

1096

FIELD BOOK

335

MICROFILMED

DEC 21 1964

9.52
Voltaire + Bacon.

15¹⁰
523
131

8/11/21 Greenwell
 center 30' ex. 65th Klaunder + 69th Sts
 E1113
 show

CROSS SECTION OF
 Distances all taken on E.

on B.M. 9.00 221.80 212.80 3pk NE 65th Atn

0+00 = N. Imperial Ave.

E of sections from Imperial to S.L. of Brothly

is on E of 65th produced from the north

15 E of E	4.1	217.70
10 " "	3.7	218.1
E	4.1	17.7
5 W	4.5	17.3
10 "	5.2	16.6
15 "	6.3	15.5

0+50.5 = center S.D. + H Ry.

15 W	4.8	17.0
10 W	4.8	17.0
E	4.7	17.1
10 E	4.6	17.2
15 E	4.6	17.2

14.00

15 E	10.0	11.8
10 "	9.3	12.5
E	8.6	13.2
10 W	9.4	12.4
15 "	10.0	11.8

14.50

15 W	10.7	11.1
10 "	10.3	11.5
E	9.4	12.4

G	9.2	212.6
8' E	4.3	12.5
10' "	9.5	12.3
15' "	10.3	11.5

30' E
 18' E
 15' E

1+90 = S. end of bridge

12 E = East of bridge

E

4' W = W rail of bridge

10' "

15' "

see page 59

2+38.5 = N. end of bridge

15 W

10' "

8' "

4.5' = W rail bridge

E

10' E

13' = East bridge

15' "

17' "

25' "

3+00

15 E

12' "

10' "

E

2.5 W

208.6	207.9
12.7	12.7
8.9	8.9
8.5	8.5
8.4	8.4
8.5	8.5
10.2	10.2
10.5	10.5
12.7	12.7
12.4	12.4
12.2	12.2
8.6	8.6
8.3	8.3
8.0	8.0
8.7	8.7
9.7	9.7
7.5	7.5
5.6	5.6
5.6	5.6
6.1	6.1
6.2	6.2

on 2
 65th Ave
 10.52 km

from
 65th Ave
 9.13.3
 10.52

221.80

8' W

10.0

11.8

10' ✓

10.0

11.8

15' ✓

10.3

11.5

3+30

15' W

8.6

13.2

10' ✓

8.2

13.6

4' ✓

4.4

17.4

6

3.9

17.9

10' E

3.8

18.0

12' ✓

3.8

18.0

15' ✓

6.1

15.7

3+37

15' E

5.3

16.5

12' ✓

3.2

18.6

10' ✓

3.2

18.6

6

3.2

18.6

3' W

3.4

18.4

8' ✓

6.1

15.7

10' ✓

6.1

15.7

15' ✓

6.0

15.8

3+50

15' W

4.5

17.3

10' ✓

4.0

17.8

4' ✓

1.9

19.9

6

2.0

19.8

10' E

1.5

220.3

6574 35

12' E

1.5

220.3

15' ✓

2.7

19.1

3+54

15' E

2.0

19.8

12' ✓

1.0

20.8

10' ✓

1.0

20.8

6

1.3

20.5

5' W

1.3

20.5

10' ✓

2.0

19.8

15' ✓

2.3

19.5

T.P.

1221

433.97✓

0.04

221.76

4+00

15' W

9.0

25.0

10' ✓

8.6

26.4

6

8.8

26.2

10' E

8.2

26.8

15' ✓

8.4

26.6

4+50

15' E

2.9

32.1

14' ✓

3.5

31.5

10' ✓

3.6

31.4

6

3.6

31.4

10' W

4.0

31.0

15' ✓

4.0

31.0

T.P.

1216

245.20

0.9✓

233.05✓

24520

5+00

15' W	9.9	235.3
10' ✓	10.0	35.2
C	10.1	34.8
10' E	10.5	34.7
15' ✓	10.7	34.5

5+50

15' E	6.5	38.7
10' ✓	6.3	38.9
C	6.3	38.9
10' W	6.4	38.8
15' ✓	6.8	38.4

6+00

15' W	2.0	43.2
10' ✓	1.3	43.9
C	1.1	43.8
10' E	1.5	43.7
15' ✓	1.3	43.9
T.P.	12.95	258.25
		0.10
		245.10

6+50

15' E	9.9	248.1
10' ✓	10.0	48.0
C	10.0	48.0
10' W	10.2	47.8
15' ✓	11.0	247.0

65th St.

