FIELD BOOK

0
25
63 600
1
+35
+63
+82
2
+40
3
+50
4
4.35
4.16
5 12
+ 46
600

IVANHOE

250
125
425

#1075

97
237.5
334.5

Ret. out N.E. Ivanhoe & Silverado

all out on E side from S.L. Park Row S. to 97 S. of S.L. Silv.
✓ ✓ ✓ ✓ ✓ Ivanhoe E (on curve) from 97 S. of Silver to 334.5
out on W side from N.L. Silver to 125' N

Ret out NW Silver & Ivanhoe
SW

S/C 17 on W side from 150 S. of S.L. Silver to 175 S. of S.L. Silver
250 425

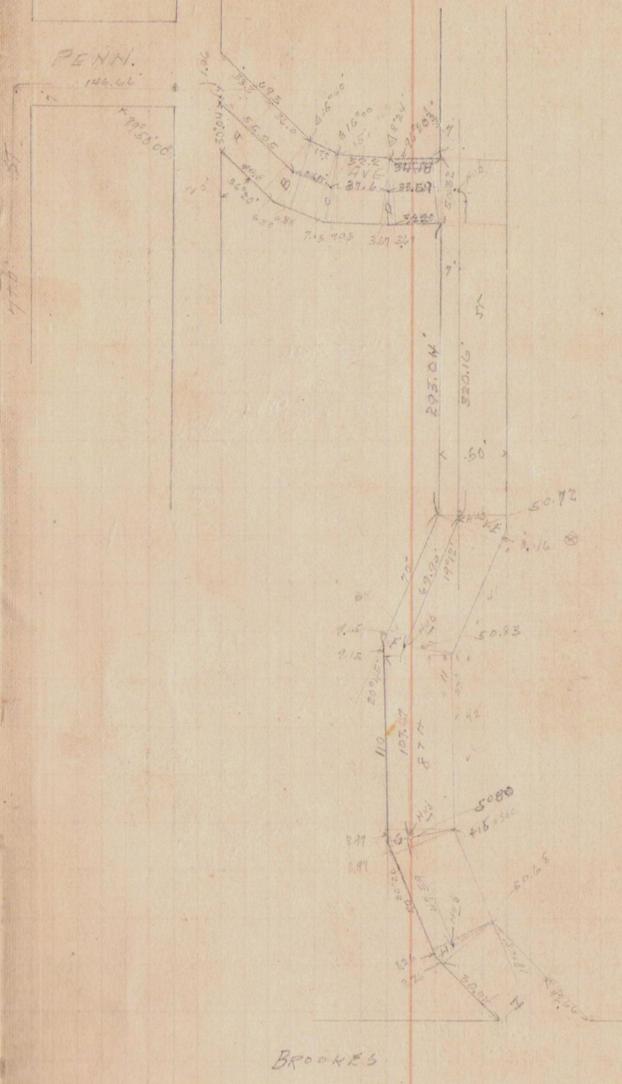
8.96

4/6/20 – Gregory, Moore, Miller

CROSS SECTION OF PENNSYLVANIA AVE 50' wide 10' obs from Alley East of 7th to WL 8th St

Posted 4/30/20

on BM	0.54	287.40		286.86	BP NW 6th + Penn
T.P.	0.55	274.87 ✓	13.08	274.32	
			4.51	270.36	spk in Pole Weida Alley
			5.40	269.47	on cb S.S. Penn + Alley
		E. L. Alley			
H	"		4.6	270.3	
cb			5.0	69.9	
1/4			5.5	69.4	
c			5.5	69.4	
1/4			5.8	69.1	
cb			6.5	68.4	
+8			6.8	68.1	
5			6.3	68.6	
	16.65' E on H				
c			5.5	69.4	
1/4			5.4	69.5	
cb			5.6	69.3	
+8			9.9	65.0	
H			4.9	70.0	
	18.65 E on H				
H			10.0	64.9	
cb			5.9	69.0	

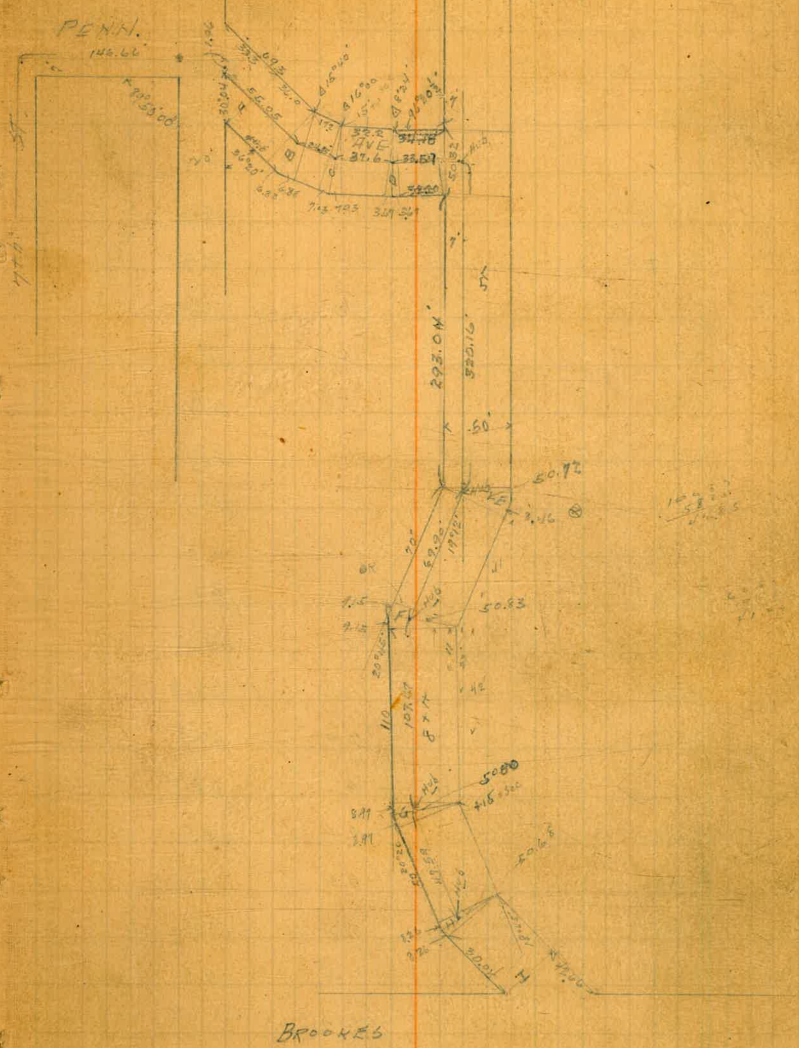


4/6/20 Gregory Moore Miller

CROSS SECTION OF PENNSYLVANIA AVE 50' wide 10' obs.
from Alley East of 7th to W.L. 8th St

Posted 4/30/20

on B.M	0.54	287.40		286.86	B.P. N.W. 6th + Penn
T.P.	0.55	274.87 ✓	13.08	274.32	
			4.51	270.36	spk in Pole Weide Alley
			5.40	269.47	on cb S.S. Penn + Weide Alley
		E. L. Alley			
N			4.6	270.3	
cb			5.0	69.9	
1/4			5.5	69.4	
c			5.5	69.4	
1/4			5.8	69.1	
cb			6.5	68.4	
+8			6.8	68.1	
3			6.3	68.6	
		16.65' E on N.			
c			5.5	69.4	
1/4			5.4	69.5	
cb			5.6	69.3	
+8			9.9	65.0	
N			4.9	70.0	
		18.65' E on N			
N			10.0	64.9	
cb			5.9	69.0	



PENNSYL 2

274.89

33.3' E on N } = SEC. A = (B) on profile
0.0 - 3 }

3		6.3	268.6
+1		6.8	68.1
cb		6.6	68.3
1/2		6.3	68.6
c		6.1	68.8
1/2		6.0	68.9
+5		6.3	68.6
cb		7.8	67.1
N		11.5	63.1
+7		12.8	62.1
	20' E. of SEC. A		
-10		11.5	63.4
N		14.2	60.7
cb		11.2	63.7
1/4		7.0	67.9
c		6.6	68.3
1/2		6.4	68.5
cb		6.4	68.5
+9		7.0	67.9
3		6.4	68.5
	36.1' E on N } = SEC. B = C on profile
42.88 - 3 }		
3		6.4	68.5
+1		7.0	67.9
~~cb~~ cb		6.6	68.3
1/2		6.6	68.3

c		6.8	68.1
TP	5.18	273.15	6.90 267.97
1/4			5.5 67.7
cb			10.9 62.3
N			14.4 58.8
+10			11.0 62.2
	17.2 on N } = SEC. C
31.11 - 3 }		
-15			15.2 58.0
N			18.5 54.7
cb			13.9 59.3
1/4			10.1 63.1
c			5.3 67.9
1/2			5.0 68.2
cb			4.8 68.4
+9			5.2 68.0
3			4.4 68.8
	1.5' E. on N } = SEC.
22.03 E on S }		
3			3.9 69.3
+1			5.0 68.2
cb			4.9 68.3
1/2			4.8 68.4
+1.5			4.6 68.6
c			8.8 64.4
1/4			13.3 59.9
cb			18.0 55.2
N			21.8 51.4

		273.15		
+15		16.8	256.4	256.4
+25		12.7		258.5
	32.2' E of N/ of C 42.9 E of S of C } = SEC D = (G)			
-40		16.3		256.9
-20		22.3		50.9
-10		27.0		46.2
N/		26.0		47.2
cb		22.0		51.2
1/4		15.8		57.4
c		10.0		63.2
1/4		4.7		68.5
cb		5.0		68.2
+60		5.0		68.2
S		3.7		69.5
	19.15' E of D on N/ 22.8 " " " S }			
S		3.9		69.3
+1		4.8		68.4
cb		4.9		68.3
1/4		4.5		68.7
c		9.1		64.1
1/4		15.7		57.5
cb		22.2		51.0
N		27.8		45.4
+15		29.6		43.6
+40		22.3		50.9

	273.2		
	32.7' E of D on N/ 30.82 " " " S } = W. L. of 8th St.		
-55.0		24.9	248.3
-30.0		32.3	40.9
-15		30.9	42.3
N/		23.5	49.7
cb		18.2	55.0
1/4		15.3	57.9
c		9.1	64.1
1/4		4.3	68.9
cb		4.8	68.4
+8		5.3	67.9
S		4.6	68.6

4/7/20 Gregory Moore Miller Shaw

CROSS SECTION OF 8th ST 50' wide 10' obs
N.L. PENNSYLVANIA TO NL. Brookes
273.15

55' N. of NL. Pennsylvania

				-15
W		24.9	248.3	E
cb		27.5	45.7	cb
1/4		30.2	42.8	1/4
c		32.9	40.3	c
1/4		36.4	36.8	1/4
cb		36.6	36.4	cb
E		38.1	35.1	W

30' N of NL. Penn

E		28.5	44.4	W
cb		30.2	43.0	+8
1/4		31.1	42.1	cb
c		32.2	41.0	1/4
1/4		33.2	40.0	c
cb		32.9	40.3	1/4
W		32.3	40.9	cb
				E

15 N. of NL. Penn. Ave

W		30.9	42.3	+10
cb		27.9	45.3	
1/4		26.2	47.0	E
c		24.2	48.8	cb
1/4		22.6	50.6	1/4
cb		22.3	50.9	c
E		22.5	50.7	1/4
+15		21.1	52.1	cb
				+5

4

273.15

No. Line Penn. See sketch

14.2	259.0
13.8	59.4
14.2	58.8
15.5	57.7
18.9	54.3
19.6	53.6
19.9	53.3
23.5	49.7

No. cb

18.2	55.0
17.8	55.4
15.6	57.6
14.2	59.0
12.4	60.8
10.5	62.7
9.5	63.7
8.9	64.3
10.3	62.9

No. Quarter

4.0	69.2
4.1	69.1
6.3	67.9
7.5	65.4
10.0	63.2
12.3	60.9
14.2	59.0

273.15

W		15.3	57.9
	Center Penn.		
W		9.1	264.1
+5		8.9	264.3
cl-		5.7	67.5
1/4		4.3	68.9
c		4.0	69.2
1/4		4.1	69.1
cl-		4.0	69.2
E		3.7	69.5
	So. Quarter.		
E		3.9	69.3
cb		4.2	69.0
1/4		4.4	68.8
c		4.3	68.9
1/4		4.4	68.8
cl-		4	69.2
W		4.3	68.9
	S. cb.		
W		4.8	68.4
cb		4.6	68.6
1/4		4.5	68.7
c		4.6	68.7
1/4		4.5	68.7
cb		4.3	68.9
E		3.9	69.3

273.15

	S cb + 8		
W		5.3	267.9
cb		5.0	68.2
	S. L. Pennsyl.		
E		3.9	69.3
cl-		4.3	68.9
1/4		4.3	68.9
c		4.2	69.0
1/4		4.8	68.4
cb		5.1	68.1
W		4.6	68.6
T.P.	2.15 273.16	3.14	270.01.5
	50' So.		
W		1.3	70.9
+1		2.2	70.0
cb		2.1	70.1
1/4		2.2	70.0
c		2.0	70.2
1/4		2.1	70.1
cb		2.3	69.9
+1		1.8	70.4
E		1.6	70.6
	100' S.		
E		0.8	71.4
+8		0.8	71.4
cb		1.3	70.9

272.16

1/4	1.2	271.0	
c	1.2	71.0	
1/4	1.4	70.8	
cb	1.6	70.6	
+9	1.6	70.6	
W	1.2	71.0	
	108.4' S = ctr ox 4' walk to house on East		
E	0.18	71.18 on cement.	
E	139.4' S = ctr ox 6' walk to house on East		
	150' S. 0.05	71.11	
W	1.4	70.8	
sh +9	1.3	70.9	
cb	1.7	70.5	
1/4	1.4	70.8	
c	1.1	71.1	
1/4	1.3	70.9	
sh	1.3	70.9	
+1	0.8	71.4	
E	0.6	71.6	
	160.8' S. = Approach to Garage on E		
E	0.25	71.91 on cement	
	200' S.		
E	0.8	71.4	
+9	1.0	71.2	
cb	1.7	70.5	
1/4	1.4	70.8	
c	1.3	70.9	

1/4	1.7	270.5	
cb	1.8	70.4	
+1	1.6	70.6	
W	1.6	70.6	Larr. 3 higher
250' S			
W	1.8	70.4	
+9	2.0	70.2	
cb	2.5	70.7	
1/4	2.0	70.2	
c	1.8	70.4	
1/4	2.0	70.2	
cb	2.1	70.1	
+1	1.6	70.6	
E	1.5	70.7	
285' S			
E	1.4	70.8	
cb	2.3	69.9	
1/4	3.0	69.2	
c	2.9	69.3	
1/4	2.8	69.4	
cb	3.0	69.2	
+5	3.4	68.8	
W	2.5	69.7	
293.0 [6.0 W / 301.5 " " E] = SEC. E			
W	3.6	68.6	
cb	3.3	68.9	

N 7 W. 16

1/2		3.7	269	0
c		3.5	68	7
1/2		3.4	68	8
+4		1.8	70	4
cb		1.9	70	3
E		1.5	70	7
	26' S. on W 34 46' " E			
E		2.5	69	7
cb		2.7	69	5
1/2		3.0	69	2
+4		3.1	69	1
c		5.0	67	2
1/2		4.9	67	3
cb		4.9	67	3
W		4.5	67	7
	? 41' S. 0 x E on W ~~34 46~~ " " " E			
W	49.46 on E	5.5	66	7
cb		5.9	66	3
1/4		6.0	66	2
c		6.1	66	1
+3.5		3.7	68	5
1/2		3.6	68	6
cb		3.5	68	7
E		3.2	69	0

8th S.T. 7

272.16

60.35 S. on W
78.46 " E } = SEC. F

E	4.1	268	1
cb	4.7	67	5
1/4	5.1	67	1
+3.5	7.9	64	3
c	7.9	64	3
1/2	7.8	64	4
cb	7.5	64	7
W	7.1	65	1
70' S. on W 78.46 " E } = SEC. F			
W	7.9	64	3
cb	8.1	64	1
1/2	8.1	64	1
c	8.2	64	0
1/2	7.1	65	1
cb	4.9	67	3
E	4.1	68	1
20.15 S. on W 11' " E			
E	4.5	67	4
cb	6.1	67	8
+1	8.2	64	0
1/2	8.6	63	6
c	8.5	63	7
1/2	9.5	62	7
cb	9.9	62	3
W	9.8	62	4

wall = 6.4 ok

		27214				
		16' S. of last X Section				
W			12.0	260 2		
cb			11.9	60 3		
1/4			11.1	61 1		
c			9.7	62 5		
1/4			8.7	63 5		
cb			8.6	63.6	in driveway ctr. walk line	
E			8.5	63.7	in driveway	
S. Pillar 6' N. of this section			15' S. of last X Section			
E			8.3	63.9	on lawn	
cb			8.4	63.8		
1/4			8.8	63.4		
+5			9.1	63.1		
c			11.1	61.1		
1/4			13.3	58.9		
cb			13.7	58.5		
W			13.5	58.7		
T.P.	0.13	259.57	12.72	259.44		
		110' S. of Sec. F on W 91.88' " " " " E = SEC. G.				
W			8.1	51.5		
cb			8.4	51.1		
1/4			8.6	51.0		
+3			8.3	51.3		
c			3.0	56.6		
1/4			+0.8	60.4		
cb			+3.4	64.0		

		259.57		
E			+4.2	263 8
		15' S. on E 23.97' " W		
E			+4.0	63 6
cb			1.5	58 1
1/4			3.7	55 9
c			8.8	50 8
1/4 + 5			11.5	48 1
1/4			11.6	48 0
cb			11.6	48 0
W			11.2	48 4
T.P.	0.77	247.82	12.52	247.05
		50' S. on W of G 32.77' " " E " G } = SEC H.		
W			2.6	45 2
cb			2.3	45 5
1/4			2.8	45 0
c			2.8	45 0
1/4			+3.8	51 6
cb			+5.8	53 6
E			+9.1	56 9
		30.0' S. on E 38.3' " " W } = SEC. I		
E			+2.9	50 7
cb			+0.4	48 2
1/4			6.7	41 1
+2			7.6	40 2
c			7.6	40 2
1/4			7.3	40 5

8th St

		~47.8~			
c.b			7.~	240.6	
W			7.1	40.7	on road
		N.L. Brookes			
W			7.1	40.7	
c.b			8.~	39.6	on road
I/C			9.0	38.8	
C			9.9	37.9	
I/C			10.7	37.1	
c.b			8.~	39.6	
E			6.9	40.9	
T.P	12.64	~60.16	0.30	~47.5~	
T.R	1~.04	~47.06	0.14	~60.~	
T.R	11.1~	~48~.03	1.15	~70.91	
T.P.	8.84	388.76	~.11	~79.9~	
chk B.M.			1.88	386.88	NW 6th & Penn = ~56.56

Posted 4/30/01

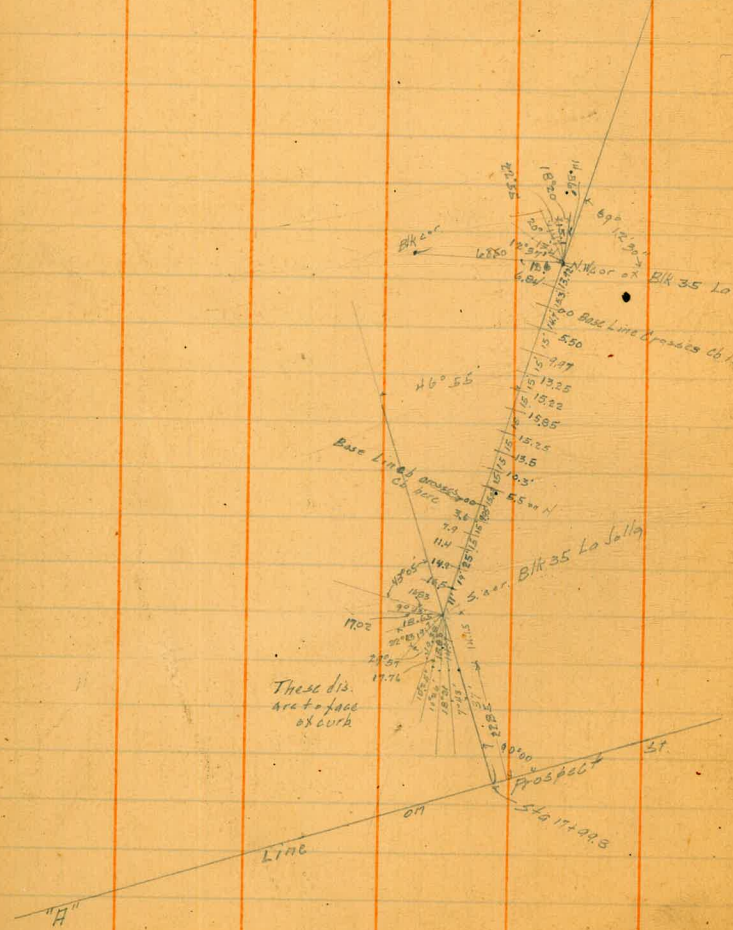
990 × 20 = 19,800 □'

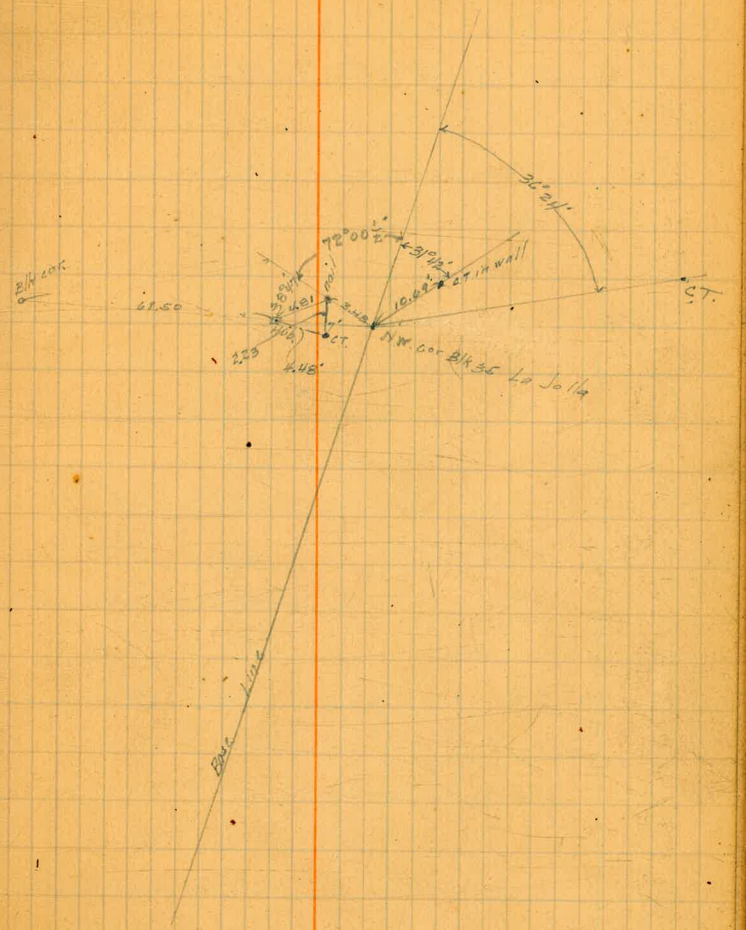
+ ~200 □' at Junction of Kearny

Total ~20,000 □'

5/10/20 Gregory Moore Miller

Location of Curb on N. side
CUVIER ST
from Prospect to Coast Blvd





1-19-20
Gregory
Miller
Shaw

X section of Alley in BLK 10 BROOKES ADD. 15' wide
running from Brookes St to Pennsylvania Ave between 1st & 3rd

on BM	2.18	281.52	279.34	B.P. N.W. 3rd & Penn.

