.1

N Line Sapphire

W	7.2	123.8
	6.9	124.1
C	6.9	124.1
	7.3	123.7
E	6.4	124.6

+50

E	4.2	126.7
	4.9	126.1
C	4.9	126.1
	5.0	126.0
W	5.2	125.8

131.04
1400

W		3.2	127.8
		3.0	128.0
C		2.8	128.2
		2.1	127.9
E		2.5	128.5
	1450		
E		0.6	130.4
		0.8	130.2
C		0.9	130.2
		1.0	130.0
W		1.3	129.7
T.P.	595	135.94	105

2+16.77-PC-38.23 S of S. Line Turquoise

Note Curve divided into 4 equal parts - 26.81 each

W	$\left\{ \begin{array}{l} \Delta 89.55' \\ R 68.33 \\ T 68.23 \\ L 107.23 \end{array} \right.$	3.5	132.4
		3.3	132.6
C		2.6	132.3
		2.5	133.4
E		2.5	133.4
E		13	134.6
		13	134.6
C		14	134.5
		20	133.9
W		27	133.2

1st Sta on Curve

2nd Sta on Curve

W	26	133.3
	1.8	134.1
C	1.0	134.9
	0.5	135.4
E	0.2	135.7

3rd Sta on Curve

NE	0.2	135.7
	0.5	135.4
C	1.0	134.9
	2.0	133.9
SW	2.0	133.3

4th Sta = EC = 28.23 W of WL Cass

S	2.9	133.0
	2.3	133.6
C	1.4	134.5
	1.2	134.7
N	1.0	134.9

5th W of WL Cass

N	1.8	134.1
	1.6	134.3
C	2.0	133.9
	2.1	133.2
S	3.2	132.7

marked stone
Side road. 549

13590

1400

S	4.3	131.6
	3.8	132.1
C	3.1	132.8
	2.9	133.0
N	3.1	132.8

1450

N	4.3	131.6
	4.0	131.9
C	4.0	131.9
	4.5	131.4
S	5.1	130.8

2400

S	6.0	129.9
	5.5	130.4
C	5.1	130.8
	5.2	130.7
N	5.3	130.6

2450

N	6.7	129.2
	6.6	129.3
C	6.5	129.4
	6.8	129.1
S	7.3	128.6

13594

14

3400

S	8.1	127.8
	7.5	128.3
C	7.4	129.5
	7.5	128.4
N	7.8	128.1

3450

N	8.6	127.3
	8.4	127.5
C	9.2	127.6
	8.7	127.2
S	9.1	126.8

3492 = EL Bayard St - 40' St.

S	9.6	126.3
	9.3	126.6
O	8.9	127.0
	8.8	127.1
N	9.1	126.8

0401 = W. L. Bayard

N	10.1	125.8
	9.9	126.0
C	9.8	126.1
	10.0	125.9
S	10.4	125.5

13594

0+50

S			11.5	1244
			11.3	1246
C			11.1	1248
			11.3	1246
N			11.6	1243
T.P.	0.35	15.33	10.96	124.98 ✓
		1+00		
N			2.1	1232
			2.1	1232
C			1.8	1235
			2.0	1233
S			2.3	1230
		1+50		
S			3.8	121.5
			3.4	121.9
C			3.2	122.1
			3.4	121.9
N			3.7	121.6
		2+00		
N			4.9	120.4
			4.7	120.6
C			4.7	120.6
			5.2	120.1
S			5.6	119.7

15

2+50

S			7.2	118.1
			6.8	118.6
C			6.4	118.9
			6.5	118.8
N			6.7	118.6
		3+00		
N			8.7	116.6
			8.2	117.1
C			8.0	117.3
			8.4	116.9
S			8.7	116.6
		3+50		
S			10.0	115.3
			9.8	115.5
C			9.6	115.7
			9.8	115.5
N			10.0	115.3
		4+00		
N			11.4	113.9
			11.5	113.8
C			11.4	113.9
			11.8	113.5
S			12.2	113.1
T.P.	0.41	114.00	11.44	113.89 ✓

110.30

16

4+50

S	2.3	112.0
	2.4	111.9
C	2.1	112.2
	2.1	112.2
N	2.0	112.3

5+00

N	3.9	110.4
	3.9	110.4
C	4.0	110.3
	4.1	110.2
S	4.4	109.9

5+50

S	6.6	107.7
	6.2	108.1
C	6.0	108.3
	5.9	108.4
N	5.8	108.5

6+00

N	8.1	106.2
	7.8	106.5
C	7.5	106.8
	7.7	106.6
S	7.9	106.4

6+36.4 = E End bridge

11.2' S. of E - Cor bridge	8.2	106.1
C	8.1	106.2
8' N. of E - Cor bridge	8.2	106.1

6+63.4 = W End bridge

8.5' N. of E - Cor bridge	8.9	105.4
C	8.9	105.4
17.6' S. of E - Cor bridge	8.9	105.4

7+00 = EL Allison

S	10.2	104.1
	10.1	104.2
C	9.8	104.5
	9.3	105.0
N	8.8	105.5

Bd. 0.24 108.23 6.31 107.99 N. of post NE Allison

EL Allison - 60 St.

N	4.4	103.8
	4.8	103.4
C	4.7	103.5
	4.8	103.4
S	4.8	103.4

W L Allison = 0 100

S	6.0	102.2
	5.5	102.7
C	5.4	102.8
	5.7	102.5
N	5.6	102.7

108.23

0+50

N	6.9	101.3
	7.2	101.0
C	6.8	101.4
	6.8	101.4
S	7.0	101.2

1400

S	82	100.0
	80	100.2
C	80	100.2
	81	100.1
N	7.3	100.9

1450

N	7.9	100.3
	8.7	99.5
C	8.8	99.4
	8.8	99.4
S	9.0	99.2

2400

S	9.8	98.4
	9.3	98.9
C	9.3	98.9
	8.9	99.3
N	8.4	99.8

17

2450

H		96	98.6	
		10.0	98.2	
C		10.3	97.9	
		10.3	97.9	
S		10.5	97.7	
T.P.	0.08	98.06	10.25	97.98

3400

S		1.5	96.6
		1.2	96.9
C		1.1	97.0
		1.1	97.0
N		0.6	97.5

3450

N		2.1	96.0
		2.5	95.6
C		2.5	95.6
		2.5	95.6
S		2.9	95.2

4400

S		4.4	93.7
		4.1	94.0
C		3.9	94.2
		4.1	94.0
N		3.9	94.2

98.00
4+50

N ₁	4.6 5.2 5.2	93.5 92.9 92.9
C	5.0 5.1	93.1 93.0
S	5.4	92.7

5+00

S	7.1	91.0
	6.7	91.4
C	6.5	91.6
	6.7	91.4
N	7.0	91.1

5+50

N	8.8	89.3
	9.5	89.6
C	8.2	89.9
	8.5	89.6
S	8.8	89.3

6+00

S	10.5	87.6
	10.1	88.0
C	9.8	88.3
	10.3	87.8
N	10.7	87.4
T.P.	0.00	86.89
		11.83
		86.23

86.89
6+50

18

N	1.1	85.8
	1.0	85.9
C	0.7	86.2
	0.7	86.2
S	1.0	85.9

6+95± E.L. La Jolla RR. RotW - Taken parallel to Line of RotW

S	3.1	83.8
	3.1	83.8
C	3.1	83.8
	3.4	83.5
+16	3.3	83.6
N	2.4	84.5

La Jolla RR RotW - Top of rail.

N	3.55	83.34
	3.58	83.31
C	3.61	83.28
	3.65	83.24
S	3.62	83.27

W.L. La Jolla RR RotW - Taken parallel to Line of RotW = 0+00

S	0.7	83.2
	3.6	83.3
C	0.7	83.2
	4.0	82.9
N	2.4	84.5

86.89

0+50

N	4.7	82.2
	4.5	82.4
C	4.2	82.6
	4.3	82.6
S	4.6	82.3

1+00

S	5.6	81.3
	5.2	81.7
C	5.0	81.9
	5.5	81.4
N	5.9	81.0

1+50

N	7.0	79.9
	6.7	80.2
C	6.4	80.5
	6.6	80.3
S	6.9	80.0

2+00

S	8.3	78.6
	7.9	79.0
C	7.7	79.2
	8.2	78.7
N	8.4	78.5

19

2+17.65=P.C

N	9.0	77.9
	8.6	78.3
C	8.2	78.7
	8.4	78.5
S	8.8	78.1

3+50

S	9.5	77.4
	9.1	77.8
C	9.0	77.9
	9.6	77.3
N	9.9	77.0

3+00

N	11.7	75.2
	11.4	75.5
C	10.6	76.3
	10.4	76.5
S	10.5	76.4

TIP 2.16

78.32

10.73

76.16

3+50

S	3.2	75.1
	3.3	75.0
C	2.6	74.7
	4.3	74.0
N	4.6	73.7

78.32

4+00

N	5.4	72.9
	5.1	72.2
C	4.6	73.7
	4.6	73.7
S	4.7	73.6

4+50

S	6.0	72.3
	5.5	72.8
C	5.5	72.8
	5.6	72.7
N	5.8	72.5

4+62.85 = EC

E	5.9	72.4
	5.8	72.5
C	5.7	72.6
	5.8	72.5
N	6.1	72.2

5+00

W	6.6	71.7
	6.3	72.0
C	6.0	72.3
	6.0	72.3
E	6.1	72.2

20

5+50

E	6.4	71.9
	6.4	71.9
C	6.3	72.0
	6.7	71.6
W	6.9	71.4

Cor 14.1.

