

1072

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LEVEL BOOK

373

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# KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

MICROFILMED

## Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

" Copyright, 1895, by Keuffel & Esser Co."

	.1	.2	.3	.4	.5	.6	.7	.8	.9		
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

Levels Catalina Blvd. P.L. Called  $\Phi$  in Level notes

1/8 Dunkle  
120 C. Moore  
B. Moore

232.71

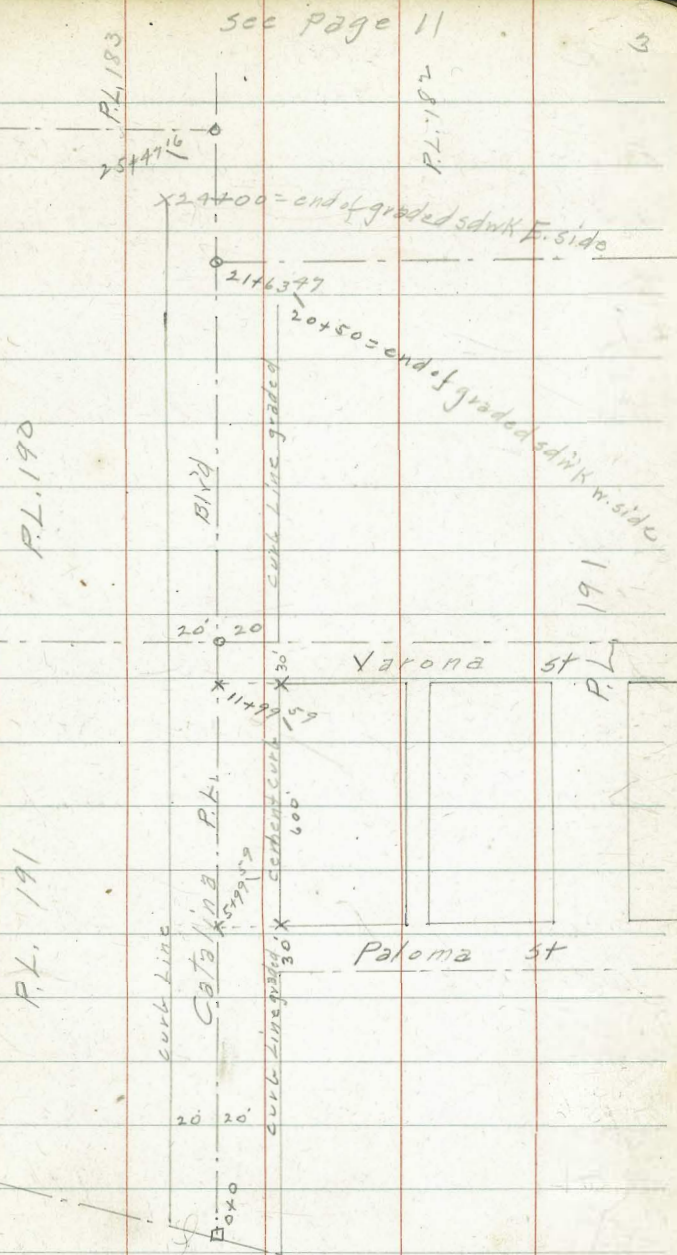
1450

B.M. N.W. R.R. Sp. N. Chatsworth	2	Catalina	209.00				
B.M.	12.26	221.26		E crk		6.7	226.0
T.P.	12.43	232.71	0.98	220.28	+5	6.7	226.0
		0+0			$\Phi$	6.0	226.7
W $\Phi$ curb line		11.2	221.5		+15	6.0	226.7
+5		12.2	220.5		W crk	5.3	227.4
$\Phi$		12.4	220.3			2+0	
+15		12.6	220.1		W crk	3.7	229.0
F $\Phi$ curb line		12.4	220.2		+5	4.5	228.2
		0+50			$\Phi$	4.7	228.0
E crk		10.0	222.7		+15	5.7	227.7
+5		10.1	222.6		E crk	5.3	227.4
$\Phi$		9.5	223.2			2+50	
+15		9.4	223.3		E crk	4.3	228.4
W crk		8.7	224.0		+5	4.7	228.0
		1+0			$\Phi$	3.6	229.1
W crk		7.0	225.7		+15	3.4	229.3
+5		7.6	225.1		W crk	2.7	230.0
$\Phi$		7.6	225.1				
+15		8.5	224.2				
E crk		8.0	224.7				

		232.71				240.28			
		3+50				4+50			2
W crk			1.6	231.1				7.9	232.4
+5			2.4	230.3				8.3	232.0
φ			2.4	230.3				7.4	232.9
+15			3.4	229.3				7.1	233.2
E. crk			3.0	229.7				6.1	234.2
		3+50				5+50			
E crk			1.8	230.9				5.7	234.6
+5			2.2	230.5				6.7	233.6
φ			1.3	231.4				6.9	233.4
+15			1.3	231.4				7.7	232.6
W crk			0.3	232.4				7.5	232.8
T. P.	8.70	240.28	1.13	231.58			5+50		
		4+50							
W crk			6.7	233.6				7.0	233.3
+5			7.7	232.6				7.3	233.0
φ			8.0	232.3				6.4	233.9
+15			8.9	231.4				6.2	234.1
E. crk			8.5	231.8				5.3	235.0

240.28  
5499<sup>59</sup> = S.L. Paloma

W. curb cement	4.86	235.42
+5	5.6	234.7
Φ	5.9	234.4
+15	7.0	233.3
E. curb	6.5	233.8
	6.750	
F. curb	5.5	234.8
+5	6.1	234.3
Φ	5.2	235.1
+15	5.2	235.1
W. curb	4.43	235.85
	7.40	
W. curb	3.44	236.84
+5	4.1	236.2
Φ	4.4	235.9
+15	5.2	235.1
E. curb	4.9	235.4



		240.25				250.58			4
		7450				8475			
E.C.V.L.			3.9	236.4	W.C.V.L.		10.20	240.38	
+5			4.2	236.1	+5		10.9	239.7	
♀			3.5	236.8	♀		11.0	239.6	
+15			3.3	237.0	+15		12.0	238.6	
W.C.V.L.			2.47	237.81	E.C.V.L.		11.5	239.1	
		840					940		
W.C.V.L.			1.30	238.98	E.C.V.L.		10.7	239.9	
+5			2.3	238.0	+5		11.4	239.2	
♀			2.3	239.0	♀		10.2	240.4	
+15			3.2	237.1	+15		10.3	240.3	
E.C.V.L.			2.6	237.7	W.C.V.L.		9.70	240.88	
		8450					9425		
E.C.V.L.			1.5	238.8	W.C.V.L.		9.00	241.58	
+5			2.2	238.1	+5		9.6	241.0	
♀			1.2	239.1	♀		9.5	241.1	
+15			1.1	239.2	+15		10.5	240.1	
W.C.V.L.			0.38	239.90	E.C.V.L.		10.0	240.6	
T.P.	10.69	250.58	0.39	239.89					

250.58  
9+50

250.58  
11+0

5

E. Crk	9.4	241.2
+5	9.7	240.9
Φ	8.9	241.7
+15	8.8	241.8
W. Crk	8.20	242.38

W. Crk	3.45	247.13
+5	4.4	246.2
Φ	4.3	246.3
+15	5.2	245.4
E. Crk	4.6	246.0

10+0

11+50

W. Crk	6.80	243.78
+5	7.6	243.0
Φ	7.4	243.2
+15	8.3	242.3
E. Crk	7.8	242.5

E. Crk	3.4	247.2
+5	4.1	246.7
Φ	2.9	247.7
+15	3.0	247.6
W. Crk	1.88	248.70

10+50

E. Crk	6.2	244.4
+5	6.6	244.0
Φ	5.9	244.7
+15	6.0	244.6
W. Crk	5.17	245.41

250.58				260.08			
11+99 N.L. Varona st				13+50			
W. curb	End of cement curb	0.42	250.16	E. curb		8.3	251.8
+5		1.7	248.9	+5		8.3	251.8
Φ		1.7	248.9	Φ		7.5	252.6
+15		2.5	247.8	+15		7.5	252.6
E. curb		2.2	248.4	W. curb		6.7	253.4
T.P.	9.92	260.08	0.42	250.16		14+0	
		12+50			W. curb	5.7	254.4
E. curb		10.4	249.7	+5		6.5	253.6
+5		10.3	249.3	Φ		6.4	253.7
Φ		9.9	250.2	+15		7.2	252.9
+15		9.6	250.5	E. curb		6.9	253.2
W. curb		9.2	250.9			14+50	
		13+0		E. curb		5.8	254.3
W. curb		7.6	252.5	+5		6.2	253.9
+5		8.5	251.6	Φ		5.4	254.7
Φ		8.6	251.5	+15		5.5	254.6
+15		9.7	250.4	W. curb		4.6	255.5
E. curb		9.3	250.8				



260.08

15+0

W.C.V.B.