S. Cb. L. Pennsylvania

E		6.5	275.00	on c.b.
W		6.95	274.57	" "

S. L. Penn.

W		6.4	275.1	= W. edge cem walk
+2.0		6.4	275.1	= E " " "
C		6.7	274.8	
E		6.0	275.5	

10' S

E	3.9	277.6	
+3.5	5.3	276.2	
C	5.7	275.8	
+5.5	5.6	275.9	
+5.5	5.3	276.2	= E edge walk
W	5.3	276.2	= W " "

50' S = 3 End 2 walk on W.

W	4.9	276.6	= W " "
+W	4.9	276.6	= E " "
C	4.7	276.8	
E	3.9	277.6	

63' S = center of 14' door

E-3.6 = edge of runway to garage	4.0	277.5	

V. 73' S = center of 16' cement runway.

5.1 W. of C = edge of runway to garage	4.1	277.4	
4' " " " = garage door.	4.8	276.7	= floor

281.52

80' S = center of 4' walk to house

E	3.3	278.2	= top of walk

102' S = center of 2' walk to house

W-1.0	4.0	277.5	= top of walk
W	3.8	277.7	
C	3.9	277.6	
E fence .3 in alley	3.5	278.0	

110' S. = center of 8' cement runway to garage

T.P. 5.11 282.90	3.73	277.79	
3.0 E. of E.L. = edge of cement runway	4.8	278.1	

111.5' S = center of 13' cement runway

3.8 W. of W.L. Alley = front of garage	5.2	277.7	= floor.
W.L.	5.2	277.7	on cement
1' E of W.L. = edge of runway	5.1	277.8	" "

150' S

E	4.0	278.9	
C	4.1	278.8	
W	4.3	278.6	

172' S = center of 12' garage door

0.5 W. of W.L. = Edge of wood floor	3.6	279.3	on floor

192' S = center of 9' garage door

0.5 W. of W.L. = Edge of wood floor	3.6	279.3	on floor

200' S

W	3.4	279.5	
C	3.2	279.7	
E fence 0.5' in alley	3.0	279.9	

218' to 250' is a plaster house on E 0.5 in alley.

		226'5 = center of 3' walk to house		
0.4 W of W.L = End of walk.		3.2	279.7	on walk
T.P.	4.61	284.58	2.93	279.97
		240'5 = center of 9' cement runway		
7.5 W of WL Alley = edge of garage runway.		5.4	279.2	
		250'5		
E		4.4	280.2	
C		4.7	279.9	
W		4.8	279.8	
		300'5		
W		5.3	279.3	
C		5.0	279.6	
E fence 0.5 in alley		4.3	280.3	
		343'5 = center of 8' garage door		
3' E of E.L. = garage dirt floor		6.5	278.1	
E		6.5	278.1	
C		6.6	278.0	
W		6.5	278.1	
		368.5 = center of 8' cement runway		
3' E of E.L.		7.0	277.6	edge
1' E - - - = edge of cement		7.2	277.4	
T.P. = nail in pole 0.70	4.75.95	9.33	275.25	
		385'5		
W		0.0	276.0	
C		0.0	276.0	
		0.0	276.0	

275.95

400'5

E	1.6	274.4	
C	1.2	274.8	
W = Edge of garage. Entrance is ^ Toward the north	1.3	274.7	= same as floor
430'5			
W	3.9	272.1	
C	2.9	273.1	
E	4.3	271.7	
443'5			
E	5.2	270.8	
C	5.2	270.8	
W =	6.1	269.9	1st floor of House = same as ^
450'5			
4' W of W.L. = door to basement of House 1st Floor = 11.5		264.5	
W	11.5	264.5	
C	8.3	267.2	
E	10.9	265.1	
+15'	11.0	265.0	
463'5			
-15	11.8	264.7	
E	11.4	264.6	
C	13.3	262.7	
465'5 = 5' E of E of House on W.			
-15'	13.3	262.7	
E	14.6	261.4	
C	13.3	262.7	
W	14.3	261.7	
+32 = under pinning of House	14.4	261.6	

FOR CORRECT SECTIONS SEE PAGE 62

+20	14.6	261.4 ✓
	476' S = S. End of Dog House	
-25	19.5	256.5 ✓
-3.5 = Edge of Dog House.	19.5	256.5 ✓
W	17.5	258.5 ✓
C	19.0	257.0 ✓
3' E of C	15.0	261.0 ✓
E	14.6	261.4 ✓
+15	13.6	262.4 ✓
	484' S. = Site of Necessary pipe at E	
-15	13.8	262.2 ✓
E	14.6	261.4 ✓
4' W of E.L.	15.0	261.0 ✓
C	17.2	258.8 ✓
W	22.8	253.2 ✓
+4	22.8	253.2 ✓
+25	23.8	252.2 ✓
+30	22.5	253.5 ✓
	492' S.	
-30	26.0	250.0 ✓
-10	23.9	252.1 ✓
W	20.0	256.0 ✓
C	15.9	260.1 ✓
E	14.7	261.3 ✓
+15	13.7	262.3 ✓

SEE PAGE 62

	499' S.	
-15	5.9	270.1 ✓
E	9.5	266.5 ✓
C	10.2	265.8 ✓
	500' S. Make outlet pt. 1's to this.	
E	8.4 ✓	267.6 ✓
C	8.7	267.3 ✓
2' W of C	14.3	261.7 ✓
W.	18.3	257.7 ✓
+15	24.4	251.6 ✓
+30	29.0	247.0 ✓
	512' S.	
-30	26.2	249.8 ✓
-15	20.0	256.0 ✓
- ✓	15.7	260.3 ✓
W	13.2	262.8 ✓
2' W of C	7.5	268.5 ✓
C	6.8	269.2 ✓
5' E	5.8	270.2 ✓
E.L.	4.6	271.4 ✓
	519' S. = N. End of garage. Entrance toward S.	
E	4.2	271.8 ✓
1.5' W. of E.L.	4.9	271.1 ✓
C	5.5	270.5 ✓
3' W. of C	5.6	270.4 ✓
W.	8.0	268.0 ✓
+3 = NE cor garage	10.6	265.4 ✓
+15	14.4	261.6 ✓

SEE PAGE 62

275.95

530 S =

W	see page 62		5.6	270.4 ✓
C			5.3	270.7 ✓

550 S = S. End of garage on W.

-3' = edge of garage Entrance to South

W			4.8	271.2 ✓
			4.9	271.1 ✓
C			4.9	271.1 ✓
E			4.6	271.4 ✓

599.7 = N.L. Brookes

E			4.5	271.5 ✓
C			4.9	271.1 ✓
W			4.8	271.2 ✓

N. cb Line Brookes

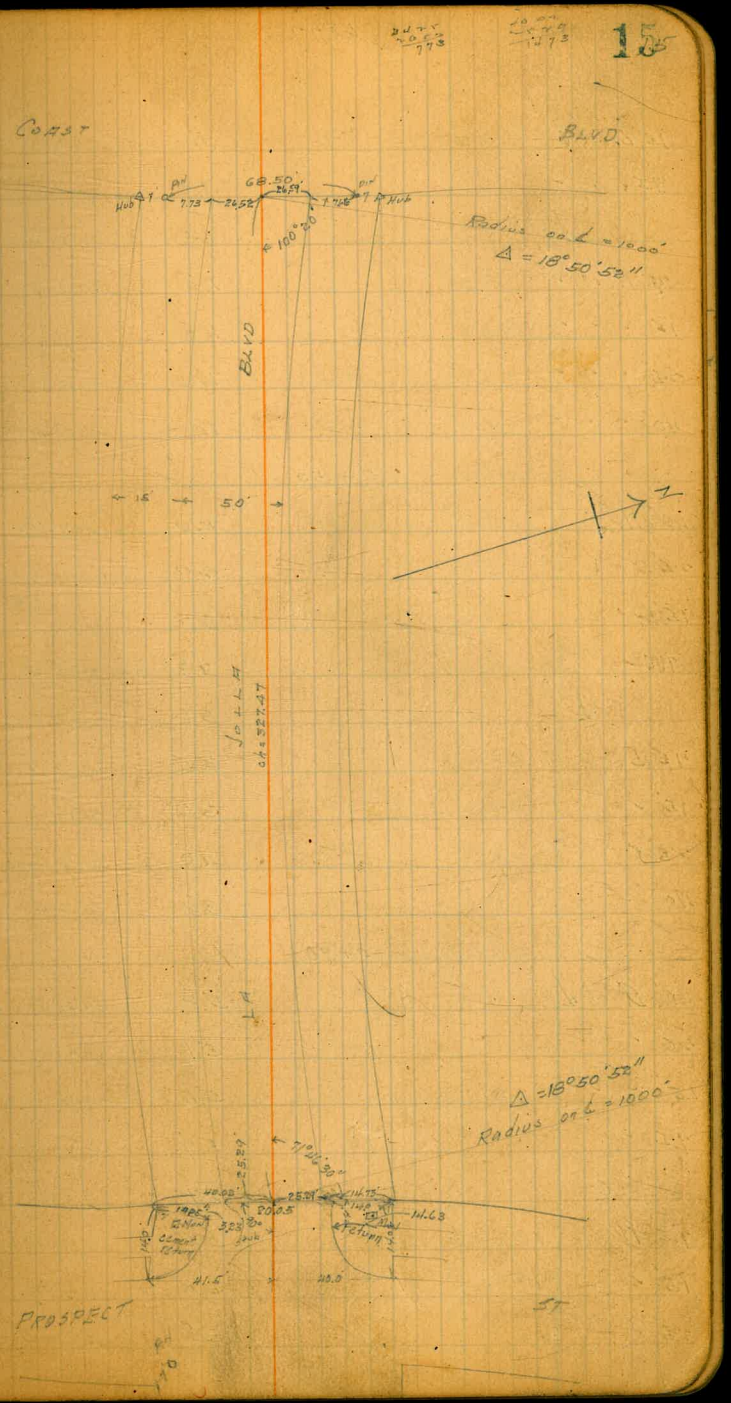
W			5.10	27085 ✓	on curb
E	8.00	279.13	4.52	271.43 ✓	✓ ✓
B.P. NW 3rd & Brookes			2.16	277.27	277.27

1/19/21 Gregory

Cross Section of La Jolla Blvd from Prospect to Coast

25' Each Side of the ℄ of La Jolla 10' obs.

B.M	0.77	68.77 ✓		68.00	NE Prospect + La Jolla
		W. L. of Prospect.			
40' S. of ℄			0.50	68.27 ✓	on cement
25' S. " "			0.8	68.0 ✓	
25' S " "			1.35	68.00	= return
15' " "			0.92	67.42 ✓	on pave.
7.5' "			0.79	67.85 ✓	" "
℄			0.72	67.98 ✓	" "
7.5' N. of "			0.91	68.05 ✓	" "
15' " " "			1.10	67.86 ✓	" "
25' " " "			1.58	67.67 ✓	" "
25.7 " " "			0.79	67.19 ✓	" "
40' " " "			0.6	67.98 ✓	
		7.95 W. on S.	3.97		
		0.0 " " N.	= 0+00	on ℄	
25' N. of ℄			1.6	67.97 ✓	
15' " "			1.1	67.7 ✓	
7.5 " "			1.1	67.8 ✓	
℄			1.0	67.8 ✓	
7.5 S. of "			1.1	67.7 ✓	
15' " " "			1.2	67.6 ✓	
25' " " "			1.0	67.8 ✓	
40' " " "			1.0	67.8 ✓	
		0+20 on ℄			
40' S. of ℄			1.5	67.3 ✓	at house
25' " " "			1.5	67.3 ✓	



	68.77			
15' S. of ℄		1.6	67.2 ✓	
7.5 ✓		1.7	67.1 ✓	
℄		1.9	66.9 ✓	
7.5 N. of ✓		1.8	67.0 ✓	
15' ✓		1.5	67.3 ✓	
25' ✓		1.1	67.7 ✓	
40' ✓		1.1	67.7 ✓	
	0+50			
40' N.		2.0	68.8 ✓	
25' ✓		2.7	66.1 ✓	
15' ✓		3.2	65.6 ✓	
7.5 ✓		3.3	65.5 ✓	
℄		3.6	65.2 ✓	
7.5 S		3.5	65.3 ✓	
15' ✓		3.6	65.2 ✓	
25' ✓		4.0	64.8 ✓	
40' ✓		3.8	65.0 ✓	garage door
	0+70			
40' S. of ℄		5.4	63.4 ✓	garage door
25' ✓ ✓		5.1	63.7 ✓	
15' ✓ ✓ ✓		5.6	63.2 ✓	
7.5 ✓		5.7	63.1 ✓	
℄		5.7	63.1 ✓	
7.5 N		5.4	63.3 ✓	
15' ✓		5.6	63.2 ✓	
25 ✓		4.8	64.0 ✓	

40' N.		3.3	65.5 ✓	
	1+00			
40' N		10.1	58.7 ✓	
25' ✓		10.1	58.7 ✓	
15' ✓		10.0	58.8 ✓	
7.5' ✓		10.5	58.3 ✓	
℄		11.2	57.6 ✓	
7.5' S		10.8	58.0 ✓	
15' S		10.8	58.0 ✓	
25' S		10.5	58.3 ✓	
40' S		10.8	58.0 ✓	on House S.W
T.P. 053 · 56.23 ✓		13.07	55.70 ✓	
	1+25			
40' S		4.2	52.0 ✓	
25' ✓		4.0	52.2 ✓	
15' ✓		3.6	52.6 ✓	
7.5 ✓		3.6	52.6 ✓	
℄		3.8	52.4 ✓	
7.5' N		3.0	53.2 ✓	
15' ✓		2.6	53.6 ✓	
25' ✓		2.8	53.4 ✓	
40' ✓		2.9	53.3 ✓	
	1+50			
40' N		8.3	47.9 ✓	
25' ✓		7.4	48.8 ✓	
15' ✓		7.6	48.6 ✓	

		56.23		
7.5' N.			7.6	48.6 ✓
℄			8.6	47.6 ✓
7.5' S			8.5	47.7 ✓
15' ✓			8.4	47.8 ✓
25' ✓			8.5	47.7 ✓
40' ✓			9.3	46.9 ✓
T.P.	2.07	45.55 ✓	12.75	43.48 ✓
		2+00		
40' S			2.7	42.9 ✓
25' ✓			2.4	43.2 ✓
15' ✓			2.1	43.5 ✓
7.5' ✓			2.1	43.5 ✓
℄			2.2	43.4 ✓
7.5 N			0.8	44.8 ✓
15' ✓			1.5	44.1 ✓
25' ✓			0.0	45.6 ✓
40' ✓			0.0	45.6 ✓
		2+24		
40' N			2.2	43.4 ✓
25' ✓			3.4	42.2 ✓
15' ✓			3.5	42.1 ✓
		2+25		
40' N			2.3	43.3 ✓
25' ✓			6.3	39.3 ✓
24' ✓			3.5	42.1 ✓
15' ✓			3.6	42.0 ✓

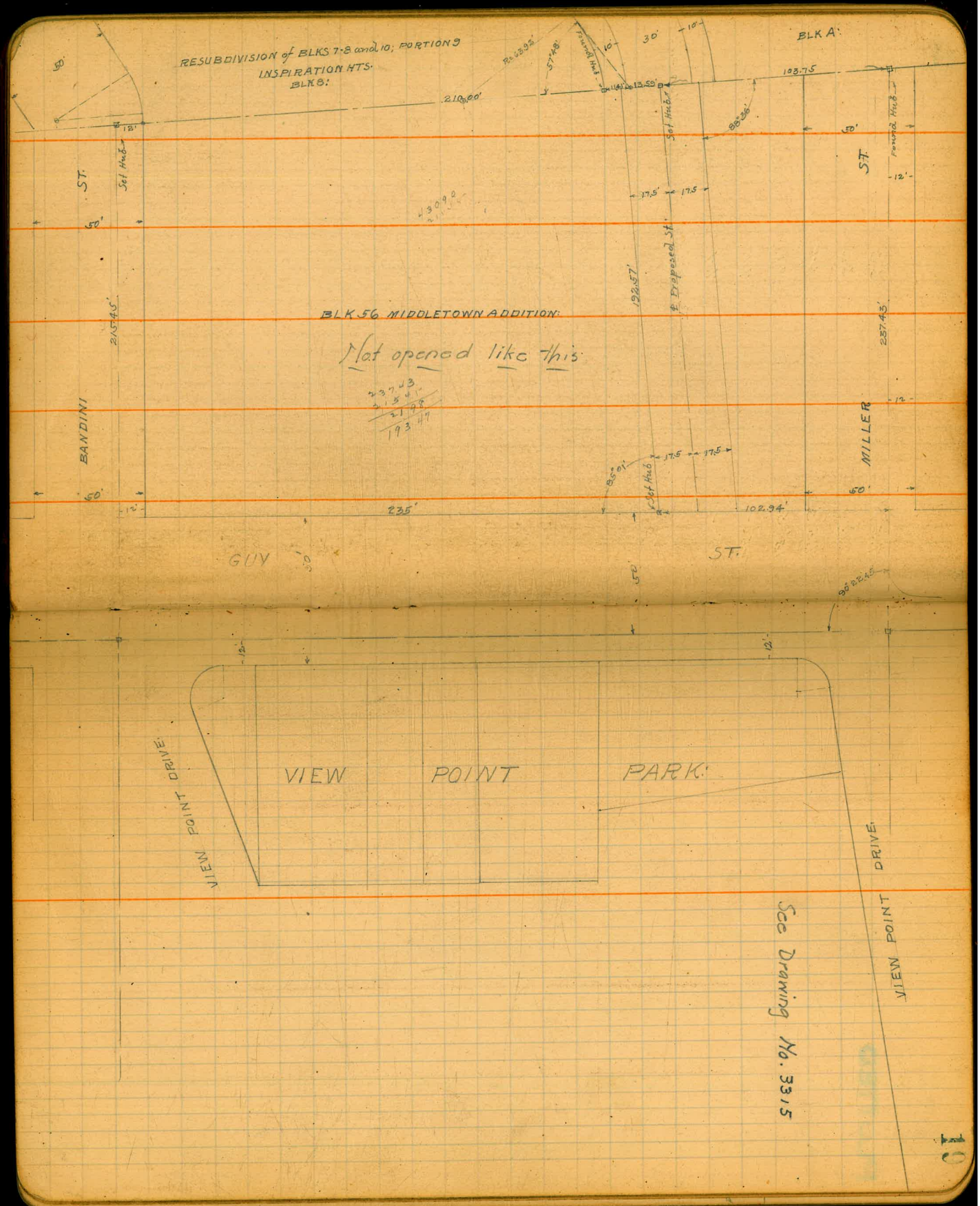
7.5' N	4.0	41.6 ✓	
℄	5.1	40.5 ✓	
7.5' S	5.2	40.4 ✓	
15' ✓	5.4	40.2 ✓	
25' ✓	5.8	39.8 ✓	
40' ✓	6.6	39.0 ✓	
2+40			
40' North	4.0	41.6 ✓	
27' ✓	4.7	40.9 ✓	
25' ✓	7.1	38.5 ✓	
19' ✓	7.1	38.5 ✓	
17' ✓	5.6	40.0 ✓	
15' ✓	5.5	40.1 ✓	
2+50			
40' S	9.3	36.3 ✓	Front yard
25' ✓	8.4	37.2 ✓	
15' ✓	7.9	37.7 ✓	
7.5' ✓	8.0	37.6 ✓	
℄	8.3	37.3 ✓	
2' N	7.0	38.6 ✓	
7.5' ✓	6.7	38.9 ✓	
13.5' ✓	6.9	38.7 ✓	
15' ✓	7.9	37.7 ✓	
21' ✓	8.0	37.6 ✓	
22' ✓	6.3	39.3 ✓	
25' ✓	5.6	40.0 ✓	
40' ✓	4.9	40.7 ✓	

		45.55		
		2+75		
40' N			7.6	38.0 ✓
25' ✓			8.4	37.2 ✓
15' ✓			8.8	36.8 ✓
7.5' ✓			9.7	35.9 ✓
℄			9.3	36.3 ✓
1' S			10.2	35.4 ✓
7.5' ✓			10.1	35.5 ✓
15' ✓			10.3	35.3 ✓
25' ✓			10.4	35.2 ✓
40' ✓			11.6	34.0 ✓
T.P.	2.78	37.21 ✓	11.12	34.43 ✓
		3+00		
40' S			5.2	32.0 ✓
25' ✓			4.5	32.7 ✓
15' ✓			4.1	33.1 ✓
7.5' ✓			3.8	33.4 ✓
℄			3.5	33.7 ✓
7.5 N			2.5	34.7 ✓
15' ✓			2.1	35.1 ✓
25' ✓			1.9	35.3 ✓
40' ✓			1.4	35.8 ✓

29.10 on ℄ { 32.10 W of Last Sec on S. / 26.11' " " " N. S. L. of Coast Blvd.