78.37

5.12

Mon 50 W 6 E C E Side

73.20 / 73.25

6+00

W	7.3	71.1
	7.0	71.4
C	6.5	71.9
	6.7	71.7
E	6.8	71.6

6+50

E	7.1	71.3
	7.0	71.4
C	6.9	71.5
	7.2	71.2
W	7.6	70.8

7+00

N	8.2	70.2
	7.8	70.6
C	7.3	71.1
	7.4	71.0
E	7.5	70.9

78.37
7+50

E		79	70.5
		78	70.6
C		79	70.5
		83	70.1
W		87	69.7
T.P.	391	74.07	821
		8400	70.16
W		49	69.2
		45	69.6
C		40	70.1
		40	70.1
E		42	69.9
	8450		
E		45	69.6
		44	69.7
C		44	69.7
		49	69.2
W		52	68.9
	9400		
W		45	69.6
+1		52	68.9
		5.1	69.0
C		45	69.6
		45	69.6
E		46	69.5

74.07
9+50

21

E		48	69.3
		46	69.5
C		45	69.6
		50	69.1
+W		51	69.0
W		44	69.7
	10400		
W		50	69.1
+1		53	68.8
		51	69.0
C		47	69.4
		46	69.5
E		47	69.4
	10450		
E		47	69.4
		46	69.5
C		47	69.4
		52	68.9
W		54	68.7
	11400		
W		55	68.6
		50	69.1
C		46	69.5
		46	69.5
E		46	69.5

74.07

11750

E		46	69.5
		46	69.5
C		46	69.5
		50	69.1
W		54	68.7

12400

W		54	68.7	
		50	69.1	
C		46	69.5	
		45	69.6	
E		45	69.6	
T.P.	4.28	73.94	4.01	69.66

12450

E		43	69.6
		43	69.6
C		44	69.5
		49	69.0
W		52	68.7

13400

W		54	68.5
		49	69.0
O		43	69.6
		43	69.6
E		44	69.5

22

13450

E		46	69.3
		45	69.4
C		44	69.5
		50	68.9
W		52	68.6

14400

W		50	68.3
		52	68.7
C		47	69.2
		47	69.2
E		49	69.0

14450

E		52	68.7
		49	69.0
C		49	69.0
		56	68.3
W		59	68.0

15400

W		58	68.1
		54	68.5
C		47	69.2
		49	69.0
W		51	68.8

$$\frac{7394}{15+50}$$

E	48	691
	46	69.3
C	42	69.5
	30	68.9
W	53	68.6
	1.6+0.0	
W	48	69.1
	44	69.5
C	39	70.0
	40	69.9
E	44	69.5
	1.6+3.0	
E	36	70.3
	34	70.5
C	33	70.6
	37	70.2
N	41	69.8
	1.7+0.0	
W	32	70.5
	31	70.8
C	26	71.3
	29	71.0
E	31	70.8

17+50

E	26	71.5
	22	71.7
C	22	71.7
	26	71.3
W	49	71.0
T.P. 10.14	81.78	2.00
	18+0.0	71.64 ✓
W	106	71.8
	96	72.2
C	92	72.6
	92	72.6
E	93	72.5
	1.8+4.8 0.0 SL. Bird Rock = 0+0.0	
E	84	73.4
	83	73.5
C	83	73.5
	87	73.1
W	90	72.8
	0+5.0	
W	78	74.0
	75	74.3
C	72	74.6
	74	74.4
E	75	74.3

P1.73

3+0.0

E	3.1	786
	3.1	786
C	2.9	788
	2.9	788
W	3.0	787

3+50

W	4.0	77.7
	3.9	77.8
C	3.8	77.9
	3.8	77.9
E	3.9	77.8

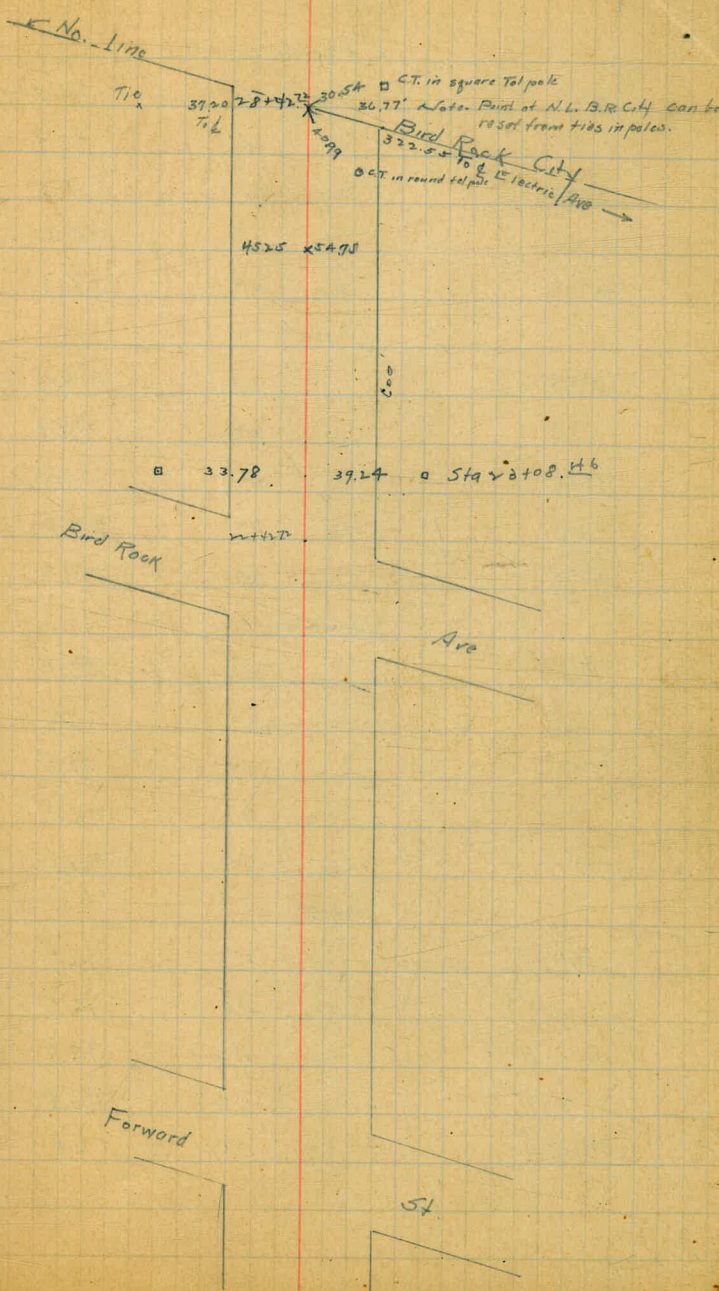
4+00

E	4.7	77.0
	4.6	77.1
C	4.6	77.1
	4.8	76.9
W	5.0	76.7

4+50

W	5.7	76.0
	5.6	76.1
C	5.4	76.3
	5.3	76.4
E	5.5	76.2

T.P.	0.77	77.15	5.35	76.38
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7215

5+00

E	17	75.5
	15	75.7
C	16	75.6
	18	75.4
W	19	75.3

5+50

W	28	74.4
	26	74.6
C	24	74.8
	24	74.8
E	25	74.7

6+00

E	35	73.7
	34	73.8
C	34	73.8
	36	73.6
W	39	73.3

6+50

W	48	72.4
	46	72.6
C	43	72.9
	43	72.9
E	44	72.8

7215

7+00

E	53	71.9
	51	72.1
C	49	72.3
	53	71.9
W	56	71.6

7+50

W	65	70.7
	62	71.0
C	57	71.5
	57	71.5
E	58	71.4

7+99 P.O.

E	63	70.9
	60	71.2
C	61	71.1
	65	70.7
W	69	70.3

8+50

W	70	70.7
	67	70.5
C	61	71.1
	67	71.0
E	63	70.9

26

77.15

9+00

E	62	71.0
	62	71.0
C	63	70.9
	68	70.4
W	71	70.1

9+50

W	67	70.5
	65	70.7
O	60	71.2
	60	71.2
E	62	71.0

10+00

E	59	71.3
	58	71.4
C	57	71.5
	61	71.1
W	60	70.8

10+50

W	60	71.2
	58	71.4
C	54	71.8
	56	71.6
E	58	71.4

T.P.

7.28

78.82

5.61

71.52

78.82

27

11+00

E	67	72.1
	66	72.2
C	66	72.2
	68	72.0
W	70	71.8

11+50

W	63	72.5
	61	72.7
C	60	72.8
	61	72.7
E	62	72.6

12+00

E	58	73.0
	56	73.2
C	56	73.2
	57	73.1
W	59	72.9

12+50

W	55	73.3
	51	73.7
O	50	73.8
	52	73.6
E	54	73.4

78.82
13400

E	5.1	73.7
	50	738
C	4.7	74.1
	50	73.8
W	5.5	73.3

13450

W	5.4	73.4
	48	74.0
C	4.4	74.4
	4.7	74.1
E	4.9	73.9

14400

E	4.7	74.1
	4.5	74.3
C	4.2	74.6
	4.5	74.3
W	5.0	73.8

141345 POC - 5 L Forward

W	4.8	74.0
	4.3	74.5
C	4.0	74.8
	4.4	74.4
E	4.6	74.2

28

15700

E	4.6	74.2
	4.2	74.6
C	3.9	74.9
	4.2	74.6
W	4.6	74.2

15750

W	4.7	74.1
	4.3	74.5
C	4.0	74.8
	4.3	74.5
E	4.7	74.1

16400

E	4.6	74.2	
	4.3	74.5	
C	4.0	74.8	
	4.4	74.4	
W	4.7	74.1	
T. P. 6.20	80.69	4.33	74.49 ✓

1613297 = FCC.

