

1079

1079

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FIELD BOOK

385

MICROFILMED

DEC 21 1964



Cement

- A 24" Pipe 20' North of road - runs East along road to point just above dam
- B 12" Corr Pipe starts 5' W of Road 2 C.Bs
- C 12" Corr Pipe at path across canyon



11/5/50  
Gregory  
Miller  
Shaw  
Dorval.

Survey of Pershing Drive  
Thru Balboa Park.

00221

12+55.68 E.C. ✓

R = 500

12+10 Δ 10°30' L

st = 45.95 ✓

lc = 91.63 ✓

11+64.05 ✓ - P.C.

693.77

5+97.47 ✓ E.C.

R = 230'

(5+22.95) Δ 39°48' L

st = 93.26 ✓

lc = 159.77 ✓

4+39.72 ✓ P.C.

475.35 ✓

2+14.30 P.T. ✓

R = 170'

1+17.30 Δ 88°52' R

st = 166.67 ✓

lc = 263.67 ✓

-0+49.37 P.C.

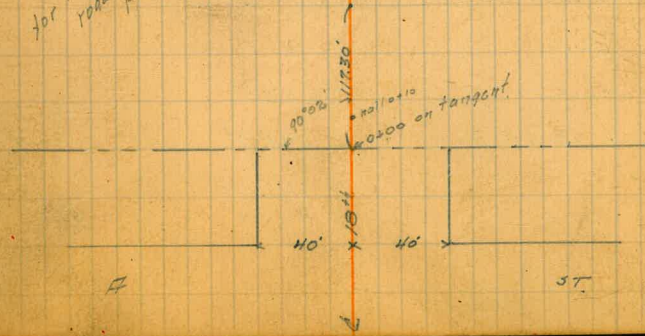
Δ = 72° 1' 31" ✓  
to park the

166.67

1466  
1467  
1468



see page 7  
for location of  
roads at this  
point





see last page for change

26+97.84 E.C. 26+96.66

$R=500$

26+50.0  $\Delta$   $11^{\circ}00'R$  10+335  $st=48.15$  46.95 58.44  
changed to  $13^{\circ}20'R$

$LC=35.99$  22.61

26+01.35 = PC. 26+03.05

22+14.44 E.C.

$R=230$

21+22.40  $\Delta$   $49^{\circ}06'L$

$st=105.06$

$LC=197.10$

20+17.34 PC

540.62

17+97.5 = End of Bridge

17+54.70 = End of Bridge

17+54.61 E.C.

$R=630$

16+82.09  $\Delta$   $13^{\circ}15'R$

$st=73.17$

$LC=145.69$

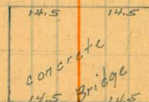
$E=2.23$

16+08.92 PC.

472.36

6 3720

121  
0067  
630  
50160  
4032  
423260





52+33.450 P.O.T.

$48+28.29 = EC.$   
 $46+93.96 = 46+93.99$  Equation  
 $46+95.46 EC.$

$45+77.0 \Delta 76^{\circ} 13' R.$   
 $45+89.59$

$44+16.12 PC.$   
 $44+49.0$

$R = 185^{\circ}$   
 $st = 145.19$  23870 L of Curur  
 $Ex = 48.39$

see last page for change from here

970.82

$x \quad 40 \quad x \quad 30 \quad 90^{\circ} 00'$

38+99.40 P.O.T.

34+57.34 E.C. 34+33.51

$32+95.06$  13' 43 38  
 $32+99.30 \Delta 13^{\circ} 40' L$

$P = 1500.00$   
 $st = 179.25$  17612  
 $EC = 357.79$  350.29

30+99.55 PC. 30+99.55

1299.61

639.61

$19' \quad 19' \quad 90^{\circ} 00'$

$15.02 \quad 29.98 \quad 89^{\circ} 10'$



76 + 61.50 E.C. ✓

R = 700

75 + 71.4 Δ 14° 50' R.

st = 91.12 ✓

lc = 181.22 ✓

74 + 80.28 P.C. ✓

1336.35

64 + 76.29 E.C. ✓

R = 1200

62 + 41.4 Δ 22° 44' L

st = 241.24 ✓

lc = 476.13 ✓

60 + 00.16 P.C. ✓

741.50

56 + 28.75 E.C. ✓

R = 500

55 + 05.4 28° 54' L

st = 128.85 ✓

lc = 252.20 ✓

53 + 76.55 P.C. ✓

70 100  
10 200  
10 300

4





94+19.66  $\Delta$  55° 50' R.

R = 780  
ST = 413.25  
LC = 760.09

90+06.38 P.C.C.

88+87  $\Delta$  9° 29' R.

R = 1444.59  
ST = 119.93  
LC = 239.31

87+67.07 P.C.

86+51.35 E.C.

85+07.80  $\Delta$  53° 31' L

R = 350  
ST = 176.67  
LC = 327.2

83+31.13 P.C.

79+50 = End of Road to Arizona.

533.12

412.34

207.62

366 last page for change

48° 39' 29"

This the center of curve  
30' HUB 40' HUB on radius line

HUB 32

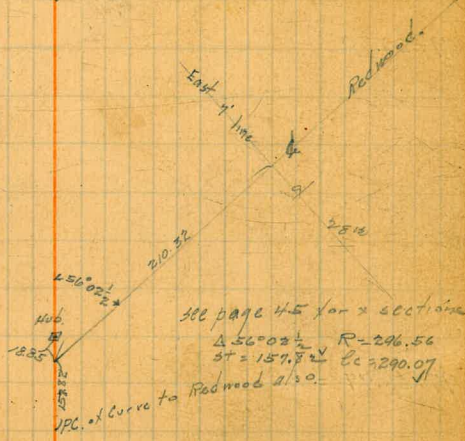
37 HUB on radius line

HUB 30

137 HUB

Defl. from 88 3° 20' to 89

60' 40"	90	9' E 14' W
85' 40"	91	10' E 18' W
Transit 11' 40"	92	11' E 20' W
Transit 16' 29"	93	11' E 18' W
00 - 19' 01"	94	12' E 17' W
Transit 22' 53"	95	12' E 17' W
00 + 22' 15' 01"	96	13' E 16' W
Transit 28' 34"	97	14' E 14' W
00 + 28' 12' 40"	98	14' E 14' W

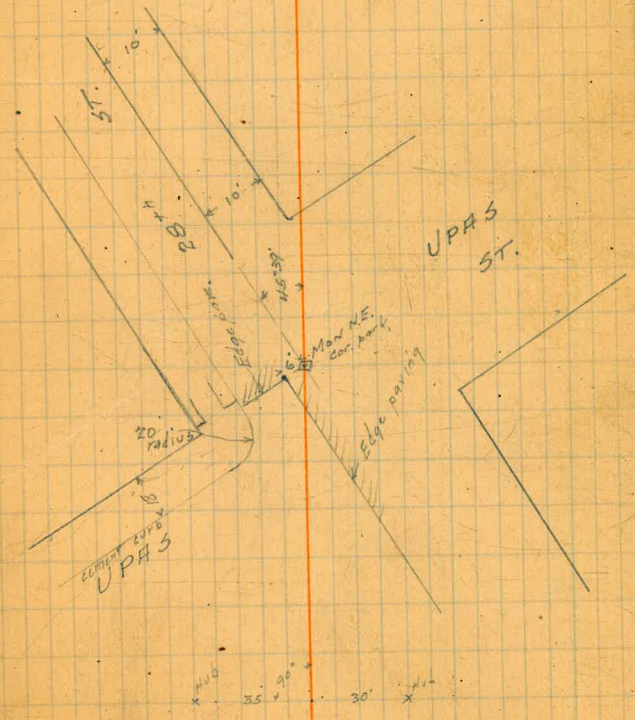




97+20.80

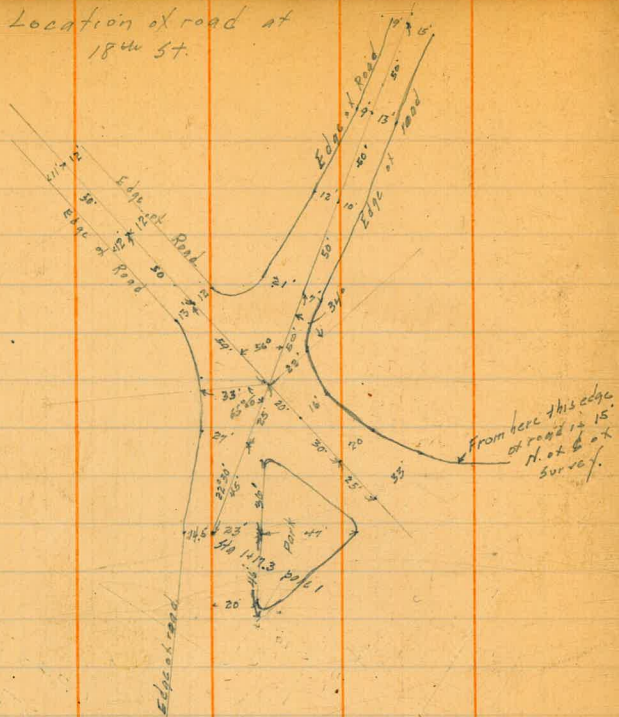
97+66.49 = E.C.

567-61





Location of road at  
18th St.



South line at 20' Bolton Park.

18th St. E. of Survey page 1



11/15/70

Gregory  
Miller  
Shaw  
Dorval

Levels on & Pershing Drive

09 B.M.	5.47	69.02 <sup>✓</sup>		63.55	B.P. SW. cor 17 <sup>th</sup> & Brady	(4' E = Wedge road	5.8	92.1	
	12.98	81.26 <sup>✓</sup>	0.74	68.28 <sup>✓</sup>		+70 = Wedge road ✓	5.9	92.0	
	9.36	90.62 <sup>✓</sup>	0.00	81.26		8+00	5.9	92.0	
- 0+4937 = P.C.			1.9	88.7		+50	5.9	92.0	
T.P.	882	99.35 <sup>✓</sup>	0.09	90.53 <sup>✓</sup>	N. End cb E side 18 <sup>th</sup> SLR	9	5.9	92.0	
0+00			8.6	90.8		+50	6.3	91.6	
+50			7.1	92.3		10	7.1	90.8	
1+00			6.4	93.0		+50	8.1	89.8	
1+50			5.9	93.5		11	9.1	88.8	
2			5.8	93.6		+50	10.4	87.5	
+1430 E.C.			5.8	93.6		T.P. 436	88.67 <sup>✓</sup>	11.54	86.31 <sup>✓</sup>
+50			5.7	93.7		12	2.1	86.6	
3			5.2	94.2		+50	3.2	85.5	
+50			4.2	95.2		13	4.1	84.6	
4			3.2	96.2		+50	4.7	84.0	
+50			2.9	96.5		14	Drain needed ✓	4.9	83.8
5			3.3	96.1		+50	4.8	83.9	
B.M.	2.68	97.95 <sup>✓</sup>	4.18	95.17 <sup>✓</sup>	S. tie hub 5+22.98	15	4.8	83.9	
+50			3.1	94.8		+50	5.0	83.7	
6			4.3	93.6		16	4.6	84.1	
+45			5.2	92.7		+50	4.2	84.5	
			5.2	92.7		17	3.7	85.0	
+70			4.0	93.9		+54.7 = W. end Bridge	2.8	85.9	
7			3.4	94.5		+77.5 = E ✓ ✓	2.5	86.2	
			5.7	92.2		18+50	2.5	86.2	
+40			3.8	94.1		19	2.2	86.5	



T.P.	12.89	99.40 ✓	2.16	86.51 ✓
19+50			12.3	87.1
20			11.3	88.1
+50			9.8	89.6
21			7.3	92.1
B.M.	12.77	105.80 ✓	6.37	93.03 ✓
+50			10.6	95.2
22			7.2	98.6
+50			4.1	101.7
23			0.9	104.9
T.P.	12.64	118.16 ✓	0.28	105.52 ✓
+50			10.1	108.1
24			7.0	111.2
+50			4.0	114.2
25			0.4	117.8
T.P.	12.64	130.80 ✓	0.00	118.16
+50			10.0	120.8
26			6.7	124.1
+50			3.7	127.1
27			0.3	130.5
T.P.	13.01	143.79 ✓	0.02	130.78 ✓
+50			10.6	133.2
28			7.6	136.2
+50			4.7	139.1
29			1.7	142.1
T.P.	12.64	156.33 ✓	0.10	143.69 ✓

East tie  
to 62100

+50					11.3	145.0
30					8.5	147.8
+50					5.3	151.0
31					2.3	154.0
T.P.	12.70	168.96 ✓			0.07	156.26 ✓
+50					12.0	157.0
32					8.9	160.1
+50					5.1	163.9
33					2.8	166.2
B.M.					4.20	164.76 ✓
T.P.	13.02	181.71 ✓			0.27	168.69 ✓
+50					12.5	169.2
34					9.5	172.2
+50					6.6	175.1
35					3.5	178.2
+50					0.6	181.1
T.P.	13.02	194.73 ✓			0.00	181.71 ✓
36					10.8	183.9
+50					7.9	186.8
37					4.7	190.0
+50					1.5	193.2
T.P.	12.68	207.31 ✓			0.10	194.63 ✓
38					10.9	196.4
+50					8.0	199.3
39					5.8	201.5
B.M.					5.78	201.53 ✓

