DIETZGEN

ENGINEERS'

FIELD BOOK

No. 403

EUGENE DIETZGEN CO

DRAWING MATERIALS, MATHEMATICAL a
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

1060

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

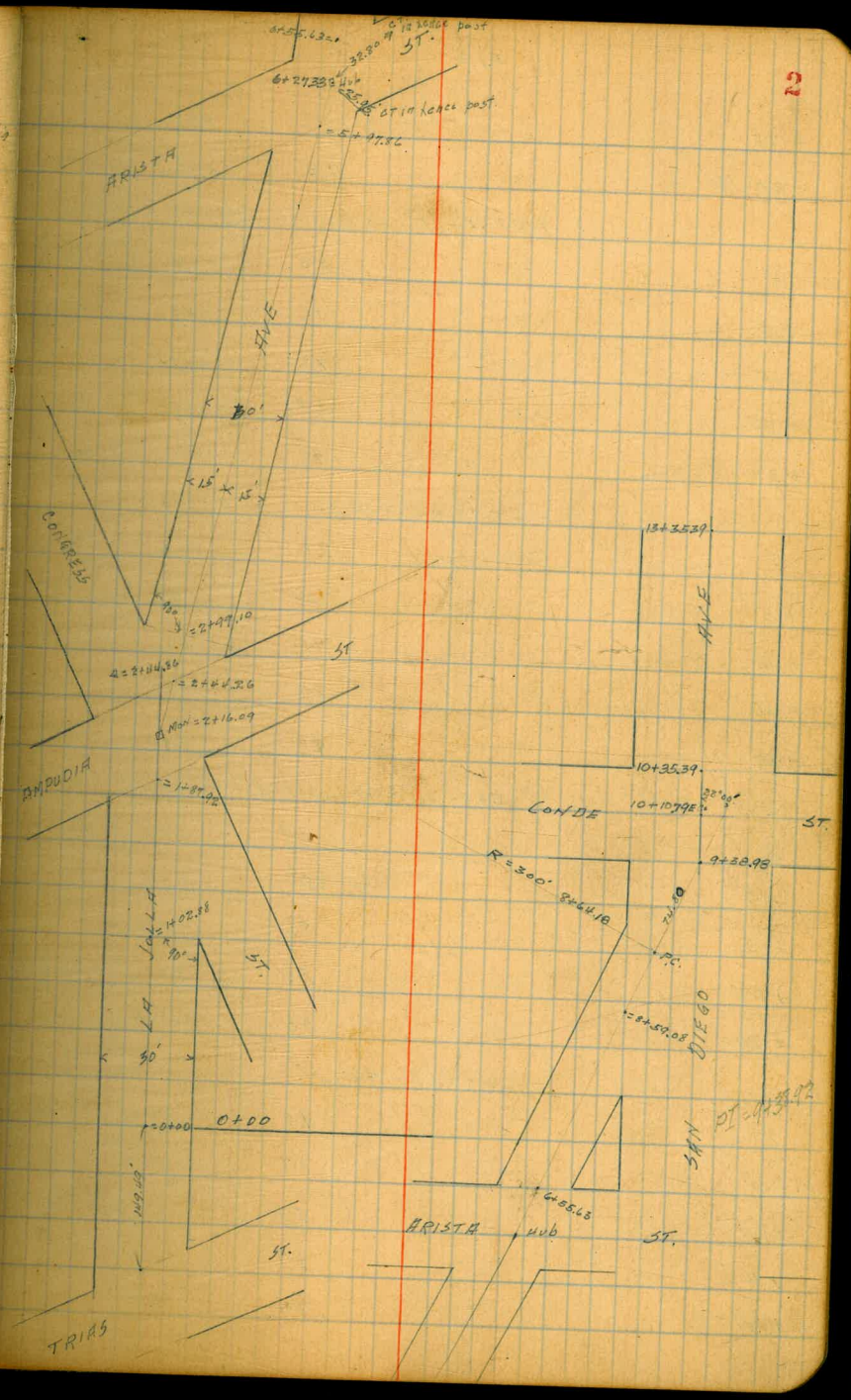
H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

4/19/19 Gregory Miller

CROSS-SECTION OF THE CENTRE 30' OF LA JOLLA AVE. SAN DIEGO AVE AND TAYLOR ST. for paving.

BM	6.89	51.32	44.43	=W. Ampudia & La Jolla
		0+00		
-5			3.6	47.7
W			2.9	48.4
+5			2.3	49.0
+15			1.7	49.6
+25			1.0	50.3
+30 = E			0.6	50.7
+5			0.4	50.9
		0+50		
E			2.6	48.7
+5			2.6	48.7
+15			3.2	48.1
+25			3.8	47.5
+30 = W			4.1	47.2
		1+02.88 = Pt L is to cor La Jolla & Congress		
W			5.9	45.4
+5			5.2	46.1
+15			4.7	46.6
+25			4.3	47.0
+30 = E			4.5	46.8
		1+50		
E			6.0	45.3
+5			5.8	45.5
+15			6.0	45.3



5132

+25		6.6	44.7
+30 = W		7.3	44.0
1+87.92 = rt L's from S.L. Ampudia St			
W		8.3	43.0
+5		7.6	43.7
+15		7.1	44.2
+25		6.9	44.4
+30 = E		7.1	44.2
2+16.09 = rt L's to L Ampudia			
E		7.8	43.5
+5		7.5	43.8
+15		7.6	43.7
+25		8.2	43.1
+30 = W		9.0	42.3
2+44.26 = rt L's to N.L. Ampudia			
W		8.9	42.4
+5		8.7	42.6
+15		8.6	42.7
+25		8.6	42.7
+30 = E		9.0	42.3
2+44.86 = △ pt.			
E		9.0	42.3
+5		8.7	42.6
+15		8.7	42.6
+25		8.7	42.6
+30 = W		8.9	42.4

2+75

W	10.1	41.2
+5	9.9	41.4
+15	9.8	41.5
+25	10.0	41.3
+29	10.3	41.0
+30 = E	9.8	41.5
+4	8.5	42.8
2+99.10 = rt L's to No. Cor La Jolla & Congress		
-3	10.2	41.1
E	11.0	40.3
+2.5	11.6	39.7
+5	11.4	39.9
+15	10.9	40.4
+25	11.0	40.3
+30 = W	11.1	40.2
T.P. 0.76 39.29 3+50		
W	12.79	38.53
+5	1.6	37.7
+15	1.4	37.9
+25	1.3	38.0
+26	1.9	37.4
+28	2.1	37.2
+30 = E	1.4	37.9
+5	1.8	37.5
	1.5	37.8

		39.29		
		4+00		
-5			3.3	36.0
E			3.3	36.0
+2			3.0	36.3
+3			3.9	35.4
+5			3.6	35.7
+15			3.1	36.2
+25			3.3	36.0
+30=W			3.7	35.6
		4+50		
W			5.6	33.7
+5			5.2	34.1
+15			5.0	34.3
+25			5.2	34.1
+30=E			5.6	33.7
		5+00		
E			6.6	32.7
+5			6.5	32.8
+15			6.5	32.8
+25			6.9	32.4
+30=W			7.2	32.1
		5+50		
-5			8.2	31.1
W			8.1	31.2
+5			7.7	31.6
+15			7.2	32.1

+25		7.1	32.2
+30=E		7.2	32.1
+5		7.0	32.3
5+97.86 = rt L's to 5L. Arista St. see sketch.			
-5		7.6	31.7
E		7.4	31.9
+5		7.5	31.8
+10		7.4	31.9
+15		7.6	31.7
+25		8.0	31.3
+30=W		8.5	30.8
+5		8.7	30.6
6+27.33 = ℄ Arista St + 4 pt.			
-5		8.0	31.3
W		7.8	31.5
+5		7.6	31.7
+15		7.3	32.0
+25		7.1	32.2
+30=E		6.8	32.5
+5		6.7	32.6
6+55.63 = N.L. Arista St			
-5		5.7	33.6
E		6.7	32.6
+5		6.7	32.6
+15		6.9	32.4
+25		6.8	32.5

		39.29		
+30=W			6.9	32.4
+5			6.9	32.4
		6+90		
W			5.8	33.5
+5			5.8	33.5
+15			5.9	33.4
+25			6.5	32.8
+30=E			5.6	33.7
T.P.	4.41	37.96	5.9	33.35
		7+15		
E			3.5	34.3
+5			5.3	32.5
+10			4.3	33.5
+15			4.5	33.3
+25			4.9	32.9
+30=W			4.0	33.8
		7+28		
-5			5.1	32.7
W			6.4	31.4
+2			6.9	30.9
+5			6.6	31.2
+10			4.8	33.0
+15			4.3	33.5
+20			4.7	33.1
+25			5.4	32.4
+30=E			3.1	34.7

	7+46	
E		
+5	4.2	33.6
+15	3.9	33.9
+20	4.5	33.3
+25	4.9	32.9
+30=W	6.8	31.0
+5	7.0	30.8
	5.3	32.5
	7+50	
-5	5.4	32.4
W	6.9	30.9
+5	6.9	30.9
+10	5.1	32.7
+15	4.6	33.2
+25	3.5	34.0
+30=E	4.9	32.9
+5	4.1	33.7
	7+75	
E	3.7	34.1
+5	4.0	33.8
+15	4.8	33.0
+19	5.6	32.2
+21	6.9	30.9
+25	7.3	30.5
+30=W	6.7	31.1
+4	5.5	32.3

		37.76			
		8+00			
-5			5.6	32.2	
W			5.7	32.1	
+5			6.7	31.1	
+9			6.6	31.2	
+12			5.1	32.7	
+15			4.8	33.0	
+25			4.1	33.7	
+30=E			3.6	34.2	
		8+25			
E			3.9	33.9	
+5			4.2	33.6	
+15			5.0	32.8	
+17			5.0	32.8	
+20			6.1	31.7	
+25			6.5	31.3	
+30=W			6.0	31.8	
+5			5.6	32.2	
		8+50			
-5			5.9	31.9	
W			6.5	31.3	
+5			6.3	31.5	
+15			4.8	33.0	
+25			4.2	33.6	
+30=E			3.9	33.9	
T.P.	5.04	37.31	5.49	32.27	PI bob

8+59.08 = M.L. San Diego Ave.

E	3.4	33.9
+5	3.8	33.5
+15	4.3	33.0
+17	4.4	32.9
+22	6.4	30.9
+25	6.4	30.9
+30=W	6.3	31.0
+3	5.3	32.0
+10	5.5	31.8

8+64.18 = P.C.

-5	5.4	31.9
-2	5.5	31.8
W	6.2	31.1
+5	5.7	31.6
+10	5.4	31.9
+15	4.3	33.0
+25	3.7	33.6
+30=E	3.6	33.7

8+80

E	3.6	33.7
+5	3.8	33.5
+15	4.4	32.9
+21	5.0	32.3
+25	6.7	30.6
+30=W	5.9	31.4
+5	5.4	31.9

		37.31			
		9+00			
-5			5.5	31.8	
W			7.1	30.2	
+5			6.6	30.7	
+7			5.4	31.9	
+15			4.4	32.9	
+25			4.1	33.2	
+30=E			5.2	32.1	
+5			4.6	32.7	
		9+25			
-5			5.3	32.0	
E			5.5	31.8	
+1			5.4	31.9	
+5			4.2	33.1	
+15			4.4	32.9	
+23			5.0	32.3	
+25			6.1	31.2	
+29			7.2	30.1	
+30=W			6.9	30.4	
+5			6.5	30.8	
		9+50			
-5			6.3	31.0	
-4			7.1	30.2	
W			6.9	30.4	
+5			5.2	32.1	
+15			4.5	32.8	

+25		4.9	32.4
+27		5.8	31.5
+30=E		5.6	31.7
+5		5.1	32.2
	9+75		
-5		5.4	31.9
E		5.8	31.5
+5		5.4	31.9
+15		5.0	32.3
+16		4.6	32.7
+24		4.9	32.4
+23		7.4	29.9
+25		7.6	29.7
+30=W		7.1	30.2
+3		6.9	30.4
+5		6.0	31.3
	9+85.39 = SL Conde SH		
-5		5.9	31.4
-2.5		6.8	30.5
W		6.9	30.4
+5		7.6	29.7
+11		4.9	32.4
+15		4.7	32.6
+19.8		4.8	32.5
+18		5.7	31.6
+25		5.7	31.6

	37+31		
+30=E		5.5	31.8
+5		5.7	31.6
	10+00		
-5		6.1	31.2
E		6.3	31.0
+5		6.6	30.7
+8		6.4	30.9
+9		5.2	32.1
+15		4.8	32.5
+20		5.5	31.8
+22		7.5	29.8
+25		7.1	29.9
+26		7.3	30.0
+30=W		6.0	31.3
+5		5.8	31.5
	10+10.79 = EC.		
-3		5.8	31.5
W		5.9	31.4
+3		6.1	31.2
+5		7.3	30.0
+11		6.8	30.5
+12		5.2	32.1
+15		4.9	32.4
+20		5.3	32.0
+25		6.8	30.5
+30=E		6.9	30.4
+5		6.3	31.0

	10+35.39 = NL CONDE		
-5		6.9	30.4
E		7.4	29.9
+5		7.1	30.2
+9		5.6	31.7
+15		5.3	32.0
+22		6.9	30.4
+25		5.9	31.4
+30=W		5.6	31.7
+4		5.7	31.6
	10+70		
-5		6.7	30.6
W		6.2	31.1
+5		5.8	31.5
+15		6.5	30.8
+20		5.6	31.7
+25		6.9	30.4
+29		7.5	29.8
+30=E		4.6	29.7
+5		7.1	30.2
	11+00		
-5		7.1	30.2
E		7.7	29.6
+5		6.6	30.7
+15		6.1	31.2
+25		5.7	31.6

		37.31		
+30=W			6.3	31.0
+1			6.4	30.9
		11+50		
-5			7.2	30.1
W			7.2	30.1
+5			6.2	31.1
+15			5.3	32.0
+25			5.8	31.5
+30=E			6.7	30.6
+5			6.5	30.8
		12+00		
-5			5.3	32.0
E			5.5	31.8
+5			5.1	32.2
+15			5.3	32.0
+22			6.0	31.3
+25			6.2	31.1
+30=W			6.7	30.6
+1			7.2	30.1
+5			7.7	29.6
		12+50		
-5			6.8	30.5
W			6.9	30.4
+5			5.9	31.4
+11			5.8	31.5
+15			5.1	32.2

+19			5.6	31.7
+25			5.4	31.9
+30=E			5.1	32.2
		13+00		
E			4.9	32.4
+5			5.5	31.8
+15			5.5	31.8
+22			5.9	31.4
+23			6.6	30.7
+25			6.5	30.8
+30=W			6.4	30.9
T.P.	3.02	36.29	4.04	33.27
		13+35.4 = 5L Harney/SF		
W			4.9	31.4
+5			4.7	31.6
+15			4.0	32.3
+25			4.1	32.2
+30=E			4.0	32.3
		13+60.4		
E			3.8	32.5
+5			3.8	32.5
+15			4.0	32.3
+25			4.4	31.9
+30=W			4.6	31.7
		13+85.4 = 7L Harney		
W			4.9	31.4

	36+79		
+5		4.8	31.5
+15		4.6	31.9
+25		4.2	32.1
+30 = E		4.2	32.1
	14+10		
E		4.3	32.0
+5		4.6	31.9
+15		4.5	31.6
+18		4.9	31.4
+25		5.0	31.3
+30 = W		5.0	31.3
	14+50		
W		4.9	31.4
+5		4.8	31.5
+12		4.8	31.5
+15		4.6	31.9
+25		4.5	31.6
+30 = E		4.5	31.6
	15+00		
E		4.4	31.9
+5		4.4	31.9
+15		4.7	31.6
+16		4.9	31.4
+25		5.2	31.1
+30 = W		5.3	31.0

	15+50		
W		5.1	31.2
+5		5.0	31.3
+15		4.9	31.4
+25		4.8	31.5
+30 = E		4.2	32.1
	16+00		
E		4.5	31.8
+5		4.8	31.5
+15		5.1	31.2
+25		5.1	31.2
+30 = W		5.2	31.1
	16+50		
W		5.5	30.8
+5		5.5	30.8
+15		5.5	30.8
+25		5.1	31.2
+30 = E		4.6	31.7
	16+85.4 = S.L. TWIGGS		
E		5.3	31.0
+5		5.6	30.7
+11		5.6	30.7
+15		6.3	30.0
+25		6.0	30.3
+30 = W		6.1	30.2
36+ BM		5.48	30.81

RR Spk
SL Twigs

36.29

17+35.4 = NL TWIGGS

W		6.9	29.4
+5		6.8	29.5
+15		7.0	29.3
+25		6.2	30.1
+30 = E		5.9	30.4
	17+65		
E		7.0	29.3
+5		7.0	29.3
+10		7.0	29.3
+14		7.5	28.8
+15		7.6	28.7
+25		7.4	28.9
+30 = W		7.4	28.9
	18+00		
W		8.3	28.0
+5		8.1	28.2
+15		8.3	28.0
+18		8.3	28.0
+20		7.6	28.7
+25		7.5	28.8
+30 = E		7.5	28.8
	18+50		
E		8.6	27.7
+5		8.7	27.6
+11		9.4	26.9
+15		9.5	26.8
+25		9.3	27.0
+30 = W		9.5	26.8
T.P. 10.5	27.94	9.40	26.89
	19+00		
W		2.2	25.7
+5		2.1	25.8
+15		2.1	25.8
+20		1.8	26.1
+25		1.1	26.8
+30 = E		1.3	26.6
	19+50		
E		2.5	25.4
+5		2.3	25.6
+9		2.7	25.2
+9.5		3.3	24.6
+15		3.3	24.6
+25		3.3	24.6
+30 = W		3.5	24.4
	20+00		
W		4.8	23.1
+5		4.7	23.2
+15		4.5	23.4
+20.5		4.4	23.5
+21		3.9	24.0
+25		3.3	24.6

	27.94	
+30 = E	3.5	24.4
20+35.4 = SL MASON ON WEST		
E	4.2	23.7
+5	4.4	23.5
+8	4.7	23.2
+8.5	5.4	22.5
+15	5.4	22.5
+25	5.6	22.3
+30 = W	5.7	22.2
20+85.4 = NL DITTO		
W	6.7	21.2
+5	6.5	21.4
+15	6.4	21.5
+22.5	6.5	21.4
+23	5.8	22.1
+25	5.4	22.5
+30 = E	5.2	22.7
21+25		
E	6.2	21.7
+4.5	6.4	21.5
+5	7.1	20.8
+15	7.1	20.8
+25	7.3	20.6
+30 = W	7.3	20.6
21+60 = SL MASON ON E		
W	7.9	20.0
+5	7.6	20.3
+15	7.3	20.6
+25	7.1	20.8
+30 = E	6.9	21.0
ch K	5.78	22.16 = 17 Book 1042 P 41

