

1094

LEVEL BACK

373

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

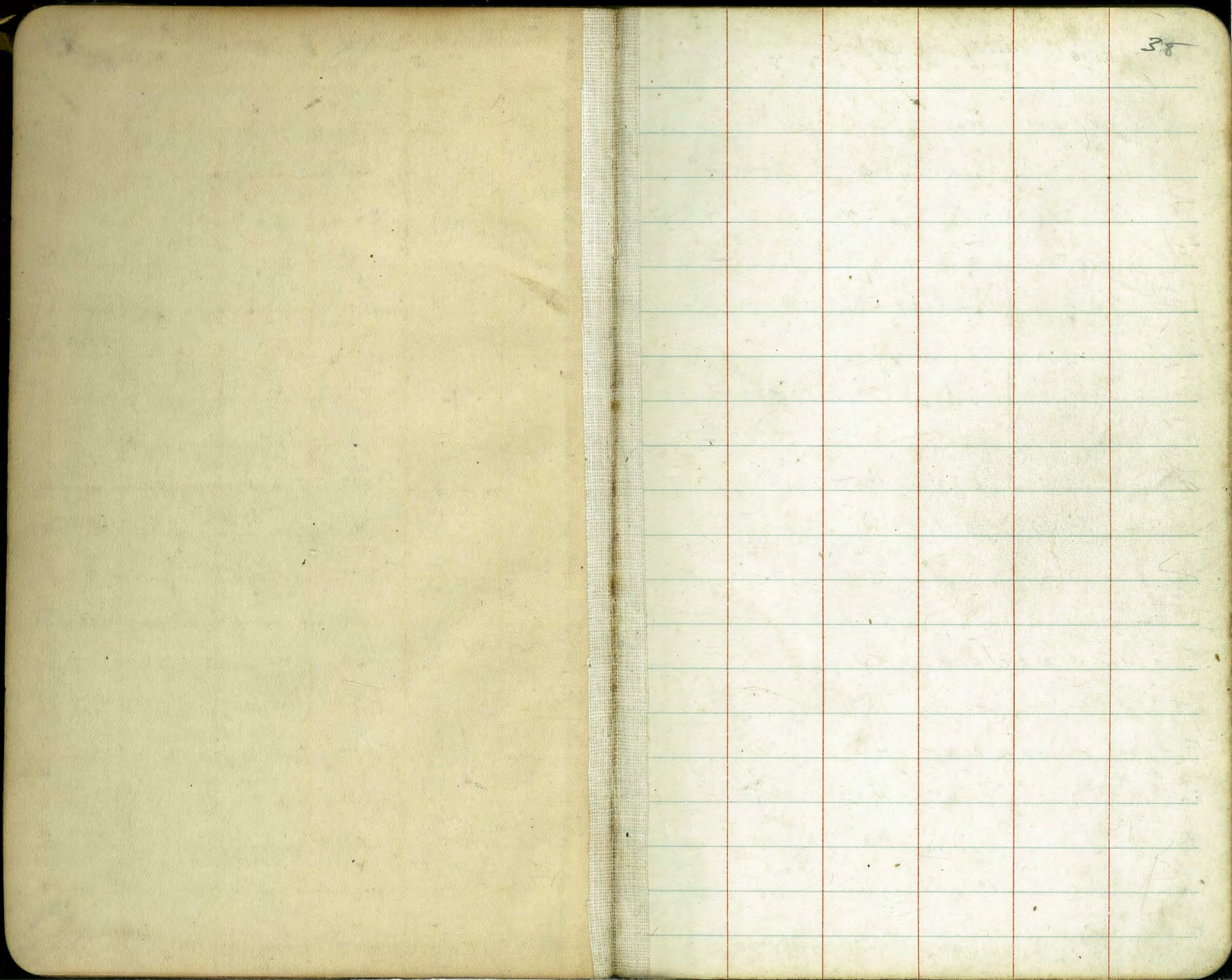
"Copyright, 1895, by Keuffel & Esser Co."

MICROFILMED

DEC 19 1968
330

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.



38

8/9/22
Gregory
1700/02
E1118
Shaw

CROSS SECTION OF 15' wide
ALLEY bet 30th Dale
from Redwood to H.

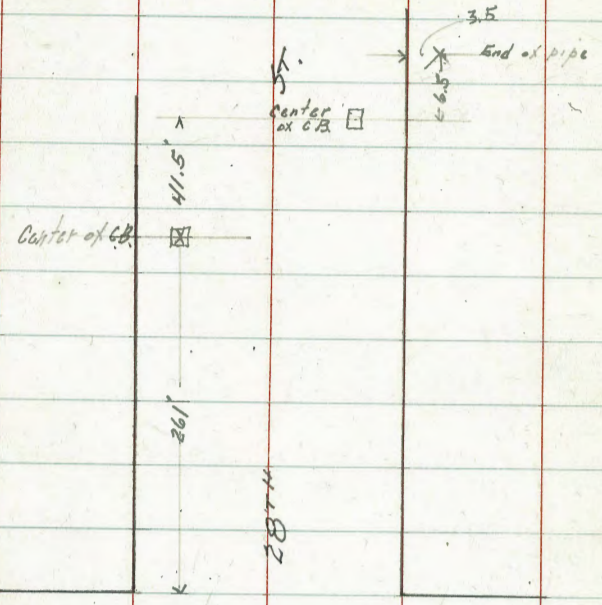
318.77

					C	5.0	309.7 313.8
	12.61	314.67	302.06	SW 30 th Redwood	E	5.2	309.5 313.6
	N. c.c. of Redwood					150' N	
W		7.40	307.27	on cement	E	8.6	306.1 310.2
E		8.07	306.60	on cement	C	7.6	307.1 311.2
	N.L. Redwood				W	6.8	307.9 312.0
E		7.4	307.8			175' N	
C		7.0	307.7		W	13.1	302.6 305.7
W		6.5	308.2		C	15.0	299.7 313.8
T.P.	585	318.77	175	312.92	E	17.0	297.7 301.8
	33' N						
W		4.4	311.3 314.3				
C		4.6	311.1 314.2				
E = floor of garage, cement		4.2	311.5 314.51				
	40' N						
E = floor of garage cement		4.15	311.52 314.64				
C		4.1	311.6 314.7				
W		4.0	311.7 314.8				
	100' N						
W		4.7	310.0 314.0				

Plotted 8/11/22
J.M.

3/10/22
Gregory
Moore
E.M.S.

Location of C.B.
28th N. of K.



K.

St.

8/9/27	Gregory Moore Ellis Shaw	X section at Greeley Ave. 30th to 31st.	80' wide		X-sec. Drq. No. 3307			
			79.0				79.0	3
	5.39	79.05	73.66	No. 50th 30th to Martin	+12		73.3	
		E.L. 30th St			+20		73.5	
					+27		74.4	
5		4.3	74.7		+30		74.1	
+10		4.2	74.8		+40		74.2	
+14		4.5	74.5		+50		74.4	
+20		4.5	74.5		+53		74.4	
+27		4.5	74.5		+60		74.0	
+30		4.5	74.5		+66		73.4	
+40		4.3	74.7		+70		73.5	
+50		4.1	74.9		5		74.2	
+53		4.3	74.7		TP	0.05	76.81	76.8
+60		4.7	74.3				76.76	
+66		4.9	74.1					
+70		4.9	74.1			50'E		
N		4.7	74.3		5		3.6	73.2
		25'E			+10		3.7	73.1
					+14		4.0	72.8
					+20		3.8	73.0
N		4.8	74.2		+27		2.8	74.0
+8		4.8	74.2		+30		2.8	74.0
+10		5.4	73.6		+40		3.0	73.8

76.81

76.8

+50	27	74.1
+53	27	74.1
+57	28	74.0
+60	35	73.3
+66	41	72.7
+70	39	72.9
+72	33	73.5
N	34	73.4
75'E		
N	37	73.1
+10	38	73.0
+14	41	72.7
+20	42	72.6
+27	33	73.5
+30	31	73.7
+40	36	73.4
+50	33	73.5
+53	36	73.2
+60	41	72.7
+66	47	72.1

+70

5

5

+10

+14

+20

+27

+30

+40

+50

+53

+60

+66

+70

+72

N

N

+10

GREELEY

76.8

41

34

100'E

36

40

50

51

40

36

39

37

42

50

47

45

42

41

125'E

47

45

72.7

73.4

73.2

72.8

71.8

71.7

72.8

73.2

72.9

73.1

72.6

71.8

72.1

72.3

72.6

72.7

72.1

72.3

76.81

768

+14	5.0	71.8
+20	5.5	71.3
+27	4.8	72.0
+30	4.7	72.1
+40	4.6	72.3
+50	4.4	72.4
+53	4.7	72.1
+60	5.3	71.5
+66	5.3	71.5
+70	5.5	71.3
5	5.2	71.6
150° E		
5	5.4	71.4
+10	5.5	71.3
+14	5.5	71.8
+20	5.5	71.8
+27	5.4	71.4
+30	5.2	71.6
+40	5.0	71.8
+50	4.9	71.9

GREELEY

768

+53	5.2	71.6
+60	5.9	70.9
+66	5.8	71.0
+70	5.3	71.5
N	5.3	71.5
175° E		
N	5.4	71.4
+10	5.8	71.0
+14	6.1	70.7
+20	6.1	70.7
+27	5.7	71.1
+30	5.6	71.2
+40	5.3	71.5
+50	5.4	71.4
+53	5.5	71.3
+60	5.6	71.2
+66	5.6	71.2
+70	5.2	71.6
5	5.2	71.6

76.81

200° E

76.8

+30

5.9

70.9

5

5.5

71.3

+40

6.3

70.5

+10

5.7

71.1

+50

6.1

70.7

+14

6.2

70.6

+53

6.2

70.6

+20

6.1

70.7

+60

6.4

70.4

+27

5.7

71.1

+66

6.5

70.3

+30

5.7

71.1

+70

6.3

70.5

+40

5.7

71.1

5

5.7

71.1

+50

5.5

71.3

350° E

+53

5.7

71.1

5

6.6

70.2

+60

6.4

70.4

+10

6.7

70.1

+66

6.6

70.2

+14

7.1

69.7

+70

6.4

70.4

+20

7.2

69.6

N

6.1

70.7

+27

7.0

69.8

225° E

+30

7.0

69.8

N

6.9

69.9

+40

7.1

69.7

+10

7.1

69.7

+50

6.7

70.1

+14

7.4

69.4

+53

6.5

70.3

+20

7.1

69.7

+60

7.7

69.1

+27

6.1

70.7

+66

8.1

68.7

GREELEY

76.8

	76.81	<u>76.8</u> 69.1			GREFLEY <u>76.8</u>	7
+70		7.7		+20	8.7	68.1
N		7.8	69.0	+27	8.8	68.0
	275' E			+30	8.8	68.0
N		8.6	68.2	+40	8.8	68.0
+10		9.0	67.8	+50	8.7	68.1
+14		9.1	67.7	+53	8.7	68.1
+20		8.7	68.1	+56	8.7	68.1
+27		8.0	68.8	+60	9.5	67.3
+30		7.9	68.9	+66	10.3	66.5
+40		8.0	68.8	+70	10.7	66.1
+50		7.8	69.0	N	10.7	66.1
+53		7.8	69.0			
+60		7.8	69.0	N		
+66		7.7	69.1		325' E	
+70		7.4	69.4	+10	11.8	65.0
S		7.3	69.5	+14	11.7	65.1
	300' E			+20	11.5	65.3
S		7.7	69.1	+27	11.3	65.5
+10		8.2	68.6	+30	10.0	66.8
+14		8.5	68.3	+40	9.5	67.3
				+50	9.5	67.3
					9.3	67.5

	76.81		76.8			375 F		GREELEY	8
								66.4	
+53			9.3	67.5					
+60			9.4	67.4		N		4.3	62.1
+66			9.5	67.4		+10		4.2	62.2
+70			9.2	67.6		+14		4.1	62.3
S			8.9	67.9		+20		3.3	63.1
		350 F				+27		2.9	63.5
S			9.1	67.7		+30		2.6	63.8
+10			10.0	66.8		+40		1.9	64.5
+14			10.2	66.6		+50		1.6	64.8
+20			10.5	66.3		+53		1.9	64.5
+27			10.3	66.5		+60		1.6	64.8
+30			10.3	66.5		+66		1.0	65.4
+40			11.1	65.7		+70		0.4	66.0
+50			12.2	64.6		S		+0.4	66.8
+53			12.1	64.7					
								400 F	
+60			12.6	64.2		S		0.6	65.8
+66			12.8	64.0		+10		1.5	64.9
+70			13.1	63.7		+14		1.8	64.6
N			12.9	63.9		+20		2.4	64.0
T.P.	1.20	66.44	11.57	65.24		+27		2.6	63.8

	66.44	(66.4)					GREELEY	9
+30		2.6	63.8		+70		2.6	63.8
+40		2.6	63.8		5		2.0	64.4
+50		3.4	63.0			450' E		
+53		3.8	62.6		5		3.0	63.4
+60		4.9	61.5		+10		3.7	62.7
+66		5.4	61.0		+14		4.0	62.4
+70		5.2	61.2		+20		4.1	62.3
N		5.1	61.3		+27		4.1	62.3
	445' E				+30		4.2	62.2
N		6.4	60.0		+40		5.2	61.2
+10		6.2	60.2		+50		6.0	60.4
+14		6.1	60.0		+53		6.4	60.0
+20		5.9	60.5		+58		7.2	59.2
					+60		8.7	57.7
+27		5.5	60.9		+66		9.4	57.0
+30		5.3	61.1		+70		10.0	56.4
+40		4.5	61.9		N		9.6	56.8
+50		3.6	62.8		+10		9.7	56.7
+53		3.8	62.6			475' E		
+60		3.4	63.0		-10		11.3	55.1
+66		3.0	63.4		N		11.5	54.9

66.44		(66.4)	GREELEY		10
+4	11.7	52.7	+27	7.7	58.7
+10	12.3	54.1	+30	8.3	58.1
+12	12.2	54.2	+33	8.5	57.9
+20	10.9	55.5	+36	10.4	56.0
+27	9.9	56.5	+40	11.2	55.2
+30	9.3	57.1	+47	12.2	54.2
+40	7.9	58.5	+50	12.9	53.5
+43	7.7	58.7	+53	13.1	53.3
+44	6.4	60.0	+60	14.5	51.9
+50	6.0	60.4	+66	14.9	51.5
+53	5.5	60.9	+70	14.8	51.6
+60	5.0	61.4	N	13.9	52.5
+66	4.8	61.6	+10	14.7	52.3
+70	4.1	62.3			
S	3.3	63.1		525' E	
	500' E		-10	16.5	49.9
			N	16.3	50.1
S	4.2	62.2	+10	16.4	50.0
+10	5.4	61.0	+14	16.3	50.1
+14	5.6	60.8	+20	16.0	50.4
+20	6.1	60.3	+27	15.2	51.2