WT tie 100  
32+1930

WT tie  
39+00



207.31

39+50			39	203.4	
40			1.9	205.4	
+50			0.1	207.2	
T.P.	12.53	219.75	0.09	207.22	
41			10.8	209.0	
+50			9.2	210.6	
42			7.6	212.2	
+50			5.9	213.9	
43			4.1	215.4	
+50			2.7	217.1	
44			1.3	218.5	
T.P.	12.46	232.02	0.19	219.56	
+50			12.2	219.9	
45			10.8	221.2	
+50			8.6	223.4	
46			7.1	222.9	
B.M.			6.50	225.52	PI hub 45+77
+50			5.1	226.9	
47			3.5	228.5	
+50			0.9	231.1	
T.P.	12.94	244.46	0.50	231.52	
48			11.1	233.4	
+70 = edge read.			8.0	236.5	
+85			6.2	238.3	
49			5.7	239.8	
+50			3.9	240.6	

250.58 30' hub 54+34.06

Pershing 10

50			2.1	242.4	
TP	9.63	253.34	0.75	243.71	
+50			9.8	243.5	
51			8.9	244.4	
+20			7.3	246.0	
+50			5.7	247.6	
52			3.5	249.8	
+50			2.6	250.7	
+75			2.7	250.6	
53			3.5	249.8	
+50			5.2	248.1	
54			6.3	247.0	
+50			6.5	246.8	
55			7.1	246.2	
B.M.	2.20	248.58	7.16	246.18	15W+16 55.04
+50			3.1	245.3	
56			5.0	243.4	
+50			7.8	240.6	
57			10.2	238.2	
+50			12.1	236.3	
58			13.4	235.0	
+50			13.8	234.6	
59			13.1	235.3	
+50			12.0	236.4	
60			10.9	237.5	
+50			9.4	239.0	



248.38

61			7.7	240.7	
+50			6.6	241.8	
62			5.3	243.1	
B.M.	11.10	256.45	3.03	245.35	PI hub 62+40
+50			12.3	244.2	
63			11.4	245.1	
+50			10.8	245.7	
64			10.5	246.0	
+50			9.7	246.8	
65			8.8	247.7	
+50			8.0	249.5	
66			7.1	249.4	
+50			6.7	249.8	
67			6.1	250.4	
+50			5.1	251.4	
68			4.2	252.3	
+50			3.3	253.2	
69	-Edge present rd		2.3	254.2	
+02.0			1.8	254.7	
+50			1.0	255.5	
70			0.5	256.0	
T.P.	8.88	264.76	0.57	256.88	
+50			8.4	256.4	
71			8.2	256.6	
+50			9.0	255.8	
72			9.3	255.5	

Pershing 11

+50			7.6	257.2	
73			6.6	258.2	
+50			6.2	258.6	
74			4.9	259.9	
+50			4.8	260.0	
+45	Edge road		5.8	259.0	
75			6.0	259.8	
+50			6.2	259.6	
B.M.			7.91		70' hub at 75+70
76			6.3	259.5	
+50			5.9	259.9	
77			5.0	259.8	
+50			4.3	260.5	
78			4.2	260.6	
+50			3.7	261.1	
79			3.1	261.7	
+50			2.1	262.7	
80			1.0	263.8	
T.P.	12.89	276.62	1.03	263.73	
+50			11.5	265.1	
81			9.2	267.4	
+50			6.3	270.3	
82			3.0	273.6	
+50			0.1	276.5	
T.P.	13.10	289.67	0.05	276.59	
83			10.0	279.7	
+50			6.5	283.2	



259.67

84			3.6	286.1
+50			1.5	288.2
85			0.3	289.4
T.P.	4.20	293.71	0.16	289.51
+50			3.7	290.0
86			3.6	290.1
+50			4.2	289.5
87			4.5	289.2
+50			4.6	289.1
B.M.			6.27	
88			4.7	289.0
+50			4.8	289.9
89			4.3	289.4
+50			3.1	290.6
90			0.4	293.3
T.P.	13.03	306.67	0.07	293.67
+50			9.7	297.0
91			5.9	300.8
+50			2.1	304.6
T.P.	13.02	319.47	0.22	306.45
92			11.7	307.8
+50			8.7	310.9
93			5.9	313.6
+50			3.5	316.0
94			1.3	318.2
T.P.	12.85	331.97	0.35	319.12
+50			11.7	320.3

West hub of P.C.

Perishing 12

95			9.7	322.3
+50			8.3	323.7
96			7.0	325.0
+50			5.6	326.4
97			4.4	327.6
+50			3.9	328.1
98			3.6	328.4
+50			3.4	328.6
99			3.0	329.0
+20.80 = paragon			3.03	328.94
			3.20	328.77 = 800K



11/18/30 Gregory Center Line Levels  
Hortensia St.

	1.70	
W.L. La Solla 20100		1.9
0+10		3.2
0+35		9.4
0+50		11.9
T.P.	0.32	13.05
0+80		2.3
1+20		6.3
1+40		10.0
T.P.	0.21	12.63
1+60		1.6
1+80		4.2
2+00		5.8
2+25		8.0
2+55		11.1
3+06		11.3
T.P.	0.79	13.0
3+15		3.3
3+50		4.8
4+00		7.9
4+50		10.5
5+00		13.8
5+50		14.4
5+65		12.9
6		13.1
T.P.	2.17	102.4

NW Kortan

6+52.3 = d Hancock	2.9
7	4.7
+50	5.7
+50	7.3
8+09 = edge paving	7.2



11/23/20 Gregory Levels on Dirt Curb  
33rd St from  
Thorn North

	7.74	322.49	314.75
		N.L. Thorn (west of 33rd) = error	
Web		7.5	315.0
Ecb		6.7	315.8
	2+0.50		
Ecb		6.5	316.0
Web		6.9	315.6
	1+00		
Web		5.9	316.6
Ecb		5.9	316.6
		1+20 = S end cemented on West	
W		5.98	316.51
		1+60 = N end cemented on West	
Ecb		4.9	317.6
W		5.64	316.85
	2+00		
Web		4.9	317.6
Ecb		4.5	318.0
	2+50		
Ecb		4.3	318.2
Web		4.8	317.7
	3+00		
Web		4.7	317.8
Ecb		4.2	318.3

		3+50	
Ecb		3.9	318.6
Web		4.6	317.9
	4+00		
Web		4.3	318.2
Ecb		4.0	318.5
	straight grade from here north		
	P.C. of curves S. of Upas		
Ecb		3.6	318.9
Web		3.7	318.8
	O.C. of curves		
SWcb		3.7	318.8
SEcb		3.8	318.7
	E.C. of Curves		
SWcb		2.7	319.8
SEcb		4.0	318.5



11/23/00  
Gregory  
Miller  
Shaw

Levels on dirt curb  
Thorn St  
Felton to 32nd St

	774	342.49	314.78
		H. L. Felton	
Ncb		26	319.9
Scb		29	319.6
	25'		
Scb		28	319.7
Ncb		26	319.9
	50'		
Ncb		26	319.9
Scb		30	319.5
	75'		
Scb		34	319.1
Ncb		45	320.0
	100'		
Ncb		31	319.4
Scb		38	318.7
	125'		
Scb		44	318.1
Ncb		35	319.0
	150'		
Ncb		40	318.5
Scb		49	317.8
	175'		
Scb		56	316.9
Ncb		47	317.8

15

	400'		
Ncb	55	317.0	
Scb	63	316.2	
	225' W		
Scb	69	315.6	
Ncb	59	316.6	
	450' W = E.L. 33rd		
Ncb	64	316.1	
Scb	75	315.0	
	H. cb. from 33rd West.		
	77	314.8	
	25' W	81	314.4
	50'	87	313.8
	100' W	10.0	312.5
	125' W	10.5	312.0
	150' W	11.3	311.2
	200' W	13.2	309.3
	T.P. 246	1293	309.56
	225' W	36	308.4
	E.L. Bancroft	49	307.1
	W.L. ✓	62	305.8
	50' W	76	304.4
	100' W	84	303.6
	150' W	88	303.2
	168' W = Catch basin	89	303.1
	Top of C.B.	95	302.20
	200' W	86	303.4
	E.L. 32nd St.	78	304.2



11/23/20 Gregory Miller Shaw

Corb Levels on  
BANCROFT ST  
X from Thorn St N

16

	312.02			
	NL Thorn			
Web		6.0	306.0	
E -		5.2	306.8	
	50' N			
Ecb		5.2	306.8	
W -		5.3	306.7	
	100' N			
Web		4.6	307.4	
E -		4.5	307.5	
	150' N			
Ecb		3.3	308.7	
W ✓		3.3	308.7	
	200' N			
Web		1.6	310.4	
E -		2.1	309.8	
	250' N			
Ecb		0.5	311.5	
TP	12.80	3.146	0.36	311.66
Web		3	11.8	312.7
	300' N			
Web		9.9	314.6	
E -		10.7	313.8	
	350' N			
Ecb		8.5	316.0	
W -		8.0	316.5	

	400' N		
Web		6.2	318.3
E -		6.5	318.0
	450' N		
Ecb		4.8	319.7
W -		4.7	319.8
	500' N		
Web		3.5	321.0
Ecb		3.3	321.2
	550' N		
Ecb	on curve	1.8	322.7
Web	✓ ✓	2.2	322.3
	S.C.L. Ups		
E.C. of curve or E.		1.8	322.7
✓ - - - - SW		0.9	323.6



11/23/20

Gregory  
Miller  
ShawLevels on Curb  
& Sidewalk on S Side of  
Ivy St  
E. of Fern

0.39

284.40

284.01

N.W. Fern  
& Ivy

99.3 E

E.L. Fern

on cb.

3.38 281.02

N.S. of walk

3.32 281.08

S. Side

3.24 281.16

25' E

on cb.

4.16 280.24

N. Edge walk

4.09 280.31

S ✓ ✓

4.12 280.28

50' E

on cb.

4.86 279.54

N. edge walk

4.90 279.50

S ✓ ✓

4.74 279.66

75' E

on cb.

5.72 278.68

N. edge walk

5.76 278.64

S ✓ ✓

5.62 278.78

90' E

on cb.

6.32 278.08

N. edge walk

6.36 278.04

S ✓ ✓

6.22 278.18

99' E

on cb.

6.65 277.75

N. edge walk

6.78 277.62

S ✓ ✓

6.57 277.83

17

N edge walk

6.72 277.68

S ✓ ✓

6.57 277.83

128' E

cb

6.22 278.18

N edge walk

6.43 277.97

S ✓ ✓

6.37 278.03

135' E

cb

6.29 278.11

N. Edge walk

6.30 278.10

S ✓ ✓

6.26 278.14

145' E

cb

6.16 278.24

N edge walk

6.10 278.30

S ✓ ✓

6.07 278.33

175' E

cb

5.81 278.59

N. edge walk

5.75 278.65

S ✓ ✓

5.64 278.76

200' E

cb

5.51 278.86

N. edge walk

5.48 278.92

S ✓ ✓

5.36 279.04

250' E

cb

5.14 279.26

N. edge walk

5.05 279.35

S ✓ ✓

5.02 279.38







99.20

3+50 ✓

15' R	4.4	94.8
10' R	4.3	94.9
C	4.1	95.1
10' L	4.2	95.0
15' L	4.4	94.8

4+00 ✓

15' L	2.2	97.0
13' L	3.5	95.7
10' L	3.4	95.8
C	3.1	96.1
10' R	3.4	95.8
13' R	3.5	95.7
15' R	2.8	96.4
T.P.	4.36	100.79 ✓
		2.77
		96.43 ✓

4+50 ✓

15' R	4.4	96.4
12' R	4.0	96.8
11' R	4.5	96.3
10' R	4.5	96.3
C	4.4	96.4
10' L	4.9	95.9
13' L	5.0	95.8
15' L	4.1	96.7

Persting 19

5+00 ✓

15' L	3.3	97.5
10' L	5.2	95.6
C	4.9	95.9
10' R	4.6	96.2
15' R	4.7	96.1

5+50 ✓

15' R	5.4	95.4
10' R	5.4	95.4
C	6.0	94.8
7' L	4.2	94.6
8' L	5.1	95.7
10' L	4.9	95.9
15' L	3.8	97.0

6+00 ✓

15' L	4.0	96.8
10' L	5.4	95.4
C	7.3	93.5
10' R	6.9	93.9
15' R	6.6	94.2

6+50 ✓

15' R	7.8	93.0
10' R	8.0	92.8
C	8.1	92.7
10' L	6.7	94.1
15' L	6.0	94.8



100.79

7+00 ✓

15'L	3.8	97.0
10'L	4.4	96.4
C	6.4	94.4
6'R	7.8	93.0
6.1'R	8.6	92.2
10'R	8.4	92.4
15'R	8.2	92.6

7+50 ✓

15'R	8.2	92.6
10'R	8.4	92.4
2'R	8.7	92.1
C	7.6	93.2
10'L	4.5	96.3
15'L	3.6	97.2

8+00 ✓

15'L	5.5	95.3
10'L	7.3	93.5
8'L	8.1	92.7
4'L	8.2	92.6
4.1'L	8.9	91.9
C	8.9	91.9
10'R	8.6	92.2
15'R	8.5	92.3

Pershing

1961  
2016  
2710  
2670

8+50 ✓

15'R	8.8	92.0
10'R	8.7	92.1
C	8.7	92.1
10'L	9.1	91.7
11'L	8.3	92.5
15'L	7.4	93.9

9+00 ✓

15'L	8.7	92.1
10'L	8.7	92.1
C	8.8	92.0
10'R	8.9	91.9
11'R	8.9	91.9
15'R	12.2	88.6

T.P.	439	94.30 ✓	888	91.91 ✓
25'R			13.2	81.1
35'R			12.5	74.8
42'R			22.6	71.7
50'R			23.9	70.4

9+50 ✓

45'R	22.9	71.4
37'R	21.4	72.9
25'R	14.6	79.7
15'R	6.8	87.5
10'R	7.8	91.5
C	2.7	91.6
10'L		



94.30

10'L	2.6	91.7
15'L	4.7	91.6
	10+00 ✓	
15'L	2.4	91.9
13'L	3.7	90.6
10'L	3.6	90.7
C	3.5	90.8
10'R	3.3	91.0
15'R	3.3	91.0
	10+50 ✓	
15'R	4.5	89.8
10'R	4.3	90.0
C	4.5	89.8
10'L	4.7	89.6
11'L	3.6	90.7
15'L	2.7	91.6
	11+00 ✓	
15'L	4.5	91.8
10'L	4.3	90.0
9'L	5.7	88.6
C	5.1	88.9
10'R	5.3	89.0
15'R	5.3	89.0
	11+50 ✓	
15'R	6.3	88.0
10'R	6.4	87.9

