

1067

DELAGA
1887

ENGINEER'S
FIELD BOOK

1887

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on $1\frac{1}{2}$ see inside of back cover.

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Book 1067

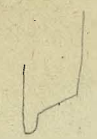
See F.B. 1061 and 1062

26900
250271

EUGENE DIETZGEN CO

DRAWING

Book 1067



See F.B. 1061 and 1062

1875
Dodge

37.50

250
 73.70
 52.80
 76.70.0
 6064.0
 1606.0
 5280.0
 68860
 6064.0
 8.22
 52.80
 61.02
 264
 38
 52.80
 5318

6064.1
 12128.2
 10598.
 1530.2

10560
 250
 10810

6064.
 5318
 746

282.57
 263.35
 545.92
 662.00
 114.08

38
 10560
 10598.

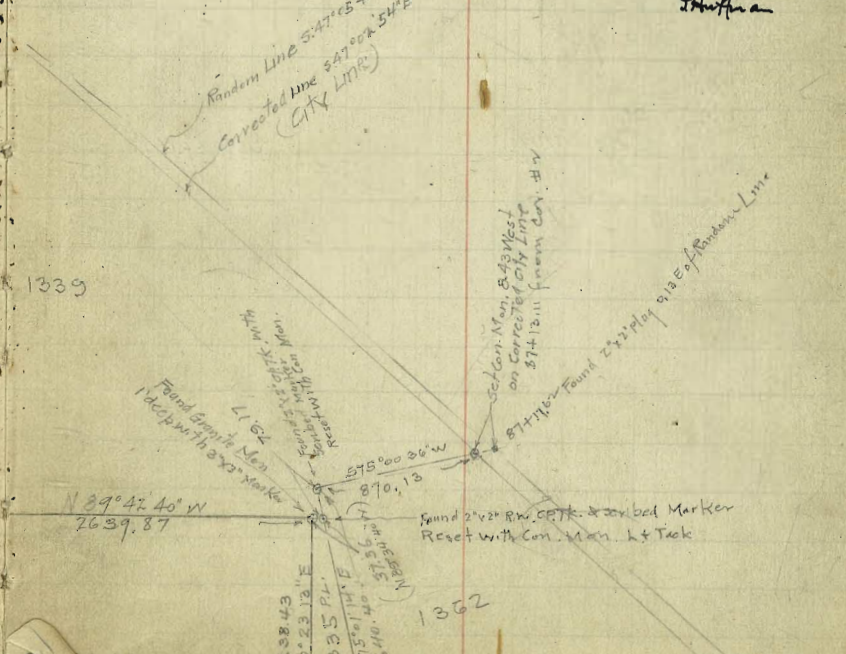
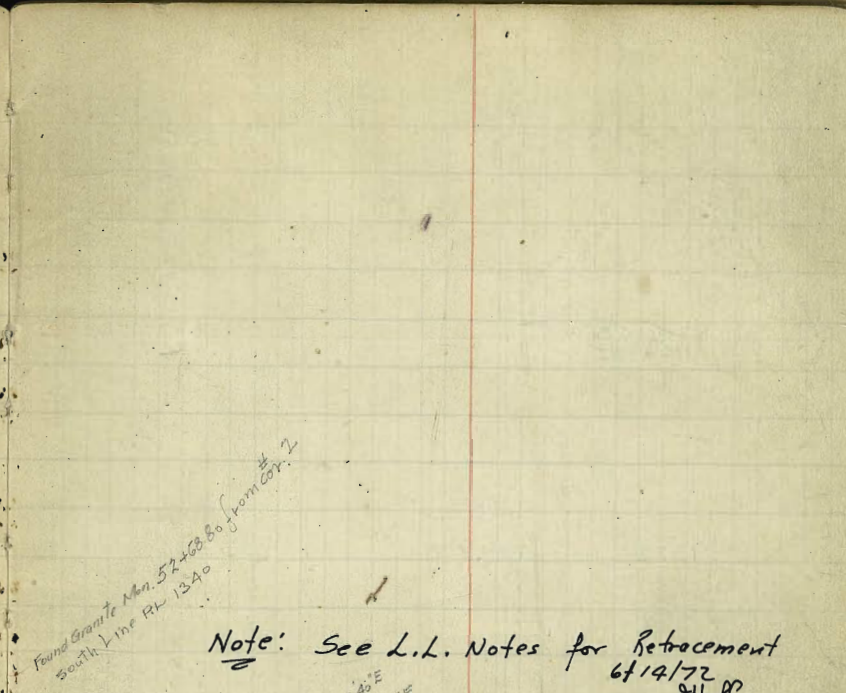
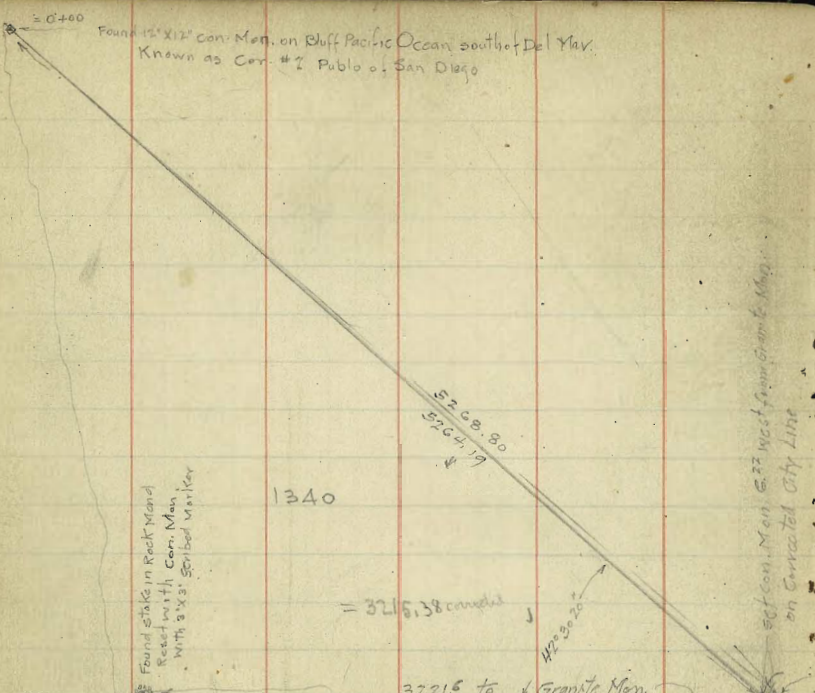
12128.
 10810
 1318

35221
 140
 3809740
 95231
 13332340
 129.83
 (627)

27720
 300

26335200

28.37



Pacific Ocean

Sct. Con. Mon. L1 Tack on Ocean Bluff

Found Stake in Rock Mand Rest with Con. Mon. with 2" x 3" Scribed Marker

Sct. Con. Mon. 8 1/2" West from Granite Mon. on Corrected City Line

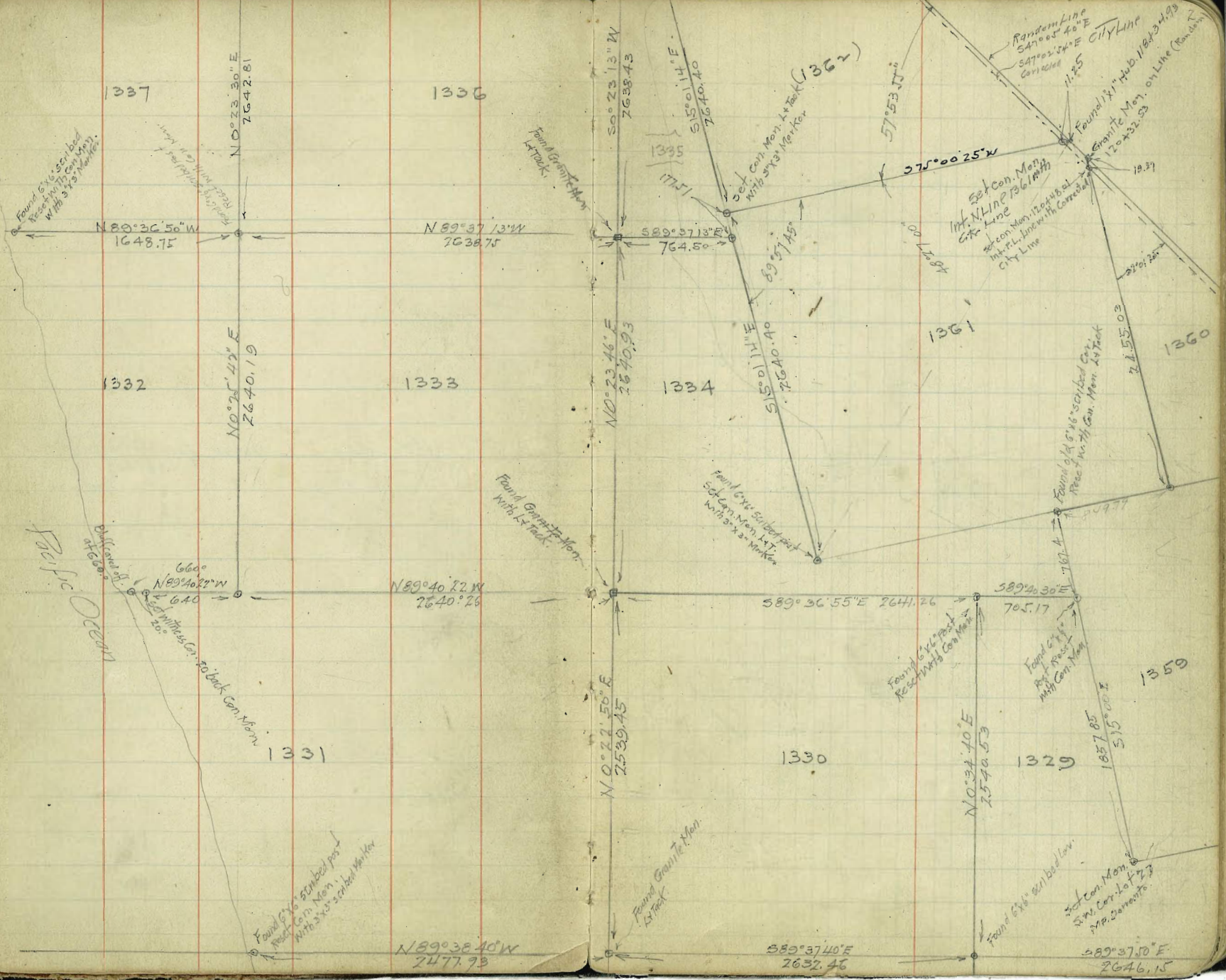
Found Granite Mon. 5 1/2" x 3 1/2" from Cor. #2 south 1/2 mile RW 1340

Note: See L.L. Notes for Retrocement 6/14/72 Huffman

Random Line 547°15'45"E Corrected Line 547°02'54"E (City Line)

Sct. Con. Mon. 8 1/2" West on Corrected City Line 571.3111 from Con. #2

Found 2" x 2" RW. City & Scribed Marker Rest with Con. Mon. & Tack



1337

1336

N 88° 36' 50" W
1648.75

N 89° 37' 13" W
7638.75

S 0° 23' 13" W
7638.43

1334

N 0° 23' 46" E
2640.93

S 89° 36' 55" E
2641.26

1330

N 0° 22' 56" E
2539.45

N 0° 34' 10" E
2540.53

1329

1332

N 0° 29' 42" E
2640.19

1333

1361

1360

N 0° 23' 30" E
7642.81

S 15° 01' 11" E
7640.40

S 89° 37' 13" E
764.50

S 15° 01' 11" E
7640.40

S 75° 00' 25" W
57153.77

S 69° 57' 14" E
6997.48

S 27° 01' 28" E
2455.03

S 89° 40' 30" E
705.17

S 89° 37' 50" E
2646.15

Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" school marker

Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" school marker

Found Granite Mon.
with 1 x 1 track

Set Con. Mon. with 1 x 1 track
with 3 x 3" marker (1362)

Set Con. Mon.
with 1 x 1 track
with 3 x 3" marker
City Line

Found 11' x 11' bed
Granite Mon. on Line
with 1 x 1 track
with 3 x 3" marker
City Line

Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" marker

Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" marker

Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" marker

Found Granite Mon.
with 1 x 1 track

Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" marker

Set Con. Mon.
with 1 x 1 track
with 3 x 3" marker
City Line

Pacific Ocean

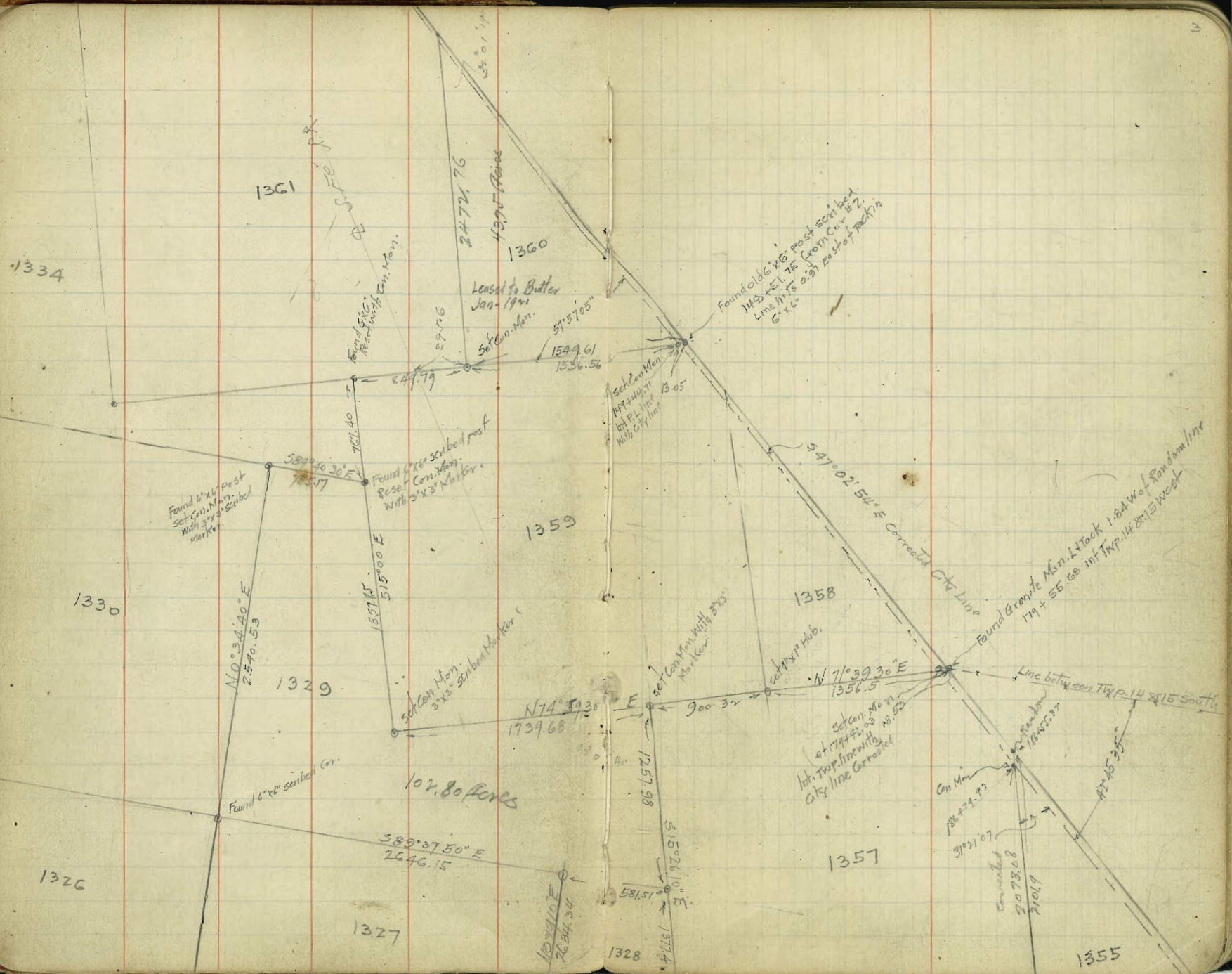
Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" marker

Found 6 1/2" x 5 1/2" bed
Resect with 15' Con. Mon.
with 3 x 3" school marker

N 89° 38' 40" W
2477.73

S 89° 37' 40" E
2632.46

S 89° 37' 50" E
2646.15



N89°38'40"W
2477.93

1325

N89°40'35"W
2601.40

1324

N89°38'55"W
2304.6

S89°37'40"E
2632.46

1326

S89°39'10"E
2639.28

1323

S89°40'E
2641.53

S89°37'50"E
2646.15

1327

S89°43'20"E
2640.68

1322

S89°41'E
2640.39

N0°21'20"E
2629.0

N0°19'20"E
2640.0

1329

589° 07' 50" E
581.51

1571.40
S15° 16' 10" E

1357

S-Santa Fe

2073.08

58° 24' 53"
2114.14

90° 16'
396.40
870.00

S47° 04' 54" E

N74° 33' 50" E

66° 19' 10" 1524.50

710.75
398.46
113° 40' 50"

Area 70.10 Ac.

1328

1356

1410.22
S15° 18' 50" E

S89° 41' 50" E
1734.37

Found Granite Mon. Lt. A Near Sorrento
226 + 2983

1355

1327
N0° 19' 10" E 2634.34

1327
N0° 19' 25" E 2643.07

1321

N74° 41' 10" E
612.71

S00° 16' 10" W
1684.21

1320

Found old 1/4 Post

2028.08
S74° 53' 45" W
1322.20

S77° 05' 42" E
Canted City
Line

1353

1352

757.7
S79° 16' 55" W 617.45

1351

N74° 15' E 127.56

S74° 47' 35" W
1713.33

S89° 40' 20" E
2640.54

S89° 40' 05" E
1589.24

S55° 55' 15" E
958.71
Found old 1/4 Post

S74° 47' 35" W
1523

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

Found old 1/4 Post

1323

589°40'E
2641.53

589°41'E
2640.39

589°40'20"E
2640.54

1314

NO 21°05'E
2639.40

1315

NO 19°40'E
2639.62

1316

NO 20°55'E
2639.01

1317

N 89°20'30"W
2638.91

90°00'

N 89°40'35"W
2640.98

90°00'30"

N 89°39'50"W
2640.00

90°00'41"