FOR X SECTIONS further No. see book 1021

set B.M.	6.62	21.32
	6.55	21.39 = R.R. spk in pole for Ramon Home

4/22/19 Gregory Miller Shaw

CROSS SECTION OF CURVE at TAYLOR and SAN DIEGO

Δ 90°03'40"
ST 50.05
R = 50.00 on ℄

on BM.	3.86	10.24		6.38	Top Hyd. Juan + Taylor
	3.31	7.57	5.98	4.26	
	S.L. of TAYLOR ST = PC of Curve.				
-15			6.3	1.3	
-5			5.5	2.1	
W			3.3	4.3	
+2			2.3	5.3	
+5			1.9	5.7	
+15			1.7	5.9	
+21			2.2	5.4	
+28.3 = scaled edge paving			5.1	2.5	
+33.6 " " berm			6.1	1.5	
+49			6.7	0.9	
	10' N. of PC.				
35' E of ℄			6.9	0.7	
20.7' E of ℄ = edge berm			6.6	1.0	
15.5' " " " paving			5.8	1.8	
6' " " "			2.1	5.5	
℄			1.9	5.7	
℄ +10			2.1	5.5	
℄ +14			2.6	5.0	
℄ +15 = W edge berm			3.0	4.6	
℄ +21			5.2	2.4	
℄ +30 = 15' from edge berm			6.2	1.4	
	20' N. of PC.				
-15			5.9	1.7	

CURVE AT TAYLOR & SAN DIEGO

3

-9	5.4	2.2
-3	3.4	5.2
W	2.2	5.3
+5	2.1	5.5
+10	1.6	6.0
+15	2.2	5.3
+20	2.7	4.9
+23	3.8	3.8
+30	6.6	1.0
+32.30 = edge paving	7.0	0.6
+37.5 = " berm	7.1	0.5
+52'	7.0	0.6
30' N. of PC.		
38' E of ℄	7.1	0.5
23.2' " " " = edge berm	7.1	0.5
18.1 " " " " = " paving	6.9	0.7
9' " " "	5.8	1.8
3' " " "	3.9	3.7
℄	3.4	4.2
℄ +4	2.2	5.2
℄ +10	1.8	5.8
℄ +15	1.9	5.7
40' N. of PC.		
15' W of ℄	1.8	5.8
10' " " "	2.0	5.6
℄	5.8	1.8

7.57

℄ + 4	6.7	0.9
℄ + 18.5 = edge paving	7.0	0.6
℄ + 23.5 " berm	7.0	0.6
℄ + 38	7.0	0.6
50' No ∝ PC.		
38' E ∝ ℄	7.0	0.6
23.2 " " = edge berm	6.9	0.7
18.1 " " = " paving	7.1	0.5
℄	7.0	0.6
℄ + 10	6.6	1.0
℄ + 15	5.7	1.9
℄ + 28	4.8	2.8
60' No ∝ PC.		
30' W ∝ ℄	7.1	0.5
15' " " "	7.3	0.3
10' " " "	7.3	0.3
℄	7.1	0.5
℄ + 17.4 = edge paving	7.2	0.4
℄ + 22.6 = " berm	7.1	0.5
℄ + 32.	7.0	
78.60' No ∝ P.C. = E.C. = 50' E ∝ ℄ ∝ San Diego Ave		
33. E ∝ ℄	7.1	0.5
18.6 " " = edge berm	7.0	0.6
13.3 " " = " paving	7.1	0.5
℄	7.1	0.5
℄ + 10	7.2	0.4
℄ + 15	7.2	0.4
℄ + 30	6.9	0.7

4/22/19 Gregor / Miller / Shaw

CROSS SECTION OF CENTER 30' OF TAYLOR ST. from E.L. Juan St. to Bridge

	4.12	10.11	5.99	spk SE Juan

E.L. Juan St.

N	4.8	5.3
+5	4.9	5.2
+15	5.1	5.0
+25	5.4	4.7
+30 = S	5.6	4.5

50' E

S	5.8	4.3
+5	5.7	4.4
+15	5.4	4.7
+25	5.2	4.9
No	5.1	5.0

100' E

No	5.2	4.9
+5	5.1	5.0
+15	5.0	5.1
+25	5.3	4.8
+30 = So	5.5	4.6

150' E

So.	5.2	4.9
+5	5.1	5.0
+15	4.8	5.3
+25	5.1	5.0
No	5.2	4.9

200' E

No	5.1	5.0
+5	4.8	5.3
+15	4.5	5.6
+25	5.0	5.1
+30 = So.	5.2	4.9

250' E

So	5.2	4.9
+5	4.9	5.2
+15	4.4	5.7
+25	4.7	5.4
+30 = No.	4.8	5.3

300' E = W.L. Sunset Blvd on No.

No	5.0	5.1
+5	4.8	5.3
+15	4.3	5.8
+25	4.7	5.4
So.	4.9	5.2

350' E = E.L. Sunset Blvd on No.

So.	4.8	5.3
+5	4.6	5.5
+15	4.3	5.8
+25	4.6	5.5
No.	4.6	5.5

400' E = W.L. Sunset Blvd on So.

No.	4.7	5.4

10.11

+5		4.5	5.6
+15		4.2	5.9
+25		4.6	5.5
+30=30.		4.7	5.4
	450' E = E.L. Sunset on 30.		
30.		4.5	5.6
+5		4.4	5.7
+15		4.1	6.0
+25		4.4	5.7
No.		4.5	5.6
	500' E		
No.		4.4	5.7
+5		4.2	5.9
+15		4.0	6.1
+25		4.3	5.8
+30=30.		4.4	5.7
	550' E		
30.		4.2	5.9
+5		4.2	5.9
+15		3.9	6.2
+25		4.2	5.9
No.		4.2	5.9
	600' E		
No.		4.1	6.0
+5		4.0	6.1
+15		3.8	6.3

+25		4.0	6.1
30.		4.1	6.0
	650' E = W.L. Whitman St.		
30		4.1	6.0
+5		3.9	6.2
+15		3.7	6.4
+25		3.9	6.2
No.		3.9	6.2
	700' E = E.L. Whitman St.		
No.		4.0	6.1
+5		3.9	6.2
+15		3.6	6.5
+25		3.9	6.2
30.		4.1	6.0
T.P. 6.26	12.44	3.95	6.16
	750' E		
30.		6.3	6.1
+5		6.2	6.2
+15		5.9	6.5
+25		6.1	6.3
No.		6.3	6.1
	800' E		
No.		6.2	6.2
+5		6.0	6.4
+15		5.9	6.5
+25		6.2	6.2
30.		6.3	6.1

	1244	
	850' E	
So	6.3	6.1
+5	6.1	6.3
+15	5.7	6.7
+25	6.0	6.4
No.	6.2	6.2
	900' E	
No.	6.0	6.4
+5	5.7	6.7
+15	5.5	6.9
+25	5.7	6.7
So.	5.9	6.5
	950' E	
So	5.7	6.7
+5	5.4	7.0
+15	5.2	7.2
+25	5.3	7.1
No	5.6	6.8
	1000' E = W.L. Chesnut St	
No.	5.2	7.2
+5	4.9	7.5
+15	4.9	7.5
+25	5.1	7.3
So.	5.3	7.1
	1050' E = E.L. Chesnut St	
So.	5.0	7.4

+5	4.7	7.7
+15	4.5	7.9
+25	4.6	7.8
No.	4.9	7.5
	1100' E	
No.	4.1	8.3
+5	3.8	8.6
+15	3.6	8.8
+25	3.8	8.6
So.	4.1	8.3
	1150' E	
So	3.1	9.3
+5	2.9	9.5
+15	2.9	9.5
+25	3.1	9.3
No	3.4	9.0
	1200' E	
No.	2.7	9.7
+5	2.4	10.0
+15	2.2	10.2
+25	2.4	10.0
So.	2.7	9.7
	1250' E	
So	1.4	11.0
+5	1.4	11.0
+15	1.5	10.9

		12.44		
+25			1.8	10.6
No.			1.9	10.5
		1300' E		
No.			0.5	11.9
+5			0.3	12.1
+15			0.2	12.2
+25			0.1	12.3
So.			0.0	12.4
T.P.	8.68	21.07	0.05	12.39
		1350' E = W.L. Hickory St.		
So.			6.9	14.2
+5			7.2	13.9
+15			7.2	13.9
+25			7.4	13.7
No.			7.6	13.5
		1372.61' E = P.C. of 215' Rad. Curve		
No.			7.2	13.9
+5			7.1	14.0
+15			7.0	14.1
+25			6.3	14.8
+30 = So.			5.7	15.4
		1400' E = E.L. Hickory St (approx)		
So.			4.7	16.4
+5			5.4	15.7
+15			6.4	14.7
+25			6.6	14.5

No.		6.7	14.4
	1425' E		
No.		6.3	14.8
+5		6.5	14.6
+15		6.4	14.7
+25		6.3	14.8
So.		6.0	15.1
+5		5.2	15.9
	1450' E		
-5		6.6	14.5
So.		6.5	14.6
+5		6.6	14.5
+15		6.4	14.7
+25		6.1	15.0
No.		6.0	15.1
+5		6.1	15.0
	1475' E		
-5		6.0	15.1
No.		6.1	15.0
+5		6.3	14.8
+15		6.4	14.7
+25		6.5	14.6
So.		6.5	14.6
+5		6.5	14.6
	1500' E		
-5		6.4	14.7

21.07

So.		6.5	14.6	
+5		6.5	14.6	
+15		6.2	14.9	
+25		6.2	14.9	
No.		6.0	15.1	
+5		5.9	15.2	

15 RR, 24' No Line Taylor St.
This section is taken on No. Line of Taylor.

No.	5.9	15.2	
+7.87 = edge paving	5.7	15.4	
℄	5.3	15.8	
+39.34 = edge paving	5.0	16.1	
+47.21 = ∠ berm	4.9	16.2	
chk TP	1.39	19.68	Coping on Concrete br. 1926

6/9/19 Gregory / Miller Shaw.

CROSS-SECTION OF Alley in Blk 1 St Louis Hghts 16' wide

	2.53 333.57		331.04	NE. Utah + Vpole
	S. L. Vpole			
E		3.83	329.74	on cement Cb.
C		4.2	329.4	
W		4.0	329.6	
		3.89	329.68	on cement cb
	16' So.			
W		3.6	330.0	
C		3.5	330.1	
E		3.1	330.5	
	26' So. = So. Edge Manhole			
E		4.0	329.6	
C		3.50	330.1	on Manhole
W		3.6	330.0	
	50' So			
W		4.4	329.2	
C		4.3	329.3	
E		4.5	329.1	
	81' So.			
E		5.0	328.6	
C		4.5	329.1	
W		4.6	329.0	
	93' So. = Ctr of 7' door to wooden garage.			
4' N. of N Line		4.6	329.0	= Cement Floor
	105' So.			
W		5.5	328.1	= Wooden Floor of garage

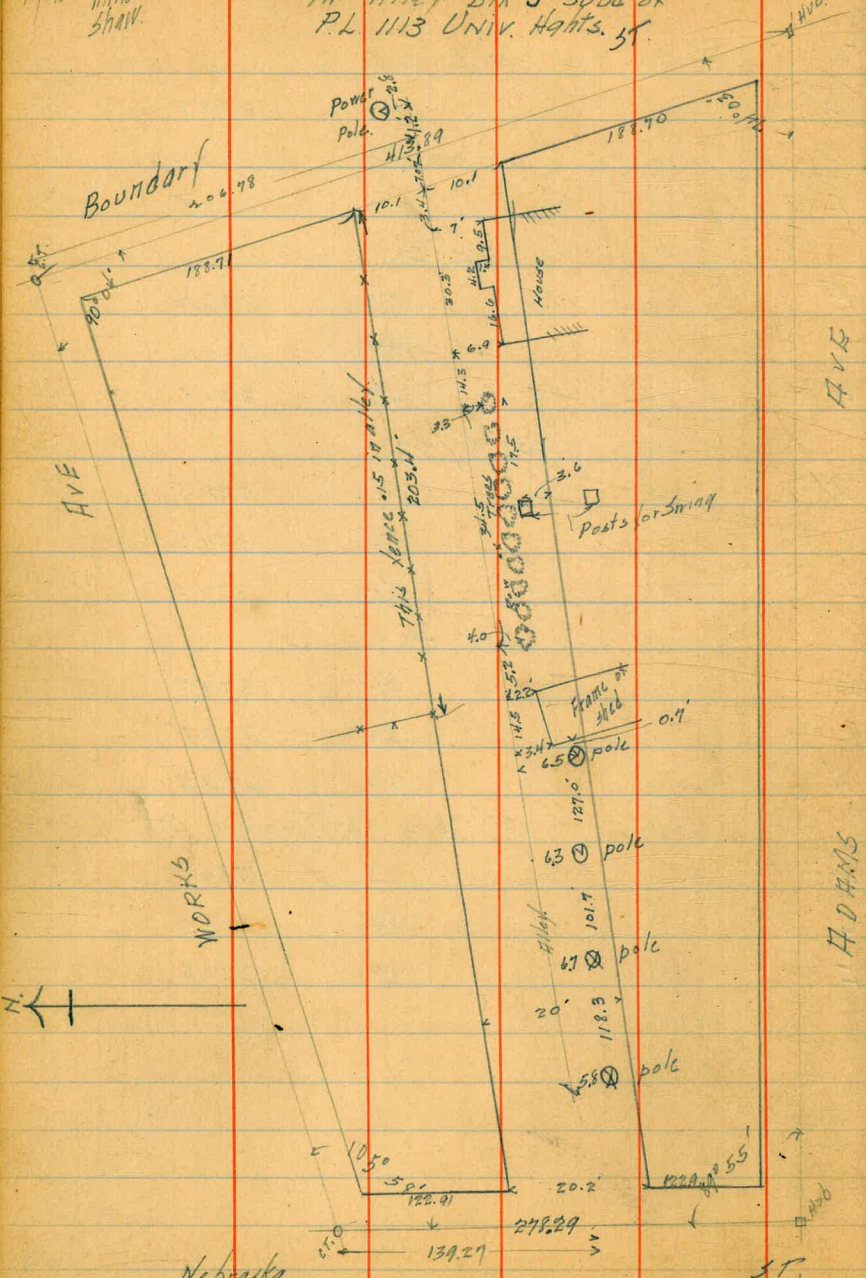
C	5.5	328.1	
+7.7	5.4	328.2	= wall of Shack
	131' So.		
E+1.2	5.6	328.0	= wall of Shack
C	5.6	328.0	
W	5.3	328.3	
	134' So. = So End Shack		
1.3' N. of E. Line	5.6	328.0	= wall of Shack
	150' So. = No End garage		
W	6.2	327.4	
C	6.2	327.4	
+9.5	6.3	327.3	= wall of garage
	166' So. = So end garage		
0.6' N of E Line	6.8	326.8	= wall of garage
T.P. 2.65 329.52	6.70	326.87	
C	2.6	326.9	
W	2.6	326.9	
	200' So.		
W	3.2	326.3	
C	3.3	326.2	
E	2.9	326.6	
	205.3 to 217.3 on E. = Shack 0.25 in alley		
	N 50' So		
E	3.7	325.8	
C	4.2	325.3	
W	4.1	325.4	

	329.52		
	296' So. = ctr of	garage door	
E		4.4	325.1 = dirt floor
	300' So.		
W		4.9	324.6
C		4.9	324.6
E		4.5	325.0
	335' So.		
E		4.2	325.3
C		5.2	324.3
W		5.5	324.0
	365' So.		
W		5.6	323.9
C		5.8	323.7
E		5.9	323.6
	400' So.		
E		5.8	323.7
C		6.0	323.5
W		6.0	323.5
	450' So.		
W		5.8	323.7
C		6.2	323.3
E		6.3	323.2
	500 So.		
E		6.5	323.0
C		6.2	323.3
W		6.0	323.5

	516' So.		
W		6.3	325.2
C		6.4	323.1
E		6.6	322.9
	532' So.		
E		5.3	324.2
C		4.9	324.6
W		4.9	324.6
	545' So		
W		5.0	324.5
C		5.0	324.5
E		5.4	324.1
	564' So		
E		6.3	323.2
C		6.4	323.4
W		6.3	323.2
	600' So = N.L. THORN ST		
W		6.5	323.0
C		6.5	323.0
E		6.7	322.8

6/9/19 Gregory Miller Shaw

Location of Improvements in Alley Blk J Subd of P.L 1113 Univ. Hghts. 5T.



22

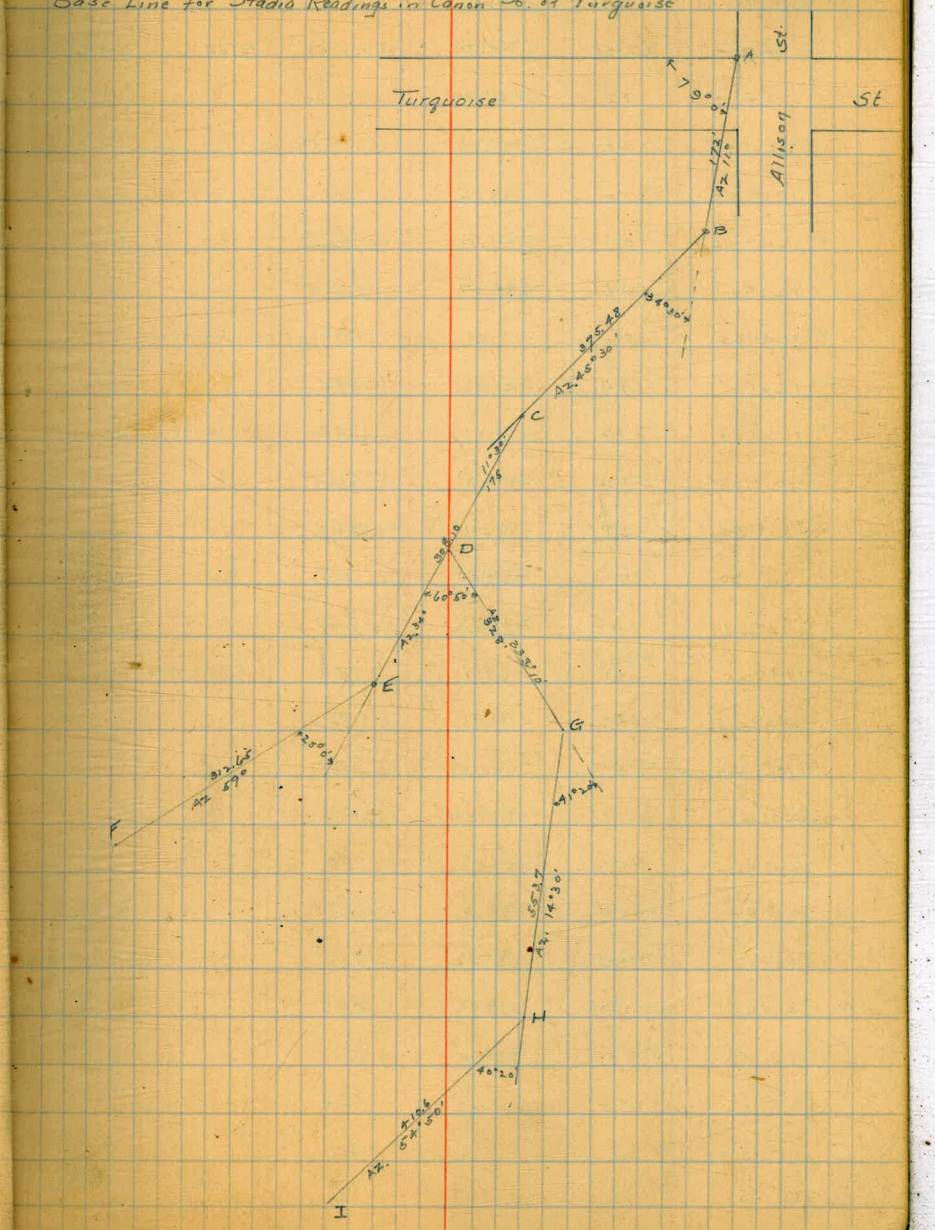
Levels & Stadia over Base Line So of Turquoise.