4.0

256.1

+5

4.7

255.4

Φ

4.6

255.5

+15

5.4

254.7

E.C.V.B.

4.9

255.2

15+50

E.C.V.B.

4.2

255.9

+5

4.6

255.5

Φ

3.8

256.3

+15

3.7

256.4

W.C.V.B.

2.8

257.3

16+0

W.C.V.B.

2.1

258.0

+5

2.8

257.3

Φ

2.9

257.2

+15

3.8

256.3

E.C.V.B.

3.4

256.7

260.08

16+50

7

E.C.V.B.

2.6

257.5

+5

2.9

257.2

Φ

2.1

258.0

+15

2.1

258.0

W.C.V.B.

1.7

258.4

17+0

W.C.V.B.

0.7

259.4

+5

1.3

258.8

Φ

1.4

258.7

+15

2.2

257.9

E.C.V.B.

2.0

258.1

T.P.

4.28

263.54

0.82

259.26

17+50

E.C.V.B.

4.7

258.8

+5

5.1

258.4

Φ

4.3

259.2

+15

4.4

259.1

W.C.V.B.

3.7

259.8

263.59  
18+0

W Crk	3.2	260.3
+5	4.0	259.5
φ	3.9	259.6
+15	4.6	258.9
E Crk	4.5	258.8

18+50

E Crk	4.2	259.3
+5	4.5	259.0
φ	4.0	259.5
+15	4.0	259.5
W Crk	3.3	260.2

19+0

W Crk	3.6	259.9
+5	4.2	259.3
φ	4.1	259.4
+15	4.9	258.6
E Crk = end of graded curb on West	4.4	259.1

263.59  
19+50

E Crk	4.7	258.8
+5	5.2	258.3
φ	4.5	259.0
+15	4.5	259.0
W Crk	4.0	259.5

20+0

W Crk	4.4	259.1
+5	5.0	258.5
φ	4.8	258.7
+15	5.5	258.0
E Crk	4.9	258.6

20+50

E Crk	4.9	258.6
+5	5.6	257.9
φ	5.0	258.5
+15	5.2	258.3
W Crk	4.7	258.8

263.59

21+0

W	4.8	258.7
+15=φ	5.1	258.4
+15	6.1	257.4
E.C.V.L	5.3	258.2

21+63<sup>97</sup> P.L. C.V.L

E.C.V.L	5.4	258.1
+5	6.1	257.4
φ	5.3	258.2
+15	5.2	258.3

22+0

W	6.0	257.5
+15=φ	5.6	257.9
+15	6.1	257.4
E.C.V.L	5.5	258.0

22+50

E.C.V.L	5.1	258.4
+15	6.1	257.4
φ	5.6	257.9
+15	6.0	257.5

263.54

23+0

W	6.0	257.54
+15=φ	5.7	
+15	6.1	
E.C.V.L	5.2	258.3

23+50

E.C.V.L	5.0	258.5
+5	5.8	
φ	5.4	
+15	5.8	257.7

24+0 - end graded walk on east side

W	5.3	258.2
+15=φ	5.1	
+15	5.3	
E.C.V.L	4.	259.5

+50

E	4.5	259.0
+15	4.1	
φ	4.4	259.1
W		

} 30'



252.13  
30+0

W 4.0

☿ 3.5

E 3.7

+50

E 4.7

☿ 4.6

W 5.1

31+0

W 6.2

☿ 5.7

E 5.8

+50

E 7.1

☿ 6.9

W 7.2

32+0

W 8.1

☿ 7.8

E 8.0

Note - Levels taken on P.L. 8 15' each side 11

N.L. U.S. Military Reservation

P.L. 102

Mon 80+93.8

Mon 71+56.58

P.L. 66

P.L. 104

Mon 61+74.90

P.L. 103

P.L. 143

Mon 56+61.31

P.L. 144

P.L. 181

Mon 41+43.1

P.L. 145

P.L. 183

Mon 34+82.76

P.L. 182

N.L. Warnerville

BLVD  
Catalina

252.13

32+25

F	8.6
♀	5.3
W	8.3

32+50

W	8.1
♀	8.0
F	8.5

33+0

F	8.1
♀	7.8
W	8.1

+50

W	7.7
♀	7.6
F	7.7

34+0

F	6.7
♀	6.8
W	7.1

252.13

34+50

W	5.6
♀	5.4
F	5.5

34+85<sup>76</sup> = P.L. COL

F	4.5
♀	4.3
W	4.5

T.P. 11.64 260.32 3.45 248.68

35+0

W	12.5
♀	12.1
F	12.3

+50

F	10.3
♀	10.4
W	10.7

36+0

W	9.1
♀	8.6
F	8.6

12

260.32  
36+50

E 6.7  
Φ 6.5  
W 7.1

37+0

W 4.9  
Φ 4.5  
E 4.5

+50

E 2.9  
Φ 2.9  
W 3.5

38+0

W 2.1  
Φ 1.4  
E 1.5

+50

E 0.2  
Φ 0.3  
W 0.8

T.P. 7.51 267.52 0.31 260.01

267.52

38+81 = Φ entrance to Theosophical school

.35' W of RL 7.9  
15' " " " 7.2

Φ 6.7  
E 6.7

39+0

E 6.4  
Φ 6.4  
W 6.9

+50

W 6.2  
Φ 5.6  
E 5.5

40+0

E 4.6  
Φ 4.7  
W 5.4

40+50

W 4.5  
Φ 4.0  
E 4.0

267.52

41+0

E 3.5

Φ 3.2

W 3.5

41493<sup>11</sup> = N.L. of Warner Villa Tract

W 3.1

Φ 2.6

E 2.3

T.P. 12.21 277.01 2.72 264.80

42+0

E 11.6

Φ 12.1

W 12.5

+50

W 11.9

Φ 11.4

E 11.4

43+0

E 10.5

Φ 10.4

W 10.8

277.01

43+50

W 9.7

Φ 9.4

E 9.4

44+0

E 8.1

Φ 8.2

W 8.6

+50

W 7.3

Φ 7.0

E 6.6

45+0

E 5.2

Φ 5.1

W 5.6

+50

W 3.8

Φ 3.4

E 3.5

14



277.01

46+0

E

6.7

Φ

11.7

W

2.2

+50

W

0.5

Φ

0.1

E

0.1

T.P.

12.71

289.54

0.18

276.83

47+0

E

10.9

Φ

10.7

W

11.2

+50

W

9.3

Φ

8.9

E

9.0

48+0

E

7.1

Φ

6.9

W

7.3

289.54

48+50

W

5.0

Φ

4.7

E

5.0

49+0

E

2.8

Φ

2.5

W

2.6

+50

W

0.3

Φ

0.3

E

0.7

T.P.

12.12

301.29

0.37

289.17

50+0

E

10.1

Φ

9.9

W

10.0

+50

W

8.3

Φ

8.1

E

8.4

301.29  
51+0

E 6.5

Φ 6.4

W 6.6

+50

W 5.3

Φ 5.0

E 5.2

52+0

E 4.4

Φ 4.2

W 4.5

+50

W 4.0

Φ 3.8

E 3.9

53+0

E 3.8

Φ 3.5

W 3.6

16

301.29  
53+50

W 3.5

Φ 3.4

E 3.5

54+0

E 3.5

Φ 3.2

W 3.6

+50

W 3.5

Φ 3.2

E 3.3

55+0

E 3.2

Φ 3.0

W 3.4

55+50

W 3.3

Φ 2.9

E 3.1

T.P.

8.04

306.43

2.90

298.39

306.43

.5640

E 7.9

Φ 8.1

W 8.4

56+61<sup>31</sup> = S.L. Warner Villa Tract

W 8.2

Φ 7.9

E 7.7

57+0

E 7.7

Φ 7.7

W 7.9

+50

W 7.7

Φ 7.5

E 7.5

58+0

E 7.2

Φ 7.3

W 7.3

17

306.43

58+50

W 6.7

Φ 6.7

E 7.0

59+0

E 6.0

Φ 6.1

W 6.2

+50

W 5.3

Φ 5.2

E 5.1

60+0

E 4.2

Φ 4.0

W 4.2

+50

W 3.4

Φ 3.2

E 3.2

306.43

61+0

E

2.1

Φ

2.1

W

2.2

+50

W

1.0

Φ

1.0

E

1.2

61+74<sup>90</sup>

← S.L.P.L. 143 Mon. cov

E

0.5

Φ

0.4

W

0.4

T.P.

12.52

318.64

0.61

305.82

62+0

W

12.0

Φ

11.9

E

12.0

318.64

62+50

E

10.5

Φ

10.3

W

10.4

63+0

W

8.6

Φ

8.4

E

8.6

+50

E

6.6

Φ

6.5

W

6.6

64+0

W

4.5

Φ

4.3

E

4.3

+50

E

1.8

Φ

1.9

W

2.2

T.P.