W	6.6	74.1
	6.2	74.5
C	5.8	74.9
	6.1	74.6
E	6.3	74.4

80.69

17+00

E	60	74.7
	58	74.9
C	56	75.1
	61	74.6
W	62	74.3

17+50

W	62	74.5
	59	74.8
C	53	75.4
	56	75.1
E	57	75.0

18+00

E	53	75.4
	52	75.5
C	50	75.7
	55	75.2
W	59	74.8

18+50

W	56	75.1
	52	75.5
C	46	76.1
	47	76.0
E	48	75.9

29

19+00

E	48	75.9
	46	76.1
C	45	76.2
	50	75.7
W	53	75.4

19+50

W	50	75.7
	47	76.0
C	42	76.5
	43	76.4
E	45	76.2

20+00

E	42	76.5
	41	76.6
C	39	76.8
	43	76.4
W	45	76.2

20+50

W	36	77.1
	36	77.1
C	34	77.3
	36	77.1
E	39	76.8

80.69

21400

E	3.4	77.3
	3.2	77.5
C	2.9	77.8
	3.4	77.3
W	3.6	77.1

21450

W	2.7	77.8
	2.8	77.9
C	2.5	78.2
	2.6	78.1
E	2.6	78.1

22400

E	1.7	79.0
	1.6	79.1
C	1.6	79.1
	2.0	78.7
W	2.0	78.7

T.P. 524 84.04 1.89 78.80

Moq N.W. Bird Rock S.