	0.30	107.34		107.04	
Sta. B			4.01	103.33	
T.P.	0.39	95.98	11.75	95.59	
Sta C			7.66	88.32	
T.P.	1.04	85.04	11.98	84.00	
Sta E			9.53	75.51	
Sta G			8.00	77.04	
	Elev 75.51				
	Dist	Vert	Hor. Dist	Elev	
	314	-2°13'	312.65	+6.34	Sta F
At G Elev 77.04	554	-1°19'	553.7	64.32	Sta H
At H Elev 64.32	412	-3°23'	410.61	40.05	Sta I.

6/19/19 Darts, C. Moore, B. Moore

23

Base Line for Stadia Readings in Cañon So. of Turquoise



2.06

⊼ at B	Elev 103.33	H.I. 108.24			on Rim
Az	Dist	Vert	Hor. Dist	Elev	Notes
225° 0'	182	+0° 39'	182.0		SW. Cor Bridge
✓ 212° 40'	120	+0° 09'	120.0		Rim
✓ 171° 50'	100	-1° 06'	100		"
✓ 124° 25'	94	-3° 57'	93.5		"
✓ 128° 0'	128	-3° 27'	127.4		"
✓ 179° 25'	182	-1° 41'	182		"
✓ 120° 0'	194	-1° 55'	194		"
✓ 112° 15'	242	-1° 47'	242		"
✓ 92° 25'	252	-1° 43'	252		"
✓ 81° 55'	268	-1° 54'	268		"
✓ 71° 30'	300	-2° 0'	300		Rim
90° 55'	242	-7° 22'	238		Botm
109° 25'	186	-8° 17'	182		"
99° 25'	102	-13° 45'	96		"
185° 35'	54	-22° 56'	46		"
247° 20'	56	-20° 24'	49		"
240° 45'	142	-5° 53'	140		"
230° 40'	184	-3° 51'	183		Botm.
230° 27'	202	+0° 52'	202		SE Cor. Bridge
✓ 243° 40'	238	+1° 31	238		Rim
✓ 251° 05'	180'	+1° 18'	180		"
✓ 277° 10'	132	+1° 02'	132		"
✓ 303° 05'	68	+1° 33	68		"
✓ 313° 45'	28'	+1° 47	28		"

Az	Dist	Vert	Hor. Dist	Elev	Notes
✓ 47° 0'	60	-2° 27'	60		Rim
✓ 76° 30'	102	-2° 41'	102		"
✓ 83° 30'	154	-2° 18'	153		"
✓ 70° 40'	146	-2° 15'	145		"
✓ 47° 15'	175	-2° 14'	174		"
✓ 40° 50'	244	-2° 07'	243		"
⊼ at C	Elev 88.32 417	H.I. 93.1			
✓ 257° 15'	64	+2° 46'	64	88.32 3.09 91.41	" 1
✓ 31° 20'	14	-2° 13'	14	88.32 54 87.78	" ✓
✓ 351° 45'	58'	-0° 46'	58	88.32 18 87.54	" 3
✓ 8° 0'	122	-1° 31'	122	88.32 3.23 85.09	" 4
✓ 25° 40'	144	-1° 54'	144	88.32 4.77 83.55	" 5
✓ 36° 40'	150	-2° 45'	150	88.32 7.19 81.13	" 6
✓ 52° 45'	152	-4° 08'	151	88.32 10.42 77.90	S.E Cor of Old LaJolla Pk Bridge 7
61° 45'	160	-13° 30'	151	52.00	Botm 8
61° 45'	120	-17° 44'	109	53.51	" 9
173° 35'	94	-37° 02	58	58.35	" 10
182° 0'	72	-33° 54	62	60.91	" 11
215° 10'	66	-33° 55	55	63.86	" 12
205° 20'	122	-11° 35	117	64.65	" 13
195° 55'	190	-7° 30	187	63.73	" 14
197° 10'	226	-4° 46	224	69.60	Botm. 15

π at C Elev 88.32 HI 93.1

	Az	Dist	Vert	Hor Dist	Elev	Notes
16	✓ 142°25'	162	+0°39'	162	90.15	Rim
17	✓ 113°30'	186	+0°41'	186	90.54	"
18	✓ 94°35'	161	-2°23'	166	81.47	"
19	71°30'	152	-3°50	151	78.18	NE cor Old Ziggurat Ruins

π at E Elev 75.51 HI 80.55

						on Rim NW Cor old Ziggurat Ruins
1	✓ 184°10'	200	+0°41'	200	77.90	
2	✓ 175°55'	246	+0°36'	246	78.08	Rim
3	✓ 171°05'	282	+1°30	282	82.89	"
4	✓ 153°0'	234	+1°11'	234	80.55	"
5	✓ 134°20'	208	+0°03'	208	75.69	"
6	✓ 114°15'	238	-0°41'	238	72.68	"
7	✓ 100°15'	230	-0°55'	230	71.83	"
8	✓ 91°35'	198	-1°09'	198	71.53	"
9	✓ 83°45'	200	-1°37	200	69.87	"
10	71°25'	158	-14°10'	149 ✓	35.61	Botm
11	100°20'	148	-14°02	139 ✓	40.70	"
12	132°10'	116	-13°44	109 ✓	48.76	"
13	154°0'	160	-9°45	155 ✓	48.81	"
14	180°55'	168	-8°18	165 ✓	51.51	"
15	✓ 194°0'	162	+0°37	162 ✓	77.26	SW Cor old Lo Jolla Ruins
16	✓ 206°15'	128	+1°35'	128	79.04	Rim
17	✓ 210°15'	78	+2°18'	78	78.64	"
18	✓ 239°35'	36'	+1°53	36	76.69	"

75.51

	Az	Dist	Vert	Hor Dist	Elev	Notes
19	✓ 199°05'	38	+4°0'	38	78.15	Rim
20	✓ 192°05'	68	+2°18'	68	78.24	"
21	✓ 270°15'	120	+2°07	120	79.94	"
22	✓ 287°15'	200	+0°55'	200	78.71	"
23	✓ 279°20'	278	+1°13	278	81.42	"
24	✓ 298°55'	282	+0°39'	282	78.71	"
25	315°25'	286	-0°10'	286	74.68	"
26	332°15'	322	-0°17'	322	73.92	"
27	347°40'	334	-0°35	334	72.11	"
28	✓ 10°45'	338	-0°56	338	70.00	"
29	10°20'	334	-1°09'	334	68.81	"
30	30°30'	358	-1°10	358	68.22	"
31	9°55'	392	-1°03	392	68.32	"

π at F' Elev 63.4 HI = 68.1

1	✓ 359°0'	320	-0°05'	320	62.93	Rim
2	13°55'	304	-0°28	304	60.63	"
3	37°10'	276	-1°08'	276	57.94	"
4	30°30'	400	-0°46'	400	58.05	"
5	32°25'	520	-0°43'	520	56.59	" at Bluff

Note Narrow ridge runs out to Sta F' did not consider it. Should be assessed as canon.

⊼ at F Elev 63.4 HI 68.1

	Az.	Dist	Vert	Hor Dist	Elev	Notes
6	56°05'	532	-6.52	523	0.25	on Bench
7	58°25'	424	-8°36'	414 ✓	0.71	Botm
8	65°15'	354	-9°52'	344 ✓	3.63	"
9	63°0'	268	-11°51'	257 ✓	9.54	"
10	50°0'	220	-13°52'	207 ✓	12.21	"
11	35°50'	180	-16°11'	166 ✓	15.22	"
12	27°25'	154	-18°41	138 ✓	16.67	"
13	16°15'	166	-14°35'	155 ✓	23.37	"
14	331°15'	94	-27°51'	73 ✓	24.58	"
15	275°30'	94	-23°17'	79 ✓	29.27	"
16	268°05'	164	-10°51	158 ✓	33.08	"
17	241°15'	126	-12°32'	120 ✓	36.71	"
18	222°25'	194	-7°28'	191 ✓	38.40	"
19	205°25'	150	+2°34'	150	70.11	Rim
20	175°20'	164	+2°02'	164	69.21	"
21	176°45'	286	+1°52'	286	72.72	"
22	154°40'	208	+1°22	208	68.36	"
23	112°15'	192	-0°12'	192	62.73	"
24	101°15'	256	-0°19'	256	62.00	"
25	88°25'	392	-0°57'	392	56.90	"

⊼ at G Elev 77.04 H.I. 92.10

	Az	Dist	Vert	Hor Dist	Elev.	Notes.
1	328°05'	62	-3°24'	62 ✓	73.37	La Jolla Ry fill
2	332°45'	156	-1°36'	156 ✓	72.68	" "
3	346°20'	232	-0°52'	232 ✓	73.53	Rim
4	6°15'	262	-1°38'	262 ✓	69.57	"
5	351°05'	276	-1°11'	276 ✓	71.35	"
6	336°0'	260	-0°59'	260 ✓	72.58	"
7	352°45'	102	-7°53'	100 ✓	63.18	Botm
8	18°40'	216	-5°44'	214	55.57	"

⊼ at H Elev 64.32 HI = 69.4

	178°35'	204	-3°46'	203 ✓	50.95	" 1
	142°35'	132	-8°0'	129 ✓	46.12	" 2
	92°50'	146	-8°07	143 ✓	43.91	" 3
	71°15'	186	-7°53	182 ✓	39.05	" 4
	60°55'	290	-6°05	286 ✓	33.76	" 5
	45°45'	412	-5°30'	407 ✓	25.01	" 6
	43°20'	314	-6°15'	310 ✓	30.34	" 7
	33°25	244	-6°47'	241 ✓	35.70	" 8
	23°05'	117	-10°43'	108 ✓	43.85	" 9
	342°35'	64	-16°28'	59 ✓	46.92	" 10
	254°25'	88	-8°44	86 ✓	51.11	" 11
	231°05'	186	-2°10	186 ✓	57.29	" 12
	231°50'	340	-0°05'	340	63.87	Top Slope La Jolla Ry. 13

At H Elev 64.32 H.I. 69.40

	Az.	Dist	Vert	Hor Dist	Elev	Notes
14	233°25'	354	+1°00'	354 ✓	70.50	Top Fill on La Jolla Ry
15	250°35'	330	+0°52'	330 ✓	69.31	"
16	244°45'	210	+1°02'	210 ✓	68.11	Rim
17	259°35'	170	+1°20	170 ✓	68.27	"
18	270°35'	114	+0°50'	114 ✓	65.98	"
19	310°45'	184	+0°05'	184 ✓	64.59	"
20	346°30'	214	−0°36'	214 ✓	62.08	"
21	358°15'	304	−0°48	304 ✓	60.78	"
22	17°55'	340	−1°09'	340 ✓	57.50	"
23						
24	182°20'	382	+1°11'	382 ✓	72.21	Rim
25	173°30'	304	+1°05'	304 ✓	70.07	"
26	164°45'	256	+0°56'	256 ✓	68.49	"
27	144°25'	260	+0°19'	260 ✓	65.76	"
28	122°40'	282	−0°55'	282 ✓	59.81	
29	94°30'	290	−2°08'	290 ✓	53.53	
30	70°30'	340	−2°31'	340	49.41	

At I Elev 40.05 H.I. = 45.1

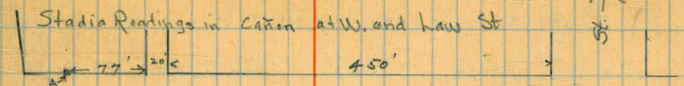
	Az	Dist	Vert	Hor Dist	Elev	on Rim Notes
1	80°10'	72	−0°57'	72 ✓	38.86	Rim
2	77°15'	120	−1°08'	120 ✓	37.68	"
3	41°35'	206	−10°54	199 ✓	1.80	on Beach
4	36°20'	118	−16°16'	109	8.32	Botm
5	325°10'	66	−13°31'	62	25.05	"
6	346°45'	86	−10°12	83	25.07	" Old block cor Marked Nevada St BLK 41
7	11°50'	138	−1°08	138 ✓	37.32	Rim
8	330°10'	150	+1°20'	150 ✓	43.54	"
9	306°10'	218	+4°04	217 ✓	55.48	"
10	286°35'	260	+3°55'	259	57.77	"
11	281°05'	348	+3°22	347	60.45	"

Levels to Law & Chalcedony Sts

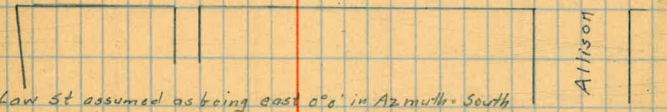
	+	Ht.	−	Elev.
	0.85	77.89		77.04 = Sta 6
T.P	0.48	66.29	12.08	65.81
T.P	0.28	54.68	11.89	54.40
T.P	0.11	42.75	12.04	42.64
A on N.L. Law St			10.55	32.20
A on N.L. Chalcedony St			8.54	34.21

9/20/19 Darin C Moore B Moore

Stadia Readings in Cairn at W. and Law St



Law St



Note - Law St assumed as being east 0°0' in Azmuth - South

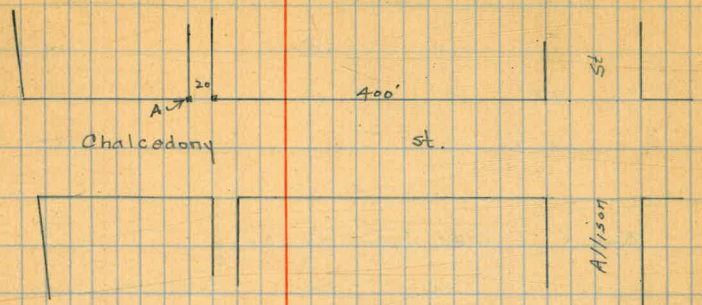
Az	Dist	Vert	Hor. Dist	Elev.	Notes
At A Elev 32.20		H.I. 37.40			
21°15'	156	−0°40'	156	30.38	Rim - Bluff
0°50'	140	−2°06'	109.9	28.17	"
23°0'	104	−2°35'	103.8	27.52	"
39°10'	78	−3°31	77.7	27.42	Rim
152°05'	6	−2°08'	6.0	32.00	"
220°15'	70	−1°02'	70.6	30.94	"
224°30'	116	−0°41'	116	30.88	"
207°50'	116	−0°31'	116	31.16	"
158°55'	74	−1°19'	74	30.50	"
84°55'	90	−2°51'	90	27.73	" Bluff
59°45'	138	−12°17'	138.9	3.51	Bttm - beach
68°05'	60	−20°30'	52.6	12.52	
184°05'	62	−9°37'	60.3	22.0	
205°05'	66	−4°28'	65.6	27.08	

Stadia Readings in Canon at West end of Chalcedony St.

T at A Elev 34.21 HI. 39.30

J. Davis
C. Moore
B. Moore

	Az	Dist	Vert.	Hor. Dist	Elev.	Notes
1	✓ 46° 40'	190	− 1°21'	189.9	29.73	Rim - bluff
2	✓ 38° 55'	116	− 1°15'	116.0	31.68	Rim
3	✓ 30° 05'	32	+ 0°04'	32.0	34.25	"
4	✓ 260° 10'	94	+ 2°28'	93.8	38.45	"
5	✓ 269° 15'	140	+ 3°15'	139.6	44.13	"
6	✓ 283° 10'	144	+ 4°00'	143.4	44.23	"
7	✓ 324° 25'	118	+ 3°58'	117.5	42.35	"
8	✓ 358° 25'	182	+ 2°02	181.8	40.66	"
9	✓ 6° 45'	258	+ 1°08	257.9	39.37	"
10	✓ 18° 15'	310	+ 0°47'	310.0	38.45	Rim - bluff
11	30° 20'	59.00 / 11.71 271	− 3°10'	270.2	19.26	Botm
12	22° 45'	260	− 3°28	259.1	18.52	"
13	13° 40'	160	− 3°27	159.5	24.60	"
14	338° 55'	68	− 4°43	67.6	28.64	"
15	279° 55'	94	− 0°50'	94.0	32.84	Botm



Note: Chalcedony st assumed as being east 0°0' in Azimuth = South.