		66.44	(66.4)			GREELEY	(54.0)	"
+30			15.2	51.2	+27	1.2	52.8	
+34			14.8	51.6	+30	2.0	52.0	
+34.1			13.9	52.5	+40	3.4	50.6	
+40			13.5	52.9	+45	3.6	50.4	
+50			11.1	55.0	+46	4.2	49.8	
+53			9.8	56.6	+50	4.6	49.4	
+60			8.0	58.4	+53	4.8	49.2	
+62			7.6	58.8	+60	4.9	49.1	
+62.1			6.8	59.6	+66	5.4	48.6	
+66			6.1	60.3	+70	6.3	49.7	
+70			5.6	60.8	N	6.1	49.9	
5			5.0	61.4	+10	6.5	49.5	
		550'E				575'E		
5			8.3	58.1	-10	7.3	46.7	on walk to house
+10			8.9	57.5	N	7.3	46.7	
+14			10.0	56.4	+10	7.5	46.5	
+17			10.6	55.8	+14	7.6	46.4	
+17.1			11.6	54.8	+20	6.8	47.2	
+20			12.2	54.2	+27	7.0	47.0	
T.P.	0.08	53.99	17.53	53.91	+30	7.2	46.8	

5399

540

+40	61	47.9	
+50	55	48.5	
+53	51	48.9	
+60	43	49.7	
+66	34	50.6	
+70	2.8	51.2	
5	1.7	52.3	
			10' obs -
	600' F = WL 3/5 ⁺	60' ST. 10' 1/2's	
5	3.9	50.1	
+10	5.6	48.4	
+14	6.0	48.0	
+20	6.1	47.9	
+27	7.0	47.0	
+30	7.7	46.3	
+40	8.5	45.5	
+50	9.5	44.5	
+53	9.3	44.7	
+60	9.3	44.7	
+66	9.3	44.7	
+70	9.1	44.9	

GREELEY

540

12

+71	9.0	45.0	
+71.2	9.8	44.2	
N	9.9	44.1	
+0.1	8.0	46.0	
+10	8.0	46.0	
			W. Corb
-10	9.6	44.4	
N	10.3	43.7	
+4	10.9	43.1	
+4.1	10.2	43.8	
+10	10.7	43.3	
+14	10.8	43.2	
+20	10.8	43.2	
+27	10.2	43.6	
+30	10.1	43.9	
+40	9.7	44.3	
+50	8.6	45.4	
+53	8.5	45.5	
+60	7.6	46.4	
+66	7.2	46.8	

	53.99							GREELEY
				54.0				54.0
+70		7.0	47.0		+10		11.3	42.7
S		6.1	47.9		+14		11.4	42.6
		N. 1/4			+20		11.5	42.5
S		7.0	47.0		+27		12.0	42.0
+10		7.7	46.3		+30		11.7	42.3
+14		8.2	45.8		+40		11.1	42.9
+20		9.0	45.0		+50		10.8	43.2
+27		10.0	44.0		+53		10.3	43.7
+30		10.3	43.7		+60		9.5	44.5
+40		10.7	43.3		+66		9.7	44.9
+50		11.2	42.8		+70		8.8	45.2
+53		11.2	42.8		S		7.7	46.3
+60		11.5	42.5					
+66		11.5	42.5		S		8.6	45.4
+70		11.2	42.8		+10		9.9	44.1
N		10.5	43.5		+14		10.2	43.8
+10		10.9	43.1		+40		10.5	43.5
		Center 3/4			+27		11.5	42.5
-10		11.6	42.4		+30		11.9	42.1
N		11.2	42.8		+40		12.3	41.7

E 1/4

5399

540

+50	126	41.4
+53	127	41.3
+60	128	41.2
+66	128	41.2
+70	126	41.4
N	123	41.7
+10	127	41.3
E. Curb		
-10	135	
N	136	
+10	137	
+14	140	
+20	137	
+27	135	
+30	134	
+40	131	
+50	127	
+53	126	
+60	117	
+66	115	

GREELEY

14

+70			11.1	
5			10.1	
		E. L. 31 st		
5			10.9	
+10			12.0	
+14			12.5	
T.P.	5.65	47.92	11.72	42.27
+20			6.6	
+27			7.4	
+30			7.4	
+40			7.7	
+50			8.3	
+53			8.5	
+60			8.7	
+66			9.0	
+70			9.1	
N			8.1	
+10			7.9	
		25' E		
N			10.4	

4792

15

+10	10.5
+14	10.7
+20	10.6
+27	10.6
+30	10.4
+40	9.8
+50	8.6
+53	8.6
+60	8.6
+66	7.9
+70	7.6
5	6.8

chk	5.35
-----	------

42.57 cement cut
SW 31st Martin

		+	+	-	Talbot St.		+	+	-		26
			136.51 ✓					137.84 ✓			
brought from last page Book 840							N.L.		23.6	114.2 ✓	
2+25 M.L.-10'			14.0		122.5 ✓		N.L. + 4		17.0	120.8 ✓	
N.L.-5'			14.2		122.2 ✓		N.L. + 10		17.0	120.8 ✓	
N.L.			20.9		115.6 ✓		+75 M.L. - 10'		18.0	119.8 ✓	
+5			20.9		115.6 ✓		N.L. - 2'		18.3	119.5 ✓	
cb			14.4		122.1 ✓		N.L.		25.5	112.3 ✓	
1/2			14.0		122.5 ✓		+5		25.5	112.3 ✓	
E			11.7		122.8 ✓		+6		18.1	119.7 ✓	
1/2			5.3		131.2 ✓		cb		19.1	118.7 ✓	
cb			0.5		136.0 ✓		1/2		15.1	122.7 ✓	
S.L.			+2.4		138.9 ✓		E		9.5	128.3 ✓	
H	11.32	137.84 ✓	10.10		126.51 ✓		1/2		4.5	133.3 ✓	
Y							cb		0.8	137.0 ✓	
2+50 S.L.			+3.3		141.1 ✓		S.L.		+4.3	142.1 ✓	
cb			1.1		136.7 ✓		3+00 S.L.		+3.5	141.3 ✓	
1/2			4.2		133.6 ✓		cb		2.5	135.3 ✓	
E			10.8		127.0 ✓		1/2		7.2	130.6 ✓	
1/2			14.9		122.9 ✓		E		12.4	127.6 ✓	
cb			17.7		120.1 ✓		1/2		16.0	121.8 ✓	
+3			17.7		120.1 ✓		cb		17.9	117.9 ✓	
+6			23.6		114.2 ✓						

	+	\bar{x} 137.84 ✓	-	Talbot St		+	\bar{x} 132.89 ✓	-		17
+5			19.5	118.3 ✓	+9			17.8	115.1 ✓	
N.L.			26.9	111.0 ✓	N.L.			22.1	110.8 ✓	
N.L. +10			19.1	118.7 ✓	N.L. +5			23.5	109.4 ✓	
2+25 N.L. -15			22.9	117.0 ✓	N.L. +11			17.5	115.4 ✓	
N.L. -10			27.6	110.2 ✓	3+75 N.L. -20			19.1	113.9 ✓	
N.L.			26.3	111.5 ✓	N.L. -5			19.3	113.6 ✓	
+5			20.7	117.1 ✓	N.L. -4			24.1	108.8 ✓	
cb			20.9	116.9 ✓	N.L.			24.1	108.8 ✓	
1/4			18.3	119.5 ✓	+1			19.4	113.5 ✓	
T			13.9	124.0 ✓	+9			19.7	113.2 ✓	
1/4			9.6	129.2 ✓	cb			15.3	117.6 ✓	
cb			4.4	133.4 ✓	1/2			9.3	123.6 ✓	
S.L.			40.3	128.1 ✓	T			2.4	130.5 ✓	
#	2.09	132.89 ✓	7.04	130.80 ✓	1/2			4.3	136.2 ✓	
2+50 S.L.			7.0	139.9 ✓	cb			7.6	140.5 ✓	
cb			1.7	134.6 ✓	S.L.			12.1	145.0 ✓	
1/2			3.0	129.9 ✓	2+100 S.L.			15.0	147.9 ✓	
T			9.7	123.2 ✓	cb			8.8	141.7 ✓	
1/2			14.2	118.7 ✓	1/2			4.0	137.4 ✓	
cb			18.1	114.8 ✓	T			1.5	131.4 ✓	

	+	π 132.89 ✓	-	Tablet St
1/2			9.1	123.8 ✓
+8			15.4	117.5 ✓
cb			20.3	112.6 ✓
N.L.			20.8	112.1 ✓
N.L.+1			24.8	108.1 ✓
N.L.+5			24.8	108.1 ✓
N.L.+7			20.6	112.3 ✓
N.L.+25			21.0	111.9 ✓
+25 N.L.-25			22.5	110.4 ✓
N.L.-8			21.8	111.1 ✓
N.L.-5			25.3	107.6 ✓
N.L.			20.3	107.6 ✓
+1			21.6	111.3 ✓
+8			22.2	110.7 ✓
cb			17.6	115.3 ✓
1/2			10.9	122.0 ✓
cb			4.0	128.9 ✓
1/4			7.2	135.1 ✓
E			17.4	140.3 ✓
S.L.			+11.2	144.1 ✓

	+	π 132.89 ✓	-	
#	0.07	130.75 ✓	2.21	130.68 ✓
+50 S.L.			+11.8	142.6 ✓
cb			+6.2	137.0 ✓
1/2			+1.0	131.8 ✓
E			3.7	127.1 ✓
1/2			10.1	120.7 ✓
+3			12.0	118.8 ✓
cb			20.3	110.5 ✓
+5			23.2	107.6 ✓
N.L.			24.1	106.7 ✓
N.L.+3			24.1	106.7 ✓
N.L.+5			21.5	109.3 ✓
N.L.+25			22.1	108.7 ✓
+813 - WL. AKRON St 30' Wide (Note: Ignored 1/4's & C on this St)				
N.L.-25			23.8	107.0 ✓
N.L.-5			25.2	105.6 ✓
N.L.			25.2	105.6 ✓
cb			21.0	109.8 ✓
+5			14.5	116.3 ✓
1/4			12.5	118.3 ✓

	+	π 130.75 \checkmark	-	Talbot St.	
t			7.7	123.1 \checkmark	cb
1/2			1.0	124.8 \checkmark	1/4
cb			+4.3	135.1 \checkmark	t
S.L.			+8.5 \checkmark	139.3 \checkmark	1/4
#	3.83	125.78 \checkmark	8.90	121.95 \checkmark Pl. Max SL of AKRON ST.	cb
571120 = cont. of Talbot E.L. of AKRON ST. = 00					
S.L.			+13.6	139.4 \checkmark	0+50 S.L.
cb			+7.2	133.2 \checkmark	cb
1/2			+6.8	126.6 \checkmark	1/4
t			3.6	127.2 \checkmark	t
1/4			9.1	116.7 \checkmark	#
cb			16.2	109.6 \checkmark	1/4
N.L.			20.9	104.9 \checkmark	cb
N.L.+3			24.5	101.3 \checkmark	+4
N.L.+7			24.5	101.3 \checkmark	+5 \checkmark
N.L.+8			20.2	105.6 \checkmark	N.L.
N.L.+20			20.2	105.6 \checkmark	N.L.+3
0+20 N.L.-20			25.0 \checkmark	100.3 \checkmark	N.L.+20
N.L.			22.0	103.8 \checkmark	0+70 N.L.-25
+3			26.4	99.4 \checkmark	N.L.-6

	+	π 125.78 \checkmark	-		
			20.2	105.4 \checkmark	
			12.2	113.6 \checkmark	
			7.5 \checkmark	118.3 \checkmark	
			1.0	124.8 \checkmark	
			+4.8	130.6 \checkmark	
			+9.0	134.8 \checkmark	
			+3.8	129.6 \checkmark	
			2.7	123.6 \checkmark	
			8.2	117.6 \checkmark	
			13.6	112.2 \checkmark	
	1.00	114.07 \checkmark	12.71	113.07 \checkmark	
			6.2	107.9 \checkmark	
			12.0	102.1 \checkmark	
			11.9	102.2 \checkmark	
			17.7	96.4 \checkmark	
			17.7	96.4 \checkmark	
			11.8	102.3 \checkmark	
			12.3	101.8 \checkmark	
			13.3	100.8 \checkmark	
			13.6	100.5 \checkmark	

	+	π 114.07 ✓	-	Te2607 St.		+	π 101.74 ✓	-	20
N.L.			19.8	94.3 ✓		N.L + 20		2.4	99.3 ✓
+6			19.4	94.7 ✓		+25 N.L - 20'		3.9	97.8 ✓
cb			12.9	100.7 ✓		N.L - 9		4.5	97.2 ✓
1/2			11.7	102.4 ✓		N.L - 8		11.9	89.8 ✓
±			7.0	107.1 ✓		N.L - 9		11.9	89.8 ✓
1/2			1.6	112.5 ✓		N.L		7.7	92.0 ✓
cb			+3.0	117.1 ✓		+4		4.2	97.5 ✓
S.L.			+8.0	122.1 ✓		cb		4.0	97.1 ✓
1+00 S.L.			+1.2	115.3 ✓		1/4		9.4	97.3 ✓
cb			3.9	110.2 ✓		±		3.4	98.3 ✓
1/2			8.5	105.6 ✓		1/4		1.6	100.1 ✓
±			12.9	101.2 ✓		cb		+2.0	103.7 ✓
#	0.56	101.74 ✓	12.89	101.18 ✓		S.L.		+6.7	108.4 ✓
1/2			2.9	98.8 ✓		1+50 S.L.		+3.2	104.9 ✓
cb			3.1	98.6 ✓		cb		1.7	100.0 ✓
+5			3.2	98.5 ✓		1/2		4.5	97.2 ✓
+6			9.7	92.0 ✓		±		5.4	96.3 ✓
N.L.			9.7	92.0 ✓		1/2		5.7	96.0 ✓
N.L + 8			8.9	92.8 ✓		cb		5.7	96.0 ✓
N.L. + 10			2.7	99.0		cb		5.8	95.9 ✓