3.21 80.83

22450

W	4.5	79.5
	4.4	79.6
C	4.0	80.0
	4.1	79.9
E	4.2	79.8

84.04

30

23700

E	3.7	80.6
	3.5	80.5
C	3.4	80.6
	3.8	80.2
W	4.1	79.9

23750

W	4.2	79.8
	4.1	79.9
C	3.7	80.3
	3.6	80.4
E	3.7	80.3

24400

E	4.2	79.8
	4.1	79.9
C	4.3	79.7
	4.6	79.4
tr	4.7	79.3
W	4.5	79.5

24450

W	4.8	79.2
	4.9	79.1
C	4.7	79.3
	4.5	79.5
E	4.6	79.4

8404

25700

E	48	79.2
	49	79.1
C	51	78.9
	52	78.6
W	52	78.8

25750

W	55	78.5
	54	78.6
C	53	78.7
	53	78.7
E	54	78.6

26400

E	55	78.5
	54	78.6
C	55	78.5
	57	78.3
W	57	78.3

26450

W	60	78.0
	62	77.8
C	60	78.0
	58	78.2
E	59	78.1

27700

E	65	77.5
	64	77.6
C	65	77.5
	68	77.2
W	66	77.4

27750

W	70	77.0
	72	76.8
C	68	77.2
	67	77.3
E	68	77.2

T.P. 070 77.96

6.78 77.26

28400

E	11	76.9
	09	77.1
C	08	77.2
	12	76.8
W	13	76.7

28450 = No. Line B. Rock City - 0400

W	15	76.5
	14	76.6
C	12	76.8
	12	76.8
E	13	76.7

77.96

0+50

E	22	75.8
	21	75.9
C	22	75.8
	24	75.6
W	26	75.4

1+00

W	37	74.3
	36	74.4
C	34	74.6
	32	74.8
E	33	74.7

1+50

E	45	73.5
	47	73.6
C	44	73.6
	46	73.4
W	49	73.1

2+00

W	59	72.1
	53	72.4
C	54	72.6
	53	72.7
E	55	72.5

32

77.96

2+50

E	64	71.6
	61	71.9
C	62	71.8
	63	71.7
W	64	71.6

3+00

W	70	71.0
	67	71.3
C	66	71.6
	65	71.5
E	65	71.5

3+50

E	66	71.4
	65	71.5
C	66	71.4
	69	71.1
W	72	70.8

4+00

W	75	70.5
	71	70.9
C	68	71.2
	66	71.4
E	68	71.2

TIP 4.03 77.70

4.29

73.67 Nailpole Street

77.70

4+50

E	62	71.5
	61	71.6
C	61	71.6
	65	71.2
W	68	70.9

5+00

W	64	71.3
	62	71.5
C	58	71.9
	58	71.9
E	58	71.9

5+50

E	55	72.2
	55	72.2
C	55	72.2
	59	71.8
W	61	71.6

6+00

W	55	72.2
	55	72.2
C	51	72.6
	50	72.7
E	52	72.5

77.70

33

6+50

E	49	72.8
	48	72.9
C	47	73.0
	51	72.6
W	53	72.4

7+00

W	49	72.8
	47	73.0
C	44	73.3
	43	73.4
E	41	73.6

7+50

E	43	73.4
	41	73.6
C	39	73.8
	43	73.4
W	44	73.3

8+00

W	41	73.6
	39	73.8
C	34	74.3
	34	74.3
E	39	73.8

77.70

8+50

E	34	74.3
	30	74.7
C	30	74.7
	34	74.3
W	36	74.1

9+00

W	33	74.4
	30	74.7
C	26	75.1
	25	75.2
E	29	74.8

9+50

E	27	75.0
	24	75.3
C	23	75.4
	27	75.0
W	29	74.8
T.P.	5.70	10.89
		2.51
		75.19

10+00

W	61	74.8
	58	75.1
C	53	75.6
	55	75.4
E	57	75.2

80.89

10+50

E	54	75.5
	52	75.7
C	50	75.9
	56	75.3
W	58	75.1

11+00

W	56	75.3
	54	75.5
C	48	76.1
	50	75.9
E	49	76.0

11+50

E	50	75.9
	49	76.0
C	47	76.2
	51	75.8
W	56	75.3

12+00

W	55	75.4
	53	75.6
C	47	76.2
	47	76.2
E	48	76.1

8089

12+50

E	48	76.1
	47	76.2
C	45	76.4
	51	75.8
W	55	75.4

13+00

W	53	75.6
	50	75.9
C	43	76.6
	45	76.4
E	42	76.5

13+50

E	45	76.4
	44	76.5
C	42	76.7
	47	76.2
W	51	75.8

14+00

W	47	76.2
	42	76.5
C	40	76.9
	41	76.8
E	44	76.5

8089

35

14+50

E	43	76.6
	39	77.0
C	37	77.2
	42	76.7
W	44	76.5

15+00

W	41	76.8
	39	77.0
C	35	77.4
	37	77.2
E	41	76.8

15+50

E	38	77.1	
	35	77.4	
C	31	77.8	
	36	77.3	
W	37	77.2	
T.P. 642	83.83	34.8	77.41

16+00

W	64	77.4
	62	77.6
C	57	78.1
	61	77.7
E	64	77.4

P383

16+50

E	61	77.7
	59	77.9
C	53	78.5
	58	78.0
W	60	77.8

17+00

D	59	77.9
	57	78.1
C	52	78.6
	56	78.2
E	58	78.0

17+50

E	54	78.4
	52	78.6
C	49	78.9
	53	78.5
W	55	78.3

18+00

W	52	78.6
	50	78.8
C	47	79.1
	50	78.8
E	52	78.6

8383

36

18+50

E	50	78.8
	48	79.0
C	46	79.2
	49	78.9
W	52	78.6

19+00

W	52	78.6
	50	78.8
C	46	79.2
	49	78.9
E	52	78.6

19+50

E	50	78.8
	49	78.9
C	48	79.0
	51	78.7
W	53	78.5

20+00

W	51	78.4
	52	78.6
C	49	78.9
	50	78.8
E	51	78.7

83.83

20+50

E	51	78.7
	50	78.8
C	49	79.0
	51	78.7
W	52	78.6

21+00

W	57	78.1
	54	78.4
C	50	78.8
	51	78.7
E	53	78.5

21+50

E	53	78.5
	51	78.7
C	51	78.7
	54	78.4
W	58	78.0
T.P	5.58	83.83
	5.58	78.25

22+00

W	57	78.1
	53	78.5
C	51	78.7
	52	78.6
E	52	78.6

83.83

37

22+50

E	53	78.5
	52	78.6
C	51	78.7
	53	78.5
W	59	77.9

23+00

W	58	78.0
	55	78.3
C	51	78.7
	53	78.5
E	53	78.5

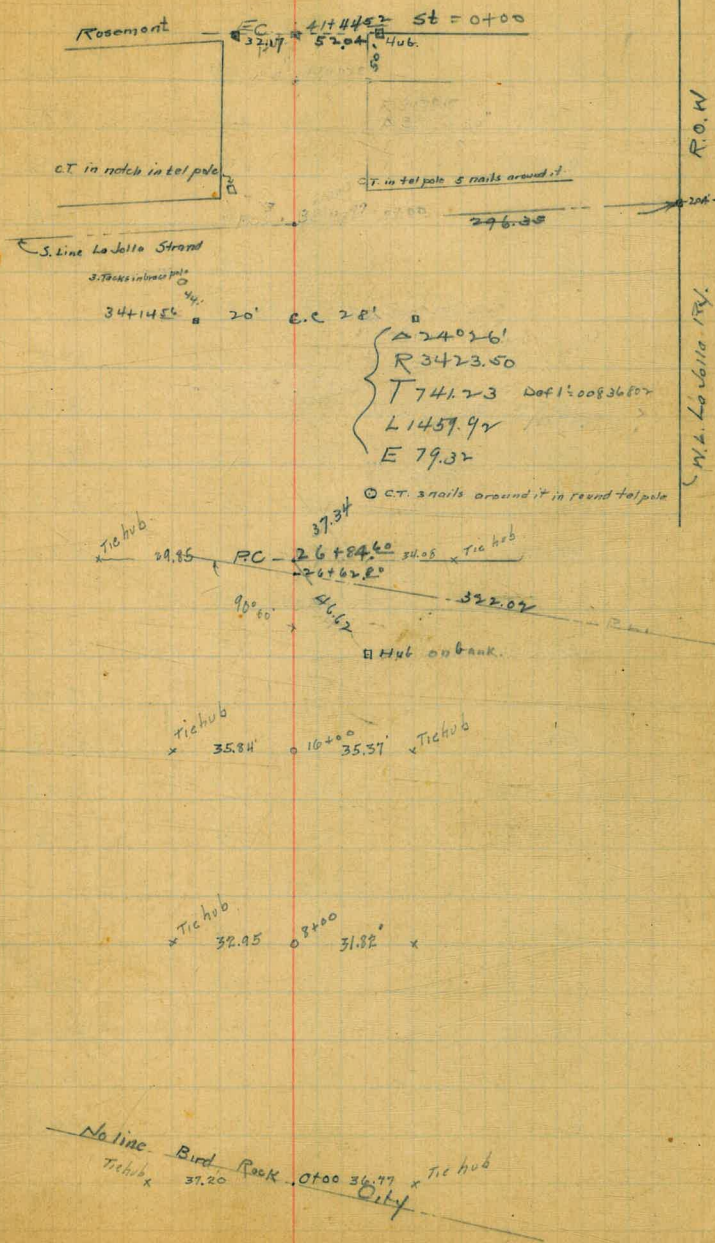
23+50

E	51	78.7
	51	78.7
C	50	78.8
	53	78.5
W	57	78.1

24+00

W	56	78.4
	51	78.7
C	46	79.2
	47	79.1
E	47	79.1

		83.83		
		24+50		
E		44	79.4	
		43	79.5	
C		42	79.6	
		46	79.2	
W		50	78.8	
		25+00		
W		47	79.1	
		44	79.4	
C		40	79.8	
		41	79.7	
E		42	79.6	
		25+50		
E		41	79.7	
		39	79.9	
C		38	80.0	
		41	79.7	
W		43	79.5	
		26+00		
W		43	79.5	
		40	79.8	
C		37	80.1	
		37	80.1	
E		39	79.9	
T.P.	3.80	85.49	2.14	81.69 Nail pole Star



8549

20+50

E	55	80.0
	52	80.1
C	52	80.1
	56	79.9
W	59	79.6

26+8450

W	57	79.8
	55	80.0
C	53	80.2
	52	80.3
C	54	80.1

27+01

E	52	80.1
	52	80.3
C	52	80.3
	55	80.0
W	57	79.8

27+50

W	56	79.9
	53	80.2
C	51	80.4
	50	80.5
E	52	80.3

8549

39

28+00

C	50	80.5
	49	80.6
C	49	80.6
	51	80.4
W	53	80.2

29+50

W	51	80.4
	49	80.6
C	46	80.9
	47	80.8
E	49	80.6

29+00

E	47	80.8
	45	81.0
C	43	81.2
	45	81.0
W	48	80.7

29+50

W	46	80.9
	44	81.1
V	42	81.3
	44	81.1
E	46	80.9

8549

30400

E	42	81.3
	40	81.5
C	38	81.7
	40	81.5
W	42	81.3

30450

W	36	81.9
	33	82.2
C	32	82.3
	37	81.8
E	38	81.7

31400

Q	34	82.1
	31	82.4
O	28	82.7
	30	82.5
W	33	82.2
T.P.	5.00	87.76
		2.73
		82.76

31450

W	47	83.1
	46	83.2
C	46	83.2
	49	82.9
E	52	82.6

87.76

32400

E	49	82.9
	46	83.2
C	42	83.6
	42	83.6
W	42	83.4

32450

W	43	83.5
	41	83.7
C	42	83.6
	45	83.3
E	47	83.1

33400

E	47	83.1
	44	83.4
C	41	83.7
	42	83.6
W	43	83.5

33450

W	46	83.2
	46	83.2
C	46	83.2
	49	82.9
E	51	82.7

87.76
34+00

E	55	82.3
	54	82.4
C	52	82.6
	52	82.6
W	54	82.4
	34+50	
W	62	81.6
	62	81.6
C	60	81.8
	62	81.6
E	62	81.6
	35+00	
E	72	80.6
	71	80.7
C	71	80.7
	72	80.4
113	75	80.3
W	72	80.6
	35+50	
W	83	79.5
	84	79.4
C	82	79.6
	83	79.5
E	84	79.4

87.76

41

36+00

E		92	78.6
		91	78.7
C		88	79.0
		90	78.8
W		91	78.7
T.P	373	82.48	9.01
		36+50	78.75
W		43	78.2
		42	78.3
C		39	78.6
		42	78.3
E		44	78.1
		37+00	
E		48	77.7
		45	78.0
C		43	78.2
		45	78.0
W		48	77.7
		37+50	
W		53	77.2
		50	77.5
C		46	77.9
		49	77.6
E		51	77.4

	82.48		
	38+00		
E	49	77.6	
	49	77.6	
C	48	77.7	
	51	77.4	
W	53	77.2	
	38+50		
W	55	77.0	
	51	77.4	
C	48	77.7	
	51	77.4	
E	52	77.3	
	39+00		
E	57	77.1	
	52	77.3	
C	50	77.5	
	55	77.0	
W	59	76.6	
	39+50		
W	57	76.8	
	54	77.1	
C	46	77.9	
	47	77.8	
E	49	77.6	

	82.48		
	40+00		
E	42	78.3	
	42	78.3	
C	44	78.1	
	50	77.5	
W	56	77.1	
	40+50		
W	46	77.9	
	43	78.2	
C	37	78.8	
	36	78.9	
E	36	78.9	
	T.P. 4.09	82.72	385
			78.63
	41+00		
E	32	79.5	
	33	79.4	
C	34	79.3	
	40	78.7	
W	43	78.4	
	41+4#5	EC: 5.1. Rosement on east - 0+00	
W	40	78.7	
	38	78.9	
C	32	79.5	
	32	79.5	
E	31	79.6	