3

7+00

15' W	7.0	251.0
10' ✓	6.0	252.0
C	6.1	51.9
10' E	6.1	51.9
15' E	6.1	51.9

7+50

15' E	2.2	55.8
10' ✓	2.3	55.7
C	2.1	55.9
10' W	2.3	55.7
15' ✓	2.5	55.5

T.P.	12.55	270.31
		0.29
		257.76

8+00

15' W	11.4	58.9
10' ✓	10.8	59.5
C	10.7	59.6
10' E	10.6	59.7
15' ✓	10.6	59.7

8+50

15' E	7.3	63.0
10' ✓	7.4	62.9
C	7.3	63.0
10' W	7.0	63.3
15' ✓	7.8	62.5
	1.43	268.88

12/1/16
J.W. Brock

27031

9+14.85 = 3.1 Brooklyn ✓

15' W	4.5	265.8
10' ✓	3.7	66.6
C	3.7	66.6
10' E	3.8	66.5
15' ✓	4.3	65.8

9+44.85 = 4 Brooklyn

15' E	3.3	67.0
10' ✓	2.6	67.7
C	2.3	68.0
10' W	2.2	68.1
15' ✓	2.6	67.7

9+74.85 = 11.2 Brooklyn

15' W	1.4	68.9
10' ✓	0.7	69.4
C	1.2	69.1
10' E	1.5	68.8
15' ✓	2.1	68.2

10+00

15' E	1.4	68.9
10' ✓	0.8	69.5
C	0.0	70.3
T.P.	11.95	281.97
10' W	11.6	70.4
15' ✓	12.0	70.0

65+0.57

4

10+50

15' W	11.0	271.0
10' ✓	10.2	71.8
C	10.3	71.7
7' E	10.5	71.5
10' ✓	11.5	70.5
15' ✓	11.6	70.4

11+00

15' E	8.8	73.2
13' ✓	9.7	72.3
10' ✓	8.9	73.1
C	8.4	73.6
10' W	8.4	73.6
15' ✓	8.6	73.4

11+50

15' W	5.8	76.2
10' ✓	6.1	75.9
C	6.1	75.9
10' E	6.5	75.5
15' ✓	6.5	75.5

12+00

15' E	3.7	78.3
10' ✓	3.5	78.5
C	3.7	78.3
10' W	3.7	78.3
15' ✓	3.7	78.3

281.97

65th 5th

5

12 + 50

15' W		0.9	281.1
10' -		1.0	281.0
C		1.0	81.0
10' E		1.0	81.0
15' ✓		1.0	81.0
T.P.	12.90	294.57	0.30 281.67

13 + 00

15' E		12.0	82.6
10' ✓		12.3	82.3
C		11.7	82.9
10' W		11.8	82.8
15' ✓		11.2	83.4

13 + 50

15' W		10.3	84.3
10' ✓		9.7	84.9
C		9.8	84.8
10' E		9.7	84.9
15' ✓		9.6	85.0

14 + 08.52 = 5.2 Wunderlin

15' E		7.6	87.0
10' -		7.5	87.1
C		7.3	87.3
10' W		7.3	87.3
15' ✓		7.6	87.0

14 + 38.52 = 6 Wunderlin

15' W		6.5	288.1
10' ✓		5.1	89.2
C		5.7	88.9
10' E		5.9	88.7
15' ✓		6.0	88.6

14 + 68.52 = 11.2 Wunderlin

15' E		4.4	90.2
10' ✓		4.6	90.0
C		4.0	90.6
10' W		4.0	90.6
15' ✓		4.2	90.4

15 + 00

15' W		3.0	91.6
10' ✓		2.7	91.9
C		2.8	91.8
10' E		3.5	91.1
15' ✓		3.2	91.4

15 + 50

15' E		1.2	93.4
10' ✓		1.0	93.6
C		0.6	94.0
10' W		0.6	94.0
15' ✓		0.9	93.7

T.P. 12.81 307.35

00.0

294.57

307.38

16+00

15' W	11.5	295.9
10' -	11.1	96.3
C	11.2	96.2
10' E	11.5	95.9
15' -	12.5	94.9

16+50

15' E	10.4	99.0
10' ✓	8.8	98.6