	T 101.74 ✓		Talbot St.		T 95.79 ✓		21
N.L.		8.5	93.2 ✓	1/2		2.7	93.1 ✓
N.L. + 4		13.4	88.2 ✓	cb		2.4	93.4 ✓
N.L. + 11		13.4	88.3 ✓	+5		2.9	85.9 ✓
N.L. + 14		5.7	96.0 ✓	N.L.		9.9	85.9 ✓
N.L. + 20		5.0	96.7 ✓	N.L. + 7		8.8	87.0 ✓
1+24 N.L. - 20		7.0	94.7 ✓	N.L. + 8		3.4	92.6 ✓
N.L. - 14		7.6	94.1 ✓	+ 15		2.8	93.0 ✓
N.L. - 5		15.2	86.5 ✓	2+25 N.L. - 10		4.4	91.4 ✓
N.L.		15.2	86.5 ✓	N.L. - 1		4.6	91.2 ✓
cb		6.9	94.8 ✓	N.L.		12.8	83.0 ✓
1/2		7.4	94.3 ✓	+5		12.8	83.0 ✓
±		6.9	94.8 ✓	cb		10.8	85.0 ✓
1/2		6.6	95.1 ✓	+3		4.1	91.7 ✓
cb		5.0	96.7 ✓	1/4		4.4	91.4 ✓
S.L.		1.3	100.4 ✓	±		3.4	92.4 ✓
2+00 S.L.		5.1	96.6 ✓	1/4		2.6	93.2 ✓
cb		6.9	94.8 ✓	cb		3.3	92.5 ✓
#	2.45	95.79 ✓	8.40	93.34 ✓	S.L.	1.4	94.4 ✓
1/2			1.8	94.0 ✓	2+50 S.L.	3.2	92.6 ✓
±			2.7	93.1 ✓	cb	4.1	91.7 ✓

	+	π 90.79 ✓	-	Tarbot St.		+	π 90.79	-		
1/4			9.1	91.7 ✓					Appx 2+92° (to hub) = Azimth point on East face where St Commences to	
±			9.8	91.0 ✓					reverts to 55.62 at the N.L. of Bessemer	
1/4			6.1	89.7 ✓		S.W.		2.2	92.15 ✓	
+3			6.1	89.7 ✓		Cb		7.0	88.8 ✓	
+6			12.5	82.3 ✓		1/4		7.8	88.0 ✓	
Cb			12.5 ✓	82.3 ✓		#	1.66	89.63 ✓	7.82	87.97 ✓
+3			12.6	83.2 ✓		±		1.8		
+6			5.9	89.9 ✓		1/2		1.9		
N.L.			6.0	89.8 ✓		+4		1.8		
N.L. +10			5.7	90.6 ✓		+6		9.8		
2+75° N.L. -10			6.8	89.0 ✓		Cb		9.8		
N.L.			7.7	88.1 ✓		+5		8.9		
+3			7.7	88.1 ✓		N.L.		2.0		
+4			15.0	80.8 ✓		N.L. +10		1.7		
Cb			13.0	82.3 ✓		(Appx 96 Q3)				
+6			6.7	89.1 ✓		2+75° N.L. -10		3.2		
1/4			7.0	88.8 ✓		N.L.		3.1		
±			6.6	89.2 ✓		+6		3.4		
1/4			6.1	89.7 ✓		+8		10.3		
S.W.			2.4	93.4 ✓		Cb		10.3		
						+9		9.3		

	+	π 89.63 ✓	-	Talbot St.		+	π 89.63 ✓	-	
1/2			3.9			+3		6.4	
+			3.0			+5		12.6	
1/4			2.1			cb		12.6	
cb			0.6			+5		10.8	
S.L.			+1.4			+7		6.7	
3+50 S.L.	(Appe 9.2 q5)		0.5			1/2		6.7	
cb			2.9			+		6.1	
1/2			4.2			1/2		6.4	
+			4.3			cb		5.0	
1/2			4.8			+9		6.6	
+2			4.9			S.L.		3.1	
+5			11.4			H	0.40	83.74 ✓	6.29
cb			12.3			EL. Bessemer = 20 S.L.		0.8	83.34 ✓ 277 1000 M.L.
+3			12.3			cb		1.7	
+2			4.9			1/2		1.6	
N.L.			5.0			+		1.8	
N.L. - 10'			4.2			+5		1.9	
3+79 ⁵¹ = N.L. of Bessemer St. (here ^{Talbot} 50.63 wide.) (Bessemer 27.06 wide)						+6		9.0	
N.L. - 10'			5.8			1/4		9.0	
N.L.			6.4			+8		9.0	
						cb		1.9	

	+	π 83.74 ✓	-	Talbot St.		+	π 83.72 ✓	-	
N.L.			2.1			+5		10.15	
N.L. +10			1.5			+6		4.6	
0+25 N.L.-10'			2.9			N.L.		4.4	
N.L.			3.0			N.L. + 2		16.2	
+8			3.5			N.L. + 9		16.2	
cb			6.0			N.L. + 10		4.4	
+2			10.5			0+85 N.L.-15'		6.9	
1/2			10.0			N.L. - 14		17.9	
+2			3.2			N.L. - 5		17.9	
4			3.6			N.L.		6.5	
1/2			2.8			+6		6.3	
cb			3.5			cb		13.2	
S.L.			+0.8			+6		13.2	
0+50 S.L.			+0.5			+8		6.7	
cb			4.8			1/2		6.5	
1/2			4.1			4		6.4	
4			4.7			1/2		5.7	
1/2			4.8			cb		4.4	
+3			11.1			S.L.		2.0	
cb			11.1						

	+	π 83.74 \checkmark	-	Tarbot St.		+	π 83.74 \checkmark	-	
0+91 S.L.			2.0			+8		7.6	76.1
CB			4.2			1/2		7.6	76.2
1/2			5.6			±		7.2	76.4
±			6.8			1/2		5.0	78.2
1/2			7.1			cb		5.1	78.6
+2			12.9			S.L.		1.7	82.0
cb			13.0			6+07 ²⁵ S.L.		1.6	82.1
+8			6.8			cb		5.3	78.4
N.L.			18.6			1/2		5.7	78.0
N.L.+9			18.0			±		7.6	76.1
N.L.+10			6.7			1/2		7.8	75.9
N.L.+15			6.7			+3		8.0	75.7
6+02 ²⁸ = PC. of 25' Radius Curve into La Roy St (La Roy 50 Wide)						±	1.86	79.21	76.35 \checkmark
N.L.-10'			7.0	76.2		+5		8.4	69.8
N.L.-3			7.3	76.4		cb		13.4	64.8
N.L.-2			18.9	64.8		N.L.		13.4	64.8
N.L.			18.9	64.8		N.L.+1		2.1	76.1
+8			18.9	64.8		N.L.+10		2.6	75.6
CB			13.6	70.1					
+6			13.0	70.7					

Add 0.3' to these elev

Talbot St.

	+	78.21 ✓	-		+	78.21 ✓	-	
G+08 ²⁸ ML-10			2.6	75.6	2.5		15.1	63.1
N.L.			2.3	75.9	1/2		15.1	63.1
+1			13.4	64.8	+6		15.1	63.1
cb			13.4	64.8	cb		8.2	70.0
G+27 ²⁸ = W.L. of Le Roy (produced)					+3		4.4	73.8
N.L.			3.8	74.4	N.L.		4.4	73.8
+7			3.8	74.4	#	0.62	79.12 ✓	73.50 E. 7' back Le Roy
cb			14.7	63.3			+1.27	75.39
1/4			14.3	63.9			0.73	73.39
+2			3.6	74.6				
#			3.0	75.2				
1/2			1.0	76.6				
cb			1.0	77.2			7.4	66.7
S.L.			+2.9	81.0			11.0	63.1
West Curb Le Roy							11.0	63.1
S.L.			+2.8	81.0			11.0	63.1
cb.			15.1	77.1			0.0	74.1
1/4			1.9	76.3			+1.7	75.8
#			3.6	74.6			+2.9	77.0
+3			3.4	74.8			+6.7	80.1

Concrete Curb West side Le Roy 25' N.

" " East " " " " "

West 1/4 of Leroy St.

+ π 74.12 ✓			- Talbot St.			+ π 74.12 ✓			- East Curb of Leroy St.		
4 of Le Roy St											
S.L		+6.2	80.3		S.L		+5.9	80.0			
cb		+2.6	76.7		cb		+1.0	75.1			
1/2		+1.0	75.1		1/2		+0.2	74.3			
±		0.0	74.1		±		0.7	73.4			
+3		11.8	62.3		+4		2.5	73.6			
1/4		11.8	62.3		+5		12.7	61.4			
+5		11.8	62.3		1/2		12.7	61.4			
cb		5.0	69.1		+3		12.4	61.7			
+4		1.3	72.8		cb		2.6	71.5			
N.L		1.3	72.8		N.L		2.2	71.9			
E 1/4 of Le Roy St:					East Line of Le Roy St: (Produced)						
N.L		1.8	72.3		N.L		2.9	71.2			
cb		2.3	71.8		cb		3.4	70.7			
+4		12.3	61.8		+8		13.3	60.8			
1/4		12.3	61.8		1/2		13.3	60.8			
+4		12.3	61.8		+6		13.3	60.8			
±		0.0	74.1		+7		1.6	72.5			
1/4		+0.8	74.9		±		1.6	72.5			
cb		71.9	76.0		1/2		0.4	73.7			
S.L		+6.0	80.1								

Add 0.3' to these elev

	+	X 74.12 ✓	Talbot St.		+	X 74.12 ✓		28
				±			15.4	58.7
Cb		0.2	73.9	+3			15.4	58.7
S.L.		+4.5	79.6	1/4			8.8	65.3
2+02 ³³ = RC of 25' Radius curve on E side of Leroy St.				+2			5.0	69.1
S.L.		+1.0	75.1	Cb			4.0	70.1
Cb		1.7	72.4	S.L.			2.0	74.1
1/4		1.8	72.3	West curb of Spathic St				
±		3.8	70.3	S.L.			3.2	70.9
+3		10.2	63.8	Cb			5.2	68.9
+8		14.2	59.8	1/4			7.0	67.1
1/4		9.7	64.4	#	0.02	67.10 ✓	7.04	67.09 ✓
+2		5.4	68.7	+8			10.0	57.1
Cb		1.9	69.2	±			10.0	57.1
N.L.		5.2	68.4	+5			5.1	62.0
2+38 ⁹² West Line of Spathic St 75.03 wide on diagonal 12.00 Curbs 12.00				1/4			5.1	62.0
N.L.		7.9	66.2	+3			4.9	62.2
Cb		7.8	66.3	+5			1.6	65.5
+7		7.8	66.3	Cb			1.6	65.5
1/4		11.4	62.7	N.L.			1.9	65.2
+3		15.9	58.2	West 1/4 of Spathic St:				

	+	\bar{x} 67.10	-	Talbot St.
N.L.	W. 1/4 of Spathic		2.6	64.5
cb			2.4	64.7
+7			2.3	64.8
1/4			10.2	56.9
±			9.8	57.3
+8			1.5	65.6
1/4			1.3	65.8
cb			+0.2	67.3
S.L.			-2.0	69.6
± of Spathic St				
S.L.			+0.3	67.4
cb			1.2	65.9
1/4			2.5	64.6
+9			3.2	63.9
±			11.0	56.10
1/4			10.5	56.6
+2			10.0	56.6
+3			3.2	63.9
cb			3.1	64.0
N.L.			3.2	63.9

	+	\bar{x} 67.10	-	
				29
				E 1/2 of Spathic St.
				N.L.
			4.0	63.1
			4.2	62.9
			4.2	62.9
			11.5	55.6
			11.7	55.4
			9.7	57.4
			7.8	59.3
			4.1	63.0
			3.5	63.6
			2.9	64.2
			1.3	65.8
				E curb of Spathic St
			3.1	64.0
			3.7	63.4
			4.6	62.5
			5.0	62.1
			10.0	57.1
			12.1	55.0
			12.4	54.7

	+	π 67.10 ✓	-	Talbot St.		+	π 67.10 ✓	-		39
	+7		12.0	53.1		+5		13.2	53.8	✓
	+8		5.0	62.1		±		12.3	54.1 53.8	✓
	cb		5.0	62.1		+5		13.3	53.8	✓
	N.L		4.8	62.3		1/2		6.0	61.1	✓
	East line of Spathic = 00					cb		6.2	60.9	✓
	N.L		5.7	61.4 ✓		N.L		6.0	61.1	✓
	cb		6.0	61.1 ✓		0+20 N.L		8.0	59.1	✓
	+4		5.8	61.3 ✓		cb		8.0	59.1	✓
	+5		12.2	54.9 ✓		1/2		8.0	59.1	✓
	1/4		12.9	54.2 ✓		+8		8.0	59.1	✓
	±		13.2	54.2 53.9 ✓		±		14.8	52.6 57.3	✓
	±2		10.2	53.9 ✓		+7		14.8	57.3	✓
	+5		5.8	61.3 ✓		1/2		8.1	59.0	✓
	1/4		5.6	61.5 ✓		cb		7.5	59.6	✓
	cb		4.9	62.2 ✓		S.L		6.9	60.2	✓
	S.L		4.3	62.8 ✓		±	102	58.25 ✓	9.7	57.23 ✓
	0+02 S.L		4.6	62.5 ✓		0+623 = P.C. of 24' radius curve on Evergreen St.				
	cb		4.8	62.3 ✓		S.L		18	56.4	✓
	1/4		5.8	61.3 ✓		+9		1.2	57.0	✓
	+3		5.8	61.3 ✓		cb		2.0	49.2	✓

*Note: Add 0.3 to these Elevations
See Check Page 38 M.N.D.*

	+	π 58.25 ✓	-	Tarbot St.
+5			9.8	48.4 ✓
+6			1.6	56.6 ✓
1/2			1.3	56.9 ✓
E			1.7	56.5 ✓
1/4			1.8	56.4 ✓
cb			1.9	56.3 ✓
N.L.			1.5	56.7 ✓
0+88 ²⁸	= West Line of Evergreen St (60 wide 100 lbs 10' 9") produced			
N.L.			4.8	53.5 ✓
cb			4.6	53.7 ✓
1/2			4.1	54.2 ✓
E			3.8	54.5 ✓
1/4			2.8	55.5 ✓
+6			3.1	55.2 ✓
+7			11.9	46.4 ✓
cb			11.9	46.4 ✓
+4			11.9	46.4 ✓
+5			3.7	54.6 ✓
S.L.			3.7	54.6 ✓

Note: Add 0.3 to these elevations:
see check Page 38 M.N.D.