1311

NO 17°53'E
2636.99

1310

NO 16°52'W
2637.81

Area 15981 aere

1309

NO 18°40'W
2636.31

1308

589°38'10"E
2640.15

589°39'E
2640.07

589°38'17"E
2639.38

1299

1300

1301

1302

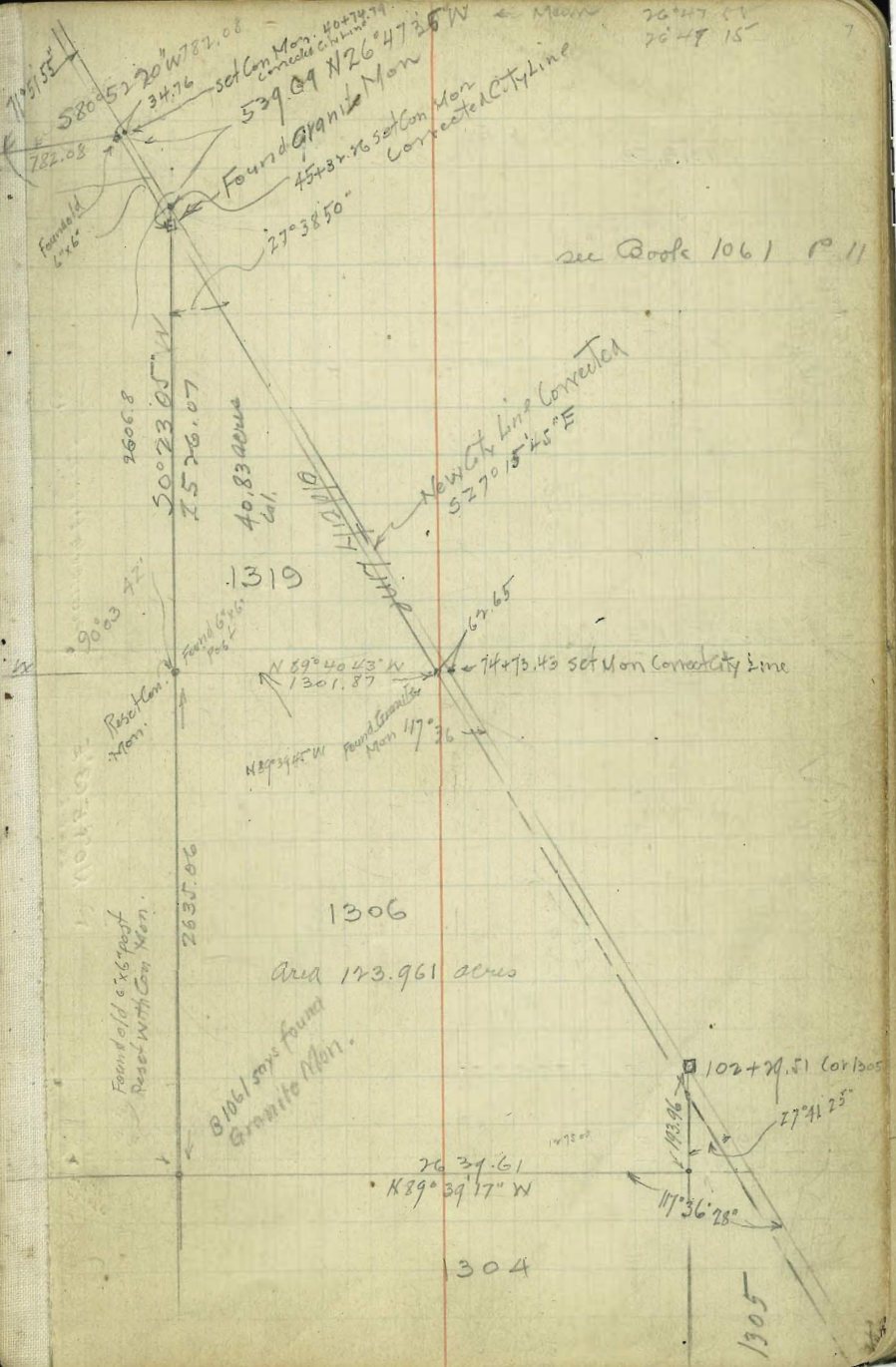
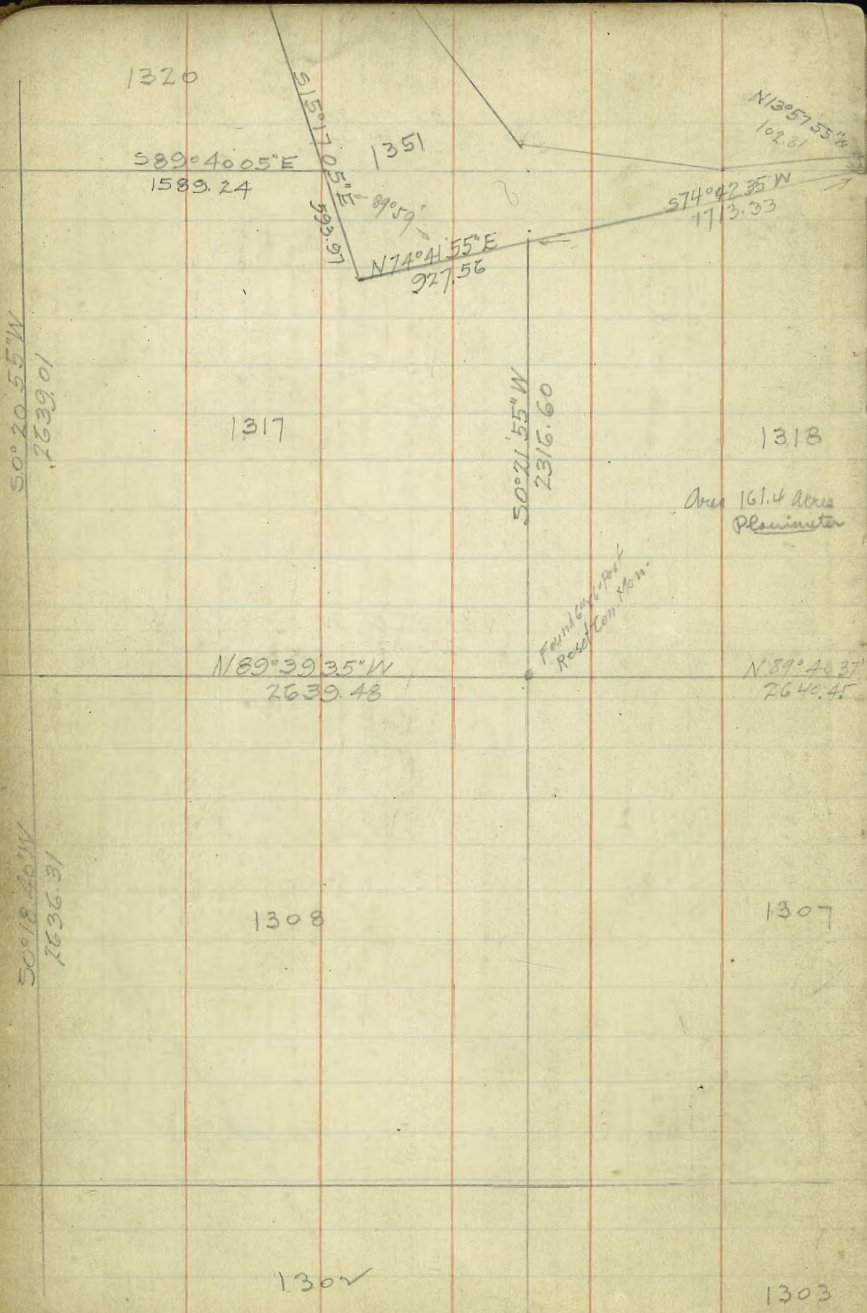
1313

NO 19°40'E 2638.90

1312

NO 18°30'W 2636.43

Area 15981 aere



1311

589°38'10"E
1319.53 1320.62

1310

26 40.07
589°39'E
1319.86 1320.21

1309

589°38'17"E
2639.38

50°20'55"W
2639.01
50°21'57"W
2627.47

1299

N0°24'23"E
2628.26

1300

1301

25°28'30"
75°07'30"

71 29 50
72 29 30
73 29 30

7-28-52 58 Marker
Ft. Cong. Mon
25 Station on P.10

589°35'38"E
1320.65



Fd. 2x2
SET IN IRON PIN
1-10-38
Moore

Found old 6x6 Post
N0°15'08"E
2640.84

589°34'52"E
1324.97
1320.58

589°35'43"E
2640.60

Found old 6x6 Post

50°18'40"W
2636.31
50°16'36"W
2639.84

1296

N0°19'25"E
2641.8

1295

1294

Area 136.48 Area
perimeter
8°54'30"

589°34'53"E
1317.75

N89°35'10"W
1318.71

N89°36'15"W
1319.56

Found old scribed
6'x6'

Found old 6x6 scribed
Res. with 100' Con. Mon.

2658.86 N75°33'30"E

3499.0 N 42°26'30"N
301.98 Found old scribed
6'x6'

N14°16'30"W

Found old scribed 6'x6'

1279

N75°47'08"E 433.73

1292

Found old scribed
6'x6'

1280
S14°28'14"E
1383.08

1290

1291

Found old 1x2
Res. with
100' Con. Mon.

1289

Found old
6'x6' Post
1271

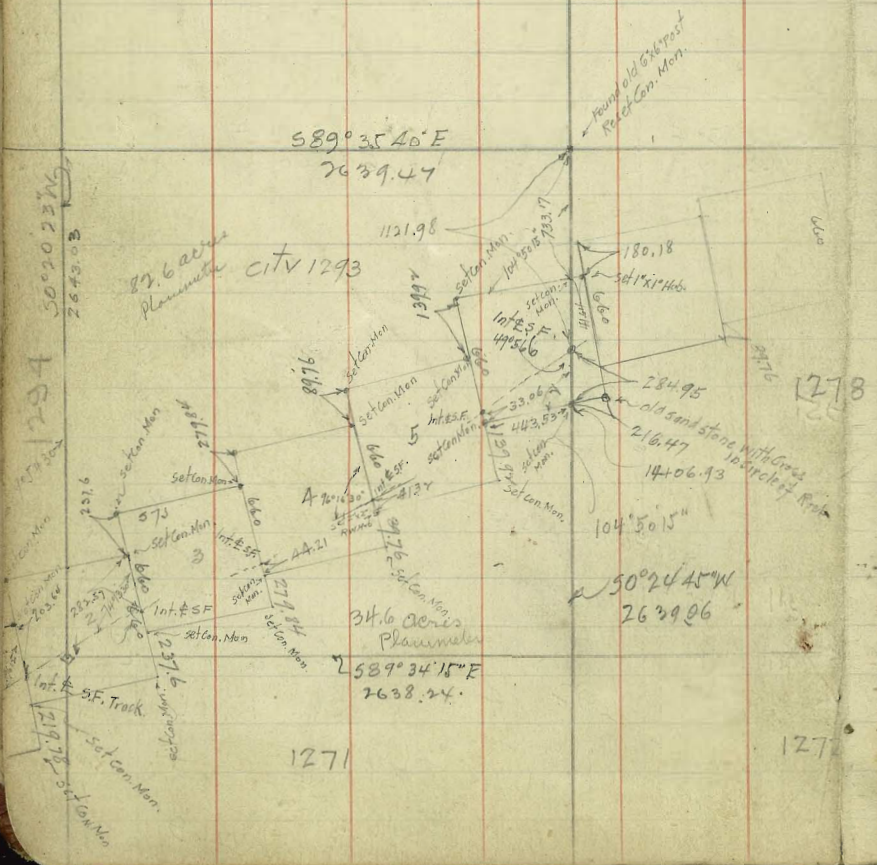
1308

1302

589°35'40"E
2639.47

87.6 acres
Plummer
City 1293

1301
5020236
2643.03
1274
1272



1271

589°34'15"E
2638.24

34.6 acres
Plummer
City 1276

50°24'45"W
2639.06

1273

284.95
old sand stone with Grass
in Circle of Post
216.47
14406.73
104°50'15"

1272

1307

1303

29.76
38.16
56.60
123.77
237.60
281.77
120.17
56.60
137.23

2638.31

1306

Area 159.85 acres

2639.61

2173.12
34.70
2208.02

2638.96

1277

2638.79 ch.

1273



2633.8

1305

93.9 acres
City 1277

89°54'17"
1481.63

Mon. City 1277

see B1001 p 74
see page 77

1276

1274

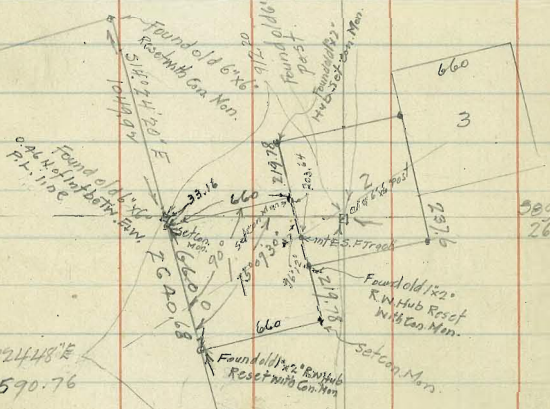
N° 09 15"

1293

1294

Found old 6'x6"
Resect with Con. Mon.

50° 20' 13" N
2649.93



589° 34' 16" E
2638.24

Found old 182°
R.N. Hub Resect
with Con. Mon.

1271

511° 24' 48" E
1590.76

To old 6'x6"
26° 36' 45" 57° 38' 19" W

CITY
1269

Found old 182°
Resect with Con. Mon.

1270

698.87
33.16

1049.92
1590.76
2640.68

934.76
897.60
33.16

10

1278

Found old 6'x6"
Resect with Con. Mon.

589° 33' 07" E
2641.42

Found old 6'x6"
Resect

589° 33' 14" E
2638.79

1272

1273

PLANIMETER

Found old 6'x6"
Resect with Con. Mon.

Found old 6'x6"
Resect with Con. Mon.

1249

1248

530
2640
4970

1277

Found old 6x6 post.

589°33'14" E
2638.79

Found old 6x6 post.

1276

N 0° 19' 56" E 201.08

589°33'14" E
2640.56

1273

1272

1274

2369.95

1275

1061-70
790
see book 1971

641.21

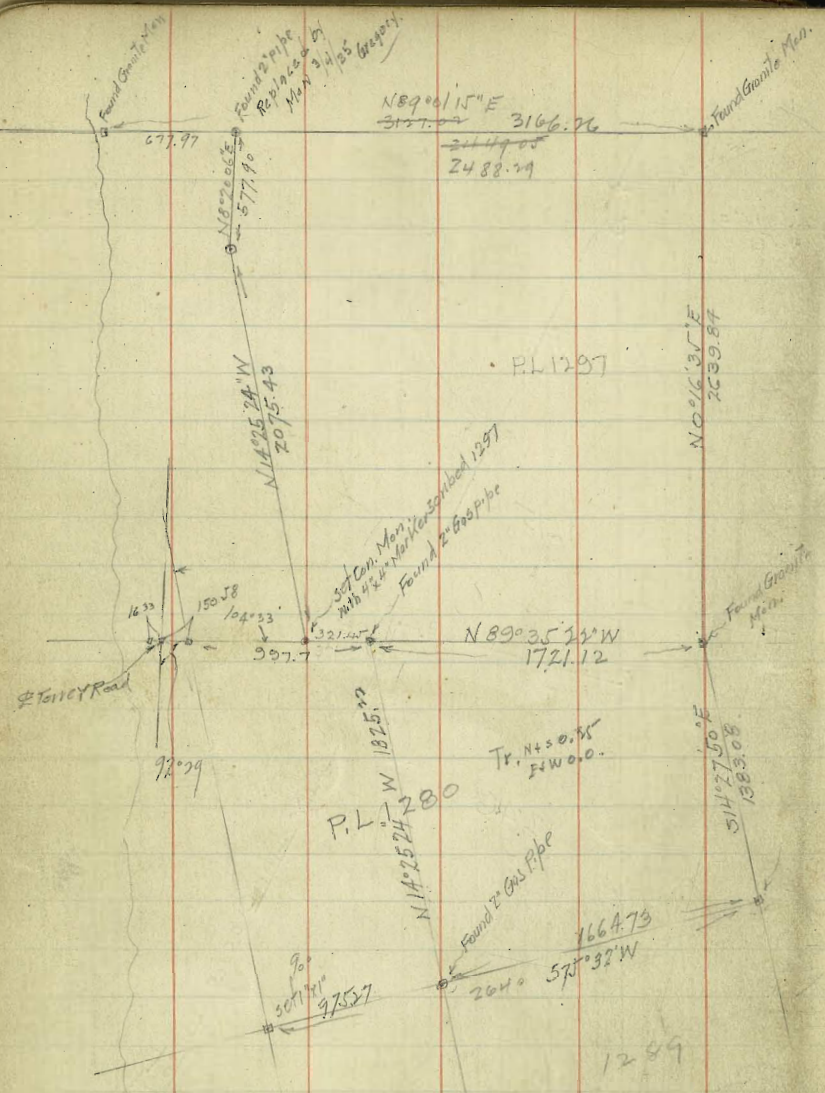
1208.90

1246

1247

1248

CITY LIBR. CREED JIMMIE TOWN SHAW



ser FA 250 / 60061

PL 1296
W 1/2 City

PL 1280

1289

second city, map 4509

12/27/23 Gregory CROSS SECTION OF 60' wide
LANDS ST 10' cbs
Louisiana to Alabama

15

	287.12	285.88	Louisiana	cb	2.0	285.1
1.24	304.11	302.87	SE Lands	+05	2.2	286.9
	W L LOUISIANA			+07	3.5	283.6
S	1.1	286.0		1/4	3.7	283.4
+03	1.1	286.0		a	3.7	283.4
+04	1.8	285.3		1/4	4.3	282.8
cb	1.8	285.3		cb	4.8	282.3
1/4	2.5	284.6		+07	4.6	282.3
c	2.4	284.7		N	3.7	283.4
1/4	2.4	284.7				
cb	2.5	284.6		N	3.2	283.9
Convent of	2.13	285.0		+03	4.8	282.3
N	2.0	285.1		cb	5.2	281.9
	0+30			1/4	4.5	282.6
N	2.9	284.2		C	4.1	283.0
+02	3.9	283.2		1/4	4.3	282.8
cb	3.3	283.8		+02	4.3	282.8
1/4	3.3	283.8		+06	2.6	284.5
c	3.7	283.4		cb	2.6	284.5
1/4	3.6	283.5		S	2.3	284.8
+04	3.4	283.7				
+05	2.3	284.8		S	2.8	284.3
cb	2.2	284.9		cb	3.1	284.0
S	2.0	285.1		+04	3.1	284.0
	50' W			+07	4.8	282.3
S	1.9	285.2		1/4	4.8	282.3

75' W

100' W

c	4.9	282.2
1/4	5.4	281.7
cb	5.9	281.2
+07	5.5	281.6
N	3.8	283.3
	145' W	
N	5.1	281.3
+03	6.4	280.7
cb	6.6	280.5
1/4	6.5	280.6
c	6.2	280.9
1/4	6.0	280.0
+03	6.0	280.0
+06	4.6	282.5
cb	4.5	282.6
S	4.2	282.9
	135' W	
S	4.7	282.4
cb	4.9	282.2
1/4	5.3	281.8
c	5.6	281.5
1/4	6.2	280.9
cb	6.8	280.3
N	6.0	281.1
	170' W	
N	6.3	280.8

cb	6.2	280.9
1/4	6.2	280.9
c	6.1	281.0
1/4	6.3	281.8
cb	5.8	281.3
S	5.5	281.6
	182' W	
S	6.1	281.0
cb	6.8	280.3
1/4	7.3	279.8
c	6.9	280.2
1/4	6.8	280.3
cb	7.1	280.0
N	6.8	280.3
	185' W	
N	7.1	280.0
cb	7.1	280.0
1/4	6.8	280.3
+01	11.4	275.7
c	12.0	275.1
+05	12.1	275.0
1/4	10.8	276.3
cb	8.2	278.9
+05	6.1	281.0
S	6.2	280.9

	195' W		
S	6.8	280.3	
+05	12.8	274.3	
cb	12.8	274.3	
1/4	12.8	274.3	
C	12.5	274.6	
1/2	12.6	274.5	
+07	11.8	275.3	
+09	7.6	279.5	
cb	7.7	279.4	
N	7.7	279.4	
	9.04	280.55	271.51
		274.92	275.28
	225' W		
N	4.0	276.6	
cb	4.4	276.2	
+3	4.6	276.0	
+4	7.5	273.1	
1/2	7.6	273.0	
C	7.1	273.5	
1/4	7.2	273.4	
cb	7.2	273.4	
+9	6.5	274.1	
S	2.0	278.6	
	255' W		
S	3.6	277.0	
+1	4.1	276.5	
+2	6.7	273.9	

SE. Miss
& Landis

cb	7.7	272.9
1/4	8.2	272.4
C	8.4	272.2
1/2	8.3	272.3
+7	8.3	272.3
+8	6.4	274.2
cb	6.6	274.0
N	6.7	273.9

1/4	8.9	271.7
cb	8.7	271.9
1/2	9.0	271.6
C	8.9	271.7
1/4	8.5	272.1
cb	8.4	272.2
+9	8.4	272.2
S	6.5	274.1

W.L. Miss

S	9.7	270.9
cb	9.6	271.0
(agreement)	10.10	270.5
1/4	10.0	270.6
C	10.0	270.6
1/2	10.2	270.4
cb	10.0	270.6
N	10.3	270.3

30' W

N	11.3	269.3
cb	10.8	269.8
1/4	11.0	269.6
C	10.9	269.7
1/2	10.9	269.7
cb	10.5	270.1
S	9.8	270.8

55' W

S	11.3	269.3
cb	12.0	268.6
1/4	12.1	268.5
C	12.6	268.0
1/2	12.5	267.8
cb	12.5	268.1
N	12.9	267.7
T.P	13.02	267.5

268.06

282.46

70' W

-15	10.0	258.1
N	7.9	260.2
cb	6.0	262.1
1/4	4.1	264.0
C	2.5	265.6
1/2	2.1	266.0
cb	1.7	266.4
+6	1.4	266.7
S	0.6	267.5

S		100' W	2.6	265.5
+1/4		272.46	3.5	264.6
cb			3.7	264.4
1/4			4.1	264.0
C			5.5	262.3
1/4			7.7	260.4
cb			9.3	258.8
N			10.5	257.6
+10			11.5	256.6
		125' W		
-10			14.0	254.1
N			13.3	254.8
cb			12.6	255.5
1/4			11.6	256.5
C			10.0	258.1
1/4			8.1	260.0
cb			6.5	261.3
S			5.4	262.7
		150' W		
S			7.6	260.5
cb			9.0	259.1
1/4			11.5	256.6
C			12.5	255.3
TP	1.69	256.72	13.03	255.03
1/4		271.12		
1/4			3.0	253.7
cb			3.8	252.9
N			4.2	252.5
+ 0.50 = Porch floor of House			3.25	253.47
		175' W		
- 8.2 = under porch of House			8.2	248.5
- 2.5 = bottom of Steps			7.2	249.5
N			6.8	249.9
cb			6.3	250.4
1/4			5.3	251.4
C			3.8	252.9
1/4			2.8	253.9