Stadia in Canon So of Bird Rock City

	0.14	69.18		69.04 - Grade Stake Sta 14+00
T.P.	1.77	59.19	11.76	57.42
Sta A			9.39	49.80

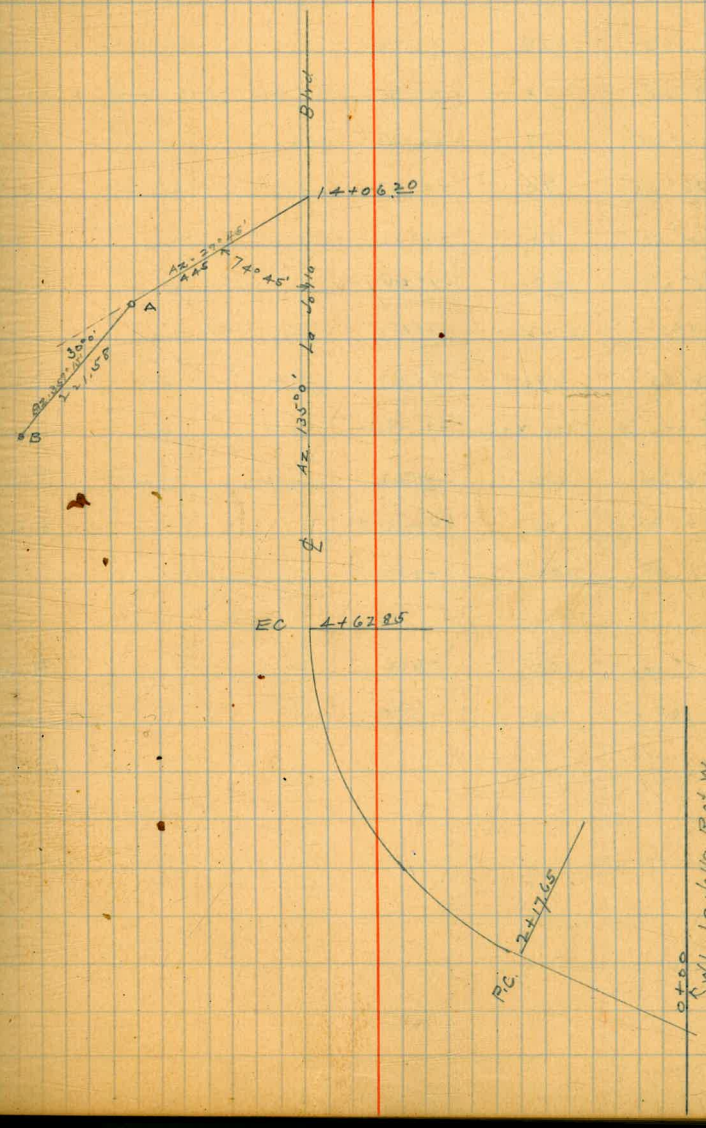
At A Elev 49.80 H.I. 55.0

Az.	Dist.	Vert	Hor Dist	Elev	Notes
359°15'	222	-2°35'	221.58	39.80 = Sta 'B' Rim	
347°10'	164	-2°23			"
335° 50'	110	-0°58			"
299° 15'	108	+0°23'			"
275° 25'	110'	+1°37'			"
258° 10'	100	+2°27'			"
217° 10'	70	+1°30			"
306° 50'	52	+1°08'			"
352° 15'	66	-1°17			"
15°15'	24	-2°35'			"
70°10'	10	-6°42'			"
194°15'	46	+2°42'			"
197°40'	142	+2°20			"
177°10'	152	+1°45'			"
184°40'	182	+2°10			"
178°10'	198	+2°16			"
172°15	192	+2°0'			"
169°0'	276	+2°04			"
174°20	320	+2°0			"

Base Line for Stadia Readings in Canon So of Bird Rock Add.

6/20/19 Davis, C. Moore, B. Moore

30



⊼ at A Elev 49.80 HI. 55.00

Az	Dist	Vert	Hor Dist	Elev	Notes
169°10'	328	+2°05'			Rim
163°45'	278	+2°,4'			"
162°20'	174	+2°30			"
159°35'	88	+1°57			"
122°05'	58'	+2°02'			"
76°05'	70	-0°32			"
32°10'	90	-1°15'			"
35°0'	168	-1°44			"
27°0'	232	-1°40'			"
32°05'	276	-1°31'			"
⊼ at B	Elev 39.80	HI. 44.80			
53°30'	206	-0°05'			Rim
22°30'	170	-12°27			Botm
17°55'	106'	-15°0'			"
0°20'	100'	-6°0'			Rim
18°0'	26'	-5°51'			"

⊼ at B Elev 39.80 HI. 44.80

Az.	Dist	Vert	Hor Dist	Elev	Notes
131°30'	54	-23°28'			Botm x
183°,5'	72	-7°03			"
190°10'	128	-1°0'			"
⊼ at A	Elev 49.80	HI 55.00			
9°50'	196	-8.43			Botm x
13°20'	138	-10°02			"
11°55'	100	-12°26'			"
88°50	46'	-24°02'			"
150°45'	44	-20°55'			"
175°20'	78	-8°10'			"
169°,5'	164	-10°55'			"
166°30'	268	+0°13'			"

6/23/17 Davis, C. Moore, B. Moore

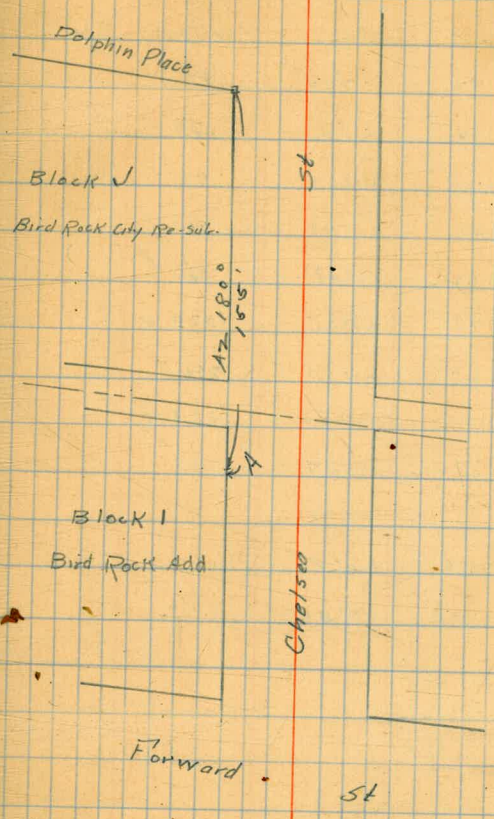
Stadia in Canon W of Chelsea St - tst Forward & Delphin

⊼ at A Elev 60.60 H.I. 65.70

Az.	Dist	Vert.	Hor Dist	Elev.	Notes
0°0'	28'	+6°20'	28		Rim
35°10'	62	+10°47	62		"
67°10'	116	-4°21	115		"
89°20'	156	-6°10'	154		"
90°40'	206	-5°17	204		"
87°55'	296	-4°40	294		"
94°0'	254	-7°34	250		Bottm
94°05'	168	-7°30'	165		"
83°0'	116	-9°06'			"
84°45'	52	-13°41			"
168°45'	74	-5°35			Toe fill
180°0'	66	+1°05	66		Top fill
179°0'	130	+1°41	130		Rim
142°40'	94	+0°37'	94		"
115°40'	104	-1°46	104		"
99°20'	154	-5°06'	152		"
97°45'	230	-5°18'	228		"
93°35'	320	-4°20'	318		"

over

⊼ at A	382	+2°24'	Elev. 60.60	76.58 BM NE Forward	

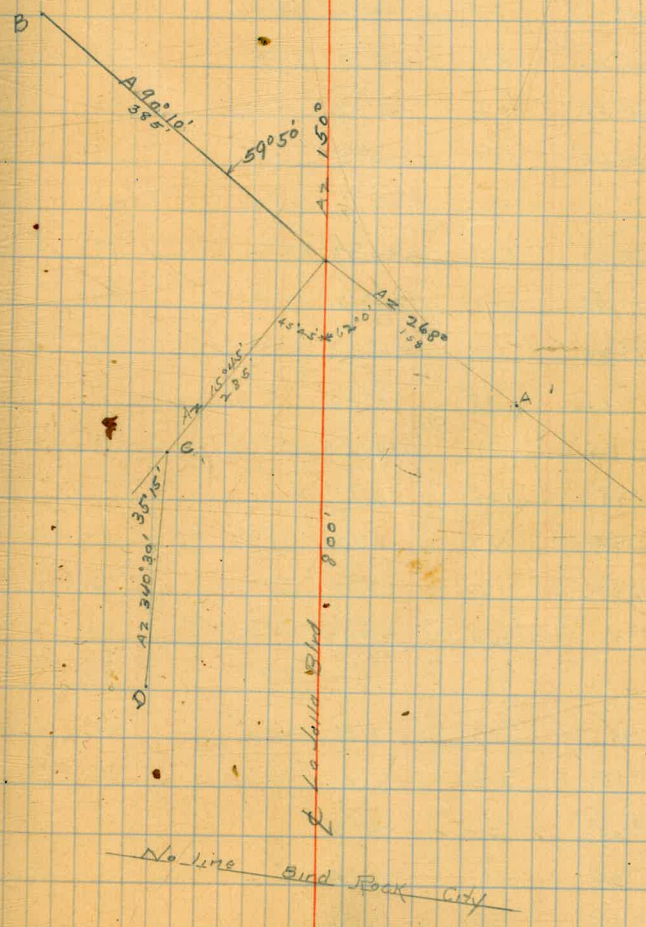


⊼ at A	Elev 606	H.I. 6.5			
Az	Dist	Vert.	Hor Dist	Elev	Notes
225° 20'	82	+2° 52'	82 ✓		Rim
237° 45'	164	+1° 15'	164 ✓		"
239° 05'	258	+1° 56'	258 ✓		"
232° 15'	302	+1° 47	302 ✓		"
230° 30	362	+1° 48'	362 ✓		"
226° 30'	374	+1° 45'	374 ✓		"
221° 15'	298	+1° 55	298 ✓		"
216° 15'	228	+2° 03	228 ✓		"
202° 0'	168	+1° 57'	168		"
221° 30'	158	+0° 28'			Bottom
225° 45'	258	+0° 46'			

6 / 13 / 19 { Davis, C Moore, B Moore

Base lines for Stadia No. of B.R. City.

	+	Hi.	−	Elev
	12.65	86.95		74.30 = Sta B+0.0
Sta A			5.30	81.65
	0.62	74.92		74.30
Sta B			15.10	59.82
Sta C			15.28	59.67



Stadia in Wash East of La Jolla Blvd - No. of B.R. City

At A Elev 81.65 HI 84.95

Az	Dist	Vert	Hor Dist	Elev	Notes
226°25'	172	+3°21'			Rim
230°35'	132	+3°45'			"
223°30'	94	+3°02'			"
194°10'	44	+4°10'			"
35°45'	34	-2°0'			"
40°35'	108	-3°17'			"
44°05'	130	-3°41'			" E. Side
14°30'	160	-3°17'			Rim "
17°50'	122	-3°13'			
350°20'	80	-1°22'			
311°10'	38	+0°05'			
250°05'	72	+2°40			
263°25'	108	+3°11			
244°30'	142	+3°12'			
247°20'	166	+3°31'			
238°0'	166	+3°22			Top La Jolla Rd
238 45'	136	+1°01			Toe Slope "
244°30'	114	0°0'			Bottom
229°05'	72	-4°16'			"
225°55'	18	-32°35'			"
327°55'	24	-26°40			"
6°0'	50	-16°01'			"
240,15'	124	-9°32'			Toe Slope

Stadia in Wash W. of La Jolla Blvd. No. of B.R. City

At C Elev 59.67 HI 64.8

Az	Dist	Vert	Hor Dist	Elev	Notes
340°30'	306	-0°44'	306	55.76	Sta D.
38°10'	200	-5°25'	198		Rim
35°10'	124	-5°51'	123		"
7°55	46	-6°20'	45		"
323°30'	46	-0°27'	46		"
266°05'	44	+1°10'	44		"
Blvd 241°25'	110	+4°25	109		"
240°20'	184	+3°34'	183		W Side Blvd
228°30'	184	+3°43'	183		" " "
220°45'	138	+4°0'	137		"
208°50'	56	+3°43'	56		"
78°30'	61	-6°07'	65		"
56°15'	140	-6°14	138		"
38°15'	116	-14°33'			Bottom
34°10'	66	-19°48'			"
347°0'	24	-28°49'			"
339°05'	68	-11°14'			"
324°25'	112	-4°43			"
334°0'	162	+0°25'			"
La Jolla Blvd.					

At D Elev 5576 H.I 6.0.80

Az	Dist	Vert.	Hor Dist	Elev	Notes
✓ 59°20'	86	−6°40'	85		Rim Wall
✓ 30°05'	22	+0°05'			"
✓ 249°0'	52	+4°30'			"
✓ 255°10'	136	+3°51			"
✓ 245°20'	236	+3°31			"
✓ 231°25'	238	+3°10'			"
✓ 244° 10'	146	+3°03			"
✓ 203°0'	138	+2°30'			"
✓ 190°45'	174	+2°25'			"
✓ 193° 20'	228	+2°33'			"
✓ 195°10'	328	+2°32'			"
✓ 192°15'	276	+2°47			"
✓ 180°50'	228	+2°16'			"
✓ 170°20'	140	+1°25			"
✓ 144°35'	78	−1°36'			"
✓ 108°0'	68	−7°0'	67'		"
87°50'	118	−5°30'			" bluffs
74°55'	118 (8.00 / 11.18)	−12°01'			Botm.
105°15'	46	−28°0'			"
185°35'	58'	−11°05'			" fork
229°45'	98	−0°24			"
238°15'	154 (10.54 / 9.00)	13°16'			"
236° 30'	22	+2°11			"
185°35'	58'	−11°05'			Botm fork
185°45'	142	−0°06'			"
184°25'	214	+1°02'			"
193°0'	258	+1°45'			"
196°35'	294	+2°01'			"

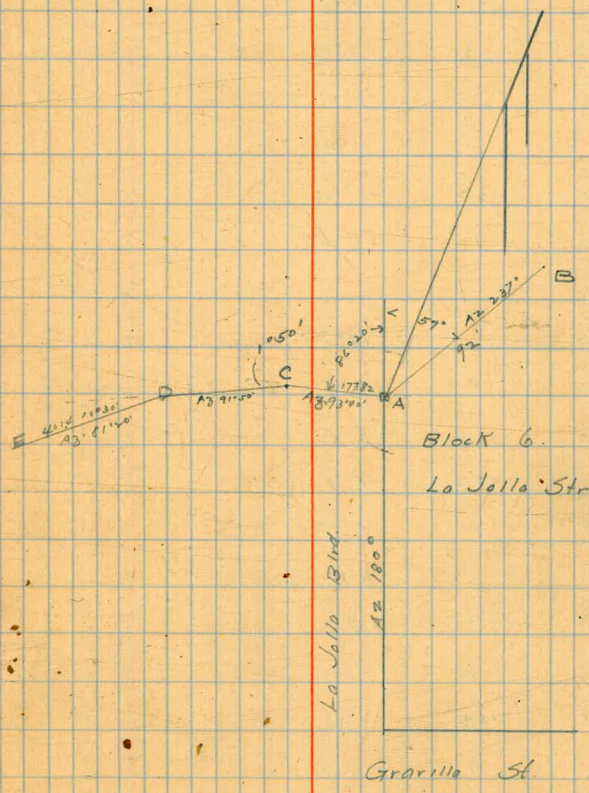
At B	Elev	59.80	HI 64.9		on Rim
Az	Dist	Vert	Hor Dist	Elev	Notes
150°45'	206	-5°06'	✓		Rim
✓ 5°40'	104	-5°54'			"
✓ 353°10'	54	-3°10'			"
✓ 215°45'	62	+1°46'			"
✓ 222°35'	126	+2°10'			"
✓ 214°40'	206	+1°56'			"
✓ 205°35'	208	+1°45'			"
✓ 197°25'	188	+1°40'			"
✓ 197°20'	138	+1°53'			"
✓ 189°40'	130	+1°58			"
✓ 177°55'	180	+1°30			"
✓ 172°35'	190	+1°28'			"
✓ 163°25'	120	+1°47'			"
✓ 165°40'	94	+1°50'			"
✓ 142°45'	102	+1°35'			"
✓ 128°45'	118	+1°30			"
✓ 108°45'	48	+1°46'			"
✓ 77°20'	76	+0°26'			"
✓ 34°20'	118	-5°23'			"
✓ 28°20'	158	-6°25'			"
32°40'	204	-5°26'			"
21°25'	180	-9°54'			Botm
20°50'	104	-12°36'			"
45°20'	48	-12°18			"
131°35'	38	-15°40'			"
188°30'	76	-4°34			"
209°45'	116	-0°55'			"

C 255/19 { Davis, C Moore, B Moore.

Stadia in Canon at La Jolla Strand.

	1.5x	Ht. 70.37		68.85 BM NW Grarilla	
			540	64.97 = A	
T at A	Elev 650'	Ht. 70.40			
Az	Dist.	Vert	Hor Dist	Elev	Notes
237° 0'	92	+1°08'	92	66.8	- B
93°48'	178	-1°47'	177.8	59.46	- C
T at B	Elev 66.8	Ht. 7.47			on Rim
114°30'	58	-3°17'			Rim
304°20'	130	+1°37'			"
295°40'	188	+1°48'			"
281°05'	172	+2°05'			"
281°05'	124	+1°51'			"
248°35'	66	-1°20			"
240°50'	84	-0°30'			"
237°50'	130	+0°12'			"
236°20'	204	+0°57'			"
218°40'	268	+1°17			"
221°10'	210	+1°02			"
230°25'	183	+1°55'			"
222°55'	140	0°0'			"
218°15'	190	+0°35'			"
210°25'	234	+1°05			"
210°10'	336	+0°52'			"
204°10'	418	+0°49'			"
200°25'	450	+0°39'			"

Base Lines for Stadia in Cañon at La Jolla Strand.