12.46

330.52

0.58

318.06

18

330.52

65+0

W

11.5

Φ

11.1

E

11.3

+50

E

8.7

Φ

8.3

W

8.5

66+0

W

5.5

Φ

5.1

E

5.3

+50

E

2.7

Φ

2.4

W

2.7

T.P.

12.53

342.53

0.52

330.00

67+0

W

11.7

Φ

11.3

E

11.6

19

342.53

67+50

E

8.7

Φ

8.4

W

8.6

68+0

W

5.3

Φ

5.0

E

5.3

+50

E

2.2

Φ

2.0

W

2.1

T.P.

12.65

355.06

0.12

342.41

69+0

W

11.8

Φ

11.6

E

11.8

+50

E

8.6

Φ

8.5

W

8.7

355.06

70+0

W 5.8

φ 5.6

E 5.9

+50

E 2.9

φ 2.6

W 2.7

T.P. 12.20 367.14 0.12 354.94

71+0

W 12.0

φ 11.8

E 12.3

71+56<sup>58</sup> = S.L. P.L. 104

E 9.6

φ 9.4

W 9.2

72+0

W 7.1

φ 7.0

E 7.2

367.14

72+50

E 4.9

φ 4.7

W 4.5

73+0

W 2.4

φ 2.5

E 2.7

+50

E 1.1

φ 0.9

W 0.9

T.P. 10.07 376.81 0.40 366.74

74+0

W 9.3

φ 9.2

E 9.4

376.81  
74+50

E 8.5

Φ 8.3

W 8.3

75+0

W 7.6

Φ 7.5

E 7.5

+50

E 6.7

Φ 6.7

W 6.9

76+0

W 6.0

Φ 5.8

E 6.0

+50

E 5.2

Φ 4.9

W 5.1

376.81  
77+0

21

W 4.2

Φ 4.1

E 4.4

+50

E 3.5

Φ 3.2

W 3.3

78+0

W 2.3

Φ 2.1

E 2.3

11.01 386.08 1.74 375.07  
+50

E 10.4

Φ 10.2

W 10.5

79+0

W 9.3

Φ 9.2

E 9.2

386.08

79+50

22

E 8.1

☿ 8.1

W 8.3

80+0

W 7.4

☿ 7.2

F 6.9

+50

E 5.7

☿ 5.8

W 6.0

80+93<sup>18</sup> = N.H. U.S. Military Reservation

W 4.6

☿ 4.2

E 4.0





269.13  
1+04 = beginning of cement curb

E 4.82  
+5 5.4  
Φ 5.0  
+15 5.4  
W 4.86

1+50

W 2.89  
+5 3.4  
Φ 3.1  
+15 3.4  
E 2.86

2+0

E 0.77  
+5 1.2  
Φ 0.9  
+15 1.3  
W 0.86

T.P. 11.23 279.95 0.41 268.72

279.95

24

2+50

W 9.50  
+5 10.0  
Φ 9.6  
+15 10.1  
E 9.50

3+0

E 7.39  
+5 7.9  
Φ 7.5  
+15 7.8  
W 7.43

3+50

W 5.39  
+5 6.0  
Φ 5.6  
+15 6.0  
E 5.39

279.95  
4+0

E	3.58
+5	4.0
φ	3.7
+15	4.2
W	3.61

4+50

W	1.79
+5	2.3
φ	1.8
+15	2.2
E	1.76

T.P. 10.53 290.12 0.36 279.59

5+0

E	10.17
+5	10.6
φ	10.1
+15	10.7
W	10.13

290.12

25

5+29<sup>30</sup> = end Cement curb on East

W	9.08
+5	9.6
φ	9.0
+15	9.5
E	9.12

5+50

E	8.7
+5	8.7
φ	8.3
+15	8.8
W	8.33

6+0

W	6.56
+5	6.9
φ	6.4
+15	6.9
E	6.9

290.12

6+25

E	5.9
+5	6.0
Φ	5.6
+15	6.0
W	5.63

6+54<sup>40</sup> = beginning of curb on East

W	4.54
+5	5.0
Φ	4.5
+15	4.9
E	4.59

6+75

E	4.00
+5	4.4
Φ	4.0
+15	4.4
W	3.89

290.12

7+0

W	3.16
+5	3.8
Φ	3.4
+15	3.8
E	3.36

7+25

E	2.91
+5	3.4
Φ	2.9
+15	3.2
W	2.60

7+50

W	2.18
+5	2.7
Φ	2.4
+15	2.9
E	2.52

290.12

7475

E

2.24

+5

2.6

Φ

2.1

+15

2.4

W

1.88

840

W

1.68

+5

2.1

Φ

2.0

+15

2.6

E

2.17

8425

E

2.24

+5

2.6

Φ

1.9

+15

2.0

W

1.65

27

290.12

8450

W

1.76

+5

2.1

Φ

1.9

+15

2.5

E

2.27

8475

E

2.47

+5

2.8

Φ

2.2

+15

2.5

W

2.00

840

W

2.36

+5

2.9

Φ

2.6

+15

3.1

E

2.78

290.12

9+25

E 3.20

+15 3.6

Φ 3.0

+15 3.3

W 2.90

9+50

W 3.47

+15 4.0

Φ 3.6

+15 4.2

E 3.76

9+75

E 4.47

+15 4.7

Φ 4.4

+15 4.9

W 4.27

290.12

10+0

W 5.22

+15 5.7

Φ 5.3

+15 5.7

E 5.27

10+15<sup>30</sup> = end cement curb on East

E 5.75

+15 6.3

Φ 5.8

+15 6.3

W 5.85

10+25

W 6.25

+15 6.7

Φ 6.2

+15 6.6

E 6.6

28

290.12

10+50

E			7.2	
+5			7.7	
Φ			7.4	
+15			7.8	
W			7.3	
T.P.	111	283.67	7.56	282.56
		10+75		
W			2.00	
+5			2.4	
Φ			1.9	
+15			2.4	
E			1.7	
		11+0		
E			2.6	
+5			3.5	
Φ			3.1	
+15			3.5	
W			3.05	

283.67

11+35 = Beginning of curb on East

29

W				4.41
+5				5.0
Φ				4.5
+15				5.0
E				4.44
		11+50		
E				5.01
+5				5.6
Φ				5.1
+15				5.5
W				5.01
		12+0		6.11
W				6.71
+5				7.2
Φ				6.8
+15				7.2
E				6.67

283.67

12+50

E 8.04

+5 8.5

Φ 8.2

+15 8.5

W 8.13

13+0

W 9.26

+5 9.7

Φ 9.2

+15 9.5

E 9.17

13+50

E 10.02

+5 10.2

Φ 10.0

+15 10.4

W 10.06

283.67

14+0

W 10.63

+5 11.0

Φ 10.5

+15 10.86

E 10.59

14+50

E 11.01

+5 11.3

Φ 11.0

+15 11.5

W 10.95

15+07<sup>30</sup> or end of curb on west  
P.C. entrance to Spaulding residence

W 11.35

+5 11.8

Φ 11.5

+15 11.8

E 11.39

T.P. 294 275.12 11.49 272.15

20



275.12

15+26<sup>60</sup> = end cement curb on East

E	2.94
+5	3.4
Φ	3.1
+15	3.4
W	3.5

15+50

W	3.6
+5	3.5
Φ	3.3
+15	3.6
E	3.8

or beginning of cement curb on west  
 15+28<sup>50</sup> = RC entrance to Spaulding residence

E	3.6
+5	4.1
Φ	3.8
+15	4.1
W	3.49

275.12

31

16+35 Grozk

W	4.28
+5	4.9
Φ	4.5
+15	5.0
E	4.1

16+75

E	5.0
+5	5.7
Φ	5.3
+15	5.8
W	5.36

17+0

W	6.13
+5	6.5
Φ	5.9
+15	6.3
E	5.6

275.12

17+25

E	6.5
+5	7.2
φ	6.7
+15	7.3
W	7.03

17+50

W	8.02
+5	8.2
φ	7.8
+15	8.2
E	7.6

or end cement curb Santa Barbara  
 17+78<sup>60</sup> = P.C. curb line 5' to west

E	8.7
+5	9.3
φ	8.8
+15	9.2
W	8.97

Note - Measurements taken on curb line

32

275.12

18+08<sup>21</sup> = P.C. Santa Barbara 5'

W	11.0			
+5	10.7			
φ	10.7			
+15	11.0			
E	10.6			
T.P.	0.08	263.25	11.95	263.17

# 1

30.63 measurements on West & 29.07 on East taken from P.C. or  
 Sta 18+08<sup>21</sup> to Sta 29+21<sup>62</sup> W & 23+90<sup>25</sup> E = P.C. sketch page 23