82.72

0 + 50

E	3.3	79.4
	3.2	79.5
C	3.3	79.4
	3.8	78.9
W	4.2	78.5

1 + 00

W	4.6	78.1
	4.2	78.5
C	3.6	79.1
	3.5	79.2
E	3.6	79.1

1 + 50

E	4.1	78.6
	4.1	78.6
C	4.2	78.5
	4.7	78.0
W	5.1	77.6

2 + 00

W	5.8	76.9
	5.4	77.3
C	5.0	77.7
	5.0	77.7
E	5.0	77.7

82.72

43

2 + 50

E	5.8	76.9
	5.7	77.0
C	5.8	76.9
	6.1	76.6
W	6.7	76.0

3 + 00

W	7.2	75.5
	6.7	76.0
C	6.5	76.2
	6.4	76.3
E	6.5	76.2

3 + 50

E	7.2	75.5
	7.3	75.4
C	7.3	75.4
	7.5	75.2
W	8.0	74.7

T.P. 0.82

75.91

76.3

75.09

4 + 00

W	2.3	73.6
	1.8	74.1
C	1.5	74.4
	1.5	74.4
E	1.5	74.4

75.91

4+50

E	21	73.5
	25	73.4
C	25	73.4
	30	72.9
W	33	72.6

5700

W	42	71.7
	40	71.9
C	38	72.1
	39	72.0
E	38	72.1

5+50

E	51	70.8
	55	70.4
C	56	70.3
	55	70.4
W	57	70.2

6+00

W	77	68.2
	74	68.5
C	77	68.2
	78	68.1
E	65	69.4

T.P. 0.07

71.45
Cor M.
71.37

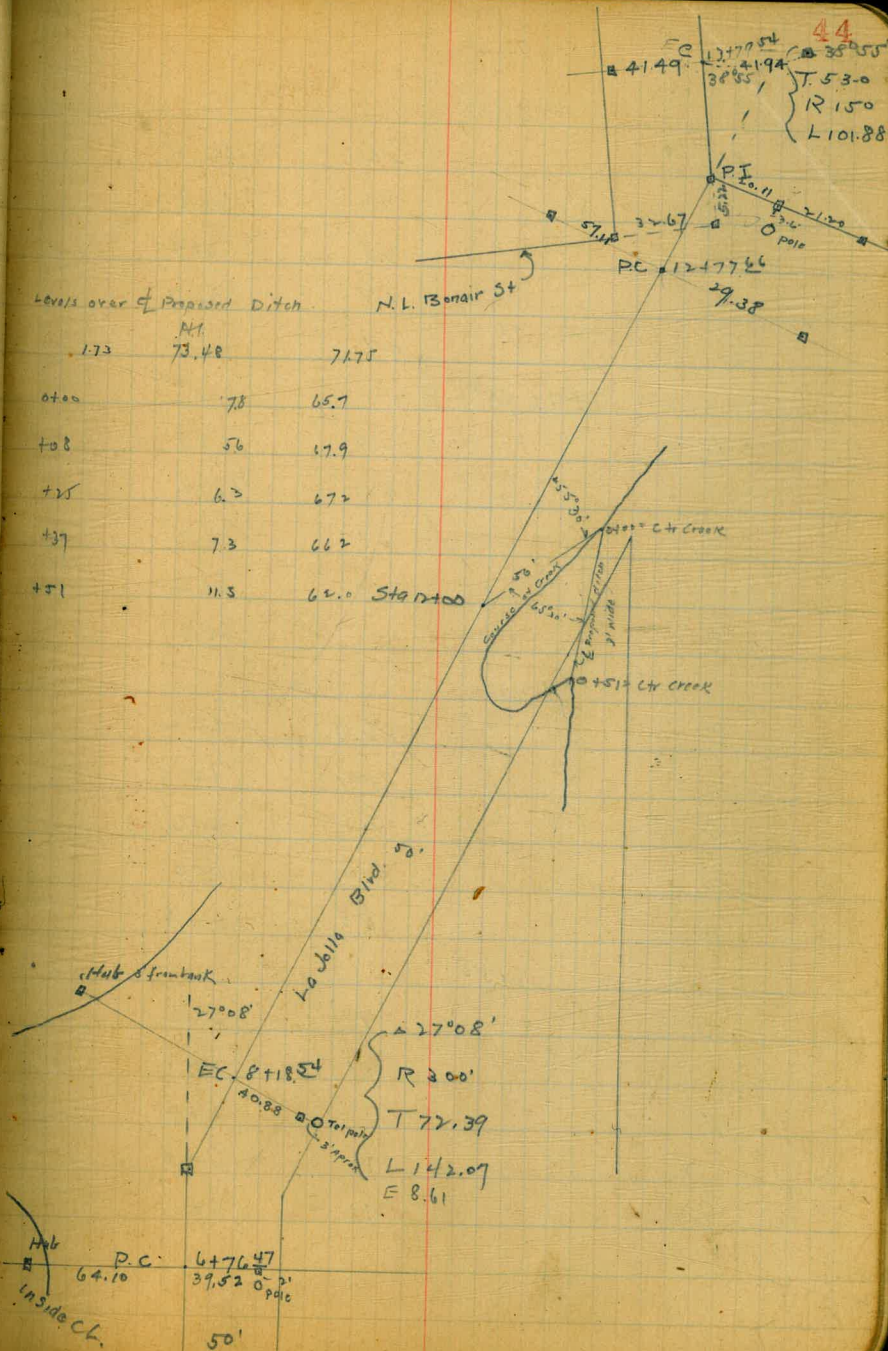
4.53	71.39
7.51	68.94

Cor Return
NE Gravilla

B.M. Plg incl NW Gravilla

Levels over Proposed Ditch

173	73.48	71.75
0+00	78	65.7
+08	56	67.9
+25	62	67.2
+37	73	66.2
+51	11.5	62.0



71.37

6+50

E	46	66.8
	46	66.8
C	45	66.9
	47	66.7
W	47	66.7

6+76 ~~47~~ P.C

W	55	65.9
	53	66.1
C	51	66.3
	52	66.2
E	55	65.9

7+0

E	60	65.4
	59	65.5
O	58	65.6
	60	65.4
W	65	64.9

7+50

W	78	63.6
	77	63.7
C	74	64.0
	72	64.2
E	73	64.1

71.37

8+00

E	82	63.2
	82	63.2
C	82	63.0
	84	63.0
W	85	62.9

8+10⁵⁴ = E.C.

20W	11.2	60.2
15W	10.2	61.2
10	8.9	62.5
C	8.5	62.9
10	8.3	63.1
E	8.2	63.2

8+50

E	8.4	63.0
	8.3	63.1
e	8.4	63.0
+8	8.5	62.9
+10	9.0	62.4
W-15	10.0	61.4
+17	11.0	60.4
+30	18.0	53.4

T.P	8.97	71.95	8.39	62.98
-----	------	-------	------	-------

71.95

46

9+00

W	9.3	62.7
	9.3	62.7
C	8.9	63.1
	8.9	63.1
E	8.8	63.2

9+50

E	7.5	64.5
	7.6	64.4
C	7.7	64.3
	7.8	64.2
W	7.9	64.1

10+00

W	6.4	65.6
	6.4	65.6
C	6.1	65.6
	6.3	65.5
	6.1	65.9
	6.2	65.8
E	6.3	65.7

10+50

E	5.3	66.7
	5.2	66.8
	4.6	67.4
	5.1	66.9
	5.0	67.0
W	4.9	67.1

71.95

11700

W		32	68.6
		34	68.6
C		37	68.3
+5		37	68.6
+10		37	68.7
+15		37	68.3
E		43	67.7
+5		49	67.1
11750			
E+20		30	69.0
+15		27	69.3
+10		23	69.7
C		18	70.2
+1		21	69.9
+10		18	70.2
W +15		19	70.1
T.P	816	79.91	0.20
71.75 - Stake 1250 Stake 12			
11772			
E		91	70.8
		85	71.4
C		90	70.9
		91	70.8
W		92	70.7

47

79.91

11787

W		86	71.3
		85	71.4
C		85	71.4
+10		87	71.2
+11		90	70.9
+18		160	63.9
+27		160	63.9
+28		122	67.7
E+35		145	65.4
12700			
35E		130	66.9
29		120	67.3
24"		148	65.1
15"		112	68.7
10"		97	70.2
7"		82	71.7
E		79	72.0
+10		80	71.9
W		81	71.8

79.91

12+50

W	62	73.7
	62	73.7
C	64	73.5
	72	72.7
E	79	72.0
+10	90	70.9
12+77.66 = AC		
E+10	72	72.7
E	65	73.4
	63	73.6
C	53	74.6
	51	74.8
W	53	74.6
13+00		
W	49	75.1
	44	75.5
C	46	75.3
	45	75.4
E	45	75.4
13+50		
E	37	76.2
	29	76.0
C	39	76.0
	40	75.9
W	42	75.7

79.91

13+79.54 = EC

W	39	76.0
	38	76.1
C	36	76.3
	35	76.4
E	34	76.5
14+00		
E	26	77.3
	29	77.0
C	31	76.8
	34	76.5
W	34	76.3
14+50		
W	26	77.3
	23	77.6
C	21	77.8
	21	77.5
	21	77.8
E	12	78.7
15+00		
E	11	78.8
	13	78.6
C+9	19	78.0
C	16	78.3
	20	77.9
W	23	77.6

79.91
15+50

W		1.9	78.0	
		1.7	78.2	
C		1.3	78.6	
C+11		1.5	78.4	
E		1.0	78.9	
E		0.4	79.5	
T.P.	5.62	84.27	1.26	78.65
16+00				
E		5.0	79.3	
11'E		5.0	79.3	
		5.6	78.7	
C		5.4	78.9	
		5.8	78.5	
W		6.0	78.3	
16+50				
W		5.6	78.7	
		5.5	78.8	
C		5.1	79.2	
+9		5.2	79.1	
		4.7	79.6	
C		4.4	79.9	
17+00				
E		4.6	79.7	
		5.1	79.2	
C		5.1	79.2	
		5.4	78.9	
W		5.6	78.7	

84.27
17+50

W		5.2	79.1
		5.2	79.1
C		4.6	79.7
		4.8	79.5
C		4.6	79.7
18+00			
E		3.9	80.4
		4.9	79.4
C		4.5	79.8
		5.2	79.1
W		5.3	79.0
18+50			
W		5.4	78.9
		5.2	79.1
C		4.7	79.6
		4.9	79.4
E		4.3	80.0
19+00			
E		4.0	80.3
		5.0	79.5
C		4.8	79.5
		5.2	79.1
W		5.5	78.8

Cor. 147.
84.30

3.08

81.19 81.22

B.M. Spk Pole S.E. Westburne

84.30

19+50

W			5.3	79.0
			5.2	79.1
C			4.8	79.5
			5.0	79.3
E			4.3	80.0
TIP	2.32	81.85	4.77	79.53
		20+00		
E			1.7	80.2
IS'ECT			1.9	80.0
			2.6	79.3
C			2.3	79.6
			2.7	79.2
W			3.0	78.9
		20+50		
W			3.3	78.6
			3.0	78.9
C			2.7	79.2
			2.8	79.1
E			2.2	79.7
		21+00		
E			2.4	79.5
			3.4	78.5
C			3.2	78.7
			3.7	78.2
W			4.0	77.9

81.85

50

21+50

W			4.7	77.2
			4.3	77.6
C			3.9	78.0
			4.3	77.6
E			3.7	78.2
		22+00		
E			4.6	77.3
			5.2	76.7
C			4.7	77.2
			5.1	76.8
W			5.5	76.4
		22+50		
W			6.4	75.5
			6.1	75.8
C			5.7	76.2
			6.0	75.9
E			5.5	76.4
		23+00		
E			6.8	75.1
			7.4	74.5
C			6.9	75.0
			7.2	74.7
W			7.5	74.4

	81.85		
	25+50		
W		85	73.4
		83	73.6
C		81	73.8
		86	73.3
E		80	73.9
	24+50		
25' ECH		110	70.9
E		10.4	71.5
11' ECH		9.0	72.9
		9.2	72.5
C		9.1	72.8
		9.2	72.7
W		9.5	72.4
T.P.	375	76.65	89.5
	24+20		72.90
W		46	72.1
		4.3	72.4
C		4.1	72.6
		4.2	72.5
E		4.2	72.5
	24+50		
NE		33	73.4
22		35	73.2
18		78	68.9
15		66	70.1
12		46	72.1
10		46	72.1
C		43	72.4
		46	72.1
W		4.8	71.9

	76.65		
	25+50		
W		53	71.4
		51	71.6
C		46	72.1
		4.8	71.9
E		4.4	72.3
	25+50		
E		3.8	72.9
		46	72.1
C		4.5	72.2
		5.0	71.7
W		5.3	71.4
	26+50		
W		5.2	71.5
		4.8	71.9
C		4.4	72.3
		4.4	72.3
E		3.7	73.0
	26+50		
E		4.5	72.2
		5.0	71.7
C		4.7	72.0
		5.1	71.6
W		5.3	71.4