C	8.5	98.9
10' W	8.6	98.8
15' ✓	8.8	98.6

17+00

15' W	6.1	301.3
10' ✓	5.6	1.8
C	5.4	302.0
10' E	6.0	301.4
15' ✓	7.2	300.2

17+50

15' E	3.3	04.1
10' -	2.0	05.4
C	2.0	5.4
10' W	2.5	4.9
15' -	2.9	4.5
T.P.	12.26	319.47
		017
		307.21

58.62
58.91
51.711903.91
51.71
1955.62

65+4.37

6

18+00

15' W	11.7	307.8
10' -	11.4	08.1
C	11.0	8.5
10' E	11.0	8.5
15' ✓	12.2	7.3 ✓

18+50

15' E	8.4	311.1
10' -	7.7	11.8
C	8.0	11.5
10' W	8.2	11.3
15' ✓	8.5	11.0 ✓

19+03.91 = 5L Bach

15' W	5.4	314.1
10' ✓	4.8	14.7
C	4.0	15.5
10' E	4.0	15.5
15' ✓	4.3	15.2

19+55.62 Δ 39°17' R

12.62	327.59 ✓	4.50	314.97	spk SW Bach
15' E	8.6	19.0		
10' -	8.5	19.1		
C	8.7	18.9		
10' W	10.0	17.6		
15' ✓	10.3	17.3		

32759

20+00

15' W	8.3	319.3
10' ✓	7.8	19.8
C	6.5	21.1
10' E	6.7	20.9
15' ✓	7.0	20.6

20+50

15' E	3.5	24.1
10' ✓	3.1	24.5
C	3.0	24.6
10' W	4.2	23.4
15' ✓	5.0	22.6

21+00

15' W	4.7	24.9
10' ✓	4.0	25.6
C	0.1	27.5
10' E	0.0	27.6
15' ✓	0.0	27.6
T.P.	1298	34037

21+50

15' E	9.7	330.9
10' ✓	9.7	30.9
C	10.0	30.6
10' W	12.0	28.6
15' ✓	12.3	28.3

65+6

7

22+00

15' W	10.0	330.6
10' ✓	8.8	331.8
C	6.9	333.7
10' E	6.5	34.1
15' ✓	6.3	34.3

22+50

15' E	2.8	37.8
10' ✓	3.1	37.5
C	3.5	37.1
10' W	5.3	35.3
15' ✓	5.9	34.7

23+00

15' W	2.4	38.2
10' ✓	1.8	38.8
T.P.	13.00	35353
C	0.0	340.53
10' E	12.1	41.1
15' ✓	12.2	41.3
	12.0	41.5

23+50

15' E	8.7	44.9
10' ✓	8.8	44.7
C	8.4	45.2
10' W	9.4	44.2
15' ✓	9.6	44.0

353.53

34

15' W	4.6	48.9
10' ✓	4.4	49.1
C	3.9	49.6
10' E	4.2	49.3
15' ✓	4.8	48.7
TP	1297	366.15

24+50

15' E	13.3	52.9
10' ✓	12.8	53.4
C	12.8	53.4
10' W	13.0	53.2
15' ✓	13.3	52.9

25+50

15' W	10.0	56.2
10' ✓	9.5	56.7
C	8.7	57.3
10' E	8.8	57.4
15' ✓	9.1	57.1

25+50

15' E	5.4	60.8
10' ✓	4.7	61.5
C	4.9	61.3
10' W	6.6	59.6
15' ✓	7.1	59.1

65th

8

36

15' W	3.6	362.6
10' ✓	3.1	63.1
C	2.0	64.2
10' E	1.9	64.3
15' ✓	1.2	65.0
TP	1496	378.92

36+50

15' E	9.2	69.7
10' ✓	12.4	66.5
C	11.8	67.1
10' W	12.0	66.9
15' ✓	14.0	64.9

37

15' W	11.6	67.3
12' W	10.0	68.9
10' ✓	10.0	68.9
C	9.8	69.1
7' E	9.9	69.0
10' ✓	9.0	69.9
15' ✓	6.0	372.9

37+50

15' E	4.8	74.1
12' ✓	5.6	73.3
10' ✓	7.1	71.8
7.5' ✓	9.0	69.9

378.92

65th ST.