La Jolla Strand

⊼ at B Az	Dist	Vert	Hor Dist	Elev	Notes
196°35'	394	+0°41'			Rim
194°55'	338	+0°35'			"
197°50'	328	+0°42'			"
197°55'	284	+0°34'			"
192°50'	230	+0°19'			"
186°05'	206	0°0'			"
188°35'	156	−0°24'			"
174°35'	122	−1°02'			"
154°35'	92	−2°28'			"
152°40'	64	−11°50'			Bottom fork
×173°50'	84	−9°53'			" "
148°50'	118	−5°55'			"
201°15'	152	−3°51'			"
191°25'	12.0 / 10.0 200	−0°50'			"
201°05'	11.25 / 9.0 295	−0°22'			"
202°20'	10.33 / 7.0 333	−0°12'			"
197°05'	11.0 / 7.2 380	+0°20'			"
202°45'	417	+0°13'			"
×173°50'	84	−9°53'			"
230°15'	108	−3°02'			"
234°35'	108.5 / 9.0 185	+1°36'			"
225°20'	10.22 / 8.0 222	+1°22'			"

La Jolla Strand

Az	Dist	Vert	Hor Dist	Elev	Notes
152°40'	64	−11°50'			Bottom
251°45'	9.0 / 9.0 40	−7°40'			"
291°20'	9.88 / 9.0 88	+0°47'			"
291°0'	166	0°0'			"
× ⊼ at C Elev 59.46	Ht. 6.46				on Rim
342°0'	174	+1°20'			"
257°25'	114	+2°0'			"
277°25'	56	+2°37'			"
107°25	64	−3°10'			"
94°25'	130	−2°38'			"
91°50'	218	−2°20'	217.6	50.60	" = D
107°25'	210	−2°50'			"
125°10'	168	−2°31'			"
145°30'	110	−2°28'			"
190°45'	84	−1°20'			"
217°15'	148	+0°22'			"
223°25'	226	+0°55'			"
227°35'	254	+0°32'			"
228°0'	230	−2°24'			Bottom
230°50'	156	−4°35'			
226°10'	98	−8°58'			
205°58'	34	−30°31'			
134°15'	74	−13°21'			
132°20'	98	−10°10'			

La Jolla Strand

⊼ at D Elev 50.60 Ht. 55.80

Az	Dist	Vert	Hor Dist	Elev	Notes
235°15'	112	-4°30'			Botm
173°0'	32	-31°50			"
97°45'	108	-9°51			"
113°25'	170	-6°44'			"
		—			
123°05'	138	-1°46			Rim
109°40'	220	-1°36'			"
89°40'	310	-2°13'			"
81°20'	402'	-2°11'	401.4	35.30	= "E
75°30'	270	-2°11			"
94°0'	156	-1°54			"
71°25'	88	-1°39'			"

⊼ at E Elev 35.30 Ht. 40.40

Az	Dist	Vert	Hor Dist	Elev	Notes
309°20'	40	-5°0'			"
100°15'	76	-4°48'			"
117°45'	138	-4°26			"
125°10'	144	-4°06'			Rim
167°20'	64	-1°42'			"
236°45'	106	+1°49'			"
234°10'	216	+2°30'			"

⊼ at E Elev 35.30 Ht. 40.40

Az	Dist	Vert	Hor Dist	Elev	Notes
248°48'	168	-2°16'			
271°40'	74	-8°19			
281°55'	22	-38°50'			
205°45'	52	-14°49'			
174°10'	78'	-10°57'			
122°05'	144	-6°48'			

7/9/19 Gregory Miller Shaw — CROSS SECTIONS OF AKIN ST from 63 to 64 St — 50' wide 10' obs.

on B.M.	12.5	204.96	192.46	NW 63 + AKIN
	E.L. 63rd St			
So.		6.3	198.7	
cb		10.5	194.5	
1/4		11.2	193.8	
c		11.5	193.5	
1/4		12.5	192.5	
+6.5		12.9	192.9	
cb		16.3	188.7	
+2		16.8	188.2	
N.		17.3	187.7	
	7.23' E on Lo 00' E & No.	= 00		
-15		18.0	187.0	
N		17.3	187.7	
+8		16.8	188.2	
cb		16.3	188.7	
+1		12.9	192.1	
1/4		12.5	192.5	
c		11.3	193.7	
1/4		11.1	193.9	
+5		10.8	194.2	
cb		9.6	195.4	
So		5.4	199.6	
	15' E			
So.		5.1	199.9	
+9		7.4	197.6	

Plotted 7/11/19

cb	9.6	195	4
1/4	10.1	194	9
c	10.0	195	0
+4	11.8	193	2
1/4	12.3	192	7
cb	12.6	192	4
+3	12.4	192	6
+4.5	15.9	189	1
No.	17.0	188	0
+15	16.8	188	2
	+34		
-15	16.6	188	4
-7	17.0	188	0
No.	14.9	190	1
+1	12.0	193	0
cb	12.0	193	0
1/4	11.3	193	7
c	7.8	197	2
1/4	8.2	196	8
+5	8.0	197	0
cb	6.7	198	3
So.	4.8	200	2
	+36		
So.	4.7	200	3
cb	6.6	198	4
+7.5	7.7	197	3

		20+96		
1/4			8.0	197.0
C			7.7	197.3
1/4			11.2	193.8
ob			12.0	193.0
No.			12.0	193.0
+1			14.9	190.1
+7			17.0	188.0
+15			16.6	188.4
		+61		
-11			12.6	192.4
No.			11.8	193.2
ob			7.5	197.5
1/4			5.2	199.8
C			5.0	200.0
1/4			5.7	199.3
+5			6.0	199.0
ob			5.5	199.5
So.			4.0	201.0
		+80		
So.			2.9	202.1
ob			4.7	200.3
1/4			4.7	200.3
C			4.4	200.6
1/4			4.9	200.1
ob			5.3	199.7
No.			10.0	195.0
+4			11.9	194.1
+10			11.3	194.5

	1400	
-15	11.9	193.1
-7	11.3	193.7
No.	9.1	195.9
ob	5.1	199.9
1/4	4.5	200.5
C	3.9	201.1
1/4	3.9	201.1
ob	3.9	201.1
So.	2.0	203.0
	1+22	
So.	2.0	203.0
ob	3.0	202.0
1/4	3.0	202.0
C	3.3	201.7
1/4	3.7	201.3
ob	4.0	201.0
No.	6.6	198.4
+13	10.8	194.2
	1+40	
No.	4.0	201.0
ob	2.6	202.4
1/4	3.0	202.0
C	2.7	202.3
1/4	2.5	202.5
ob	2.6	202.4
So.	2.2	202.8

	204.96		
	1+70		
So.		2.0	203.0
cl		2.4	202.6
1/4		2.7	202.3
C		3.1	201.9
1/4		3.1	201.9
cl		3.4	201.6
No.		3.8	201.2
	2+05		
No.		5.4	199.6
cl		4.4	200.6
1/4		3.6	201.4
C		3.0	202.0
1/4		2.3	202.7
cl		1.9	203.1
So		1.6	203.4
	2+30		
So.		1.3	203.7
cl		1.8	203.2
1/4		1.9	203.1
C		2.2	202.8
1/4		2.6	202.4
cl		3.4	201.6
No.		3.8	201.2

		2+75		
No.			2.4	202 6
cl			1.7	203 3
1/4			1.7	203 3
C			1.3	203 7
1/4			0.8	204 2
cl			0.8	204 2
So.			0.6	204 4
		3+00		
So.			0.3	204 7
cl			0.2	204 8
1/4			1.1	203 9
C			1.3	203 7
1/4			1.8	203 2
+5.5			1.9	203 1
cl			3.2	201 8
T.P.	4.13	207.18	204.96	1.91	203 0.5
No.				10.9	196 3
+15				11.3	195 9
		3+13		
-15				15.0	192 2
-2				14.3	192 9
No.				10.7	196 5
+7				10.1	197 1
cl				7.1	200 1
+5				4.5	202 7

		207.18		
1/4			4.3	202.9
C.			3.9	203.8
1/4			3.6	203.6
ab			2.9	204.8
So			2.5	204.7
		3+16		
So.			2.6	204.2
ab			2.9	204.8
+2			3.1	204.1
1/4			3.6	203.6
C			3.6	203.6
1/4			4.3	202.9
+2.5			4.4	202.8
ab			6.9	200.3
+4			9.5	197.7
+9			10.8	196.4
No.			14.7	192.5
+15			15.0	192.2
		3+31		
-15			14.7	192.5
No.			15.2	192.0
+7			16.5	190.7
ab			5.6	201.2
1/4			3.3	203.9
C			3.9	203.8
1/4			3.7	203.5

	217.2		
ab		2.5	204 7
So.		2.7	204 5
	3+39		
So.		2.7	204 5
ab		2.5	204 7
+2		2.6	204 6
1/4		3.7	203 5
C		3.2	204 0
1/4		4.0	203 2
+5		16.6	190 6
ab		16.0	191 2
No.		14.5	192 7
+15		11.6	195 6
	3+43		
-15		11.7	196 1
No.		13.0	194 2
+2		12.9	194 5
+5		14.8	192 4
ab		15.9	191 3
+4		16.7	190 5
1/4		5.4	201 8
+2		3.9	203 3
C		3.2	204 0
1/4		3.7	203 5
ab		2.6	204 6
So.		2.7	204 5

217.18

3+55

So.		2.8	204.2
cl		2.7	204.5
1/4		3.8	203.4
+6.5		3.6	203.2
C		6.0	201.2
+6.5		15.4	191.8
1/4		15.5	191.7
cl		15.4	191.8
+2		12.4	194.8
No.		11.0	196.2
+15		10.9	196.3.
	3+63.36 on So 3+70.59 ~ No	} = W.L. STORK ST.	
-15		10.7	196.5
No.		10.6	196.6
+5		11.6	195.6
+8		16.1	191.1
cl		16.2	191.0
1/4		14.9	192.3
+2		13.6	193.6
C		6.5'	200.7
+1		3.7	203.5
1/4		3.7	203.5
cl		2.8	204.4
So.		2.7	204.5

For Stork St see Book 1026

AKIN 45

207.18

E. L. STORK

So		2.2	205 0
cl		2.4	204 8
1/4		3.8	203 4
C		5.2	202 0
1/4		5.5	201 7
cl		6.4	200 8
No.		5.46	201 72 = Top of 3" cement walk.
	50' E of No. 57.29 ~ So	= 00	
No.		4.93	202.25 = Top walk
cl		4.7	202 5
1/4		4.5	202 7
C		4.3	202 9
1/4		3.7	203 5
cl		3.3	203 9
So		2.7	204 5
	+ 50'		
So		2.1	205 1
N		2.9	204 3
1/4		3.0	204 2
C		3.4'	203 7
1/4		3.9	203 3
cl		4.1	203 1
No		4.49	202 7 = Top walk

		2+78			
		1+00			
No.			4.00	203.2	= Top walk
ob			3.6	203.6	
1/4			3.6	203.6	
c			3.4	203.8	
T.P.	6.87	210.70	3.35	203.83	
1/4			6.3	204.4	
ob			6.0	204.7	
10			5.4	205.3	
		1+50			
10.			5.3	205.4	
ob			5.3	205.4	
1/4			5.7	205.0	
c			6.1	204.6	
1/4			6.3	204.4	
ob			6.4	204.3	
+3			7.0	203.7	
No			7.02	203.68	Top walk
		2+00			
N			6.89	203.81	✓ L
+7			6.8	203.9	
ob			6.2	204.5	
1/4			5.9	204.8	
c			5.6	205.1	
1/4			4.9	205.8	
ob			4.6	206.1	

	210.7			
S		4.4	206 3	
	2+50			
S		3.7	207 0	
ob		4.8	205 9	
1/4		5.3	205 4	
c		6.3	204 4	
1/4		6.5	204 2	
ob		6.9	203 8	
+2		7.6	203 1	
+7		6.94	203.76	= walk
N		7.01	203.69	= ✓
	3+00			
N		6.70	204 00	= ✓
ob		6.9	203.8	
1/4		6.8	203 9	
c		6.4	204 1	
1/4		6.0	204 7	
ob		5.1	205 6	
S		4.3	206 4	
	3+85			
S		4.1	206 6	
ob		5.4	205 3	
1/4		6.1	204 6	
c		6.6	204 1	
1/4		6.6	204 1	
ob		6.5	204 2	
N		6.4	204.3	= walk

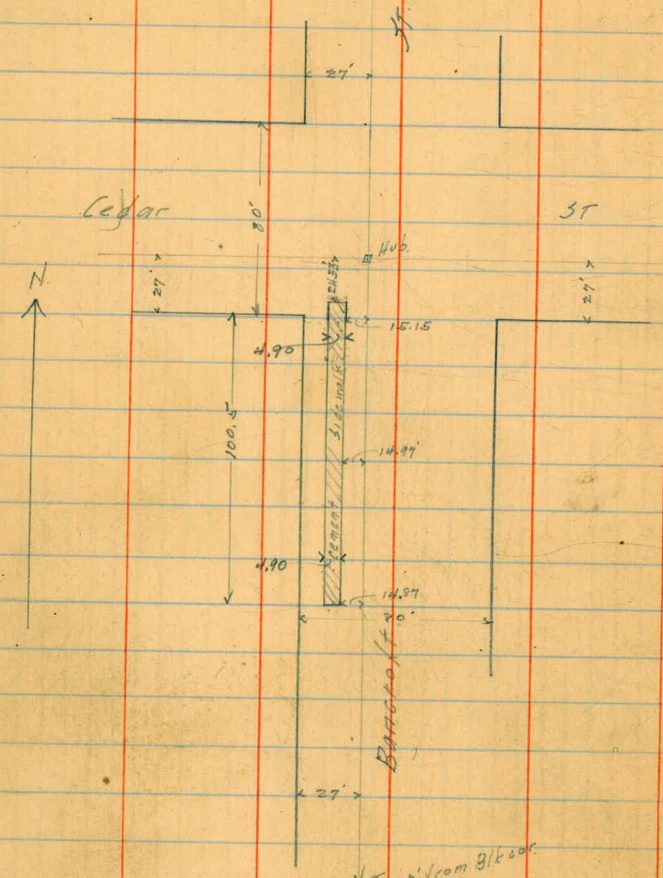
210.7

405.6 on No. } = W.L 64th
398.37 - So }

No.	6.30	204.4 = walk.
cb	6.5	204.2
1/4	6.5	204.2
c	6.4	204.3
1/4	5.8	204.9
cb	4.9	205.8
So.	2.9	207.8

8/23/19 Gregory Miller Shaw

Survey to Locate S/W on West Side Bancroft bet. Beech + Cedar



Levels on walk shown on opposite page.

8.96 Zh3.66 N34.70 Mon SE 33+ Cedar

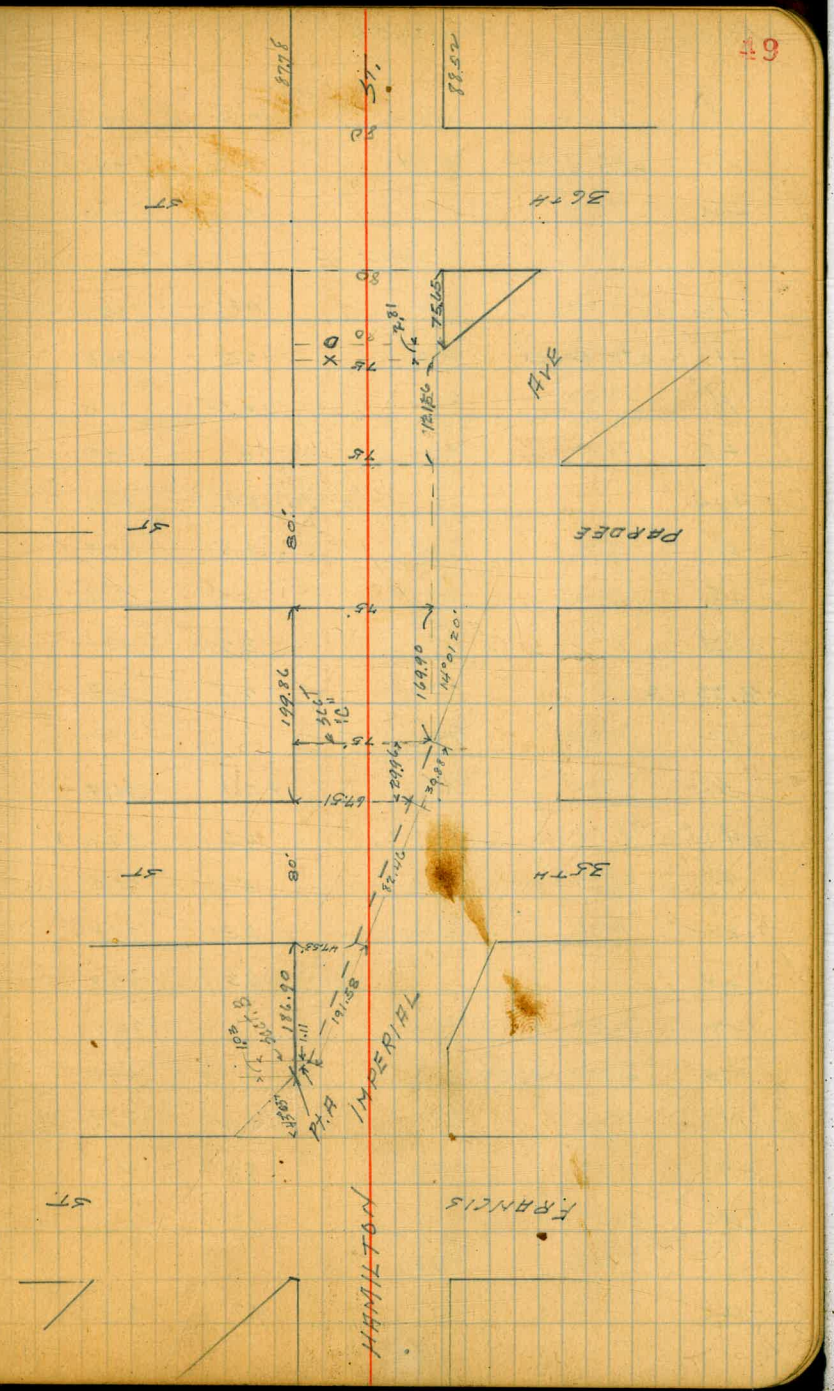
	Outside edge rod	Outside edge elev	Inside edge rod	Inside edge elev
No. end of walk = 2.67 S of SL Cedar	3.95	239.71	3.80	239.86
30. L. of Cedar	3.93	239.73	3.78	239.88
23.3 So. " "	3.85	239.81	3.67	239.99
35' " " "	4.16	239.50	4.01	239.65
48.5 " " "	4.47	239.19	4.32	239.34
77' " " "	6.1~	237.54	6.07	237.59
100.5 " " " = So end walk	7.95	235.71	7.86	235.80

9/6/19 Gregory Miller Folke.