40' N			6.1	31.1 ✓
25' ✓			6.3	30.9 ✓
15' ✓			6.2	31.0 ✓

7.5' N	6.3	30.9 ✓
℄	6.4	30.8 ✓
7.5' S	6.7	30.5 ✓
15' S	8.1	29.1 ✓
25' ✓	7.1	30.1 ✓
40' ✓	7.9	29.3 ✓
	7.66	29.55 ✓ hub SW cor


RESUBDIVISION of BLKS 7-8 and 10; PORTION 9
INSPIRATION HTS.
BLK 8:
BLK A:
210.00'
103.75'
50'
12'
Set Hub
Found Hub
ST.
50'
17.5'
17.5'
Proposed St.
192.57'
257.43'
BLK 56 MIDDLETOWN ADDITION:
Not opened like this
BANDINI
MILLER
60'
235'
102.94'
GUY
ST.
VIEW POINT PARK:
VIEW POINT DRIVE
See Drawing No. 3315

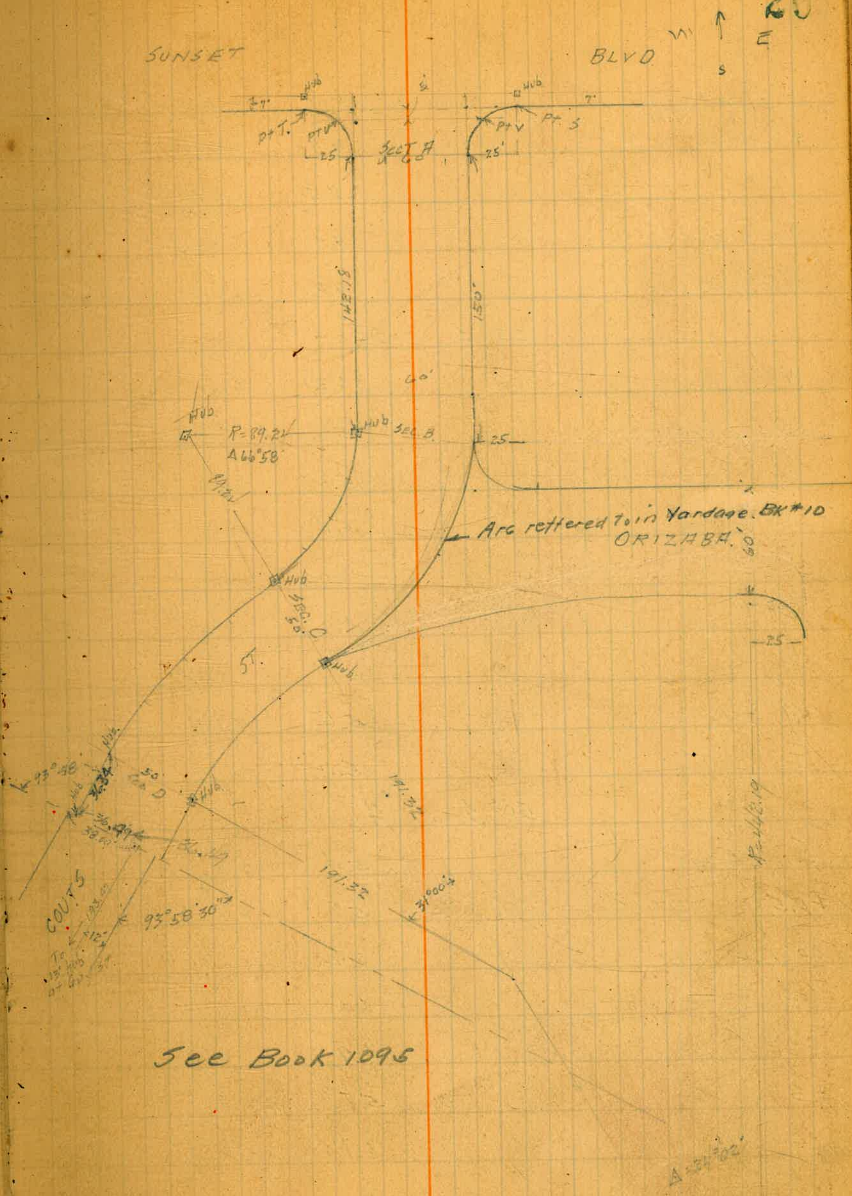
6/26/21 Gregory / Moore / Miller / Shaw

Cross Section of Couts St from SL Sunset Blvd To Middletown Add Line

Widths as shown on sketch. 10' cbs. on both widths. 10'/4's on 60'. 7.5'/4's " 50'. Mon

PLOTTED

	2.06	284.96		282.90
	5.15	278.26	11.85	273.11
S. L. Sunset Blvd				
E. End of East Curve = PT S			4.6	73.7
20' W of Above			5.3	73.0
25' " " Pt 3 = E.L. of St produced			6.3	72.0
E. 1/4 = 20' from last above			7.1	71.2
℄ of St produced			7.5	70.8
W 1/4			7.7	70.6
W.L. of St produced N.			8.3	70.0
W End of W. Curve = PT T.			9.1	69.2
5' S				
Int. of W Curve & 5' S. of SL Sunset = Pt V			7.9	70.4
W.L. of St produced			7.0	71.3
W. 1/4 " "			6.5	71.8
℄ of "			5.5	72.8
0.5 E of ℄			7.5	70.8
E 1/4 of St "			6.7	71.6
E.L. " "			5.8	72.5
3' E of E.L. "			4.1	74.2
Pt V			3.5	74.8
Sect A = 25' S. of Sunset Blvd. 60' wide				
E			5.9	72.4
℄			5.9	72.4
W			5.9	72.4



See Book 1095

278.26

c	6.3	72.0
+1	4.9	73.4
1/4	5.5	72.8
cb	5.7	72.6
W	6.3	72.0

25' S. of SECT A.

W	6.2	72.1
cb	5.8	72.5
1/4	5.3	73.0
+9	5.4	72.9
c	6.2	72.1
1/4	6.0	72.3
cb	5.9	72.4
+9	5.6	72.7
E	5.2	73.1

50' S. of "A"

E	5.4	72.9
+0.5	5.8	72.5
cb	6.2	72.1
1/4	6.6	71.7
c	6.9	71.4
+3	5.8	72.5
1/4	6.1	72.2
cb	6.2	72.1
W	6.4	71.9

75' S. of A

W	8.1	70.2
cb	7.2	71.1
1/4	7.0	71.3
+7	6.6	71.7
c	7.5	70.8
1/4	7.4	70.9
cb	6.8	71.5
+9.5	6.6	71.7
E	6.1	72.2

100' S. of A"

E	5.9	72.4
+1	7.7	70.6
cb	7.8	70.5
1/4	8.1	70.2
c	8.2	70.1
1/4	8.2	70.1
cb	8.9	69.4
W	8.7	69.6

125' S. of A"

W	10.1	68.2
cb	9.7	68.6
1/4	9.5	68.8
c	9.0	69.3
1/4	9.0	69.3
cb	8.7	69.6

+8			8.4	69.9
E			7.2	71.1
		142.18' on W, 150' " E	3.0 x A = Sect B	
E			9.5	68.8
cb			9.8	68.5
1/4			10.0	68.3
C			10.0	68.3
1/4			10.3	68.0
cb			11.0	67.3
W			10.7	67.6
		26.08' 3.0 on W, 31' on E		
W			11.8	66.5
cb			11.5	66.8
+9.5			11.4	66.9
+19.0			11.0	67.3
+47.5			10.3	68.0
T.P.	1.69	267.58	12.37	265.89
		52.16' 3.0 x "B" on W		
55' E. of W.L.			0.9	266.7
35 " " "			2.6	65.0
27.5 " " "			2.7	64.9
18 " " "			2.2	65.4
10 " " "			1.9	65.7
W.L.			1.6	65.8

78.2W 3.0 x B on W.

W	3.4	64.2
cb	3.7	63.9
18' E of W.L.	4.0	63.6
76' " " "	4.6	63.0
52.5 " " "	4.9	62.7
104.32' 3.0 x B on W = SECT C 5T 50' WIDE		
E	6.5	61.1
cb	6.0	61.6
1/4	5.7	61.9
C	5.2	62.4
1/4	4.7	62.9
cb	4.3	63.3
W	3.8	63.8
32.64' 3.0 x C on W		
25.88' " " " E		
W	4.4	63.2
cb	4.3	63.3
1/4	4.8	62.8
C	4.9	62.7
1/4	5.3	62.3
cb	6.0	61.6
E	6.6	61.0
65.28' 3.0 x C on W		
51.76' " " " E		
E	6.9	60.7
cb	6.0	61.6
1/4	5.6	62.0

		467.58		
+2			6.1	61.5 ✓
C			5.7	61.9 ✓
1/4			5.2	62.4 ✓
+2.6			5.8	61.8 ✓
CB			4.9	62.7 ✓
W			4.8	62.8 ✓
		97.92' 3.0 x C on W 77.64' ✓ ✓ ✓ E		
W			6.0	61.6 ✓
CB			6.0	61.6 ✓
1/4			6.0	61.6 ✓
+7			6.2	61.4 ✓
C			7.5	60.1 ✓
1/4			6.9	60.7 ✓
CB			7.4	60.2 ✓
+2			8.2	59.4 ✓
+3			7.5	60.1 ✓
E			8.0	59.6 ✓
		130.54' 3.0 x C on W 103.52' ✓ ✓ ✓ E } = SEC. D		
E			8.7	58.9 ✓
+4			9.0	58.6 ✓
CB			8.1	59.5 ✓
1/4			8.3	59.3 ✓
+2			9.0	58.6 ✓
+3			7.5	59.8 ✓
C			7.7	59.9 ✓
1/4			7.4	60.2 ✓

COUTS

10.17

CB		7.5	60.1 ✓
W		7.8	59.8 ✓
	36.82' 3.0 on W 33.50' ✓ ✓ E } = MIDDLETOWN ADD LINE		
W		10.2	57.4 ✓
CB		10.3	57.3 ✓
1/4		10.3	57.3 ✓
C		10.2	57.4 ✓
+1.6		10.1	57.5 ✓
1/4		11.3	56.3 ✓
+2		10.6	57.0 ✓
CB		10.1	57.5 ✓
+7		10.5	57.2 ✓
E		10.0	57.6 ✓

6/16/21 Gregory Moore Miller Shaw

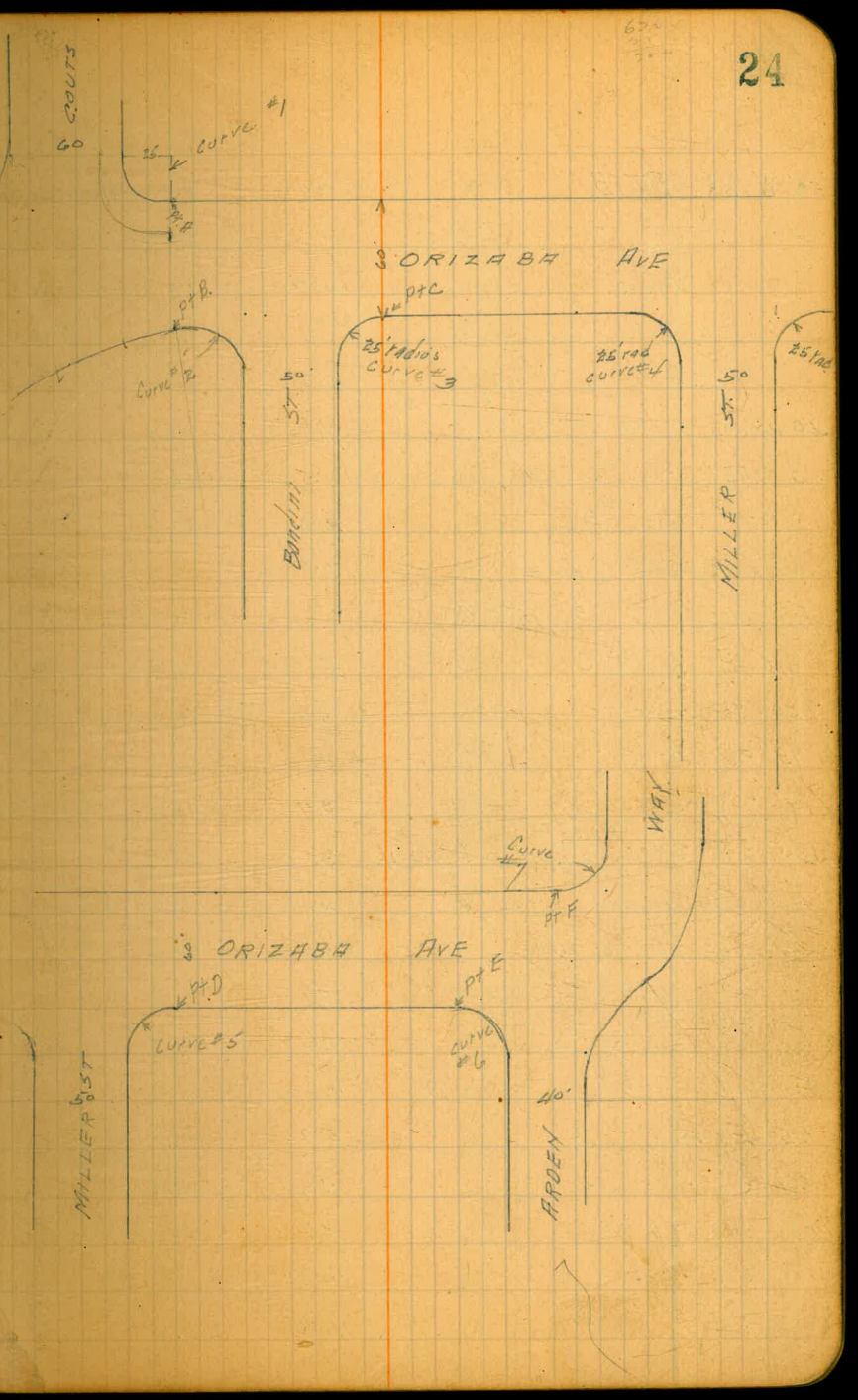
Levels on Dirt Curb
Orizaba St
End to End.

PLOTTED 10.76 279.85 269.09 SE NW Corner Orizaba

Curve #1

N. End.		11.20	68.7
.25 around curve		11.6	68.3
.5 " "		11.7	68.2
.75 " "		11.3	68.6
East End of Curve = Pt. A		10.6	69.3
25' E. of Pt A		9.5	70.1
50' " " "		8.9	71.0
75' " " "		7.8	72.1
100' " " "		6.6	73.3
125' " " "		5.6	74.3
150 " " "		4.9	75.0
175' " " "		4.3	75.6
200' " " "		3.8	76.1
225 " " "		3.4	76.5
250 " " "		3.5	76.4
275 " " "		3.7	76.2
300 " " "		4.0	75.9
325 " " "		4.7	75.2
350 " " "		5.6	74.3
375' " " "		6.6	73.3
400' " " "		8.0	71.9
425' " " "		9.6	70.3
450' " " "		11.3	68.6

Fillon North Curb



279.85

50' W of Pt B.	Curb S. S. side	12.2	67.7	✓
75' " " "		11.5	68.4	✓
Pt. B.		10.7	69.2	✓
Pt. B	Curve #2	10.7	69.2	✓
.50 around curve #2		9.8	70.1	✓
S. end " #2		10.5	69.4	✓
" " " #3		9.9	70.0	✓
Halfway around curve #3		7.9	72.0	✓
E. End Curve #3 = Pt C.		6.6	73.3	✓
75' E of Pt C		5.6	74.3	✓
50' " " "		4.6	75.3	✓
75' " " "		4.1	75.8	✓
100' " " "		3.7	76.2	✓
130' " " " = W. end of Curve #4		3.2	76.7	✓
Halfway around curve #4		4.0	75.9	✓
S. End Curve #4		5.1	74.8	✓ ✓
" " " #5		5.1	74.8	✓ ✓
Halfway on " #5		4.6	75.3	✓
E. End " #5 = Pt D		4.8	75.1	✓
75' E. of Pt D.		5.9	74.0	✓
50' " " "		7.2	72.7	✓
75' " " "		8.6	71.3	✓
100' " " "		10.4	69.5	✓
T.P.	0.77	268.87	11.75	268.10 ✓

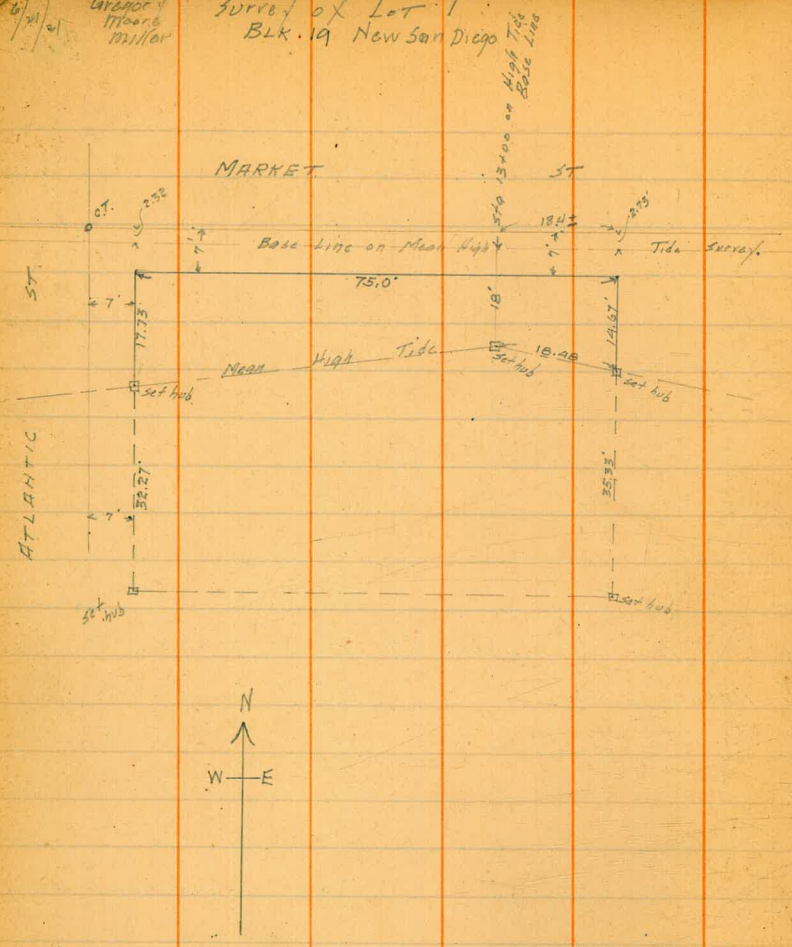
268.87

125' E of Pt D	1.4	67.5	✓
150.75 " " " = Pt E	3.2	65.7	✓
Quarter around curve #6	4.5	64.4	✓
Halfway " " #6	6.1	62.8	✓
.75 " " #6	7.3	61.6	✓
S. End " " #6	7.8	61.1	✓
N. S. side again			
475' E of Pt A	2.4	66.5	✓
500 " " "	4.6	64.3	✓
525 " " "	6.6	62.3	✓
550 " " " = W. End Curve #7	8.9	60.0	✓
.25 around curve #7	9.5	59.4	✓
.50 " " #7	10.4	58.5	✓
.75 " " #7	11.2	57.7	✓
N. End " #7	11.7	57.2	✓
12.83 71.44 on Curb W. side Arden Way & S. Line of Lot 12 Blk 10. Insp. Hghts	10.2C	258.61	✓
	7.9	268.50 = Pt d NW Arguello & Sunset.	