9

C	8.6	370.3
10' W	9.0	69.9
15' ✓	11.1	67.9
28		
15' W	10.6	68.3
10' ✓	9.2	69.7
7' ✓	8.0	70.9
C	7.9	71.0
10' E	8.1	70.8
15' ✓	5.3	73.6
28+50		
15' E	7.0	71.9
10' ✓	7.1	71.8
C	7.3	71.6
7' W	9.5	69.4
10' ✓	10.2	68.7
15' ✓	10.6	68.3
29		
15' W	10.5	68.4
10' ✓	9.4	69.5
C	7.1	71.8
2' E	6.1	72.8
10' ✓	5.8	73.1
15' ✓	6.1	72.8
29+50		
15' E	4.7	74.2

10' E	4.8	374.1
C	4.8	74.1
10' W	7.9	71.1
15' ✓	8.4	70.3
30		
15' W	4.8	74.1
10' ✓	4.2	74.7
C	3.1	75.8
10' E	2.1	76.8
15' ✓	1.9	77.0
T.P. 1195 390.52	0.35	378.57
30+50		
15' E	9.6	380.9
10' ✓	9.8	80.7
C	10.5	80.0
10' W	11.7	78.8
15' ✓	12.1	78.4
31		
15' W	7.6	82.9
10' ✓	7.0	83.5
C	5.8	84.7
10' E	5.7	84.8
15' ✓	5.7	84.8
31+50		
15' E	3.1	387.4
10' ✓	3.3	87.2

3905~

KLAUBER

10

C	3.1	987.4
10' W	3.7	86.8
15' ✓	3.9	86.6
T.P.	12.07	400.07
	2.52	388.00
	31+98.46	Δ
15' W	11.6	388.5
10'	11.3	88.8
C	11.4	88.7
10' E	12.1	88.0
15' ✓	12.7	87.4

32+50

15' E	10.1	90.0
10' ✓	10.1	90.0
C	9.8	90.3
10' W	9.7	90.4
15' ✓	9.9	90.2

33+00

15' W	9.1	91.0
10' ✓	7.6	92.5
C	7.5	92.6
10' E	7.6	92.5
15' ✓	7.8	92.3

33+50

15' E	4.6	95.5
10' ✓	4.8	95.3
C	4.9	95.2

10' W	5.0	95.1
15' ✓	6.3	93.8
	34+00	
15' W	3.1	96.7
10' ✓	1.5	98.6
C	1.4	98.7
10' E	1.9	98.2
15' ✓	1.7	398.4
T.P.	12.86	412.68
	0.25	399.82

34+50

15' E	10.4	402.3
10' ✓	11.1	401.6
C	10.9	401.8
10' W	11.2	01.5
15' ✓	11.5	01.2

35+00

15' W	6.2	406.5
10' ✓	6.2	06.5
C	6.3	06.4
10' E	6.2	06.5
15' ✓	5.7	07.2

35+50

15' E	1.9	410.8
10' ✓	1.7	411.0
C	1.3	411.4
10' W	1.4	11.3
15' ✓	1.6	11.1

41268

TP	12.81	42530	0.19	412.47
		36+00		
15' W			7.1	18.2
10' "			7.9	17.4
C			8.2	17.1
10' E			8.3	17.0
15' "			8.7	16.6

36+50

15' E			5.8	19.5
10' "			4.6	20.7
C			3.9	21.4
10' W			3.8	21.5
15' "			1.7	423.6

36+80.28 Δ

TP	9.37	433.01	1.66	423.44
15' W			6.0	27.0
10' "			9.2	23.8
C			9.9	23.1
10' E			11.3	21.7
15' "			12.0	21.0

37+00

20' E			12.9	20.1
15' "			12.4	20.6
10' "			11.7	21.3
C			9.4	23.6
10' W			8.7	24.3

15' W	7.8	425.2
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37+50

15' W = edge of road	7.2	25.8
10' " = edge of road	7.5	25.5
C	11.7	22.3
10' E	14.3	18.7
15' "	14.4	18.6
20' "	16.0	417.0

38+00

20' E	16.2	416.8
15' "	15.1	17.9
10' "	13.8	19.2
C	10.8	22.2
10' W	8.2	24.8
15' " = edge of road	5.7	27.3

38+50

15' W	4.5	428.5
10' " = edge of road	4.4	28.6
5' " = edge of road	4.5	28.5
C	7.5	25.5
10' E	9.5	23.5
15' "	10.6	22.4
20' "	12.6	20.4