E	1.2
+5	0.8
φ	0.4
+15	0.4
W	0.5

# 2

W	2.0
+5	2.0
φ	2.2
+15	2.6
E	2.6

263.25

# 3

E	4.6
+5	4.6
φ	4.0
+15	3.8
W	4.0

# 4

W	6.1
+5	6.0
φ	6.2
+15	6.5
E	6.6

# 5

E	8.4
+5	8.3
φ	8.0
+15	8.2
W	8.4

160.6' from P.C. = beginning of cement curb on East

E	8.81
---	------

263.25

33

# 6 = 194.92<sup>69</sup> = beginning cement curb on East  
or P.C. Curb Line 5' to west 20' radius

W	9.64
+5	10.0
φ	9.7
+15	10.2
E	9.63

# 7

E	11.37
+5	11.9
φ	11.5
+15	11.8
W	11.38

# 8

W	13.16
+5	13.5
φ	13.3
+15	13.6
E	13.10

T.P. 0.12 250.27 13.10 250.15

250.27

# 9

E. End cement curb

2.1

+5

2.5

Φ

2.2

+15

2.3

W

1.98

# 10

W

3.74

+5

4.1

Φ

3.8

+15

4.3

no curb

# 11

E beg. cement curb

5.56

+5

6.1

Φ

5.7

+15

6.0

W

5.53

250.27

# 12

W

7.33

+5

7.7

Φ

7.4

+15

7.8

E

7.29

# 13

E

9.04

+5

9.7

Φ

9.3

+15

9.7

W

9.10

# 14

W

11.12

+5

11.5

Φ

11.1

+15

11.5

E

10.79

34

Note - curb washed out from #9 to #11

250.27

#14 + 27.5° on west 26° on E = PC. of curb street to west 5' Radius

E			12.39	
+5			13.1	
⊕			12.7	
+15			13.2	
W = end cement curb			12.95	
T.P.	0.85	238.18	12.94	237.33

#16

W. No curb			3.2	
+5			2.8	
⊕			2.4	
+15			2.9	
E			2.30	

#17

E			4.17	
+5			4.7	
⊕			4.2	
+15			4.7	
W			4.9	

238.18

35

#18

W			6.5	
+5			6.4	
⊕			6.1	
+15			6.5	
E			5.85	

#19

E			7.66	
+5			8.4	
⊕			8.0	
+15			8.1	
W			8.3	

#19 + 13 on west = PC. curb street to west

W. cement curb begins here 8.32

#20 = Pt. = 29 + 21<sup>62</sup> W 23 + 90<sup>35</sup> E

W			9.43	
+5			10.0	
⊕			9.7	
+15			10.2	
E			9.47	



		215.01				202.73	
		3+50				5+0	
E			7.01			W	3.64
+5			7.7			+5	4.1
Φ			7.4			Φ	3.8
+15			7.7			+15	4.1
W			7.09			E	3.63
		4+0					5+50
W			10.08			E	6.30
+5			10.6			+5	6.7
Φ			10.4			Φ	6.5
+15			10.7			+15	6.9
E			10.00			W	6.30
T.P.	0.37	202.73	12.65	202.36			
		4+50					5+68 <sup>5</sup> - end cement curb on W
E			0.69			W	7.18
+5			1.3				6+0
Φ			0.9			W	9.7
+15			1.2			+5	9.5
W			0.75			Φ	9.0
						+15	9.2
						E	8.62

Note - sidewalks not graded from 5+68<sup>5</sup> to P.R.C. on west.

202.73

6+17<sup>67</sup> = P.C. = 30+31<sup>29</sup> W 30+08<sup>05</sup> E

192.90

38

#3

E	9.43	W	2.6
+5	10.0	+5	2.5
Φ	9.8	Φ	2.8
+15	10.4	+15	3.0
8YW	10.6	E	2.54

31.90' Measurements on west &amp; 30.29' on east Taken from P.T. - sketch page 23

#4

#1		E	3.10
W	11.5	+5	3.6
+5	11.3	Φ	3.5
Φ	10.8	+15	4.3
+15	10.9	W	4.5
E	10.67		

#5

#2		W	5.1
E	11.66	+5	5.0
+5	12.0	Φ	4.0
Φ	12.0	+15	4.1
+15	12.2	E	3.57
W	12.4		

T.P. 2.51 192.90 12.34 190.39



192.90

# 6

E 3.96

+5 4.5

Φ 4.5

+15 5.3

W 5.3

# 7

W 6.1

+5 6.0

Φ 4.8

+15 4.8

E 4.13

# 8

E 4.22

+5 5.1

Φ 5.0

+15 6.7

W 6.8

192.90

beginning cement curb

39

# 8 + 12.1 = P.P.C. Sta 33+06<sup>57</sup> to P.C.C. Sta 32+62<sup>31</sup>  
 curb 1' to far west  
 W cement curb begins

+5 6.55

Φ 6.9

+15 5.1

E 4.26

X-section taken on P.L.

E 4.0

+5 4.2

Φ 4.7

+15 5.2

W 5.5

P.T. on Pt Loma Ave S curb w/ Catalina

10.34 182.56



12441				12441				CANYON	Rd	41
0+70				1+23						
W	10.7	113.7	in creek	E		10.2	114.2	10.6		
C	8.9	15.5	on bank	C		12.1	12.3	on edge bank		
E	7.9	16.5		T.P.	0.37	112.17 113.17	111.80 112.80			
				W		4.0	108.1	in creek		
E	10.4	14.0				1+28				
C	11.4	13.0	in creek	W		4.3	7.8	in creek		
W	10.2	14.2		C		4.5	7.6	✓	✓	
				E		+1.2	13.3			
W	12.3	12.1	in creek			1+30.6 = Δ				
C	10.3	14.1	on bank	E		2.1	9.0	in creek		
E	8.6	15.8		C		5.2	6.9	✓	✓	
				W		4.4	7.7	✓	✓	
E	9.0	15.4				1+50				
C	10.8	13.6		W		6.0	6.1	✓	✓	
W	11.6	12.8		C		5.6	6.5	✓	✓	
				E		1.7	10.4	edge on bank		
W	12.8	11.6	on bank			1+78				
C	12.2	12.2		E		2.9	9.2	on edge bank		
E	10.0	14.4		C		8.6	3.5	in creek		
				W		8.2	3.9	✓	✓	

112.17					112.17				
1+54					2+74.0 = Δ				
W		87	103.4	in crack	E		9.9	102.2	
C		93	2.8	- -	C		12.7	99.4	
E		84	3.7	- -	W		14.8	97.3	edge bank
2+00					3+00				
E		88	3.3	- -	W		16.1	96.0	edge of bank = 5' west of this
C		10.0	2.1	- -	C		13.3	98.8	
W		10.2	1.9	- -	E		10.5	101.6	
2+05					3+25				
W		10.7	1.4	- -	E		12.8	99.3	
C		10.1	2.0	- -	T.P.	0.0	99.39	99.39	
E		4.4	8.1	on bank	C		100.39	12.78	100.39
2+34					3+25				
E		4.4	7.7		W		4.7	94.6	
C		7.4	104.7		3+50				
W		13.4	98.7	edge creek	W		6.6	92.7	creek 13.8' W. of this
2+59					3+50				
W		15.2	96.9	11' creek	C		4.6	94.7	
C		14.4	97.7	edge	E		2.8	96.5	
E		7.5	104.6		3+71.7 = Δ				
2+59					3+71.7 = Δ				
W		15.2	96.9	11' creek	E		5.93	93.4	on hub
C		14.4	97.7	edge	C		8.2	91.1	
E		7.5	104.6		W		10.2	89.1	creek 13.12' W.