0+92²⁸ = West Cb of Evergreen St.

	+	π 58.25 ✓	-	
S.L.			4.7	53.6 ✓
+2			4.0	54.3 ✓
+5			13.6	44.7 ✓
cb			11.9	46.4 ✓
1/4			6.3	52.0 ✓
+5			4.0	54.3 ✓
E			4.7	53.6 ✓
1/2			5.0	53.3 ✓
cb			5.6	52.7 ✓
N.L.			6.4	51.9 ✓
			6.73	51.52 ✓
	On Concrete West curb of Evergreen 25' North of our N.L.			
	1+02 ²⁸ = West 1/2 of Evergreen:			
N.L.			6.5	51.8 ✓
cb			6.3	54.0 ✓
1/2			5.9	54.5 ✓
E			5.5	54.8 ✓
1/4			4.5	53.8 ✓
+4			10.4	47.9 ✓
cb			13.0	45.3 ✓
+6			13.7	44.6 ✓

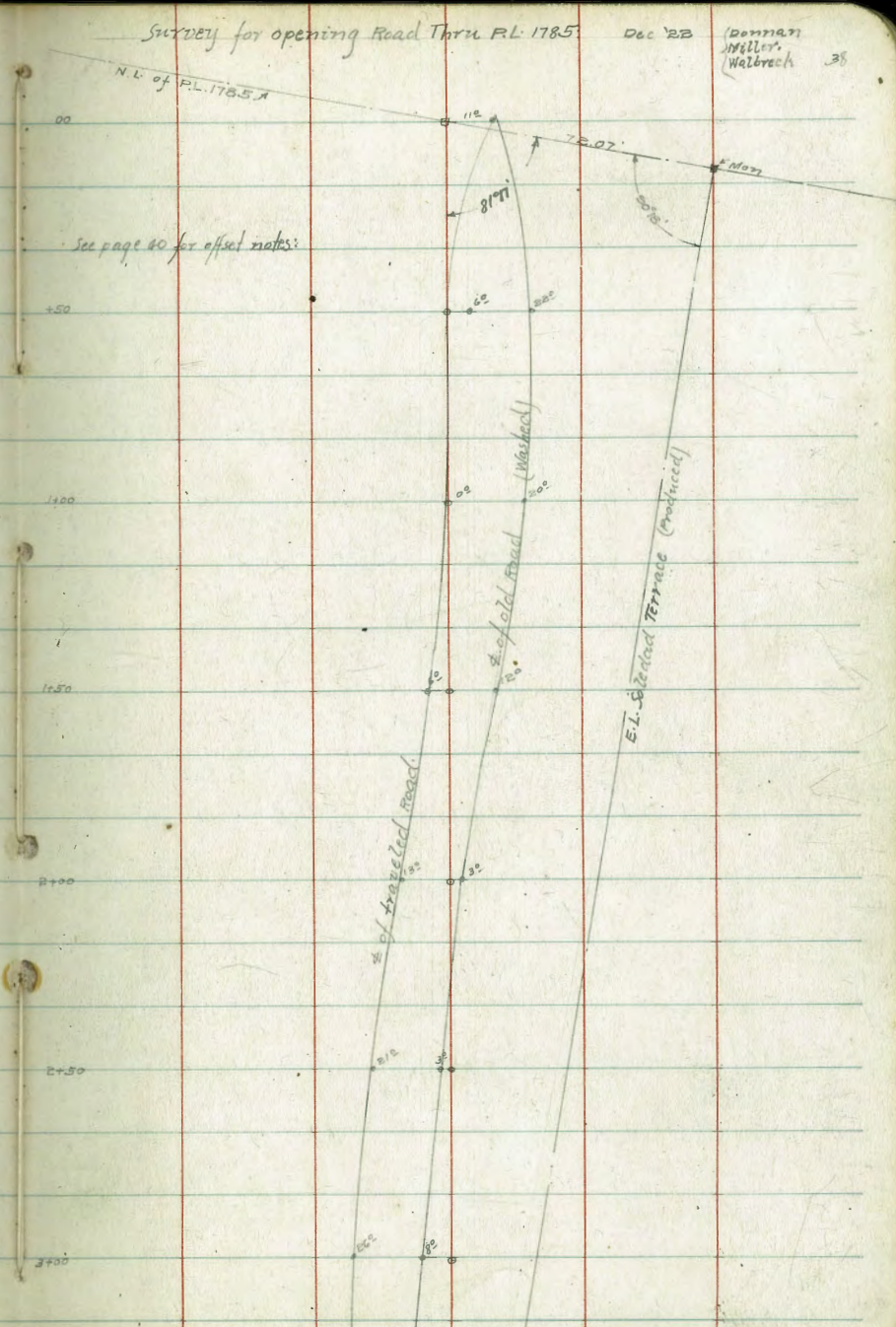
	+	58.25 ✓	-	Talbot St.		+	58.25 ✓	-	32
+8			4.2	54 .1 ✓	cb			14.5	43 .8 ✓
S.L.			4.3	54 .0 ✓	+6			15.0	43 .3 ✓
1+18 ²⁵ = E. of Evergreen St.					+7			6.4	52 .1 ✓
S.L.			5.3	53 .0 ✓	S.U.			6.6	51 .7 ✓
+V			5.0	53.3 ✓	1+38 ²⁵ = S. Curb of Evergreen St.				
+3			14.6	43 .7 ✓	S.L.			8.6	49 .7 ✓
cb			15.4	44 .9 ✓	+1.5			8.3	50 .0 ✓
+1			5.8	52 .5 ✓	+6			14.9	43 .5 ✓
1/4			5.2	53 .1 ✓	cb			14.8	43 .5 ✓
E			6.2	52 .1 ✓	+1			8.5	49 .8 ✓
1/4			6.9	51 .4 ✓	1/4			8.8	49 .5 ✓
cb			6.8	51 .5 ✓	E			8.9	49 .4 ✓
N.L.			7.1	51 .2 ✓	1/4			8.4	49 .9 ✓
1+28 ²⁵ = E. 1/4 of Evergreen St.					cb			8.2	50 .1 ✓
N.L.			7.7	50 .6 ✓	N.L.			8.8	49 .5 ✓
cb			7.5	50 .8 ✓	1+48 ²⁵ = E.L. of Evergreen St.				
1/4			7.7	50 .6 ✓	N.L.			9.9	48 .4 ✓
E			7.9	50 .4 ✓	+0			8.9	49 .4 ✓
1/4			7.2	51 .1 ✓	cb			9.0	49 .3 ✓
+9			6.9	51 .4 ✓	1/4			8.9	49 .4 ✓

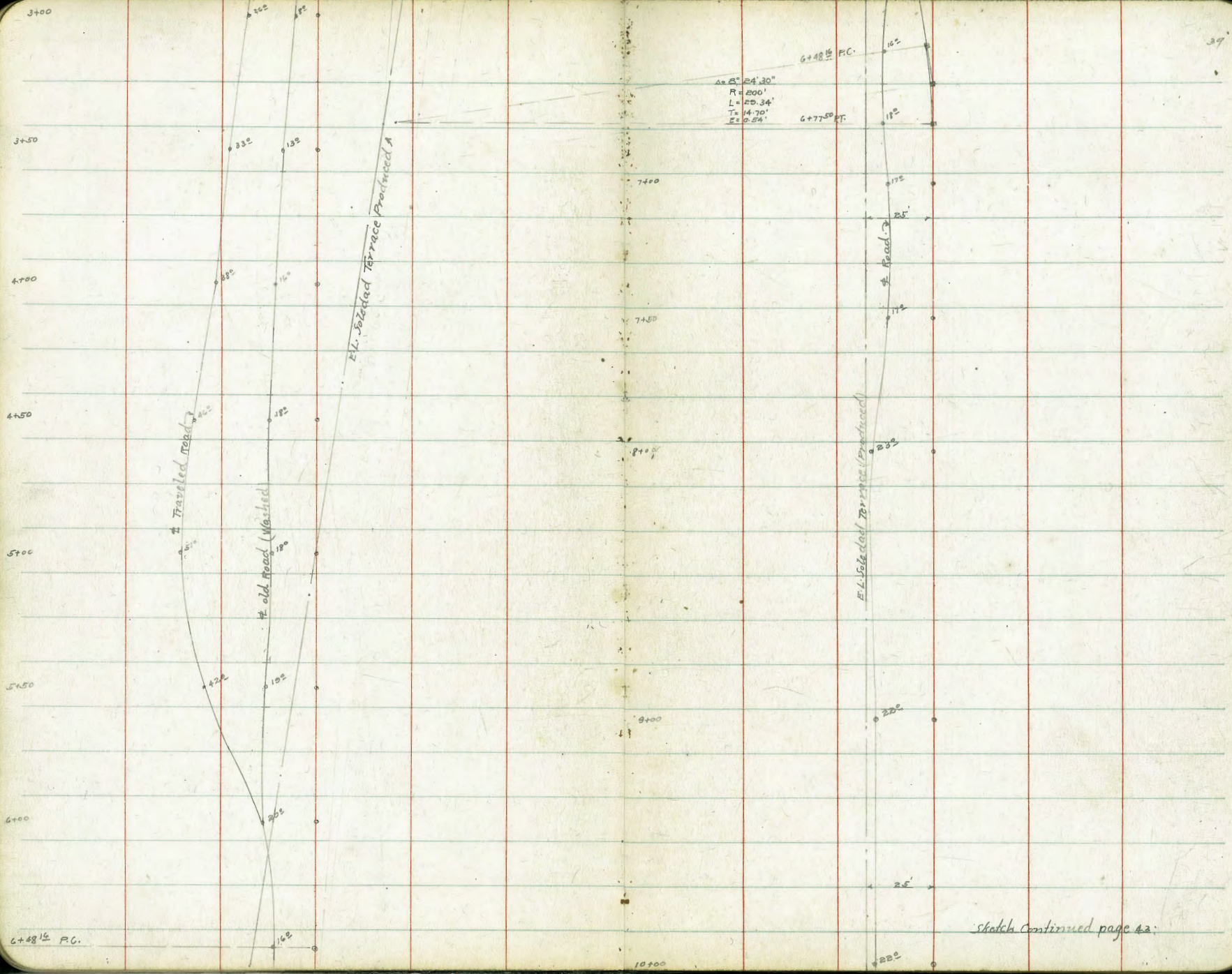
	+	π 58.25 ✓	-	Talbot St.		+	π 50.76 ✓	-	
±			9.6	48.7 ✓	1+90 Nil			5.0	45.8 ✓
1/4			9.6	48.7 ✓	cb			4.4	46.4 ✓
+8			9.4	48.9 ✓	1/4			4.4	46.4 ✓
cb			15.6	42.7 ✓	-5			4.3	46.5 ✓
+4			15.6	42.7 ✓	±			8.0	42.8 ✓
+5			9.4	48.9 ✓	+3			11.0	39.8 ✓
S.L.			9.4	48.9 ✓	+9			11.0	39.8 ✓
#	2.78	50.76 ✓	10.37	47.9 ✓	1/4			4.3	46.5 ✓
1+65 S.L.			2.7	48.1 ✓	cb			4.3	46.5 ✓
+1			2.6	48.2 ✓	S.L.			4.2	46.6 ✓
+2			8.7	42.1 ✓	2+00 S.L.			4.7	46.1 ✓
cb			8.5	42.3 ✓	cb			4.8	46.0 ✓
+3			8.5	42.3 ✓	+7			5.0	45.8 ✓
+4			3.5	47.3 ✓	+8			11.6	39.2 ✓
1/4			2.7	48.1 ✓	1/4			11.6	39.2 ✓
±			2.9	47.9 ✓	±			10.3	40.5 ✓
1/4			2.6	48.2 ✓	+9			7.4	43.4 ✓
cb			2.6	48.2 ✓	1/4			5.2	45.6 ✓
+6			2.7	48.1 ✓	cb			5.4	45.6 ✓
Nil			3.5	47.3 ✓	Nil			5.3	45.5 ✓

	+	π 43.83 ✓	Talbot St.		π 43.83 ✓		36
1/4			6.2 37.4 ✓			9.2 34.6 ✓	
+1			9.7 34.1 ✓		+7	9.1 34.7 ✓	
+5			9.7 34.1 ✓		+8	11.4 32.4 ✓	
+6			6.6 37.2 ✓		t	11.4 32.4 ✓	
t			6.0 37.8 ✓		+4	11.4 32.4 ✓	
1/4			5.8 38.0 ✓		1/4	9.5 34.3 ✓	
cb			6.2 37.6 ✓		cb	8.6 35.2 ✓	
N.L.			6.1 37.7 ✓		N.L.	8.8 35.0 ✓	
0+25 N.L.			7.6 36.2 ✓		0+75 N.L.	10.4 33.4 ✓	
cb			7.5 36.3 ✓		cb	10.4 33.4 ✓	
1/4			7.3 36.5 ✓		+5	10.3 33.5 ✓	
+9			7.9 35.9 ✓		1/4	13.3 30.5 ✓	
t			10.6 33.2 ✓		+4	13.3 30.5 ✓	
+7			10.6 33.2 ✓		t	10.5 33.3 ✓	
+9			8.0 35.8 ✓		1/4	10.6 33.2 ✓	
1/4			8.0 35.8 ✓		cb	10.2 33.6 ✓	
cb			7.3 36.5 ✓		S.L.	10.2 33.6 ✓	
S.L.			7.5 36.3 ✓		100 S.L.	11.6 32.2 ✓	
0+50 S.L.			8.7 35.1 ✓		cb	11.6 32.2 ✓	
cb			8.8 35.0 ✓		1/4	11.9 31.9 ✓	