76.65

27+00

W	62	70.5
	60	70.7
C	53	71.4
	55	71.2
E	50	71.7

27+50

E	52	71.5
	58	70.9
C	57	71.0
	61	70.6
W	64	70.3

28+00

W	65	70.2
	60	70.4
C	59	70.8
	63	70.4
E	57	71.0

28+50

E	64	70.3
	65	70.2
C	63	70.4
	68	69.9
W	70	69.7
TIP	3.22	73.12
		675
		69.90

73.12

52

29+00

W	38	69.3
	36	69.5
C	33	69.8
	36	69.5
E	32	69.9

29+50

E	35	69.6
	39	69.2
C	36	69.5
	41	69.0
W	44	68.7

30+00

W	49	68.2
	45	68.6
C	39	69.2
	41	69.0
E	37	69.4

30+50

E	37	69.4
	41	69.0
C	39	69.2
	42	68.8
W	46	68.5

73.12

31400

W	4.4	68.7
	4.2	68.9
C	3.8	69.3
	4.0	69.1
E	3.8	69.3

31450

E	4.0	69.1
	3.9	69.2
C	3.9	69.2
	4.4	68.7
W	4.7	68.4

3146551=51 Genter On Paring

W	4.84	68.28
	4.52	68.60
C	4.15	68.97
	4.16	68.96
E	4.23	68.89
Sidewalk Stake S.E Genter	3.71	69.41 ✓

53

18+1512 Huts 20' E & W of C

	1.77	H1 82.16	50.39 SE Rosemont	
+1+44 ⁵ EC			27	79.5
41			29	79.3
+50			3.4	78.8
40			4.0	78.2
+50			4.3	77.9
39			4.7	77.5
+50			4.5	77.7
103 - Cul			4.5	77.5
38			4.5	77.7
+50			4.3	77.9
37			4.0	78.2
T.P. +50	89.0	87.43	3.63	78.53
36			8.5	78.9
+50			7.9	79.5
35			6.8	80.6
+50			5.7	81.7
34			4.8	82.6
+50			4.3	83.1
33			5.39	83.5
+50			5.1 Top pipe	82.3
			3.8	83.6
T.P. 32	2.81	86.29	3.95	83.48
32+13 = Top pipe			3.80	82.5
31+50			3.1	83.2
31			3.6	82.7
+50			4.0	82.3

Nail Cl	30	46	81.7
+50		50	81.3
29		51	81.2
+50		52	80.9
28		57	80.6
+50		59	80.4
27		60	80.3
26+84 = pc		61	80.2
P.L.		61	80.2

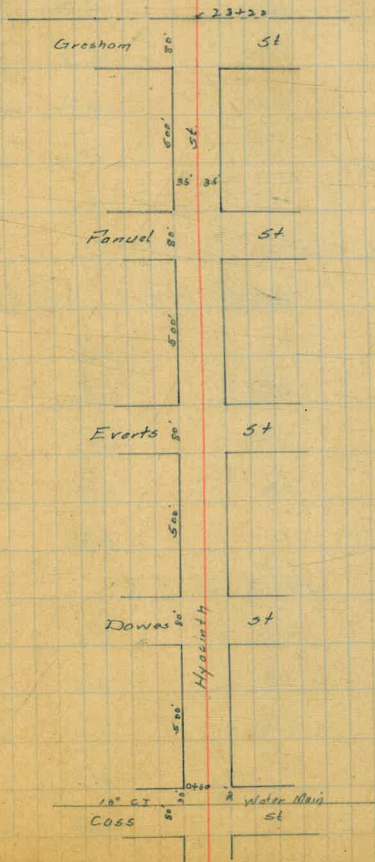
6 } Davis
 10 } C. Moore
 19 } O. Moore

55



Location of 4" Water Main on Hyacinth St to Reservoir

Note: Pipe to be laid 10' So. and East of Line shown on sketch.



4/13/25 Gregory

CROSS SECTION OF
VOGT PL. 30' wide
5' walk on S. Side

2.90 349.63 346.73 SE 46° Maryland.

E. L. Maryland = Sec. A.

25 S. of S.L. = P.C.	4.38	345.2	on hub
5 L.	4.5	345.1	
5 cb	4.4	345.2	
17.5 N. of S.L.	4.4	345.2	
30' = N.L.	4.6	345.0	

12.5' E of E.L.

10 N. of N.L.	8.3	341.3	
N.L.	6.8	342.8	
12.5 S	4.8	344.8	
25' ✓	4.2	345.4	
S.L.	4.1	345.5	
3.3 S = on Curve.	4.1	345.5	

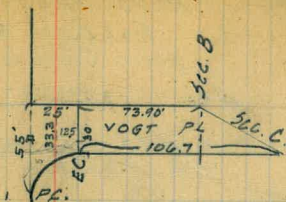
25' E of E.L. = E.C.

5	3.8	345.8	
5 N = cb	4.0	345.6	
17.5 ✓	5.0	344.6	
30' ✓ = N.L.	6.9	342.7	
10' out.	8.6	341.0	

25' E of E.C.

10 out.	9.2	341.4	
N	7.4	342.2	
12.5 S	5.0	344.6	
25' ✓	4.8	344.8	
5	4.3	345.3	

MARYLAND ST



50' E of E.C.

5	4.0	345.6	
5 N	4.7	344.9	
17.5 ✓	6.3	343.3	
30' ✓ = N	8.1	341.5	
10' out	10.1	339.5	

73.9' E of E.C. = Sec. B

10' out	10.6	339.0	
N	8.7	340.9	
12.5 S	6.6	343.0	
25' ✓	5.1	344.5	
S.L.	4.5	345.1	

Sec. C.

S.L.	4.3	345.3	
cb.	4.9	344.7	
12.5	6.8	342.8	
N.L.	8.7	340.9	

4/13/25 Gregory CROSS SECTION OF 40' ST
 GOLDEN GATE AVE 5' obs
 from Cleveland To Delaware 7.5' 1/4's
 490 351.63 346.73 SE 66° Maryland

Cb + Walk in on S. Side from Cleveland To 100' W
 W.L. Cleveland

S. Cb on cement	3.47	348.16
v gutter	4.1	347.5
1/4	3.8	347.8
c	3.8	347.8
1/4	3.9	347.7
cb	4.1	347.5
N	4.0	347.6

25' W

N	3.9	347.7
cb	3.9	347.7
+2.5	4.3	347.3
1/4	3.9	347.7
c	3.9	347.7
1/4	3.7	347.9
gutter	4.1	347.5
S. Cb. on cement.	3.60	348.03

50' W

S. Cb on cement	3.62	348.01
v gutter	4.2	347.4
1/4	3.7	347.9
c	3.6	348.0
1/4	3.9	347.7
+5	4.1	347.5
cb	3.8	347.8
N	3.7	347.9

75' W

N	3.4	348.2
cb	3.6	348.0
+3	4.0	347.6
1/4	3.8	347.8
c	3.5	348.1
1/4	3.8	347.8
gutter	4.2	347.4
S. Cb on cement	3.75	347.88

100' W = W. end Cb + walk.

S. Line	3.70	347.93
v curb on cement	3.90	347.7
v gutter	4.4	347.2
+1	3.9	347.7
1/4	3.8	347.8
c	3.6	348.0
1/4	3.7	347.9
+4	3.9	347.7
cb	3.5	347.1
N	3.5	348.1

125' W

N	3.5	348.1
cb	3.5	348.1
1/4	3.6	348.0
c	3.6	348.0
1/4	3.7	347.9

351.63

+5	40	347.6
+6	46	347.0
cb	3.8	347.8
S	3.5	348.1

150' W

S	3.7	347.9
cb	4.2	347.4
+2	4.7	346.9
+3	4.2	347.4
1/4	3.9	347.7
c	3.8	347.8
1/4	3.9	347.7
cb	3.9	347.7
N	3.7	347.9

175' W

N	3.4	348.2
cb	3.7	347.9
1/4	3.8	347.8
c	3.9	347.7
1/4	4.0	347.6
+5	4.2	347.4
+6	4.7	346.9
cb	4.0	347.6
S	3.7	347.9

200' W

S	3.8	347.8
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Golden Gate,

58

cb	40	347.6
+1	4.7	346.9
+4	3.6	348.0
1/4	4.0	347.6
c	3.9	347.7
1/4	3.6	348.0
cb	3.8	347.8
N	3.4	348.2

225' W

N	3.3	348.3
cb	3.5	348.1
1/4	4.0	347.6
c	3.9	347.7
1/4	3.9	347.7
+2	3.4	348.2
+6	4.8	346.8
cb	4.0	347.6
S	3.8	347.8

250' W

S	3.7	347.9
cb	4.2	347.4
+1	4.8	346.8
+2	4.1	347.5
1/4	4.2	347.4
c	4.4	347.2
1/4	4.2	347.4

351.63

cb	3.9	347.7
N	2.4	349.2
275' W	3.1	
N	3.5	348.1
cb	4.2	347.4
1/4	4.4	347.2
C	4.5	347.1
1/4	4.4	347.2
+5	4.3	347.3
+6	5.0	346.6
cb	4.3	347.3
S	4.2	347.4
287.5' W		
3' S. x 3' L. = on curve.	3.0	348.6
3.1	4.5	347.1
cb	4.7	346.9
+1	5.2	346.4
+3	4.6	347.0
1/4	4.5	347.1
C	4.5	347.1
1/4	4.6	347.0
cb	4.3	347.3
+3	4.0	347.6
NL	3.4	348.2
3' N. x 1/2	2.9	348.7

Golden Gate 39

296.7

13.2' N. x 1/2 produced	3.2	348.4
N.L. produced.	3.7	347.9
- cb -	4.6	347.0
1/4 -	4.9	346.7
C	4.9	346.7
+4	5.2	346.4
1/4	4.7	346.9
+2	4.5	347.1
+4	4.8	346.8
+5	5.5	346.1
cb	4.8	346.8
5L. produced.	4.5	347.1
5' S	3.0	348.6
13.2' = on curve	2.4	349.2
300' W = E.L. Maryland		
25' S. x 5L produced = PC.	4.75	346.88
on cb opp.	3.5	348.1
5' - - - -	3.7	347.9
5L. produced	4.6	347.0
cb	4.8	346.8
+2	5.4	346.2
1/4	5.0	346.6
C	4.8	346.8
1/4	5.0	346.6
cb	4.8	346.8
N	4.6	347.0