39+00

20' E	7.9	25.2
15' "	6.7	26.3

433.01

10' E		5.1	427.6
5' ✓ = edge of road		2.9	430.1
C		2.7	30.3
10' W = edge of road		3.0	30.0
T.P.	10.70	44.23	2.48 430.53
15' W		7.2	34.0
	39+50		
15' W		4.6	436.6
10' ✓		5.9	35.3
6' ✓ = edge of road		9.8	31.4
C		10.2	31.0
10' E = edge of road		10.1	31.1
15' ✓		11.9	29.3
	40+00		
15' E		11.1	30.8
10' ✓ = edge of road		9.0	32.2
C		9.3	31.9
3' W = edge of road		9.2	32.0
6' ✓		6.3	34.9
10' ✓		5.1	35.8
15' ✓		4.2	37.0
	40+50		
15' W		6.4	34.8
10' ✓		7.3	33.9
C		7.8	33.4
5' ✓ = edge road		9.3	31.8

KLAUBER

14

		9.1	432.1
10' E = edge road		8.9	32.3
15' ✓		10.6	30.6
	41+00		
15' E		11.6	29.6
10' ✓		10.5	30.7
5' ✓		9.6	31.6
C = d of road		10.2	31.0
10' W		10.0	31.2
15' ✓		9.5	31.7
	41+50		
15' W		12.4	28.8
10' ✓		12.3	28.9
C		12.4	28.8
10' E		12.8	28.4
15' ✓		13.6	427.6
T.P.	1.18 429.56	12.85	428.38
	42+00		
15' E		5.8	423.8
10' ✓		5.2	24.4
C		4.7	24.9
10' W		4.5	25.1
15' ✓		4.2	25.4
	42+50		
15' W		7.2	22.4
10' ✓		7.4	22.2

429.56

C	8.0	421.6
10' E	8.2	21.4
15' ✓	8.5	21.1

43+00

15' E	10.7	18.9
10' ✓	10.3	19.3
C	9.8	19.8
10' W	9.9	19.7
15' ✓	9.8	419.8

TP	0.77	419.54	12.79	416.77
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44+00

15' W	2.0	415.5
10' ✓	2.1	15.4
C	2.4	15.1
10' E	3.0	14.5
15' ✓	3.3	14.2

45+00

15' E	8.2	409.3
10' ✓	7.8	09.7
C	7.1	410.4
10' W	6.8	10.7
15' ✓	6.9	10.6

45+77.86 = Δ

15' W	10.7	406.8
10' ✓	10.6	06.9
C	10.5	407.0

KLAUBER

13

10' E	10.8	406.7
15' ✓	10.8	406.7
36' BM	9.17	408.37

3 nails
E side

46+00

15' E	11.2	406.3
10' ✓	11.3	6.2
C	11.2	6.3
10' W	11.2	6.3
15' ✓	11.2	6.3

46+50

15' W	13.1	404.4
10' ✓	13.1	4.4
C	12.9	4.6
10' E	12.9	4.6
15' ✓	12.9	4.6
TP	3.83	408.68

47+00

15' E	5.3	403.4
10' ✓	4.7	404.0
C	4.7	4.0
10' W	4.9	3.8
15' ✓	5.5	3.2

48+00

15' W	5.4	3.3
10' ✓	5.4	3.3
C	5.4	403.3

408.68

10' E	5.5	403.2	
15' ✓	6.0	02.7	
	49+00		
15' E	5.8	2.9	
10' ✓	5.3	3.4	
C	4.7	4.0	
10' W	4.6	4.1	
15' ✓	4.2	4.3	
	49+45 =	2 of H/por 5+ (produced)	
15' W	4.0	4.7	
10' ✓	4.5	4.2	
C	4.9 ✓	403.74	on 3/4" pipe
10' E	5.6	3.1	
15' ✓	6.3	2.4	
	50+00		
15' E	6.7	2.0	
10' ✓	6.3	2.4	
C	4.8	3.9	
10' W	4.1	4.3	
15' ✓	3.7	5.0	
	51+00		
15' W	7.5	6.2	
10' ✓	7.9	5.9	
C	7.9	5.8	
10' E	3.6	5.1	
15' ✓	4.1	4.6	