		LAHOIS		16
cb			1.1	255.6
S			+ 0.5	257.2
		200' W		
S			0.7	256.0
+5			2.7	254.0
cb			3.8	252.9
1/4			5.2	251.5
C			6.4	250.3
1/4			7.4	249.3
cb			8.3	248.4
N			9.2	247.5
+6 = end of Driveway to Garage			9.1	247.3
+7			8.8	247.9
+10			9.6	247.1
		225' W		
-5 = against house			9.5	247.2
N			9.5	247.2
cb			9.8	246.9
1/4			9.8	246.9
C			9.2	247.5
1/4			8.2	248.5
+5			7.5	248.9
cb			6.4	250.3
+5			5.8	250.8
S			2.0	254.7
		239.5' W		
S			2.8	253.9
+6			7.2	249.5
cb			8.2	248.5
+6			9.2	247.5
1/4			9.2	247.2
C			9.6	246.5
			10.2	246.5
S on cement walk		249.5' W = Edge of walk to house	4.8	251.9
+3			5.2	251.5
+6			7.2	249.5
cb			8.2	248.5
+6			9.4	247.3
1/4			9.6	247.1
C			10.3	246.3
1/4			10.2	246.7
cb			10.2	246.7
+5 = against house			9.7	247.0
		271.5' W = EL. F/A	10.2	246.5
N			10.4	246.3
cb			10.6	246.1
1/4			11.2	245.3
C			11.2	245.3
1/4			11.2	245.3
cb			10.8	245.7
			10.6	246.1

2640
1331
3540.00
3643.85
2661.17

5280.00
50 69.12
216.78

5280.00
11.32
68.64

Milami
Dunkle
Evans Aug 20-1919
Folke

Survey PL 1780

39460
152.0
41412.0
4 62.0
45274.0
4 59.12
7063.72
78.46
51432.58
72.38
52113.36
36.36
5247.62
45.00
488.36
533.36
33.00
74.00
640.36
489.49
96.00
1235.85
459.10
62.00
1726.95
487.45
93.00
2327.40
263.62
3.10
2624.12

2640.00
49.72
3427.72
486.13
43.00
35.00
3693.85

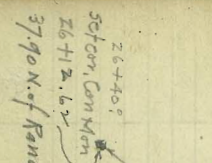
5708 30°

1155 99946
440
8941760
397776
48979560
712
99211
418
297790
396204
42613390
124 77660
710
199532
697760
199532
26790220
266.15
3.75
888330 518 99512
399242 464
48910330 378288
577432
399242
551 448 248201403
440 3.24
895320 71721
399242 418
4878520 783290
399242
440
99946
264.2 1137 97452
249526 687921
398968 69524
598454 705604
199484
263618106 441 9970
73
74910
69790
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440
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2137 99716
418
1990640
399514
459470

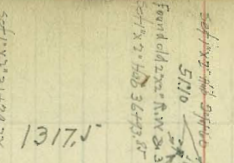
161
185
377
111
185

768
384

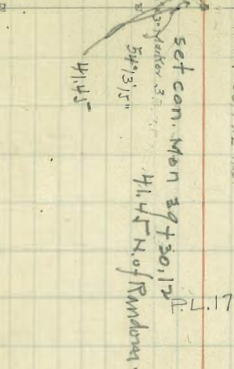
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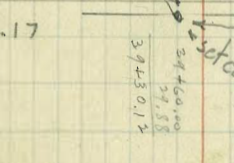
3790 N. of Random Line of 26 17.5 m



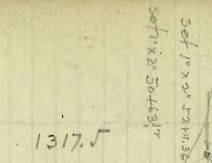
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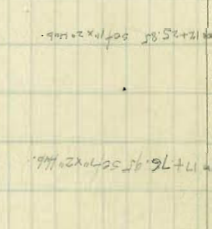
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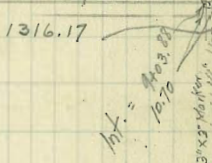
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1070
7403.88
N 13 E



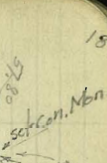
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1316.17



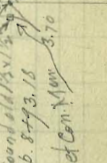
8403.8
1070
7403.88
N 13 E



5780



1316.17



8403.8
1070
7403.88
N 13 E

set con. Men
2634.1
5247.62
N 13 E
5708 30°

set con. Men
2634.1
5247.62
N 13 E

set con. Men
2634.1
5247.62
N 13 E

10/15/21 Gregor Levels on Track, 12th St

Moore
Miller
Shaw

from A North

Measurements are taken on Δ of Each
Track, Plot profiles according to Δ

	12.80	118.27	105.47	NW A + 12 th St BP
		N.L.A. St		
W Track		12.27		
E ✓		11.87		
		100' N		
E Track		7.38		
W ✓		7.91		
		150' N = where car stops now		
W Track		5.48		
E ✓		5.10		
		200' N = Approx PC on W Track		
E Track		2.56		
W ✓		2.84		
T.P.	13.01	130.93	0.35	117.92
		250' N = Approx PC on E Track		
		300' ✓		
W Track		10.14		
E Track		10.13		
		400' N		
E Track		5.34		
W ✓		5.22		
		500' N		
W Track		0.30		
E ✓		0.22		
T.P.	12.68	143.59	0.02	130.91

5' wide plank xing 600' N = Approach to Bldgs

E Track 7.78

W ✓ 7.80

700' N

W Track 2.90

E ✓ 2.71

750' N

E Track 0.20

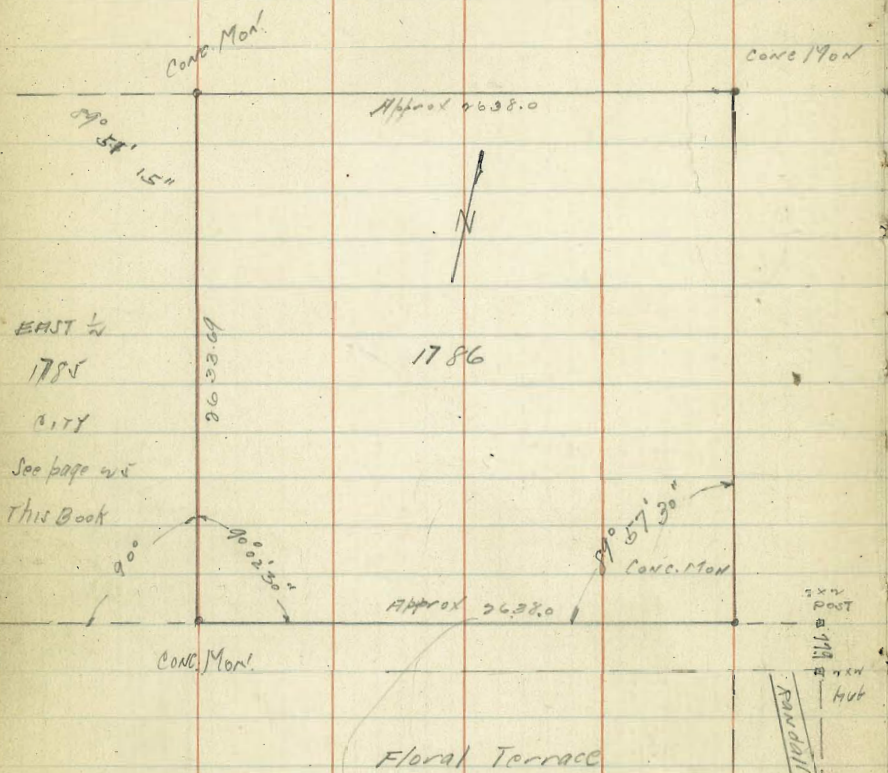
W ✓ 0.42







PLOT 1786



See Pac Beach Tie pt BK.

1541.10
1098.30
7640.80

290.61
99.25
390.51
499.27
889.78
114.92
1040.47
499.56
1504.26
448.85
1998.51
85.38
2083.57
496.95
3580.54
51.43
2631.27

120.15
1418.95
1541.10
66
9246
101704

1098.4 73000 (66)
1934
70660

1057 296
.95179
296
589874
883611
198358
290.60924
49907 232 100
300 500
90874 49727
207 115
99937
115 7
44660
99929
99929
11492180

2074 500
99912 49926
855 500
9871
49395
11025 87
98135
87 26
886945
798080
85.3 2745
60 20 500
7929 44651
801 5
98804
52
99794
44445
514464

Solar on South line P.L. 1785
Set up. S.E. Cox E. 1/2 P.L. 1785 Latitude 32°48'30"
Time Horiz Ang Vert Ang
2-55-30 11°10' 34°40'
2-58 10°29' 41' 34°01'
3-01 10°00' 29' 33°3'
3-07 8°46' 30' 32°18'

Left to Sun.

493.88
279.32
773.20
216.48
970.19
395.87

1386.05
829.40
499.10
828.50
64.68
893.18
90.00
9483.18
439.78
441.96
1.63
1443.59
16402.20
421.50
11080.80

16051.67
186.62
1843.29
184.93
2003.22
43.28
2066.50
496.78
44.00
2607.28
316.87
29220.15
179.56
2999.71
499.81
3499.52

186.625735
133 185
99963
165
499815
799704
99963
1849315
1148 4438
97515
44.38
780120
293545
390060
390060
432771570
60 30 500
913570496785

1312.40
1321.77
2634.67
828.50
64.68
893.18

1424.96
37.17
1459.13
128.62
96.26
294.88
57.17
332.05
244.86
486.22
781.10
221.25
1002.85
41.52
1602.37
497.93
3971.80
1602.30
49.37
16051.67
9029 50.04
9562
50.04
390649
49331000
493704608
49933
198.668804
0.57 186.65
99987
186.65
499935
159922
599922
799846
79987
186.625735
13024 500
97344 48622
22029 240
92344 3
367596
186798
2217596
395410
0.581 500
99916 49993
300 422.07
422
199726
109726
399452
47142186
421.47
2036 373.5
49112
13115
499570
247346
693793
297242
37019790

99637
200.6
597822
2989110
298911
328397922
300 500
.79821 49910
3040
9999
43968
798860
598740
998155
299385
3971.80
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2066.1988
999336
1988
799464
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999377
49933
198.668804
3033 96.45
99808
96.45
497000
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898272
96.2648160
13024 500
97344 48622
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92344 3
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99916 49993
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109726
399452
47142186
421.47
2036 373.5
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297242
37019790

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1221.65
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32.90

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7800
6200

99637
200.6
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3971.80
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2066.1988
999336
1988
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999464
999377
49933
198.668804
0.57 186.65
99987
186.65
499935
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13024 500
97344 48622
22029 240
92344 3
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99916 49993
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499570
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297242
37019790

2640
1220
15380
15380
3905 477
99766
477
648362
648362
349064
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18
493.92
139 313 2059 280
9996
913 56 99758
29918
9996
798064
29988 199516
3128748 2793254
7012 80.2 0048 217
9921 9999
802 217
19924 69993
793680 9999
7956643 19998
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1020 80 2640 26
2640

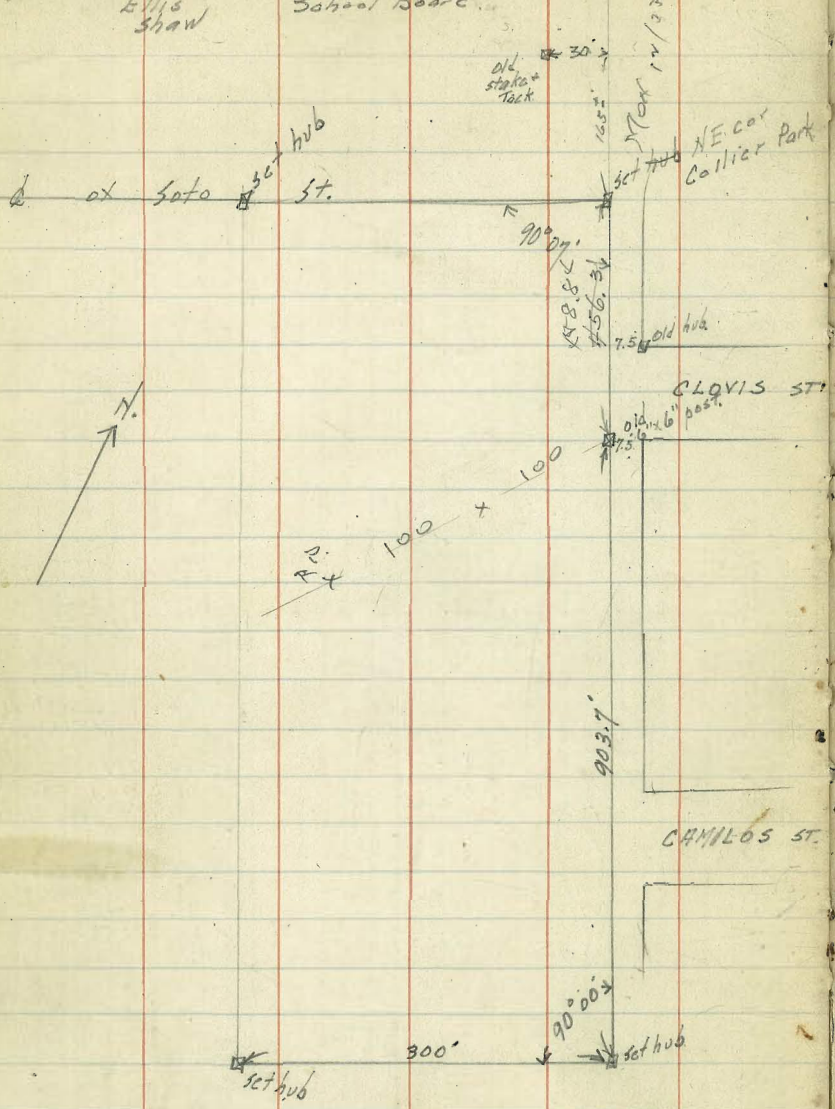
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6200

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200.6
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2989110
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300 500
.79821 49910
3040
9999
43968
798860
598740
998155
299385
3971.80
438.7786560
2066.1988
999336
1988
799464
999464
999377
49933
198.668804
0.57 186.65
99987
186.65
499935
159922
599922
799846
79987
186.625735
13024 500
97344 48622
22029 240
92344 3
367596
186798
2217596
395410
0.581 500
99916 49993
300 422.07
422
199726
109726
399452
47142186
421.47
2036 373.5
49112
13115
499570
247346
693793
297242
37019790

2640
1220
15380
15380
3905 477
99766
477
648362
648362
349064
49548382
18
493.92
139 313 2059 280
9996
913 56 99758
29918
9996
798064
29988 199516
3128748 2793254
7012 80.2 0048 217
9921 9999
802 217
19924 69993
793680 9999
7956643 19998
2169783
1301 500 1220 346
99963 49911 99967
346
599802
899703
299901
39586932

11/5/22
Gregory
Moore
Ellis
Shaw

Survey of Portion of
Collier Park for
School Board



11/5/22
Gregory
Moore
Ellis
Shaw

Project Gregor

CROSS SECTION OF
3RD ST.
from N.L. Redwood to N.L. Quince
N.L. Redwood

6.93	272.46	265.53
W	0.1	272.3 ✓
14' E		
20' E = cb line	0.5	271.9 ✓ 272.0
30'		
50' ✓	1.0	271.2 ✓ 271.2
70'	4.5	267.9 ✓
80' ✓	9.7	262.7 ✓

N. Curb line Redwood = 14' S. of N.L.

20' E of W.L.	10.2	262.2 ✓
65' ✓	7.9	262.5 ✓
50' ✓	4.2	266.0 ✓
49' ✓	2.4	270.0 ✓
40' ✓	0.4	272.0 ✓
20' ✓	0.5	271.9 ✓ 271.9
W.L.	0.9	271.5 ✓ 271.5

6' S. of N. Cb Line Redwood.

W.L.	1.0	271.2 ✓ 271.2
37' E	0.6	271.8 ✓ 271.8
50' ✓	5.5	266.9 ✓
65' ✓	7.7	262.7 ✓
80' ✓	11.0	261.2 ✓

13' S. of N. Cb Line of Redwood

80' E. of W.L.	10.8	261.6 ✓
60' ✓	5.2	267.2 ✓
40' ✓	3.3	269.1 ✓
30' ✓	0.6	271.8 ✓
W.L.	0.8	271.6 ✓ 271.7

Center of Redwood

W.L.	1.1	271.3 ✓ 271.3
15' E of W.L.	1.1	271.3 ✓
35' ✓	3.1	269.3 ✓
55' ✓	6.0	266.2 ✓
80' ✓	9.7	262.7 ✓

13' S. of Center of Redwood

80' E of W.L.	9.5	262.9 ✓
65' ✓	8.3	262.1 ✓
40' ✓	4.4	266.0 ✓ 269.1
20' ✓	2.2	270.2 ✓ 270.2
W.L.	1.7	270.7 ✓ 270.7

26' S. of Center of Redwood

W.L.	1.4 ✓	271.0 ✓ ✓ on corner
7' E	1.6	270.8 ✓ 270.8
20' ✓	3.2	269.2 ✓ 269.2
40' ✓	5.1	267.3 ✓ 268.3
60' ✓	7.8	262.6 ✓
80' ✓ on Edge gravel drive	10.4	262.0 ✓

5' S. of Redwood

80' E of W.L. on Edge drive	10.8	261.6 ✓
65' ✓ on lawn	9.6	262.8 ✓
55' ✓	9.5	262.9 ✓
45' ✓ in path	11.1	261.3 ✓
35' ✓	10.7	261.7 ✓ 266.7
29' ✓ = edge roadway	6.4	266.0 ✓

	272.46	272.4	266.7
11' E of W.L.		5.6	√66.8 ✓
W.L.		2.0	√70.4 ✓
10' 5.0 x 5.0 L Redwood.			
W.L.		3.6	√68.8 ✓
TP.	3.93	269.41	6.98 265.48
10' E. of W.L.		4.3	√65.1 ✓
14' " " "		5.5	√63.9 ✓ 263.9
20' " " "		5.1	√64.3 ✓
29' " " "	wedge of Roadway.	5.3	√64.1 ✓ 263.4
33' " " "	in path wedge garden	8.0	√61.2 ✓
45' " " "		9.1	√60.3 ✓
53' " " "	on lawn.	7.2	√62.1 ✓
65' " " "		6.9	√62.5 ✓
80' " " "		7.6	√61.8 ✓
27' 5.0 x 5.0 L Redwood			
80' E. of W.L.		7.7	√61.7 ✓
65' " " "	on lawn.	7.8	√61.6 ✓
45' " " "		9.9	√59.5 ✓
33' " " "	W. edge garden	9.0	√60.4 ✓
19' " " "		7.4	√62.0 ✓ 260.4
10' " " "		6.0	√63.2 ✓ 262.2
W.L.		2.5	√66.9 ✓
40' 5.0 x 5.0 L Redwood			
W.L.		2.9	√66.5 ✓
13' E. of W.L.		7.3	√62.1 ✓
33' " " "	W. Edge of garden.	9.4	√60.0 ✓ 260.3

	269.4	3rd
49' E. of W.L.	10.3	√59.1 ✓
50' " " "	11.2	√58.1 ✓
65' " " "	13.4	√56.0 ✓
68' " " "	16.2	√53.1 ✓
55' 5.0 x 5.0 L Redwood.		
69' E. of W.L.	16.7	√54.7 ✓
61' " " "	16.3	√53.1 ✓
60' " " "	13.7	√55.7 ✓
49' " " "	12.3	√57.1 ✓
48' " " "	11.0	√58.2 ✓
35' " " "	10.3	√59.1 ✓ 259.2
18' " " "	8.6	√60.8 ✓
10' " " "	7.1	√61.3 ✓ 261.2
W.L.	1.7	√67.7 ✓
70' 5.0 x 5.0 L Redwood		
W.L.	2.1	√67.3 ✓
10' E	6.7	√62.7 ✓ 261.9
25' "	9.6	√59.8 ✓ 258.2
45' "	12.4	√57.0 ✓
56' "	13.5	√55.9 ✓
61' "	18.3	√51.1 ✓
65' "	19.0	√50.4 ✓
75' 5.0 x 5.0 L Redwood = N.L. of Garage		
65' E. of W.L.	18.3	√51.1 ✓
61' " " "	17.6	√51.5 ✓
56' " " "	13.0	√56.4 ✓

26941

269.4

50' E of W.L. = NW cor. of garage

12.8 ✓ 56.6 ✓

25' " " "

10.1 ✓ 59.3 ✓

6' " " "

5.3 ✓ 62.1 ✓

W.L.

2.8 ✓ 66.6 ✓

75.4' 5.0 x Redwood

W.L.