	+	π 43.83 ✓	-	Talbot St.		+	π 31.85 ✓	-		37
\pm			12.2	31.6 ✓	$\frac{1}{8}$			2.9	29.0 ✓	
+6			10.9	29.9 ✓	\pm			2.2	29.7 ✓	
$\frac{1}{4}$			12.9	30.9 ✓	49			2.0	29.9 ✓	
cb			11.6	30.2 ✓	$\frac{1}{6}$			3.6	28.3 ✓	
N.W			11.8	30.0 ✓	+7			3.6	28.3 ✓	
#	0.63	31.80 ✓	12.61	31.22 ✓	+9			1.9	30.1 ✓	
1+20 N.W			1.0	30.9 ✓	cb			2.3	29.6 ✓	
cb			0.9	30.0 ✓	N.W			2.3	29.6 ✓	
+3			0.8	31.1 ✓	2+00 N.W			4.8	27.1 ✓	
+2			2.7	29.2 ✓	cb			4.5	27.4 ✓	
$\frac{1}{4}$			3.2	28.7 ✓	+5			5.9	26.0 ✓	
+5			2.3	29.6 ✓	+9			5.9	26.0 ✓	
+6			1.2	30.7 ✓	$\frac{1}{4}$			4.9	27.0 ✓	
\pm			1.2	30.7 ✓	\pm			4.7	27.2 ✓	
$\frac{1}{6}$			1.3	30.6 ✓	$\frac{1}{4}$			5.7	26.2 ✓	
cb			0.7	31.2 ✓	cb			5.9	26.0 ✓	
S.W			0.8	31.1 ✓	+7			6.1	25.8 ✓	
1+50 S.W			2.2	29.7 ✓	S.W			4.8	27.1 ✓	
+2			2.8	29.1 ✓	2+50 S.W			8.0	23.9 ✓	
cb			2.9	29.0 ✓	cb			8.1	23.8 ✓	

	π 31.85		Talbot St.	
1/4		7.1	24.8	✓
1/2		6.4	25.5	✓
3/4		6.6	25.3	✓
+1		8.1	23.8	✓
+2		8.1	23.8	✓
+6		6.7	25.2	✓
cb		6.8	25.1	✓
N.L.		7.1	24.8	✓
N.L. 2+50 S.L. = Appe 2+85' N.L. Section on N.L. Rosecrans St.				
cb		8.8	23.1	✓
1/4		8.8	23.1	✓
1/2	5+75 =	8.8	23.1	✓
3/4		7.8	24.1	✓
cb		8.2	23.7	✓
S.L.		8.0	23.9	✓
	1.36	24.23	8.98	22.87 Hub Cox Rosecrans & Talbot
#		3.85	20.38 = 20.67	BM Canyon Road E. Rosecrans



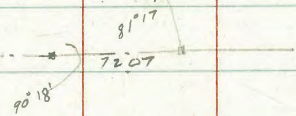


Sketch Continued page 42

offsets to traveled road PL 1785; (Note plotted on sketch)

40

Sta	Off	N.			
				10	22 R.
00			10 L	11	22 R.
+50	20 L	6 L		12	20 R.
100	20 L	0.0		12	17 R.
1+50	12 L	6 R.		14	14 R.
2	3 L	13 R.		15	12 R.
+50	2 R	21 R.		16	12 R.
3	8 R	26 R.		+50	10 R.
+50	12 R.	23 R		17	7 R.
4	16 R	38 R		+60	6 R.
+50	18 R.	46 R.		18	4 R.
5	18 R.	51 R		19	6 R. = N. End x'd bridge
+50	19 R.	42 R		+47	6 R = S " " "
6	20' R	20' R		19+85 ³⁴ = PC	6 R.
6+48 ¹⁶ RC.		16 R.		C.C.	2 R.
6+77 ⁵⁰ RT		18 R		20+40 ⁹⁰ PT	4 L.
7		17 R.		20+83 ⁶⁶ RC	7 L.
+50		17 R.		C.C.	11 L.
8		23 R.		22+39 ⁸³ = P.C.	0.0
9		22 R.		C.C.	8 L.
				23+25 ⁸² RT.	40 L.



	+	+	-	Dec 1922	Deming, Miller, Waterbach	+	+	-	
Levels for sidewalk									
Thru Rt 59 La Jolla:									
	1.02	106.06	106.1	105.09	Tranholer Prospect:	2+20		2.9	53.5
On W. Curb of Prospect St.			4.54	101.52		2+20		8.3	48.1
Opp. W.L. Prospect St.			4.3	101.8		2+62 = top step of flight of five stairs:		10.2	46.1
0+25			5.2	100.9		#	2.10	45.78	43.68
0+30			6.7	99.2		2+72 = bottom stairs:		41.8	43.3
0+75			8.4	97.2		2+74 Concrete on Rt to house:		2.62	43.15
#	0.60	92.00	12.66	93.20		2+90 " " " "		3.34	42.44
1+00			94.0	90.9		2+00 Opp. Center of concrete floor		3.65	42.15
1+25			8.1	90.9		2+10		4.4	41.4
#	0.15	81.20	7.6	86.5		2+25		4.9	40.9
1+47 Little wooden landing Rt			12.95	81.05		2+23 top Concrete Step Note steps at:		6.40	39.35
1+50			81.7	79.1		2+51 P.L. bottom of steps:		8.88	36.90
1+75			2.1	79.1		On Curb:		9.19	35.59
#	0.67	68.99	4.2	77.0		#		49.09	36.03
1+92 Cement landing from house Rt			11.7	69.3					
1+90			12.88	68.32					
2+00			63.0	64.0					
#	0.39	56.42	5.0	64.0					
2+19 Concrete walk to house Rt.			8.6	60.4					
			12.95	56.04					
			56.4	55.4					

10+00

822

Sketch from page 39

13+10.5

Gas pipe

43

816'

11+00

822

14+00

8142

12+00

820

15+00

8121

E.L. Salcedo Terrace: Production

Present Road

825

8172

13+00

13+15.46

Gas pipe shown N.E. Cor Salcedo Terrace Sub

16+00

18+50

E.L. Salcedo Terrace

Present Road

8123

8105

11 17+00

10 17+50

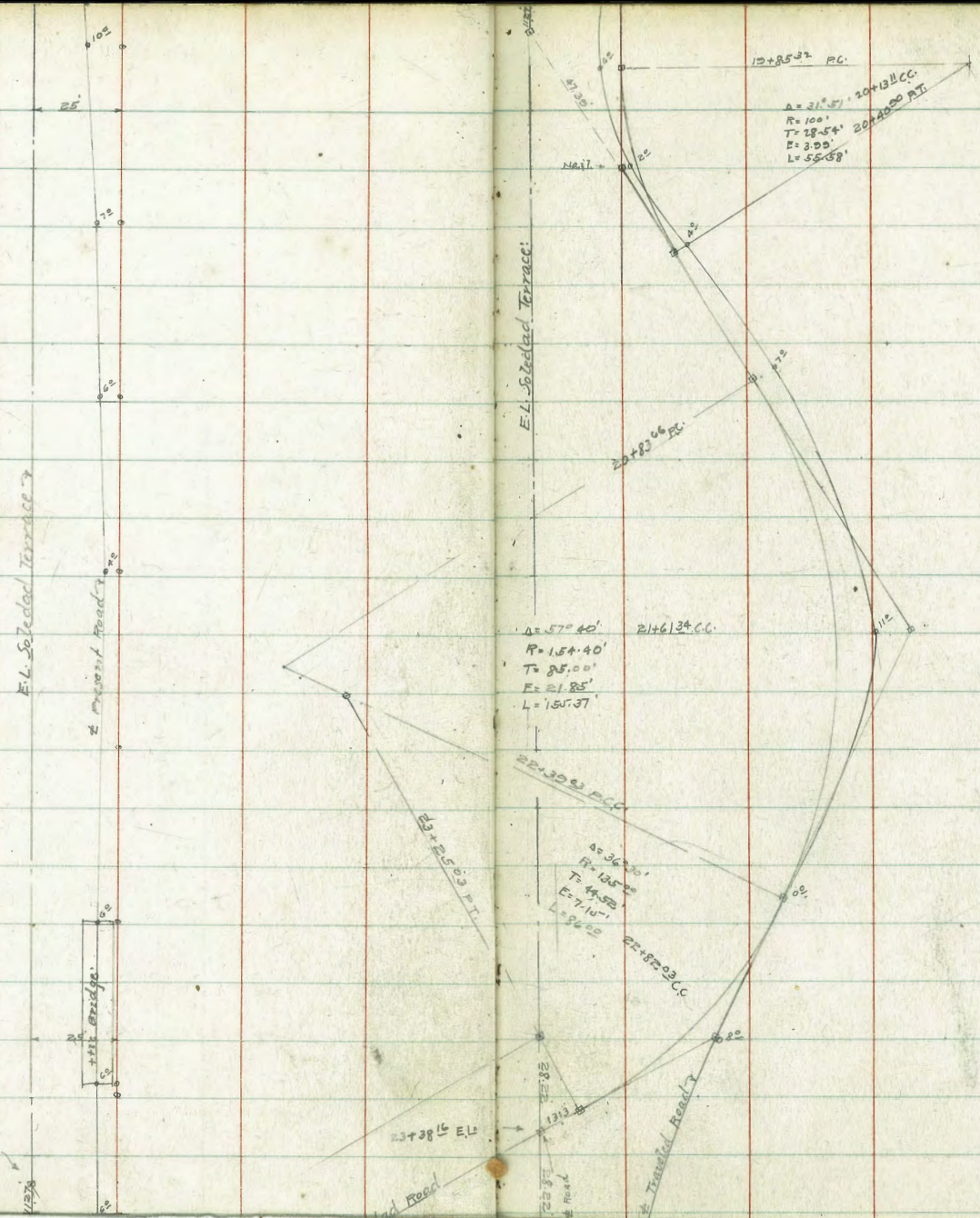
9 18+50

8 19+00

7 19+47

6 19+50

5 SE-Cor Lot 24 Siedad Terrace



15+85.37 P.C.
 $\Delta = 21^{\circ} 37'$
 $R = 100'$
 $T = 28.54'$
 $E = 3.88'$
 $L = 55.58'$
 20+131.66
 20+130.00 P.T.

$\Delta = 57^{\circ} 40'$
 $R = 154.40'$
 $T = 85.00'$
 $E = 21.85'$
 $L = 150.37'$
 21+6134.66

$\Delta = 36^{\circ} 20'$
 $R = 105.72'$
 $T = 49.52'$
 $E = 7.10'$
 $L = 96.65'$
 22+398.82 P.C.
 22+872.66

23+381.6 E.L.

1/23/23

Gregory & Levels in Alley Bet. 33rd
Thayer
Walker
Shaw
and Felton from St. of Redwood
to N.W. of Nutmeg

					+50	23+27.8	313.46	8.2	305.3	
BM	1.85	313.46	311.61	NW cor Redwood 33 rd	8	+77.8		10.3	303.7	
	15+77.8									
0+00 = S.L. Redwood			1.0	317.5	+50	24+27.8		13.0	300.5	
+50	16+27.8		1.7	311.8	T.P.	1.02	301.77	12.71	300.75	
1	+77.8		2.2	311.3	9	+77.8		3.7	298.1	
+50	17+27.8		2.9	310.6	+50	25+27.8		6.5	295.3	70' west is Elev. 299.3
2	+77.8		4.6	308.9	+75	25+52.8		8.3	293.5	
+50	18+02.8		5.4	308.1	10	25+77.8		11.0	290.8	65' west is Elev. 285.3
+50	+27.8		5.7	307.8	T.P.	0.42	289.28	12.91	288.86	
3	+77.8		6.2	307.3	+50	26+27.8		4.0	285.3	65' west is Elev. 281.3
+50	19+27.8		6.1	307.4	11	26+77.8		9.4	279.9	
+65	19+42.8		6.5	307.0	+35	27+12.8		12.3	277.0	
4	+77.8		5.8	307.7	T.P.	0.22	277.17	12.33	276.95	
+50	20+27.8		5.2	308.3	+50	+27.8		2.4	274.8	
5	+77.8		5.0	308.5	+75	+52.8		6.0	271.2	
+50	21+27.8		4.9	308.6	+93	+70.8		11.7	265.5	
+98.6 = N.L. Palm	21+76.4		5.4	308.1	12	+77.8		11.7	265.5	
6+28.6 =	22+06.4		5.8	307.7	+18	+95.8		14.4	262.8	
+58.6 = S.L.	22+36.4		6.0	307.5	+29	28+06.8		8.0	269.2	
7	22+77.8		7.1	306.4	+53.96 = N.L. Nutmeg	28+31.75		5.6	271.6	
					T.P.	13.05	269.28	0.14	271.43	
					T.P.	12.82	301.94	0.36	269.12	
								9.51	262.43	Hub NE Nut +38

Planted
11/29/23
2183

1/23/23

Gregory & Levels on Alley bet 33rd + Bancroft from NL Nutmeg to SL Palm.

	9.51	301.91		292.40	
0+00 = NL Nutmeg	12+53 ⁵⁶		1.5	300.4	
+50	12+02 ⁵⁶		3.0	298.9	
1	11+53 ⁵⁶		5.0	296.9	
+50	11+03 ⁵⁶		5.2	296.7	
2	10+53 ⁵⁶		3.8	298.1	
+50	10+03 ⁵⁶		2.1	299.8	
3	9+53 ⁵⁶		0.0	301.9	
T.P.	13.25	315.15	0.01	301.90	
+50	9+03 ⁵⁶		11.0	304.7	
4	8+53 ⁵⁶		10.3	304.9	
+50	8+03 ⁵⁶		10.3	304.9	
5	7+53 ⁵⁶		10.4	304.8	
+50	7+03 ⁵⁶		10.2	305.0	
	6+53 ⁵⁶				
+94.96 = SL Palm	6+28 ⁵⁶		9.4	305.8	
6 + 24.96 = 2 ✓			9.6	305.6	
6 + 50	6+03 ⁵⁶		9.5	305.7	
7	5+53 ⁵⁶		9.5	305.7	
+75	5+28 ⁵⁶		9.4	305.8	