		99.37				86.31	CANYON #3
		4400			E	3.2	83.1
W			13.3	86.0			
C			11.4	87.9	E	4.8	81.5
E			8.7	90.6	+L	5.8	80.5 edge bank
		4425			C	8.5	77.8 in creek
E			7.1	92.2	W	7.0	79.3 edge w. bank
C			9.6	89.7			
W			12.1	87.2	W	7.3	79.0
		4450			C	7.8	78.5 edge w. bank
W			14.4	84.9	E	9.3	77.0 in creek
C			12.0	87.3			
E			9.8	89.5	E	8.1	78.2 edge w. bank
		4465.38 = $\Delta$			C	8.0	78.3
E			10.0	89.3	W	7.8	78.5
C			13.3	86.0			
T.P.	0.20	86.31 4994	13.25	86.14 47.11	W	7.8	78.5
W			3.0	83.3	C	8.5	77.8
		4477			E	9.0	77.3
W			4.7	81.6 on bank			
			8.1	78.2 in creek			
C			4.3	82.0			

86.31

5+55

E		68	79.5	
C		4.4	81.9	Allen's fence
W		3.6	82.7	
6+10 = Δ				
W		8.4	77.9	Allen's fence
C		9.3	77.0	
E		12.9	73.4	

6+50

E		19.6	66.7	
C		15.8	70.5	
W		12.6	73.7	1' outside of fence
T.P.	0.17	<del>7.4</del> 7.4	<del>73.2</del> 73.2	
		13.07	71.24	

7+00

W		3.6	69.8	
C		5.7	67.7	
E		7.8	65.6	

73.41

CANYON 44

7+30 = Δ

E		10.2	63.2	
C		8.4	65.0	
W		7.7	65.7	
7+50				
W		7.6	65.8	
C		9.8	63.6	
E		11.8	61.6	

8+00

E		13.0	60.4	
C		12.8	60.6	
W		12.4	61.0	
T.P.	n.02	<del>62.48</del> 62.48	<del>60.46</del> 60.46	
		12.95	61.46	

8+50

W		3.7	58.7	
C		4.1	58.3	
E		4.7	57.7	

		62.48		50.12		45	
		9+00		10+50			
W		88	53.6	E		49	45.2
C		87	53.7	C		48	45.3
E		92	53.2	W		47	45.4
		9+59		11+00			
E		114	51.0	W		63	43.8
C		115	50.9	C		63	43.8
W		120	50.4	E		64	43.7
		9+94		11+50			
T.P.	0.19	<del>12.55</del>	49.93				
W		50.12	50.93	E		84	41.7
		50.12	48.1	C		84	41.7
C		24	47.7	W		83	41.8
E		27	47.4				
		10+00 = ctr present road		12+00			
E		40	46.1	W		97	40.4
C		38	46.3	C		97	40.4
W		35	46.6	E		97	40.4
		10+35		12+47.55 = ctr of new grade			
W		23	47.8	E		10.7	39.4
C		26	47.5	C		10.7	39.4
E		29	47.2	W		10.6	39.5
				T.P.	4.5W	46.0W	8.62
							41.50

T.P.	6.24	40.19	12.07	33.95	
			6.57	33.62	-Mon/Bermals



Cross Sec. Bush Goldfinch East		St. 50' wide	Moore Miller Shaw	H.I.	261.26	Bush St. 50' wide	47
B.M.	El. 259.98	Plug and return	N.E. Cor Bush & Goldfinch	1/4		10.9	250.4 ✓
	B.S. 126	H.I. 261.26	Elec.	0		10.3	251.0 ✓
	E.L. Goldfinch			1/4		10.3	251.0 ✓
S.H.		1.9	259.4 ✓	1/4		10.3	251.0 ✓
curb		1.91	259.4 ✓	curb		10.0	251.3 ✓
1/4		2.1	259.2 ✓	N.H.		9.6	251.7 ✓
C		1.9	259.4 ✓		1+25		
1/4		1.8	259.5 ✓	S. curb		12.5	248.8 ✓
curb		1.29	260.0 ✓	curb		11.5	249.8 ✓
N.L.		1.1	260.2 ✓	S.L.		10.2	251.1 ✓
	+50			T.P.	0.65	248.8 ✓	248.17 ✓
					1+50	13.09	
N.L.		5.8	255.5 ✓	S.L.		2.2	246.6 ✓
curb		5.6	255.7 ✓	cb		2.2	246.6 ✓
1/4		5.9	255.4 ✓	1/4		2.5	246.3 ✓
C		6.0	255.3 ✓	C		2.1	246.7 ✓
1/4		6.7	254.6 ✓	1/4		2.0	246.8 ✓
curb		6.3	255.0 ✓	cb		1.7	247.1 ✓
S.L.		6.4	254.9 ✓	N.L.		1.2	247.6 ✓
	1+00				2+00		
S.H.		10.2	251.1 ✓	N.L.		5.5	243.3 ✓
curb		10.4	250.9 ✓	cb		6.2	242.6 ✓

ground Elv.  
Rock Wall

ground Elv.  
Cem. Wall

ground Elv.  
Cem. Wall

248.82			237.10			Bush St. 50' Wide 48	
1/4		6.4	242.4 <sup>v</sup>	cb		2.4	234.7 <sup>v</sup>
c		6.5	242.3 <sup>v</sup>	S.L.		2.4	234.7 <sup>v</sup> Cement Wall Ground Ely.
1/4		6.8	242.0 <sup>v</sup>		3+50		
cb		6.2	242.6 <sup>v</sup>	SL		6.4	230.7 <sup>v</sup>
sh		6.2	242.6 <sup>v</sup>	cb		6.8	230.3 <sup>v</sup>
		2+50		1/4		8.1	229.0 <sup>v</sup>
S.L.		9.9	238.9 <sup>v</sup>	c		7.9	229.2 <sup>v</sup>
cb		10.2	238.6 <sup>v</sup>	1/4		8.1	229.0 <sup>v</sup>
1/4		10.6	238.2 <sup>v</sup>	cb		8.5	228.6 <sup>v</sup>
c		10.6	238.2 <sup>v</sup>	N.L.		8.4	228.7 <sup>v</sup>
1/4		10.6	238.2 <sup>v</sup>		3+70		
cb		10.3	238.5 <sup>v</sup>	N.L.		12.4	224.7 <sup>v</sup>
N.L.		10.2	238.6 <sup>v</sup>	cb		10.7	226.4 <sup>v</sup>
T.P.	0.66	237.10 <sup>v</sup>	12.38	236.44 <sup>v</sup>	1/4	10.4	226.7 <sup>v</sup>
		3+00			44	10.5	226.6 <sup>v</sup>
				c		11.5	225.6 <sup>v</sup>
N.L.		2.7	234.4 <sup>v</sup>	1/4		11.2	225.9 <sup>v</sup>
cb		2.8	234.3 <sup>v</sup>	cb		10.2	226.9 <sup>v</sup>
1/4		3.1	234.0 <sup>v</sup>	S.L.		8.1	229.0 <sup>v</sup>
c		3.2	233.9 <sup>v</sup>				
1/4		3.2	233.9 <sup>v</sup>				

237.10  
 50  
 238.60  
 11.8  
 240.40  
 50  
 240.90  
 12.40  
 240.75  
 0.75  
 240.00  
 266

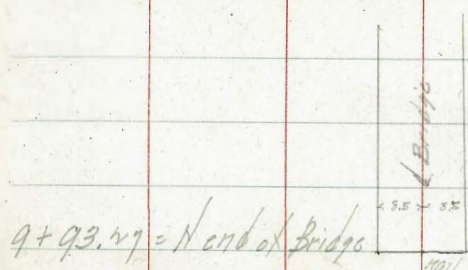
5/13/20 Gregory  
Moose  
1771/er

Alignment + Levels on  
Dyke from S. End of  
Morang Paving to  
Old Town Bridge

Levels

49

Not at Greenwood



7+87.18 A 11°06' Right

R = 1380.0  
T = 124.1

E = 6.5'

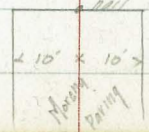
3+54.68 A 7°54' Left

R = 1459.2  
ST = 27.0

nail

E = 3.5 or 4.5 or 6.5

0+00 = End of Morang Paving



9.17	18.06	8.89	
	0+00		
10' E of L	4.05	14.01	= paving
L	3.95	14.11	= paving
10' W of L	4.05	14.01	=
	0+25		
14.5' W of L = edge	4.2	13.9	
10' - - -	4.1	14.0	
L	4.0	14.1	
10' E of -	3.9	14.2	
14.5' - - - = edge of Kearril paving	3.9	14.2	
	0+50		
14.5' - - - = - - -	4.2	13.9	
10' - - -	4.2	13.9	
L	3.9	14.2	
10' W of -	4.2	13.9	
12.5' - - - = edge	4.3	13.8	

	18.06 2+25		
15.5' W of L = edge	4.4	13.7	
10' - - -	4.2	13.9	
4	4.0	14.1	
10' E of L	4.2	13.9	
14.5' - - - = edge	4.2	13.9	
	14.00		
14.5' E of L = edge	4.1	14.0	
10' - - -	4.1	14.0	
4	4.0	14.1	
10' W of L	4.6	13.7	
15.5' - - - = edge	4.3	13.8	
	14.25		
15' W of L = edge	4.1	14.0	
10' - - -	4.2	13.9	
4	4.0	14.1	
10' E of L	4.3	13.8	
14' - - - = edge	4.2	13.7	
	14.50		
14' E of L = edge	4.4	13.7	

10' E of L	4.1	14.0	
4	4.0	14.1	
10' W of L	4.0	14.1	
15' - - - = edge	4.0	14.1	
	14.75		
14.5' W of L = edge	3.8	14.3	
10' - - -	3.9	14.2	
4	3.8	14.3	
10' E of L	4.2	13.9	
14' - - - = edge	4.4	13.7	
	2+00		
14' E of L = edge	4.2	13.9	
10' - - -	4.1	14.0	
4	3.9	14.2	
10' W of L	4.0	14.1	
14' - - - = edge	3.9	14.2	
	2+25		
14' W of L = edge	4.0	14.1	
10' - - -	4.0	14.1	
4	4.0	14.1	