351.63

5' N of N.L. produced	40	347.6
25' " " " " = EC.	45	347.1
on curb opp.	5.35	346.28
W.L. Maryland.		
on curb	5.33	346.30
25' N of N.L. produced = PC.	49	346.7
N.L. produced.	47	346.9
- cb ✓	46	347.0
- 1/4 ✓	47	346.9
c	47	346.9
5 1/4 ✓	48	346.8
- cb ✓	45	347.1
- L ✓	44	347.2
15' S of ✓ ✓ ✓	39	347.7
25' " " " " ✓	39	347.7
	4.98	346.85
3.3' W of W.L. Maryland.		
13.2 S of S.L. produced = on curve.	2.6	349.0
" " ✓	3.8	347.8
- cb ✓	3.7	347.9
- 1/4 ✓	3.8	347.8
c	4.0	347.6
N 1/4 ✓	4.1	347.5
- cb ✓	3.8	347.8
- L ✓	3.9	347.7
13.2 N of ✓ ✓ ✓	3.8	347.8

478

Golden Gate

60

12.5' W of W.L.		
3' N of N.L. produced	41	347.5
" " ✓	41	347.5
- cb ✓	41	347.5
- 1/4 ✓	40	347.6
c	42	347.4
5 1/4 ✓	41	347.5
- cb ✓	40	347.6
- L ✓	40	347.6
3' S of ✓ ✓ ✓	40	
25' W of W.L. Maryland = E.C.		
S	42	347.4
cb	42	347.4
1/4	41	347.5
c	37	347.9
1/4	37	347.9
cb	34	348.2
+3	31	348.5
N	33	348.3
15' W of E.C.		
N	31	348.5
cb	2.8	348.8
1/4	2.7	348.9
c	3.6	348.0
1/4	3.9	347.7
cb	4.2	347.4
S	4.4	347.2

351.63

30' W of E.C.

S	4.4	347.2
cb	4.3	347.3
1/4	4.3	347.3
c	3.7	347.9
1/4	3.4	348.2
cb	3.4	348.2
N	3.3	348.3

40' W of E.C.

N	4.4	347.2
cb	4.3	347.3
1/4	4.3	347.3
c	4.3	347.3
1/4	4.2	347.4
cb	4.2	347.4
S	4.4	347.2

55' W of E.C.

S	4.3	347.3
cb	4.0	347.6
1/4	3.7	347.9
c	3.4	348.2
1/4	3.9	347.7
+3	4.5	347.1
cb	4.4	347.2
N	4.3	347.3

70' W of E.C.

N	4.7	346.9
cb	4.8	346.8
1/4	4.7	346.9
c	4.7	346.9
1/4	4.7	346.9
cb	4.7	346.9
S	4.8	346.8

80' W of E.C.

S	4.8	346.8
cb	4.8	346.8
1/4	5.0	346.6
c	5.0	346.6
1/4	5.0	346.6
cb	5.1	346.5
N	5.0	346.6

100' W of E.C.

N	5.1	346.5
cb	5.2	346.4
1/4	5.1	346.5
c	5.0	346.6
1/4	4.5	347.1
cb	4.2	347.4
S	3.8	347.8

112.5 W of E.C.

S	3.9	347.7
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351.63

cb	3.9	347.7
1/4	4.4	347.2
c	4.8	346.8
1/4	5.2	346.4
cb	5.3	346.3
N	5.3	346.3

125' W of E.C.

N	5.2	346.4
cb	5.3	346.3
1/4	5.4	346.2
c	5.2	346.4
1/4	5.0	346.6
cb	4.9	346.7
S	5.0	346.6

150' W of E.C. = P.C. into Harvey.

S	5.1	346.5
cb	5.3	346.3
1/4	5.4	346.2
c	5.3	346.3
1/4	4.8	346.8
+4	4.4	347.2
cb	4.5	347.1
N	4.7	346.9

12.5' W of P.C.

3.3' N of N.L. produced	4.4	347.2
N.L. prod.	4.6	347.0

Golden Gate 62

N.cb.	4.9	346.7
1/4	5.3	346.3
c	5.5	346.1
1/4	5.5	346.1
cb	4.9	346.7
S	4.5	347.1

25' W of P.C. = E.L. Harvey produced.

S	4.7	346.9
cb	4.9	346.7
1/4	5.6	346.0
c	5.8	345.8
1/4	5.7	345.9
cb	5.6	346.0
N	5.5	346.1

4' Harvey produced.

N	6.0	345.6
cb	6.0	345.6
1/4	5.8	345.8
c	5.6	346.0
1/4	5.4	346.2
+6	5.2	346.4
cb	5.0	346.6
S	4.9	346.7

10' W of 4' produced

S	5.4	346.2
cb	5.2	346.4

1/4	5.2	346.4
c	5.5	346.1
1/4	5.5	346.1
cb	6.1	345.5
N	6.1	345.5

W.L. of Harvey produced

N	6.2	345.4
cb	6.2	345.4
1/4	6.0	345.6
c	5.6	346.0
1/4	5.4	346.2
cb	5.4	346.2
S	5.4	346.2

12.5' W. of W.L. Harvey produced.

S	6.3	345.3
cb	6.4	346.2
1/4	6.3	345.3
c	6.2	345.4
1/4	6.4	345.2
cb	6.0	345.0
N.L. produced	6.0	345.6

3.3 N. of - - - - - 6.1 345.5

25' W. of W.L. produced = E.C.

N	6.5	345.1
cb	6.5	345.1
1/4	6.7	344.9

C	6.8	344.8
1/4	6.7	344.9
cb	6.7	344.9
S	6.6	345.0

10' W. of E.C. = P.C. on S.

S	5.7	345.9
cb	5.9	345.7
1/4	6.6	345.0
c	6.9	344.7
1/4	7.0	344.6
cb	7.1	344.5
N	7.1	344.5

25' W. of E.C.

N	7.3	344.3
cb	7.3	344.3
1/4	7.2	344.4
c	6.7	344.9
1/4	5.8	345.8
cb	5.4	346.2
S	5.5	346.1

44.88' W. of E.C. = E.L. Delaware ^{60' 3" 10' cbs} prod.

S	7.5	344.1
cb	7.4	344.2
1/4	7.4	344.2
c	7.7	343.9
1/4	7.7	343.9

35163

cb	7.8	343.8
N	8.0	343.6
E. Cb. Delaware.		
N	7.7	343.9
cb	8.2	343.4
1/4	8.0	343.6
c	7.7	343.9
1/4	7.2	344.4
cb	7.0	344.6
S	7.2	344.4
E 1/4		
S	6.2	345.4
cb	6.1	345.5
+3	7.1	344.5
1/4	7.4	344.2
c	7.7	343.9
1/4	7.9	343.7
cb	7.7	343.9
N	8.3	343.3
Center Delaware.		
N	10.3	341.3
+3	8.4	343.2
cb	8.3	343.3
1/4	8.0	343.6
c	7.7	343.9
1/4	7.6	344.0

Golden Gate, 64

cb	7.5	344.1
+3	7.3	344.3
S	6.6	345.0
W 1/4		
S	7.7	343.9
cb	7.9	343.7
1/4	8.1	343.5
c	8.0	343.6
1/4	8.8	342.8
+5	13.7	337.9
W. Curb.		
5' No. 1	12.2	339.4
3' v - -	9.6	342.0
c	8.8	342.8
5 1/4	8.5	343.1
cb	8.0	343.6
S	8.0	343.6

CROSS SECTION OF 60' ST
 Delaware ST
 from Madison To Golden Gate

351.63 from page 64

Cb. & Walk in on W Side from Madison to Golden Gate
 N.L. Madison

W. Cb on cement	7.07	44.56
✓ gutter	7.3	
1/4	7.0	
c	6.9	
1/4	7.1	
cb	7.1	
E	6.5	45.1
25' N		
E	7.0	44.6
cb	6.9	
1/4	6.8	
+9	6.8	
c	7.4	
1/4	7.4	
W gutter	7.8	
✓ curb	7.07	44.56
50' N		
W curb	7.09	44.54
✓ gutter	7.8	
1/4	7.3	
c	7.3	
+1	6.9	

6.59
 34.5

Delaware

65

1/4	7.1	
cb	7.0	
E	7.0	44.6
65' N		
E	7.1	44.5
cb	6.1	
1/4	5.6	
+9	6.1	
c	7.2	
1/4	7.3	
gutter	7.8	
W curb	7.12	44.51
75' N		
W curb	7.16	44.47
gutter	7.8	
1/4	7.3	
+ c	7.2	
+1	5.9	
1/4	5.3	
cb	6.1	
E	7.1	44.5
95' N		
E	6.5	45.1
cb	7.0	
1/4	7.0	
c	7.2	

351.63

1/4	7.3	
gutter	7.8	
cb	7.24	44.39
110' N		
W cb	7.34	44.29
1/4	7.1	
c	7.1	
1/4	7.0	
cb	6.8	
E	6.4	45.2
120' N		
E	6.8	44.8
cb	7.0	
1/4	7.2	
c	7.3	
1/4	7.2	
+7	7.1	
gutter	7.8	
W curb	7.40	44.23
135' N		
W curb	7.48	44.15
gutter	7.8	
+3	7.4	
1/4	7.2	
c	7.1	
1/4	5.7	

Delaware

66

cb	5.6	
E	6.9	44.7
145' N		
E	6.8	44.8
+6	5.8	
cb	5.5	
1/4	5.9	
c	7.2	
1/4	7.4	
+7	7.6	
gutter	8.0	
curb	7.52	44.11
155' N		
W curb	7.50	44.13
gutter	8.0	
+3	7.5	
1/4	7.4	
c	7.4	
1/4	7.0	
cb	6.8	
E	7.2	44.4
173.7 = N. End of Ch. 52 Golden Gate on W.		
E	7.3	44.3
cb	6.8	
+5	6.4	
1/4	6.5	

35163

C	7.3	
1/4	7.7	
gutter	7.9	
W curb = end of cement cb.	7.58	44.05
185' N.		
W.	8.0	
cb	8.1	
1/4	8.0	
c	7.7	
1/4	7.3	
cb	7.3	
E	7.4	

Delaware

67

4/13/68 Gregory. CROSS SECTION OF 40' wide
 HARVEY Road 5' cbs
 Entire Length

351.63 from page 67

12.5' N. of N.L. Golden Gate.