6/21/21

Gregor & Moore Miller

Survey of Lot 1 Blk. 19 New San Diego



[illegible] Gregory Mears Miller

Elevations on Water Main Arctic St

on B.M.	1.27	79.14 ✓		77.87	SE Maple & Indiana
T.P.	0.80	67.14	12.80	66.34	
T.P.	0.43	54.57	13.00	54.14	
T.P.	0.85	43.02	12.40	42.17	
Elev. Top of Main	S. Cb Line	Laurel	10.83	32.19 ✓	
" " " " old	" "	Maple	10.54	32.48 ✓	
T.P.	12.53	55.00	0.55	42.47	
Top of Main	N. Line	Nutmeg (Bell)	8.98	46.02 ✓	
" " "	14' No. of ℄ of	Olive (Bell)	1.46	53.54 ✓	
T.P.	12.24	65.78	1.46	53.54	
Top of Main	45' S. of S.L.	Palm	9.38	56.40 ✓	
Top of Main	18.5 N. of	Palm	9.63	56.15 ✓	
" " "	S. Cb. Line	Quince	9.50	56.28 ✓	
T.P.	0.85	64.81	1.82	63.96	
Top of Main	5.5 S. Cb. Line	Redwood	8.59	56.22 ✓	
T.P.	4.60	56.32	11.09	53.72	
Top of Gate	S.L.	Spruce	4.60	51.72 ✓	
" " Main	N.L.	"	6.55	49.77 ✓	
" " "	S.L.	Sassafras	8.50	47.82 ✓	
T.P.	12.56	68.22	0.66	55.66	
T.P.	10.97	78.72	0.47	67.75	
T.P.	11.11	87.99	1.84	76.88	
chk B.M.			3.16	84.83 – 83	BP SE Indiana & Sassafras
off " "	1.33	46.66		45.32	
Top of Main	10' S. of N.L.	Thorn	9.30	37.35 ✓	
T.P.	4.19	43.87	6.97	39.68	

[illegible]

43.87

Top of Bell S.Cb Line Upas St.			3.70	40.17 ✓	
" " Main North " Vine St.			6.20	37.67 ✓	
T.P.	5.35	46.22	3.00	40.87	
T.P.	11.65	57.25	0.62	45.60	
Top of Main St.		Chalmers	9.25	48.00 ✓	
T.P.	12.24	68.32	1.17	56.08	
Top of Main 16' E. & N. Arctic & Nicobwinder			9.13	59.19 ✓	
T.P.	13.01	79.42	1.91	66.41	
chk B.M.			2.49	76.93 = 77.00	BP SW Indiana & Winder

8/16/24 Gregory Moore Shaw

CROSS SECTION OF Alley in Blk P VALLE VISTA TERRACE 15' wide distances are on ℄

SW Adams Misc. spk

9.98 360.30 350.32

N.L. CLIFF ST = 0+00

W 4.1

(on cement cb 3.98)

C 4.3

E on cement cb 3.92 4 in alley

0+26.6 = S. end of walk running parallel to alley

−0.5 = on edge of walk 2.74

E 3.2

C 3.5

W 3.3

0+50

W 2.8

C 3.2

E 3.0

+0.6 = on edge of walk 2.67

0+68.5 = N. end of walk

−0.6 = on edge of walk 2.49

E 2.8

C 2.9

W 2.7

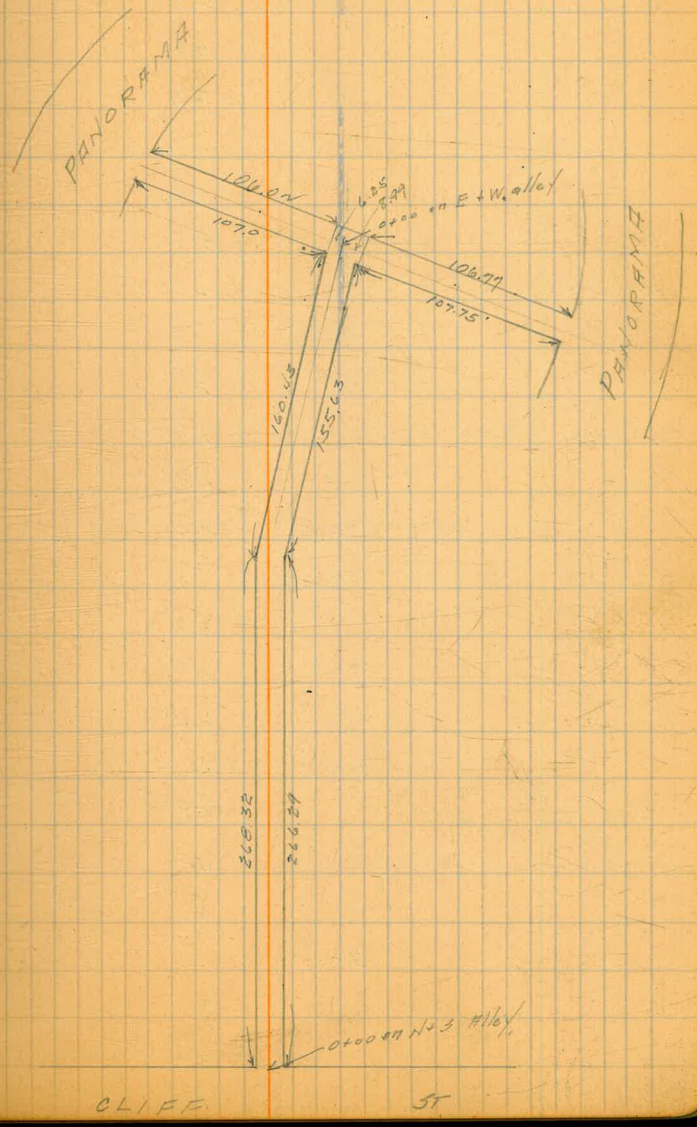
+1.0 = ℄ of walk to house 2.6

1+00

W 2.5

C 2.4

E 2.4



		360.30		
		1+06.80 = center of 8' garage door		
E-5.5 = front of garage dirt fl.				
		1+30		
E			2.3	
C			2.4	
W			2.3	
		1+50		
W			2.2	
C			2.1	
E			2.1	
		2+00		
E			1.6	
C			1.6	
W			1.6	
T.P.	6.20	364.95	1.58	358.75
		2+30		
W			5.8	
C			5.9	
E			6.0	
		2+67.30 = Apt.		
.5 W. of E.L. = fence			5.6	
C			5.8	
W			5.8	
		3+00		
W			5.4	
C			5.3	
+7.1 o fence			5.3	

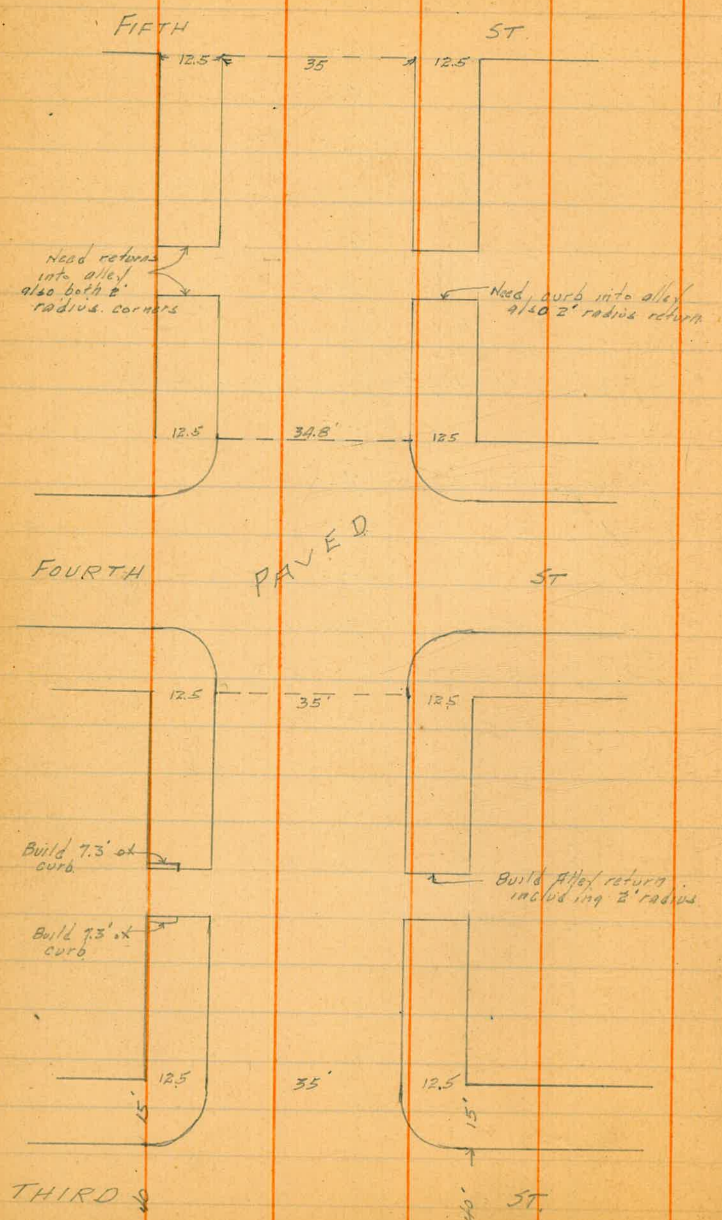
	3+50	
E		5.2
C		5.2
W		5.1
	4+00	
W		4.6
C		4.7
E		4.8
	4+25.3 = P.L. of E + W Alley	
E		4.7
C		4.7
W		4.6
	℄ of N+S Alley = 0+00 on Alley Toward West.	
S		4.7
C		4.5
N		4.4
	0+6.35 = W.L. of N+S alley	
N		4.5
C		4.5
S		4.6
	0+50	
S		4.0
C		4.0
N		4.1

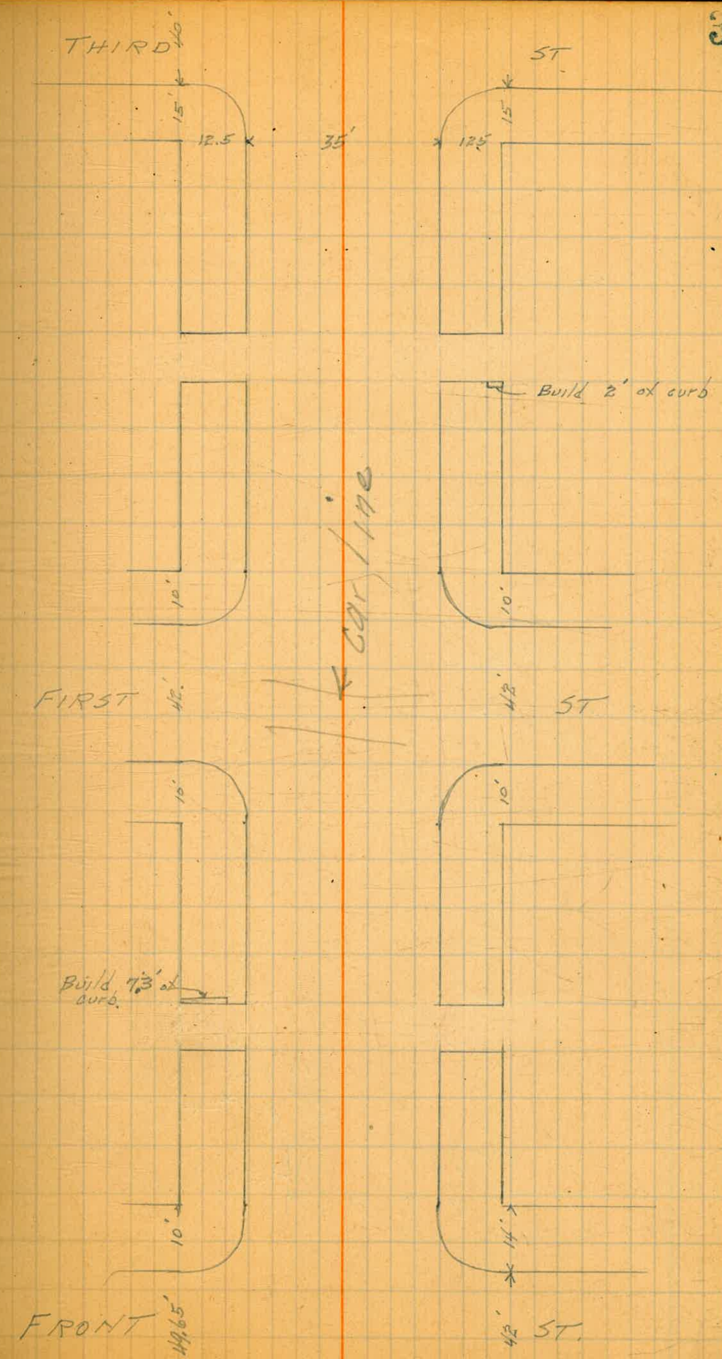
	1+00	
N		4.0
C		4.1
S		4.0
	1+08	
S		4.3
C		4.2
N		4.4
	1+12.76 = E.L. Panorama	
N		5.1
	on cement cb	5.05
C		5.2
	on cement cb	5.06
S		4.8
	℄ of N+S alley = 0+00 Alley toward East	
S		4.7
C		4.5
N		4.4
	0+8.99 = E.L. of N-S alley	
N		4.5
C		4.5
S		4.7
	0+50	
S		5.3
C		5.3
N		5.3

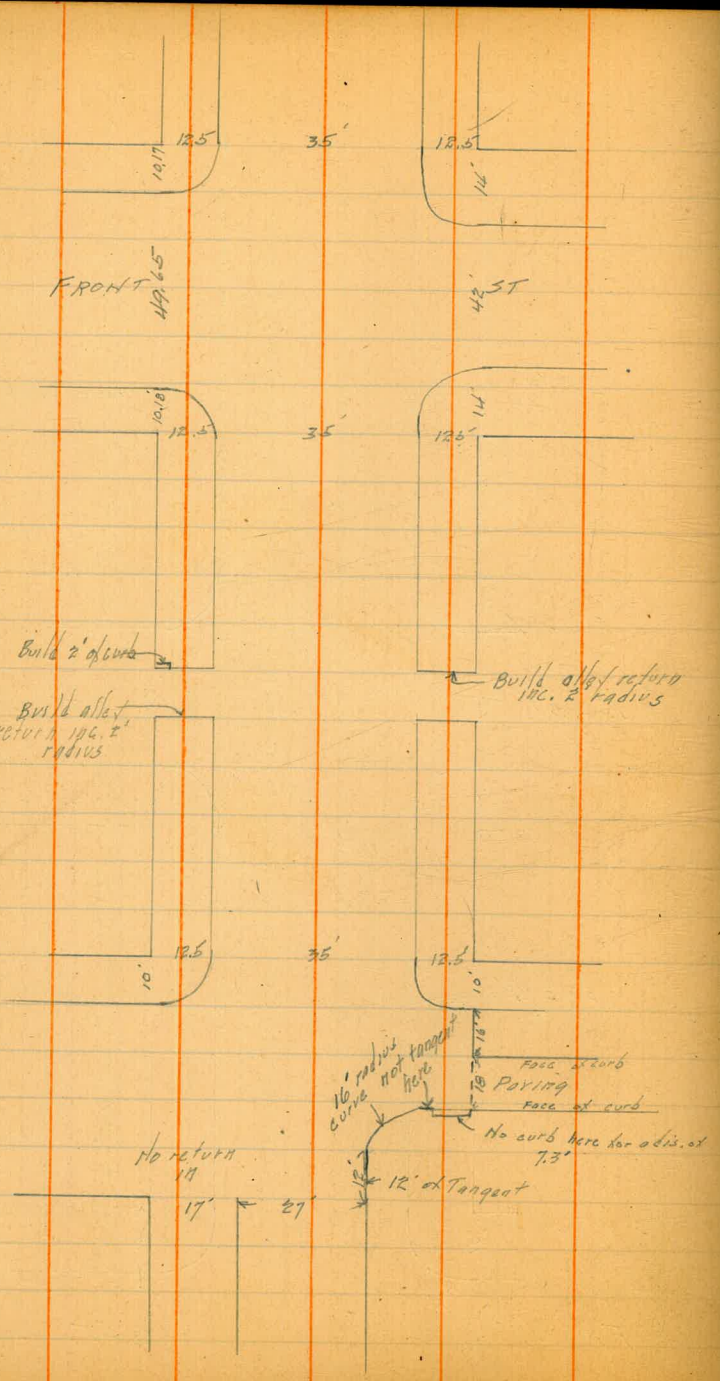
	1+00	
N		6.4
C		6.5
S		6.5
	1+10	
S		6.8
C		6.9
N		6.6
	1+16.25 = W.L. Panorama	
N		7.8
	on cement cb	7.18
C		7.9
S		7.9
	on cement cb	7.40

8/29/21 Gregory Milley Shaw

CURB DATA
ROBINSON AVE
for Paving






12.5
10.17
35'
12.5
14'
FRONT
43' ST
10.18'
12.5
35'
12.5'
14'
Build 2' of curb
Build offset return inc. 2' radius
Build offset return inc. 2' radius
10'
12.5
35'
12.5'
10'
16' radius curve not tangent here
Face of curb
20' Paving
Face of curb
No curb here for a dis. of 7.3'
No return in
12' of Tangent
17'
27'

9/17/21 Oregon Miller Shaw

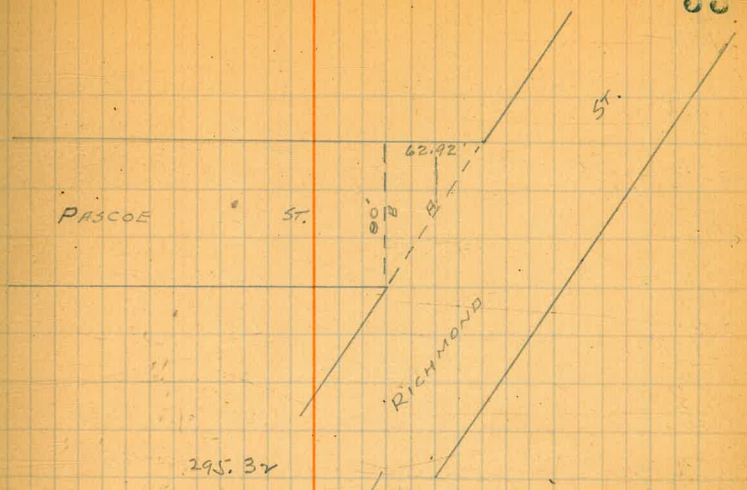
CROSS SECTION OF PASCOE ST

from W.L. Richmond to 303.5' West

80' wide

Notes taken for various widths of sidewalk etc.

B.M.	1.10	314.06		312.96	BP Iron Bolt & Line
T.P.	1.67	305.14	10.59	303.47	
	0.62	294.56	11.20	293.94	BP SW Pascoe & Rich
		W.L. Richmond			
S			0.1	294.5	
+6.36 on angle = 5' at 1t angles			0.6	94.0	
+12.72 ✓ ✓	=10' ✓ ✓ ✓		0.7	93.9	
+17.80 ✓ ✓	=14' ✓ ✓ ✓		0.8	93.8	
+25.44 ✓ ✓	=20 ✓ ✓ ✓		1.2	93.4	
+31.80 ✓ ✓	=25 ✓ ✓ ✓		1.3	93.3	
+34.34 ✓ ✓	=27 ✓ ✓ ✓		1.6	93.0	
+38.16 ✓ ✓	=30 ✓ ✓ ✓		1.7	92.9	
+44.52 ✓ ✓	=35 ✓ ✓ ✓		2.0	92.6	
+50.88 ✓ ✓	=40 ✓ ✓ ✓		2.1	92.5	
+57.23 ✓ ✓	✓ 45' ✓ ✓ ✓		2.1	92.5	
+63.60 ✓ ✓	✓ 50 ✓ ✓ ✓		2.2	92.2	
+67.42 ✓ ✓	✓ 53 ✓ ✓ ✓		2.7	91.7	
+69.96 ✓ ✓	✓ 55		2.9	91.7	
+76.32 ✓ ✓	✓ 60 ✓ ✓ ✓		3.3	91.3	
+83.96 ✓ ✓	✓ 66 ✓ ✓ ✓		3.1	91.5	
+89.04 ✓ ✓	✓ 70 ✓ ✓ ✓		3.1	91.5	
+95.40 ✓ ✓	✓ 75 ✓ ✓ ✓		3.0	91.6	
+101.75 ✓ ✓	✓ =80 ✓ ✓ ✓ =N.L.		2.9	91.7	
	1.38	295.32	0.62	293.94	



295.32

24' W. on N.