6	18.06	4.3	13.8	6	4.7	13.4
10' W of - = edge		4.4	13.7	10.5' W = edge	5.0	13.1
	4+25				5+25	
10' - - - = edge		4.5	13.6	10.5' W = edge	5.1	13.0
6		4.4	13.7	6	4.8	13.3
10' E of -		4.6	13.5	10' E	5.0	13.1
10' - - - = edge		4.6	13.5	10' E = edge	5.0	13.1
	4+50				5+50	
12.5' E of 6 = edge		4.9	13.2	12' E = edge	5.2	12.9
10' - - -		4.8	13.3	10' E	5.1	13.0
6		4.5	13.6	6	4.9	13.2
10.5' W = edge		4.9	13.2	11' W = edge	5.1	13.0
	4+75				5+75	
11' W = edge		4.8	13.3	11' W = edge	5.3	12.8
6		4.6	13.5	6	5.1	13.0
10' E		5.0	13.1	11' E = edge	5.3	12.8
12.5' - = edge		5.0	13.1		6+00	
	5+00			11' E = edge	5.5	12.6
12' E = edge		5.1	13.0	6	5.3	12.8
10' E		5.0	13.1	11' W = edge	5.6	12.6

	18.06 6+25				4		53	12.8
11' W = edge		5.6	12.5		10' E = edge		5.6	12.5
↓		5.3	12.8			7+50		
11' E = edge		5.4	12.7		8.5' E = edge		5.5	12.6
	6+50				↓		5.4	12.7
11' E = edge		5.5	12.6		10' W		5.6	12.5
↓		5.4	12.7		15' W = edge		5.8	12.3
11' W = edge		5.7	12.4			7+75		
	6+75				17.5' W = edge		5.9	12.2
11' W = edge		5.6	12.5		10' ✓		5.5	12.6
↓		5.4	12.7		↓		5.3	12.8
10' E = edge		5.7	12.4		7' E = edge		5.7	12.4
	7+00					7+87.18 Δ		
10' E = edge		5.5	12.6		6.5' E = edge		5.6	12.5
↓		5.3	12.8		↓		5.3	12.8
10' W		5.7	12.4		10' W		5.4	12.7
12.5' W = edge		5.8	12.3		19' W = edge		5.7	12.4
	7+25					8+25		
14' W = edge		5.6	12.5		16' W = edge		5.8	12.3
10' W		5.5	12.6		10' ✓		5.5	12.6

	18.06		
d		5.4	12.9
9.5' E = edge		5.6	12.5
	8+50		
10.5' E = edge		5.3	12.8
d		5.1	13.0
10' W		5.6	12.5
15' W = edge		6.0	12.1
	8+75		
15' W = edge		5.9	12.2
10' W		5.5	12.6
d		5.1	13.0
10.5' E = edge		5.1	13.0
	9+00		
10.5' E = edge		5.1	13.0
d		5.0	13.1
10' W		5.3	12.8
14.5' W = edge		5.4	12.7
	9+25		
14' W = edge		5.3	12.8
10' W		5.1	13.0

			57
d		4.8	13.3
10' E = edge		4.9	13.2
	9+50		
10' E = edge		4.7	13.4
d		4.5	13.6
10' W		4.8	13.3
14' W = edge		5.0	13.1
	9+93.27 = N end of Bridge		
8.5' W = edge of roadway		4.1	14.0
d		4.1	14.0
8.5' E = edge of roadway		4.1	14.0

This elevation may be higher when  
new deck is put on Bridge



Grades Old Town Dike

Station	1932	1933	1934	1935	1936	1937	1938	1939	1940	1941	1942	1943	1944	1945
0+00 = End paving		14.1												
0+50	13.95	14.05												
1	13.90	14.0												
+5.0	13.85													
2	13.80													
+5.0	13.75													
+67.68 = P.C.	13.70													
3	13.70													
+5.0	13.65													
4	13.60													
+161.40 = E.C.	13.56													
5	13.50													
+5.0	13.45													
6	13.4													
+50.8 P.C.														
7	13.3													
+5.0														
8	13.2	13.3												
+5.0														

889  
10+20  
1933  
1325 1390 1355 11 553 558 1370  
5.38 5.23 4.98  
W +1.7 +1.6 +2.1 +2.3 +2.3 +2.2 +2.6 +1.9 +1.3 +1.4 +1.4  
E +2.0 +1.9 +1.9 +1.9 +2.2 +2.1 +1.5 +1.6 +1.4 +1.4

1938 1939 1940 1941 1942 1943 1944 1945  
6.51 4.15 4.20 4.45 4.20 4.25  
12.75 4.11 +1.0 +1.1 +1.2 +1.2 +1.0 +0.5 +1.1  
4.27 +1.1 +1.1 +1.2 +1.3 +1.2 +1.5 +1.7 +2.1  
17.55  
13.45  
4.15

879 1395 1320 1375  
934 4.30 4.30 4.35  
7820 4.25  
4.05 13.80 13.75  
13.58 4.90 4.18  
4.78 13.70 4.74  
19.31 4.57 13.54

13.56 13.40  
4.76 4.75 4.81  
13.85  
13.85 13.30  
4.30 4.39  
17.69  
4.44 13.00 4.39  
4.49  
3.20

7/9/20 Gregory  
 Miller  
 Shaw  
 CROSS SECTION OF 20' Alley  
 Dewey to Crosby  
 bet Woolman & Harrison

56

B.P. HW  
 Irving & Dewey

11.59 79.52 67.93

W. curb of Dewey

S 2.90 76.6 on Alley curb

H 4.08 77.4 ✓ ✓ ✓

T.P. 6.32 82.94 76.62

7' W. of W. curb of Dewey

H 5.3 77.6

C 5.8 77.1

S 6.1 76.8

W.L. of Dewey = 0+00

S 5.4 79.5

C 5.1 77.8

H 2.4 80.5

0+20

H 0.8 82.1

C 2.5 80.4

S 2.2 80.7

0+35

S 2.0 80.9

C		1.9	81.0		
N		1.5	81.4		
	0+69				
N		2.6	80.3		
C		3.2	79.7		
S		4.1	78.8	= center	of gate to house
	1+00				
S		4.7	78.2		
C		4.7	78.2		
N		4.2	78.7		
	1+39				
N		5.9	77.0		
C		6.7	76.2		
S		7.1	75.8	= center	of 18' double garage.
	1+75				
S		8.7	74.2	= center	of 10' garage. grade can be .5 lower than this
C		8.6	74.3		
N		8.2	74.7		
	1+89	9.9	73.0	= center	of gate use this for grade line if possible.
	2+00				
N		10.0	72.9	= gate	to house

C			9.6	73.3	= sewer	Manhole
S			10.0	72.9	= gate to	house
T.P.	0.56	71.30	12.20	70.74		
		2+39				
S			1.1	70.2		
		2+42				
S			3.0	68.3	= center of	9' garage
C			3.2	68.1		
N			2.1	68.2		
		2+60				
S			4.9	66.4	= center	of gate
		2+74				
N			7.0	64.3	= center	of 17' double garage
C			7.5	63.8		
S			6.2	65.1		
		3+00				
S			10.0	61.3		
C			10.5	60.8		
N			9.9	61.4		