CROSS SECTION OF HAMILTON ST. from Imperial Ave to N.L. of Cemetery

14' cb on 13' 1/4's N

	10.35	36.76	26.41	3E 36th + Imperial
	with NL of Ham.			
PT A = Intersection of	NL Imperial	7.7	29.1	
	1.03' E = SECT. B			
N.		7.8	29.0	
+1.11 = S = NL Imperial		7.8	29.0	
	30' E of SECT B.			
N		9.1	27.7	
+7.6 E S = NL Imperial		8.7	28.1	
	70' E of B.			
S = NL Imperial		8.7	28.1	
+3.85 = N cl		8.9	27.9	
+4		9.3	27.5	
N		9.3	27.5	
	95' E of B.			
N		9.7	27.1	
+9		9.6	27.2	
cl		8.0	28.8	
+21.23 S = NL Imperial		6.6	30.2	
	107' E			
S = NL Imperial		4.3	32.5	
+1.29 = N 1/4		4.4	32.4	
+3		5.7	31.1	
cl		7.1	29.7	
+2		7.4	29.4	
+6		9.8	27.0	



	3676	
N	10.3	26.5
+10 = ctr creek	12.7	24.1
+20	10.1	26.7
	115' E	
-12	9.8	27.0
-1 = ctr creek	12.3	24.5
N	12.2	24.6
+8	10.1	26.7
+12	6.9	29.9
cb	6.5	30.3
+8	5.7	31.6
1/4	3.7	33.1
+2.33 = S	2.5	34.3
	125' E	
S	+0.1	36.9
+4.88 = 1/4	2.6	34.2
cb	5.8	31.0
+12	6.3	30.5
+4	9.3	27.5
+7	11.3	25.5
+13 = ctr creek	12.2	24.6
N	12.2	24.6
+7	9.7	27.1
+10	9.7	27.1
	136' E	
-10	9.7	27.1

-1	9.5	27.3
N	11.5	25.3
+5 = ctr creek	12.0	24.8
+9	11.8	25.0
cb	8.2	28.6
+1	5.0	31.8
1/4	2.6	34.3
T.P. 82 N 38.80	6.18	30.55
+7.68 = S	1.2	37.6
	140' E	
S	1.1	37.7
+8.70 = 1/4	4.5	34.3
+12	7.6	31.2
cb	10.8	28.0
+5	14.7	24.1
+8 = ctr creek	14.8	24.0
+13	13.7	25.1
N	11.5	27.5
+10	11.8	27.0
	160' E	
-10	11.4	27.4
N	11.1	27.7
cb = ctr creek	13.9	24.9
+5	10.3	28.5
1/4	11.2	27.6
C	4.6	34.2
+0.8 = C	4.0	34.8

38.80

175' E

S	6.0	32.8
+4.63 = C	8.9	N29.9
+5	10.8	N28.0
1/4	12.1	N26.7
+3 = S edge creek	13.3	N25.5
+9 = N " "	13.5	N25.3
cb	12.1	N26.7
N	10.7	N28.1
+10	11.1	N27.7

185.87' E = W.L. 35th St 80 iride 1/4 cbs

-10	10.5	N28.3
N	10.4	N26.4
+8	11.3	N27.5
cb	11.0	N27.8
+5	11.6	N27.2
+8 = N edge creek	13.5	N25.3
1/4	13.3	N25.5
+1 = S edge creek	13.3	N25.5
C	10.7	N28.1
+7.53 = S	8.5	30.3
11.10		

W cb

S	9.5	N29.3
+9	10.1	N28.7
+11.1 = C	11.2	N27.6
+5 = S. Edge Creek	13.1	N25.7
+11 = N Edge creek	13.3	N25.6
1/4	12.3	N26.5
+3	10.8	N28.0
cb	10.1	N28.7
N	10.6	N28.2
+10	9.8	N29.0

W. 1/4

-10	9.5	N29.3
N	9.8	N29.0
cb	9.5	N29.3
1/4	10.3	N28.5
+2	10.5	N28.3
+8 = N. Edge Creek	13.0	N25.8
C = ctr. creek	13.0	N25.8
+1 = S Edge "	12.7	N26.1
+5	11.2	N27.6
1/4	9.6	N29.2
+1.41 = S	9.3	N29.6

center 35th

S	9.6	N29.2
+4.93 = 1/4 = S. Edge Creek	13.0	N25.8
C = N edge Creek	12.0	N26.8
+7	10.2	N28.6
1/4	9.9	N28.9
cb	9.3	N29.5
N	9.6	N29.2
+5	9.5	N29.3

38.80

E. 1/4

-5	9.2	29.6
N	9.4	29.4
cb	9.2	29.6
1/4	9.6	29.2
+8	10.1	28.7
c	11.2	27.6
+9 = ctr creek		
1/4 =	12.6	26.2
+2 = S edge ✓	12.7	26.1
+4	8.9	29.9
+8.04 = S	7.6	31.2

E Cb.

S	6.5	32.3
+5	8.6	30.2
+8 = S. Edge Creek.	12.2	26.6
+11.36' 1/4 = Center ✓	12.3	26.5
c	10.9	27.9
1/4	9.5	29.3
cb	9.1	29.7
N	9.2	29.6

E.L. 35+4 St.

N	9.1	29.7
cb	8.6	30.2
1/4	9.1	29.7
c	10.9	27.9
+5 = N edge creek	12.3	26.5'
+9 = ctr ✓	12.2	26.6
1/4	11.9	26.9
+10	9.4	29.4
cb	6.4	32.4
+0.93 = S	5.6	33.2

10' E of E L.

S	4.9	33.9
+3.48 = cb	7.3	31.5
+4	9.7	29.1
1/4	11.0	27.8
+6 = S edge creek	12.4	26.4
+11 = N ✓ ✓	12.4	26.4
c	11.4	27.4
1/4	9.2	29.6
cb	8.8	30.0
N	8.9	29.9

29.96' E = SECT. C

N	8.6	30.2
cb	8.6	30.2
+9	8.9	29.9
1/4	9.9	28.9
+6 = N edge Creek.	12.2	26.6
+11 = S ✓ ✓	12.5	26.3
c	11.4	27.4
+8	9.6	29.2

38.80

1/4	9.7	29.1
+9	9.2	29.6
cb.	6.4	32.4
+9 = S.	2.7	36.1
25' E. of SECT C.		
S	3.3	35.5
+9 = cb	5.5	33.3
+2	6.7	32.1
1/4	8.2	30.6
C	9.4	29.4
+6	10.6	28.2
+9 = S edge Creek	12.3	26.5
1/4 = N ~ ~	12.1	26.7
+7	9.5	29.3
cb.	8.5	30.3
N	8.3	30.5
50' E		
N	7.9	30.9
+11	8.9	29.9
+12 = N edge creek	11.5	27.3
cb	11.7	27.1
+8 = S ~ ~	11.6	27.2
1/4	10.1	28.7
C	8.5	30.3
1/4	7.6	31.2
cb	6.2	32.6
+9 = S	1.7	37.1

75' E

S	0.4	38.4
+9 = cb	5.6	33.2
1/4	6.8	32.0
C	7.7	31.1
1/4	8.9	29.9
+8	9.7	29.1
+10 = S Edge creek	11.3	27.5
cb.	11.7	27.1
+3 = N ~ ~	11.6	27.2
+7	9.3	29.5
N	7.9	30.9
100' E		
-10	7.7	31.1
N	8.7	30.1
+3	9.7	29.1
cb	9.4	29.4
+3 = N Edge Creek	11.0	27.8
+12 = S ~ ~	10.7	28.1
1/4	8.0	30.8
C	7.0	31.8
1/4	5.7	33.1
+10	4.7	34.1
cb	3.7	35.1
T.P. 11.86 30.19	0.47	38.33
+9 = S	9.9	40.3

50.19

108' E

S	10.0	40.2
+9 = cb	15.0	35 ±
+6	16.2	34.0
1/4	17.0	33.2
C	20.0	30.2
+7 = S edge Creek	22.5	27.7
1/4 = ctr ~	22.8	27.4
+5 = N edge ~	227	27.5
cb	20.2	30.0
+12	20.7	29.5
N	19.9	30.3
+10	19.8	30.4

125' E

-10	19.3	30.9
N	19.8	30.4
+1	21.2	29.0
cb	20.1	30.1
+9	19.0	31.2
1/4	20.6	29.4
+4 = N edge Creek	21.9	28.3
+9 = S ~ ~	21.9	28.3
C	19.8	30.4
+10	18.1	32.1
1/4	15.6	34.6
+12	14.4	35.8

cb	12.8	37.4
+9 = S	8.8	41.4

150' E

S	9.0	43 ±
+9 = cb	10.2	40.0
+1	12.5	37.7
+3	13.4	36.8
1/4	14.4	35.8
+3	14.6	35.6
+6	17.5	32.7
C	18.9	31.3
+5	20.0	30 ±
+7 = S edge Creek	22.7	27.5
1/4 = N ~ ~	22.5	27.7
+2	19.7	30.5
cb	19.0	31 ±
+6	19.7	30.5
+8	22.0	28 ±
N	21.0	29 ±
+10	19.3	30.9

169.9' E = W. L. PARDEE 80 wide in walks

-10	19.1	31.1
N	20.0	30 ±
cb	19.6	30.6
+6 = N edge Creek	21.3	28.9
1/4	21.1	29.1
+4 = S ~ ~	21.0	29.2

50.19

C	15.2	35.0
+4	13.6	36.6
1/4	12.6	37.6
+6	12.0	38.2
cb	9.1	41.1
+9 = 5	6.0	44.2
W. Cb.		
5	5.3	44.9
+3	7.1	43.1
+9 = cb	8.4	41.8
1/4	12.7	37.5
C	13.0	37.2
1/4	16.0	34.2
+7	18.5	31.7
+8 = 3 Edge Creek	21.0	29.2
cb = N " "	21.4	28.8
+8	19.1	31.1
N	19.0	31.2
+10	19.1	31.1
W. 1/4		
-10	18.2	32.0
N	19.0	31.2
+9 = otr creek		
+12 = S. Edge "	21.4	28.8
cb	16.3	33.9
1/4	14.7	35.5

+7	13.0	37.2
C	12.8	37.4
1/4	10.8	39.4
cb	8.2	42.0
+5	6.9	43.3
+9 = 6	4.4	45.8
Ctr Pardee		
5	3.6	46.6
+9 = cb.	6.7	43.6
1/4	9.4	40.8
C	12.8	37.4
1/4	13.3	36.9
cb	15.2	35.0
+5	15.9	34.3
+7 = 3 Edge creek	21.4	28.8
N	20.4	29.8
+3 = N. " "	20.0	30.2
+15	18.5	31.7
10' E of C		
-15 = W edge creek	20.2	30.0
N	20.4	29.8
+12	16.2	34.0
cb	14.7	35.5
11' E		
N cb	14.6	35.6
N	16.3	33.9

5019

+12 = 3 Edge creek	20.2	30.0
+15	20.2	30.0
E 1/4	creek Turns Northerly	
-40 = ctr creek	19.9	30.3
-15 = ctr creek	20.4	29.8
-4 = 3 edge creek	20.4	29.8
N	16.0	34.2
cb	14.6	35.6
1/4	18.0	37.2
C	12.2	35.0
+6	9.7	40.5
1/4	8.5	41.7
cb	5.6	44.6
+5	4.5	45.7
+9=3	2.6	47.6
E Cb		
3	1.7	48.5
+9=cb	4.9	45.3
1/4	7.4	42.8
C	9.9	40.3
+6	12.5	37.7
1/4	12.6	37.6
cb	13.3	36.9
N	15.1	35.1
+10	16.2	34.0

E. L. PARDEE

-10	15.1	35.1
N	13.7	36.5
cb	13.2	37.0
1/4	12.1	38.1
+4	11.6	38.7
+6	9.7	40.5
C	8.7	41.5
1/4	6.1	44.1
2 +11	4.0	46.2
cb	2.8	47.4
T.P. 12.12 61.39	0.92	49.27
3	10.5	50.9
20° E		
3	7.7	53.7
9=cb	11.0	50.4
1/4	15.1	46.3
C	18.1	43.3
+3	19.5	41.9
+10	20.9	40.5
1/4	22.0	39.4
cb	23.1	38.3
+3	24.1	37.3
N	24.7	36.7
+5	25.2	36.2

61.39

40' E

-5	24.9	36.5
N	24.5	36.9
+8	23.3	37.1
+11	22.4	39.0
cl	22.0	39.4
+7	21.4	40.0
1/4	19.5	41.9
+6	18.1	43.3
+10	14.1	47.3
c	13.8	47.6
1/4	9.9	51.5
cl	6.7	54.7
+9=5	3.7	57.7

60' E

5	+1.4	62.8
+9=cl	1.3	60.1
1/4	5.5	58.9
c	9.9	51.5
+8	13.3	49.1
+8.3	14.1	47.3
1/4	17.5	43.9
+4	19.3	42.1
+9	20.4	41.0
cl	20.6	40.8
+5	21.0	40.4

+9	23.2	38.2
N	23.4	38.0
+1	23.4	38.0 = house

70' E

-1	23.4	38.0 = house
N	23.4	38.0
+4	23.4	38.0
+9	21.0	40.4
cl	21.0	40.4
+3	20.9	40.6
+10	18.4	43.0
1/4	16.1	45.3
+3	12.3	49.1
c	9.1	52.3
1/4	4.8	56.6
cl	+0.4	61.8
+8	+1.7	63.1
+9=5	+2.1	63.5

80' E

5	+1.9	63.3
+9=cl	+0.4	61.8
1/4	4.6	56.8
c	9.2	52.2
+11	12.9	48.5
1/4	15.5	45.9
+10	21.3	40.1
cl	21.5	39.9

		61.39		
+5			21.4	40.0
N			23.1	38.3
+1			23.1	38.3 = house
		93' E		
-5			23.5	37.9
N			23.3	38.1
cb			22.7	38.7
+3			22.3	39.1
1/4			18.0	43.4
C			14.1	49.3
1/4			6.8	54.6
cb			1.4	60.0
+9=5			+0.7	62.1
		105' E		
5			1.9	59.5
+9=cb.			5.0	56.4
1/4			9.6	51.8
C			16.0	45.4
+5			17.5	43.9
1/4			21.4	40.0
+6			24.6	36.8
cb			24.4	37.0
N			24.5	36.9
+5			24.8	36.6

		141.56' E = SECTION X		
N				under shed
+4			24.4	37.0 shed
cb			25.0	36.4
1/4			24.8	36.6
+8			24.1	37.3
+9			21.5	39.9
C			20.4	41.0
1/4			14.9	46.5
cb			10.0	51.4
+9=5			7.0	54.4
		124.37' E = SECTION Y		5' 13 80' wide
				x from here on
5			5.4	56.4
cb			10.7	40.7
1/4			15.5	45.9
C			21.1	40.3
+4			22.6	38.8
+5			24.1	37.3
1/4			25.0	36.4
cb			25.0	36.4
+9			24.4	37.0 shed ~~house~~
N			—	under ~~house~~ shed
T.P.	1.19	50.51	1.17	49.22
		140' E		
N			13.6	36.9
cb			14.1	36.4

		50.51		
1/4			14.1	36.4
+11			13.6	36.9
C			12.6	37.9
1/4			9.5	41.0
dr			4.5	46.0
+14 = S			+0.3	50.8
		155' E		
S			4.0	46.5
dr			9.2	41.3
+7			11.3	39.2
1/4			12.1	38.4
T.P.	5.86	43.79	12.58	37.93
C			6.7	37.1
1/4			6.7	37.1
dr			6.9	36.9
N			6.9	36.9
		170' E		
N			6.6	37.2
dr			6.3	37.5
1/4			6.2	37.6
C			5.6	38.2
1/4			4.5	39.3
dr			3.4	40.4
+9			2.3	41.5
S			1.5	42.3

200 E = W.L. 36th St 80' wide

S	4.5	39.3
dr	4.5	39.3
1/4	5.2	38.6
C	5.8	38.0
1/4	5.4	38.4
dr	5.5	38.3
N	5.8	38.0
West Curb		
N	5.9	37.9
dr	5.7	38.1
1/4	5.1	38.7
C	5.5	38.3
+8	6.2	37.6
1/4	6.0	37.8
dr	5.6	38.2
S	4.8	39.0
West Quarter		
S	4.5	39.3
+10	5.5	38.3
dr	6.7	37.1
1/4	6.5	37.3
C	5.3	38.5
1/4	5.1	38.7
dr	5.3	38.5
N	5.7	38.1

4379

Center 36th

N	5.6	38.2
cl	5.2	38.6
1/4	4.9	38.9
C	4.9	38.9
1/4	6.3	37.5
+3	6.9	36.9
cl	6.8	37.0
+8	5.5	38.3
S	5.1	38.7

East Quarter

S	5.1	38.7
+11	5.4	38.4
cl	6.1	37.7
+3	6.8	37.0
+8	6.9	36.9
1/4	5.5	38.3
C	4.7	39.1
1/4	4.8	39.0
cl	5.1	38.7
N	5.3	38.5

East Curb

N	5.1	38.7
cl	4.8	39.0
1/4	4.7	39.1
C	4.5	39.3
1/4	5.2	38.6
+7	6.9	36.9
cl	6.9	36.9
+5	5.9	37.9
S	5.2	38.6

East Line 36th St

S	5.6	38.2
+5	5.9	37.9
+8	7.3	36.5
cl	6.9	36.9
+5	5.5	38.3
1/4	4.6	39.2
C	4.3	39.5
1/4	4.5	39.3
cl	4.6	39.2
N	4.5	39.3

15' E

N	4.0	39.8
cl	4.0	39.8
1/4	3.9	39.9
C	3.9	39.9
1/4	4.3	39.5
cl	4.8	39.0
+4	5.7	38.1
+6	7.1	36.7
+10	6.9	36.9
50	5.9	37.9

	43.79		
	30' E		
-5		6.8	37.0
3		7.1	36.7
+6		4.9	38.9
cl		4.4	39.4
1/4		3.9	39.9
c		3.6	40.2
1/4		3.4	40.4
cl		3.3	40.5
N		3.5	40.3
	35' E		
N		3.1	40.7
+7		3.5'	40.3
cl		2.9	40.9
1/4		3.2	40.6
c		3.4	40.4
1/4		3.9	39.9
cl		4.6	39.3
S.		5.0	38.8
	65' E		
S		4.3	39.5
cl		3.9	39.9
1/4		3.5	40.3
c		3.1	40.7
1/4		3.1	40.7
cl		2.6	41.2
N		2.3	41.5

	83' E		
N		2.5	41.3
cl		3.0	40.8
1/4		3.2	40.6
c		3.4	40.4
1/4		3.8	40.0
cl		4.2	39.6
S		4.5	39.3
	88.5 W E on S 87.78 ↓ ↓ N = East End of Street		
S		5.3	38.5
cl		5.3	38.5
1/4		5.2	38.6
c		4.5'	39.3
1/4		5.43	38.36
		3.7	40.1
		3.1	40.7
cl		2.9	40.9
N		2.8	41.0
	0.18 40.20	3.77	40.02
	chk BM.	13.78	26.42

19' Mon

9/25/19 Gregory Miller Shaw

Cross Section of Glenwood Drive Entire Length 40' ST 5' cbs

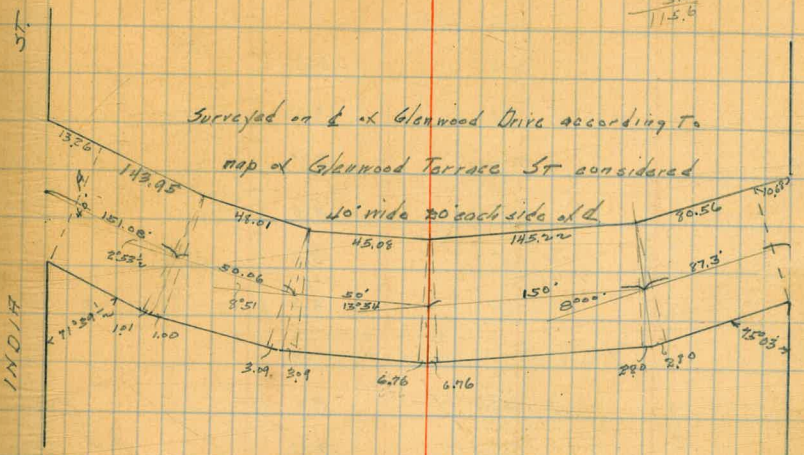
Taken 30' on each side of ℄ of Drive as shown on map. Map does not make at 40' wide.