✓

3/5/5

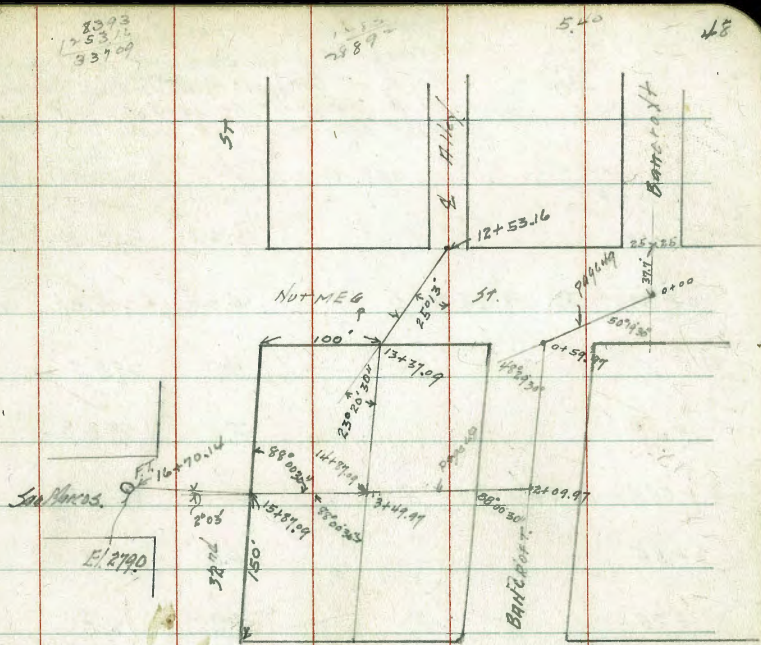
46

	+50	5+03 ⁵⁶	8.8	306.4	
		Hub NE Nutmeg +33			
	+75	4+78 ⁵⁶	8.8	306.4	
	8	4+53 ⁵⁶	8.2	307.0	
	+50	4+03 ⁵⁶	7.7	307.5	
	+75	3+78 ⁵⁶	6.8	308.4	
	9	3+53 ⁵⁶	6.7	308.5	
	+30	3+28 ⁵⁶	6.6	308.6	
	+50	3+03 ⁵⁶	5.8	309.4	
	10	2+53 ⁵⁶	5.0	310.7	
	+50	2+03 ⁵⁶	4.1	311.1	
	11	1+53 ⁵⁶	3.1	317.1	
	+50	1+03 ⁵⁶	1.8	313.4	
	12	0+53 ⁵⁶	1.2	314.0	
		00			
	+53.56	SL Redwood	0.8	314.4	

Platted
1/30/23
2/23

1/23/23	Gregory Morse Miller Shaw	Levels on Alley bet 32nd + Bancroft from 5L Redwood to NL Nutmeg	see sketch page 48			315.18					
				BP NW	8			11.9	303.3		
		3.57	315.18	Redwood 33rd	+50			13.1	302.1		
		0+00 = 5L Redwood	5.7	70' West 13 4' lower	T.P.	0.75	302.97	12.96	302.22		
		+50	5.7	70' West 13 4' lower	9			2.2	300.8		
1			5.6	70' West is 11.4' lower	+50			3.6	299.4		70' west is 2.6 lower
		+50	6.0	70' West is 3.8 lower	10			5.3	297.7		70' west is 2.7 lower
2			6.3		+50			7.4	295.6		70' west is 3.1 lower 60' East is level
		+50	6.9		11			9.0	294.0		90' - 15.7' lower Bottom of draw 80' East is 45' - 15.07' ✓ 50' West is 4.4 ✓ 50' West is 5.2 ✓
3			7.2		+50			10.9	292.1		30' East is level 45' - 12.23' lower Bottom of draw
		+50	7.7		T.P.	1.49	292.78	11.68	291.29		Bottom of draw 70' E is 9.6' lower 35' - 10.0' lower 35' W is 4.1 ✓
4			8.4		12			3.0	289.8		
		+45	8.0		+45			5.8	287.0		
		+50	8.6		+53.16 = NL Nutmeg 225' 3" R			9.28	283.5		45' E is 2.2 lower 40' - 15.53' - Bottom draw
5			8.7		T.P.	0.96	289.88	(3.86)	288.92		
		+50	9.0		+60			8.30	281.6		
		+98.6 = NL Palm	9.3		+71			13.6	276.3		
6		+28.6 = 2 ✓	9.5		+76			16.3	273.6		
		+50	9.8		+87			16.4	273.5		
7			10.1		+95			14.8	275.1		
		+50	10.8		+96			13.7	276.2		

	289.88		
13+10	9.8	280.1	
13+27	6.1	283.8	
13+37.09	10.11 A 23°20'30" L 296.03	3.96	285.92 on stub
+50	7.6	288.4	
+70	5.9	290.1	
14	6.1	289.9	
+25	5.9	290.1	
+60	5.5	290.5	
+87.09	A 88°00'30" R	5.25	290.78 on stub
15	5.4	290.6	
+15	5.5	290.5	
+50	7.4	288.6	
+87.09	A 2°30' R	8.50	287.53 on stub
16	8.9	287.1	
+07.0	8.6	287.4	
+10.0	11.2	284.8	
+40	11.10	284.93	
+70.14	F.T.	11.04	284.99 Top of Core
		16.44	279.59 Bottom of cement pit



8303
5316
33709
2889
5.40
48

2/10/23
Gregory
Miller
Shaw

Sewer Levels from 6' of
Nutmeg rd 6' of Bancroft in Carmel Heights
to 6' of Bancroft S. of Nutmeg thence
on 6' Bancroft to 150 S. of
West thru the Block to 100' W. of Bancroft

	7.63	298.41	(5.25)	290.78	stub at
6' of Nutmeg & 6' of Bancroft N. of Nutmeg = 0+00			4.6	293.8	6' Bancroft N. of Nutmeg on stub
			3.28	291.13	
0+59.97 Δ 48°29'30" L			5.20	293.21	on stub
1			4.7	293.7	
+50			5.0	293.4	
2+09.97 Δ 88°00'20" R			5.18	293.23	
+35			4.6	293.8	
+75			5.9	292.5	
3			6.4	292.0	
+25			6.6	291.8	
+49.97 = 14+87.09 page 48	7.63	290.78			on stub

8/13/23

Property
a party.

Sewer Construction for
CARMEL HEIGHTS

M.H. 47 16+101 page 48
146
300 sketch for location page 48
29523 290.78 516 of 14579

20+20			10.11	285.12	279.59	+ 5.53
+ 50			10.69	284.54	280.81	+ 3.73
+ 13.05 Δ	2'03" L		7.50	287.73	281.62	+ 6.11
1			7.20	288.03	282.04	+ 5.99
+ 50			4.93	290.30	283.26	+ 7.04
V			3.47	291.76	284.48	+ 7.28
+ 50			2.68	292.55	285.71	+ 6.84
TP	5.74	299.80	1.17	294.06		
3			6.05	293.75	286.93	+ 6.82
+ 23.05 Δ	88°00'30"	M.H. 47	6.51	293.29	287.5	+ 5.79
+ 50			6.28	293.52	287.68	5.84
4			6.47	293.33	288.01	5.32
+ 50			6.47	293.33	288.34	+ 4.99
+ 73.05 Δ	48°29'30"	P.M.H.	6.85	292.95	288.5	4.45
5+33.02 Δ	50°19'30"	M=6.40	5.95	294.05	289.0	5.05
6			4.73	295.07	290.31	+ 4.76
+ 50			4.50	295.30	291.88	+ 4.02
7			3.75	296.05	292.26	+ 3.79
+ 50			4.54	297.26	293.83	+ 4.03
8	9.39	308.26	0.93	298.87	294.22	+ 4.65

1670.14
1487.00
1592.9
1830.5
4930.1
5997
13302
3499
1230.1
1230.2

+65.52 M.H.	7.05	301.21	295.5	+5.71	310.41	497
9	5.91	302.35	295.76	+6.59	305.44	461
+50	4.87	303.39	296.14	+7.25	310.05	
10	4.41	303.85	296.52	+7.33		
+50	4.55	303.71	296.90	+6.81		
11	3.54	304.42	297.28	+7.14		
+50	4.61	310.05	297.66	+6.97		
+95.58 M.H. to Palm st. $\Delta 90^{\circ}00'R$.	7.82	305.44	298.0	+7.44		
12+50	4.90	305.15	298.31	+6.84		
13	4.52	305.53	298.59	+6.94		
+450V M.H. to Alley. $\Delta 33^{\circ}$ + Bancroft.	4.39	305.66	298.83	+6.83		
14	4.30	305.75	299.15	+6.60		
+50	3.63	306.42	299.43	+6.99		
15	3.12	306.93	299.70	+7.23		
+50	2.65	307.40	299.98	+7.42		
16	2.34	307.71	300.15	+7.46		
+450V = M.H. to Alley $\Delta 90^{\circ}00' L$ 312.47 $\Delta 33^{\circ}$ + Palton	2.23	307.82	300.5	+7.32		
17	11.53	300.94	300.94	10.50		
+50	11.13	301.32	301.0	11.0		
18	10.12	301.76	301.76			

5.16
2.780
2.250
20.58

4.1
2.780
2.250
2.1

806
50
4000

25802
3325
8652
330

19552
1470
131502

+ 50

10.32

Feb

302.15

800

19

9.91

302.56

51
4-20
4-30

+ 55.00 M.H.

9.47

303.0

out 0.50

119
41
595
120
5345

20

8.93

303.54

+ 50

8.34

304.13

Top stakes from here

21

7.52

309.95

1.19

304.73

+ 5.22

+ 50

1.12

311.35

305.32

+ 6.08

22

0.67

311.80

305.92

+ 5.48

+ 50.00 DE = 236.5 at 56 Redwood

0.39

312.08

306.5

+ 5.54

8/19/23 Gentry

Sewer Construction & Alley bet 33rd Felton from & Palm St to 140' S.

MH 16 + 45.00 page 51

20+00	288	310.90	307.82	300.5	
+50			3.84	306.86	200.85 +6.01
1			4.80	305.90	301.21 +4.69
+40 DE			6.15	304.55	301.5 +3.05

300.2

254

678

Sewer Construction & Alley bet.

33rd + Bancroft from & Palm to 605' N.

Drop MH 15 + 45.00 page 51

20+00		310.05	4.39	305.66	300.00
+50		312.50		1223	300.57
1				1147	301.13
+50				11.11	301.69
2				10.54	302.46
+50				9.88	302.82
3 + 10 M.H.				9.30	303.5
+50				8.69	304.11
4				7.93	304.89
+50				7.16	305.64

152
200
6120

cut 0.25

cut 0.50

cut 0.50

3/2.80

31251
 526
 30273
 568
 31241
 6.7 0.50

54

5		6.40	30640	
+50		5.64	307.16	
6	H. Stakeset	4.77	307.93	
+05 = DE	236.5 of SL Redwood	4.80	308.0	cut 0.50

Inner Construction to Palm 9th of May

bet 3rd & Bancroft. from & Bancroft

M.H. 11495.54

319.41

20400		4.97	30544	298.0	+7.44
+50		4.92	30549	298.33	+7.16
1		4.89	305.52	298.67	+6.85
+50.5 M.H. 90°00R		4.70	305.71	299.0	+6.71
2		11.04	299.29		
+50		10.83	299.56		679
3		12.04	299.87		5.79 60 32940
+50		12.43	300.16		
4		12.84	300.45		
+60.5 M.H.		11.80	300.79		
5		11.56	301.03		
+50		11.27	301.32		
6		10.98	301.61		

312.59

+50

Bottoms

12.68

301.20

311.61 BP NW 33rd Redwood

~~6.95~~
318.56
~~7.66~~
310.90
~~2.67~~
313.57

~~5.51~~
~~2.90~~
~~2.20~~

55

7

12.39

302.20

+55.5 DE 736 S. 1 SL Redwood

-10.09

302.5

Grades in Alley Brooks to Penn Bet 4th 45th 9/13/20

mills
C.W.
M.L.

B.M.		W	E		B.M. 283.32 NW 4 th - Brooks
	4:30 = 4.50 Paving			4:48 = 6.3	3.19
00 = S. Line Penn	4:47 ^{4.19} / ₊₁₀	284.09	283.91	5.71.0 ^{shoring}	286.51
+25	4:47	284.00	283.82	4.65	4.38
0	+50			00	282.13
	4.64	283.92	283.74		5.00
				4.82	287.13
1+00	00	283.75	283.57	00	4.22
	4.80			4.98	282.91
+50	00	283.59	283.41	6.18	5.44
	3.61			-1.21	288.37
	00			5.85	
2+00	3.87	283.42	283.24	00	
	00			4.05	
+50	4.04	283.26	283.08	00	0.04
				4.22	4.09
3+00	00	283.09	282.91	00	
	4.21			4.39	
+50	00	282.92	282.74	00	
	4.38			4.56	
4+00	00	282.75	282.57	6.99	
	4.54			-2.43	
+50	+10	282.59	282.41	4.72	
	4.71			+1.0	
5+00	+10	282.42	282.24	4.89	
	4.25			+1.0	
+50	+10	282.26	282.08	5.05	
	4.42			4.15	
N. Line Brooks +00		282.09	281.91	4.78	
				4.60	

Grades in Alley Brooks to Penn Bet 3rd & 4th 9/13/23

mill.
C.W.
mil

		W	E		
	4.97 on paving			4.80 on paving	285.36
00-S line Penn		282.83	282.90		3.70
	5.02			4.71	285.86
+50	+1.0	282.68	282.79	21.0	5.69
	5.17			5.01	282.97
+100	+1.0	282.53	282.69	+1.0	4.72
	5.30			5.30	287.70
+40	+1.0	282.40	282.6	+1.0	6.02
	5.90			5.70	281.12
2+00	00	281.80	282.0	+0.05	4.43
	6.40			6.20	285.55
+50	+1.0	281.80	281.80	+1.0	
+80	4.55 +1.0	281.00	281.2	4.35 +1.0	
3+00	4.59	281.96	281.16	4.39	
	+1.0			+1.0	
+50	4.70	280.05	281.05	4.50	
	0.0			4.45	
	4.01			+0.05	
4+00	+1.0	280.74	280.94	4.61	
	4.92			+1.0	
+50	00	280.63	280.83	4.72	
	5.03			00	
5+00	4.87	280.52	280.72	4.83	
	+0.16			+1.0	
	5.12			4.94	
+50	+1.0	280.41	280.41	+1.0	
	5.25			5.05	
N. Line of Brooks 6+00	1.00	280.30	280.50	00	