94.30

Pershing

21

C	6.7	87.6
6'L	7.0	87.3
7'L	5.7	88.6
10'L	5.2	89.1
15'L	4.2	90.1
	12+00 ✓	
15'L	1.9	92.4
10'L	5.6	88.7
7'L	6.5	87.8
6'L	7.8	86.5
C	7.8	86.5
10'R	7.5	86.8
15'R	7.4	86.9
	12+50 ✓	
15'R	8.7	85.6
10'R	8.7	85.6
C	8.8	85.5
6'L	9.1	85.2
10'L	7.7	86.6
15'L	5.7	88.6
	13+00 ✓	
15'L	9.3	85.0
10'L	9.6	84.7
C	9.7	84.6
10'R	9.6	84.7
15'R	9.6	84.7



13+50 ✓ put in 12" pipe + basin. ✓

T.P.	474	88.72 ✓	10.32	83.98 ✓
35' R			11.4	77.3
31' R			10.3	78.4
26' R			7.9	80.8
21' R			4.5	84.2
15'			4.5	84.2
10'			4.6	84.1
C			4.6	84.1
10' L			5.0	83.7
15' L			5.2	83.5
20' L			5.2	83.5
		14+00 ✓		
15' L			1.5	87.2
10' L			4.8	83.9
C			5.0	83.7
10' R			4.5	83.9
15' R			4.9	83.8
		14+50 ✓		
15' R			4.9	83.8
10' R			4.5	83.9
C			4.5	83.9
7' L			5.0	83.7
10' L			3.9	84.8
15' L			2.4	86.3

15+00 ✓

15' L		1.4	87.3
10' L		3.9	84.8
7' L		5.0	83.7
C		4.5	83.9
10' R		4.7	84.0
15' R		4.7	84.0
		15+50 ✓	
15' R		4.9	83.8
10' R		4.9	83.8
C		5.0	83.7
7' L		5.1	83.6
8' L		4.6	84.1
10' L		4.4	84.3
15' L		1.8	86.9
		16+00 ✓	
15' L		5.7	83.0
13' L		5.0	83.7
10' L		5.0	83.7
C		4.7	84.0
10' R		4.8	83.9
15' R		4.9	83.8
		16+50 ✓	
15' R		4.9	83.8
10' R		4.6	84.1
C		4.3	84.4



8872

10' L 42 84.5

15' L 44 84.3

17+00 ✓

15' L 36 85.1

10' L 36 85.1

C 37 85.0

10' R 41 84.6

15' R 44 84.3

17+54.7 ✓ = End of Bridge

15' R 33 85.4

10' R 32 85.5

C 29 85.8

10' L 27 86.0

15' L 28 85.9

17+97.5 ✓ = E. End Bridge

15' L 28 85.9

10' L 27 86.0

C 26 86.1

10' R 26 86.1

15' R 26 86.1

T.P. 11.71 197.88 ✓ 2.55 86.17 ✓

18+50 ✓

15' R 11.9 86.0

10' R 11.6 86.3

C 11.6 86.3

10' L 12.0 85.9

Pershing 23

13' L 12.3 85.6

15' L 13.6 84.3

20' L 14.6 83.3

19+00 ✓

20' L 13.7 84.2

15' L 13.1 84.8

10' L 12.0 85.9

C 11.4 86.5

10' R 11.3 86.6

15' R 11.4 86.5

19+50 ✓

15' R 10.8 87.1

10' R 10.6 87.3

C 10.7 87.2

10' L 11.2 86.7

12' L 11.2 86.5

15' L 12.4 85.5

20' L 12.5 85.4

20+00 ✓

20' L 12.0 85.9

15' L 10.8 87.1

12' L 10.0 87.9

10' L 10.0 87.9

C 9.7 88.2

10' R 9.5 88.4

15' R 9.7 88.2



97.88

20+50 ✓

15'R	81	89.8
10'R	80	89.9
C	82	89.7
10'L	85	89.1
15'L	88	89.1

21+00 ✓

15'L	68	91.1
10'L	62	91.5
C	58	92.1
10'R	5.6	92.3
15'R	5.7	92.2

21+50 ✓

15'R	2.2	95.7
10'R	2.2	95.7
C	2.7	95.2
10'L	3.1	94.8
14'L	3.6	94.3
15'L	4.2	93.7
16'L	4.7	93.2
20'L	5.7	92.2

22+00 ✓

20'L	2.8	95.1
17'L	2.5	95.4
15'L	0.9	97.0
14'L	0.1	97.8

Persting 64

TP 11.88 109.11 ✓

00.5

97.83 ✓

10'L	11.6	98.1
C	11.2	98.5
10'R	10.6	99.1
15'R	10.5	99.2

22+50 ✓

15'R	7.3	102.4
10'R	7.5	102.2
C	8.0	101.7
10'L	8.5	100.9
12'L	8.9	102.8
15'L	11.0	98.7
20'L	13.2	96.5
25'L	14.4	95.3

23+00 ✓

30'L	14.1	95.6
43'L	12.8	96.9
15'L	7.7	102.0
11'L	5.2	104.5
10'L	5.0	104.7
C	4.8	104.9
10'R	4.7	105.0
15'R	4.7	105.0

23+50 ✓

15'R	1.8	107.9
10'R	1.7	108.0



10971

C			1.6	108.3
10'L			1.5	108.2
15'L			1.5	108.2
T.P.	13.04	121.53 <sup>v</sup>	0.92	108.77 <sup>v</sup>
		24+00 <sup>v</sup>		
15'L			10.2	111.6
10'L			10.3	111.5
C			10.7	111.1
10'R			11.0	110.8
10'R			10.6	111.2
15'R.			8.6	113.2
		24+50 <sup>v</sup>		
15'R			6.9	114.9
10'R			7.1	114.7
C			7.6	114.2
10'L			7.2	114.6
15'L			6.9	114.9
		25+00 <sup>v</sup>		
15'L			3.5	118.3
10'L			3.8	118.0
C			4.1	117.7
7'R			3.0	118.8
10'R			+1.3	123.1
15'R			+3.0	124.3

Pershing 25

				25+50 <sup>v</sup>
15'R			+6.3	128.1
10'R			+5.0	126.8
3'R			0.9	120.9
C			0.9	120.9
10'L			0.5	121.3
15'L			0.3	121.5
T.P.	12.87	134.45 <sup>v</sup>	0.25	121.58 <sup>v</sup>
		26+00 <sup>v</sup>		
15'L			9.8	124.7
10'L			10.0	124.5
C			10.3	124.2
4'R			10.3	124.2
7'R			8.3	126.2
10'R			7.4	127.1
15'R			3.7	130.8
		26+50 <sup>v</sup>		
15'R			2.0	132.5
10'R			4.5	130.0
5'R			5.3	129.2
2'R			7.2	127.3
C			7.2	127.3
10'R ?			6.8	127.7
15'R ?			6.6	127.9



134.45

27+00 ✓

15'L			33	131.2
10'L			36	130.9
C			39	130.6
T.P.	13.17	147.62 ✓	0.00	134.45
10'R			12.0	135.6
15'R			91	138.5

27+50

15'R			6.0	141.6
13'R			13.5	134.1
10'R			13.8	133.8
C			14.3	133.3
10'L			13.8	133.8
15'L			13.6	134.1

28+00 ✓

15'L			10.5	137.1
10'L			10.9	136.7
C			11.4	136.2
10'R			11.1	136.5
15'R			10.4	137.2

28+50 ✓

15'R			6.6	141.0
10'R			7.6	140.0
6'R			8.8	138.8
C			8.4	139.2
10'L			7.9	139.7

Pershing 46

15'L

7.7 139.9

29+00 ✓

15'L			5.0	142.6	edge of hill
10'L			5.2	142.4	
C			5.4	142.2	
10'R			5.7	141.9	
15'R			5.0	142.6	

29+50 ✓

15'R			3.2	144.2	
10'R			3.9	144.7	
C			2.5	145.1	
10'L			2.1	145.5	
15'L			1.9	145.7	edge of hill

130.7 160.42 ✓

0.27 147.35 ✓

30+00 ✓

15'L			11.9	148.5	edge of hill
10'L			12.0	148.4	
C			12.4	148.0	
10'R			12.7	147.7	
15'R			13.1	147.3	

30+50 ✓

15'R			10.1	150.3
10'R			9.7	150.7
C			9.3	151.1
10'L			9.1	151.3
15'L			9.2	151.2



160.42

31+00 ✓

15'L	6.0	154.4
10'L	6.0	154.4
C	6.2	154.2
10'R	6.8	153.6
15'R	6.3	154.1

31+50 ✓

15'R	2.6	157.8
10'R	3.6	156.8
C	3.2	157.2
10'L	3.1	157.3
15'L	3.0	157.4

32+00 ✓

15'L	0.0	160.4
10'L	0.0	160.4
C	0.2	160.2
10'R	0.1	160.3

T.P.	12.22	172.57 ✓	0.07	160.35 ✓
------	-------	----------	------	----------

13'R	11.8	160.8
------	------	-------

15'R	10.4	162.2
------	------	-------

32+50 ✓

15'R	9.0	165.6
------	-----	-------

10'R	9.0	163.6
------	-----	-------

10'R	9.2	163.4
------	-----	-------

C	9.3	163.3
---	-----	-------

10'L	9.2	163.4
------	-----	-------

Pershing 27

15'L

9.1 163.5

33+00 ✓

15'L	6.2	166.4
------	-----	-------

10'L	6.2	166.4
------	-----	-------

C	6.3	166.3
---	-----	-------

10'R	6.4	166.2
------	-----	-------

15'R	5.8	166.8
------	-----	-------

33+50 ✓

15'R	3.6	169.0
------	-----	-------

10'R	3.4	169.2
------	-----	-------

C	3.2	169.4
---	-----	-------

10'L	3.2	169.4
------	-----	-------

15'L	3.1	169.5
------	-----	-------

34+00 ✓

15'L	0.1	172.5
------	-----	-------

10'L	0.0	172.6
------	-----	-------

C	0.1	172.5
---	-----	-------

10'R	0.5	172.1
------	-----	-------

15'R	0.7	171.9
------	-----	-------

T.P.	12.54	185.37 ✓	0.02	172.55 ✓
------	-------	----------	------	----------

34+50 ✓

15'R	10.6	174.8
------	------	-------

10'R	10.4	175.0
------	------	-------

C	10.1	175.3
---	------	-------

10'L	10.0	175.4
------	------	-------

15'L	9.8	175.6
------	-----	-------



185.39

35+00 ✓

15'L	66	178.8
10'L	68	178.6
C	69	178.5
10'R	75	177.9
15'R	80	177.4

35+50 ✓

15'R	5.2	180.2
10'R	4.6	180.8
C	40	181.4
10'L	36	181.8
15'L	33	182.1

36+00 ✓

15'L	0.4	185.0
10'L	0.7	184.7
C	1.1	184.3
10'R	1.7	183.7
15'R	+0.6	186.0
TP	1.16	197.39 ✓
	0.16	185.23 ✓

36+50 ✓

15'R	6.1	191.3
13'R	10.9	186.5
10'R	11.0	186.4
C	10.2	187.2
10'L	9.5	187.9
15'L	9.3	188.1

Pershing

25

37+00 ✓

15'L	6.4	191.0
10'L	6.6	190.8
C	7.1	190.3
10'R	7.5	190.0
15'R	6.9	190.5

37+50 ✓

15'R	2.9	194.5
10'R	5.0	192.4
C	3.8	193.6
10'L	3.2	194.0
15'L	3.1	194.3

38+00 ✓

15'L	0.6	196.8
10'L	0.7	196.7
C	0.9	196.5
10'R	1.5	195.9
15'R	1.3	196.1

38+50 ✓

TP	1.252	210.11 ✓
	0.10	197.29
15'R	11.3	198.8
10'R	10.9	199.2
C	10.7	199.4
10'L	10.7	199.4
15'L	10.7	199.4

edge



850

210.11

39+50

15'L	83	201.8
10'L	83	201.8
C	84	201.7
10'R	87	201.4
15'R	87	201.4

39+50

15'R	62	203.9
10'R	67	203.4
C	64	203.7
10'L	61	204.0
15'L	60	204.1

40+00

15'L	41	206.0
10'L	41	206.0
C	44	205.7
10'R	47	205.4
15'R	36	206.5

40+50

15'R	24	207.9
10'R	28	207.3
C	27	207.4
10'L	23	207.8
15'L	23	207.8

Pershing 29

41+00

15'L	0.4	209.7
10'L	0.6	209.5
C	1.0	209.1
10'R	1.3	208.8
15'R	0.6	209.5
T.P.	1262	221.98

41+50

15'R	11.3	210.5
10'R	10.2	210.6
C	11.1	210.7
10'L	10.5	211.3
15'L	10.3	211.5

42+00

15'L	8.8	213.0
10'L	8.9	212.9
C	9.3	212.5
10'R	9.7	212.1
15'R	9.9	211.9

42+50

15'R	8.1	213.7
10'R	7.9	213.9
C	7.5	214.0
10'L	7.5	214.3
15'L	7.4	214.4



221.78

43+00

15' L	5.7	216.1
10' L	5.8	216.0
C	6.2	215.6
10' R	6.2	215.6
15' R	4.0	217.8

43+50

15' R	4.2	217.6
10' R	4.9	216.9
C	4.6	217.2
10' L	4.3	217.5
15' L	4.2	217.6

44+00

15' L	2.5	219.3
10' L	2.6	219.2
C	2.9	218.9
10' R	3.7	218.1
15' R	3.7	218.1

44+50

15' R	0.6	221.2
10' R	2.3	219.5
C	1.4	220.4
10' L	0.9	220.9
15' L	0.8	221.0

TP

21.78

233.54

0.02

221.96

233.54

Pershing

30

45+00

15' L	11.1	222.4
10'	11.2	222.1
C	12.2	221.3
5' R	11.5	222.0
10'	9.2	224.1
15' R	8.9	224.6

45+50

15' R	7.0	226.5
10'	7.1	226.4
5'	7.5	226.0
2'	10.2	223.3
C	10.2	223.3
5' L	16.0	223.5
8'	10.9	222.6
10'	10.7	222.8
15' L	10.2	223.3