-20	13.7	281.6
-15	17.6	77.7
N	17.1	78.2
+5	14.9	80.9
+10	12.1	83.2
+14	11.1	84.2
+20	8.1	87.2
+25	5.0	90.3
+27	4.0	91.3
+30.5 = W.L. Richmond	3.2	92.1
31.46' W. on N.		
W.L. Richmond = 46' 5.0 x H	2.9	92.4
35' S. of N.L.	4.4	90.9
30' ✓ ✓ ✓	7.4	87.9
27' ✓ ✓ ✓	8.8	86.5
25 ✓ ✓ ✓	10.0	285.3

295.32

20' S. of N.L.		12.0	283.2
14' " " "		14.6	80.7
10' " " "		15.8	79.5
5' " " "		17.7	77.6
N.L.		18.6	76.7
+20		17.9	77.4
	43.25' W. on N.		
-25		19.1	76.2
N.		24.4	70.9
+5'5		22.4	72.9
+10		21.4	73.9
+14		19.8	75.5
+20		18.0	77.3
+25		15.3	80.0
+27		14.0	81.3
+30		12.8	82.5
+35		10.0	85.3
+40		7.6	87.7
+45		4.9	90.4
+50		2.0	93.3
+53		0.1	93.2
+55 = W.L. Richmond		2.1	93.2
	52' W. on N.		
W.L. Richmond = 66.1 S. of N.L.		1.5	93.8
60 " " "		2.0	93.8
55 " " "		1.0	94.3

295.32

53' S. of N.L.		2.2	293.1
50' " " "		3.0	92.3
45 " " "		6.5	88.8
40' " " "		10.3	85.0
35' " " "		13.3	82.0
30' " " "		15.2	80.1
27' " " "		16.8	78.5
25' " " "		17.2	78.1
20' " " "		19.4	75.9
14' " " "		21.9	73.4
10' " " "		22.8	72.5
5' " " "		24.2	71.1
N.L.		25.7	69.6
+16'		26.6	68.7
+25		22.7	72.6
	62.92' W. on N. = Sec. B.		
-25		26.1	69.2
-23		24.4	67.9
N.		26.5	68.8
+3		25.9	69.4
+5		23.5	71.8
+10		21.6	73.7
+14		19.7	75.6
+20		17.5	77.8
+25		15.7	79.6
+27		14.8	280.5

295.32

+30 S	13.5	281.8
+35	11.0	84.3
+40	8.2	87.1
+45	5.8	89.5
+50	2.1	93.2
+53	2.2	93.1
+55	2.1	93.2
+60	1.8	93.5
+66	1.6	93.8
+70	1.3	94.0
+75	1.2	94.1
+80 = S.L.	0.8	94.5
	10° W of B	
S.L.	0.6	94.8
+5	1.3	94.0
+10	1.6	93.8
+14	1.6	93.7
+20	2.0	93.3
+25	2.1	93.2
+27	2.3	93.0
+30	2.4	92.9
+35	2.3	93.0
+40	4.9	90.4
+45	8.1	87.2
+50	11.3	84.0
+53	13.0	282.3

295.32

+55	13.8	281.5
+60	15.7	79.6
+66	18.2	77.1
+70	19.8	75.5
+75	22.2	73.1
+79	23.8	71.5
+80 = N.L.	26.5	68.8
+30	27.6	67.7
	19° W	
-30	28.2	67.1
-4	27.0	68.3
N.L.	22.9	72.4
+5	20.9	74.4
+10	18.6	76.7
+14	17.0	78.3
+20	14.7	80.6
+25	12.6	82.7
+27	11.6	83.7
+30	9.7	85.6
+35	6.1	89.2
+40	4.0	91.8
+45	2.3	93.0
+50	2.9	92.4
+53	2.5	92.8
+55	2.2	93.1
+60	2.2	293.1

295.32

+66	2.1	293.2
+70	2.0	93.3
+75	1.6	93.7
+80 = S.L	0.5	94.8
40' W.		
S.L = 2' under house	0.1	95.2
+5	1.6	93.7
+6	2.1	93.2
+10	2.2	93.1
+14	2.1	93.2
+20	2.3	93.0
+25	2.5	92.8
+27	3.4	91.9
+30	3.9	91.4
+35	3.9	91.4
+40	3.5	91.8
+45	6.5	88.8
+50	9.0	86.3
+53	10.4	84.9
+55	11.4	83.9
+60	13.4	81.9
+66	15.2	80.1
+70	16.4	78.9
+75	18.5	76.8
+80 = N.L	20.2	75.1
+12	27.9	67.4
+35	29.1	266.2

295.32

56' W

-35	30.1	265.2
-24	30.1	65.2
-18	26.4	68.9
N	19.8	75.5
+5	16.0	79.3
+10	14.8	80.5
+14	14.0	81.3
+20	11.9	83.4
+25	9.6	85.7
+27	8.8	86.5
+30	7.1	88.2
+35	4.7	90.6
+40	4.2	91.1
+45	4.2	91.1
+50	3.6	91.7
+53	2.8	92.5
+55	2.3	93.0
+60 = N edge of Garage	2.1	93.2
+66 = under garage	2.2	93.1
+70 = " "	2.2	93.1
+73 = " "	2.2	93.1
+75	1.1	94.2
+80 = S.L	0.0	95.3
63' W.		
14' S. of N.L	13.5	281.8

295.32

10' S. of N.L.	14.7	280.6
5' S of N.L.	15.9	79.4
N.L.	17.1	77.9
+10	22.2	73.1
+25	27.0	68.3
80' W		
S.L.	0.0	95.3
+5	1.3	94.0
+10	1.7	93.6
+14	1.8	93.5
+20	1.9	93.4
+25	1.9	93.4
+27	2.3	93.0
+30	2.6	92.7
+35	3.5	91.8
+40	4.0	91.3
+45	4.1	90.9
+50	5.9	89.1
+53	6.5	88.8
+55	7.1	88.2
+60	8.2	87.1
+66	11.1	84.2
+70	13.2	82.1
+76	14.5	80.8
+80 = N.L.	16.4	278.9

295.32

+7	18.1	277.2
+30	26.7	68.6
100' W		
-20	32.2	73.1
N	15.1	80.2
+5	13.2	82.1
+10	10.8	84.5
+14	9.9	85.4
+20	8.5	86.9
+25	7.0	88.3
+27	6.3	89.0
+30	5.6	89.7
+35	4.7	90.6
+40	3.8	91.5
+45	2.0	93.3
+50	1.2	94.1
+53	1.2	94.1
+55	1.3	94.0
+60	1.2	94.1
+66	0.9	94.4
+70	0.4	94.9
+76	0.4	94.9
+80 = S.L.	0.2	95.1
T.P. 4.60	295.40	45.2 = 290.80

295.40

125' W

S	0.4	295.0
+5	0.7	94.7
+10	0.5	94.9
+14	0.9	94.5
+20	1.6	93.8
+25	1.7	93.7
+27	1.8	93.6
+30	1.8	93.6
+35	2.2	93.2
+40	3.4	92.0
+45	4.7	90.7
+50	5.9	89.5
+53	6.5	88.9
+55	6.9	88.5
+60	8.0	87.4
+66	8.9	86.5
+70	9.8	85.6
+75	12.8	82.6
+80 = N.L.	16.2	79.2
N+20	23.4	72.0

150' W

-20	25.4	70.0
N	18.1	77.3
+5	16.1	79.3
+10	13.1	282.3

295.40

+14	11.2	284.2
+20	9.2	86.2
+25	7.9	87.5
+27	7.6	87.8
+30	7.2	88.2
+35	6.7	88.7
+40	5.7	89.7
+45	4.7	90.7
+50	3.7	91.7
+53	3.1	92.3
+55	2.6	92.8
+60	2.1	93.3
+66	1.7	93.7
+70	1.7	93.7
+75	1.5	93.9
+80 = S	1.1	94.3

175' W

S	2.2	93.2
+5	3.5	91.9
+10	4.3	91.1
+14	4.8	90.6
+20	5.9	89.5
+25	6.9	88.5
+27	7.4	88.0
+30	7.8	87.6
+35	8.3	287.1

295.40

+40		9.0	286.4
+45		10.1	85.3
+50		11.0	84.4
+53		11.5	83.9
+55		12.5	82.9
+60		14.1	81.3
+66		16.8	78.5
+70		18.7	76.7
+75		19.7	75.7
+80 = N		21.1	74.3
+25		32.4	63.0
	200' W		
-30		38.7	56.7
-20		33.2	62.2
N		26.5	68.9
+5		23.9	71.5
+10		22.7	72.7
+14		21.7	73.7
+20		20.5	74.9
+25		19.1	76.3
+27		18.5	78.9
+30		16.4	79.0
+35		13.9	81.5
+40		12.0	83.3
+45		10.7	84.7
+50		10.0	285.4

295.40

+53	9.5	285.9
+55	9.4	86.0
+60	8.7	86.7
+66	7.5	87.9
+70	5.7	89.7
+75	4.8	90.6
+80 = S.L	3.6	91.8
225' W		
S	5.3	90.1
+5	6.2	89.2
+10	7.4	88.0
+14	8.1	87.3
+20	9.9	85.5
+25	10.8	84.6
+27	11.4	84.0
+30	12.6	82.8
+35	14.5	80.9
+40	17.6	77.8
+45	20.1	75.3
+50	21.9	73.5
+53	22.8	72.6
+55	23.8	71.6
+60	25.5	69.9
+66	27.0	68.4
+70	28.5	66.9
+76	30.5	264.9

295.40

+80 = NL	33.2	262.2
+7	35.8	59.6
+19	42.5	52.9
+32	43.7	51.7
250' W		
-30	39.7	55.7
-13	45.9	49.5
N	37.6	57.8
+5	36.0	59.4
+10	33.8	61.6
+14	32.2	63.2
+20	29.7	65.7
+25	27.4	68.0
+27	26.7	68.7
+30	25.5	69.9
+35	23.1	72.3
+40	20.8	74.6
+45	17.7	77.7
+50	15.1	80.3
+53	13.0	82.4
+55	12.6	82.8
+60	11.4	84.0
+66	10.3	85.1
+70	9.9	85.5
+75	8.9	86.5
+80 = S	7.5	287.9

295.40

275' W		
S	10.2	285.2
+5	10.5	84.9
+10	10.9	84.5
+14	14.4	81.0
+20	16.2	79.2
+25	17.8	77.6
+27	16.5	78.9
+30	19.7	75.7
+35	22.5	72.9
+40	24.3	71.1
+45	26.0	69.4
+50	28.2	67.2
+53	29.6	65.8
+55	30.8	64.6
+60	33.6	61.8
+66	36.7	58.7
+70	40.7	54.7
+75	44.4	51.0
+76	47.3	48.1
+80 = N	47.1	48.3
+10	43.3	52.1
+20	40.4	55.0
290' W		
-25	37.2	58.2
-8	44.7	250.7

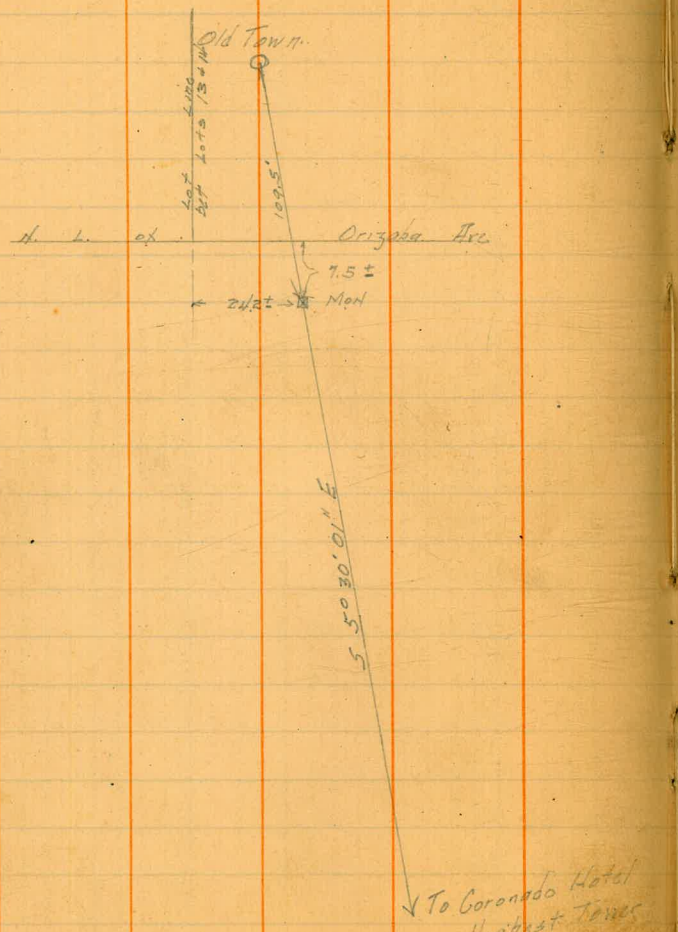
	295.40			
N		49.5	245.9	
+2		49.1	46.3	
+5		44.6	50.8	
+10		42.6	52.8	
+14		40.2	55.2	
	303.5 W.			
-25		37.5	57.9	
-12		44.6	50.8	
-5		50.2	45.2	
N		48.2	47.2	
+5		45.5	49.9	
+10		43.7	51.7	
+14		42.1	53.3	
+20		39.9	55.5	
+25		37.3	58.1	
+27		36.0	59.4	
+30		34.9	60.7	
+35		31.9	63.5	
+40		30.2	65.2	
+45		28.1	67.3	
+50		26.1	69.3	
+53		25.1	70.3	
+55		24.0	71.4	
+60		21.4	74.0	
+66		18.0	77.4	
+70		15.1	80.3	
+75		12.3	283.1	

+80 = 5 11.5 283.9

Hurrah.

9/21/21 Gregory Miller Shaw

Tie Out for USC&G Survey Initial Point Called "Old Town"



11/18/21 Gregory / Moore / Miller / Shaw

CROSS SECTION OF WITHERBY ST from N L Sunset Blvd To S L of Guy St

50' wide
10' cbs

Estimate Book 8 Page 234.
Donnan Jan 23

NE Orizaba + Couts

	1.63	270.72 ✓	269.09

SECT A = 0+00

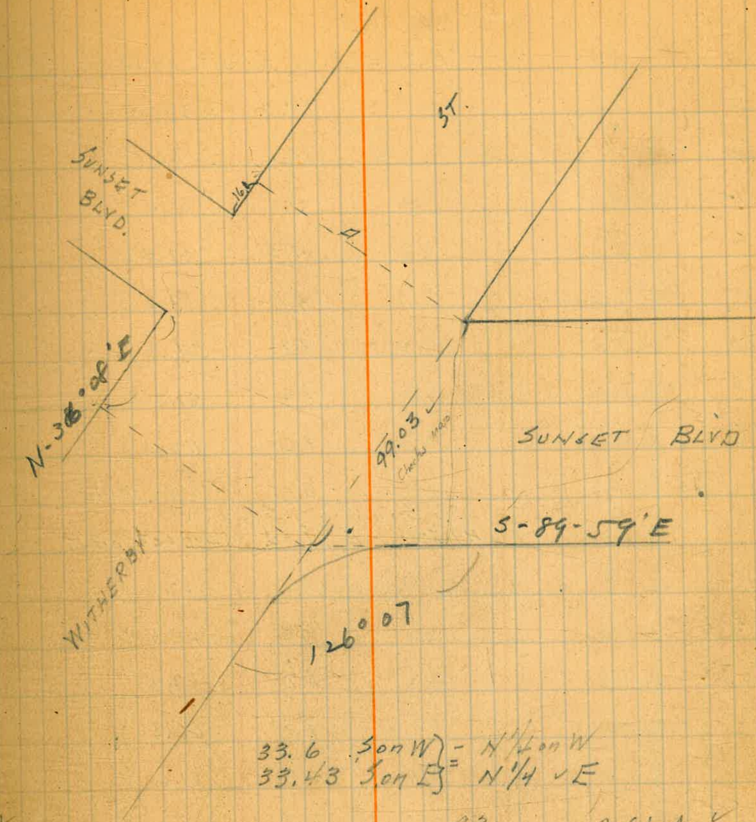
E	10.7	60.0 ✓
cb	10.9	59.8 ✓
1/4	11.1	59.6 ✓
c	10.8	59.9 ✓
1/4	10.7	60.0 ✓
cb	10.9	59.8 ✓
W	11.3	59.4

16.1 ' S. on W } = NL Sunset on W
17.33 " " E } = N. cb " " E

W	10.6	60.1 ✓
cb	10.2	60.5 ✓
1/4	10.1	60.6 ✓
c	10.3	60.4 ✓
1/4	10.7	60.0 ✓
cb	10.7	60.0 ✓
E	10.4	60.3 ✓

46.1 S. N. Cb of Sunset on West.

E	10.4	60.3 ✓
cb	10.5	60.2 ✓
1/4	10.3	60.4 ✓
c	10.1	60.6 ✓
1/4	9.7	61.0 ✓
cb	9.6	61.1 ✓
W	9.9	260.8 ✓



33.6 S on W } = N 1/4 on W
33.43 S on E } = N 1/4 " E

W	9.3	261.4 ✓
1/4	9.7	261.0 ✓
cb	9.2	61.5 ✓
1/4	9.8	60.9 ✓
c	10.0	60.7 ✓
1/4	10.4	60.3 ✓
cb	10.3	60.4 ✓
E	10.1	60.6 ✓

PLOTTED

470.72

41.1 S = L of Sunset on W

E	10.2	260.5 ✓
cb	10.0	60.7 ✓
1/4	9.7	61.0 ✓
C	9.3	61.4 ✓
1/4	9.1	61.6 ✓
cb	8.9	61.8 ✓
+8	9.2	61.7 ✓
W	8.3	62.4 ✓
on N.P.	8.15	262.57 ✓

48.6 S on W } = 5 1/4 on W
49.5 " E } = L of Sunset on E

W	8.1	62.6 ✓
+2	8.8	61.9 ✓
cb	8.7	62.0 ✓
1/4	8.9	61.8 ✓
C	9.1	61.6 ✓
1/4	9.4	61.3 ✓
cb	9.8	60.9 ✓
E	10.2	60.5 ✓

56.1 S = 5 cb on W

E	9.9	60.8 ✓
cb	9.6	61.1 ✓
1/4	9.1	61.6 ✓
C	8.7	62.0 ✓
1/4	8.5	62.2 ✓
cb	8.3	62.4 ✓

+7	8.4	62.3 ✓
W	7.0	63.7 ✓

66.1 on W } = 5 L Sunset on W
65.61 " E } = 5 1/4 " " E

W	6.5	64.2 ✓
+3	7.9	62.8 ✓
cb	7.8	62.9 ✓
1/4	8.1	62.6 ✓
C	8.3	62.4 ✓
1/4	8.7	62.0 ✓
cb	9.2	61.5 ✓
E	9.6	61.1 ✓

81.70 S = cb on E

E	9.0	61.7 ✓
cb	8.3	62.4 ✓
1/4	7.4	63.3 ✓
C	7.4	63.3 ✓
1/4	7.4	63.3 ✓
cb	7.4	63.3 ✓
+7	6.6	64.1 ✓
W	6.2	64.5 ✓

99.03 S = 5 L. Sunset on E

W	5.4	65.3 ✓
+3	5.7	65.0 ✓
+5	7.0	63.7 ✓
cb	6.7	64.0 ✓
1/4	6.6	64.1 ✓

	270.72		
C		6.5	64.2 ✓
1/4		6.9	63.8 ✓
cb		7.6	63.1 ✓
E		8.4	62.3 ✓
	+ 2.0		
E		4.9	65.8 ✓
+4		8.0	62.7 ✓
cb		7.4	63.3 ✓
	+ 10.0		
E		4.4	66.3 ✓
cb		4.6	66.1 ✓
+4		6.5	64.2 ✓
1/4		6.5	65.7 ✓
C		6.2	64.5 ✓
1/4		6.2	64.5 ✓
cb		6.3	64.4 ✓
+5		6.4	64.3 ✓
W		5.2	65.5 ✓
	+ 3.0		
W		5.0	65.7 ✓
+5		6.4	64.3 ✓
cb		6.1	64.6 ✓
1/4		6.0	64.7 ✓
C		6.0	64.7 ✓
1/4		6.0	64.7 ✓
+3		4.6	66.1 ✓

cb		4.4	66.3 ✓
E		4.3	66.4 ✓
	+ 5.0		
E		5.1	65.6 ✓
cb		4.9	65.8 ✓
+3		4.7	66.0 ✓
+5		6.3	64.4 ✓
1/4		6.1	64.6 ✓
C		5.7	65.0 ✓
1/4		5.7	65.0 ✓
cb		6.2	64.5 ✓
+5		6.3	64.3 ✓
+6		5.4	65.3 ✓
W		5.2	65.5 ✓
	1+00		
W		6.5	64.2 ✓
+4		6.5	64.2 ✓
+5		7.5	63.2 ✓
cb		7.2	63.5 ✓
1/4		6.9	63.8 ✓
C		6.5	63.8 ✓
1/4		7.1	63.6 ✓
+3		7.3	63.4 ✓
+5		6.3	64.4 ✓
cb		6.3	64.4 ✓
E		6.0	64.7 ✓

	270.72			
	1+50			
E		8.0	62.7 ✓	
cb		8.0	62.7 ✓	
+2		8.0	62.7 ✓	
+4		9.3	61.4 ✓	
1/4		9.1	61.6 ✓	
c		9.0	61.7 ✓	
1/4		9.0	61.7 ✓	
cb		9.6	61.1 ✓	
W		9.4	61.3 ✓	
	2+00			
W		11.3	59.4 ✓	
cb		11.5	59.2 ✓	
1/4		11.1	59.6 ✓	
c		10.8	59.9 ✓	
1/4		11.0	59.7 ✓	
+2		11.1	59.6 ✓	
+3		8.9	61.8 ✓	
cb		9.1	61.6 ✓	
E		9.1	61.6 ✓	
	2+20			
E		10.4	60.3 ✓	
cb		11.5	59.2 ✓	
+3		11.4	59.3 ✓	
+4 = 12" pipe Line		12.7	58.0 ✓	
+6		12.7	58.0 ✓	
1/4		12.7	58.0 ✓	

c		12.6	58.1 ✓	
1/4		12.7	58.0 ✓	
cb		13.0	57.7 ✓	
+4		13.4	57.3 ✓	
W		13.1	57.6 ✓	
T.P.	0.23	258.22	12.73	257.99 ✓
		267.07 = N.L. Juan St 50' wide		
W		6.2	52.0 ✓	
cb		5.6	52.6 ✓	
1/4		4.9	53.3 ✓	
c		4.7	53.5 ✓	
1/4		4.6	53.7 ✓	
+3		4.2	54.0 ✓	
+5		3.7	54.5 ✓	
cb		3.6	54.7 ✓	
E		3.4	54.8 ✓	
	W. Curb			
E		4.1	54.1 ✓	
cb		4.6	53.6 ✓	
1/4		5.1	53.1 ✓	
c		5.6	52.7 ✓	
1/4		5.8	52.4 ✓	
cb		6.3	51.9 ✓	
W		7.0	51.2 ✓	

258.22

N. ½

W	7.1	51.1 ✓
cb	6.5	51.7 ✓
½	6.0	52.2 ✓
c	5.7	52.5 ✓
½	5.6	52.6 ✓
cb	5.1	53.1 ✓
E	4.7	53.5 ✓

center Juan

E	5.4	52.8 ✓
cb	6.0	52.2 ✓
½	6.3	51.9 ✓
c	6.6	51.6 ✓
½	6.5	51.7 ✓
cb	6.8	51.4 ✓
W.	7.3	50.9 ✓