71.30

3+40

N			13.1	58.2
C			13.1	58.2
S			12.4	58.9
T.P.	1.64	59.94	13.00	58.30

3+53

S			2.0	57.9	= center of S garage
---	--	--	-----	------	----------------------

3+85

S			4.3	55.6
C			4.4	55.5
N			4.0	55.9

4+30

N			6.4	53.5	
C			6.0	53.9	
S			5.6	54.3	= center of walk 8' wide to house

4+41 ± = SL Pueblo St. N

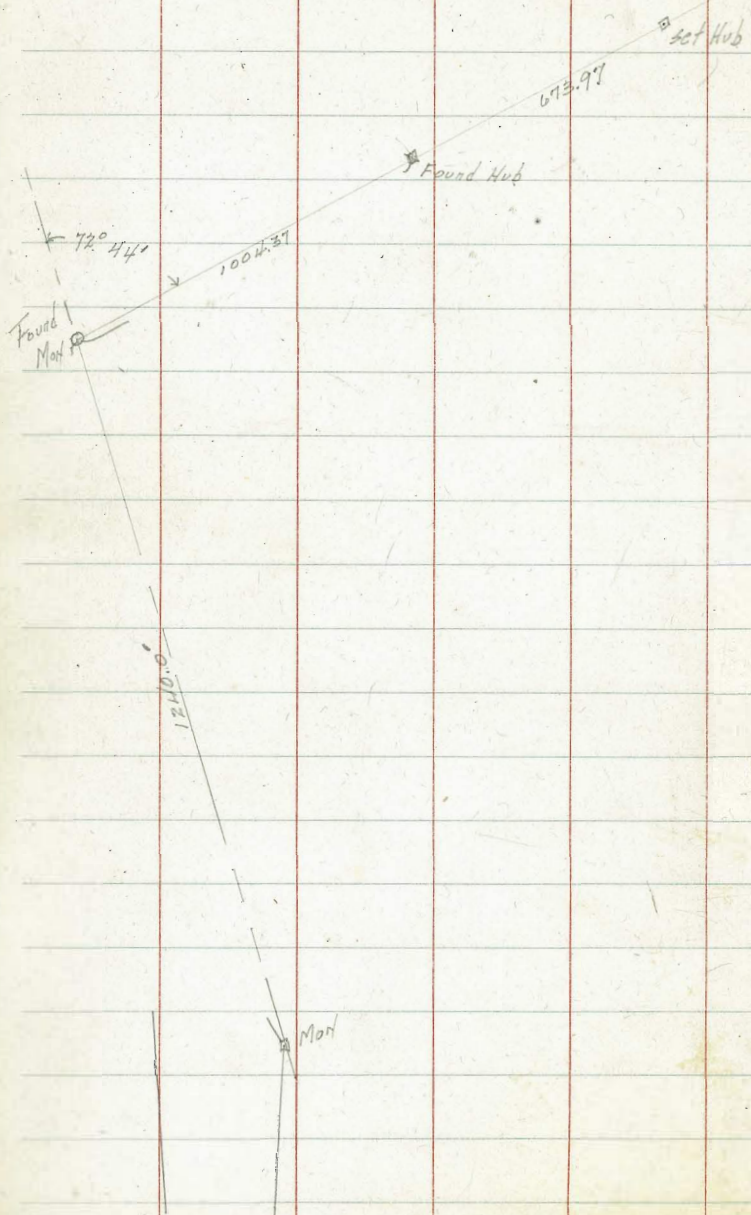
S			6.6	53.3
C			8.1	51.8
N			9.1	50.8

57

4+50

N			10.1	49.8
C			9.8	50.1
S			8.9	57.0

8/6/20 Gregory Survey to Locate Monks on  
NL Ex Mission Lot 32  
564W as placed according to Notes  
in Book 1020 Page 21



7/18/21

Noone  
Miller  
Shaw

Cross Section of 20' Alley  
Lincoln to Polk  
bet. Idaho & Utah

Blk 167  
Univ. Hqts.

9.26 370.11 360.85

SP. SE. Idaho  
+ Lincoln

M.H. of LINCOLN = 0+00

W	7.4	362.7
C	7.1	363.0
E	6.7	363.4

0+4.50

E	6.7	363.4
C	7.2	362.9
W	7.4	362.7

ctr 8' Garage door 10.8 from ctr divl floor

0+50

W	7.0	363.1
C	6.8	363.3
E	6.6	363.5

Fence 9.7 from ctr

Fence 9.3 from ctr

0+88

E	6.1	364.0
C	6.3	363.8

" 9.6 " "

W	5.9	364.2
---	-----	-------

ctr Double door Garage 17.0' wide cement floor 11.8 from ctr

1+23

W	5.85	364.26
---	------	--------

" " " " 14.0 " " " 13.5 " "

370.11

62

C		5.8	364.3			
E		5.4	364.7	Fence	9.6	from ctr
		1+50				
E		5.1	365.0	"	9.6	" "
B		5.8	364.3	"	9.7	" "
W		5.6	364.5			
		2+00		"	10.3	" "
W		4.7	365.4			
C		4.7	365.4	"	9.7	" "
E		4.8	365.3			
		2+18				
E		4.2	365.9	8' Garage door	Dirt floor	14.5 from ctr
C		4.2	365.9			
W		4.4	365.7	Fence	9.7	from ctr
		2+58				
W		3.9	366.2	"	10.0	" "
C		3.8	366.3			
E		3.6	366.5	8' Garage floor	Wood floor	11.3 from ctr
		3+00				
E		3.1	367.0	Barn	no door	9.0 from ctr



C			3.0	367.1			
W			3.3	366.8		Fence	10.0 from ctr
			3+50				
W			2.8	367.3		"	9.5 " "
C			2.7	367.4		"	9.5 " "
E			2.7	367.4			
			4+00				
E			1.6	368.5		"	9.6 " "
C			1.7	368.4			
W			1.8	368.3		"	9.5 " "
			4+57				
W			1.4	368.7		"	9.7 " "
C			1.5	368.6			
E			1.4	368.7		9' Garage door	Wood floor Eline 10.5 from ctr
T.P.	5.02	373.61	1.52	368.59			
			4+93				
E			4.9	368.7		Fence	9.5 from ctr
C			4.6	369.0			
W			4.6	369.0		9' Garage door	Dirt Floor 10' from ctr

Elev. at above

373.61

64

5+50

W 4.4 369.7

Barn no door

10.5 from ctr

E 4.9 368.7

E 4.8 368.8

Fence 9.8 from ctr

6+00

So. line Park Ave.

E 4.7 368.9

C 4.6 369.0

W 4.5 369.1

Fence 11.0 from ctr

ck Elev. 375 369.86

SE. Park a

100 ft. 369.96

64  
25  
87

Levels Wheelers house

65

4.39

253.81

251.42

Mon Jan  
+ Wetherby

4.56

244.78

11.59

242.22

Elev. Flow line of 4" C.I. from Toilet.

9.28

235.50

88' S. of E. of GUY ST

#B' W. of W.L. of Courts.

X Section of 32<sup>nd</sup> From Landis to Upas

65' Street  
10' Curbs  
11.25' <sup>1</sup>/<sub>4</sub>

B.M. 338.77 Plg. W.W. Cor Landis & 32<sup>nd</sup>  
B.S. 4.1  
528 343.75

10/3/22 Miller  
Eight  
Walbricht

343.75

N Curb Line Landis

				C		5.7
				<sup>1</sup> / <sub>4</sub>		5.7
				E		5.7
W		6.0		<sup>1</sup> / <sub>4</sub>		5.7
C		5.9		C		5.7
<sup>1</sup> / <sub>4</sub>		5.8		E		5.8
E		5.7			S <sup>1</sup> / <sub>4</sub>	
<sup>1</sup> / <sub>4</sub>		5.7		E		5.7
C		5.9		E		5.8
E		6.2		<sup>1</sup> / <sub>4</sub>		5.7
	N <sup>1</sup> / <sub>4</sub>			E		5.8
E		5.9		<sup>1</sup> / <sub>4</sub>		5.7
C		5.8		C		5.4
<sup>1</sup> / <sub>4</sub>		5.5		W		5.7
E		5.6			S.C.	
<sup>1</sup> / <sub>4</sub>		5.6		W		5.7
C		5.8		C		5.6
W		5.9		# 5 <sup>1</sup> / <sub>4</sub>		6.0 5.7
	E			E		5.6
W		5.8		<sup>1</sup> / <sub>4</sub>		5.6
				E		

343.75

C		5.8	
E		5.6	
	S Line Landis		Line of Trees 5' W of E Prop. Line
-5		5.6	
E		6.9	
+5		5.0	
C		5.6	
1/4		5.5	
E		5.5	
1/4		5.6	
E		5.8	
W		5.4	
	50' S		
W		5.5	
E		6.0	
1/4		6.0	
E		6.1	
1/4		6.3	
E		6.5	
+5		5.9	
E		6.9	
+5		6.1	

343.75

67

	100' S	
-5		
E		7.6
		6.5
+5		5.6
E		6.1
1/4		5.8
E		6.0
1/4		6.0
C		5.8
W		5.4
	150' S	
W		4.7
E		4.8
+8		5.2
1/4		5.7
E		6.0
1/4		6.0
E		6.2
+6		5.3
E		7.5
+5		6.3

	343.75 200' S			
E		6.9		
+6.		5.9		
C		6.2		
1/4		5.8		
E		5.7		
1/4		5.5		
C		5.3		
W		5.1		
	250' S			
W		5.3		
C		5.4		
1/4		5.4		
E		5.4		
1/4		5.4		
C		5.4		
E		5.7		
	300' S			
E		6.6		
C		6.2		
1/4		5.7		

	343.75			68
E			5.3	
1/4			5.0	
C			4.7	
W			5.0	
	350.5			
W			5.3	
C			5.4	
1/4			5.5	
E			5.7	
1/4			5.6	
C			5.7	
E			6.1	
	400.5			
E			5.8	
C			5.6	
1/4			5.7	
E			5.9	
1/4			5.9	
+8.			6.1	
C			5.7	
W			5.4	