46+00

15' L	8.8	224.7
10' L	9.2	224.3
C	7.0	226.5
10' R	6.5	227.0
15' R	6.5	227.0

46+50

15' R	6.5	226.7
10'	6.7	226.8



233.54

C	6.7	226.8
10' L	6.6	226.9
15' L	6.4	227.1

47400

15' L	4.5	229.0
10'	4.6	228.9
C	5.1	228.4
10' R	5.3	228.2
15' R	5.3	228.2

47450

15' R	2.1	231.4
10' R	2.6	230.9
C	2.2	231.1
10' L	2.3	231.2

15' L	2.5	231.0
T.P.	11.48	233.01
	24469	0.53
	48400	

15' L	10.2	234.5
10' L	11.5	233.2
C	11.4	233.3
10' R	11.4	233.3
15' R	11.5	233.2

48450

15' R	9.0	235.7
10' R	9.0	235.7
C	9.4	235.3
3' L	9.4	235.3

Pershing 31

6' L	7.8	236.9
10' L	7.7	237.0
15' L	7.8	236.9

49100

15' L	5.5	238.9
10' L	5.8	238.9
C	6.0	238.7
4' R	6.1	238.6
4' R	7.2	237.5
10	7.2	237.5
15' P	7.0	237.7

49450

15' R	5.1	239.6
10	5.2	239.5
8' R	4.2	240.5
C	4.1	240.6
10' L	3.9	240.8
15' L	4.0	240.7

50400

15' L	2.5	242.2
10' L	2.6	242.2
C	2.5	242.2
10' R	2.6	242.2
11' R	3.1	241.6
15' R	3.1	241.6



244.69

50+50

15'R			1.1	243.6
10'R			1.0	243.7
T.P	9.56	253.28	0.97	243.72
C			9.7	243.6
10'L			10.1	243.2
15'L			10.5	242.8

51+50

15'L			9.6	244.2
10'L			9.0	244.3
C			8.8	244.5
10'R			8.4	244.9
15'R			8.1	245.2

51+50

15'R			6.3	247.0
13'			5.7	247.6
10'			5.7	247.6
C			5.7	247.6
10'L			5.8	247.5
15'L			5.8	247.5

52+50

15'L			3.6	249.7
10'L			3.5	249.8
C			3.5	249.8
10'R			3.5	249.8
15'R			3.4	249.9

Perching

32

52+50

15'R			2.5	250.8
10'R			2.5	250.8
C			2.5	250.8
10'L			2.6	250.8
15'L			2.6	250.8

53+50

15'L			3.0	250.3
10'L			3.3	250.0
C			3.4	249.9
10'R			3.5	249.8
15'R			4.0	249.3

53+50

15'R			5.7	247.6
10'R			5.9	247.4
C			5.3	248.0
C			5.1	248.2
10'L			4.9	248.4
15'L			4.9	248.4

54+50

15'L			6.2	247.1
10'L			6.4	246.9
C			6.2	247.1
10'R			5.9	247.4
15'			5.9	247.4



	54+50		
15'R	6.6	246.7	
10'R	6.5	246.8	
C	6.7	246.6	
10'L	7.1	246.2	
15'L	7.5	245.8	
	55+00		
15'L	7.1	246.2	
10'L	7.2	245.9	
C	7.1	246.2	
10'R	7.1	246.2	
15'R	7.0	246.3	
	55+50		
15'R	8.2	245.1	
10'R	8.0	245.3	
C	8.1	245.2	
10'L	8.3	245.0	
13'L	6.3	247.0	
15'L	6.2	247.1	
	56+00		
15'L	9.0	244.3	
14'L	9.9	243.4	
10'L	10.0	243.3	
9' Don't need	9.9	243.4	
C	9.9	243.4	
10'R	10.1	243.2	
15'R	10.0	243.3	

	T.P. 1.12	241.97 <sup>✓</sup>	12.43	240.85 <sup>✓</sup>
			56+50	
15'R			1.9	240.1
10'R			1.6	240.4
C			1.3	240.7
10'L			1.4	240.6
15'L			1.4	240.6
			57+00	
15'L			2.5	239.5
13'			3.7	239.3
10			3.8	239.2
C			3.7	239.3
10'R			3.9	239.1
15'R			4.0	239.0
			57+50	
15'R			5.8	236.2
10'			5.8	236.2
C			5.6	236.4
10'L			5.9	236.1
15'L			4.5	237.5
			58+00	
15'L			6.7	235.3
10'			6.9	235.1
C			6.9	235.1
10'R			6.9	235.1
15'R			6.9	235.1



2.11.97

	58+50		
15' R	7.2	234.8	
10'	7.3	234.7	
C	7.4	234.6	
8' L	7.5	234.5	
10'	7.1	234.9	
15'	7.2	234.8	
	59+00		
15' L	7.1	234.9	
10' L	6.9	235.1	
C	6.7	235.3	
10' R	6.8	235.2	
15' R	6.6	235.4	
	59+50		
15' R	5.0	237.0	
14' R	5.7	236.3	
10' R	5.7	236.3	
C	5.6	236.4	
10' L	6.0	236.0	
13'	5.4	236.6	
15' L	6.1	235.9	
	60+00		
15' L	5.4	236.6	
13	4.4	237.6	
10	4.9	237.1	
C	4.5	237.5	

Perishing 34

10' R	4.4	237.6	
14'	4.5	237.5	
15' R	5.7	238.3	
TP	10.75	249.53	31.9
	60+50		
10' R	9.6	239.9	
13'	10.8	239.7	
10'	10.6	239.9	
C	10.6	239.9	
10' L	11.0	239.5	
15' L	10.8	239.7	
	61+00		
15' L	9.4	240.1	
10'	9.4	240.1	
C	8.9	240.6	
10' R	9.0	240.5	
15' R	7.6	242.0	
	61+50		
15' R	6.2	243.3	
10'	6.7	242.8	
7'	7.6	241.9	
C	7.6	241.9	
10' L	7.9	241.6	
15'	8.1	241.4	



62+00

15' L	6.7	242.8
10' L	6.6	242.9
C	6.5	243.0
3' R	6.4	243.1
5'	5.7	243.8
10'	4.7	244.8
15'	3.8	245.7

62+50

15' R	3.4	246.1
10'	3.4	246.1
2'	5.4	244.1
C	5.4	244.1
10' L	5.4	244.1
15' L	5.5	244.0

63+00

15' L	4.5	245.0
10' L	4.5	245.0
C	4.6	244.9
1' R	4.6	244.9
2	3.7	245.8
10'	2.6	246.9
15'	3.0	246.5

63+50

15' R	4.5	245.0
10'	4.0	245.5
3'	3.5	246.0
C	4.0	245.5
10' L	3.8	245.7
15'	3.8	245.7

64+00

15' L	3.4	246.1
10'	3.4	246.1
C	3.6	245.9
3' R	2.8	246.7
10'	3.1	246.4
15'	3.1	246.4

64+50

15' R	1.0	249.5
10' R	1.2	249.3
5'	1.7	247.8
3'	2.8	246.7
C	2.8	246.7
10' L	2.7	246.8
15' L	2.9	246.6

65+00

15' L	4.0	247.5
10' L	1.8	247.7
C	1.9	247.6



249.53

5' R			21	247.4
10' R			0.9	248.6
15' R			0.8	248.7
		65+50		
15' R			+0.2	249.7
10'			0.2	249.1
8'			1.3	248.2
C			1.1	248.4
10' L			1.3	248.2
15' L			1.2	248.3
TP	11.59	26089 ✓	0.23	249.30
		66+00		
15' L			11.6	249.3
10'			11.9	249.0
C			11.6	249.3
10' R			11.5	249.4
12'			10.6	250.3
15'			10.5	250.4
		66+50		
15' R			10.1	250.8
12'			10.9	250.0
10'			10.9	250.0
C			11.2	249.7
10' L			11.5	249.4
12'			10.9	250.0
15'			11.9	249.00

Perching 3L

				67+00
15' L			10.1	250.8
11' L			10.1	250.8
10' L			10.9	250.0
C			10.6	250.3
10' R			10.4	250.5
12'			10.2	250.5
15' R			9.0	251.9
		67+50		
15' R			8.7	252.2
10' R			9.5	251.4
C			9.7	251.2
10' L			10.0	250.9
12' L			9.5	251.1
13' L			9.1	251.8
15' L			9.0	251.9
		68+00		
15' L			9.2	251.7
10'			8.9	252.0
C			8.7	252.2
7' R			8.5	252.4
10' R			7.9	253.0
15' R			7.7	253.2
		68+50		
15' R			6.7	254.2
10'			6.7	254.2



260,89

C	7.8	253.1
10'L	7.9	253.0
15'L	8.3	252.6
69+00		
15'L	7.1	253.8
10'L	6.9	254.0
C	6.8	254.1
1'R	6.1	254.8
10'R	5.8	255.1
15'R	5.6	255.3
69+50		
15'R	5.1	255.8
10'	5.3	255.6
C	5.3	255.6
10'L	6.0	254.9
15'L	6.1	254.9
70+00		
15'L	5.6	255.3
10'L	5.7	255.2
8'	4.9	256.0
C	5.0	255.9
10'R	4.8	256.1
15'R	4.9	256.0
70+50		
15'R	4.4	256.5
10'R	4.5	256.4

Pershing 37

C	4.5	256.4
10'L	4.2	256.7
15'L	4.0	256.9
71+00		
15'L	3.8	257.1
10'L	4.0	256.9
C	4.3	256.6
10'R	4.4	256.5
15'R	4.2	256.7
71+50		
15'R	4.8	256.1
10'R	5.0	255.9
C	5.2	255.7
10'L	4.8	256.1
15'L	4.5	256.4
72+00		
15'L	5.0	255.9
10'L	5.1	255.8
C	5.5	255.4
10'R	6.2	254.7
15'R	6.2	254.7
T.P.	7.69	264.67 ✓
72+50		
15'R	8.8	255.9
10'R	8.3	256.4
C	7.7	257.0



26468

10' L	7.2	257.5
15' L	7.2	257.5
	73+00	
15' L	5.8	258.9
10' L	6.1	258.6
C	6.5	258.2
10' R	7.2	257.5
15' R	7.4	257.3
	73+50	
15' R	6.4	259.3
10' R	6.3	258.4
C	6.0	258.7
10' L	5.7	259.0
15' L	5.5	259.2
	74+00	
15' L	5.4	259.3
13' L	5.5	259.2
12' L	4.7	260.0
10'	4.6	260.1
C	4.8	259.9
10' R	4.8	259.9
15'	4.7	260.0
	74+50	
15' R	5.2	259.5
10'	4.9	259.8
C	4.9	259.8

Forsberg 38

2' L	4.9	259.8
3' L	5.5	259.2
10'	5.4	259.3
15	5.4	259.3
	75+00	
15' L	6.0	258.7
10' L	5.9	258.8
C	5.9	258.8
10' R	5.6	259.1
15	5.5	258.9
	703 265.44 ✓	6.27 258.41 ✓
	75+50	
15' R	6.5	258.9
10'	7.1	258.3
C	6.9	258.5
10' L	7.2	258.1
15' L	7.7	257.7
	76+00	
15' L	8.6	256.8
10' L	7.2	258.2
C	7.0	258.4
10' R	7.0	258.4
15' R	7.1	258.3
	76+50	
15' R	6.3	258.9
10' R	6.3	258.9



265.44

C	66	258.8
10'L	69	258.5
15'L	77	257.7
77+00		
15'L	56	259.8
11'	54	260.0
10'	59	259.5
C	57	259.7
10'R	56	259.8
15'R	55	259.9
77+50		
15'R	48	260.6
10'	50	260.4
C	50	260.4
10'L	51	260.3
12'	46	260.9
15'	46	260.8
78+00		
15'L	52	260.2
10'	52	260.2
C	49	260.5
10'R	49	260.5
15'R	48	260.6
78+50		
15'R	49	260.6
10'	45	260.9

Pershing

39

C	44	261.0
10'L	49	260.5
15'L	50	260.4
79+00		
15'L	43	261.1
10'L	41	261.3
C	38	261.6
9'R	40	261.4
10'R	37	261.7
15'R	43	261.1
79+50		
15'R	38	261.6
10'	49	262.5
C	28	262.6
10'L	29	262.5
15'L	32	262.2
80+00		
15'L	18	263.6
10'L	18	263.6
C	17	263.7
9'R	19	263.5
10'	29	262.7
15'	34	262.0
20'	37	261.7