KLAUBER

14

	51+50		
15' E	0.5	408.2	
10' ✓	0.1	8.6	
C	0.1	8.6	
10' W	0.0	8.7	
15' ✓	0.0	8.7	
T.P.	12.92	421.10	0.50 408.15
	52+00		
15' W	7.1	414.0	
10' ✓	7.9	13.2	
C	8.1	13.0	
10' E	7.1	13.7	
15' ✓	7.3	13.8	
	52+50		
15' E	1.1	420.0	
10' ✓	1.3	19.8	
C	1.8	19.3	
10' W	2.0	19.1	
15' ✓	2.0	19.1	
T.P.	14.87	433.36	0.61 420.49
	53+00		
15' W	8.6	424.8	
10' ✓	8.5	424.9	
C	7.9	425.5	
10' E	7.3	26.1	
15' ✓	7.6	25.8	

433.36

53+50

15'E	2.3	431.1
10'✓	2.4	31.0
C	3.4	30.0
10'W	4.2	29.2
15'✓	4.2	29.0
54+00		
15'W	2.0	31.4
10'✓	1.8	31.6
C	1.9	31.5
10'E	0.4	33.0
15'✓	0.0	33.4
T.P.	12.31	445.29
	54+50	038 432.98
15'E	11.4	433.9
10'✓	12.1	33.2
C	12.5	32.8
10'W	12.8	32.5
15'✓	14.2	31.1
55+00		
15'W	15.7	29.6
10'✓	15.6	29.7
6'✓	13.7	31.6
C	13.3	32.0
6'E	13.4	31.9
10'✓	11.9	33.4

KLAUBER

15

445.29

15'E

11.1

434.2

55+50

15'E

7.7

35.6

10'✓

11.1

34.3

6'✓

11.3

34.0

5.9

12.4

32.9

0

11.9

33.4

10'W

14.5

32.8

15'✓

13.2

32.1

56+00

15'W

9.5

35.8

10'✓

8.9

36.4

C

8.2

37.1

6'E

8.3

37.0

6.1'✓

7.1

38.2

10'✓

7.1

38.2

15'✓

6.6

38.7

56+50

15'E

2.3

43.0

10'✓

3.5

41.8

C

3.2

41.9

10'W

4.4

40.9

15'✓

4.8

40.5

56+75

15'W

2.4

42.9

10'✓

1.3

44.0

445.29

C		1.1	444.2
10'E		0.9	44.4
15'✓		0.7	44.6
T.P.	9.40	454.02	0.67 444.62
		57+00	
15'E		8.9	445.1
10'✓		9.5	44.5
C		9.6	44.4
10'W		10.3	43.7
15'✓		10.3	43.7
		57+50	
15'W		8.7	45.3
10'✓		8.3	45.7
C		8.3	45.7
10'E		7.4	46.6
15'✓		6.6	47.4
		58+00	
15'E		6.2	47.8
10'✓		6.3	47.7
C		6.4	47.6
10'W		7.1	46.9
15'✓		7.5	46.5
		58+50	
15'W		6.9	47.1
10'✓		6.6	47.4
C		5.9	48.1

KLAUBER

16

10'E		5.4	448.6
15'✓		4.3	49.7
		59+00	
15'E		5.0	49.0
10'✓		5.0	49.0
C		5.1	48.9
10'W		5.0	49.0
15'✓		5.8	48.2
		59+50	
15'W		5.4	48.6
10'✓		5.5	48.5
C		5.2	48.8
10'E		4.8	49.2
15'✓		4.6	49.4
		60+00	
15'E		4.1	49.9
10'✓		4.3	49.7
C		3.8	50.2
10'W		4.1	49.9
15'✓		4.2	49.8
		60+50	
15'W		4.4	49.6
10'✓		4.2	49.8
C		3.4	50.6
10'E		3.5	50.5
15'✓		3.0	51.0