2.8 ✓ 66.6 ✓

6' E

5.3 ✓ 62.1 ✓

25' ✓

10.1 ✓ 59.3 ✓

50' ✓ = front line of garage

12.8 ✓ 56.6 ✓

65' ✓ = back of garage

12.9 ✓ 56.5 ✓

100' 5.0 x Redwood

66' E = back line of garage

13.4 ✓ 56.0 ✓

50' ✓ = S.W. cor. garage

12.7 ✓ 56.7 ✓

40' ✓

11.3 ✓ 58.1 ✓

30' ✓

9.1 ✓ 60.3 ✓

16' ✓

7.4 ✓ 62.0 ✓

W.L.

2.2 ✓ 67.4 ✓

104' 5.0 x Redwood

W.L.

2.1 ✓ 67.5 ✓

7' E of W.L.

4.7 ✓ 64.7 ✓

16' " " "

7.4 ✓ 62.0 ✓

30' " " "

9.1 ✓ 60.3 ✓

50' " " "

10.7 ✓ 58.7 ✓

64' " " "

11.6 ✓ 57.8 ✓

70' " " "

13.8 ✓ 55.6 ✓

30

269.4
3rd
114' 5.0 x 5.0 Redwood

70' E of W.L.

133 ✓ 56.1 ✓

57' " " "

113 ✓ 58.1 ✓

35' " " "

93 ✓ 60.1 ✓

15' " " "

73 ✓ 62.1 ✓

6' " " "

49 ✓ 64.5 ✓

W.L.

22 ✓ 67.4 ✓

120' 5.0 x 5.0 Redwood

W.L.

24 ✓ 67.0 ✓

6' E of W.L.

5.4 ✓ 64.0 ✓

10' " " "

6.6 ✓ 62.8 ✓

30' " " "

88 ✓ 60.6 ✓

49' " " "

110 ✓ 58.2 ✓

59' " " "

138 ✓ 55.6 ✓

70' " " "

154 ✓ 52.0 ✓

135' 5.0 x 5.0 Redwood

80' E of W.L.

243 ✓ 45.1 ✓

73' " " "

220 ✓ 47.2 ✓

60' " " "

196 ✓ 49.8 ✓

50' " " "

172 ✓ 52.2 ✓

35' " " "

118 ✓ 57.6 ✓

25' " " "

88 ✓ 60.6 ✓

8' " " "

62 ✓ 63.2 ✓

W.L.

30 ✓ 66.2 ✓

149' 5.0 x 5.0 Redwood

W.L.

28 ✓ 66.6 ✓

26941

13' E. of WL	5.4	√61.0	263.2
15' " " "	6.1	√63.3	
23' " " "	7.2	√62.2	
24' " " "	8.8	√60.6	259.6
35' " " "	14.4	√55.0	
50' " " "	20.8	√48.6	
62' " " "	24.0	√45.4	
70' " " "	26.6	√42.8	

150' S

70' E. of WL	26.7	√42.7	
62' " " "	24.1	√45.3	
50' " " "	20.8	√48.6	
35' " " "	14.5	√52.9	275
24' " " "	8.8	√60.6	
23' " " "	7.2	√62.2	
15' " " "	6.1	√63.3	263.9
10' " " "	2.7	√66.7	
W.L. on walk	1.1	√68.3	

165' S of S.L. Redwood

W.L. on walk front of house	0.8	√68.6	
10' E. of WL	1.3	√68.1	266.1
19' " " "	6.3	√63.1	
25' " " "	10.0	√59.4	
32' " " "	13.2	√56.1	257.1
41' " " "	18.7	√50.7	
58' " " "	24.3	√45.1	
70' " " "	31.0	√38.4	

177' 3rd St

60' E. of WL	25.1	√42.3	
50' " " "	21.1	√48.3	258.00
28' " " "	10.4	√59.0	
24' " " "	9.1	√60.3	
23' " " "	6.8	√62.6	
18' " " "	5.8	√63.6	264.4
11' " " "	1.0	√68.6	
W.L. on walk	0.8	√68.6	

185' S. of S.L.

W.L. on walk	0.75	√68.7	
11' E. of WL	1.0	√68.4	265.8
16' " " "	4.6	√62.8	
24' " " "	6.6	√62.8	
25' " " "	8.4	√61.0	260.7
34' " " "	9.0	√60.4	
40' " " "	11.3	√58.1	
49' " " "	16.8	√52.6	
60' " " "	24.1	√45.3	

200' S. of S.L. Redwood

60' E. of WL	20.7	√48.7	
41' " " "	8.6	√60.8	
39' " " "	6.7	√62.7	265.2
19' " " "	4.2	√65.2	
15' " " "	1.3	√68.1	268.1
W.L. on walk	0.75	√68.7	

TR	0.63	268.24	266.7	1.50	267.61
		206.5			
W.L.			0.0	268.1	✓ 267.9
16 E			0.3	✓ 267.4	✓ 267.9
20 ✓			2.2	✓ 266.0	✓
30 ✓			3.9	✓ 264.3	✓
41 ✓			5.7	✓ 262.5	✓
55 ✓			16.1	✓ 252.1	✓
60 ✓			18.6	✓ 249.2	✓

		211.5			
65 E. of W.L.			21.3	✓ 241.9	✓
55 ✓			16.0	✓ 252.2	✓
40 ✓			3.7	✓ 264.5	✓
33 ✓			0.9	✓ 267.5	✓ 267.9
15 ✓			0.3	✓ 267.9	✓ 267.9
W.L.			0.0	✓ 268.7	✓

		235.5			
W.L.			0.1	✓ 268.1	✓
2' E of W.L.			0.5	✓ 267.7	✓
20 ✓			1.1	✓ 267.1	✓ 267.2
33 ✓			1.2	✓ 267.0	✓ 267.0
37 ✓			3.9	✓ 262.3	✓
41 ✓			10.8	✓ 257.2	✓
55 ✓			19.5	✓ 248.7	✓
65 ✓			26.0	✓ 241.2	✓

3rd

		253.5	268.2	
55' E. of W.L.			24.8	✓ 243.2 ✓
50 ✓			19.8	✓ 248.2 ✓
37 ✓			11.1	✓ 257.1 ✓
33 ✓			1.5	✓ 266.7 ✓ 266.5
27 ✓			1.7	✓ 266.5 ✓
14 ✓			14	✓ 266.8 ✓
W.L.			0.0	✓ 268.2 ✓

To house 4' wide

256.5 5 = N. edge of walk	260.5			
W.L. on walk to house		+ 0.38		268.58
+ 14.0 E. edge of cement ed.		0.95		✓ 267.39 ✓
14.2 ✓ of W.L.		1.8		✓ 266.2 ✓
29 ✓		1.8		✓ 266.2 ✓ 266.5
32 ✓		1.6		✓ 266.6 ✓
36 ✓		4.6		✓ 263.6 ✓
38 ✓		10.3		✓ 257.9 ✓
48 ✓		18.2		✓ 250.0 ✓

		270.5		
48' E of W.L.			17.4	✓ 250.8 ✓
40 ✓			10.5	✓ 257.7 ✓
32 ✓			2.1	✓ 266.1 ✓ 265.9
27 ✓			2.5	✓ 265.7 ✓
14.2 ✓			2.7	✓ 265.5 ✓
14.0 ✓ = cement ed.			1.95	✓ 266.3 ✓
W.L.			0.3	✓ 267.9 ✓

268 25

290' S. 268 25

W.L. on lawn	1.7	√66.5	✓
14' E of W.L. = curb	4.13	√64.1	✓
14.2 " " "	4.6	√63.7	✓
21 " " "	4.1	√64.1	✓
27' E " " "	4.3	√63.9	✓
30 " " "	3.7	√64.5	✓
40 " " "	16.3	√51.9	✓

301.5' S. = N.L. Quince

39 E of W.L.	16.0	√54.2	✓
37 " " "	11.7	√56.5	✓
38 " " "	7.1	√61.1	✓
31 " " "	5.0	√63.2	✓
27 " " "	4.6	√63.7	✓
26.9 " " "	4.9	√63.3	✓
14.0 " " " = cement curb	5.34	√64.9	✓
W.L. on lawn	4.4	√63.8	✓
chk on curb W.L. 3 rd Ncb Quince	5.40	√64.8	✓

3rd St.

1/21/23 Gregory

CROSS SECTION OF
PALM ST. 80' wide 14' cbs
from E.L. 1st to

209.04

PALM, 214.76

34

	1.09	264.12	263.03	2nd Q. 100	+L
T.P.	0.07	252.39	11.80	252.32	+9
	0.75	249.04	4.10	248.29	cb
	E.L. 1st St. 80' St 14' cbs				+9
2' N. of N.L.		0.2	248.8		1/4
N.L.		2.6	246.0		c
cb		12.6	236.4		1/4
+3		15.1	233.9		cb
+11		16.4	237.6		5
1/4		19.3	229.7		
c		28.5	220.5		5
1/2		34.4	214.6		cb
cb		37.1	211.9		1/4
5		39.4	209.6		c
	E. Curb				1/4
5		48.9	200.1		+2
+10		46.1	202.9		+9
cb		44.7	204.3		cb
1/4		36.2	212.8		+4
c		28.6	220.4		N
1/4		20.1	228.9		
+5		15.6	233.2		N
cb		13.4	235.4		+3
N		1.0	248.0		+5
	6' W. of E. Curb				cb
N		1.1	247.9		+8

E. Quarter

24	246.6	✓
12.0	237.6	✓
13.2	235.8	✓
15.6	233.4	✓
21.8	227.8	✓
28.6	220.4	✓
36.4	212.6	✓
43.7	205.3	✓
51.2	197.8	✓
48.9	200.1	✓
41.6	207.4	✓
35.6	213.4	✓
27.9	221.1	✓
20.6	228.4	✓
16.6	232.4	✓
13.2	235.8	✓
12.5	236.5	✓
11.7	237.3	✓
1.3	247.7	✓
Center 1st		
1.3	247.7	✓
1.6	247.9	✓
6.4	242.6	✓
12.2	236.8	✓
12.6	236.6	✓

249.04

1/4	15.6	233.4	✓
+5	22.5	226.5	✓
C	24.2	222.8	✓
1/4	31.0	218.0	✓
cb	35.2	213.8	✓
S	42.8	206.2	✓
W. 1/4			
S	37.0	217.0	✓
cb	30.7	218.3	✓
1/4	26.0	223.0	✓
C	20.2	228.8	✓
+4.5	17.7	231.3	✓
+7	15.1	233.9	✓
1/4	12.2	236.8	✓
+8	10.7	238.3	✓
cb	6.8	242.2	✓
+3	2.4	246.6	✓
N	2.4	246.6	✓
W. Curb			
N	2.9	246.3	✓
(on cement curb)	(2.12)	246.92	✓
cb.	2.9	246.1	✓
+6	3.2	245.8	✓
+12	4.9	244.3	✓
1/4	10.8	238.2	✓
+9	11.7	237.3	✓

PALM ST

35

C	14.5	234.5	✓
+8	1.84	230.6	✓
1/4	20.9	228.1	✓
cb	28.3	220.7	✓
S	34.6	214.4	✓
W. Line 1st St.			
S	30.8	218.2	✓
cb	24.0	225.0	✓
1/4	17.3	231.7	✓
C	11.2	237.8	✓
+9	11.1	237.9	✓
1/4	8.8	240.2	✓
+1	4.3	244.7	✓
cb	3.6	245.4	✓
+6	3.2	245.8	✓
N	2.2	246.8	✓
5' W			
-5	3.2	245.8	✓
N	3.7	245.3	✓
cb	4.0	245.0	✓
+12	3.8	245.2	✓
1/4	9.4	239.6	✓
+4	11.1	237.9	✓
cb	11.6	237.4	✓
+2	11.6	237.4	✓
+2.3	12.0	236.0	✓

24904

1/4	16.6	237.4	✓
cb	23.0	226.0	✓
S	29.8	219.2	✓

25' W.

S	31.9	217.1	✓
cb	24.4	224.6	✓
1/4	18.4	230.6	✓
C	12.4	236.6	✓
+9	11.5	237.5	✓
1/4	10.0	239.0	✓
+1	5.1	243.9	✓
cb	6.0	243.0	✓
N	5.5	243.5	✓

40' W.

N	7.2	241.8	✓
cb	7.4	241.6	✓
+10	7.5	241.5	✓
1/4	9.3	239.7	✓
+4	10.5	238.5	✓
+9	10.8	238.2	✓
C	13.0	236.0	✓
1/4	17.2	231.8	✓
cb	24.4	224.6	✓
S	32.9	216.1	✓

52' W.

S	31.8	217.2	✓
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157

PALM

30

cb	25.3	223.7	✓
1/4	18.6	230.4	✓
C	12.8	236.2	✓
+4	10.5	238.5	✓
1/4	9.1	238.9	✓
cb	8.7	240.3	✓
N	8.5	240.5	✓
T.P.	170	239.98	✓

67' W.

N	1.0	239.0	✓
cb	1.3	238.7	✓
1/4	1.8	238.2	✓
+8	3.1	236.9	✓
C	6.0	234.0	✓
1/4	10.9	229.1	✓
+9	13.3	226.7	✓
cb	17.3	222.7	✓
+5	18.4	221.6	✓
S	24.0	216.0	✓

85' W.

S	21.9	218.1	✓
cb	13.5	226.5	✓
+10	7.9	232.1	✓
1/4	7.5	232.5	✓
C	5.7	234.9	✓
+5	3.6	236.4	✓

239.98

1/4	3.6	236.4 ✓
ct	3.1	236.9 ✓
N	3.0	237.0 ✓
	103' W	
N	4.5	235.5 ✓
ct	4.8	235.2 ✓
1/4	5.2	234.8 ✓
C	5.5	234.5 ✓
1/4	5.9	234.1 ✓
+7	6.9	233.1 ✓
+9	11.0	229.0 ✓
ct	11.8	228.2 ✓
S	13.9	226.1 ✓ ^{ct. of drive}
	121' W	
S	16.0	224.0 ✓ ^{W. of drive}
+3	8.6	231.4 ✓
ct	7.8	232.2 ✓
1/4	7.3	232.7 ✓
C	7.3	232.7 ✓
1/4	6.9	233.1 ✓
ct	6.6	233.4 ✓
N	6.2	233.8 ✓
	125' W	
N	6.8	233.2 ✓
ct	7.1	232.9 ✓
1/4	7.2	232.8 ✓

239.98

Palm St 37

C	7.7	232.3 ✓
1/4	7.8	232.2 ✓
ct	8.1	231.9 ✓
S	9.1	230.9 ✓ ^{Lane}
	155' W	
S	11.0	229.0 ✓ ^{Lane}
ct	11.1	228.9 ✓
1/4	10.9	229.1 ✓
C	10.7	229.3 ✓
1/4	10.1	229.9 ✓
ct	9.6	230.4 ✓
N	9.7	230.3 ✓
	180' W	
N	11.6	228.4 ✓
ct	12.2	227.8 ✓
1/4	12.6	227.4 ✓
C	12.7	227.3 ✓
1/4	13.0	227.0 ✓
ct	12.9	227.1 ✓
S	13.3	226.7 ✓ ^{ct. of drive garage}
T.P. 027	227.31 ✓	12.94 227.04 ✓
	197' W	
S	1.6	225.7 ✓
ct	2.0	225.3 ✓
1/4	1.3	226.0 ✓
C	1.3	226.0 ✓

227.31

1/4	1.3	226.0 ✓
cb	1.6	225.7 ✓
N	1.1	226.2 ✓
EL Front		80' wide 20' deep
N	2.8	224.5 ✓
cb	1.8	225.5 ✓
1/4	1.7	225.6 ✓
c	1.6	225.7 ✓
1/2	2.0	225.3 ✓
cb	2.2	225.1 ✓
S	1.8	225.5 ✓
E cb		
S	3.1	224.2 ✓
+7	3.0	224.3 ✓
cb	3.6	223.7 ✓
1/4	3.3	224.0 ✓
c	3.0	224.3 ✓
1/2	2.9	224.4 ✓
cb	3.4	223.9 ✓
N	3.9	223.9 ✓
E 1/2		
N	4.2	223.1 ✓
cb	3.4	223.9 ✓
1/4	3.6	223.7 ✓
c	3.5	223.8 ✓
1/2	3.9	223.4 ✓

227.31

Palm St 38

cb	4.0	223.3 ✓
+6	3.7	223.6 ✓
S	3.8	223.5 ✓
C		
S	4.3	223.0 ✓
+13	4.6	222.7 ✓
cb	5.0	222.3 ✓
1/2	4.6	222.7 ✓
c	4.2	223.1 ✓
1/4	4.2	223.1 ✓
cb	4.0	223.3 ✓
+11	4.2	223.1 ✓
N	5.0	222.3 ✓
W 1/4		
N	6.1	221.2 ✓
cb	5.2	222.1 ✓
1/2	4.6	222.7 ✓
c	4.8	222.5 ✓
1/4	5.2	222.1 ✓
cb	5.3	222.0 ✓
S	5.2	222.1 ✓
W cb		
S	5.8	221.5 ✓
cb	5.9	221.4 ✓
1/2	5.8	221.5 ✓
c	5.5	221.8 ✓

227.31

1/4	5.3	222.0 ✓
cb	5.7	221.6 ✓
N	6.7	220.6 ✓

Cocos Palm 11' W of cb + 12' N of St

W Front

N	7.8	219.5 ✓
cb	7.3	220.0 ✓
1/4	6.4	220.9 ✓
c	6.3	221.0 ✓
1/4	6.7	220.6 ✓
cb	6.9	220.4 ✓
S	7.2	220.1 ✓

Cocos Plumosa Palm 10' W 11.7' N of St

20' W

S	7.7	219.6 ✓
cb	7.7	219.6 ✓
1/4	7.3	220.0 ✓
c	7.1	220.2 ✓
1/4	7.0	220.3 ✓
cb	7.2	220.1 ✓
N	7.3	220.0 ✓

Cocos Palm 29.5' W 11.6' N of St

50' W

N	8.5	218.8 ✓
cb	8.1	219.2 ✓
1/4	7.9	219.4 ✓

227.31

Palm St 39

c	8.0	219.3 ✓
1/4	8.4	218.9 ✓
cb	8.2	219.1 ✓

+ 2.3 Cocos palm

S	9.1	218.2 ✓
---	-----	---------

Cocos palm 70' W + 11.7' N of St

" " 90' + 11.7' " "

105' W

S	9.9	217.4 ✓
+ 2.8	9.65	217.66 ✓ NE Cor of Garage
+ 4.8	9.72	217.59 ✓ " " " " " " " " " " " " " " " " " "
cb	9.8	217.5 ✓
1/4	9.7	217.6 ✓
c	9.2	218.1 ✓
1/4	9.3	218.0 ✓
cb	9.4	217.9 ✓
N	9.8	217.5 ✓

116' W Cocos Palm 11' N of St

117.7' W

cb + 9.4	9.83	217.48 ✓ NW Cor of Garage
cb + 11.4	9.73	217.58 ✓ " " " " " " " " " " " " " " " " " "

140.5' W Cocos Palm 10' N of St

150' W

N	11.4	215.9 ✓
cb	10.9	216.4 ✓
1/4	10.4	216.9 ✓

227.31

C	10.3	217.0 ✓
1/4	10.7	216.6 ✓
cb	11.0	216.3 ✓
+11	11.0	216.3 ✓ edge of lawn
S	10.4	216.9 ✓ lawn

166' w/ Casco Palm 9.5' N of sb

190.3 - - - 9' - - -

EV H/lot cross

80' ST
14' sidewalk

S	11.9	215.4 ✓ lawn
+2	12.2	215.1 ✓ edge of lawn
A	12.2	215.1 ✓
1/4	12.1	215.2 ✓
C	11.5	215.8 ✓
1/4	11.7	215.6 ✓
cb	12.1	215.2 ✓
N	11.9	214.6 ✓
T.P.	2.50 217.11 ✓	12.90 214.61 ✓

E Curb

N	2.6	214.5 ✓
cb	2.2	214.9 ✓
1/4	2.1	215.0 ✓
C	1.5	215.6 ✓
1/4	1.9	215.2 ✓
cb	2.3	214.8 ✓
S	2.2	214.9 ✓

PALM.