263.40

		80+50		
20' R			1.9	263.5
15' R			1.7	263.7
10'			0.5	264.9
C			0.3	265.1
10' L			0.5	264.9
15' L			0.8	264.6
TP	12.66	278.04 <sup>✓</sup>	0.06	265.35 <sup>✓</sup>
		81+00		
15' L			11.4	266.6
10' L			11.1	266.9
C			10.6	267.4
10' R			10.8	267.2
12			10.7	267.3
15			11.8	266.2
20			12.7	265.3
		81+50		
20' R			8.8	269.2
15'			7.9	270.1
11			7.2	270.6
10'			7.8	270.2
C			7.7	270.3
10' L			8.1	269.9
15'			8.2	269.8
		82+00		
15' L			5.1	272.9

Pershing 40

10'			4.9	273.1
C			4.2	273.6
10' R			4.5	273.5
15' R			4.2	273.8
		82+50		
15' R			1.1	276.9
13			1.6	276.4
10'			1.6	276.4
C			1.4	276.6
10' L			1.7	276.3
15'			1.9	276.1
TP	12.28	290.16 <sup>✓</sup>	0.16	277.88 <sup>✓</sup>
		83+00		
15' L			11.5	278.7
10' L			11.1	279.1
C			10.5	279.7
10' R			10.4	279.8
15' R			10.6	279.6
		83+50		
15' R			6.5	283.7
10'			6.6	283.6
C			6.9	283.3
10' L			7.5	282.7
15' L			7.6	282.6
		84+00		
15' L			5.1	285.1



290.16

10' L		4.9	285.3
C		4.3	285.9
10' R		3.5	286.7
15'		2.8	287.4
	84+50	2.71	287.45 ✓
15' R		1.6	288.6
110'		1.6	288.6
C		2.0	288.2
10' L		2.1	287.8
15' L		2.6	287.6
	85+00		
15' L		1.2	289.0
10' L		1.2	289.0
C		0.5	289.4
10' R		0.5	289.7
15' R		0.4	289.8
	85+50		
15' R		+0.1	290.3
10'		+0.1	290.3
C		0.1	290.1
10' L		0.9	289.3
15' L		1.0	289.2
T.P.	4.04	290.11	0.09 290.07 ✓

41

			86+00
15' L		4.7	289.4
10' L		4.6	289.5
C		4.0	290.1
10' R		3.6	290.5
15' R		3.5	290.6
	86+50		
15' R		4.4	289.7
10' R		4.4	289.7
C		4.5	289.6
10' L		4.9	289.2
15' L		4.7	289.4
	87+00		
15' L		5.2	288.9
10' L		5.1	289.0
C		4.8	289.3
10' R		4.8	289.3
15' R		4.9	289.2
	87+50		
15' R		4.6	289.5
10' R		5.0	289.1
C		4.8	289.3
10' L		4.9	289.2
15' L		5.0	289.1



294.11

	88+00		
15'L		5.0	289.1
10'		5.1	289.1
C		5.0	289.1
9'R		5.2	288.9
10'		4.5	289.6
15'R		4.5	289.6
	88+50		
15'R		4.0	290.1
10'		4.6	289.5
9'R		5.5	288.6
C		5.1	289.0
10'L		5.1	289.0
15'L		5.1	289.0
	89+00		
15'L		5.0	289.1
10'		4.9	289.2
C		4.7	289.4
10'R		5.0	289.1
13'		4.8	289.3
15'		3.6	290.5
	89+50		
15'R		3.2	290.9
14'		3.8	290.3
10		3.9	290.3
C		3.5	290.6

Pershing 42

10'L		3.6	290.5	
15'		4.0	290.1	
	90+00			
15'L		1.4	292.7	
10'		0.9	293.2	
C		0.8	293.3	
10'R		1.0	293.1	
15'R		1.1	293.0	
TP	13.08	307.95	0.14	293.97
		90+50		
15'R		10.4	296.6	
10'		10.3	296.7	
C		10.1	296.9	
10'L		10.2	296.8	
13'L		10.5	296.5	
15'L		9.5	297.5	
	91+00			
15'L		6.2	300.8	
14'L		6.9	300.1	
10'		6.5	300.5	
C		6.3	300.7	
10'R		6.4	300.6	
15		6.4	300.6	
	91+50			
15'R		3.1	303.9	
10'		2.8	304.2	



307.05

C		2.5	304.5
10' L		2.8	304.2
15'		3.0	304.0
T.P.	1250	319.34	0.21 306.84
		92+00	
15' L		12.2	307.1
10'		11.9	307.4
C		11.6	307.7
10' R		11.7	307.6
15' R		12.2	307.1
		92+50	
15' R		8.9	310.4
10'		8.7	310.6
C		8.6	310.7
10' L		9.1	310.3
15' L		9.7	309.6
		93+00	
15' L		6.7	312.6
10'		6.5	312.8
C		5.9	313.4
10' R		5.9	313.4
15'		5.8	313.5
		93+50	
15' R		3.7	315.6
10'		3.5	315.8
C		3.4	315.9

319.34

Patching L3

10' L		3.7	315.6
15' L		3.8	315.5
		94+00	
15' L		1.8	317.5
10' L		1.3	318.0
C		1.2	318.1
10' R		1.4	317.9
15' R		1.7	317.6
T.P.	11.98	331.14	0.18 319.16
		94+50	
15' R		11.3	319.8
10'		11.1	320.0
C		10.8	320.3
10' L		11.0	320.1
15' L		11.2	319.9
		95+00	
15' L		9.3	321.8
10'		9.0	322.1
C		8.9	322.2
10' R		9.2	321.9
15' R		9.5	321.6
		95+50	
15' R		7.8	323.3
10' R		7.6	323.5
C		7.4	323.7
10' L		7.7	323.4
15'		7.4	323.7



331.14

96+00

15' L	6.6	324.5
10' L	6.2	324.7
C	6.1	325.0
10' R	6.3	324.8
15' R	6.5	324.6

96+50

15' R	5.3	325.8
10'	5.1	326.0
C	4.7	326.4
10' L	5.2	325.9
15' L	5.4	325.7

97+00

15' L	4.3	326.8
10' L	3.9	327.2
C	3.5	327.6
10' R	4.1	327.0
15' R	4.0	327.1

97+50

15' R	2.8	328.3
10' R	3.5	327.6
C	3.0	328.1
10' L	3.1	328.0
15' L	3.4	327.7

Perking 44

98+00

15' L	3.1	328.0
10'	2.6	328.5
C	2.7	329.4
10' R	3.1	328.0
12'	3.0	328.1
15'	2.1	329.0

98+50

15' R	2.7	328.4
10'	2.6	328.5
C	2.4	328.7
10' L	2.6	328.5
15' L	2.8	328.3

99+00

15' L	2.7	328.4
10'	2.5	328.6
C	2.2	328.9
10' R	2.1	328.7
15' R	2.4	328.7
B.M.	2.33	328.85

99+50.8

15' R	2.37	328.77	on paring
10' R	2.27	328.97	-
C	2.20	328.94	-
10' L	2.30	328.84	-
15' L	2.40	328.74	-



X section of Curve to Redwood  
from Pershing Drive

30628

45

6.60 29405 287.45

see page 5 0+00 of Curve to Redwood = 83+31.13 of Pershing

15' L	13.1	280.2
10' L	12.5	281.2
C	12.2	281.8
10' R	12.1	281.9
15' R	12.3	281.7

0+50

15' R	8.3	285.7
10' R	8.2	285.8
C	8.2	285.8
10' L	8.9	285.1
15' L	9.2	284.8

1+00

15' L	4.3	289.7
10' L	4.2	289.8
C	3.7	290.3
10' R	4.0	290.0
15' R	3.8	290.2

T.P. 12.39 30628 0.16 292.89

1+50

15' R	10.3	296.0
10'	10.0	296.3
5	11.1	295.2
C	10.5	295.8
10' L	10.4	295.9

15' L

15' L	5.3	301.0
10' L	5.4	300.9
C	5.4	300.9
10' R	6.1	300.2
15' R	5.5	300.8

2+00

2+50

15' R	2.4	303.9
10' R	2.4	303.9
C	1.7	304.6
10' L	2.0	304.3
15' L	2.2	304.1
T.P.	5.75	311.90

3+00

15' L	5.0	306.9
10' L	5.2	306.7
C	4.8	307.1
10' R	5.4	306.5
15' R	5.5	306.4

3+49.57 = E.L. 28<sup>th</sup> 54.

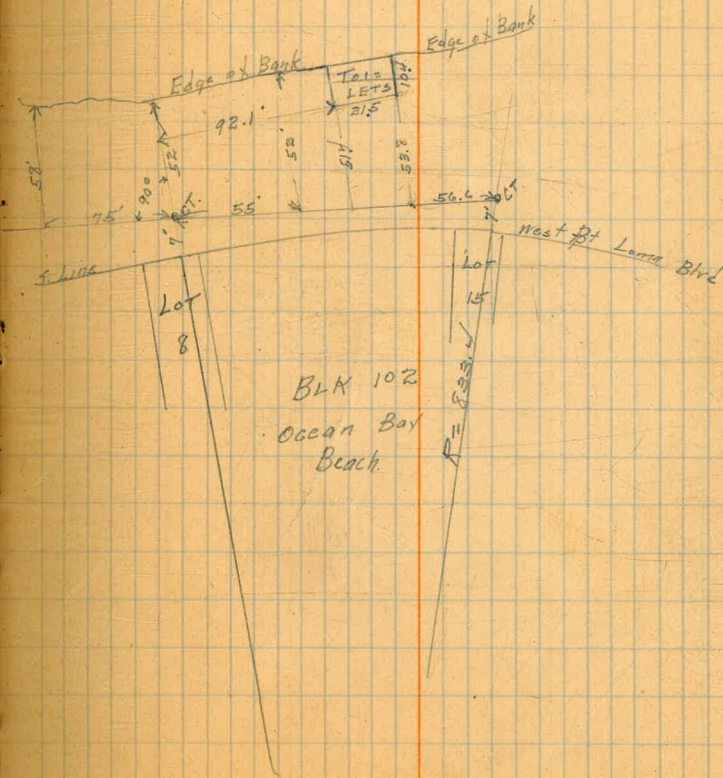
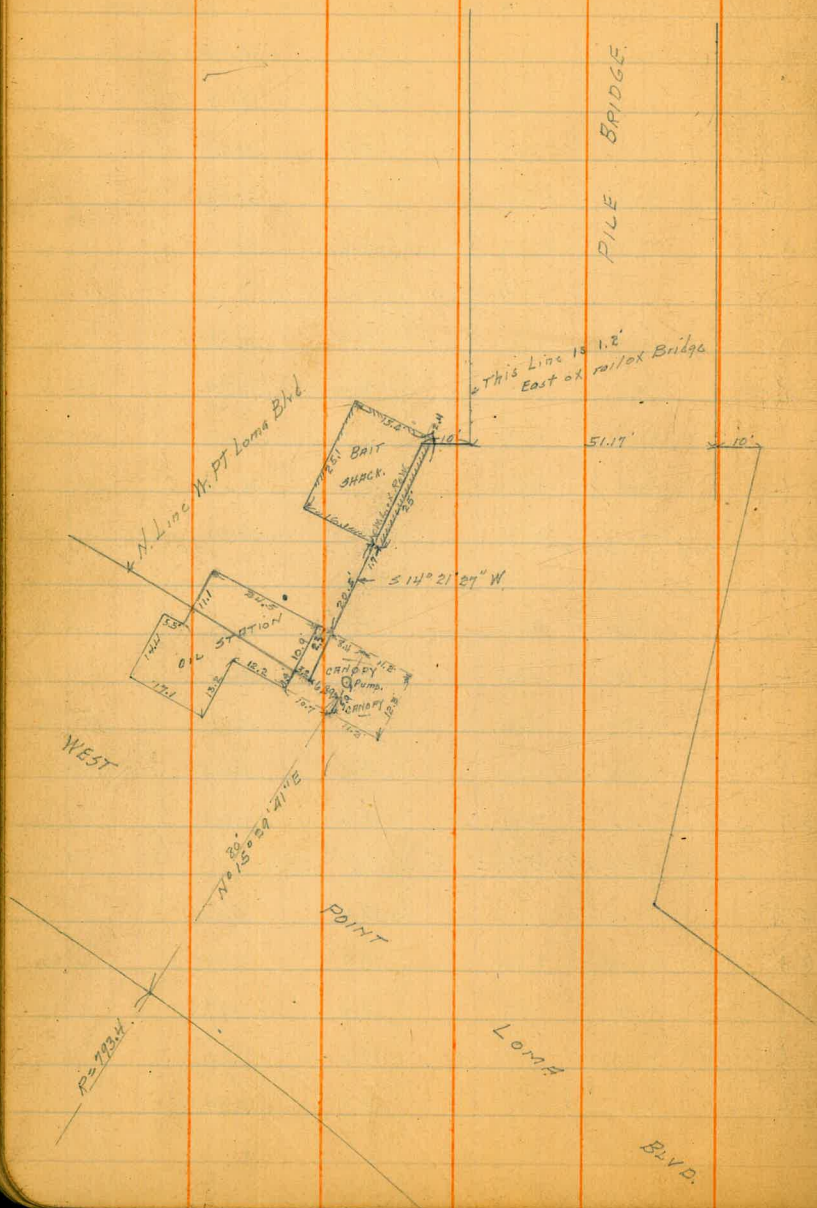
15' R	3.4	309.5
10' R	3.0	308.9
C	2.6	309.3
10' L	2.6	309.3
15' L	2.9	309.0