3.3' W. of W.L. produced 6.4 345.2

W. L. 6.5 345.1

cb 6.3 345.3

1/4 6.1 345.5

c 6.1 345.5

1/4 5.9 345.7

cb 5.5 346.1

E.L. produced 5.2 346.4

3.3' E. of W. L. 4.9

25' N. of N.L. Golden Gate = EC.

E 5.8 345.8

cb 5.8 345.8

1/4 6.0 345.6

c 6.2 345.4

1/4 6.3 345.3

cb 6.5 345.1

W 6.6 345.0

25' N. of EC.

W 6.6 345.0

cb 6.3 345.3

1/4 5.8 345.8

c 5.7 345.9

1/4 5.6 346.0

Harvey Rd. 68.

cb 58 345.8

E 60 345.6

50' N. of EC.

E 61 345.5

cb 61 345.5

1/4 58 345.8

c 57 345.9

1/4 62 345.4

cb 63 345.3

W 66 345.0

80' N. of EC.

W 60 345.6

cb 59 345.7

1/4 61 345.5

c 63 345.3

1/4 62 345.4

cb 61 345.5

E 60 345.6

100' N. of EC.

E 54 346.2

cb 57 345.9

1/4 58 345.8

c 63 345.3

1/4 65 345.1

cb 66 345.0

W 68 344.8

35/63

115' N of EC.

W	6.9	344.7
cb	6.8	344.8
1/4	6.6	345.0
c	6.1	345.5
1/4	5.9	345.7
cb	5.6	346.0
E	5.4	346.2

135' N of EC.

E	6.7	344.9
cb	6.8	344.8
1/4	6.9	344.7
c	6.8	344.8
1/4	6.9	344.7
cb	6.9	344.7
W	7.0	344.6

160' N of EC.

W	7.0	344.6
cb	7.1	344.5
1/4	7.0	344.6
c	6.8	344.8
1/4	7.0	344.6
cb	7.1	344.5
E	7.1	344.5

Harvey Rd

69

ALLEY CROSS SECTION 20' wide
 KANSAS + 30th - ADAMS + MADISON

SEBP 30th + ADAMS 337 392.41 389.0

SL ADAMS = 0+00

E on paving 4.7v 387.69
 C ✓ ✓ 5.0↓ 387.37
 W ✓ ✓ 4.8↓ 387.57

10'S

W 4.1 388.3
 C 4.1 88.3
 E 4.2 88.4

10'S

E 4.1 88.3
 C 3.7 88.7
 W 4.3 88.1

75'S

W 5.0 87.4
 C 4.6 87.8
 E 4.8 87.6

110'S

R 5.1 87.0
 C 4.8 87.1
 W 4.9 87.5
 +5 Garage dirt floor 4.8 87.6

T.P. 395 391.07 5.29 387.17

135'S

W 3.8 87.3
 C 4.1 87.0

Moore 8/11/25 391.07
 Preston
 Walker
 Mel

71.

E 4.3 86.8

175'S

E 4.6 86.5
 C 4.7 86.4
 W 4.6 86.5

200'S

W 4.0 87.1
 C 4.7 86.4
 E 5.1 86.0

221'S

E 4.6 86.5
 C 5.1 86.0
 W 4.7 86.4

232'S

W Garage dirt floor 4.50 86.6 ON IN ALLEY
 C 4.5 86.6
 E 4.3 86.8

245'S

E 5.3 85.8
 C 5.0 86.1
 W 4.3 86.8

282'S

W Garage dirt floor 5.2 85.9 OS IN ALLEY
 C 5.1 86.0
 E 4.6 86.3

Plotted Oct 13, 1925
 Larry Golden

391.07

	300'S		
E		4.9	86.7
C		5.3	85.8
W		5.6	85.5
	325'S		
W		5.8	85.3
C		5.5	85.6
E		5.2	85.9
	355'S		
E		5.5	85.6
C		5.7	85.4
W		6.5	84.6
	365'S		
W		6.1	84.7
C		6.6	84.5
E		6.9	84.2
	400'S		
E		7.3	83.8
C		7.8	83.3
W		7.8	83.3
	425'S		
W		7.7	83.4
C		8.1	83.0
E		7.5	83.6
	450'S		
E		7.9	82.11

391.07

72

C		5.2	84.9
W		5.3	84.8
	475'S		
W		8.0	83.1
C		8.3	82.8
E		7.5	83.6
	500'S		
E		8.2	82.9
C		8.4	82.7
W		8.6	82.5
	525'S		
W		8.1	83.0
C		8.1	83.0
E		8.1	83.0
	550'S		
E		8.4	82.7
C		8.1	83.0
W		8.2	82.9
	492'S Garage	7.8	83.3 2.5 E of BK dirt floor
	509'S ✓	8.5	82.6 on BK. ✓ ✓
	531'S ✓	8.9	83.0 3.4 W of BK Conc floor
	same Garage ✓ ✓ Conc. Apron	8.2	83.0 2.3 in Alley
	575'S		
W		8.4	82.7
C		8.4	82.7
E		8.5	82.6

391.07

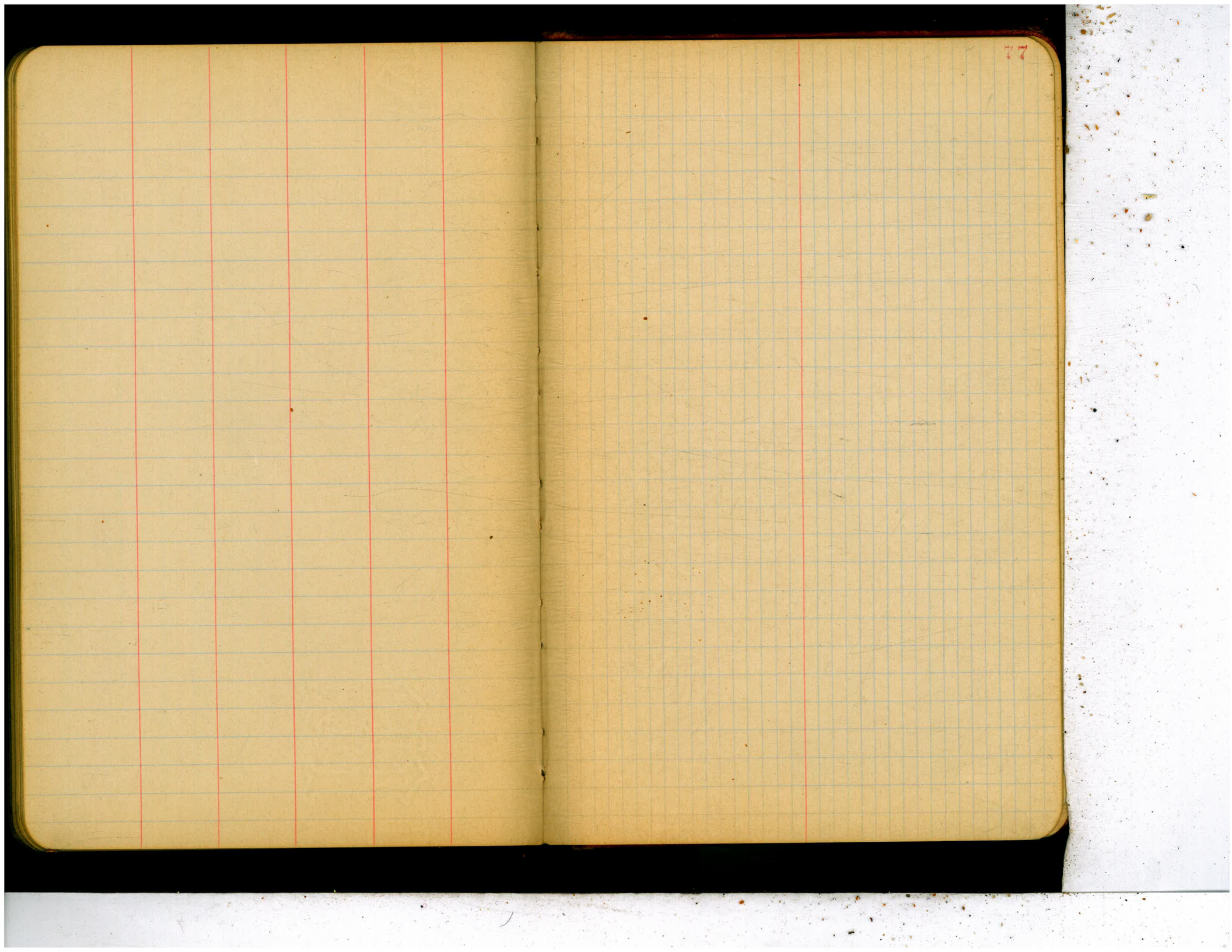
590'S

E	8.7	Pr. 4
C	8.8	Pr. 3
W	8.7	Pr. 4

600'S - NW MADISON FIVE

W	on Conc. Alley Return	9.74	381.33	
C		9.6	381.50	
E	✓ ✓ ✓ ✓	9.36	381.71	3890 ✓
		2.08	388.99	Check to BM

73



Location of Naylor's Bath House Etc

29
 15 } Doris
 19 } Roche
 } Sherwin