40

E 1/4

S	2.5	214.6 ✓
cb	2.4	214.7 ✓
1/4	2.1	215.0 ✓
C	2.0	215.1 ✓
1/4	2.2	214.9 ✓
cb	2.4	214.7 ✓
N	2.7	214.4 ✓

Center

N	3.4	213.7 ✓
cb	2.8	214.3 ✓
1/4	2.6	214.5 ✓
C	2.43	214.68 ✓ ^{214.76} on floor
1/4	2.4	214.7 ✓
cb	2.2	214.9 ✓
S	2.5	214.6 ✓

W 1/4

S	3.0	214.1 ✓
cb	2.8	214.3 ✓
1/4	2.8	214.3 ✓
C	2.7	214.4 ✓
1/4	3.0	214.1 ✓
cb	3.1	214.0 ✓
N	3.0	214.1 ✓

W Cb

N	4.2	212.9 ✓
---	-----	---------

No use improving beyond this Cb line

217.11

cb	2.8	214.3	✓
1/4	3.0	214.1	✓
c	3.3	213.8	✓
1/4	3.5	213.6	✓
cb	3.7	213.4	✓
S	3.6	213.5	✓

6' W. of W. CB

S	4.2	212.9	✓
cb	4.7	212.4	✓
1/4	4.5	212.6	✓
c	4.0	213.1	✓
1/4	3.4	213.7	✓
cb	4.6	212.5	✓
N	10.7	206.4	✓

W. L. Albatross

N	16.0	201.1	✓
cb	11.0	206.1	✓
1/4	8.2	208.8	✓
c	8.5	208.6	✓
1/4	10.1	207.0	✓
cb	10.5	206.6	✓
S	8.0	209.1	✓

PALM

41

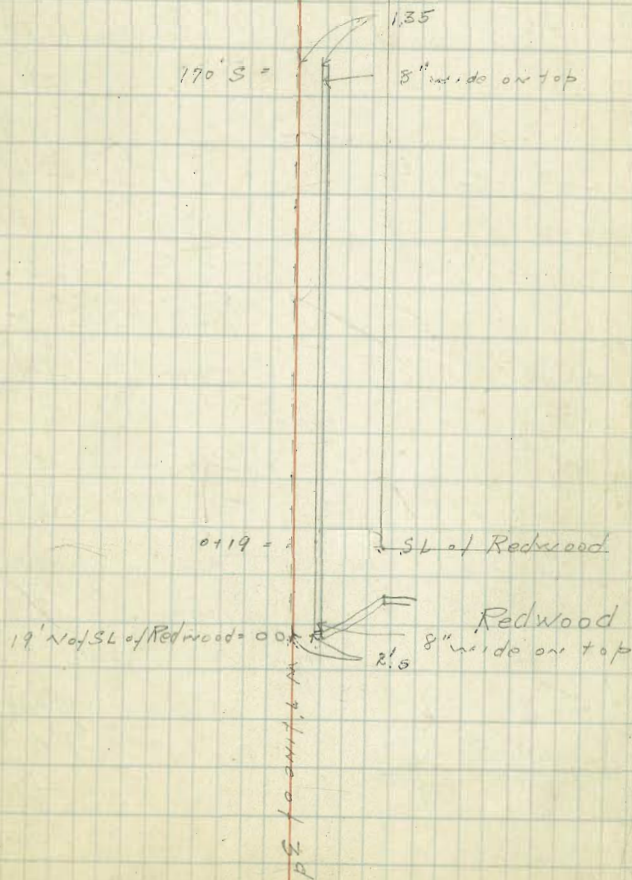
Moore 1/6/25
Walker
Preston W side of 34th St betw Redwood + Quince

Levels on Retaining W/9/1

on BM	670	272.23	265.53	NWCP 2 nd Redwood
19' N of SL of Redwood = 000 top of wall	✓	✓	1.2'	271.02
✓ ✓ ✓ on paving	✓	✓	1.56	270.67
19' S = SL of Redwood top of wall	✓	✓	1.28	270.95
✓ ✓ ✓ feet ✓ ✓	✓	✓	5.5	266.73
39' S top ✓ ✓	✓	✓	3.17	269.06
✓ ✓ ✓ feet ✓ ✓	✓	✓	7.4	264.83
61' S top ✓ ✓	✓	✓	3.38	268.85
✓ ✓ ✓ feet ✓ ✓	✓	✓	9.3	262.93
77' ✓ top ✓ ✓	✓	✓	3.28	268.95
✓ ✓ ✓ feet ✓ ✓	✓	✓	8.20	264.03
101' S top ✓ ✓	✓	✓	3.24	268.99
✓ ✓ ✓ feet ✓ ✓	✓	✓	8.5	263.73
119' S top ✓ ✓	✓	✓	3.24	268.99
✓ ✓ ✓ feet ✓ ✓	✓	✓	7.5	264.73
159' S top ✓ ✓	✓	✓	3.33	268.90
✓ ✓ ✓ feet ✓ ✓	✓	✓	8.3	263.43
170' S top ✓ ✓	✓	✓	3.33	268.90
✓ ✓ ✓ feet ✓ ✓	✓	✓	7.5	264.73

QUINCE

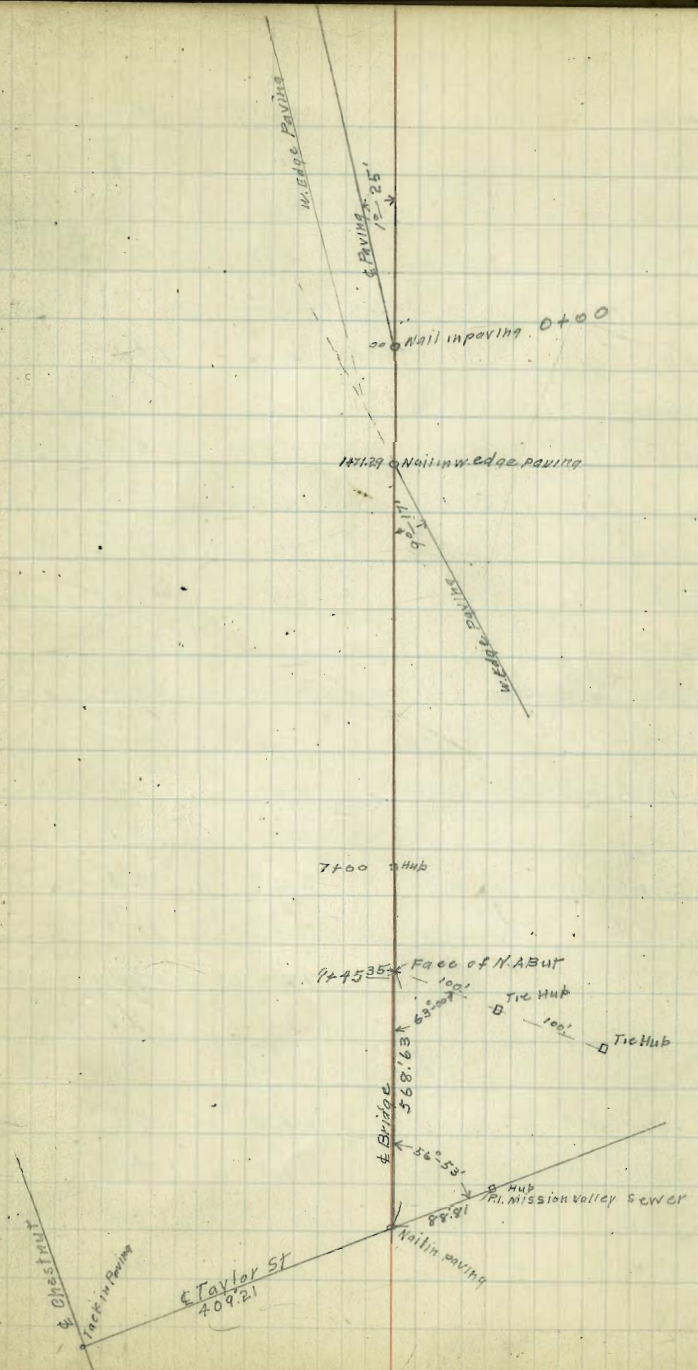
41



10/24/24 X. Sec. for Dyke N. of New Old Town Bridge

multi
shap
wall

B.M.	4.54	13.20	8.66	Hy. Cont. Whitman Taylor
T.P.	8.21	20.58	0.83	12.37
Set B.M. Elec Poles 79001 20'S. E. Taylor				
40' E of Mission Bell S. of Old Town Bridge		4.14	16.44	SPK
	6.46	17.87	9.17	11.41
00 Nail in paving Pt. Main Road				
10' E of E		4.15	12.7	ch edge paving
B		4.10	12.8	on paving
10' W of A		4.15	12.7	ch edge paving
15' W		4.0	13.9	edge of Berm
	0+50			
C		4.15	13.7	
8.7' W		4.20	13.7	edge paving
14' W		4.3	13.6	
21' W		9.0	8.9	
35' W		8.5	9.4	
	1+00			
40' W		8.2	9.7	
19' W		7.9	10.0	
12' W		4.5	13.4	
6.7' W		4.30	13.7	edge paving
	1+25			
4.9' W		4.32	13.6	edge paving
11' W		4.5	13.4	
17' W		7.8	10.1	
40' W		7.8	10.1	



	17.87 1+35			
40' W		7.8	10.1	
24' W		7.0	10.9	
9' W		4.6	13.2	
4' W		4.30	13.6	edge paving
	1+65			
0.8' W		4.35	13.5	
20' W		6.3	11.6	
40' W		7.5	10.4	
	1+7122 R.F. & Dyke			edge paving
35' W		8.3	9.6	
15' W		6.5	11.4	
12' W		5.4	12.5	
⊕ Dyke = wedge paving		4.50	13.4	
	1+80			
1.5 E of ⊕		4.60	13.3	on edge paving
⊕		5.0	12.9	
3' W of ⊕		5.5	12.4	
10' W		9.0	8.9	
22' W		14.4	3.5	
40' W		14.5	3.4	
	1+90			
40' W		14.5	3.4	
15' W		13.9	4.0	
5' W		8.6	9.3	
4' W		5.8	12.1	
⊕		4.7	13.2	
3' OE		4.54	13.3	on wedge paving

	17.87 2+15			
7' E		4.45	13.2	on paving
4' E		4.7	13.2	
⊕		8.8	9.1	
15' W		16.7	1.2	
35' W		15.3	2.6	
	2+35			
35' W		15.1	2.8	
5' W		12.4	5.5	
⊕		10.7	7.2	
8' E		4.4	13.5	
10' OE		4.40	13.5	on paving
	2+72			
16' E		4.46	13.4	" "
14' E		4.5	13.4	
⊕		12.3	5.6	
6' W		14.2	3.7	
35' W		14.2	3.7	
	3+00			
35' W		14.2	3.7	
⊕		13.7	4.7	
5' E		12.3	5.6	
14' E		8.6	9.5	
19' E		4.4	13.5	
21.5 E		4.53	13.3	edge paving

old town dyke

44

	3+50 17.87		
26'E	4.4	13.5	edge berm
20'E	10.1	7.8	
10'E	13.0	4.9	
⊕	14.1	3.8	
35'W	15.5	2.4	

	3+75		
35'W	14.7	3.2	
⊕	13.5	4.4	
17'E	13.0	4.9	
24'E	10.1	7.8	
31'E	4.7	13.2	edge berm

	3+80		
31'E	4.7	13.2	
26'E	9.4	8.5	
18'E	14.4	3.5	
⊕	14.1	3.8	
35'W	14.7	3.2	

	4+40		
35'W	14.3	3.6	
⊕	13.8	4.1	
10'E	13.6	4.3	
25'E	12.7	5.2	
35'E	9.5	8.4	

	17.87 4+80		
35'E	11.5	6.4	
25'E	13.0	4.9	
15'E	14.2	3.8	
⊕	14.2	5.8	
10'W	14.4	3.5	
35'W	12.7	5.2	

	5+00		
35'W	12.5	5.4	
⊕	14.3	3.6	
15'E	15.0	2.9	
25'E	13.6	4.3	
35'E	12.2	5.7	

	5+50		
35'E	11.7	6.2	
⊕	13.7	4.2	
10'W	13.4	4.5	
35'W	12.7	5.2	

	5+80		
35'W	13.0	4.9	
10'W	13.4	4.5	
⊕	13.7	4.2	
10'E	13.8	4.1	
35'E	13.6	4.3	

6+00

5.13

BM	6.30	17.71	11.41	5.13	9'W	8.5	-3.4
		6700			4	5.4	-1.3
35'E		13.4	4.3		13'E	2.3	+2.8
25'E		13.9	3.8		25'E	1.2	+3.9
4		14.3	3.4		34'E	0.0	+5.1
10'W		13.6	4.1			7750	
35'W		12.7	5.0		35'E	2.2	+2.9
		6750			25'E	3.0	+2.1
35'W		13.3	4.4		12'E	5.2	-0.1
15'W		14.0	3.7		2'E	7.4	-2.3 Water Level
4		14.1	3.6		4	8.9	-3.8
15'E		13.2	4.5		25'W	13.0	-7.9
35'E		12.0	5.7		45'W	8.8	-3.7
		7700				7760	
35'E		11.8	5.9		55'W	9.6	-4.5
25'E		12.5	5.2		25'W	12.5	-7.4
4		14.2	3.5		4	13.8	-8.7
T.P.	0.33	5.13	12.91	4.80	15'E	9.3	-4.2
10'W		5.1	0.0		25'E	7.3	-2.4
17'W		6.4	-1.3		35'E	4.7	+4
30'W		5.5	-0.4			7775	
39'W		4.8	+3		50'E	6.1	-1.0
		7725			45'E	7.4	-2.3 Water Level
43'W		7.0	-1.7		25'E	12.2	-7.1
20'W		11.3	-6.2		4	14.2	-9.1
15'W		11.0	-5.9		25'W	11.4	-6.5

5.13
5.13
5.13

	5.13		
		7+75 (cont)	
50'W		11.0	-5.9
	8+00		
50'W		9.4	-4.3
25'W		10.0	-4.9
☐		12.4	-7.3
25'E		13.6	-8.5
50'E		11.8	-6.7
60'E		10.9	-5.8
	8+25		
65'E		10.8	-5.7
25'E		11.7	-6.2
☐		11.3	-6.2
17'W		11.3	-6.2
25'W		9.4	-4.3
50'W		6.2	-1.1
	8+40		
35'W		1.3	+3.8
22'W		4.7	+4
☐		9.5	-4.4
25'E		7.6	-2.5
40'E		6.2	-1.1
55'E		7.0 ^{20?}	+3.1
	8+45		
55'E		6.6	-1.5
50'E		6.8	-1.7
38'E		5.3	-2

	5.13		
26'E		7.3	-2.2
5'E		7.3	-2.2
☐		6.0	-0.9
22'W		3.2	+1.9
31'W		0.3	+4.8
40'W		0.5	+4.6
	8+55		
40'W		0.5	+4.6
17'W		0.8	+4.3
☐		0.0	+5.1
25'E		3.4	+1.7
38'E		3.2	+1.9
50'E		6.4	-1.3

Moore Walker Preston
 1/2 Cross Section of Wightman
 1/2 Alabama to Louisiana
 60' wide
 10' s/w

Wightman - MSE Louisiana	0.59	290.50	289.91
WL Louisiana			
S Cem. cb		1.55	288.95
gut		2.0	288.5
1/4		1.7	288.8
c		1.4	289.1
1/4		1.2	289.3
gut		1.2	289.3
N cem. cb		0.53	289.97
NL		0.2	290.3
25' W			
NL		0.5	290.0
cb		1.7	289.8
1/4		2.0	288.5
c		2.3	288.7
1/4		2.5	288.0
gut		2.8	287.7
S Cem. cb		2.47	288.03
50' W			
S Cem. cb		3.35	287.15
gut		3.7	286.8
1/4		3.5	287.0
c		3.2	287.3
1/4		3.2	287.3
cb		2.7	287.8

	290.50	
N	1.9	288.6
75' W		
N	2.0	288.1
cb	3.3	287.2
1/4	3.8	286.7
c	3.7	286.8
1/4	4.2	286.3
gut	4.5	286.0
S cem. cb	4.7	286.73
100' W		
N	5.22	285.28
S gut	5.4	285.1
1/4	4.9	285.6
N	4.8	285.7
1/4	4.5	286.0
cb	4.0	286.5
N	3.1	287.4
125' W		
N	4.6	285.9
cb	5.0	285.5
1/4	5.2	285.3
c	5.6	284.9
1/4	5.7	284.8
S cem. cb + gut	6.14	284.36
135' W		
SL	5.9	284.8

Note: 135' curb + sidewalk in good shape.

290.50

End of Cemct	good for ydgs.	6.50	284.0
1/4		6.0	284.5
c		5.5	285.0
1/4		5.5	286.0
cb		-5.3	285.2
N		5.2	285.1
	150' W		
N		5.7	284.8
cb		5.8	284.7
1/4		5.9	284.6
c		6.4	284.1
1/4		6.6	283.9
cb		7.0	283.5
+5		6.6	283.9
S		5.8	284.7
	175' W		
S		5.8	284.7
+3		7.0	283.5
cb		7.3	283.2
1/4		7.0	283.5
c		7.2	283.3
1/4		6.5	284.0
cb		6.2	284.3
N		6.0	284.5
	200' W		
N		6.9	283.6

290.50

Wrightman

49

cb		7.1	283.4
1/4		7.2	283.3
c		7.5	283.0
1/4		8.0	282.5
cb		8.1	282.4
+7		7.2	283.3
SL		6.2	284.3
	225' W		
S		6.9	283.6
+H		8.0	282.5
cb		8.6	281.9
1/4		8.5	281.0
c		8.3	281.2
1/4		7.6	282.9
cb		7.6	282.9
N		7.5	282.0
	250' W		
N		8.7	281.8
cb		8.5	282.0
1/4		8.6	281.9
e		8.9	281.6
1/4		9.1	281.4
cb		9.0	281.5
+8		8.3	282.2
SL		7.6	282.9

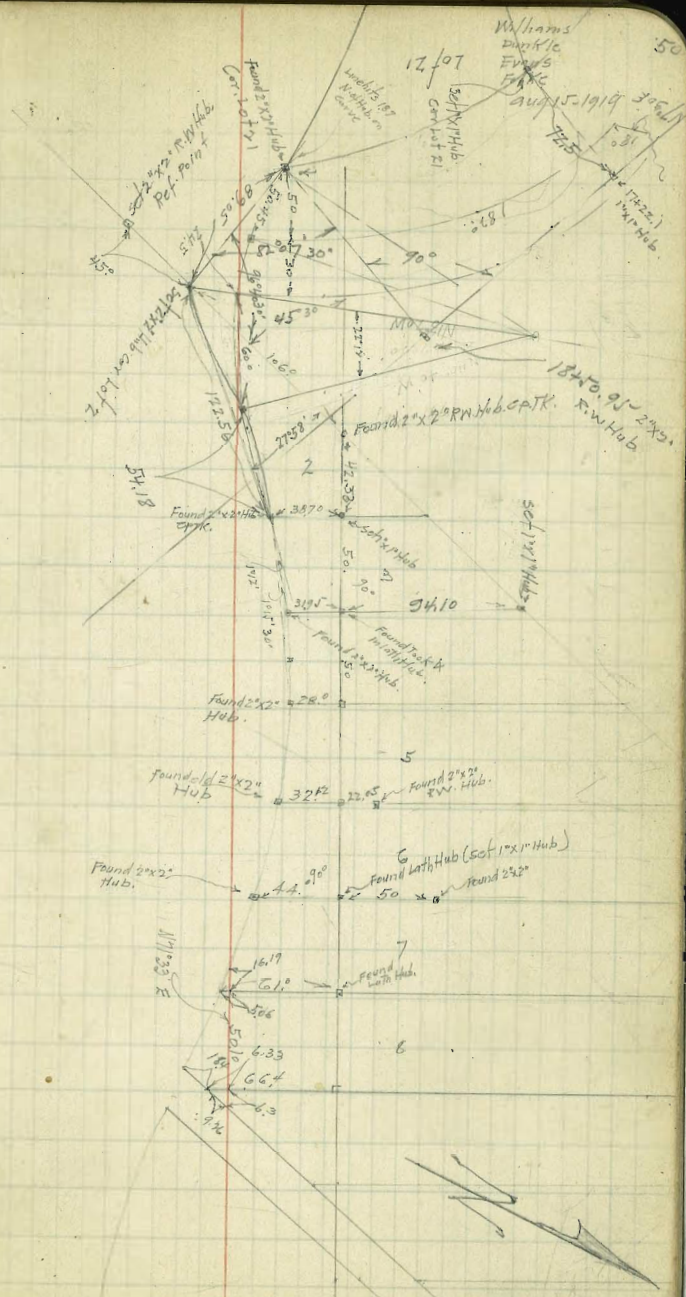
Continued Page 51

Resurvey of Amalfi LaSella
to determine North line Torrey Road

42.56
129.12

30
59.01

89.01



12/19/1919
12/19/1919
12/19/1919

From P 49

290.50

260' W

S	8.2	282.3
45	9.3	281.2
cb	9.3	281.2
1/4	9.4	281.1
e	9.6	280.9
1/4	9.8	280.7
cb	9.3	281.2
N	9.5	281.0

270' W = EL of Mississip

N	10.7	279.8
cen. dt good for ydgs	11.00	279.5
1/4	11.4	279.1
c	11.2	279.3
1/4	11.4	279.1
cen. dt ✓ ✓ ✓	11.50	279.0
S	11.0	279.5