1/7/41  
Goreard  
Miller  
Shaw

Location of Improvements  
on West Point Loma Blvd  
at Mission Bay Bridge

46



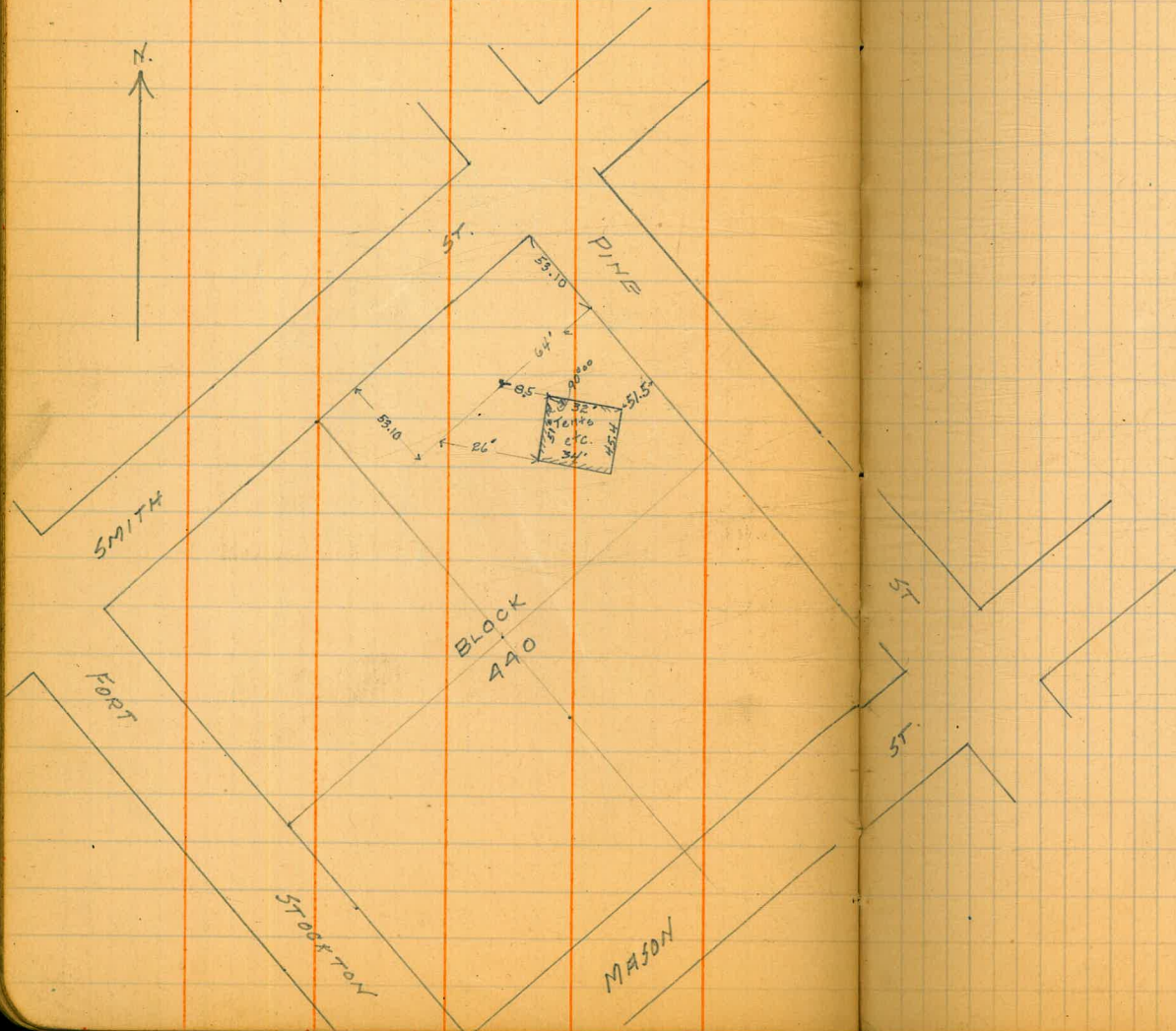


Gregory  
Miller  
Shaw

Location of Campers on  
BLK 440 OLD TOWN

Gregory  
Miller  
Shaw

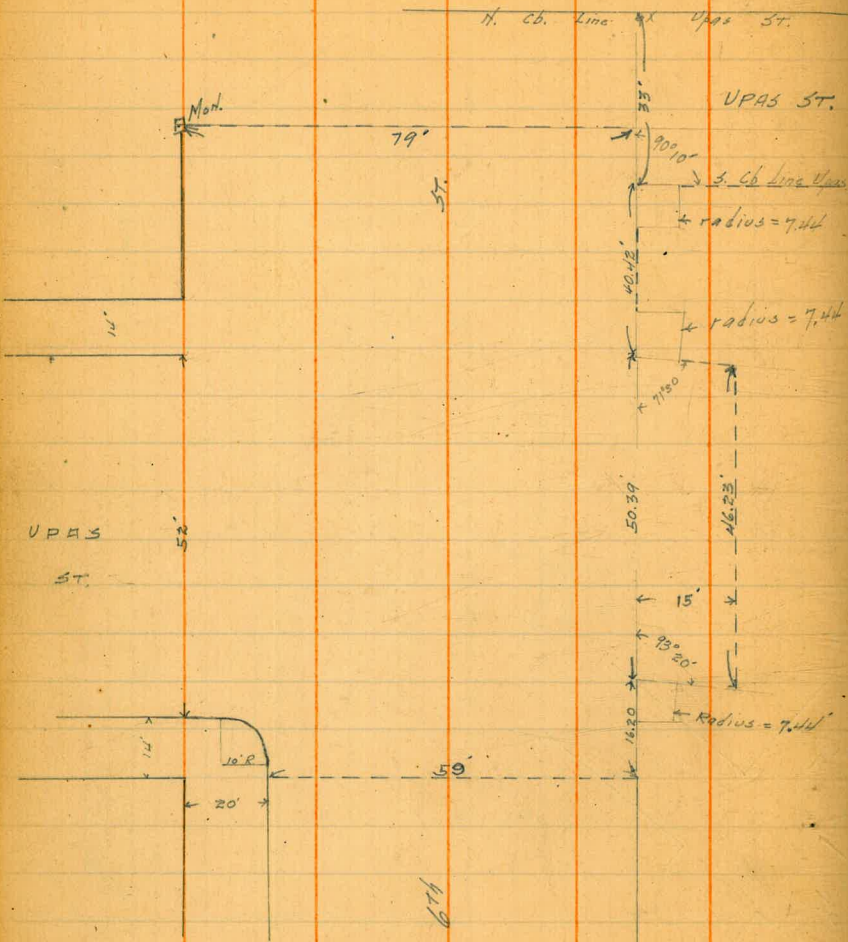
47





Gregory  
Miller  
Shaw

Survey of Intersection of  
6th + Upas for  
Paving







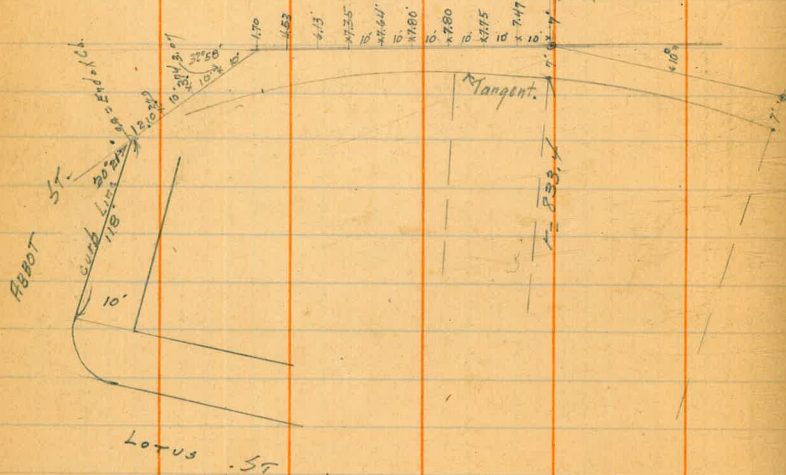


2/1/21

Location of Curb of West Pt Loma Blvd  
and Abbot St.

-These distances are taken to outside of  
Curb.

West Pt Loma Blvd.





Levels on Curb Abbott +  
W. Pt. Loma Blvd. from  
Lotus to Bacon

4.25      6.72      7.47      BP SW Abbott + Yd.

These levels taken on East Cb. of Abbott +  
S. Curb of W. Pt. L. Blvd. Distances

given are all on Curb as constructed.

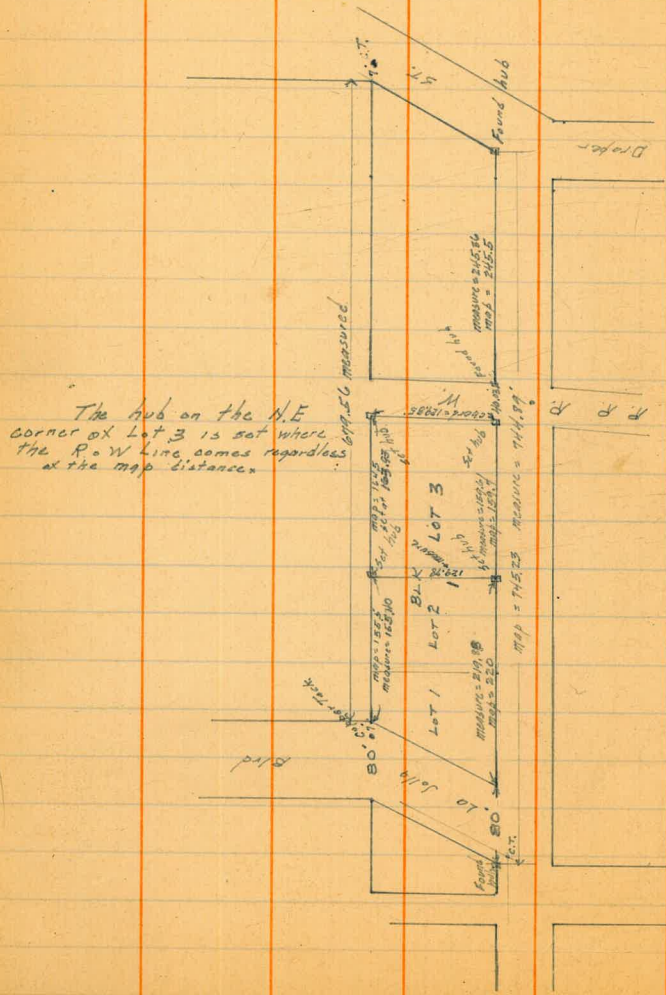
N.L. Lotus		4.25	7.52
118' N. 20+00		4.53	7.19
0+50	3.71	5.70	4.73
1+00			3.84
1+34.6 = P.C. on P/L = 0+00 R=53340		3.93	1.77
0+50		4.13	1.57
1+00		4.44	1.26
1+53.2 = Catch Basin		4.69	1.01
1+78.6 = P.R.C. on P/L = 0+00		4.69	1.01
0+50		3.97	1.73
1+00	5.61	8.09	3.22
1+64.9 = P.T. on P/L = 0+00		4.74	3.35
SW. cor. of Bacon + W. Pt. L. Blvd.		1.58	6.51



4/7/21  
Gregory  
Moore  
Miller  
Shaw

Survey of Lot 3 BLK 1  
F. T. Scripps Add.

52





4/7/21 Gregory  
 171.16  
 Moore  
 Shaw

Levels on  $\Delta$  at 8 8 1010  
 7775

Norwich Ave.  
 from + the E.L. of La Jolla Blvd  
 To - W.L. - Draper St

	B.M.	12.73	84.55	71.82
0-15 = E.L. of La Jolla Blvd. - edge paving.			13.3	71.3
0.0 = 17.1 Angles to NE cor. Marine & La Jolla Blvd.			12.8	71.3
+ 20			10.5	74.1
+ 50			9.5	75.1
1			7.5	77.1
+ 50			5.5	79.1
2			3.5	81.1
+ 40			2.9	81.7
+ 50			3.5	81.1
3			3.4	81.2
T.P.	12.18	95.77	0.96	83.59
+ 50			11.5	84.3
+ 78			9.7	86.1
+ 82			8.4	87.4
+ 88			12.3	83.5
4			11.6	84.2
+ 08.0			11.4	84.4
+ 13			6.9	88.9
+ 50			5.3	90.5
5			2.5	93.3
T.P.	9.45	104.00	1.22	94.55
+ 50			8.7	95.3
6			6.9	97.1
+ 35 = W.L. Draper.			5.2	98.8

NE Sea Lane  
 + La Jolla

+ 65

3.9 100.1  
 37.2 100.28

100.15 SW  
 Marine & Draper



12/3/21

Gregory  
Moore  
Miller  
ShawLevels on Proposed  
Drain Laurel + Curlew

54

## A Line (which runs under Cement Return)

	8.20	152.33	144.13	Spk SW Laurel & Horton
0700 on Curb			4.29	
0+00 in gutter			5.10	
0+17			4.1	
0+35			5.0	
0+50			4.6	
1+00	2+14		4.5	
+10			3.7	
+35			4.8	
+42			3.5	
+50			6.6	
+65			11.6	

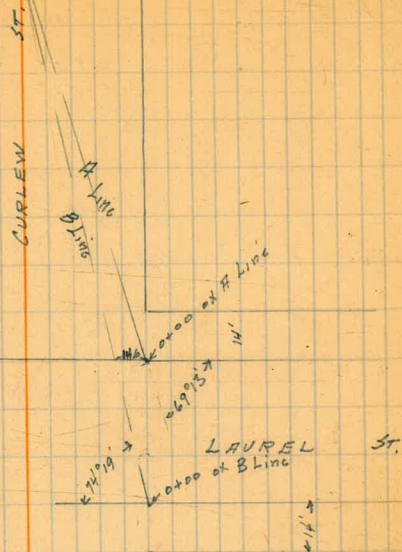
## B Line

	8.20	152.33	144.13
0+00 in gutter			6.97 45.3
0+00 on curb			6.32 46.0
0+27			4.9 47.4
0+50			3.8 48.5
0+54 = 0+146 on A Line			4.4 47.9
1+00			4.5 47.8
+50			4.5 47.8
+60			4.1 48.2
+87			5.0 47.3
+92			3.4 48.9
2			6.4 45.9
+14			11.6 40.7

187 50

190 34

24 60





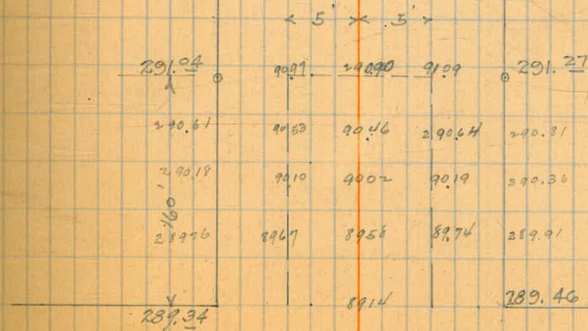
Grade stakes alley in Blk 8.  
Park Add.