454.02

61+00

15'E	3.0	451.0
10'~	3.9	50.1
C	4.2	49.8
10'W	4.5	49.5
15'~	5.0	49.0

61+50

15'W	6.1	47.9
10'~	6.3	47.7
C	6.2	47.8
10'E	6.3	47.7
15'~	6.2	47.8

62+00

15'E	7.0	47.0
10'~	7.7	46.3
C	7.8	46.2
10'W	7.9	46.1
15'~	8.0	46.0

62+25.0

15'W	9.1	44.6
10'~	9.2	44.8
C	9.5	44.5
10'E	9.2	44.8
15'~	7.9	46.1

62+50

15'E	10.4	43.6
------	------	------

KLAUBER

17

10'E	11.8	442.2
C	11.9	42.1
10'W	12.0	42.0
15'W	12.2	41.8
T.P.	1.46	442.86
	12.62	441.70

63+00

15'W	7.1	435.8
10'~	6.7	36.2
C	5.2	37.7
10'E	5.1	37.8
15'~	3.8	39.1

63+50

15'E	5.1	37.8
10'~	5.9	37.0
C	5.8	37.1
10'W	7.3	35.6
15'~	8.7	34.2

64+00

15'W	4.9	38.0
10'~	4.5	38.4
C	4.6	38.3
10'E	4.4	38.5
15'~	3.9	39.0
T.P.	1.24	455.29
	0.17	442.69

455.09

64+50

15'E	9.9	445.2
10'✓	10.2	44.9
6'✓	11.4	43.7
C	11.5	43.6
10'W	12.2	42.9
15'✓	11.6	43.5

65+10

15'W	6.6	48.5
10'✓	6.3	48.8
C	5.8	49.3
10'E	5.1	50.0
15'✓	5.2	49.9

65+50

15'E	1.8	53.3
10'✓	3.3	51.8
C	3.7	51.4
10'W	3.4	51.7
15'✓	3.1	52.0

66+00

15'W	0.6	54.5
10'✓	0.5	54.6
C	0.5	54.6
10'E	0.5	54.6
15'✓	0.2	54.9

14.47

467.39

0.17 454.72

KLAUBER.

18

467.39

66+50

15'E	9.7	457.7
10'✓	9.8	57.6
C	10.0	57.4
10'W	10.3	57.1
15'✓	11.0	56.4

67+00

15'W	7.4	480.0
10'✓	7.8	59.6
C	7.9	59.5
10'E	7.8	59.6
15'✓	7.2	60.2

67+50

15'E	5.8	61.6
10'✓	6.5	60.9
C	6.1	61.3
10'W	6.6	60.8
15'✓	6.6	60.8

67+75

15'W	4.0	63.4
10'✓	4.0	63.4
C	4.0	63.4
10'E	4.1	63.3
15'✓	3.8	63.6

68+00

15'E	3.6	63.8
------	-----	------

467.39

10'E	3.5	463.9
C	3.6	63.8
10'W	4.3	63.1
15'✓	4.4	62.9
68+35'		
15'W	3.5	63.9
10'✓	2.7	64.7
C	2.4	65.0
10'E	2.4	65.0
15'✓	2.2	65.2
69+00		
15'E	0.7	66.7
10'✓	1.2	66.2
C	2.3	65.1
10'W	2.8	64.6
15'✓	2.8	64.6
69+50		
15'W	3.0	64.4
10'✓	3.0	64.4
C	2.4	65.0
10'E	2.8	64.6
15'✓	2.1	64.3
70+00		
15'E	7.6	59.8
10'✓	7.5	59.9
C	7.1	60.3

KLHUBER

19

467.39

10'W	6.8	460.6
15'✓	5.9	61.5
X 70+50		No road from here on.
15'W	10.0	57.4
10'✓	10.5	57.2
C	11.4	56.0
10'E	12.2	55.2
15'✓	13.3	54.1
70+93.38 = Δ pt = d. of 69 th st (30' wide)		
15'E	15.0	52.4
10'✓	13.6	54.4
C	12.7	54.7
10'W	11.5	55.7
15'✓	10.9	56.5
71+25		
15'W	8.7	58.7
10'✓	8.6	58.8
C	8.8	58.6
10'E	8.8	58.6
15'✓	8.9	58.5
71+50		
15'E	6.4	61.0
10'✓	6.6	60.8
C	6.2	61.2
10'W	6.1	61.3
15'✓	6.1	61.3