290.50

Wightman 51

W L of Miss. = 0700

S	12.3	278.2
S cen. dt good for ydgs	12.50	278.0
1/4	11.8	278.7
c	12.1	278.4
1/4	12.0	278.5
cen. dt ✓ ✓ ✓	12.01	278.49
N	11.7	278.8

12' W

N	9.0	281.0
cb	8.9	281.6
1/4	9.3	281.2
c	9.5	281.0
1/4	9.7	280.8
cb	9.7	280.8
S	10.0	280.5

35' W

S	10.6	279.9
cb	10.5	280.0
1/4	10.8	279.7
c	10.5	280.0
1/4	10.5	280.0
cb	10.0	280.5
N	9.9	280.6

65' W

N	11.1	279.4
---	------	-------

290.50

dt			11.3	279.2
1/4			11.7	278.8
c			11.9	278.6
1/4			12.0	278.5
cb			11.7	278.8
S			12.0	278.5
		90' w		
S			13.6	276.9
cb			13.6	276.9
T.P.	0.72	278.28	12.9	277.56
1/4			1.7	276.6
c			1.3	277.0
1/4			1.2	277.1
dt			0.8	277.5
N			0.7	277.6
		115' w		
N			2.7	275.6
cb			3.1	275.2
1/4			3.5	274.8
c			3.5	274.8
1/4			3.8	274.5
+8			4.1	274.2
cb			3.7	274.6
S			3.2	275.1
		140' w		
S			5.4	272.9

278.28

Wrightman

52

+8			5.3	273.0
cb			5.9	272.4
+5			6.6	271.7
1/4			6.5	271.8
c			6.2	272.1
1/4			6.1	272.2
cb			5.8	272.5
N			5.8	272.5
		165' w		
N			7.6	270.7
cb			8.4	269.9
1/4			8.8	269.5
c			8.7	269.6
1/4			8.6	269.7
+5			9.1	269.2
cb			9.0	269.3
S			7.7	270.6
		190' w		
S			9.6	268.7
+5			10.5	267.8
cb			11.2	267.1
1/4			11.2	267.1
c			11.1	267.2
1/4			10.8	267.5
cb			10.7	267.6
N			10.3	268.0

278.28

215 W

N		12.1	266.2
+6		12.3	266.0
cb		13.2	265.1
1/4		13.4	264.9
C		13.3	265.0
1/4		13.0	265.3
cb		12.8	265.7
+2		12.2	266.1
SL		11.8	266.5
T.P	0.89	266.21	12.96 265.32
	240 W		
S		2.0	264.2
+8		2.4	263.8
cb		3.1	263.1
1/4		3.9	262.3
+5		4.3	261.9
C		4.2	262.0
1/4		3.6	262.6
+5		3.8	262.8
cb		3.1	263.1
+6		2.3	263.9
N		1.6	264.6
	255 W		
N		3.2	263.0
cb		4.0	262.2
+3		4.8	261.4

266.21

Wightman

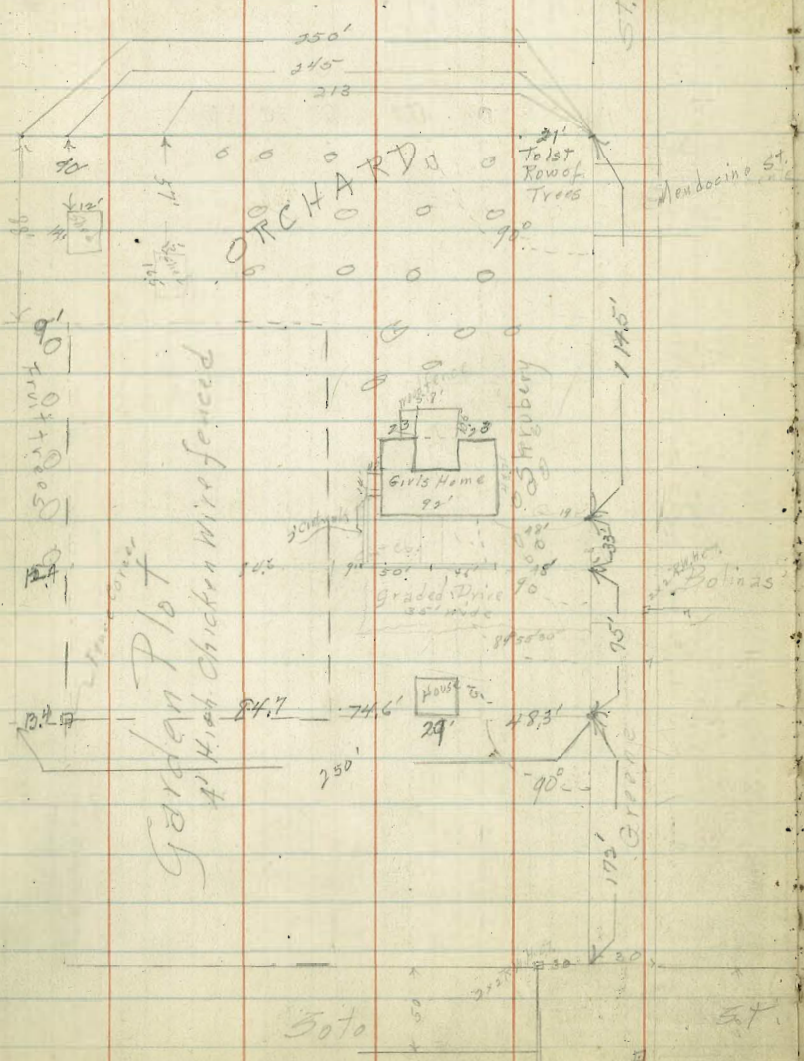
53

1/4		5.3	260.9
+6		6.2	260.0
C		6.8	259.4
1/4		7.0	259.2
cb		7.4	258.8
+4		6.8	259.4
+8		5.4	260.8
SL		4.0	262.2
	268 W = EL of Alabama Approx.		
S		10.0	256.2
3 cem. cb. good for ydgs		10.66	255.55
1/4		9.8	256.4
C		9.5	256.7
1/4		8.8	257.4
✓ cem. ct		10.20	256.0
cb. for ydgs		9.5	256.7
NL		9.4	256.8
T.P check to BMSERP		10.67	255.54

File in
Wightman
255.55

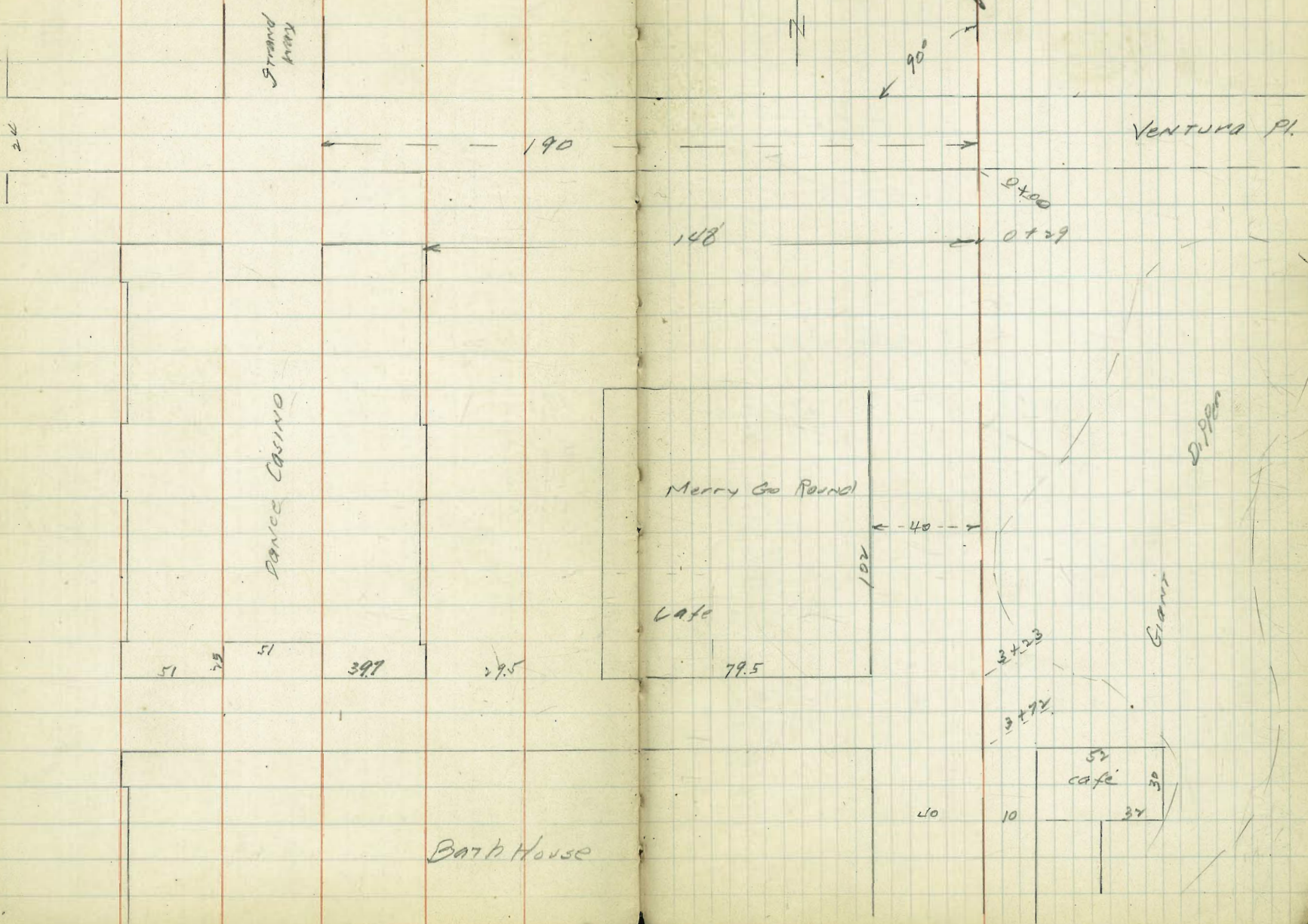
The image shows an open notebook with two facing pages. The pages are cream-colored and feature light blue horizontal ruling. The left page is divided into five vertical columns by four red lines. The right page is divided into two vertical columns by one red line. The notebook is bound in the center, and the pages are otherwise blank.

Survey of Girls Home
Collier Park

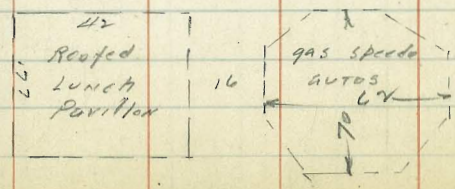
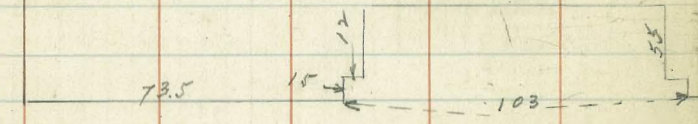


LOCATION of Bldgs.
MISSION BEACH AMUSEMENT CENTER

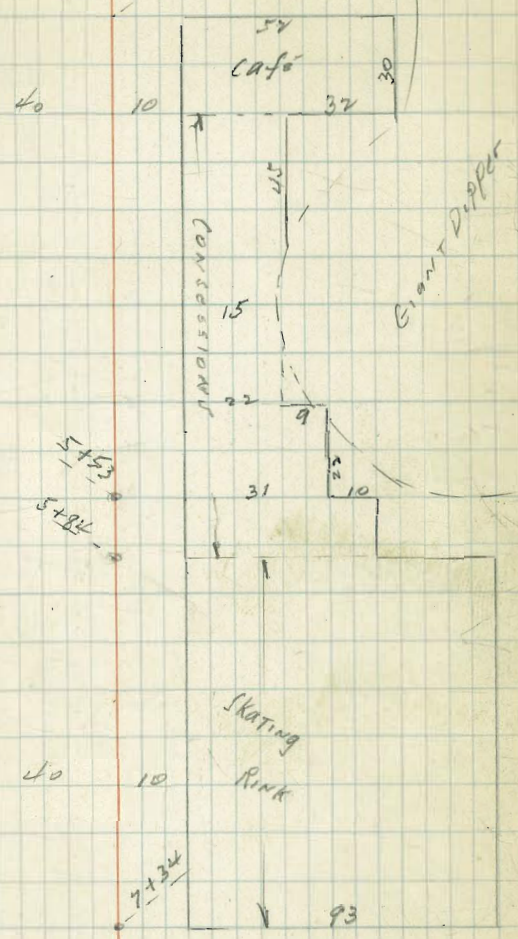
Moore
1-7-39 56



Bath House

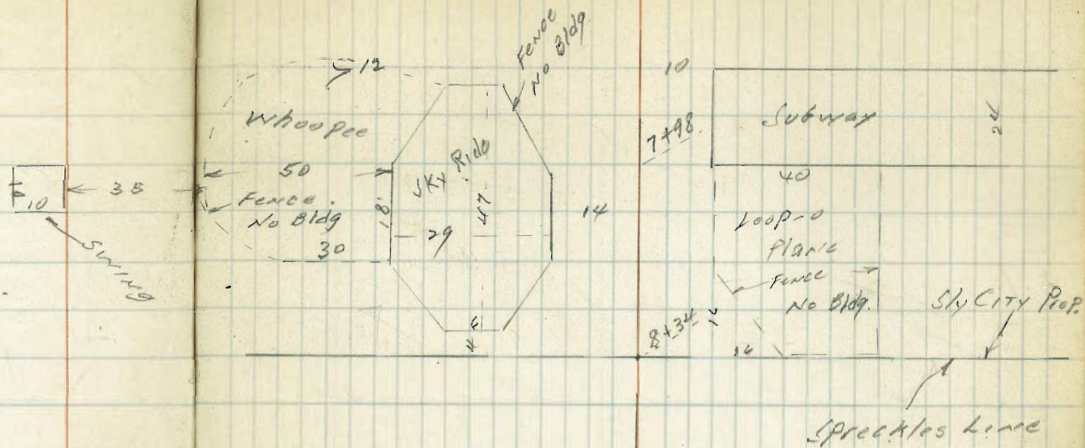


Baseline
3+24

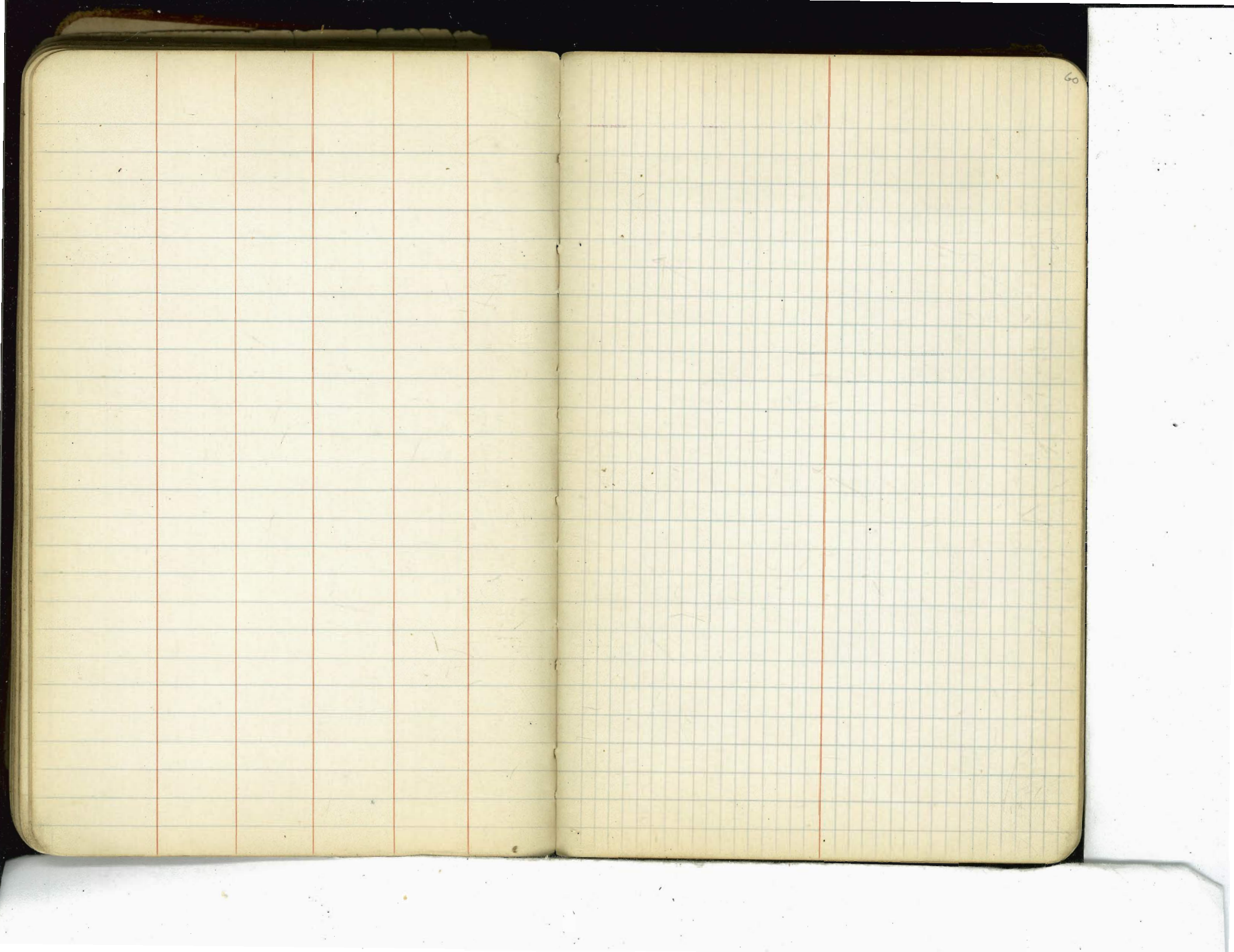


2+98

Subway to R.R.







Pipe Line to Sorrento from 215+00

Sta	+	X	-	Elev
	1.47	398.29		396.82
	5.13	395.53	7.87	390.44
0+00	12.95	402.21	6.27	389.46
1+00			7.9	394.31
2+00			0.1	404.1
			0.17 T.P.	404.04
3+00	11.93	413.97	4.1	409.9
4+00			1.4	411.6
	5.82	419.13	0.66 T.P.	413.31
3+94.6 P.O.F.			5.40	413.7
4.			5.30	413.8
5			5.30	413.83
6			5.6	413.5
+40			5.41 T.P.	413.72

B. Men Man. 224+56.5 (396.82 Elev.)

On top Air Valve 0+00 Sorrento line
215+00 Cement Line

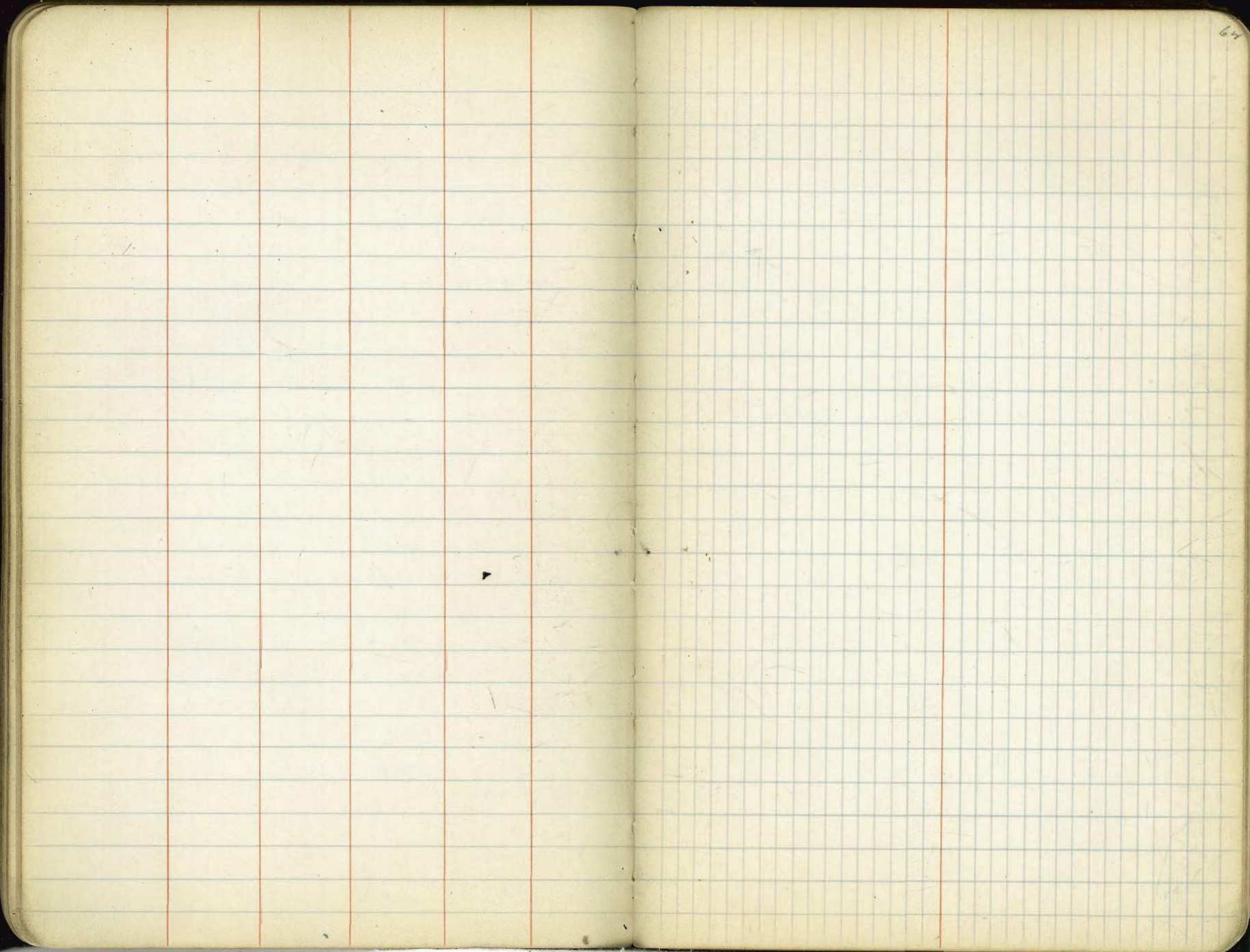
106' RT of F.S. Reservoir
original ground Elev. at 0+00 1.9
below T.P.