489.71 5<sup>th</sup> 30<sup>th</sup> Juniper  
310  
293.66

8974	9019	9064	9109
8972	347	307	357
8967	9010	9053	9097
399	356	313	369

29th

St.



30th

St.



1/26/22  
 Proposed  
 Moorg  
 Miller  
 Stand  
 Tido + Lytton Sts

CROSS SECTION OF  
 New Layout at  
 Tido + Lytton Sts

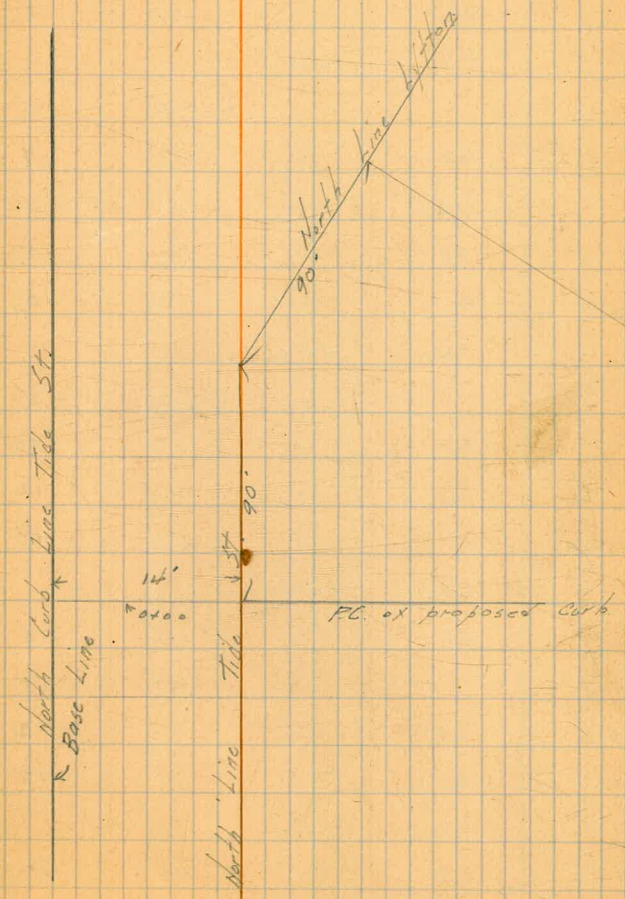
Sections are all taken at Right Angles

To North curb Line of Tido St. Starting 90° E of  
 Intersection of N. property Lines of Tido + Lytton

1.38      3.25      1.27      EP SW  
 Tido + Lytton

P.C. of proposed Curb = 0+00

N. curb Line Tido	1.9	1.4
12' N	2.4	0.9
20' ✓	3.7	-0.4
0+9.0		
20' N	3.8	-0.5
14' ✓	2.3	1.0
3' ✓	2.3	1.0
N. Curb	4.3	-1.0
0+12		
N. Curb	4.4	-1.1
25' N	3.8	-0.5
0+22		
30' N	3.9	-0.6
7' ✓	3.3	0.0
6' ✓	2.0	1.3
N. curb	2.0	1.3
0+25		
N. Curb	2.0	1.3
14' N	1.8	1.5
20' ✓	3.8	-0.5
30' ✓	3.9	-0.6





3.25

0+43

40' N	3.8	-0.5
41' ✓	4.0	-0.7
13' ✓	1.7	1.6
N. cb.	1.8	1.5

0+54

N. cb.	1.5	1.8
13' N	1.6	1.7
21' ✓	4.8	-1.5
30' ✓	4.0	-0.7
45' ✓	4.2	-0.9

0+60

50' N	6.5	-3.2
22' ✓	5.3	-2.0
14' ✓	2.0	1.3
N. cb.	1.5	1.8

0+65

N. cb.	4.1	-0.8
15' N	6.2	-2.9
25' ✓	7.5	-4.2
50' -	8.0	-4.7

0+70

50' N	8.0	-4.7
20' ✓	8.0	-4.7
15' ✓	6.0	-2.7
N. cb.	5.0	-1.7

57

0+73

N. cb.	2.0	1.3
3' N	1.1	2.7
16' N	1.5	1.8
18' ✓	8.9	-5.6
50' -	8.0	-4.7

0+81

60' N	5.7	-2.4
40' ✓	5.7	-2.4
25' ✓	7.2	-3.9
15' ✓	2.0	1.3
4' ✓	1.2	2.1

0+87

5' N	1.5	1.8
15' ✓	1.5	1.8
35' ✓	4.5	-1.2
50' -	5.6	-2.3
70' ✓	5.9	-2.6

1+00

80' N	5.8	-2.5
44' ✓	4.9	-1.6
27' ✓	1.2	2.1
15' ✓	1.1	2.2

1+05

25' N	1.2	2.1
35' ✓	1.2	2.1



	325		
43' N		2.7	0.6
50' ✓		5.3	-2.0
80' ✓		5.6	-2.3

	1+31		
90' N		5.8	-2.5
70' ✓		5.1	-1.8
67' ✓		0.8	2.5
55' ✓		1.0	2.3

	1+42		
65' ✓		0.8	2.5
80' ✓		0.5	2.8
93' ✓		5.4	-2.1



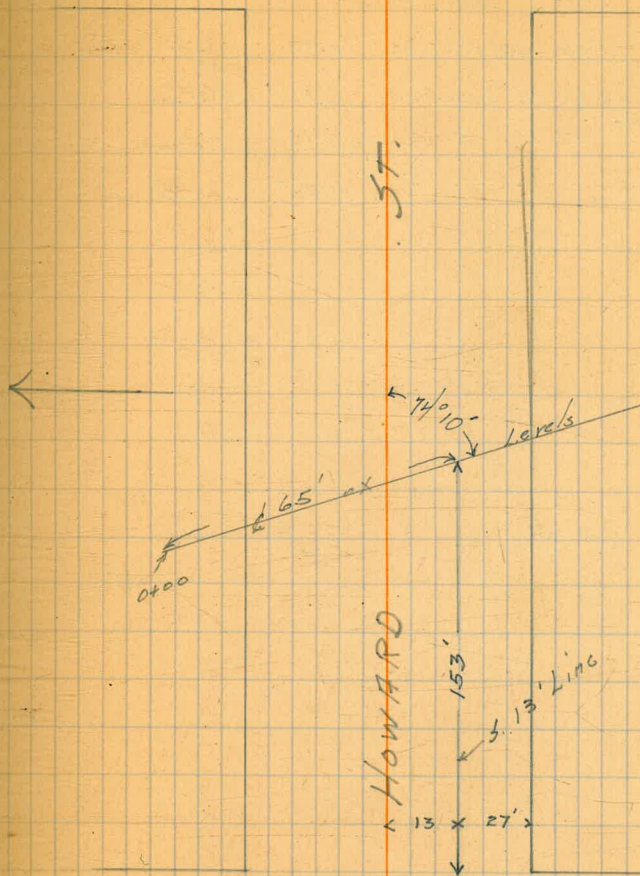
1/26/24 Gregory Culvert on  
 Moore HOWARD ST.  
 Miller  
 Shaw bet Florida, + Alabama.

	0.89	30154		300.65
T.P.	1.42	29201	10.95	290.59
0+00			4.9	87.1
0+38			5.0	87.0
0+50			3.4	88.6
0+71			4.6	87.4
0+73			6.9	85.1
0+80			6.0	86.0
0+85			5.7	86.3
+05.0			7.3	84.7

BD 3W  
 El Cajon Sta

ALABAMA

ST.



FLORIDA

ST.



1/26/22

Levels on 12" Culvert  
on Herman St  
N. of Upas

586  
272  
291

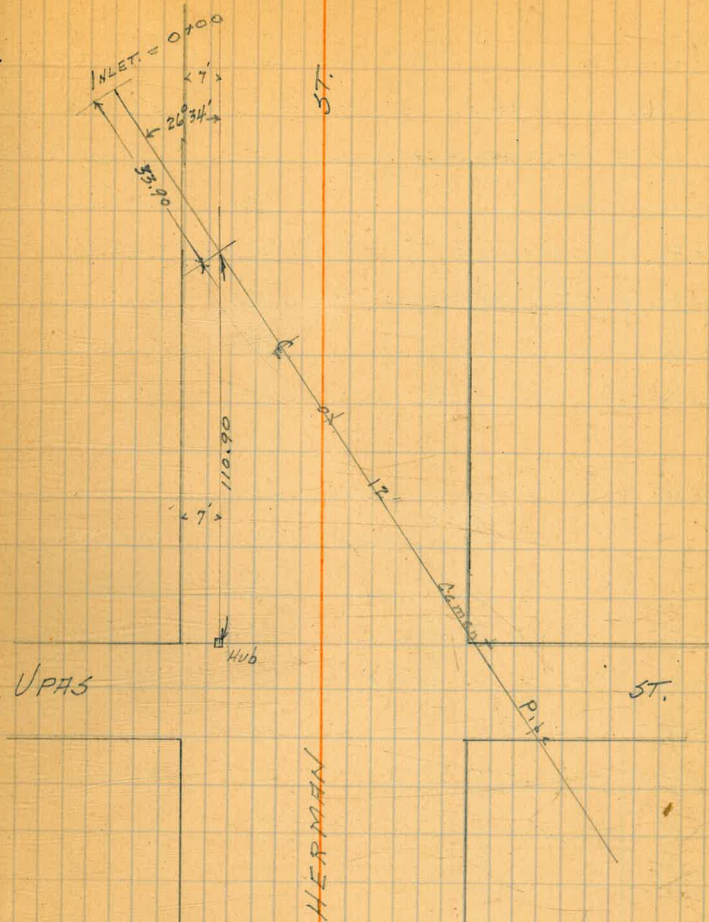
N. of Herman  
+ Upas

on BM	4.18	326.44		322.26
0+00		Flow Line of 12" pipe	6.80	319.64
0+52		Top. of 12" cement pipe	6.91	319.53
1+34	✓	✓	✓	8.78 317.66
1+89	✓	✓	✓	9.95 316.49

586  
272  
291

17.8

60



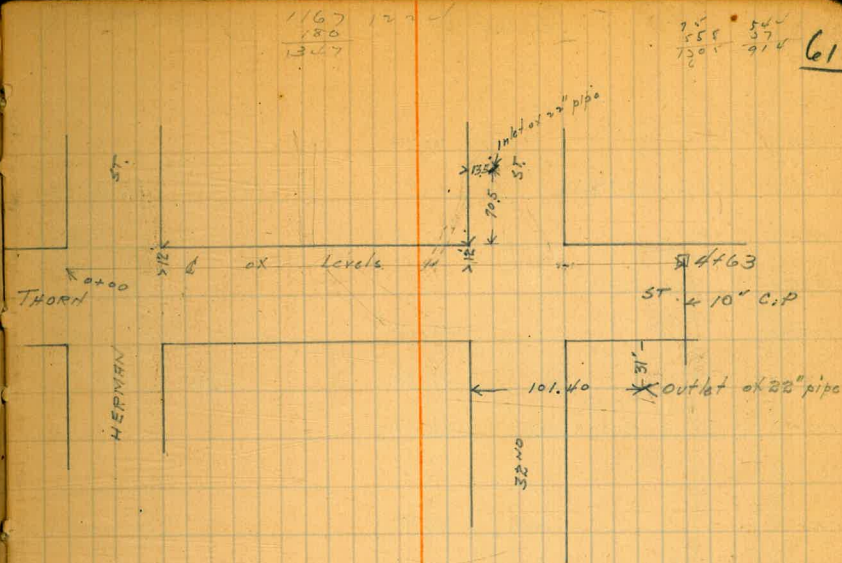


Gregory Levels on a proposed Drain.  
Miller. 2' outside N Curb Line of  
Shaw. Thorn St  
from W.L. Herman to Drain  
under Thorn E. of 3<sup>rd</sup>

on B.M.	1.70	321.06	319.36	36 <sup>th</sup> NW Herman Thorn
0+00 =	W.L. Herman	3.3	317.8	
0+12		3.5	317.6	
0+32.5		3.9	317.2	
0+65 =	E.L. Herman	4.6	316.5	
1+00		5.9	315.2	
+50		8.5	312.6	
2		10.3	310.8	
+50		12.3	308.8	
T.P.	2.44	310.77	14.73	308.33
3		4.2	306.6	
+39 =	W side C.B. Top.	6.3	304.5	
+39 =	✓ ✓ ✓ bottom	8.6	302.2	
+41.5 =	E ✓ ✓ ✓	8.6	302.2	C.B. = 2' x 2.5'
+41.5 =	✓ ✓ ✓ Top	5.8	305.0	
+61		7.9	302.9	
+67		7.1	303.7	
4		7.4	303.4	
+50		8.1	302.7	
+63 =	Center of 2' x 2' C.B.	8.6	302.2	
T.P.	6.06	305.86	10.97	299.80
			14.38	291.48
T.P.	3.70	297.06	12.50	293.56
			13.47	283.59

Flow Line  
Inlet of 22"