S. ½

W	7.5	50.7 ✓
cb	7.4	50.8 ✓
½	8.0	50.2 ✓
c	7.7	50.5 ✓
½	7.3	50.9 ✓
cb	6.6	51.6 ✓
E	6.2	52.0 ✓

S. curb

E	6.6	51.6 ✓
cb	7.3	50.9 ✓
½	7.9	50.3 ✓
c	8.5	49.7 ✓
½	9.2	49.0 ✓
cb	9.5	48.7 ✓
W	10.2	48.0 ✓

S. Lime Juan

W	11.3	46.9 ✓
cb	10.9	47.3 ✓
½	10.4	47.8 ✓
c	9.8	48.4 ✓
½	9.2	49.0 ✓
cb	8.3	49.9 ✓
E	7.9	50.3 ✓
T.P. 0.0	6.80	251.42 ✓ Mon ✓

50 S

E	4.3	47.1 ✓
cb	5.4	46.0 ✓
½	6.0	45.4 ✓
c	6.7	44.7 ✓
½	7.4	44.0 ✓
cb	7.9	43.5 ✓
W.	8.7	42.7 ✓
+10	9.3	42.1 ✓

		251.42		
		100.5		
-10			13.1	38.3 ✓
W			12.2	39.2 ✓
cb			11.0	40.4 ✓
1/4			10.5	40.9 ✓
C			9.6	41.8 ✓
1/4			8.4	43.0 ✓
cb			7.8	43.6 ✓
E			6.2	45.2 ✓
		1+32		
E			6.6	44.8 ✓
cb			8.7	42.7 ✓
		1+348	= NL Guy St 50 wide 10 cb	
E			7.9	43.5 ✓
cb			8.7	42.7 ✓
1/4			9.4	42.0 ✓
C			10.3	41.1 ✓
1/4			11.4	40.0 ✓
cb			12.8	38.6 ✓
W			14.5	37.1 ✓
+10			15.9	35.5 ✓
		N. Curb		
-10			17.7	33.7 ✓
W			15.4	36.0 ✓
cb			13.3	38.1 ✓
1/4			11.5	39.9 ✓

cb			10.2	41.2 ✓
1/4			9.5	41.9 ✓
cb			9.0	42.4 ✓
E			8.5	42.9 ✓
T.P.	1.127	244.17 ✓	8.5 ±	242.90 ✓
		N. 1/4		
E			1.2	43.0 ✓
cb			3.0	42.2 ✓
1/4			4.6	41.6 ✓
C			3.5	40.7 ✓
1/4			5.0	39.2 ✓
cb			7.1	37.1 ✓
W			9.2	35.0 ✓
+10			10.8	33.4 ✓
		Center Guy		
-10			11.3	37.7 ✓
W			9.7	34.5 ✓
cb			7.1	37.1 ✓
1/4			5.7	38.5 ✓
C			4.3	39.9 ✓
1/4			3.4	40.8 ✓
cb			2.7	41.5 ✓
E			2.0	42.2 ✓
		S 1/4		
E			2.8	41.4 ✓
cb			3.4	40.8 ✓

244.17

1/4		4.2	40.0
c		5.2	39.0
1/4		6.1	38.1
cb		7.9	36.3
W		10.2	34.0
+10		11.5	32.7
	S. Curb		
-10		12.4	31.8
W		11.2	33.0
cb		8.5	35.7
1/4		6.5	37.7
c		5.3	38.9
1/4		4.5	39.7
cb		3.9	40.3
E		3.4	40.8
	S.L. Guy St.		
E		3.9	40.3
cb		4.7	39.5
1/4		5.0	39.2
c		6.4	37.8
1/4		7.8	36.4
cb		10.3	33.9
W		12.4	31.8
+10		13.8	30.4

10' S.

-10	14.8	29.4
W	13.6	30.6
cb	10.9	33.3
1/4	8.9	35.3
c	7.3	36.9
1/4	6.0	38.2
cb	5.3	38.9
E	4.6	39.6

11/19/21 Gregory, Moore, Miller, Shaw

CROSS SECTION OF LEWIS ST
from Front to First
55' wide
10 cbs. on S. 8.125' 1/45
12.5 " " N

287.97

ESTIMATE
BOOK 10, PAGE 293.
11-21-21. W.N.D.

	B.S.	H.I.		Rod	Elev.	
	7.14	292.10			284.96	B.P. S.E. Front & Lewis

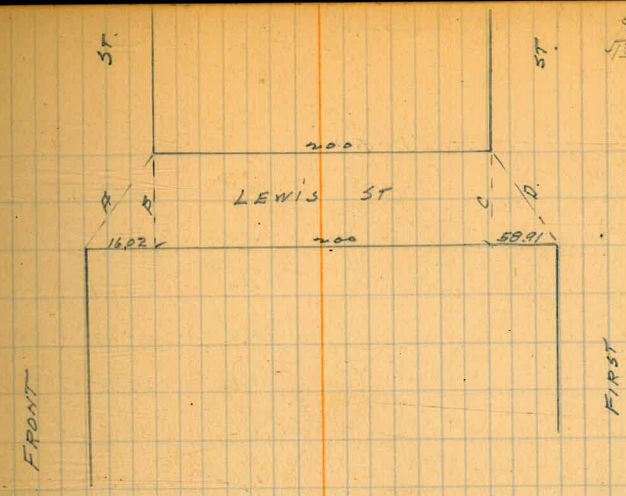
SECT A

Point		Rod	Elev.	Remarks
S		6.7	285.4 ✓	on walk.
+5		7.0	285.1 ✓	
+6		5.9	286.2 ✓	
cb		5.4	286.7 ✓	
1/4		5.8	286.3 ✓	
c		5.6	286.5 ✓	
1/4		5.8	286.3 ✓	
cb		6.0	286.1 ✓	
N		5.0	287.1 ✓	

SECT B = 0+00

Point	Station	Rod	Elev.
N.		5.0	287.1 ✓
cb		5.4	286.7 ✓
1/4		5.1	287.0 ✓
c		4.8	287.3 ✓
1/4		5.2	286.9 ✓
cb		4.8	287.3 ✓
S		4.4	287.7 ✓
	0+05.0		
S		4.1	288.0 ✓
cb		4.5	287.6 ✓
1/4		4.8	287.3 ✓
c.		4.6	287.5 ✓
1/4		4.8	287.3 ✓

55
225
√325
8.125



Point	Station	Rod	Elev.
cb		4.7	287.4 ✓
N		3.4	288.7 ✓
	0+50		
N		4.2	287.9 ✓
cb		4.5	287.6 ✓
1/4		4.7	287.4 ✓
c		4.6	287.5 ✓
1/4		4.8	287.3 ✓
cb		4.7	287.4 ✓
S		4.6	287.5 ✓
	1+00		
S.		4.7	287.4 ✓
cb		4.7	287.4 ✓
1/4		4.7	287.4 ✓
c		4.7	287.4 ✓
1/4		4.7	287.4 ✓
cb		4.6	287.5 ✓
N		4.2	287.9 ✓

	2+20.10		
	1+50		
N		3.7	288.4 ✓
cb		4.4	287.7 ✓
1/2		4.4	287.7 ✓
c		4.4	287.7 ✓
1/2		4.6	287.5 ✓
cb		4.6	287.5 ✓
S		4.6	287.5 ✓
	2+00 = SECT C		
S		4.1	288.0 ✓
cb		4.1	288.0 ✓
1/2		4.1	288.0 ✓
c		4.2	287.9 ✓
1/2		4.2	287.9 ✓
cb		4.3	287.8 ✓
N		3.8	288.3 ✓
		4.47	287.63 ✓ = cb N.W. First + Lewis
	SECT. D		
N		3.8	288.3 ✓
cb		4.2	287.9 ✓
1/2		4.0	288.1 ✓
c		3.7	288.4 ✓
1/2		3.8	288.3 ✓
cb		4.1	288.0 ✓
S		4.7	287.4 ✓
		4.13	287.97 ✓ BP SL

11/23/21 Gregory Moore Miller Shaw

CROSS SECTION OF ALBERT ST.

80' wide 20' cbs 10' 1/4s from N.L. Brookes to N.L. Cypress

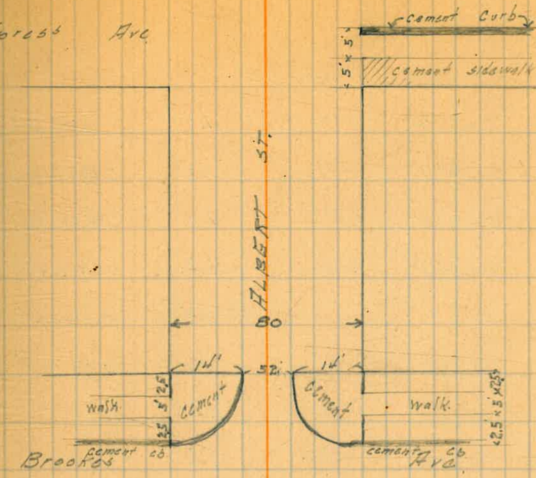
	0.20	290.69		290.49	BP 5E Cypress + Herb
	11.2	291.55	10.38	280.31	
on curb and Return			3.47	288.08	

N.L. Brookes = 0+0.0

E	3.17	288.38
+10	3.40	288.15
cb	4.0	287.6
1/4	3.9	287.7
c	4.0	287.6
1/4	3.8	287.8
cb	4.2	287.4
+10	4.3	287.3
W	4.13	287.42
on curb and Return	4.43	287.12

0+5.0

W	2.5	289.1
+10	2.7	288.9
cb	3.0	288.6
1/4	3.0	288.6
c	3.2	288.4
1/4	3.4	288.2
cb	3.4	288.2
+5	2.5	289.1
+10	2.7	288.9
E	2.5	289.1



0+10

E	2.0	289.6
+10	2.2	289.4
+14	2.0	289.6
cb	3.2	288.4
1/4	3.2	288.4
c	2.9	288.7
1/4	3.0	288.6
cb	2.8	288.8
+10	2.0	289.6
W	2.3	289.3

0+12.5

12.5' E. of W.L. = Gas Co pole #3602

Estimates Book 10 Page 293

	291.55		
	0+35		
W		1.7	289.9 ✓
+10		1.4	290.2 ✓
cb		1.4	290.2 ✓
1/4		1.3	290.3 ✓
C		1.4	290.2 ✓
1/4		1.7	289.9 ✓
cb		1.5	290.1 ✓
+10		1.6	290.0 ✓
+13		2.0	289.6 ✓
E		1.6	290.0 ✓
	0+70		
E		1.7	289.9 ✓
+10		1.8	289.8 ✓
cb		2.0	289.6 ✓
1/4		1.7	289.9 ✓
C		1.7	289.9 ✓
1/4		1.2	290.4 ✓
cb		1.3	290.3 ✓
+10		1.3	290.3 ✓
W		1.4	290.2 ✓
	1+00		
W		1.6	290.0 ✓
+10		1.8	289.8 ✓
cb		1.9	289.7 ✓
1/4		2.0	289.6 ✓
C		1.9	289.7 ✓
1/4		2.2	289.4 ✓
cb		2.4	289.2 ✓
+10		2.3	289.3 ✓
E		2.0	289.6 ✓
	1+35		
E		2.4	289.2 ✓
+10		2.7	288.9 ✓
cb		2.9	288.7 ✓
1/4		2.7	288.9 ✓
C		2.9	288.7 ✓
1/4		2.8	288.8 ✓
cb		2.6	289.0 ✓
+10		2.6	289.0 ✓
W on lawn		2.2	289.4 ✓
	1+51		
13' E ox W.L = Gas Co pole #3648			
	1+60		
W		3.3	288.3 ✓
+10		3.4	288.2 ✓
cb		3.6	288.0 ✓
1/4		3.6	288.0 ✓
C		3.6	288.0 ✓
1/4		3.4	288.2 ✓
cb		3.1	288.5 ✓
+10		2.9	288.7 ✓

291.56

E	2.5	289.1 ✓

1+75

E	2.4	289.2 ✓
+10	3.3	288.3 ✓
cb	4.4	287.2 ✓
1/4	4.5	287.1 ✓
c	4.0	287.6 ✓
1/4	3.8	287.8 ✓
cb	3.9	287.7 ✓
+10	4.1	287.5 ✓
W	3.5	288.1 ✓

1+93

12' E ox W Line = spare brace pole Gas Co

1+00

W	3.8	287.8 ✓
+3	5.2	286.4 ✓
+10	5.4	286.2 ✓
cb, 1/4	5.5	286.1 ✓
c	5.2	286.4 ✓
1/4	5.3	286.3 ✓
cb	4.5	287.1 ✓
+10	3.6	288.0 ✓
E	3.0	288.6 ✓
	2.7	288.9 ✓

1+25

E	2.0	289.6 ✓
+10	3.0	288.6 ✓
cb	3.6	288.0 ✓
1/4	4.3	287.3 ✓
c	5.5	286.1 ✓
1/4	6.3	285.3 ✓
cb	7.0	284.6 ✓
+10	7.0	284.6 ✓
+17	6.7	284.9 ✓
W	5.4	286.2 ✓

1+50

W	6.2	285.4 ✓
+1 = Top wall ✓	6.2	285.4 ✓
+1.3 = bottom wall ✓	9.5	282.1 ✓
+10	10.3	281.3 ✓
cb	9.3	282.3 ✓
1/4	7.1	284.5 ✓
c	6.0	285.6 ✓
1/4	4.3	287.3 ✓
cb	3.7	287.9 ✓
+10	3.2	288.4 ✓
E	2.0	289.6 ✓

1+75

E	2.0	289.6 ✓
+10	3.2	288.4 ✓

		291.55		
cb			3.8	287.8
1/4			5.0	286.6
c			6.3	285.3
1/4			9.9	281.7
cb			12.8	278.8
+9			13.7	277.9
+10			14.8	276.8
W			15.7	275.9
		3+00		
W			20.0	271.6
+10			19.1	272.5
cb			15.9	275.7
1/4			11.4	280.2
c			7.6	284.0
1/4			6.0	285.6
cb			6.1	285.5
+10			3.6	288.0
E			2.3	289.3
		3+17		
E			2.4	289.2
+5			7.0	284.6
+10			8.4	283.2
		3+18.8 = S.L. Cypress		60' wide 10' cbs
E	on cement walk		10.34	281.21
+10			9.2	282.4
T.P.	2.19	284.27	9.47	282.08

ALBERT

cb		2.0	282.3
1/4		0.7	283.6
c		1.9	282.4
1/4		7.0	277.3
cb		10.5	273.8
+10		13.2	271.1
W		17.0	267.3
	S Curb		
W		19.5	264.8
+10		15.2	269.1
cb		12.0	272.3
1/4		8.2	276.1
c		2.7	281.4
1/4		1.9	282.4
cb		2.7	281.6
+10		3.3	281.0
E	on cement curb	3.23	281.04
	S Quarter		
E		3.8	280.5
+10		3.3	281.0
cb		2.4	281.9
1/4		2.7	281.6
+3		3.2	281.1
c		7.1	277.2
1/4		11.7	272.6
cb		15.1	269.2

284.27

+10		17.9	266.4 ✓
W		21.3	263.0 ✓
	Center		
W		23.1	261.2 ✓
+10		20.7	263.6
cb		17.9	266.4 ✓
+5		16.4	267.9 ✓
1/4		14.4	269.9 ✓
C		10.8	273.5 ✓
1/4		5.7	278.6 ✓
+3		3.8	280.5 ✓
cb		3.0	281.3 ✓
+10		3.0	281.3 ✓
E		3.7	280.6 ✓
	N. Quarter		
E		4.4	279.9 ✓
+10		3.3	281.0 ✓
+16		4.1	280.2 ✓
cb		6.0	278.3 ✓
1/4		10.1	274.2 ✓
C		14.6	269.7 ✓
+6		17.1	267.2 ✓
1/4		18.0	266.3 ✓
cb		21.4	262.9 ✓
+10		20.9	261.4 ✓
W		24.7	259.6 ✓

N. Curb

W		28.5	255.8 ✓
+10		26.7	257.6 ✓
cb		24.6	259.7 ✓
1/4		22.0	262.3 ✓
C		18.6	265.7 ✓
1/4		15.5	268.8 ✓
cb		10.6	273.7 ✓
+5		10.3	274.0 ✓
+10		7.5	276.8 ✓
+14		4.7	279.6 ✓
E	on end cement cb	4.29	279.98 ✓
	N.L. Cypress		
E		4.1	280.2 ✓
+10		11.3	273.0 ✓
cb		15.3	269.0 ✓
1/4		18.1	266.2 ✓
C		21.9	262.4 ✓
1/4		25.9	258.4 ✓
cb		28.4	255.9 ✓
~~W~~ +10		30.0	254.3 ✓
W		32.6	251.7 ✓

1/25/24 Gregory Moore Miller Shaw

GRADES ON 16" Pipe Line from Exchange Place & Terrace Road To Bird Rock

		8.44 020 039	196.32 193.67 171.25	12.85 12.81	187.88 183.47 176.36	BP Prospect & College	
						GRADE	
0+00 = 10" S+E ox & ox Terrace Road & Exch.				6.44	164.81	160.0	4.81
+50 = Gate Valve				7.15	164.10	159.0	5.10
1				8.42	162.83	156.0	4.83
+50				9.70	161.55	157.0	4.55
2				10.90	160.35	156.0	4.35
+50				12.10	159.15	155.0	4.15
T.P.	1.63	160.03		12.85	158.40	15	
3				13.20	157.83	154.0	3.83
+50				3.15	156.88	153.0	3.88
4				4.20	155.83	152.0	3.83
+50				5.13	154.90	151.0	3.90
5				6.10	153.93	150.0	3.93
+50 = E.L. IVANHOE				6.87	153.16	149.0	4.16
+80 = 16" x 6" cross ←				7.63	152.40	148.40	4.0
6				8.07	151.96	148.0	3.96 break
+50				9.47	150.56	146.5	4.06
7				10.77	149.26	145.0	4.26 break
+50	0.36	147.82		12.57	147.46	142.75	4.71
8				3.32	144.50	140.5	4.0 break
+50				7.02	140.80	136.33	4.47
9				12.05	135.77	132.16	3.61
T.P.	0.80	136.10		12.52	135.30		
+50				4.10	132.0	128.0	4.0 break
10				6.72	129.38	125.68	3.70
+50				8.66	127.44	12336	4.08

Main Laid 10" 3.0 x 6.0 x Terrace Road

136.10

11			11.13	124.97	GRADE 121.03 3.94
T.P.	0.76	124.03	12.83	123.27	
+50			1.30	122.73	118.71 4.02
12			3.40	120.63	116.39 4.24
+50			6.00	118.03	114.07 3.96
13			8.43	115.60	111.75 3.85 break
+50			10.50	113.53	109.88 3.65
14	1.03	112.76	12.30	111.73	108.00 3.73
+50			2.57	110.19	106.13 4.06
15			3.44	109.32	104.25 5.07
+50			4.30	108.46	102.38 6.08
16			6.57	106.19	100.50 5.69
+50			9.00	103.76	98.63 5.13
17			11.37	101.39	96.75 4.64
T.P.	2.20	102.13	12.83	99.93	
+50			3.03	99.10	94.87 4.23
18		break.	4.80	97.33	93.0 4.33 break
+50			5.73	96.40	94.33 4.07
19			6.48	95.65	91.67 3.98
+50			7.00	95.13	91.0 4.13
T.P. 7' Mon Girard		107.75	6.78	95.35	
+86.1 = 16" x 6" Special = 10' E. ox & Girard			12.40	95.76	90.5 4.9 4.38
20			12.40	95.76	90.97 4.41
+50			11.1	96.65	92.65 4.0
21			9.1	9805	94.33 3.9

Main Laid 14" 5.0 x 6.0 x 10' 3.0 x 6.0 ox Terrace Road

8) 1585 / 1.98   107.75   6) 126.60 / 7

+50			7.7	100.05	95.91	4'-2"
22			5.8	101.95	97.69	4'-3"
+50			3.9	103.85	99.27	4'-7"
23			1.8	106.0	101.05	4'11"
	12.68	120.33	0.10	107.65		
+50			12.4	107.9	102.73	5'2"
24			10.7	109.6	104.41	5'2"
+50			9.0	111.3	106.12	5'2"
25			7.4	112.9	107.80	5'1"
			6.5	113.8		4'10"
+36.1	Δ=10'S. of ℄ of Pearl		6.2	114.1	109.0	5'7"
26			6.9	113.4	108.0	5'5"
+50			7.3	113.0	107.20	5'10"
27			7.7	112.6	106.44	6'3"
+50			7.7	112.6	105.68	7'0"
28			8.8	111.5	104.92	6'8"
+50			9.6	110.7	104.16	6'6"
29			11.5	108.8	103.40	5'5"
+26.1	=Δ 10' E. of ℄ of Fay		11.9	108.4	103.0	5'5"
+50			11.7	108.6	103.90	4'8"
30			10.2	110.1	105.88	4'3"
+50			8.2	112.1	107.86	4'3"
31			6.2	114.1	109.84	4'3
+50			4.2	116.1	111.82	4'3"
32			2.3	118.0	113.80	4'3"
+50	12.97	133.04	0.26	120.07	115.78	4'3"
33			11.2	121.8	117.76	4'0"
+50	break		9.4	123.6	119.75	3'9"