343.75

342.26

69

T.P. Station 3790

5.35

338.40

oneement walk  
entrance to House

W

4.4

3.86

342.26

550.5

450 S

W

4.9

W

4.1

E

4.9

E

4.6

+3

5.4

+4

4.9

1/4

5.3

1/4

4.8

E

5.0

E

4.5

1/4

4.7

1/4

4.4

E

4.9

E

4.5

+5

4.7

+4

3.8

E

4.9

E

5.1

500 S

600 S = N. Line Dwight

Line of Trees 8' W of E Prop Line

-5

4.9

E

6.1

E

5.3

+5

4.7

E

4.8

E

4.4

+5

5.2

1/4

4.4

1/4

5.0

E

4.7

E

5.3

1/4

4.6

1/4

5.5

+9

5.0

+9

5.7

E

4.2

E

5.1

W

5.1

342.26

N. Curb

W	5.5
E	5.5
+4	5.8
1/4	5.6
E	5.4
1/4	5.5
E	5.2
E	5.2

N 1/4

E	5.3
C	4.9
1/4	5.4
E	5.6
1/4	5.5
E	5.6
W	5.5

E Dwight

W	5.9
---	-----

342.26

70

E	5.7
1/4	5.6
E	5.6
1/4	5.5
E	5.4
E	5.3

S 1/4

E	5.4
E	5.5
1/4	5.6
E	5.6
1/4	5.5
E	5.3
W	5.6

S Curb

W	5.8
E	5.6
1/4	5.8
E	6.1
1/4	5.5



342.26

339.07 100' S

O 5.5

E 3.1

E 5.4

C 3.4

S Line Dwight

1/4 3.6

E 5.5

E 3.7

C 5.6

1/4 3.6

1/4 5.6

C 3.8

E 6.0

W 3.6

1/4 6.0

W 3.7

C 5.7

C 3.8

W 6.1

1/4 3.8

T.P. 1.63

339.07

4.85

337.41

B.M. Pig An  
Stump at Dwight  
337.40

50' S

E 3.9

W 3.3

1/4 3.8

C 3.2

C 3.8

1/4 3.4

E 3.4

E 3.4

E 3.6

1/4 3.2

C 3.8

C 2.7

1/4 3.9

E 2.5

E 4.0

1/4 3.9

E 3.8

W 4.2

200' S

339.07  
250 S

W	4.7	
E	4.6	
1/4	4.6	
LE	4.7	
1/4	4.5	
E	4.2	
E	4.0	
E	4.7	300 S
C	4.8	
1/4	5.2	
LE	5.2	
1/4	5.2	
C	5.2	
W	5.4	320 S
E	4.45	on cement walk to house
W	5.6	350 S
E	5.3	
1/4	5.0	
LE	5.2	
1/4	5.2	

339.07

72

E	5.0	
E	4.8	
E	4.87	on cement walk to house
E	5.1	370 S
E	5.8	400 S
1/4	5.7	
E	5.7	
1/4	5.7	
E	5.7	
W	5.9	
E	5.29	on cement walk to house
W	5.88	on cement walk to house
W	6.05	442' S
W	6.2	450' S
W	6.2	" " driveway
E	6.2	
1/4	5.9	
LE	6.1	
1/4	6.3	
E	6.0	
E	5.7	
T.P.	254	335.70
		5.91
		333.16

335.70  
470 S

335.70

72

W		3.10	cement walk	1/4		4.9	
	492 S						
W		3.10	" drive	E		4.9	
	500 S						
E		2.7		1/4		4.8	
C		3.1		E		5.0	
1/4		3.3		W		5.0	
E		3.3		T.P.	1.70	4.89	330.81
1/4		3.3					BM. SPK S.W. Myrtle 330.82
C		3.6		W		2.2	
W		3.6		E		2.4	
	520 S			1/4		2.6	
W		3.81	on cement walk	E		2.3	
	540 S						
W		4.06	" " drive	1/4		2.8	
	550 S						
W		4.4		E		2.8	
C		4.2		E		2.4	
1/4		4.1					
					50' S	3.7	
E		4.1		E		3.8	
1/4		4.1		E		3.6	
E		3.9		1/4		3.6	
				E		3.6	
E		3.5		1/4		3.6	
	600' S = N LINE MYRTLE			E		3.6	
E		4.5					
C		4.7		W		3.4	

335.70

100'S

W	4.4
C	4.4
1/4	4.3
E	4.4
1/4	4.0
C	4.0
E	4.2
E	4.4
C	4.5
1/4	4.8
E	4.9
1/4	5.0
C	4.9
W	4.8
W	5.6
C	5.5
1/4	5.5
E	5.4
1/4	5.2
C	5.3
E	5.4

150'S

200'S

335.7

250'S

E	5.5
C	5.5
1/4	5.8
E	6.0
1/4	6.4
C	6.6
W	6.6
W	7.4
C	7.3
1/4	7.4
E	7.0
1/4	6.8
C	6.5
E	6.3
E	7.5
C	8.3
1/4	8.4
E	8.3
1/4	8.4
C	8.6
W	8.0

298'S

300'S = N Line Upas

74

N.W. Cor Yerona Wests B.M. 250.17

110 251.27 250.17 B.M. B.P.

1.77 240.74 12.30 238.97

5.77 235.47 = B.P. SW. Cor in Grob La Paloma = West 235.47

0.96 234.00 7.70 233.04

9.61 224.39 = 2 nails in fence  
File West side Catalina Blvd. 50' South of end present paving. At Point Loma Ave.

B.R. Spk Bottom board South East Egyptian Gate to Tingleys = 296.00 = West 295.96 B.M. RR Spk

5.56 301.56 296.00

5.70 303.88 3.43 298.13

2 nails in Cor Redwood fence post. South side of lane leading to Robinsons Poultry Farm.  
Note: Eucalyptis trees on each side of lane; North Road to Robinsons.

3.18 300.70 B.M. 2 nails;

12.15 315.23 0.11 302.77

12.26 327.04 0.24 315.68

File E.S. Catalina Appe 306 North of mast 8.80 319.14 B.M.  
South by entrance to Theosophical grounds; 2 nails

12.43 340.07 0.30 327.64

2 nails 10" x 10" post South post of entrance to Theosophical grounds;

3.77 336.30 B.M.

12.60 352.57 0.10 339.97

12.92 365.29 0.21 352.30

+	365.29 X	-		
		5.48	359.81	nails in Pale C <sup>no</sup> 250 opposite Montezuma St?
10.18	375.19	0.28	365.01	
nails in top of 8" x 8" bumper Post Cen of most southerly gallery into Theosophical grounds;		1.24	370.25	
8.65	382.61	1.23	373.96	
nails in green fence post NW Cor reservoir site; E side Catalina Blvd;		5.24	377.37	
206	377.43		377.37	
0.94	368.71	9.66	367.77	
0.29	356.30	12.70	356.01	
0.10	343.43	12.97	343.23	
0.46	331.18	12.71	320.72	
1.44	319.89	12.73	318.45	
0.26	307.14	13.01	306.88	
3.89	302.92	8.10	299.04	
4.65	301.55	6.03	296.90	
		5.48	296.07 = 296.02 = 295.96	

7+9527  
7187.15  

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20604  
1341  

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7199  
92012  

---

99215

342.26  
4.84  

---

337.42

335.70  
1.92  

---

339.07 333.78  

---

333.78  
5.29

6174.90  
 981.68  
 7156.58 = S.W.P.L. 104  
 936.60  
 8093.18 = U.S.G.R

3190  
 5  
 255.20  
 12.10  
 267.30 west

28715  
 25465  
 43250  
 1341  
 21925  
 57  
 2174  
 44135 E  
 N 85° 55'

3027  
 5  
 24216  
 1210  
 2542.26 East

11900  
 2617  
 11467  
 37230  
 8038 30

300800  
 25426  
 3582262.31 E  
 303429  
 267.30  
 3306.59 W

300800  
 25426  
 3582262.31 E  
 N 80° 35' 30" E  
 5327  
 2111 E  
 1787  
 2936  
 7997  
 26800  
 9165

26765  
 24737  
 44140  
 6659  
 2100  
 6848  
 17600  
 2112450  
 14200  
 9165

1206  
 1278  
 1328  
 1307  
 1295  
 1255  
 862  
 1207  
 657  
 10450

371.7 Δ 45° 54' R  
 371.7 Δ 45° 54' R  
 192 Δ 40° 22' R  
 371.7 Δ 45° 54' R  
 465.38 Δ 53° 27' L  
 471.0 Δ 41° 12' R

837  
 37  
 20  
 17  
 202  
 19  
 452  
 624  
 2208  
 1207  
 657  
 10450

226  
 192  
 400  
 400  
 465.38 Δ 53° 27' L

886  
 442  
 928

1009  
 1044

1604

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.  
 ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.  
 FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Compiled by Julien A. Hall, M. Am. Soc. C. E.