Flow Line  
Outlet of 22"





Grades on Pershing Drive

Station	W	E
5+50	+11.0	+11.5 nail
	+3.77	+0.67
5+00	+3.60	+0.35
4+50	+3.11	+0.45
4+39.72 P.C.	96.46	96.95
4+00	17.93 Break. 96.0	96.10
3+50		95.4
3+00	+0.62	94.7
2+50		94.0
2+14.30 P.T.	+0.20	93.5
2+00	+0.20	93.3
1+50	+1.14	92.6
1+00	+1.54	91.9
0+50	+1.46	91.2
0+00	+1.0	90.50

4 parts  
5.264

6 parts

Station	W	E
12+00		
11+64.05 P.C.	+5.5	87.12
11+50		
11+00	+5.1	break
10+50		89.78
10+00	+3.7	Break
9+50		91.28
9+00	+1.5	91.50
8+50		92.28
8+00	+4.56	92.78
7+50		93.28
7+00	+4.6	93.78
6+50		94.08
6+00		94.38
5+99.49 P.C.	+3.5	93.91

11 88.1  
89.6  
10 90.1  
90.9  
9 91.5  
8 92.0  
8 92.4

32  
06  
192  
94.6  
95.1  
95.6  
95.9

94.88  
594  
95.88  
544  
95.88  
494  
96.88  
444  
96.88

160  
9090  
451  
9298  
96.0  
25947  
37943  
40939  
51924  
52922  
2530  
319  
96.0  
389  
98.0  
93.5  
50

95.17  
332  
98.9

48 101.33  
630  
7523  
350  
100.53

726  
813  
853  
903  
993  
1193  
126  
134  
133  
134  
135

0.3  
0.2  
0.2  
0.2



18+00		86.17	86.5
17+97.5 = N End of Bridge		86.14	86.35
17+54.70 = S End of Bridge		85.84	
17+54.61 F.C.		85.84	
17+50		85.83	
	CCP - 1.7		- 2.9
17+00		85.70	
16+50		85.58	
16+08.92 P.C.	85.87	85.47	85.07
16+00		85.46	
15+50		85.33	
15+00		85.20	- 2.1
14+50	Break.	85.08	
14+00		85.18	
13+50	Break.	85.29	112.5 104.5 7.7
13+00		85.94	
12+55.68 E.C.		86.54	
12+50		85.70	

86.67

9303	8574	997	1002	1007	1013	8547	8528	851	27	2478	2490
268	797	2483	8470	8559	10319	310.19	1048	1062	1068	1068	1071
7826	1033	1033	70.96	1009	8518	1048	8527	8540			
977	8504	8654	917	8619	87.24	8759	1037	1026			
8789	97	917		8779	8.42	8759	8795	877			
180											
9672											
24+50						114.54					
24+00						111.30			87.42	85.59	183
23+50						108.07			89	86.8	86
23+00						104.84			87.1	83	87.2
22+50						101.61			77	87.8	77
22+14.44 E.C.						99.30			85.6	84.02	86.52
22+00						98.37			84.96	87.44	88.0
21+50	E.V.C.					95.14					
21+46						93.60					
21+00						92.24					
20+75						91.05					
20+50						90.04					
20+35						89.19					88.67 = 400
20+17.34 P.C.						88.51					
20+00						88.51					
19+75						88.01					
19+50	P.V.C.					87.67					
19+00						87.17					86.67
18+50						86.67					86.50



31+02.84 PC

154.17

31+00

154.7

30+50

151.7

30+00

148.7

29+50

145.7

29+00

142.7

28+50

139.7

28+00

136.7

27+50

133.7

27+00

Break

130.7

26+96.66 EC

130.59

26+50

127.47

26+03.05 PC

124.43

26+00

124.24

25+50

121.0

25+00

117.77

37+50

193.7

37+00

190.7

36+50

187.7

36+00

184.7

35+50

181.7

35+00

178.7

34+53.51 EC

175.91

34+50

175.7

34+00

172.7

33+50

169.7

33+00

166.7

32+50

163.7

32+00

160.7

31+50

157.7



44+14.5Z PC	220.19
44+00	219.70
43+50	218.0
43+00	216.3
42+50	214.6
42+00	212.9
41+50	211.2
41+00	209.5
40+50	207.8
40+00	E.V.C. 206.1
+75	205.21
39+50	204.24
+25	203.19
39+00	202.05
+75	200.83
38+50	199.44
+25	198.16
38+00	P.V.C. 196.7

51+00	245.95
50+50	243.9
50+00	241.85
49+50	239.80
49+00	237.75
48+50	235.70
48+00	233.65
47+50	Break 231.6
47+00	229.9
46+42.29	229.64
46+23.86 = E.C.	
46+50	228.2
46+00	226.5
45+50	224.8
45+00	223.1
44+50	221.4



+75	P.V.C.	237.80
57+50		238.63
57+00		240.28
56+50		241.93
56+28.75 E.C.		242.62
56+00		243.58
55+50	Break.	245.23
55+00		246.13
54+50		247.03
54+00		247.93
53+76.55 P.C.		
53+50		248.83
53+00	E.V.C.	249.73
+75		250.05
52+50		250.13
+75		249.91
52+00		249.56
+75		248.91
51+50	P.V.C.	248.00

64+00		246.25
63+50		245.4
63+00		244.55
62+50		243.70
62+00		242.85
61+50	Break.	242.0
61+00		240.88
60+50		239.77
60+00, 16 P.C.		238.66
59+50		237.55
+75	E.V.C.	237.00
59+00		236.56
+75		236.34
58+50		236.31
+75		236.61
58+00		237.10



70+50 256.40

70+00 256.0

69+50 Break 255.6

69+00 254.76

68+50 253.90

68+00 253.05

67+50 252.20

67+00 251.35

66+50 250.5

66+00 249.65

65+50 248.8

65+00 247.95

64+76.29 EC 247.56

64+50 247.10

77+00 260.34

76+61.50 EC 260.17

76+50 260.12

76+00 259.9

75+50 259.68

75+00 259.46

74+80.28 PC 259.38

74+50 259.24

74+00 259.02

73+50 Break 258.8

73+00 258.4

72+50 258.0

72+00 257.6

71+50 257.2

71+00 256.8



+75	P.V.C.	284.1
83+50		282.6
83+31.13	P.C.	281.46
83+00		279.6
82+50		276.6
82+00		273.6
81+50		270.6
+25	E.V.C.	269.1
81+00		267.69
+75		266.45
80+50		265.39
+25		264.5
80+00		263.79
+75	P.V.C.	263.25
79+50		262.8
79+00		261.9
78+50	Break	261.0
78+00		260.98
77+50		260.56

90+06.38	P.C.C.	
90+00		293.98
+75		292.88
89+50		291.93
+25		291.13
89+00		290.48
+75		289.99
88+50		289.66
+25		289.48
88+00	P.V.C.	289.45
87+67.07	P.C.	289.52
87+50		289.55
87+00		289.65
86+51.35	E.C.	289.75
86+50		289.75
86+00		289.85
+75	E.V.C.	289.9
85+50		289.85
+25		289.61
85+00		289.18
+75		288.55
84+50		287.73
+25		286.71
84+00		285.50

29.15 = 42

290.10 = 42



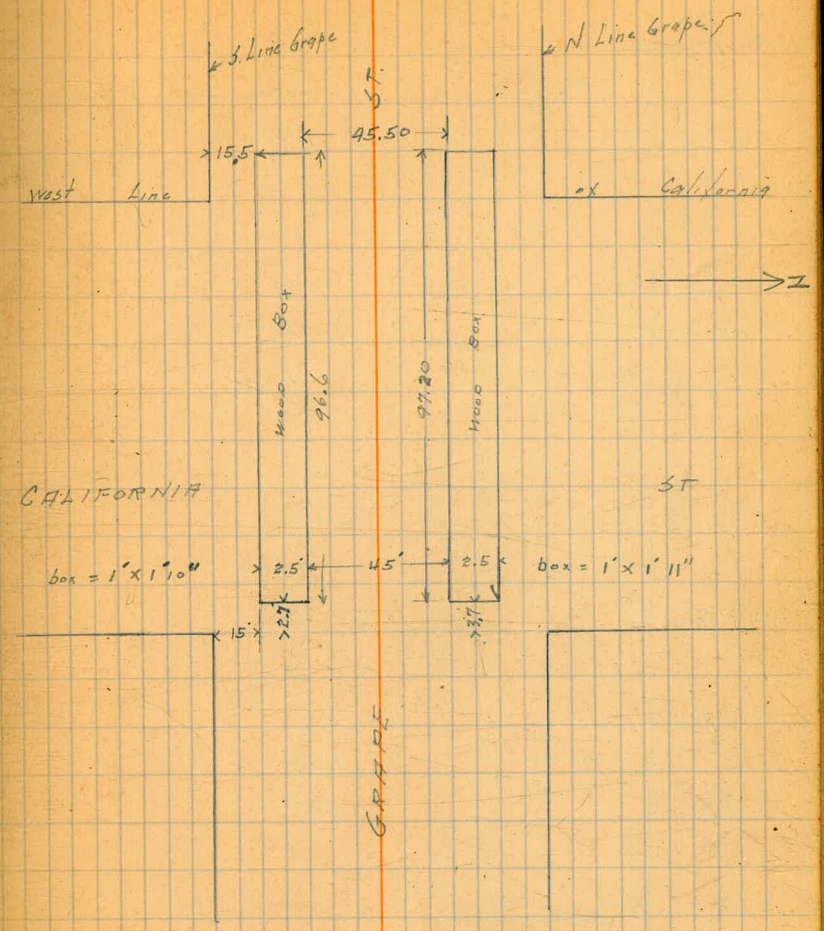
+75		327.30
96+50		326.82
+75		326.23
96+00		325.54
+75		324.75
95+50	P.V.C.	323.85
95+00		321.95
94+50		320.05
94+00	E.V.C.	318.15
+75		317.15
93+50		316.04
+75		314.82
93+00		313.50
+75		312.07
92+50		310.54
+75		308.9
92+00	P.V.C.	307.15
91+50		303.55
91+00	E.V.C.	299.95
+75		298.23
90+50		296.66
+75		295.25

99+20.8 = Mon	328.94 = Pavement
99+00	328.85
98+50	328.61
98+00	328.37
97+66.47 EC	
97+50 E.V.C.	328.13
	327.96
97+00	327.68



1/20/20 Oregon Show Culverts at Grape and California

on BM.	0.60	4/10	4/10	BP SW Grape Indit
	076	32.46	12.92	31.70
	4.50	24.42	12.56	19.92
Inlet of Box on N.			5.72	
Outlet ✓ ✓ ✓ ✓			7.90	
✓ ✓ ✓ ✓ S			7.79	
Inlet of ✓ - S			5.41	
East Track over S Box.			4.96	
Center ✓ ✓ ✓ ✓			5.22	
Main ✓ ✓ ✓ ✓			5.32	
✓ ✓ - N ✓			5.50	
Center ✓ ✓ ✓ ✓			5.40	
East ✓ ✓ ✓ ✓			5.20	





36+70.99 EC.

35+78 Δ 16°30' L

33+83.01 PC.

R=1000'

st=174.99

EC=487.98

30+86.11 EC

29+48° Δ 16°00' L

48+07.46 PC

R=1000

st=140.54

EC=499.25

47+68.01 EC

46+55 Δ 18°40' L

45+39.95 PC.

R=700

st=115.05

EC=228.06

20+17.93 EC.

19+50.0 Δ 75°30' R.

18+53.41 PC.

R=145

st=96.79

EC=164.72

12+00 ⊙

7+39.49 EC.

5+55 Δ 14°10' L

3+68.61 PC

R=1500

st=186.39

EC=370.88

R=500

st=58.44

0+00 =

app. 46+50  
pp. 46

Δ 13°40' P

20' x 30' x  
hub

20' x 30' x  
hub hub

20' x 30' x  
99' 20' x hub

29' x hub  
stump  
bush  
20' app. nail

hub 82' 25'  
x 29' nail  
12' x hub  
40' app. x nail

hub  
x 10' 30' x  
33' app. x hub



87+67.57 = Bolo P.C. on "A line"  
 61+55.31 = Equ.

60+49.66 EC R=350  
 58+97.20 Δ 54° 25' Lt ST=179.95  
 57+17.25 PC Ex=43.51

55+11.91 EC R=6000  
 53+20 Δ 3° 40' Rt ST=192.06  
 51+27.94 PC Ex=9.06

49+20.89 = 49+22.41 new EC.

48+17.60 EC R=800 1500  
 47+00 Δ 17° 0' Rt ST=119.56 224.17  
 45+80.44 PC 44+75.83 Ex=16.67  
 Ex=445.06

42+46.01 EC R=2200  
 40+45 Δ 10° 30' L ST=704.16  
 38+44.84 PC Ex=403.17

Hub (X) 30 37 AM No 6

**DIRECTIONS FOR USE OF TABLES**

TABLE No. 1.

Distance of slope stake from side or shoulder  
 stake for any width roadway, slope 1 to 1.  
 If ground is nearly level the cut or fill at side  
 stake is located by the double entry method in  
 the table. The number in the  
 column and row gives distance  
 from stake to center of roadway.  
 PI = 550' Δ 55° 9' ST=161.59

**IMPROVED TABLES**

AND

**INFORMATION**

If it does not make the right adjustment

TABLE No. 2.

To find tangent and external distance of  
 curve of degree of curve and  
 add correction found in column of  
 correction.  $98.30 \div 3 = 32.76$   
 $30 \times 20 = 600$

Degree of curve with a given L may be found  
 by dividing tangent (or external), opposite L by  
 given tangent (or external).

The distance from a point on the tangent to  
 the curve is very nearly the square of the tangent  
 length divided by twice the radius.

• 40 x 30 x