389.9
12.95
402.81
1.17
402.68
11.93
414.61
0.66
413.95
5.82
419.77
5.30
414.47

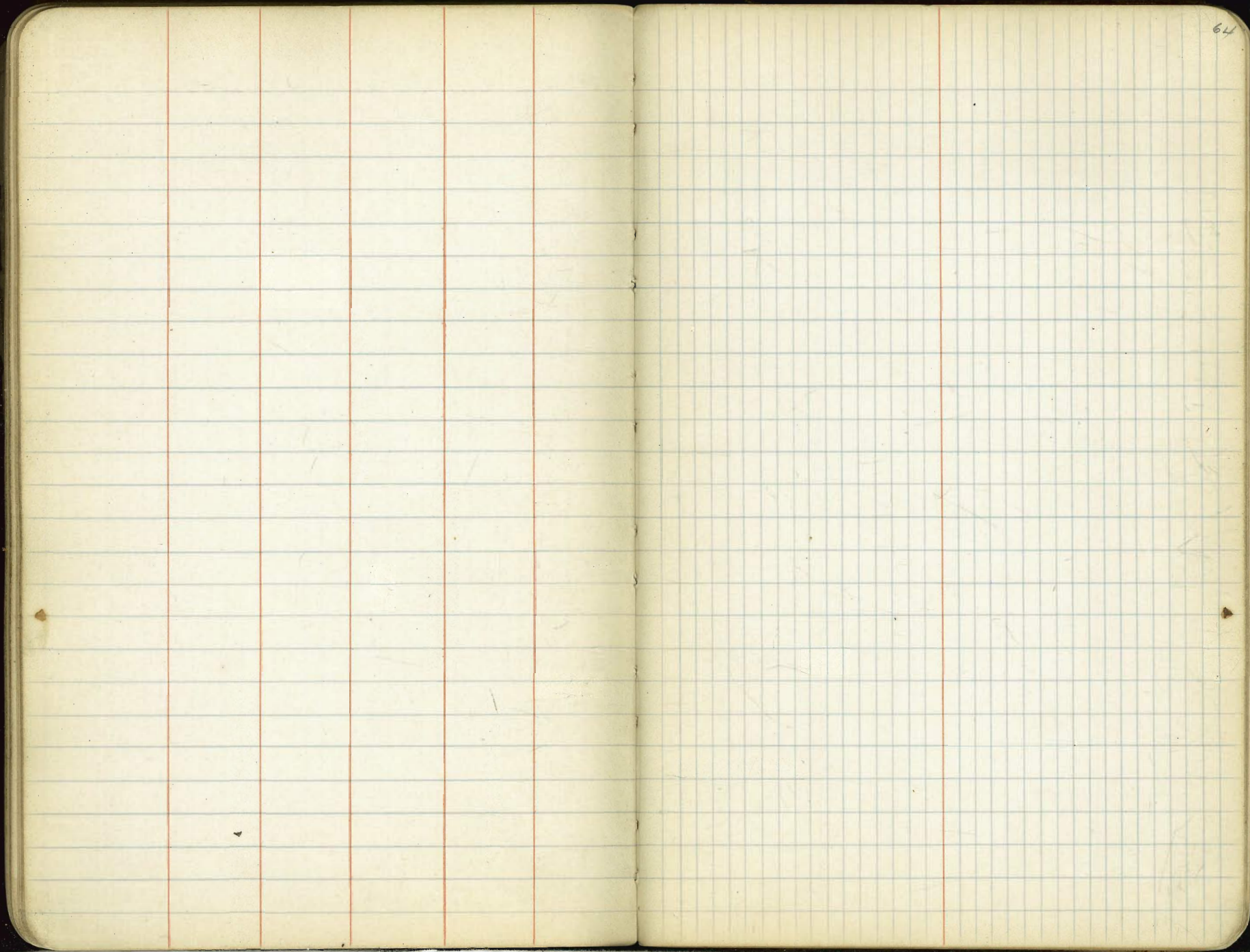
Δ 5+98.6

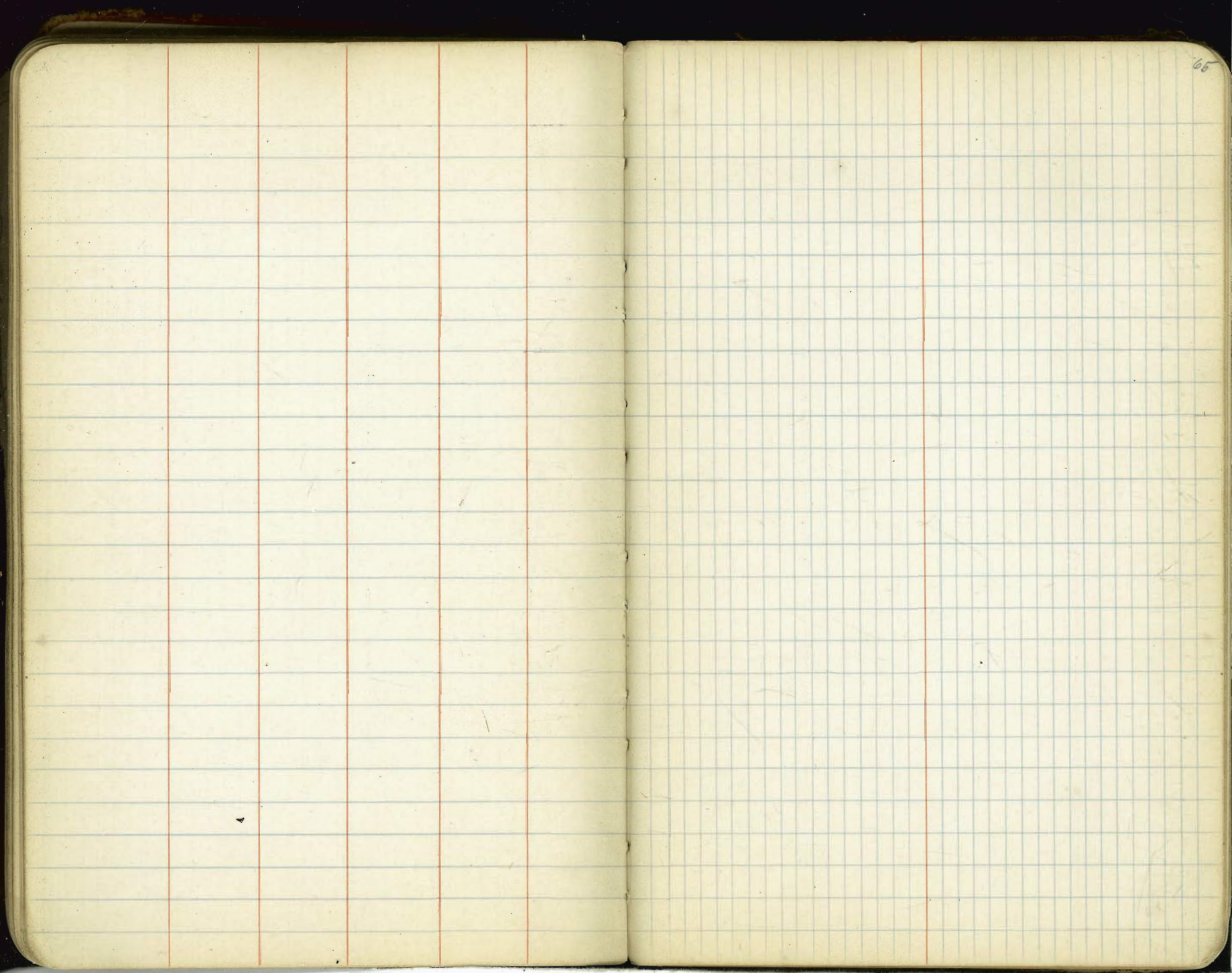
approx & Highway 6+40

Head of Canyon 11+00 approx
Foot of Canyon 76+00 "
P.C. near school 60+60
Mid Point Curve 61+60
E.C. near fence 62+60
opposite & Bldg Ser. School 64+50
N side Sorrento Road 65+47
3' east of east edge line

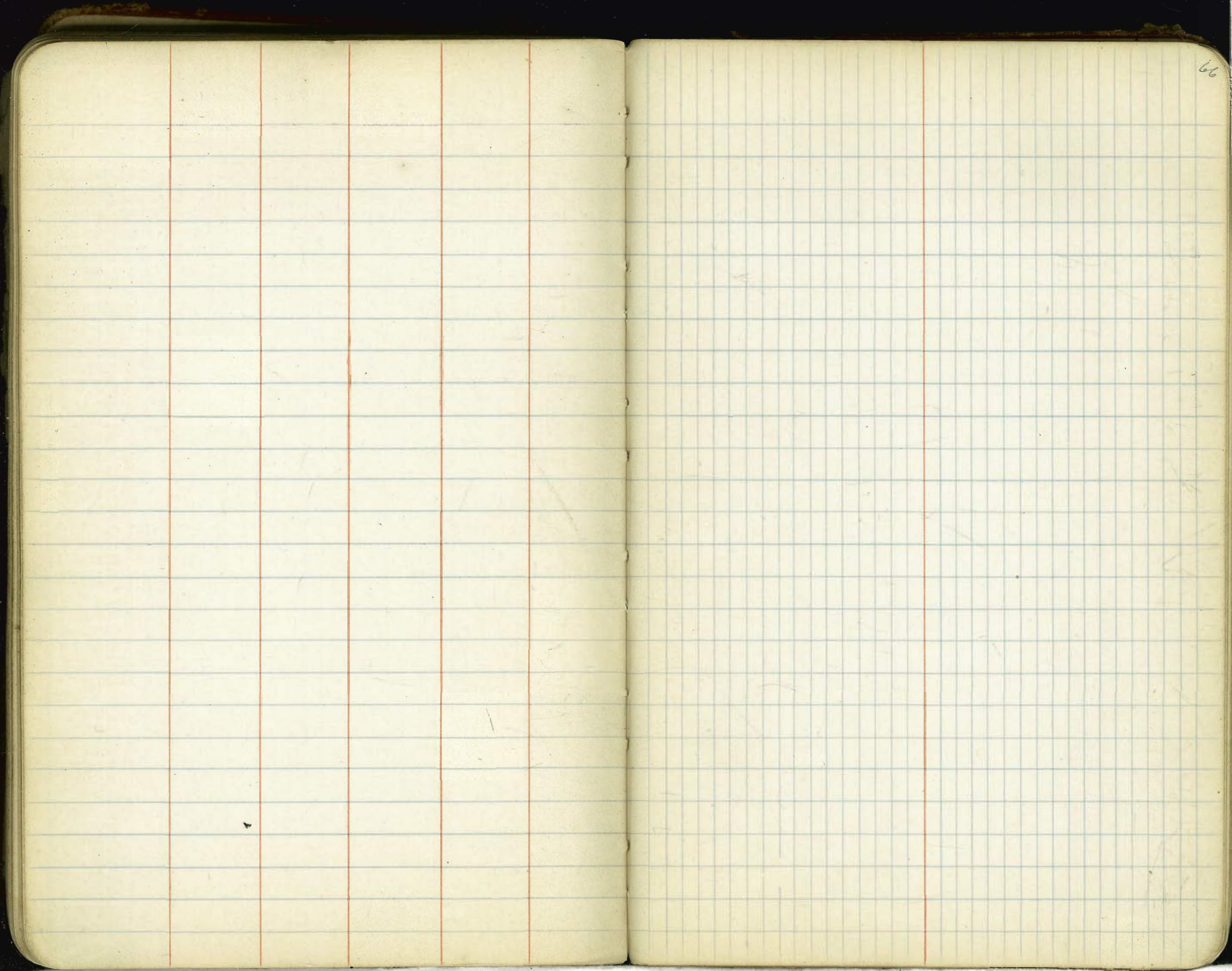


The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. Each page has a red vertical margin line on the left side. The notebook is bound in the center, and the pages are slightly aged. The number '63' is written in the top right corner of the right page.