E.M.N.W. 4th & Brooks

285.55
277.6
7.95
5.39
+ 2.56 sewer let #4

Grades on Palm Est 32nd and Falton

	S. Line	S. Ch.	N. Ch.	N. Line									
E. Line 32 nd	= 00	303.75	303.5	304.0	304.25	31125 40	S	375	395	415	435	455	475
						320 308.08 320 311.28		75 47 +2.8	73 51 +2.2	71 57 +1.4	69 61 +0.8	67 62 +0.5	65 62 +0.3
	+50	303.95	303.7	304.2	304.45	31067 308.91 523 308.44 308.44							
	+100	304.15	303.9	304.4	304.65	308 304.77 304.54 391 414 437 441 408 421 403 -010 406 406 090 Bond	N	421 70 63 +0.7	446 68 52 +1.0	465 66 52 +1.3	485 64 52 +1.2	505 62 50 +1.2	
	+150	304.35	304.1	304.6	304.85		S	475	495	515	535	555	575
	+200	304.55	304.3	304.8	305.05		S	65	63	61	59	57	55
W. Line Barecroft 2+50		304.75	304.5	305.0	305.25	3045 3043 441 461 407 430 424 401 -009	S	65 63 +0.2	63 60 +0.3	61 59 +0.2	59 57 -0.2	57 55 -0.2	55 53 -0.2
E. Line Barecroft 00		304.75	304.5	305.0	305.25	30475 30472 30446 418 419 442 381 344 422 402 404 419	N		545	565	585	605	625
	+50	304.95	304.7	305.2	305.45			58 61 -0.3	56 61 -0.5	54 57 +0.2	52 50 +0.2	50 46 +0.4	48
	+100	305.15	304.9	305.4	305.65	S 3041 3039 481 461 460 451 402 404	S	625	645	665	685	705	725
	+150	305.35	305.1	305.6	305.85		N	50 49 +0.1	48 44 +0.4	46 42 +0.2	45 42 +0.2	47 44 +0.4	51 49 +0.2
	+200	305.55	305.3	305.8	306.05	N 30423 3040 465 491 451 475 407 404	N	675	715	755	80	745	685
W. Line 33 rd	+50	305.75	305.5	306.0	306.25	S 3037 3035 481 461 461 440	S	45 37 +0.8	41 32 +0.9	37 30 +0.5	33 32 +0.1	30 28 +0.8	28 26 +1.0
E. Line 33 rd	00	306.25	306.0	306.5	306.75		N	675	715	755	80	745	685
	+50	306.45	306.2	306.9	307.15		S	575	575	575	575	575	575
	+100	306.65	306.4	307.3	307.55		N	55 49 +0.8	52 46 +0.1	50 44 +0.2	48 42 +0.2	46 40 +0.1	44 38 +0.1
	+150	306.75	306.5	307.5	308.0	308.34 7.33 31061	S	575	575	575	575	575	575
	+200	306.85	306.6	307.6	308.1		N	575	575	575	575	575	575
	+250	306.95	306.7	307.8	308.3		S	575	575	575	575	575	575
	+300	307.05	306.8	308.0	308.5		N	575	575	575	575	575	575
W. Line Falton 2+50		305.75	305.5	306.0	306.25		S	575	575	575	575	575	575
E. Line Falton		305.75	305.5	306.0	306.25		S	575	575	575	575	575	575

Grades on Banerott Bay Redwood and Palm

S Line	W.H.C.	W.C.B.	E.C.B.	E Line										
Redwood = 00	314.25	314.0	314.5	314.75	315.57 HI	W	313.75	313.25	312.2	311.5	310.10	309.25	308	
					7.85 307.72 356 311.88		1.8 1.8 +0.7	2.8 1.8 +0.5	3.8 4.2 +0.4	4.8 5.8 +0.1	5.8 6.6 -0.1	6.8 7.1 -0.1	7.6 7.1 +0.5	
+50	313.75	313.5	314.0	314.25										
1400	313.25	313.0	313.5	313.75	311.61 BM 334 F	E	312.25	313.75	312.5	311.05	310.15	309.25	307.7	
					7.17 318.78 9.94 308.82 2.99 311.81		1.8 1.8 +0.5	1.8 1.8 +0.5	2.8 2.8 +0.7	3.8 4.2 +0.7	4.8 5.8 +0.2	5.8 6.6 +0.4	6.8 7.1 +0.6	
+50	312.20	311.95	312.3	312.55										
2400	311.15	310.9	311.1	311.35		W	307.4	306.85	306.35	305.80	305.25			315.0 3.78
							8.1 7.9 +0.2	4.4 5.6 +0.5	4.9 4.0 +0.9	5.8 4.4 +1.1	6.0 4.8 +0.7			
+50	310.10	309.85	309.9	310.15										
3400	309.05	308.8	308.7	308.95		E	307.2	306.7	306.2	305.7	305.25			
							8.3 7.9 +0.4	4.5 4.1 +0.4	5.0 4.2 +0.8	5.5 5.1 +0.4	6.0 5.5 +0.5			
+50	308.0	307.75	307.8	307.75										
4400	307.45	307.20	307.0	307.25		W	314.0	313.5	313.0	311.95	310.90	309.85		
							4.78 4.98 +0.68 0.15	5.28 5.08 +0.28	5.78 5.37 +0.41	6.28 6.45 +0.38	7.28 7.68 +0.20	8.28 8.93 0.0		
+50	306.90	306.65	306.5	306.75										
5400	306.35	306.10	306.0	306.25		E	314.5	314.0	313.5	312.3	311.1	309.9		
							4.28 4.36 +0.18 0.04	4.78 4.45 +0.33	5.28 5.33 -0.05	6.48 6.48 0.0	7.68 7.27 +0.41	8.88 8.50 +0.38		
+50	305.80	305.55	305.5	305.75										
6400	305.25	305.0	305.0	305.25		W	309.8	307.75	307.2	306.65	306.10	305.55	305.0	
							9.98 9.94 +0.02	4.06 3.65 +0.41	4.61 4.48 +0.20	5.16 5.03 +0.13	5.71 5.46 +0.25	6.26 5.94 +0.32	6.81	
+50														
7400						E	308.7	307.5	307.0	306.5	306.0	305.5	305.0	
							10.08 9.80 +0.28	4.31 3.88 +0.43	4.81 4.67 -0.14	5.31 5.07 +0.24	5.81 5.74 +0.47	6.31 5.97 +0.34	6.81 6.54 +0.23	
+50														

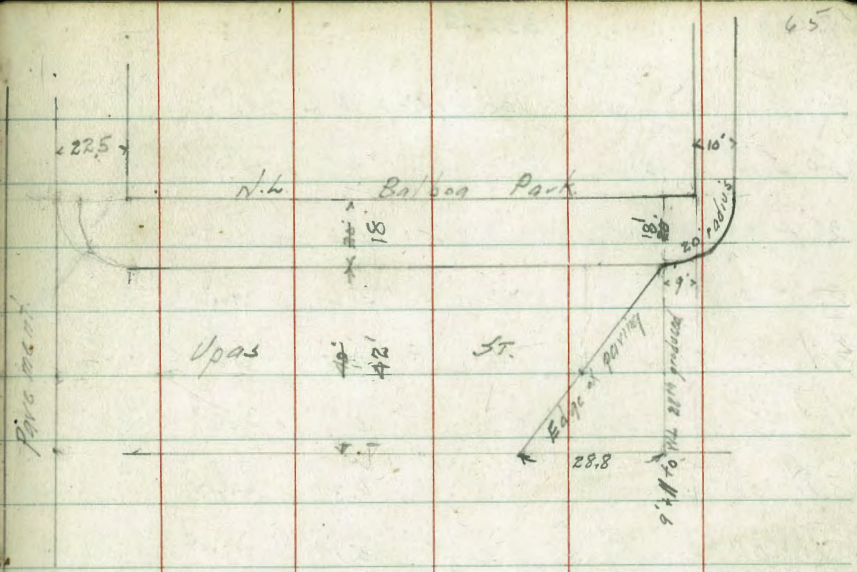
W.H.C.
Palm 5+9800

9/17/23

X section of Upas ST
 28th to Oregon 18'
 Upas 15' 60' wide, with 28' cbs on N.
 N.L. Upas 15' N.L. of Balboa Park

BP 5E
 28th + Upas

B.M.	363	332.43	328.80	
	9' W. of W.L. 28th			
N.cb		371	378.7	✓
✓ gutter on paring edge		4.27	378.16	
	23.4' W. of W.L. 28th			
20' 5" of N.cb = edge paring		3.61	378.8	✓
10' - - -		4.1	378.3	
N.gutter		4.6	377.8	
N.cb		3.98	378.45	✓
	37.8' W. of W.L. 28th			
N.cb		4.18	378.25	✓
✓ gutter		5.0	377.4	
10' 5"		4.6	377.8	
20' "		4.3	378.1	
30' "		4.1	378.3	✓
40' " = edge of paring		3.98	378.65	✓
	50' W. of W.L. 28th			
40' 3" of N.cb		4.0	379.4	
38' " " "		4.7	377.7	



30' 5" of N.cb		4.6	377.8	✓
20' - - -		4.6	377.8	
10' - - -		4.8	377.6	
N.gutter		5.3	377.1	
✓ cb		4.43	378.0	✓
	75' W. of W.L.			
N.cb		4.98	377.65	✓
N.gutter		5.6	376.8	
10' 5"		5.4	377.0	
20' "		5.1	377.3	
30' "		5.2	377.2	
38' "		5.3	377.1	
40' "		3.7	378.7	

332.43

	100' W. of W.L.	28 th	
40' S. of N.cb	3.6	318.8	
38' " " "	5.5	316.9	
30' " " "	5.6	316.8	
20' " " "	5.5	316.9	
10' " " "	5.6	316.8	
N gutter	6.2	316.1	
N. curb	5.19	317.1	

	150' W. of W.L.	28 th	
N. curb	5.96	316.47	
✓ gutter	6.6	315.8	
10' S. of N.cb	6.5	315.9	
20' " " "	6.1	316.3	
30' " " "	6.2	316.1	
40' " " "	6.2	316.1	

	200' W. of W.L.	28 th	
40' S. of N.cb	7.2	315.1	
30' " " "	7.1	315.3	
20' " " "	7.0	315.4	
10' " " "	7.2	315.2	

N gutter

✓ curb

N curb

✓ gutter

10' S.

20' "

30' "

40' "

1/2 S. of N.cb Line on paving

20' " " " " " " "

N.cb Line produced

7.6

6.70

7.55

8.7

7.9

7.7

8.2

8.6

8.50

8.30

8.25

314.8

315.7

314.88 ✓

315.7

314.5

314.7

314.1

313.8

313.9

314.1

314.8

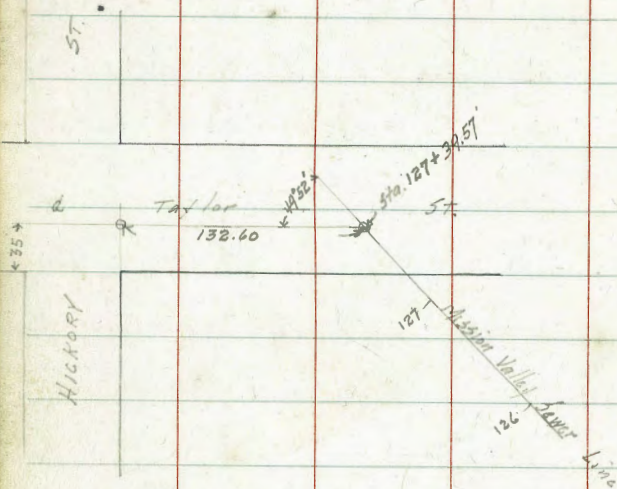
256.5' W. of W.L. = E.L. Oregon

22.5' W. of E.L. Oregon = E. Edge paving

5/26/26 Gregory Tie from Mission Valley Sewer
To Taylor St.

67

See Book 1109, p 46.



8/26/21 Report	Levels for Contours		Taylor St. N. of Hickory					
	423	12.95 12.89		8.72 8.66	Top Hydrant Whitman's Cabin	87 S. of G. of Taylor	7.0	16.0
			6.91	6.044 5.98	Man NW Taylor's Shop	102 ✓ - - -	+0.9	23.9 = Foot of perpendicular bank
T.P.	11.13	22.99 22.93	1.09	11.86 11.80		213 E. of E.L. Hickory		
			175' E. of E.L. Hickory			126 S. of G. of Taylor	+4.0	27.0 = Foot of bank
15' S. of Taylor			8.7	14.3		123 - - - -	0.2	22.8
30 - - -			9.0	14.0		113 - - - -	5.8	17.2
45 ✓ - - -			8.6	14.4		95 - - - -	8.3	14.7
60 ✓ - - -			5.9	17.1		70 - - - -	9.1	13.9
80 ✓ - - -			0.8	22.2		50 ✓ - - -	8.8	14.2
90 - - -			+1.3	24.3	= Foot of bank			
			192' E. of E.L. Hickory			5 L. Taylor	8.5	14.5
93 S. of Taylor			4.1	18.9		30' S. of S.L. Taylor	9.4	13.6
88 - - -			5.9	17.1		65 S - - -	7.8	15.2
70 - - -			7.7	15.3		75 - - - -	4.7	18.3
50 - - -			9.1	13.9		87.5 - - -	+3.6	26.6 = Foot of bank
15 - - -			8.3	14.7				
			200' E. of E.L. Hickory			99' S. of S.L. Taylor	+9.8	32.8 = Foot of bank
15' S. of Taylor			8.3	14.7		90 - - - -	+4.2	27.2
50 - - -			9.2	13.8		80 - - - -	2.2	20.8
75 - - -			7.7	15.3		76 - - - -	6.0	17.0
						235' E. of E.L. Hickory		

71' S. of S.L. Taylor	8.1	14.9	
40' ✓ ✓ ✓ ✓ ✓	9.5	13.5	
S.L. Taylor	8.4	14.6	
250' E. of E.L. Hickory			
S.L. Taylor	9.0	14.0	
35' S. of S.L. Taylor	8.5	14.5	
60' - - - - -	9.7	13.3	
78' - - - - -	7.9	15.1	
100' - - - - -	0.1	22.9	
107' ✓ - - - -	+1.5	24.5	
(4' Wood Last)	+6.3	29.3	
120' S. of S.L. Taylor	+2.7	25.7	= Foot of Bank
260' E. of E.L. Hickory			
131' S. of S.L. Taylor	+0.9	23.9	
120' - - - - -	3.4	19.6	
105' - - - - -	4.1	18.9	
85' - - - - -	8.2	14.8	
70' - - - - -	9.5	13.5	
35' - - - - -	8.5	14.5	

270' E. of E.L. Hickory			
35' S. of S.L. Taylor	8.3	14.7	
70' - - - - -	9.3	13.7	
95' ✓ ✓ ✓ ✓ -	9.2	13.8	
120' - - - - -	7.7	15.3	
127' ✓ ✓ ✓ ✓ -	4.5	18.2	
145' - - - - -	+7.0	30.0	Not yet Foot of Bank
	6.90	16.09	Chk hub Sta 12700 M.W. Sewer