133.04

34	break		7.6	125.4		121.0	4'5"
+50			6.2	126.8		122.54	4'3"
35			4.6	128.4		124.08	4'4"
+50			3.1	129.9		125.62	4'3"
36			1.6	131.4		127.16	4'3"
	12.76	145.73	0.07	132.97			
+50			12.6	133.4		128.70	4'5"
37			11.0	134.7		130.24	4'5
+50			9.4	136.3		131.78	4'6"
38			7.9	137.8		133.32	4'6"
+50			6.6	139.1		134.86	4'3"
39			5.8	139.9		136.40	3'6"
+50			3.2	142.5		137.94	4'7"
40			2.0	143.7		139.48	4'3"
+50	break		0.3	145.4		141.0	4'5"
	7.65	153.52	+0.14	145.87	BM.		
41	break		7.8	145.7		142.0	3'8"
+50			7.6	145.9		142.13	3'9"
42			7.2	146.3		142.25	4'0"
+50			7.0	146.5		142.37	4'2"
43			6.6	146.9		142.5	4'5"
+50			6.5	147.0		142.62	4'4"
44			6.2	147.3		142.75	4'6"
+50			5.9	147.6		142.87	4'9"
45			5.5	148.0		143.0	5'0"
+50			5.1	148.4		143.12	5'3"
46			4.8	148.7		143.25	5'5"
+50			3.9	149.6		143.37	6'3"

℄ Fay ℄ of ditch

stakes set 14' E of ℄

47		153.52	31	150.4	143.5		6'10"
+50			2.2	151.3	143.62		7'8"
48			1.3	152.2	142.75		9'5"
+50			1.2	152.3	142.87		9'5"
49	break		5.8	147.7	144		3'7"
+50			4.7	148.8	143.55		5'3"
50	1.10	154.32	0.30	153.22	143.10		10'1"
+50			0.6	153.7	142.65		11'0"
51			5.0	149.3	142.20		7'1"
+50			5.5	148.8	141.75		7'0"
52			8.5	145.8	141.3		4'6"
+30.1 =	10'3.0 x NL	Prospect Park	8.00	146.32	141.0		5'4"
53	068	14648	2.9	43.6	139.65		4'0"
+50			5.3	41.2	138.52		2'8"
54			6.1	40.4	137.4		3'0"
+50			7.9	38.6	134.73		3'11"
55			10.2	36.3	132.07		4'3"
+50	0.26	33.98	12.76	33.72	129.40		4'1"
56			3.2	30.78	126.74		4'1"
+50			6.5	27.48	124.07		3'5"
57			8.1	25.88	121.41		4'6"
+50	0.43	21.59	13.63 13.0	20.35 20.96	118.74		1'7"
58			5.1	16.5	116.08		0'5"
+50			4.0	17.6	113.71		3'11"
59			6.5	15.1	110.75		4'4"
+50			8.2	13.4	108.38		5'0"

		21.59	60	9.8	11.8	105.4	6'5"
			+50	11.9	9.7	103.7	6'0"
	0.37	109.14	61	12.82 1.6	8.77 07.5	101.99	5'6"
			+50	4.0	10514	100.29	4'10"
			62	6.8	10234	98.58	3'9"
			+50	8.4	10074	96.88	3'11"
			63	10.2	98.94	95.17	3'9"
			+50	11.8	9734	93.47	3'11"
	0.10	96.41	64	12.83 1.0	9631 954	91.76	3'8"
			+50	2.7	93.7	90.06	3'8"
			65	4.2	92.2	88.35	3'10"
			+50	5.8	90.6	86.65	4'0"
			66	7.4	89.0	8494	4'1"
			+50	8.7	87.7	83.24	4'5"
			67	11.6	848	81.53	2'4"
	1.07	84.78	+50	12.1 12.70	84.3 83.71	79.83	4'6"
			68	1.87	2.9	78.13	4'9"
			+50	3.6	81.18	76.42	4'9"
			+91.8	6.5	78.28	75.0	

4/15/22 Gregory Moore Miller Shaw

CROSS SECTION of Alley bet Vermont & Richmond and ✓ Essex & University — 20' wide

299.79 299.94 297.15 SW Richmond & Univ.

West Curb Line Richmond St

N.L.	on cement Curb	3.76	296.18
S.L.	" " "	3.83	296.11

N.L. Richmond

N.	on cement Curb	3.48	296.46
C		3.6	296.34
S	on cement Curb	3.56	296.38

25' W.

S		4.1	295.84
C		3.7	296.2
N		3.8	296.1

Platted HRB. 12/30/52 ✓

63' W

N		4.2	295.5
C		4.2	295.5
S	Garage dirt floor	4.2	295.5

100' W

S	Garage board floor	4.9	295.0
C		4.8	295.1
N		4.8	295.1

135' W

N		4.9	295.0
C		5.0	294.9
S	sidewalk to house	5.2	294.7

163' W

S	Garage dirt floor	6.0	293.9 ✓

299.94

C		.59	294.0
N		.56	294.3

182' W.

N	Garage dirt floor	6.1	293.8
C		6.2	293.7
S		6.1	293.8

200' W

S	walk to house	6.1	293.8
C		6.5	293.4
N		6.5	293.4

240' W

N		7.1	292.8
C		7.0	292.9
S	garage dirt floor	7.0	292.9

300' W

S		7.8	292.1
C		7.8	292.1
N		7.8	292.1

350' W

N		8.6	291.3
C		8.5	291.4
S		8.5	291.4

400' W

S	garage dirt floor	9.0	290.9
C		9.0	290.9
N		8.8	291.1 ✓

299.94

435' W

N	garage dirt floor	9.6	290.4
C		9.6	290.3
S		9.5	290.4

475' W

Platted 12/20/24 JB

S		10.1	289.8
C		10.1	289.8
N		10.2	289.7
	293.35		
T.P.	3.2 W (293.45)	9.81	290.13

512' W

N	garage dirt floor	3.6	289.8
C		3.3	290.1
S		3.4	290.0

544' W

S	garage dirt floor	3.3	290.1
C		3.4	290.0
N	garage dirt floor	3.7	289.7

600.7' W = EL Vermont

N		3.6	289.8
C		3.6	289.8
S		3.6	289.8

E. cb Line Vermont

S	on cement Cb	3.84	289.51
N	" "	3.64	289.71

Alley Curbs run on ½ from E. Cb of Vermont to W. edge of sidewalk which is 5' E of E. cb of Vt.

289.71
3.64
293.35

12/17/22 Gregory Moore Ellis Shaw — Reconnaissance of a portion of Alley Blk 10 Brookes

	2.16	279.43	277.27	B.P. NW 3rd & Brookes

see page 14 for sections on N.L. Brookes

and 550 S. of Penns'l.

T.P.	2.60	274.17	7.86	271.57

530' S. of Penns'l.

W	3.9
C.	3.8
E	4.5

500' S. of Penns'l.

E	4.7	
C	4.8	269.4
+4	4.9	
W	6.6	
+10	13.0	

468' S. of Penns'l.

-5	11.0
W	5.9
+3	4.2
C	4.7
E	4.8

466' S.

E	4.8
C	4.7
W	4.4

450' S. of Penns'l.

W	4.1
C	4.2
E	4.3

430' S. of Penns'l.

E	2.4
C	2.6
W	2.4

T.P.	7.28	280.40	105	273.12

400' S. of Penns'l.

W	5.8
C	5.7
E	6.0

For sections from here to Penns'l.

see page 12

4/24/24 Gegory. Levels on Curb Date St
To establish Grades

	10.25	170.23		159.98	BP SW 8th & Cedar
	8.33	165.57	12.99	157.24	
S.L. of Park and 14' E of W.L of 9th			10.43	55.14	on curb
This curve is 30' Radius					
16' W. of W.L. of 9th and 32.5' N. of S.L. of Park.			7.99	57.56	✓ ✓
50 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓			5.90	59.67	✓ ✓
75 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓			4.46	61.11	✓ ✓
100 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓			3.18	62.39	✓ ✓
125 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓			2.16	63.41	✓ ✓
150 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓			1.39	64.18	✓ ✓
175 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓			0.84	64.73	✓ ✓
200 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ = E.L. 8th			0.61	64.96	
?					52' between curbs
14' E of E.L. 9th & S.L. of Park			11.70	53.87	on curb
16' W. ✓ W.L. ✓ & 34.5 N. of S.L. of Park.			6.30	59.27	
50 ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓			4.98	60.59	
75 ditto			4.05	61.52	
100 ✓			3.18	62.39	
125 ✓			2.30	63.27	
150' ✓			1.41	64.16	
153' ✓ = P.C.			1.29	64.28	
T.P.	1.90	166.82	0.65	164.92	
14' W of E.L. 8th & 22.3 N. of S.L. of Park.			1.82	65.0	= 10' S. of Park Cb.
✓ ✓ ✓ ✓ ✓ ✓ ✓ S.L. of Park.			1.87	64.95	
14' E ✓ W.L. ✓ ✓ ✓ ✓ ✓			1.89	64.93	
✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ and 21.5 N. of S.L. of Park			1.53	65.29	
4' E ✓ ✓ ✓ ✓ ✓ ✓ ✓ 31.5 ✓ ✓ ✓ ✓ ✓			1.58	65.24	= break in grade

and the grade is straight from last above to the next below

4' W. of E.L. 7th & 31.5 N. of S.L. of Park.	9.58	157.24	= break.
14' ✓ ✓ ✓ ✓ ✓ ✓ & 21.5 ✓ ✓ ✓ ✓ ✓ ✓	9.46	157.36	
14 ✓ ✓ ✓ ✓ ✓ ✓ ✓ S.L. of Park	9.20	157.62	
50' W. of W.L. 8th & 83.5 N. of S.L. of Park.	3.23	163.59	
Grade is straight from here to Next Reading on the North Side			
14' E of W.L. of 7th & S.L. of Park	12.15	154.67	
14 ✓ ✓ ✓ ✓ ✓ ✓ ✓ 21.5 N. of S.L. Park	12.44	154.38	
4' ✓ ✓ ✓ ✓ ✓ ✓ ✓ 31.5 ✓ ✓ ✓ ✓ ✓	13.00	153.82	= break.
TP 0.24 154.06	13.00	153.82	
93' E of E.L. of 6th and 83.5 N. of S.L. of Pk.	5.23	148.83	
TP 4.00 147.99	10.07	143.99	
E.L. of 7th & 31.5 N. of S.L. of Park	4.57	143.42	
✓ Curb Line of 7th 17.5 ✓ ✓ ✓ ✓ ✓ ✓	5.95	142.04	
✓ ✓ ✓ ✓ ✓ and ✓ ✓ ✓ ✓	6.77	141.22	
W ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓ ✓	6.75	141.24	
✓ ✓ ✓ ✓ ✓ 17.5 N. of ✓ ✓ ✓ ✓	5.73	142.26	
S. Cb Line of Date & W.L. of 7th	5.83	142.16	
9' E of E.L. of 7th & N cb of Date = P.C.	3.41	144.58	
36' N. of N.L. of Date and E. Cb of 6th	4.11	143.88	= E.C.
12.07 153.76		141.69	BP NW 5th & Elm
S.L. of Elm & E Cb of 6th	4.02	149.74	
N.L. ✓ ✓ ✓ ✓ ✓ ✓ 6th	1.86	151.90	
TP 12.50 165.56	0.70	153.06	
10' S. of S.L. of Fir & E cb of 6th	4.73	160.83	N End of = Cb. on E

see page 71 for Cb bet Fir & Grape

Gregory, Moore, Miller, Shaw

Cross Section on E & W Alley, 20' wide, Blk 39 H.M. Higgins Add.

on B.M.	8.30	205.22	196.92	BP SW 26th St.
		N Cb. Line 26th St.		
S.		4.36	200.86	on cement.
N		3.98	201.24	" "
	Need. 10' Cb? on both Alley returns.			
		W L 26th St.		
N		3.8	201.4	
C		4.2	200.8	
S		4.2	201.0	
	25' W.			
S		4.3	200.9	
C		4.3	200.9	
N		3.8	201.4	
	50' W			
N		3.6	201.6	
C		4.0	201.2	
S		4.0	201.2	
	70' W.			
S		3.06	202.16	cement driveway
C		3.3	201.9	
N		3.2	202.0	
	93' W			
N		1.6	203.6	dirt center door
C		1.8	203.4	
S		1.4	203.8	
TP	11.48	216.30	0.40	204.82

See 1036-68 for N & S alley 216.30

	125' W		
S	9.3	207.0	
C	9.6	206.7	
N	9.1	207.2	Bldg. 1' in alley
	150' W		
N	5.9	210.4	Fence .1' in alley
C	6.4	209.9	
S	5.8	210.5	
	175' W		
S	3.9	212.4	
C	3.9	212.4	
N	3.7	212.6	Fence 1' in alley
	193' W		
N = center 16' door	3.4	212.9	dirt floor
C	3.7	212.6	
S	3.7	212.6	
	196' W		
C = Flush Tank.	3.83	212.47	
	215' W		
S	4.0	212.3	
C	3.8	212.5	
N	3.5	212.8	
	240' W		
N	4.8	211.5	Fence 1.1 in alley
C	5.0	211.3	
S	5.3	211.0	

216.30

	355' W		
S		6.1	210.2
C		5.8	210.5
N = center door dirt		5.7	210.6
	280' W		
N		6.9	209.4
C		7.1	209.2
S		7.1	209.2
	300' W		
S		7.5	208.8
C		7.5	208.8
N		7.6	208.8
	330' W		
-1.5 = cement floor		8.0	208.3
N		8.2	208.1
C		8.7	207.6
S		8.5	207.8
	355' W		
S = center door (dirt)		9.6	206.7
C		9.7	206.6
N		9.1	207.2
	400' W = E.L. of N+S Bldg		
N		10.6	205.7
C		11.3	205.0
+8.6 = N. side of Bldg		11.2	205.1

1' in alley

4/15/22

Levels on Cement Curb
West Side of 6th St

Curb is 36' E of W.L. Balboa Pk. Juniper to Date
bet S.L. Juniper & N.L. Hawthorn

	7.96	237.94		229.98	NW 5th Juniper
6' S. of S.L. Juniper = S. end of Curve into Jun. 0+00			1.09	36.85	
50' S			3.19	34.75	
100' S	0.13	232.80	5.27	232.67	
150' S			2.70	30.1	
200' S			5.32	27.48	
214.4' S			6.06	26.74	
250' S			8.68	24.12	
275' S			10.17	22.63	
289' S = N. end of Curve into Ivy			10.72	22.08	
W. This pt. lines up with Cb. Line of Ivy. & is 16' E of W.L. of Balboa Park.			10.38	22.42	
T.P.	0.43	220.41	12.82	219.98	
W. end of Curve into Ivy = S. Cb of Ivy.			0.67	19.74	
0+00 = S " " " " " = 6' S. of S.L. Ivy			2.62	17.79	
+50			4.88	15.53	
1+00			7.45	12.96	
+50			10.09	10.32	
2+00	0.42	208.21	12.62	207.79	
+50			2.99	205.22	
+88. = N end of 20' radius curve into Hawthorn. This curb is on N Cb Hawthorn.			5.02	203.19	
W end of " " " " "			6.02	202.19	
16' W of above pt = W.L. Balboa Pk			5.96	202.25	on N. cb Line Haw.
W. End of 20' radius curve on S. Cb. Hawthorn = W.L of Balboa Park.			8.54	199.67	
0+00 S. End of 20' radius curve = 6' S. of S.L. of Hawthorn.			9.72	198.49	

Curb from here to Date is 20 E of W.L. of Balboa Pk.

		208.21	3.92 / 4.19 / 8.49	4.19 / 197.79
0+50	6.73	202.68	12.26	195.95
1+00			9.37	193.31
+50			11.87	190.81
T.P.	0.24	190.22	12.70	189.98
2+00			1.92	188.30
+50			4.62	185.60
+89 = N. End of 20' radius Curve into Grape = 6' N. of N.L. Grape.			6.66	183.56
W end of above curve " " = W.L. Balboa Pk & N. Cb Line of Grape.			8.29	181.93
W. end of 20' radius curve into Grape = W.L. Balboa Park & S. cb line Grape.			10.40	179.82
	0.72	178.74		
0+00 S end of 20' radius curve into Grape = 6' S of S.L. of Grape & 20' E of W.L. of Park.			12.20	178.02
0+50			2.85	175.89
0+60.5			3.28	175.46
1+00			5.55	173.19
+38			8.11	170.63
+67			8.92	169.82
2+00			10.50	168.24
T.P.	0.14	166.04	12.84	165.90
+50			0.24	165.80
+89 = N. end of 20' radius Curve into Fir = 20' E. of W.L. Balboa Pk & 6' N. of N.L. Fir			2.10	163.94
W. End of Above curve = W.L. of Park and N. cb of Fir.			3.36	162.68
W. End of 20' radius Curve into Fir = S. Cb of Fir + W.L. of Park			5.11	160.93

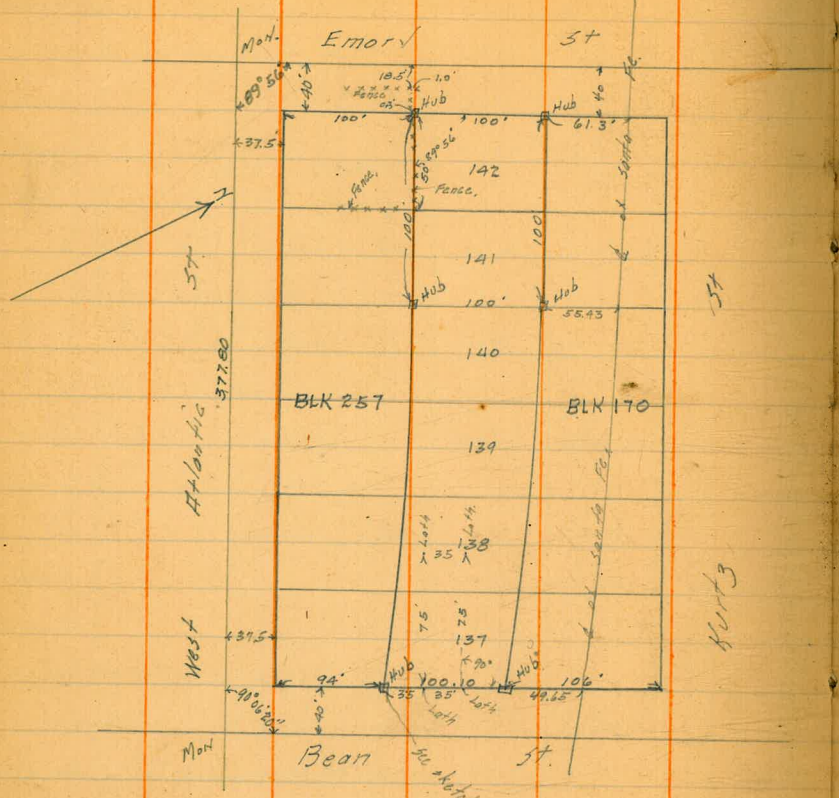
14217

	166.02			
0+00 = S End of 20' rad. Curve =				
6' S. of S.L. Fir + 20' E of W.L. Park.		5.71	160.33	
1+00		8.66	157.38	
2+00		11.53	154.51	
TR 1.01 20' radius	154.13	12.92	153.12	
+ = N. end of Curve into Elm =				
6' N. of N.L. of Elm and 20' E. of W. L. Park.		2.12	152.01	
W. end of above curve = " " "				
and N. cb. of Elm		3.13	151.00	
W. end of 20' radius curve =				
W.L. of Park + S. cb of Elm		4.53	149.60	
0+00 = S End of 20' radius curve into				
Elm = 6' S. of S.L. Elm + 20' E of W.L. Park		4.73	149.40	
1+00		7.41	146.72	
2+00		10.13	144.00	
2+94.5 = N. end of 14' radius curve				
into Date = N.L. of Date + 20' E. of W.L. Park.		12.66	141.47	
W. end of 14' radius curve into Date =				
W.L. Park + N cb Line of Date.		12.97	141.16	
chk B.M.		12.02	142.11	B.P. SW 6th + Date. = 142.17

4/27/22

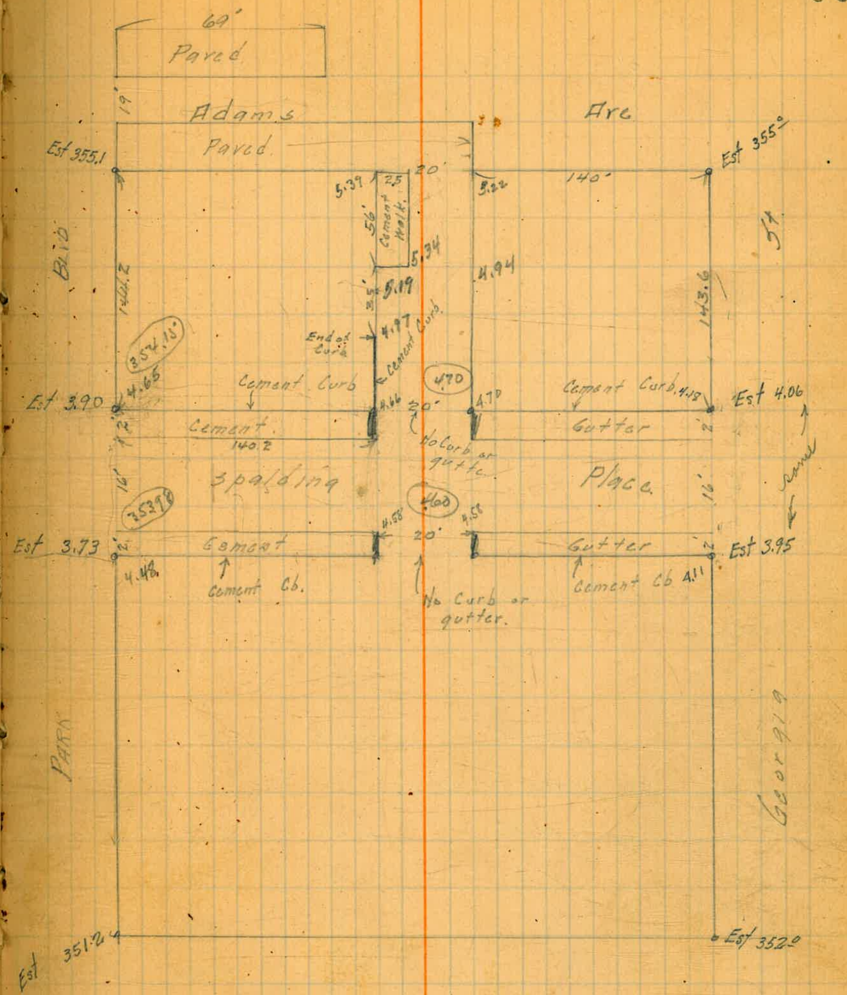
Gregory
Moore
Miller
Shaw

Survey of R. o W. Lots
137 to 142 inclusive



5/2/22 Gregory / Moore / Miller / Shaw — Levels on Curb (Cement) Spalding Place.