65

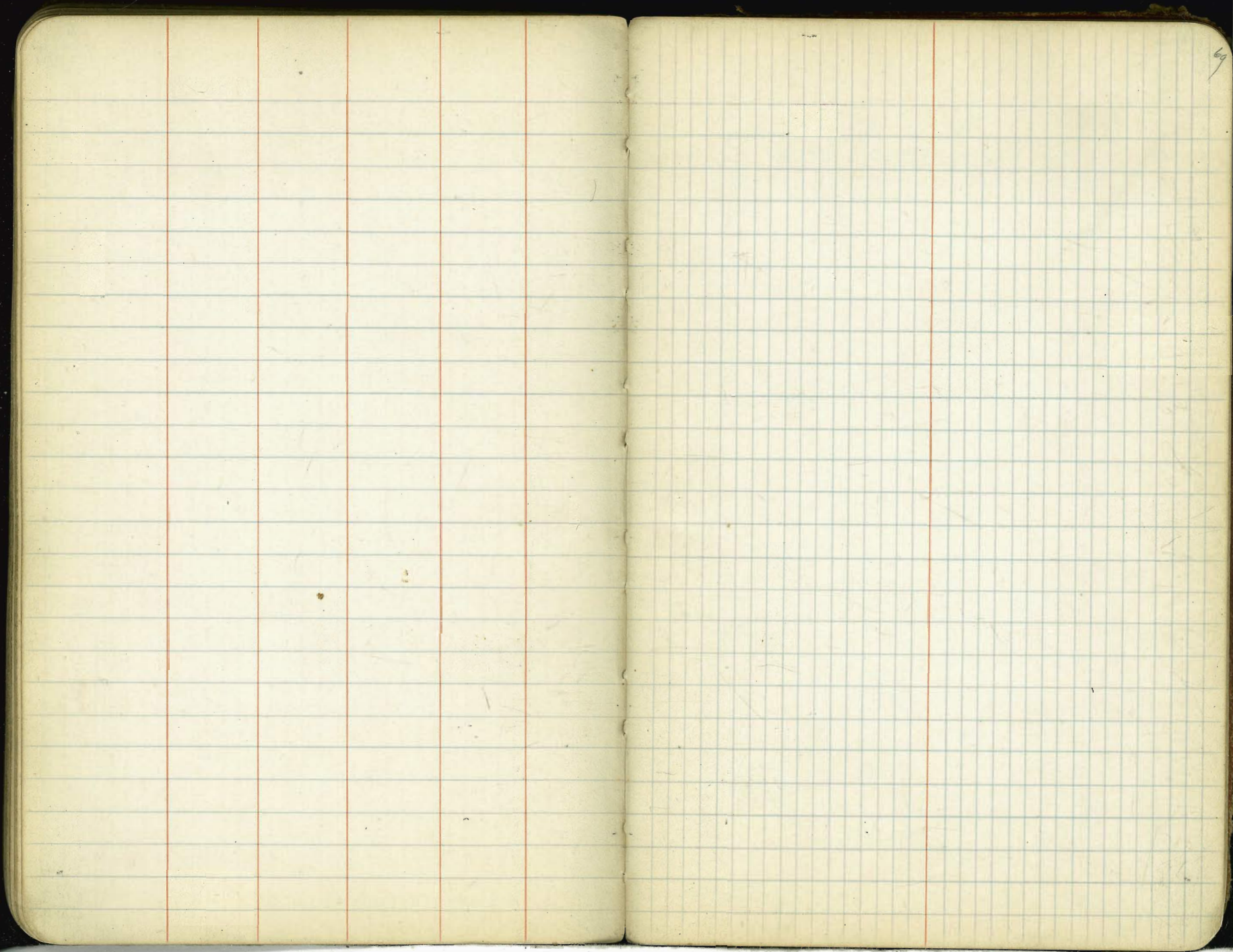


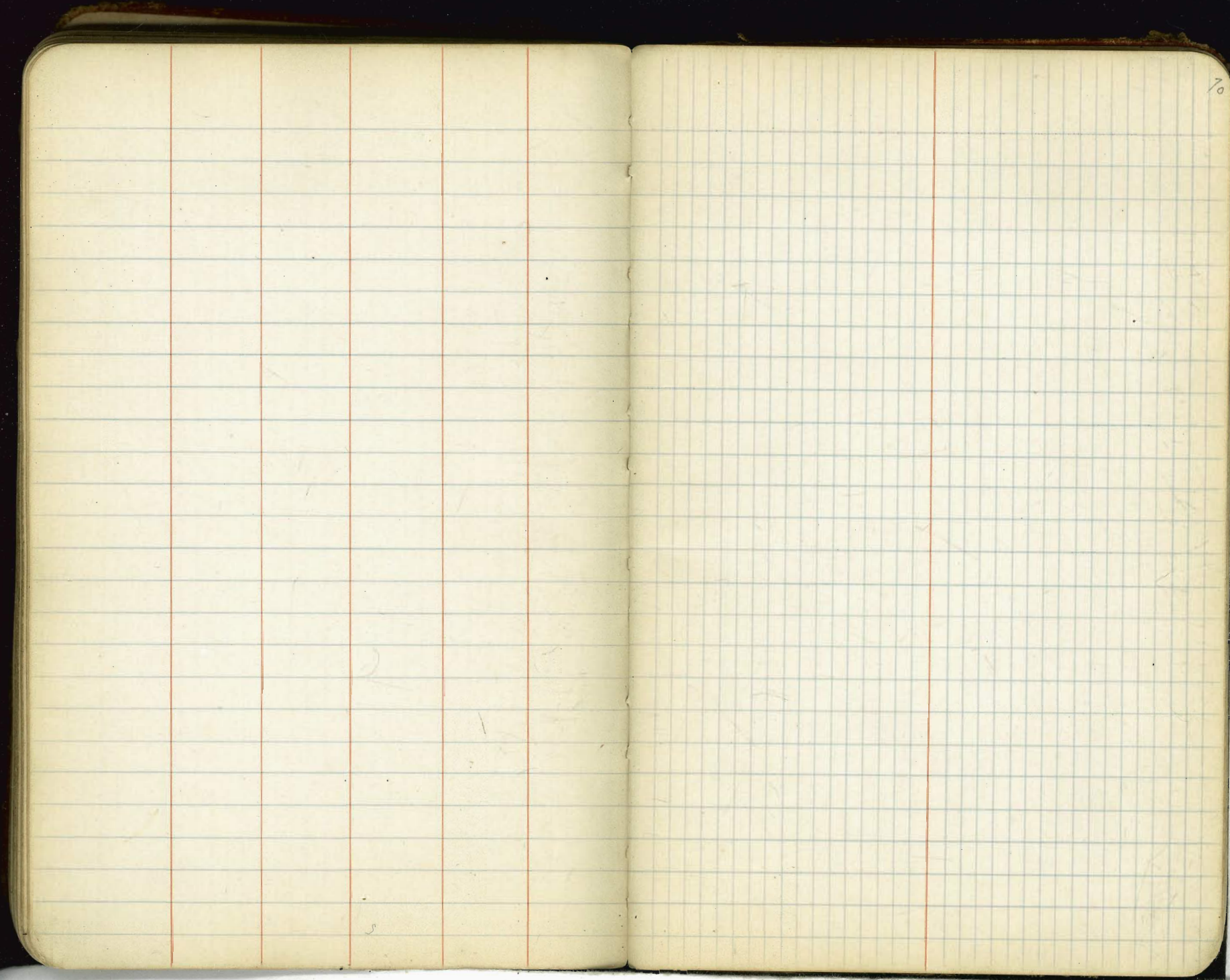
66



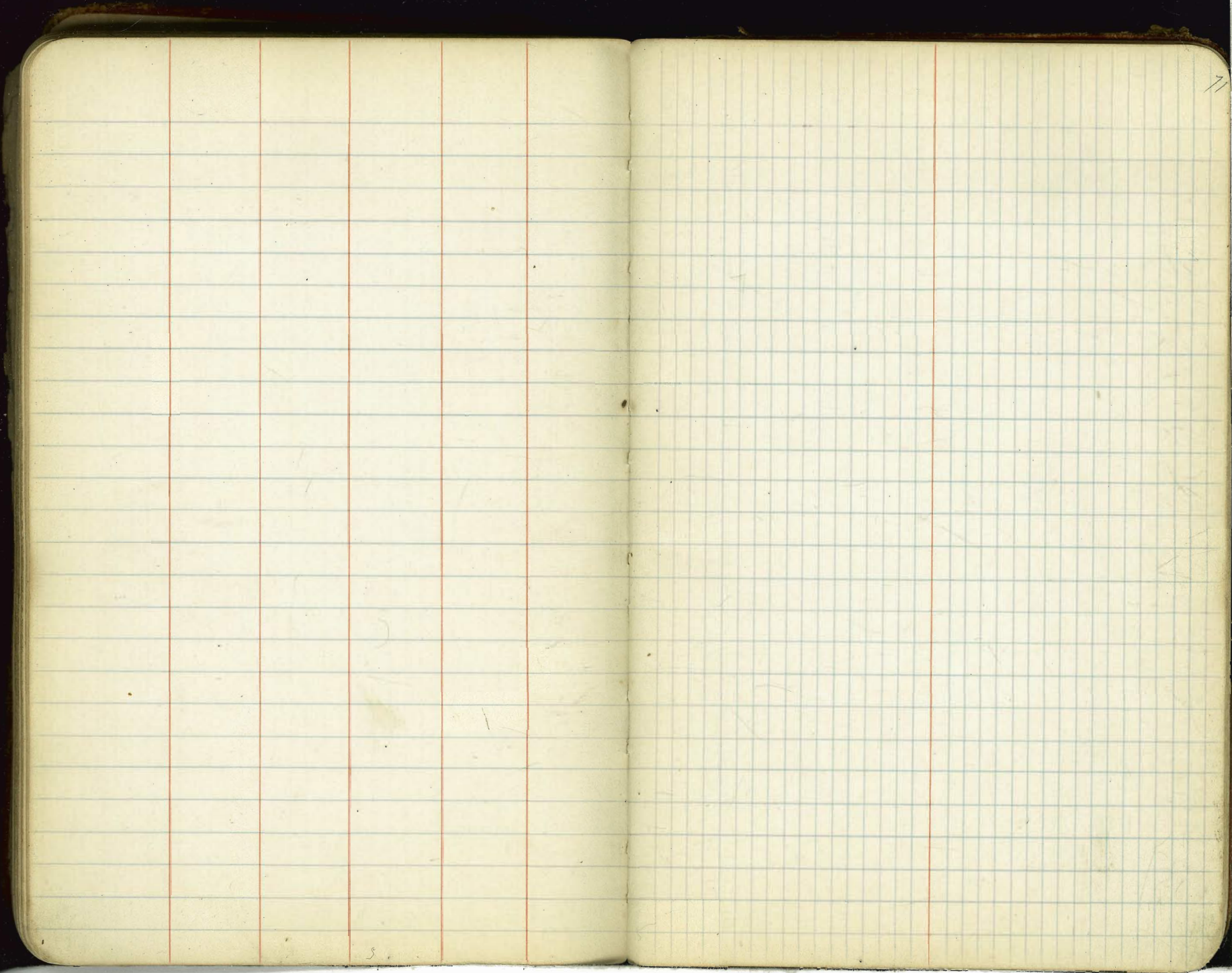
67

The image shows an open notebook with two facing pages. Both pages are cream-colored and feature light blue horizontal ruling. The left page is divided into four columns by three vertical red lines. The right page is divided into two columns by one vertical red line. The notebook is lying flat on a white surface, and the pages are completely blank.





70



14+50	x	58°41'30" RT
13+75	y	43°09'30" RT
12+75	x	28°09'30" RT
9+10.51	x	8°17'30" RT
8+00	x	14°47' RT
6+47°	x	19°15'30" LT
5+78°	x	14°04' LT
4+49	x	45°31'30" RT
3+25	x	40°25'30" RT
1+90	x	45°07'30" LT
1+00	x	84°47'30" RT
0+00	x	39°38'41" RT

100°
90°
135°
124°
129°
69°
153°
110.51
364.49
100
75
50

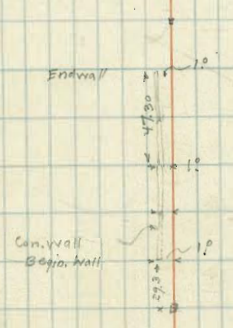
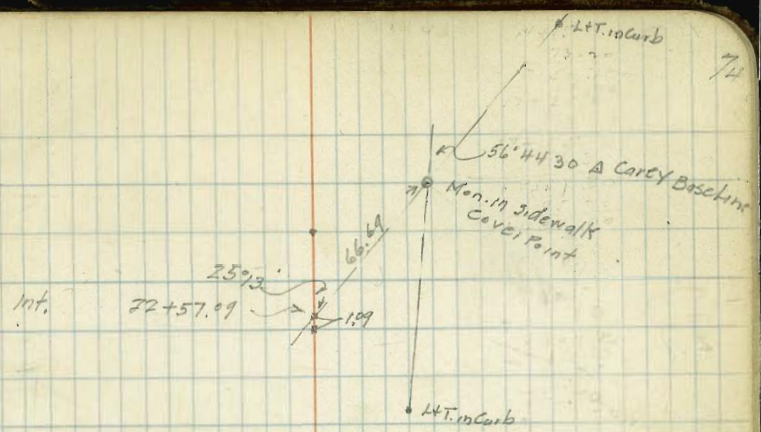
140.48'

Found
TACKIN 2" x 2" Hob

Transit at N. E. con. Coast Blvd.
and Ocean St. B.S. on Ocean St

24+50	31° 33' 30" RT
22+92	10° 28' 30" RT
22+56	62° 13' 30" RT
21+80	17° 01' 30" LT
20+80	29° 29' LT
20+10	14° 58' LT
19+37.0	34° 04' RT
18+41.30	47° 01' LT
17+65	41° 57' RT
17+38.0	62° 53' LT
15+58.2°	67° 30' LT
14+85	37° 23' RT

35°
 23.20
 179.8
 27
 76.30
 95.70
 73
 70
 100
 76
 36
 158



This course is along railing
of 34th House Promenade

28+07	X	66°11' Rt to old Curb.
	X	
27+85	X	25°49' Lt
	X	
27+53	X	60°11'30" Lt
	X	
27+22	X	21°25' Lt
	X	
26+87	X	15°34'30" RL
	X	
26+42.0	X	18°01'30" Lt
	X	
25+18.43	X	192° P.of.

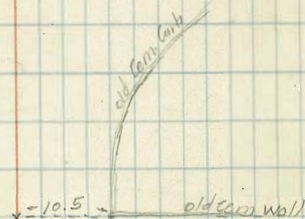
68.43
123.57
172.00

24.10
26.42
192

25+18.43
90.00
38.17
16+42.00

25

26+67
35
27+22



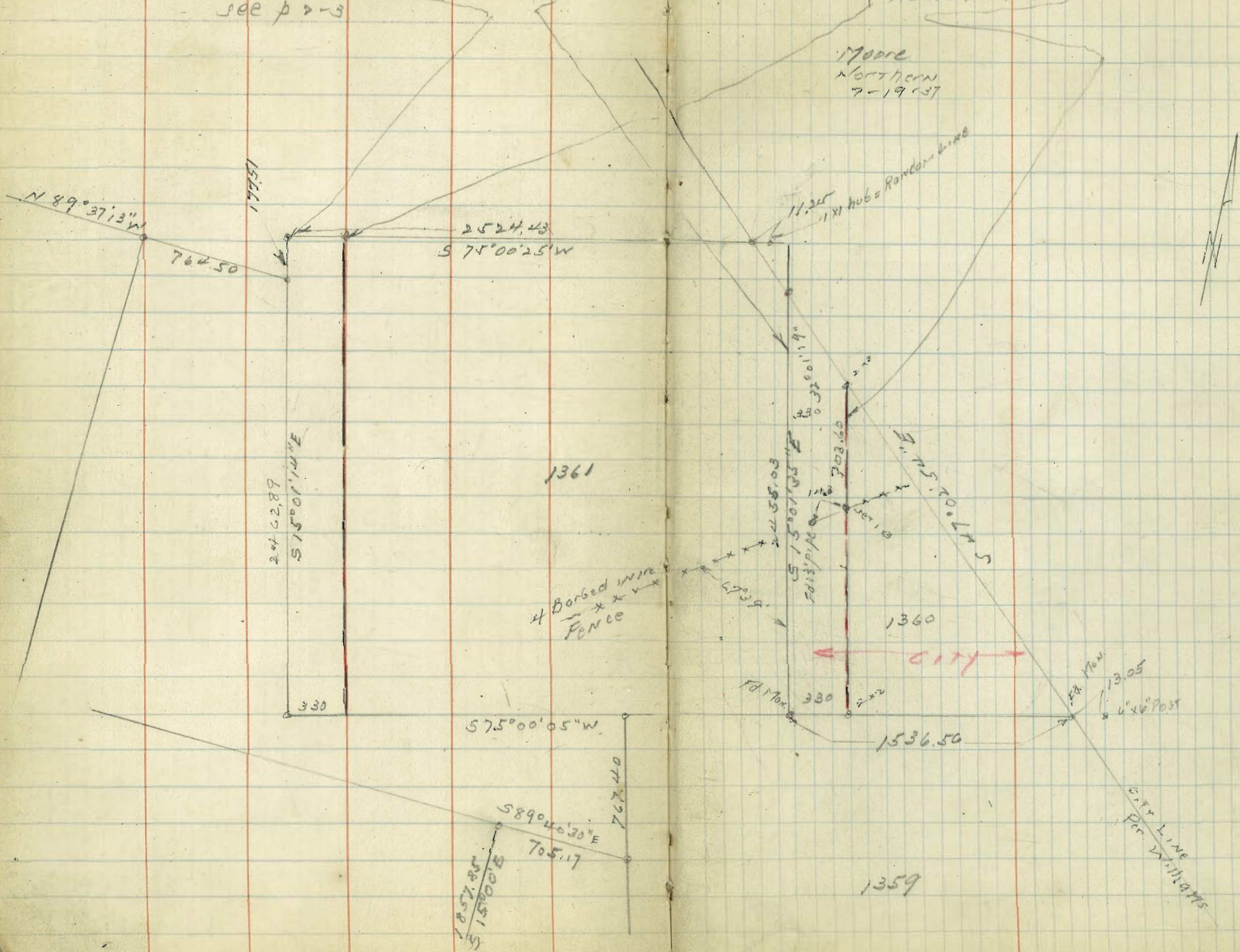
Survey of 1360 by J.W. Williams
 according to Pasco Map
 about 1919

see p 2-3

Survey of 1360
 according to
 Hesse Map

Indexed
 C.S.K.

76



$$0.8226 = 9,915,887$$

$$1387.79 = 31460023$$

$$\frac{6,774,5864}{2,741,1595} \text{ } 0^{\circ} 02' 30''$$

$$551.01 = 7,515,7459 \text{ } .32790$$

$$\frac{1,1726}{.35} = 8226$$

$$\frac{1.35}{1.68} = 5 + 58.01$$

Tobie Moved North.

$$\frac{551.01}{1.17} = 557.20$$

$$\frac{309045}{901415} = 309045$$

$$\frac{552.10}{79.46} = 6.95$$

$$\frac{1382.29}{652.16} = 2.12$$

	E	N		
$S 27^{\circ} 15' 45'' E$	427.87		370.33	196.00
$N 89^{\circ} 40' 03'' W$	879.47	4.81		879.46
$N 59^{\circ} 25' 40'' E$	10.06	5.12		8.66
$N 59^{\circ} 19' 40'' E$	726.02	370.36		624.45
	380.29	380.33	829.11	829.46

containing 3.7 acres

$$\frac{8200.095}{81440.09} = 180.57$$

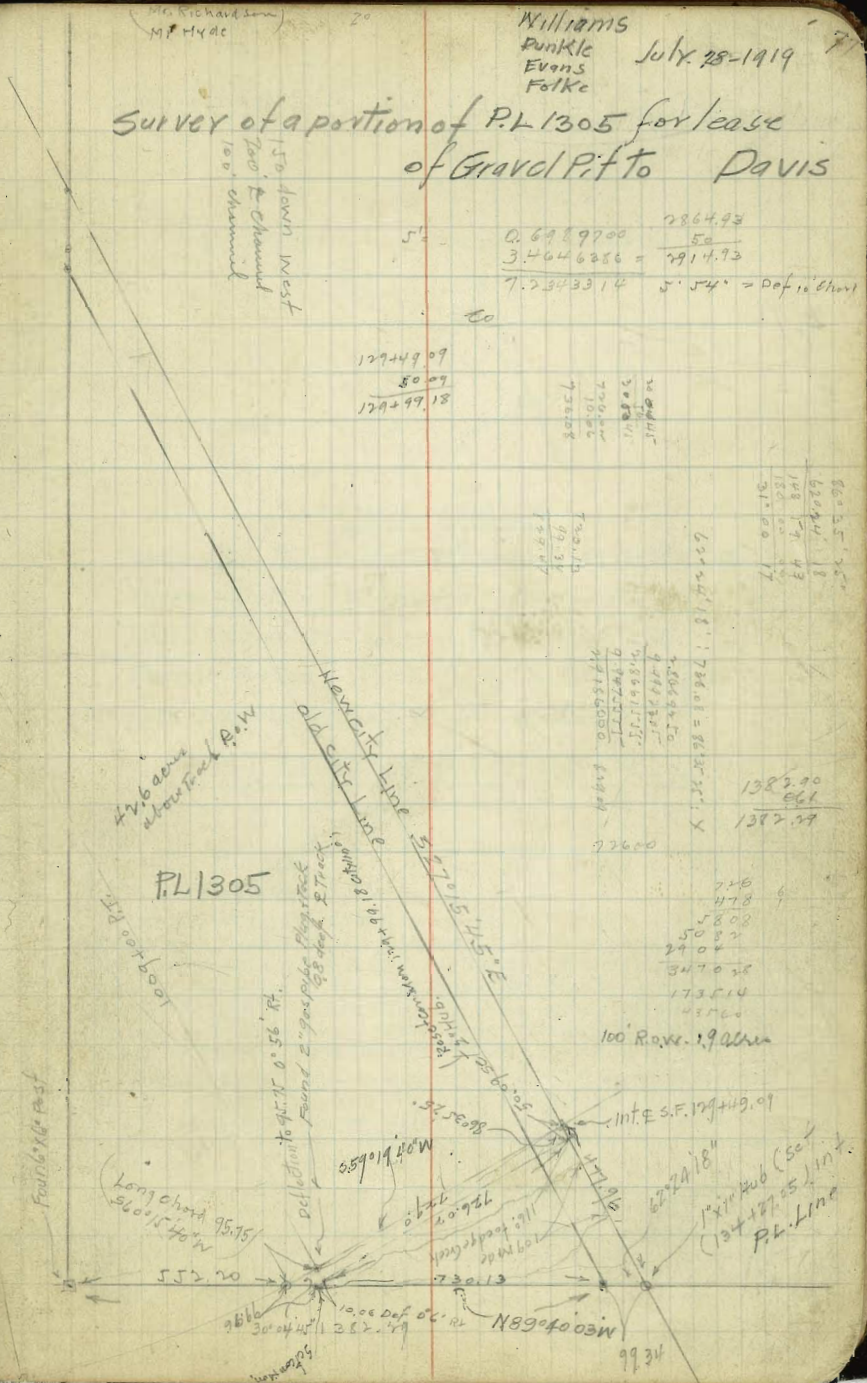
$$\frac{3064.06}{14.55.88}$$

$$\frac{20196.7}{866} = 23319.6$$

Williams
Dunkle
Evans
Folke

July 28-1919

Survey of a portion of P.L. 1305 for lease
of Gravel Pit to Davis



$$\frac{2864.93}{50} = 57.2986$$

$$\frac{3464.6286}{7914.73} = 0.4377$$

$$\frac{7.2343314}{5.54} = 1.3058$$

$$\frac{12749.09}{800} = 15.9476$$

$$\frac{73028}{7025} = 10.408$$

$$\frac{73017}{92.38} = 791.46$$

$$\frac{9484.80}{9484.80} = 1$$

$$\frac{9484.80}{9484.80} = 1$$

$$\frac{9484.80}{9484.80} = 1$$

$$\frac{62844}{91.55} = 687.55$$

$$\frac{1382.90}{661} = 2.0921$$

$$\frac{173.14}{45760} = 0.0038$$

100 R.R. 1920

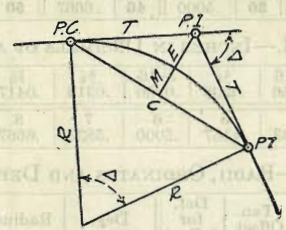
INT. E.S.F. 179149.99

1272018
1271705
PL Line

2° 30'	275.6	1017 599925	19534	3
	999	1423	231	6
	5804	199950	9534	
	24804	399900	298602	
		99975	199068	
	2753244	142264425	22992354	

DIETZGEN'S RAILROAD CURVE AND REDUCTION TABLES

Copyright, 1914, by Eugene Dietzgen Co., New York City



CURVE FORMULAS

- Radius= $R = \frac{50}{\sin \frac{D}{2}}$ (1) Degree of Curve= D and $\sin \frac{D}{2} = \frac{50}{R}$ (2)
- Tangent= $T = R \tan \frac{\Delta}{2}$ (3) Length of Curve= $L = 100 \frac{\Delta}{D}$ (4)
- Middle ordinate= $M = R(1 - \cos \frac{\Delta}{2})$ (5) $= R \text{vers} \frac{\Delta}{2}$ (6)
- External= $E = T \tan \frac{\Delta}{4}$ (7) $= R \div \cos \frac{\Delta}{2} - R$ (8) $= R \text{exsec} \frac{\Delta}{2}$ (9)
- Long Chord= $C = 2 R \sin \frac{\Delta}{2}$ (10) $\Delta =$ Central Angle

EXPLANATION AND USE OF TABLES

Stations.—Given P. I.—Sta. 161+60.35 to find Sta. of P. C. and P. T. $\Delta = 62^\circ 10'$ $D = 8^\circ 20'$. From Table IV for 1° curve $T = 3454.1$ and $\div 8\frac{2}{3} = 414.49$ ft. From Table V correction—.36 or $T = 414.85$ ft. P. C.—Sta. P.I.— $T = 157 + 45.50$. Also from (4) $L = 746.00$ and P. T.—Sta. P. C. + $L = 164 + 91.50$.

Offsets.—Tangent offsets vary (approximately) directly with D and with square of the distance. Thus tangent offset for Sta. 158 on above curve is 2.16 ft. found as follows. From Table III tangent offset for 100 ft.—7.27 ft. Distance—158—Sta. P. C.—54.50, hence offset— $7.27 (54.50 \div 100)^2 = 2.16$ ft. Also square of any distance divided by twice the radius equals (approximately) the distance from tangent to curve. Thus $(54.50)^2 \div (2 \times 688.26) = 2.16$ ft.

Deflections.—Deflection angle— $\frac{1}{2} D$ for 100 ft., $\frac{1}{4} D$ for 50 ft., etc. For c ft.—(in minutes) $.3 \times C \times D^\circ$ or—defl. for 1 ft. from Table III $\times C$. For Sta. 158 of above curve— $.3 \times 54.5 \times 8\frac{2}{3} = 136.2'$ or $2^\circ 16.2'$, or— $2.50 \times 54.5 = 136.2'$ from Table III. For Sta. 159 deflection angle— $2^\circ 16.2' + 8^\circ 20' \div 2 = 6^\circ 26.2'$, etc.

Externals.—May be found in similar manner to tangents. Thus E for curve above is 115.37 For from Table IV for 1° curve $E = 960.6$ for $8^\circ 20' = 960.6 \div 8\frac{2}{3} = 115.27$ and from Table V correction—.10 or $E = 115.37$ Or suppose $\Delta = 32^\circ$ and E is measured and found to be 42 ft. What is D ? From Table IV $E = 230.9$ and $\div 42 = 5.5$ or $D = 5^\circ 30'$.

DISTANCES FROM CENTER OF ROADWAY FOR
CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.5	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.