Indiana-Georgia
Robt. Cypress

Cross Section of Alley 20' wide
BIK. 250 Univ Heights Moore

313.11

70

ONS WP

112

313.11

311.99

Robt. Georgia

E

3.4

309.7

SL Robinson

80' S

E Alley Return

5.20

307.9

E

4.5

308.6

C

4.9

308.7

C

5.0

308.1

W ✓ ✓

5.71

307.4

+H

4.7

308.4

2' S

+7 Eucalyptus 16" DIAM

W

3.7

309.4

W

3.6

309.5

+3

4.3

308.8

109 S

C

4.7

308.4

W

3.1

310.0

+7

4.5

308.6

+2 ✓

18" DIAM

3.8

309.3

E

3.8

309.3

+H

4.9

308.7

10' S

E

3.3

309.8

E

4.8

308.3

+3

4.1

309.0

145' S

C

4.0

309.1

E

5.9

307.3

W

3.1

310.0

C

5.4

307.7

40' S

W

4.8

308.3

W

3.9

309.2

190' S

C

4.2

308.9

W

4.9

308.8

+6

4.0

309.1

C

6.0

307.1

Plotted Dec 23 1924
Larry Golden

313.11				313.11				71
+7		5.7	307.4	C		2.7	310.4	
E		6.5	306.6	F		3.8	309.3	
	197'S			E	Garage Conc. Apron	3.9	309.2	on Lin
E - b	Garage Conc. Floor	6.40	306.7	S. entrance	T.T. 41' D	314.93 ✓	2.3 ~	310.79
	225'S					350'S		
E		5.2	307.9	E		4.8	310.1	
C		4.8	308.3	C		3.7	311.2	
W		4.0	309.1	W		3.4	311.5	
	275'S			+ b	Conc Run to Garage	3.55	311.4	
W		2.6	310.5		400'S			
+4		3.5	309.6	W	Reference 1.6 in Alley	3.8	311.1	
C		4.1	309.0	C		4.0	310.0	
E		4.6	308.5	E		3.7	311.2	
	300'S					447'S		
E		3.9	309.2	E		4.7	310.2	
C		3.2	309.7	C		4.7	310.2	
+ b		2.8	310.3	W	Garage Conc. Floor	4.50	310.4	2' in Alley
W		2.1	311.0		460'S			
	321'S			W	✓ ✓ ✓	4.55	310.4	2' in Alley
W		1.7	311.4	E	✓ ✓ Apron	5.53	309.4	4' E. 1.64

31493				314.93			
		494'S					72
W	Garage Conc. floor	4.75	310.2	2.3 in Alley		5.9	309.0
W		4.7	310.2		609'S	5.5	309.4
E		5.1	309.8	E Garage Conc. floor		6.14	308.8 4'E of EL
E		5.2	309.7		614'S		
		511'S		W Double ✓		5.24	309.7 1'W of WL
E-6.5	✓	✓	593		650'S		
		550'S		W		5.4	309.5
E		5.8	309.1	E		5.7	309.2
C		5.5	309.4	E		5.7	309. ✓
W		5.3	309.6		665'S		
		560'S		E		5.7	309.2
E-5	Garage Conc. floor	6.2	308.7	C		5.9	309.0
		580'S		W		5.4	309.5
W	Shed 6 in Alley	5.3	309.6		678'S		
+S		5.9	309.0	W		5.8	309.1
C		5.9	309.0	+3		6.5	308.4
E		6.5	308.4	C		6.7	308.2
		600'S		E		6.4	308.5
W		6.1	308.8				

314.93

73

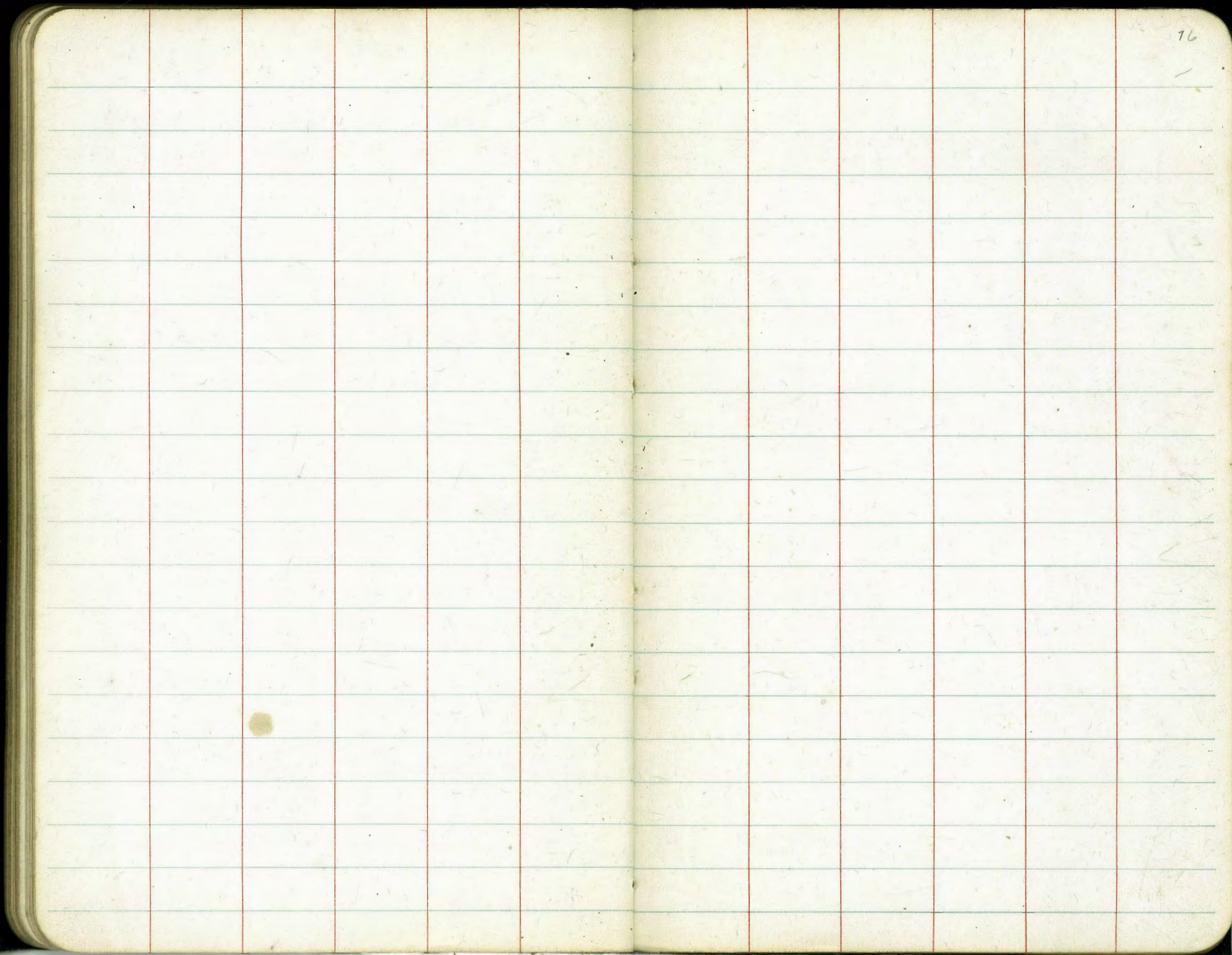
690.5 S = N L Cypress

E	1/4 of Alley Return	1008	304.85	
C		9.5	305.4	
W	✓ ✓ ✓	9.18	305.75	
TP	246	307.98	9.41	305.57
check B.M.		696	301.02	300.98

Strike Cyprus
Indiana
300.98

Levels for Side walk Thru Bk 59 to Lake Park				93.92					
				3/3/20 Inlet	2'N		6.3	87.62	72
BM	1.44	106.48	105.04	Prospect Silvanhoe	3'N		5.4	88.52	
		00 = N. Line Prospect				124'W = S. End wooden stairs			
4'S		4.8	101.68		3'S		7.0	86.92	
4		4.8	101.68		4		7.0	86.92	
4'N		4.7	101.78		3'N		6.9	87.02	
	2.5'W								
4'S		5.2	101.28	4'N - cont walk to House			6.3	87.62	
4		5.7	100.78		T.P.	0.44	81.53 147'W	12.87	81.05
4'N		5.4	101.08		3'S		3.8	77.73	
	50'W								
4'S		6.7	99.78		4		3.8	77.73	
4		7.2	99.28		3'N		3.3	78.23	
4'N		6.9	99.58	4'SN door to House			1.7	80.83	Flag pole
	6.5'W					162'W			
4'S		8.1	98.38		3'S		8.4	72.73	
4		8.9	97.58		4		8.4	72.73	
4'N		8.4	98.08		3'N		8.2	73.33	
T.P.	0.27	93.92 100.	92.85	93.63	T.P.	0.58	67.05 183'W	13.06	68.47
3'S		1.4	92.52		3'S	3.5' cont walk to House		3.1	65.95
13'S		2.8	91.12		4		3.0	66.05	
4		2.8	91.12						
1.5'N		2.8	91.12		3'N		2.8	66.25	
3'N		1.9	92.02			12'W = E. end cont walk 1.5 wide wooden stairs over it Extends to Coast Blvd			
	115'W								
2'S		5.4	88.52		4		5.3	63.75	on walk
2'S		6.3	87.62						
4		6.3	87.62						

		69.05			45.83		
194	194' W				R 72' W Bottom 5. Steps		75
3'S		6.6	62.45		3'S & 3'N	2.6	43.23
3'N	emt walk to House	4.7	64.3		R 97' W E. edge emt Platform 9.4 wide		
T.P.	0.36	56.58	12.83	56.22	⊥	3.7	42.13
		R 19' W N. end wooden stairs			307' W = W edge emt Platform 9.4 wide		
3'S		2.1	54.48		⊥	3.9	41.93
⊥		1.8	54.78	on emt walk 1.5 wide	308' W		
3'N	emt walk to House	1.4	55.18		4, 3'S & 3'N	4.4	41.43
		R R 3' W			312' W		
3'S	emt walk to House	2.7	53.88		3'S	4.9	40.93
⊥	on 1.5 wide emt walk	2.7	53.88		⊥	5.1	40.73
3'N		2.2	54.38		3'N	5.1	40.73
3'S		7.6	48.98		344' W Top stairs. OK 5.4 wide		
⊥		7.1	49.48	on emt walk 1.5 wide	Property owner wants new steps	6.6	39.23
3'N		6.8	49.78		351' W = Bottom steps = E. line East Blvd		
		R 63' N Top of emt stairs			⊥	4.9	36.9
3'S, & 3'N		10.5	46.08				
		These stairs OK. Property owners want replaced to conform with rest of work			Landing	124	on N. 9' wide
						183	" S. 4' "
						194	" N. 1' W. 3.2' E
						219	" H. 4' wide
						223	" S. 3' wide
T.P.	2.15	45.83	18.90	43.68			



The image shows an open notebook with two facing pages. Both pages are cream-colored and feature horizontal blue ruling lines. Each page is divided into two columns by a vertical red margin line. The pages are otherwise blank, with no handwriting or printed text. The notebook is positioned on a white surface, and the page number '27' is visible in the top right corner of the right-hand page.

An open notebook with two blank, lined pages. The pages are cream-colored with horizontal blue lines and vertical red lines forming columns. The right page has the number '78' written in the top right corner. The notebook is placed on a white surface.

8/9/24

SEWER 00 3rd from 6 Juniper

5.

74

	532	214.27		208.95	Grade	
0+00 = 6 3" Juniper			2.13	211.54	193.0 196.0	15.54
0+25			3.34	210.93	193.75	15.18
+50			3.88	210.39	195.50	14.89
1			7.90	206.37	195.0	11.37
+75			9.96	204.31	194.75	9.56
+50			11.83	202.44	194.50	7.94
T.P.	0.27	201.87	12.67	201.60		
+75			1.33	200.54	194.45	6.29
2					191.00 194.00	
+49 = 6" pipe			15.90	185.97	= Flow Line	
basement floor				201.0		

New Cuts Redwood 31st E to Bridge

	Set	Set
W.L. 31 st	300.0	300.0
EL 31 st	299.0	300.0
+50	299.91	300.91
+85	300.85	301.55
	300.80	301.81
	300.88	301.82
	300.74	301.65
	300.44	301.24
	299.92	300.61
	299.21	299.76
	298.80	298.69
	297.20	297.40
W.L. Herman	296.0	296.0
EL ✓	295.0	295.0
+60	294.5	294.5
+20	294.0	294.0

3116
730
318.93
12.75
306.18
0.29
306.47
12.53
293.94
9.41
303.35

2939
668
300.62
2.95
5.62

N	295.0 8.5 4.5 +0.10	96.0 7.35 6.8 +0.55	97.40 5.95 4.5 +0.1	98.69 4.66 4.5 +1.6	99.76 3.54 2.9 3.3 +1.4	300.61 2.74 2.4 2.4 +0.1
S	295.0 8.5 4.5 +0.10	96.0 7.35 6.8 +0.55	97.20 6.15 4.5 +0.1	98.30 5.05	99.21 4.14 3.3 +1.4	99.92 3.43 2.3 +0.1
N	301.24 0.11 2.5 -1.4 +0.1	301.65 1.70 2.1 -1.0 +0.2	307.84 1.51 2.8 -1.4 +0.2	301.81 1.54 1.95 -1.4 -0.5	301.55 1.80 0.0 2.80 0.0	
S	300.44 2.9 2.8 +0.1	300.74 2.61 2.6 +0.2	300.88 2.07 2.6 -1.2	300.80 1.85 3.2 -0.5	300.55 2.80 0.0	
N	300.91 2.44 0.0	300.0 3.35 0.3 +1.0	300.0 5.25 4 +1.0			
S	299.91 3.44 0.0	299.0 4.35 3.1 +1.2	94.5 3.85 6.1 +0.7			



Handwritten calculations and notes on the left page of the notebook. Includes various arithmetic problems and a diagram of a cross-section.

Diagram description: A horizontal line representing a roadway cross-section. A circle on the left is labeled "F.T." and "2'03". A diagonal line from the circle to the right is labeled "100".

Handwritten notes and calculations include:

- 117, 118, 115, 240
- 70, 80, 50, 1590
- 78.25, 78.25, 391.25, 15650, 61600, 59175, 613302.5
- 379, 270
- 179, 58, 60, 8800, 30, 9189, 30
- 3600, 2800, 6100
- 133.39
- 484.12, 2.41, 4.8173
- 217.00, 31.80, 310, 362.10
- 2017, 30.8, 362.000
- 11.47, 10.5, 93
- 11.27, 10.10, 1.37
- 1557.09, 530.1, 1690.14
- 99.97, 6.98, 105.45, 8.41, 110.04
- 0.5997, 1.50, 2.0977
- 2620, 261.95

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

By Julien A. Hall, M. Am. Soc. C. E.