	3.68	358.26 ✓		354.58	B.P. NE Adams
W.L. Park Blvd.				—	
S cb			3.78	354.48	
N cb			3.61	354.65	
		140.2' E			
N. cb			3.60	54.66	
S. cb			3.68	54.58	
		160.2 E			
S cb			3.68	354.58	
N cb			3.56	354.70	
		300' E = W.L. Georgia			
N cb			4.08	354.18	St. cb is .27 higher
S cb			4.15	354.11	St. cb is .09 higher
		Levels on N + S Alley in same block			
		from S.L. Adams to Spalding Pl.			
	4.74	359.32 ✓		354.58	
		S.L. Adams			
W.L			3.93	355.39	on alley curb
E.L.			4.10	355.22	" " "
		56' S			
Outside edge of walk.			3.98	55.34	
		61' S. = Center of Drive to Garage on E			
E.L.			4.38	54.94	
		68' S = Center of Drive to Garage on W.			
W.L.			4.13	55.19	
		91' S			
W.L on W. Cement Curb			4.35	54.97	

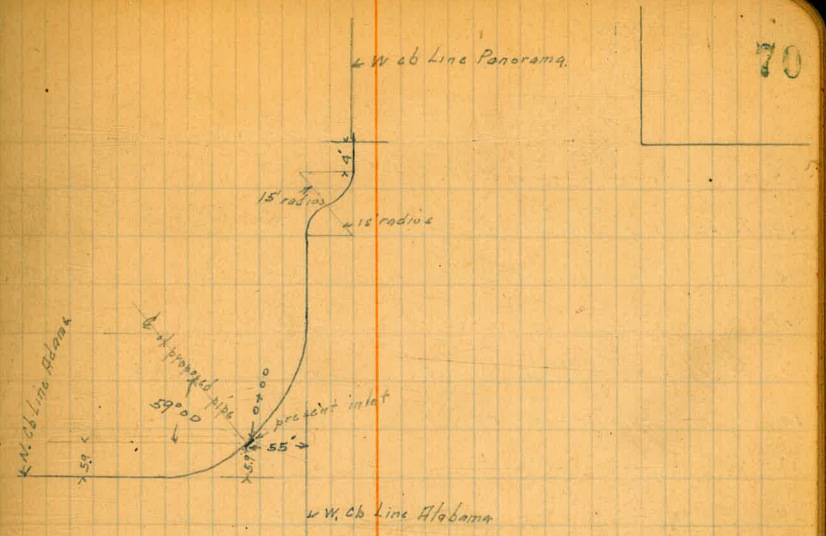


5/6/22 Gregory Moore Miller Shaw — Levels on curb S. Side Adams Ave Alabama to Florida

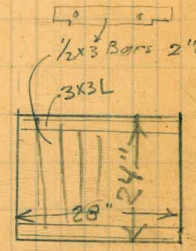
	W.L.	342.64	340.00	BP SW Florida
E.L. Florida on Curb, =00		3.70	338.94	
50 E. of 0+00		4.20	38.44	
60 " "		4.35	38.29	
100 " "		4.38	38.26	
125 " "		4.49	38.15	
150 " " = W.L. Alley N		4.72	37.96	* See opposite for Catch Basin.
170 " " = E.L. Alley noreturn in		5.22	37.42	
195 " "		4.60	38.04	
225 " "		4.54	38.10	
250 " "		4.38	38.26	
310 " " = W.L. Alabama		4.26	38.36	

Levels for proposed pipe shown on opposite page

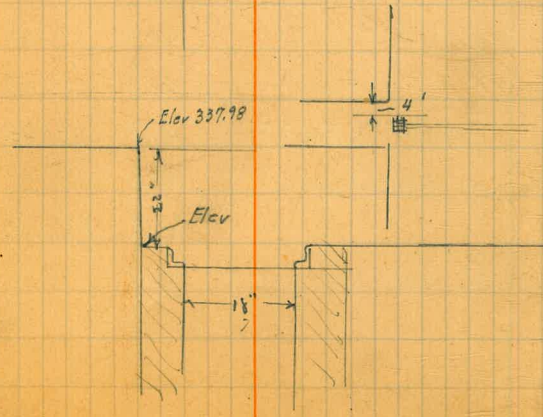
0+00 = Inlet and of pipe	Rd.	342.64	338.39	= Top of Curb
0+10.5		4.04	38.60	
0+14		4.6	38.04	
0+19		7.2	35.42	
0+25		13.2	29.42	
T.P.	0.53	330.36	1.81	329.83
0+35			8.4	22.0
0+50			16.3	14.1



ADAMS AVE



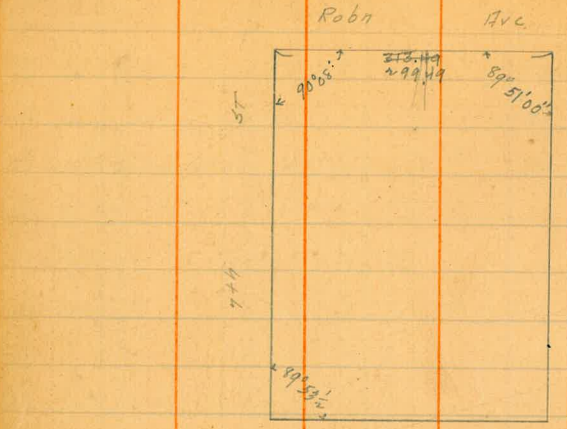
ALABAMA



4/24/24 Category Curb Levels on 6th St Fir to Grape

HI 165.56 from page 63

N. Cb Line of Fir + WL of Park = PC.	2.90	162.66	
10' N.E. on 20' Radius Curve.	2.31	163.25	
6' N. of NL of Fir on Wab Line of 6th	1.59	163.97	= EC.
20' " " " " " " "	1.00	164.56	
T.P. 1.30 176.86	1.00	164.56	
40' N. of NL of Fir on Wab Line of 6th	11.32	165.54	
60' " " " " " " "	10.31	166.55	
80 " " " " " " "	9.31	167.55	
100 " " " " " " "	8.40	168.46	
120' " " " " " " "	7.40	169.46	
140 " " " " " " "	6.68	170.18	
156 " " " " " " "	6.31	170.55	
180 " " " " " " "	4.70	172.16	
200 " " " " " " "	3.44	173.42	
220 " " " " " " "	2.37	174.49	
235 " " " " " " "	1.43	175.43	
240 " " " " " " "	1.22	175.64	
260 " " " " " " "	0.43	176.43	
TP 5.92 182.35	0.43	176.43	
280' N. of NL of Fir on W Cb Line of 6th	5.23	177.12	
294 " " " " " " "	4.42	177.93	= PC.
S. Cb Line of Grape + WL of Park	2.57	179.78	= EC.



IMPROVED TABLES

AND

INFORMATION

Table II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find **c, B, A.**
Use Law of Lines.

Given A, B, c; to find **a, b, C.**
Use Law of Lines.

Given a, b, c; to find A, B, C.

Let $\frac{a+b+c}{2} = s$, $\sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$

$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$

$\tan \frac{1}{2} A = \frac{r}{s-a}$

$\tan \frac{1}{2} B = \frac{r}{s-b}$

$\tan \frac{1}{2} C = \frac{r}{s-c}$

Area of a triangle:

Area $= \frac{1}{2}$ ab Sin C

Area $= \sqrt{s(s-a)(s-b)(s-c)}$

PRISMOIDAL FORMULA.

Vol. $= \frac{h}{6}(B+b+4M)$

h = altitude; b, B = bases; M = midsection

Table III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
1/16	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	1/16
1/8	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	1/8
3/16	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	3/16
1/4	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	1/4
5/16	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	6927	.7760	.8594	.9427	5/16
3/8	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	3/8
7/16	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	7/16
1/2	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	1/2
9/16	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	9/16
5/8	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	5/8
11/16	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	11/16
3/4	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	3/4
13/16	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	13/16
7/8	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	7/8
15/16	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	15/16
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

Table IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

360° = 21600′ = 1296000″
Radius = arc of 57.2957790°
Arc of 1° (radius = 1) = .017453292
Arc of 1′ (radius = 1) = .000290888
Arc of 1″ (radius = 1) = .000004848

$\pi = 3.141592654$ $\qquad \sqrt{\frac{1}{4}} = 0.564190$

$\frac{\pi}{4} = 0.785398163$ $\qquad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$

$\frac{\pi}{6} = 0.523598776$ $\qquad \pi^2 = 9.869604401$

$\sqrt{\frac{4}{\pi}} = 1.128379167$ $\qquad \frac{1}{\pi^2} = 0.101321184$

$\frac{\pi}{6} = 0.523598776$ $\qquad \sqrt{\pi} = 1.772453851$

$\frac{4.\pi}{3} = 4.188790205$ $\qquad \frac{1}{\pi} = 0.3183099$

Curvature of Earth's surface = about 0.7 feet in 1 mile
Curvature in feet = 0.667 (Dist. in miles)²
Difference between arc and chord length, 0.05 feet in 11½ miles

Probable error of a single observation $= 0.6754 \sqrt{\frac{\Sigma v^2}{n-1}}$

Error in chaining of 0.01 feet in 100 feet:
Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

Horizontal Distance $= R - R \sin^2 a + C \cos a$
Vertical Distance $= R \frac{1}{2} \sin 2a + C \sin a$

$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.
a = angle of elevation for mid Reading

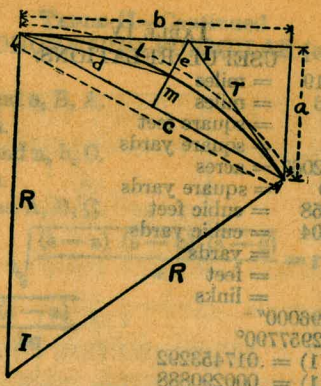


Table V

CURVE FORMULAE FOR SIMPLE CURVES

Compiled by J. Calvin Locke, C.E.

(1) $c = \sqrt{2Ra}$ (2) $c = \sqrt{a^2+b^2}$

(3) $c = \sqrt{2R\,(R-\sqrt{(R+b)\,(R-b)}} = \sqrt{2R(R-\sqrt{R^2-b^2})}$

(4) $c = 2\sqrt{m\,(2R-m)}$

(5) $c = 2R \sin \frac{1}{2} I$ (6) $c = 2T \cos \frac{1}{2} I$

(7) $e = R \operatorname{exsec} \frac{1}{2} I$

(8) $e = R \tan \frac{1}{2} I \tan \frac{1}{4} I$ (9) $e = T \tan \frac{1}{4} I$

(10) $b = \sqrt{a\,(2R-a)}$

(11) $b = \sqrt{\left(c+\frac{c^2}{2R}\right)\left(c-\frac{c^2}{2R}\right)} = \sqrt{c^2-\frac{c^4}{4R^2}}$

(12) $b = R \sin I$ (13) $b = a \cot \frac{1}{2} I$

(14) $R = \frac{a^2+b^2}{2a} = \frac{c^2}{2a}$ (15) $R = \frac{d^2}{2m} = \frac{c^2+4m^2}{8m}$

(16) $d = \sqrt{R\,(2R-\sqrt{(2R+c)\,(2R-c)}} = \sqrt{R(2R-\sqrt{4R^2-c^2})}$

(17) $d = \sqrt{2Rm}$ (18) $d = 2R \sin \frac{1}{4} I$ (19) $m = \frac{d^2}{2R}$

(20) $m = R \mp \sqrt{\left(R+\frac{c}{2}\right)\left(R-\frac{c}{2}\right)} = R \mp \sqrt{R^2-\frac{c^2}{4}}$

(21) $m = R \operatorname{vers} \frac{1}{2} I$ (22) $m = R \sin \frac{1}{2} I \tan \frac{1}{4} I$ (23) $m = \frac{1}{2} c \tan \frac{1}{4} I$

(24) $a = \frac{c^2}{2R}$ (25) $a = R - \sqrt{(R+b)\,(R-b)} = R - \sqrt{R^2-b^2}$

(26) $a = 2R\,(\sin^2 \frac{1}{2} I)^2$ (27) $a = R \operatorname{vers} I$ (28) $a = R \sin I \tan \frac{1}{2}$

(29) $a = b \tan \frac{1}{2} I$ (30) $a = T \sin I$ (31) $T = R \tan \frac{1}{2} I$

(32) $I = \frac{L}{R} \times 57.295780$ (33) $R = \frac{L}{I} \times 57.295780$

(34) $L = IR \times 0.01745329$ (35) $L = \frac{8d-c}{3}$

(36) Area Seg. $= \frac{LR - R^2 \sin I}{2} = \frac{LR - Rb}{2}$

Table VI

SINES, COSINES, TANGENTS, COTANGENTS

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
0	0000	0000	0029	0029	0058	0058	0087	0087	0116	0116	0145	0145	89
1	175	0175	0204	0204	0233	0233	0262	262	291	291	320	320	88
2	349	349	378	378	407	407	436	437	465	466	494	495	87
3	523	524	552	553	581	582	610	612	640	641	669	670	86
4	698	699	727	729	756	758	785	787	814	816	843	846	85
5	872	875	901	904	929	934	958	963	987	992	1016	1022	84
6	1045	1051	1074	1080	1103	1110	1132	1139	1161	1169	190	198	83
7	219	228	248	257	279	287	305	317	334	346	363	376	82
8	392	405	421	435	449	465	478	495	507	524	536	554	81
9	564	584	593	614	622	644	650	673	679	703	708	733	80
10	736	763	765	793	794	823	822	853	851	883	880	914	79
11	908	944	937	974	965	2004	994	2035	2022	2065	2051	2095	78
12	2079	2126	2108	2156	2136	186	2164	217	193	247	221	278	77
13	250	309	278	339	306	370	334	401	363	432	391	462	76
14	419	493	447	524	476	555	504	586	532	617	560	648	75
15	588	679	616	711	644	742	672	773	700	805	728	836	74
16	756	867	784	899	812	931	840	962	868	994	896	3026	73
17	924	3057	952	3089	939	3121	3007	3153	3035	3185	3062	217	72
18	3090	249	3118	281	3145	314	173	346	201	378	228	411	71
19	256	443	283	476	311	508	338	541	365	574	393	607	70
20	420	640	448	673	475	706	502	739	529	772	557	805	69
21	584	839	611	872	638	906	665	939	692	973	719	4006	68
22	746	4040	773	4074	800	4108	827	4142	854	4176	881	210	67
23	907	245	934	279	961	314	987	348	4014	383	4041	417	66
24	4067	452	4094	487	4120	522	4147	557	173	592	200	628	65
25	226	663	253	699	279	734	305	770	331	806	358	841	64
26	384	877	410	913	436	950	4462	986	488	5022	514	5059	63
27	540	5095	566	5132	592	5169	617	5206	643	243	669	280	62
28	695	317	720	354	746	392	772	430	797	467	823	505	61
29	848	543	874	581	899	619	924	658	950	696	975	735	60
30	5000	774	5025	5812	5050	851	5075	890	5100	930	5125	969	59
31	150	6009	175	6048	200	6088	225	6128	250	6168	275	6208	58
32	299	249	324	289	348	330	5373	371	398	412	422	453	57
33	446	494	471	536	495	577	519	619	544	661	568	703	56
34	592	745	616	787	640	830	664	873	688	916	712	959	55
35	736	7002	760	7046	783	7089	807	7133	831	7177	854	7221	54
36	878	265	901	310	925	355	948	400	972	445	995	490	53
37	6018	536	6041	581	6065	627	6088	673	6111	720	6134	766	52
38	157	813	180	860	202	907	225	954	248	8002	271	8050	51
39	293	8098	316	8146	338	8195	361	8243	383	292	406	342	50
40	428	391	450	441	472	491	494	541	517	591	539	642	49
41	561	693	583	744	604	796	626	847	648	899	670	952	48
42	691	9004	713	9057	734	9110	756	9163	777	9217	799	9271	47
43	820	325	841	380	862	435	884	490	905	545	926	601	46
44	947	657	967	713	988	770	7009	827	7030	884	7050	942	45
45	7071	1.0000	7092	1.0058	7112	1.0117	133	1.0176	153	1.0235	173	1.0295	44
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	20 cot	10′ cos	10′ cot	deg.

Table VI (continued)

SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	30′ cot	10′ cos	10′ cot	deg.

TABLE VII

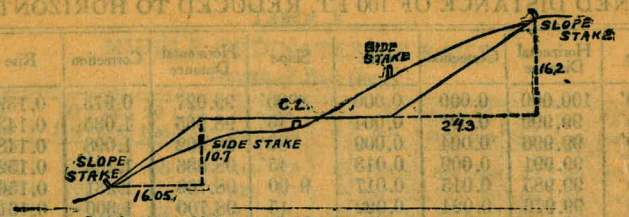
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16—6	21	346—6	41	676—6	61	1006—6	81	1336—6
2	33—0	22	363—0	42	693—0	62	1023—0	82	1353—0
3	49—6	23	379—6	43	709—6	63	1039—6	83	1369—6
4	66—0	24	396—0	44	726—0	64	1056—0	84	1386—0
5	82—6	25	412—6	45	742—6	65	1072—6	85	1402—6
6	99—0	26	429—0	46	759—0	66	1089—0	86	1419—0
7	115—6	27	445—6	47	775—6	67	1105—6	87	1435—6
8	132—0	28	462—0	48	792—0	68	1122—0	88	1452—0
9	148—6	29	478—6	49	808—6	69	1138—6	89	1468—6
10	165—0	30	495—0	50	825—0	70	1155—0	90	1485—0
11	181—6	31	511—6	51	841—6	71	1171—6	91	1501—6
12	198—0	32	528—0	52	858—0	72	1188—0	92	1518—0
13	214—6	33	544—6	53	874—6	73	1204—6	93	1534—6
14	231—0	34	561—0	54	891—0	74	1221—0	94	1551—0
15	247—6	35	577—6	55	907—6	75	1237—6	95	1567—6
16	264—0	36	594—0	56	924—0	76	1254—0	96	1584—0
17	280—6	37	610—6	57	940—6	77	1270—6	97	1600—6
18	297—0	38	627—0	58	957—0	78	1287—0	98	1617—0
19	313—6	39	643—6	59	973—6	79	1303—6	99	1633—6
20	330—0	40	660—0	60	990—0	80	1320—0	100	1650—0

Table VIII

LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0- 7.92	18	11-10.56	35	23- 1.20	52	34- 3.84	69	45- 6 48	86	56- 9 12
2	1- 3.84	19	12- 6.48	36	23- 9.12	53	34-11.76	70	46- 2 40	87	57- 5 04
3	1-11.76	20	13- 2.40	37	24- 5.04	54	35- 7.68	71	46-10 32	88	58- 0 96
4	2- 7.68	21	13-10.32	38	25- 0.96	55	36- 3.60	72	47- 6.24	89	58- 8.88
5	3- 3.60	22	14- 6.24	39	25- 8.88	56	36-11.52	73	48- 2 16	90	59- 4 80
6	3-11.52	23	15- 2.16	40	26- 4.80	57	37- 7.44	74	48-10.08	91	60- 0 72
7	4- 7.44	24	15-10.08	41	27- 0.72	58	38- 3.36	75	49- 6.00	92	60- 8.64
8	5- 3.36	25	16- 6.00	42	27- 8.64	59	38-11.28	76	50- 1.92	93	61- 4 56
9	5-11.28	26	17- 1.92	43	28- 4.56	60	39- 7.20	77	50- 9.84	94	62- 0.48
10	6- 7.20	27	17- 9.84	44	29- 0.48	61	40- 3 12	78	51- 5.76	95	62- 8 40
11	7- 3.12	28	18- 5.76	45	29- 8.40	62	40-11.04	79	52- 1.68	96	63- 4 32
12	7-11.04	29	19- 1.68	46	30- 4.32	63	41- 6.96	80	52- 9.60	97	64- 0 24
13	8- 6.96	30	19- 9.60	47	31- 0.24	64	42- 2.88	81	53- 5.52	98	64- 8.16
14	9- 2.88	31	20- 5.52	48	31- 8.16	65	42-10.80	82	54- 1.44	99	65- 4.08
15	9-10.80	32	21- 1.44	49	32- 4.08	66	43- 6.72	83	54- 9.36	100	66- .000
16	10- 6.72	33	21- 9.36	50	33- 0.00	67	44- 2.64	84	55- 5.28	101	66 -7.92
17	11- 2.64	34	22- 5.28	51	33- 7.92	68	44-10.56	85	56- 1.20	102	67- 3.84



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19.35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54.15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57.75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58.95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61.80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

Prospect + LaJolla Blvd

NE 68.00

Sec A
+ 20

318.8 = Express

+6707 = st

5L
+50
1+00
+348 = st.

55 : 40 :: x : 3146

55 : 3146 : x : 40

44 : x :: 3146 : 40

52 : x :: 3146 : 40