B.M.	11.78	81.84		70.06	BP NW India + Willow
	E.L. India				
N			4.5		
cb			4.9		
	on cement cb		(5.18)		
+ 2			5.4		
1/4			5.0		
C	on pavement		5.0		
1/4			4.9		
cb	on cement cb		3.94		
30			3.7		
	Section A = 0+00				
S			3.7		
cb			3.7		
1/4			4.8		
C			4.9		
1/4			4.9		
+4			5.2		
cb			4.7		
N			4.3		
		+15			
N			4.2		
cb			4.6		
+4			4.9		
1/4			4.7		

±6.5 To steps
42.8 "
28.8 " Garage

4+50
+70

8 8 8
3 4
8 5 4
3 3 C
11 4.0
3.4
11 5.6



C		4.5
+6		4.7
1/4		4.5
cb		3.9
+4		4.1
S		4.7
	+50	
-15		11.4
-5		10.4
S		6.2
+1		4.3
cb		4.1
1/4		4.1
C		3.9
1/4		4.0
cb		4.2
N		3.9

81.8 ✓

1+00

N		3.3
cl		3.5
1/4		3.5
C		3.3
+6		3.7
1/4		3.3
cl		2.7
S		3.8
+10		10.8
+20		10.3

1+18 = steps on N.

bottom step 2.48

on ground 3.00

1+43.95 on N
1+44.96 ~ S } = Angle pt.

wall is .6 in street here.

N + 0.6		2.6
cl		2.6
1/4		2.9
C		2.7
1/4		3.0
+4		2.3
cl		2.6
S.		2.3

36.5' E of Angle pt

S. 2.2

cl		1.5
1/4		2.1
C		2.1
1/4		2.3
cl		2.0
N		1.6

on bottom step 0.8

48.01 E on N
52.10 ~ S } = Angle pt.

N		1.5
cl		1.7
+6		2.2
1/4		2.0
C		1.9
1/4		2.2
cl		1.1
S		1.9

45.08 E on N
54.93 ~ S } = Angle pt.

S		0.8
cl		0.7
1/4		1.0
C		0.7
1/4		1.0
cl		0.5
T.P. 1+87 9 to N		0.69 81.15
N		1+3

94.0 ±

40.0 E on N } = steps on N
46.8 - - S }

N	on ground	10.1
	bottom step.	9.5
cl		10.6
1/4		11.0
+3		11.5
C		11.2
1/4		11.3
+6		11.5
cl		9.9
S		9.0

31' E of Last Section

S	7.4
cl	8.0
+1	9.8
1/4	9.2
C	9.3
+2	9.6
1/4	8.5
cl	8.1
N	8.1

15' E. of Last Section = center garage

N = elev of dirt floor	6.1
cl	7.0
1/4	7.9
+4	8.2

Glenwood 64

C	8.0
+4	7.9
1/4	8.2
cl	8.3
+0.5	6.8
S	6.4

34' E of Last Section

S	3.9
+4	4.2
cl	5.9
1/4	5.3
C	5.3
+6	5.6
1/4	5.0
cl	4.9
N	4.7

25.22 E of Last Sect. on N }
28.02 - - - - - S } = Angle pt.

N	4.8
cl	2.9
1/4	3.5
C	3.1
1/4	3.3
+6.5	3.6
cl	2.2
S	1.7

T.P. 807 101.60 0.49 93.53

		101.6	
		25' E on N 26.40 " S	
S			7.0
+2.9			7.5
+3.0			9.3
cl			9.3
1/4			8.6
C			8.6
+4			9.2
1/4			8.9
cl			8.3
N			7.8
		25' E of last Sect.	
N			5.5
cl			5.7
+4			5.9
1/4			6.5
C			6.1
1/4			6.0
cl			6.8
+1			6.9
+1.1			5.3
S			5.2
		20' E of last Sect.	
S			2.7
cl			3.1
+1			4.7

1/4	3.8
C	3.9
1/4	4.8
+2	4.8
+5	3.3
cl	3.3
N	2.7
21.24' E of last Sect. on N 10.56' " " " " S	= W.L. STATE ST.
N	0.9
+1	2.6
cl	2.6
1/4	2.2
C	2.0
+4	2.1
1/4	2.7
+3	3.4
cl	1.1
S	0.3

10/4/19 SECOND ST NOTES

Curb in on N side 2nd 3.50' N. of NUTMEG

PAVE TO 280' NO. OF NUTMEG.

PIPE IN ON W GUTTER FROM 284 TO 305'

INLET IN FAIR SHAPE

Cement gutter on West Side from NL Laurel to 150' N { 5' wide 10" deep dip in center } N.G.

" " " East " " " " " 150' No { 5' wide 8" deep dip in center } N.G.

50' " " " " " 100' N of Kalmia { 3' wide 8" deep No dip } Might use this piece

granite curb opposite above gutter. should be replaced or straightened

Curb on E. side from 88' S of grate to 145.5 is out + broken.

B.M.	0.10	157.13		157.03	NW 2nd + Fir
W. end of SW ret. 2nd + Fir			3.38	153.75	
str. of SW " " "			2.84	154.29	
3 end. " " " "			3.10	154.03	
15.5' So. of Fir W. Cb			4.96	152.17	
22.5 " " "			5.4	151.73	
57' " " "			7.24	149.89	
64.5' " " "	0.07	145.26	11.94	145.19	
84' " " "			2.87		
93' " " "			4.34		
100' " " "	= .5 jog in curb.		5.24		
107' " " "			5.72		
121.6' " " "			8.31		
130' " " "			9.30		
150' " " "		132.81	12.38	132.88	
200' " " "			4.52		
250' " " "			9.23		
T.P.	4.55	145.30	12.06	140.76	

NL Elm St

Cement gutter on E side from NL Elm to 100' No. { 5' wide 8" deep dip in center } N.G.

	0.77	119.67	
SL Elm W. side			
50' So. of Elm W Cb			
100' " " " " "			Jog in line + grade
" " " " " "			
150' " " Cb " "		108.49	
Cement gutter on E Side Elm to 100' So.			
100' So. of Elm W Cb			
150' " " " "			
W side Date			

130 100.21

SL Date W Cb

" " E "

16' So. " "

50' " " "

74' " " "

84' " " "

100' " " "

90' " " W. Cb.

100' " " W "

6.50		
6.45	118.85	
	118.90	NW 2nd + Elm
3.67	116.00	OK = 116.0
6.48	113.19	OK = 113.1C
9.29	110.38	OK = 110.33
8.82	110.85	OK = 110.33 = .3 in 5ft
11.64	108.03	OK = 107.6
5' wide 1' deep N.G. Too high on east side		
3.29	105.20	OK = 104.97 = .3 in 5ft
3.80	104.69	OK = 104.67
6.59	101.90	OK = 101.87
9.50	98.99	OK = 99.0
9.53	98.96 = 91	
	98.91	
4.30	95.91	
1.22	98.99 ✓	4 acre curb = 5
1.87	98.34 ✓	
2.90	97.31	
3.49	96.72 ✓	
4.07	96.14	
4.52	95.69	
6.62	93.59	
7.23	92.98	

66

		100.21		
125' 30.0X	Date E. Cb	5.10	95.10	✓✓
127.4 " "	" " "	4.77	95.44	✓
150' " "	" " "	5.30	94.91	
173' " "	" " "	5.75	94.46	
185' " "	" " "	6.26	93.95	
195' " "	" " "	6.27	93.94	
200' " "	" " "	6.70	93.51	
200' " "	W. Cb	9.64	90.57	OK=90.67
150' " "	W "	8.28	91.93	OK=92.0
125' " "	W "	7.76	92.45	OK=92.67
W sidewalk W Cb all low from SL Date to 150'S.				
	N.59 77.46		74.87	
S.L. Beech	W Cb.	3.02	74.44	
" "	E "	0.55	76.91	OK=77.5
51' 3.0X "	E "	2.12	75.34	OK=75.64
51' " "	" "	1.86	75.60	OK=75.64
100' " "	E "	3.72	73.74	OK=73.83
151' " "	E "	5.64	71.82	OK=71.97
151' " "	E "	5.23	72.23	OK=71.97
201' " "	E "	6.98	70.48	OK=70.14
202.7 " "	E "	7.36	70.10	OK=70.07
226' " "	E "	8.07	69.39	OK=69.21
250' " "	E "	9.24	68.22	OK=68.39
N.L. Ash	" "	11.05	66.41	OK=66.50

		77.46		
N-L. Ash	W Cb		13.15	64.31 OK=64.2
50' N.0X "	W "		11.43	66.03 OK=66.17
85' " "	W "		10.30	67.16 OK=67.28
100' " "	W "		9.40	68.06 OK=67.73
120' " "	W "		8.50	68.96 OK=68.50
132' " "	W "		8.60	68.86 OK=68.90
144.5 " "	W "		7.96	69.50 OK=69.30
150' " "	W "		7.99	69.47 OK=69.5
OK from here to Beech				

12/30/19 Gregory Miller Shaw

CROSS-SECTION OF ARNOLD PLACE 60' wide 10' cbs + 1/4 End to End

on B.M.	0.24'	334.31		334.07	B.P. N.W. Neale & Maryland
T.P.	0.12	321.49	12.94	321.37	
T.P.	0.96	309.88	12.57	308.92	
T.P.	2.55	301.65	10.78	299.10	
T.P.	2.50	300.74	3.41	298.24	C.T. in wall SW Arnold & Mary

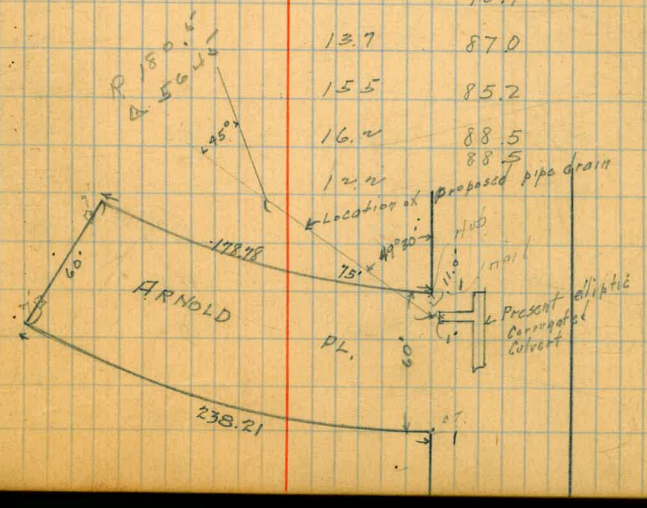
W. Cb. of Maryland.

S.		5.79	94.9	on Cement
N.		5.8 ±	94.9	" "

W. Line of Maryland.

S ⓐ		5.2	95.5	✓
+9		5.0	95.7	
cb		5.6	95.1	✓
1/4		5.6	95.1	
c		5.5	95.2	✓
1/4		5.6	95.1	
+3		5.9	94.8	
cb		8.4	92.3	
+1		5.9	94.8	
N		6.3	94.4	✓
	18' on No 23.98 - 30	W. of Maryland		
-13 ⓐ		10.8	89.9	
-8		13.1	87.6	
N		13.6	87.1	✓
+5		12.5	288.2	
cb		9.1	291.6	

+7		6.0	94.7
1/4		5.6	95.1
c		5.6	95.1 ✓
1/4		5.5	95.2
cb		4.5	96.2 ✓
+5		4.0	96.7
S		4.0	96.7 ✓
	24' on No 31.99 - 5	West of Mary	
S ②		3.4	97.3 ✓
+6		3.5	97.2
cb		4.2	96.5 ✓
1/4		5.4	95.3
c		5.5	95.2 ✓
1/4		5.5	95.2
+2		5.7	95.0
cb		9.2	91.5
+6		10.0	90.7
N		13.7	87.0
+2		15.5	85.2
+7		16.2	88.5
+15		12.2	88.5



300.7H

30' on N. 39.96 - S } W. of Mary

-20	③	13.6	87.1	
-12		18.1	82.6	
-7		19.1	81.6	
N		12.0	88.7	✓
cb		9.2	91.5	
+8		5.5	95.2	
1/4		5.5	95.2	
C		5.5	95.2	✓
1/4		5.3	95.4	
cb		3.7	97.0	✓
+3		3.1	97.6	
S		2.7	98.0	✓

45' on N. 59.94 - S } W of Mary

S	④	1.9	98.8	✓
cb		2.4	98.3	✓
+5		2.5	98.2	
+8		4.1	96.6	
1/4		4.7	96.0	
C		5.0	95.7	✓
1/4		5.0	95.7	
cb		8.4	92.3	
N		11.5	89.2	✓
+11		17.1	83.6	
+14		21.1	78.6	
+20		21.8	78.9	
+30		18.1	82.6	

70' on N 93.24 - S } W. of Mary

-50	⑤	23.6	77.1	
-35		26.9	73.8	
-25		27.8	72.9	
-19		19.5	81.2	
N		12.3	88.4	✓
cb		8.5	92.2	
1/4		4.9	95.8	
+3		3.6	97.1	
C		3.6	97.1	✓
1/4		3.5	97.2	
+5		3.2	97.5	
+7		2.1	98.6	
cb		2.2	98.5	✓ walk 5' E same color as or lower A
S		2.1	98.6	

85' on N 113.22 - S } W. of Mary

S	⑥	1.9	98.8	✓ on low A
cb		2.3	98.4	✓
1/4		3.2	97.5	
C		3.3	97.4	✓
1/4		4.1	96.6	
cb		7.9	92.8	
N		10.5	90.2	✓
+25		21.5	79.2	

		300.74			
		100' on N 133.24 ~ S	W ox Mar ✓		
-25	①		20.7	80.0	
-15			15.6	85.1	
N			10.9	89.8	✓
cb			7.0	93.7	
1/4			3.5	97.2	
C			3.1	97.6	✓
1/4			3.2	97.5	
cb			2.5	98.2	✓
S			1.9	98.8	on Dirt Walk to House
		130' on N 173.21 ~ S	W ox Mar ✓		
S	②		2.2	98.3	✓ on lawn
cb			2.7	98.0	✓
1/4			3.3	97.4	
C			3.1	97.6	✓
1/4			3.6	97.1	
~~1/4~~ +3			3.9	96.8	
cb			6.0	94.7	
N			9.6	91.1	✓
+10			12.3	88.4	
+25			18.8	81.9	
		160' on N 213.16 ~ S	W. ox Mar ✓		
-25	③		18.8	81.9	
N			9.2	91.5	✓
cb			6.5	94.2	
1/4			3.9	96.8	

C		3.1	97.6	✓
1/4		3.4	97.3	
cb		2.7	98.0	✓
S		2.6	98.1	✓
	178.78' on N. 238.21 ~ S	W ox Mar ✓ = End.		
S	⑩	2.7	298.0	
cb		2.5	298.2	✓
+8		3.6	297.1	
1/4		3.3	297.4	
C		3.4	297.3	
1/4		4.1	296.6	
cb		6.6	294.1	
N		9.7	291.0	✓
+12		13.8	286.9	

Levels on Proposed Pipe Location

0+00		8.4	
0+25		15.2	
0+50		21.3	
0+75		27.8	
1+00		34.2	

2/7/20 Gregory Miller B Moore.

Levels for Proposed Walk at End of Niagara St

	4.62	11.12	6.50	Newport BP Abbott
0+00 = End of Present Board Walk		4.45	6.67	Top of Walk
T.P.	5.15	6.88	9.39	1.73 3/4 Hub Niagara
0+00				
W		7.1	-.2	
C		6.3	.6	
E		5.5	1.4	
0+28.5 = center of Platform in front of Toilets 13.4 East of ℄ of Proposed Walk				
Top of cement.		1.2	5.7	
E		5.4	1.5	
C		6.1	.8	
W		6.8	0	
0+72.6 = SL of Niagara				
W		6.0	.9	
C		5.2	1.7	
E		4.5	2.4	
Present Steps are 8.5 E. of ℄ of Proposed Walk.				
Elev. of Bottom Step.		3.9	3.0	
.5 riser + .86 Tread.				
0+80.6 = Angle Point 28°50				
E		4.2	2.7	
C		5.0	1.9	
W		5.8	1.1	

6.88

1+15

W	7.2	-.3
C	6.3	.6
E	5.4	1.5
~~1+00~~	1+65	
E	6.8	.1
C	7.6	-.7
W	8.2	-1.3
~~1+80~~	2+20	
W	8.7	-1.8
C	8.0	-1.1
E	7.2	-.3

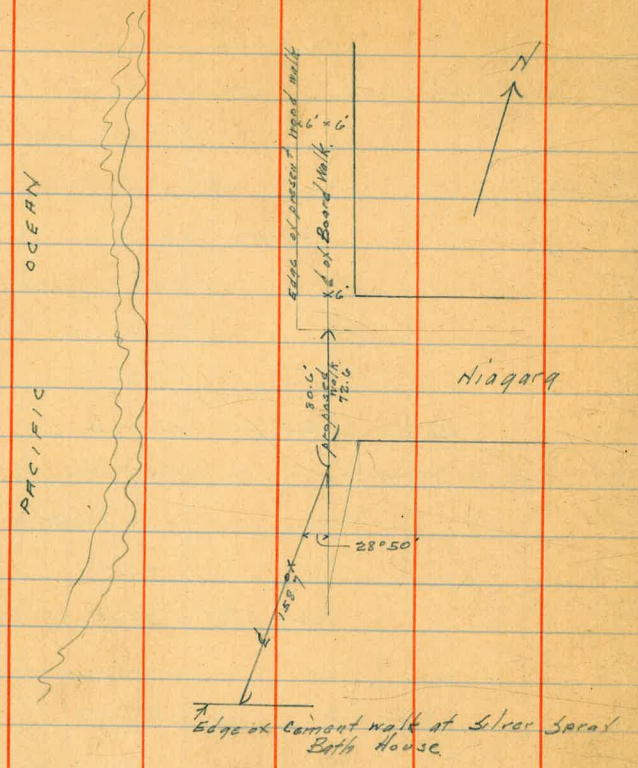
2+38.7 = Edge of Walk at Silver Spray Bath House

E	6.8	.1
C	7.7	-.8
W	8.6	-1.7

Top of Cement Walk at Silver Spray

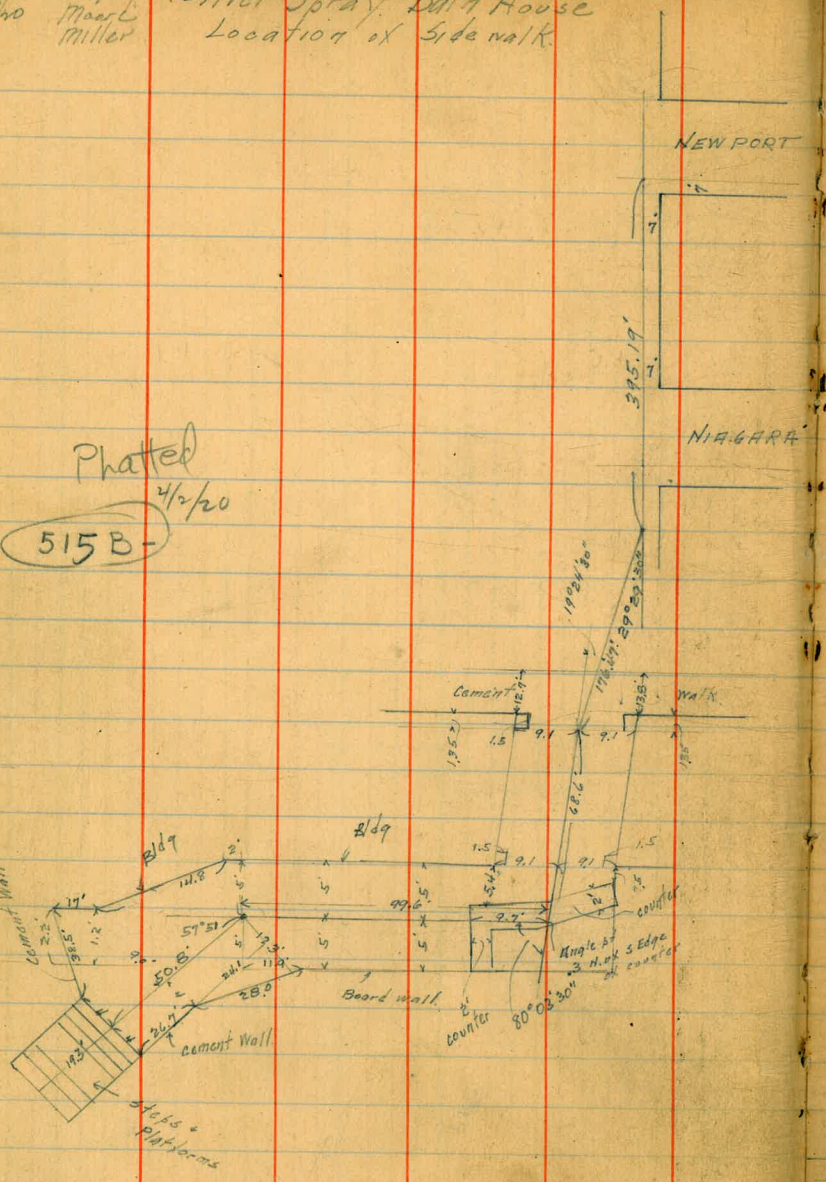
W	2.1	4.8
C	1.7	5.2
E	1.3	5.6

over

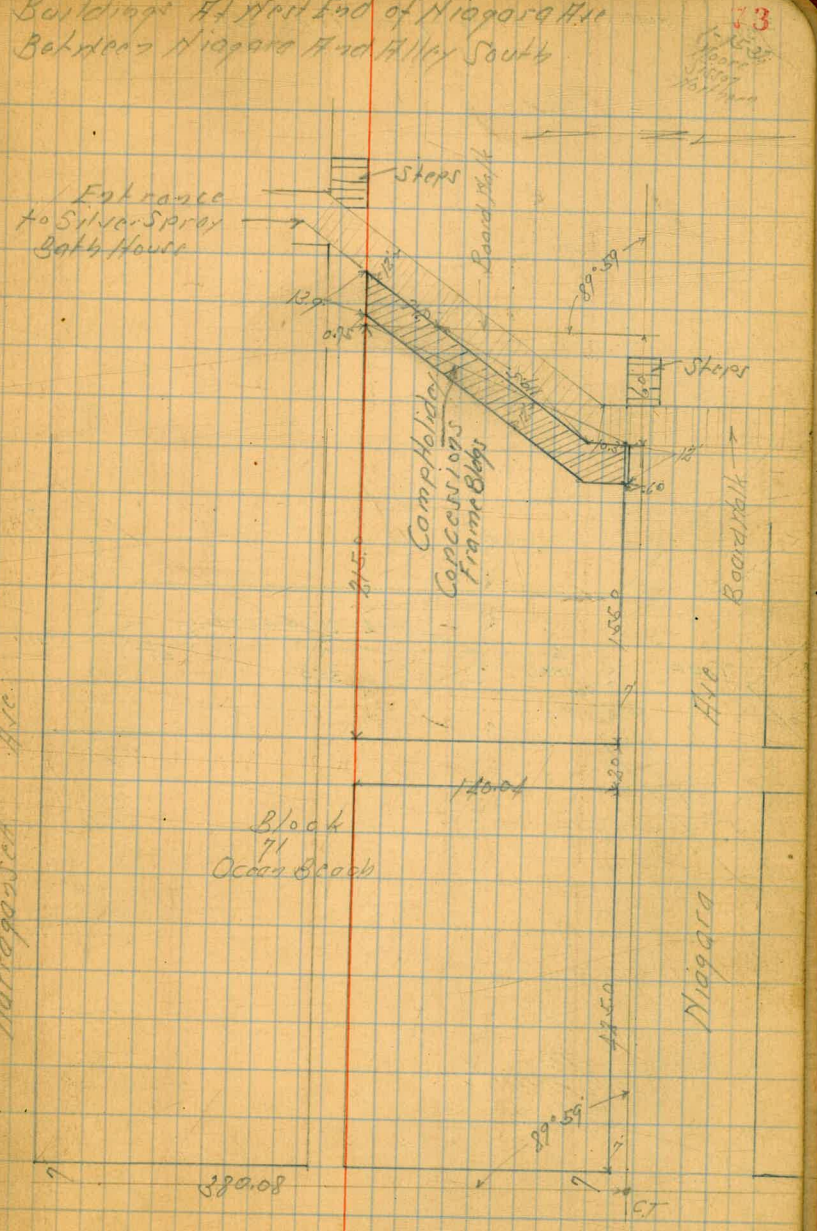

OCEAN
PACIFIC
N
Edge of Concrete Walk at Board Walk
6' x 6'
26'
Niagara
30.6'
(Accurate)
102.6'
72.6'
28°50'
138.9'
Edge of Cement Walk at Silver Spray
Bath House

3/30/20 Gregory Moore Miller

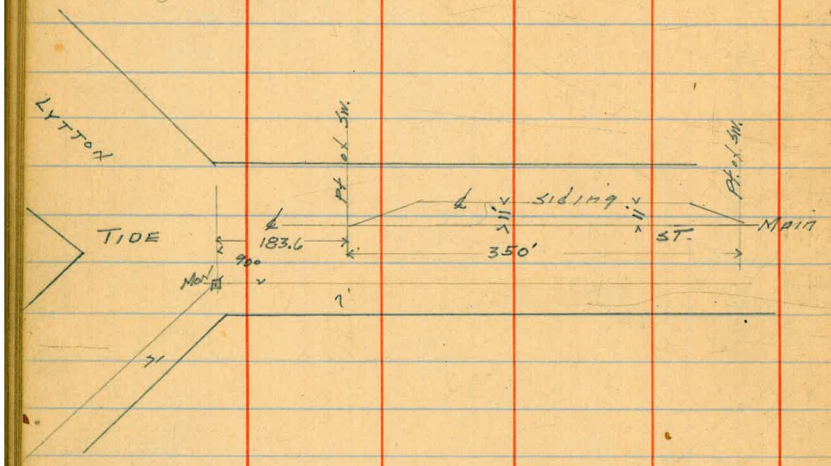
Silver Spray Bath House
Location of Sidewalk



Buildings At West End of Niagara Ave
Between Niagara And Alley South

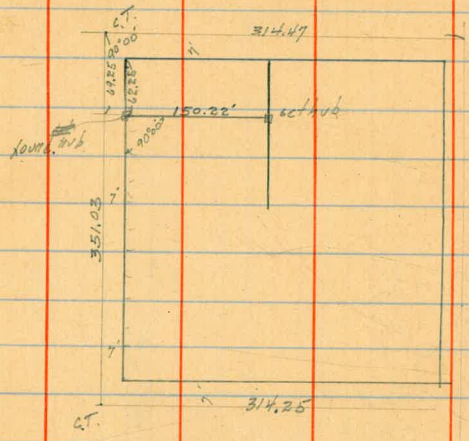


3/30/20 Gregory Siding on Tide St.



7/3/20 Gregori/ Miller Shaw

Survey of So. Line Lot 2 Blk 131 Univ. Hghts



9/8/22 Gregory Moore Ellis

Cross Section of Extension of Marcey Ave from 28th to 29th

	5.69	74.14		68.45	BP NW Logan = 3.9
		WL 29th St			
S			4.1	70.0	
+10	on M.H.		3.6		
+17.5			3.8		
+25			3.8	70.3	
+32.5			4.0		
+40			3.7		
+50			3.3	70.8	
TP	6.18	77.88'	2.44	71.70'	
		50' W.			
-50			7.2	70.7	
-40			7.3		
-32.5			7.8		
-25			7.6	70.3	
-17.5			7.3		
-10			7.2		
S			7.5	70.4	
		100' W			
S	= garage dirt		6.8	71.1	
+10			6.8		
+17.5			6.8		
+25			7.1	70.8	
+32.5			6.9		
+40			6.6		
+50			6.9	71.0	

77.88

150' W

-50	6.0	71.9
-40	5.7	
-32.5	6.4	
-25	6.6	71.3
-17.5	6.4	
-10	6.4	
S	6.2	71.7

200' W

S	7.0	70.9
+10	6.4	
+17.5	6.4	
+25	6.3	71.6
+32.5	6.3	
+40	6.1	
+50	6.2	71.7

250' W

-50	5.8	72.1
-40	6.1	
-32.5	6.5	
-25	6.7	71.2
-17.5	6.8	
-10	6.9	
S = garage dirt	6.9	71.0

7788

300' W

S	6.5	71.4
+10	6.5	
+17.5	6.6	
+25	6.6	71.3
+32.5	6.6	
+40	6.6	
+50	6.2	71.7

350' W

-50	5.6	72.3
-40	5.9	
-32.6'	6.0	
-25'	6.0	71.9
-17.5'	6.2	
-10	6.2	
S	6.5	71.4

380' W

S = garage dirt	6.0	71.9
+10	5.7	
+17.5'	5.8	
+25'	5.7	72.2
+32.5'	5.5'	
+40	5.4	
+50	4.5	73.4

400' W

-50	4.7	73.2
-40	5.3	
-32.6'	5.1	
-25'	5.2	72.7
-17.5'	5.1	
-10	5.2	
S	5.3	72.6

450' W

S	6.0	71.9
+10	6.2	
+17.5'	5.6	
+25'	6.0	71.9
+32.6'	5.9	
+40	5.9	
+50	5.8	72.1

475' W

-50	5.9	72.0
-40	5.8	
-32.6'	6.1	
-25'	6.1	71.8
-17.5'	6.0	
-10	6.5	
S	6.3	71.4

77.88

500' W

S	6.1	71.8
+10	6.3	
+17.5'	6.4	
+25'	6.1	71.8
+32.5'	5.5	
+40	5.3	
+50	5.0	72.9

525' W

-50	6.4	71.5
-40	6.6	
-32.5'	6.6	
-25'	6.6	71.3
-17.5'	6.6	
-10	6.9	
S	6.7	71.2

550' W

S	7.1	70.8
+10	7.0	
+17.5'	6.9	
+25'	6.9	71.0
+32.5'	7.0	
+40	6.8	
+50	6.7	71.2

575' W

+50	6.6	71.3
+40	6.6	
+32.5'	6.0	
+25'	6.4	71.5
+17.5'	6.4	
+10	7.2	
S	6.8	71.1

595' W

S	7.9	70.0
+10	8.0	
+17.5'	7.3	
+25'	6.6	71.3
+32.5'	6.7	
+40	6.5	
+50	6.6	71.3

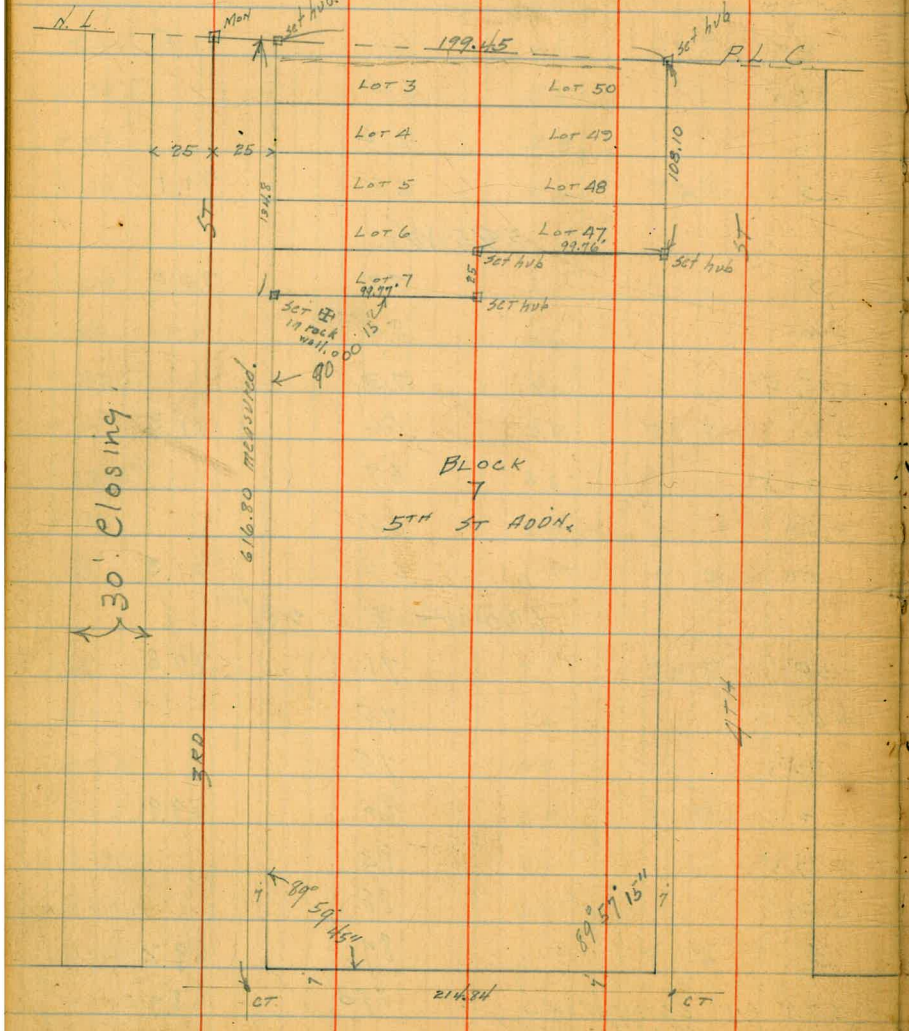
600' W = E.L. 78.4+

-50	7.1	70.8
-40	7.5	
-32.5'	7.8	
-25'	8.0	69.9
-17.5'	8.3	
-10	8.8	
S	8.7	69.2
chk on Cement curb SE side of Norway	8.93	68.95

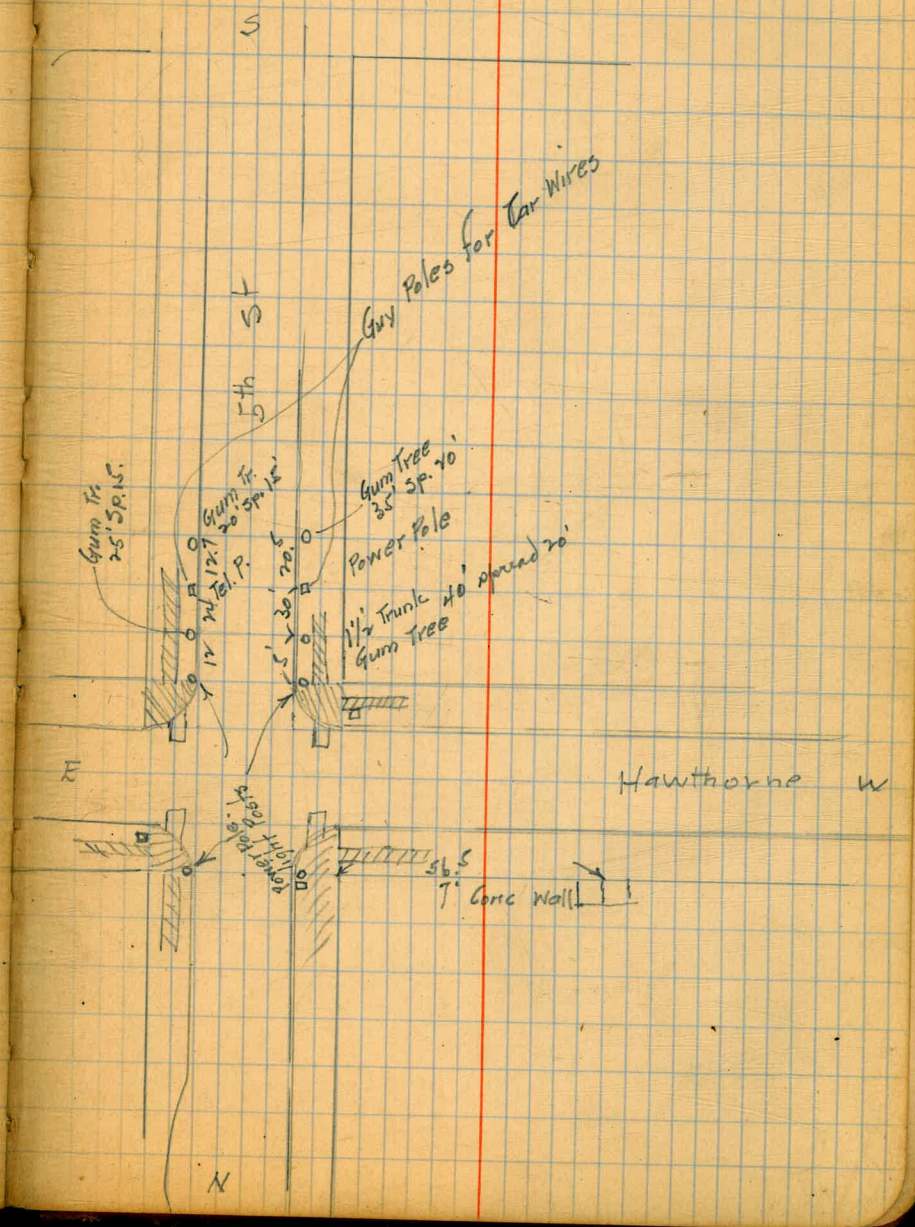
4/12/23 Gregory Moore

Survey Lots 2 to 7 and 47 to 51 inc. Block 7 Fifth St Addn.

See 832-22 for Bldgs.



79


S
5th St
Guy Poles for Car Wires
Gum Tr. 25' Sp. N.S.
Gum Tr. 20' Sp. 12'
12" Tel. P.
Gum Tree 35' Sp. 20'
Power Pole
1½' Trunk Gum Tree
E
Hawthorne
W
Concrete Foot Path
56.5
7' Conc. Wall
N

cl
1
J
C
+J
+5
1
1
cl
+9
N

10.7
15.5
21.1
w.6
24.1
25.0
25.0
w.J

under house

1.1.08
6.6.J
104.45

42.9
3 4
39.4
36
75.4
33 6
104.0

36.2
1.0
37.6

.2570
6
1.5420

1346

110
2950
1.2.5.

2664
6
1.5954

13.1
100

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59 6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.