467.39

72+00

15' W	3.9	463.5
10' ✓	4.1	63.3
C	4.2	63.2
10' E	4.3	63.2
15' ✓	4.3	63.2
T.P.	5.79	468.78
	4.40	467.99

72+50

15' E	4.5	464.3
10' ✓	4.7	64.1
C	5.2	63.6
10' W	5.9	62.9
15' ✓	6.0	62.8

73+00

15' W	7.4	61.4
10' ✓	7.3	61.5
C	7.0	61.8
10' E	6.5	62.3
15' ✓	6.2	62.6

73+50

15' E	8.5	60.3
10' ✓	8.4	60.4
C	9.3	59.5
10' W	9.6	59.2
15' ✓	9.9	58.9

KLAUBER

468.78

20

74+00

15' W	11.3	457.5
10' ✓	11.1	57.7
C	9.8	59.0
10' E	8.1	60.7
15' ✓	7.9	60.9

74+50

15' E	8.2	60.6
10' ✓	8.2	60.6
C	8.1	60.7
10' W	9.7	59.1
15' ✓	11.3	57.5

75+00

15' W	11.5	57.3
10' ✓	10.9	57.9
C	9.7	59.1
10' E	7.2	61.6
15' ✓	6.0	62.8

75+50

15' E	7.5	61.3
10' ✓	8.7	60.1
C	9.3	59.5
10' W	10.0	58.8
15' W	11.1	57.7

76+00

15' W	11.8	57.0
-------	------	------

468.78

10' W	10.9	457.9
C	9.2	59.6
10' E	8.1	60.4
15' ✓	8.3	60.5
76+50		
15' E	8.1	60.7
10' ✓	8.7	60.1
C	9.2	59.6
10' W	9.9	58.9
15' ✓	10.5	58.3
77+00		
15' W	7.0	61.8
10' ✓	6.9	61.9
C	6.7	62.1
10' E	6.8	62.0
15' ✓	6.0	62.8
77+50		
15' E	4.5	64.3
10' ✓	4.9	63.9
C	6.3	62.5
10' W	6.8	62.0
15' ✓	6.2	62.6
78+00		
15' W	5.0	63.8
10' ✓	5.5	63.3
C	6.1	62.7

KLAUBER

27

468.78

10' E	4.9	463.9
15' ✓	4.4	64.4
78+50		
15' E	5.3	63.5
10' ✓	5.1	63.4
C	4.5	64.3
10' W	4.1	64.7
15' ✓	3.9	64.9
79+00		
15' W	3.1	65.7
10' ✓	3.2	65.6
C	4.0	64.8
10' E	4.6	64.2
15' ✓	4.6	64.2
79+50		
15' E	4.0	64.8
10' ✓	4.0	64.8
C	4.1	64.7
10' W	4.1	64.7
15' ✓	3.9	64.9
80+00		
15' W	3.2	65.6
10' ✓	2.7	66.1
C	2.3	66.5
10' E	3.2	65.6
15' ✓	2.3	65.5

468.78

80+50

15'E

4.4

466.4

10'✓

4.7

66.1

C

3.6

65.2

10'W

4.5

64.3

15'✓

4.7

64.1

81+00

15'W

4.2

64.6

10'✓

3.8

65.0

C

2.8

66.0

10'E

2.1

66.7

15'✓

2.2

66.6

81+50

15'E

3.5

65.3

10'✓

3.5

65.3

C

3.5

65.3

10'W

3.6

65.2

15'✓

2.8

66.0

82+00

15'W

4.6

64.2

10'✓

4.3

64.5

C

4.0

64.8

10'E

4.0

64.8

15'✓

3.8

65.0

82+16.55 North Boundary of City.

15'E

4.1

64.7

65.77

22

4.3

464.5

4.5

64.3

4.5

64.3

4.8

64.0

2.83

465.75

Top of Mont
NE. cor. of
city

= 465.70

EL's along East Line of Balboa Park for Profile

10-29-22

Donnan;

245.30

23

	0.56	311.47 ✓		310.91 BM. OF RECOR Granada & Pilon;
	-0.22	301.56 ✓	9.89	301.55 ✓
	0.73	290.86 ✓	11.73	289.83 = Granite Mon E.L. Bolton & S.L. Natsmeg St.
00 = E.L. Park & S.L. Natsmeg;			1.1	
+50			3.7	
+100			5.0	
+150			7.7	
2			12.0	
#	0.00	277.83 ✓	12.73	277.83 ✓
+50			4.3	
+70			7.0	
#	0.55	265.48 ✓	12.90	264.93 ✓
3+01.27 = N.L. Maple St. (80' wide)			1.4	
#	"	"	8.2	
0			11.02	264.46 = 13' Mon maple;
#	0.54	253.11 ✓	12.91	252.57 ✓
00 = S.L. Maple St.			3.1	
+34			8.5	
+50			13.1	
#	0.56	240.95 ✓	12.72	240.39 ✓
1			11.9	
#	-0.01	227.94 ✓	13.00	227.95 ✓
+50			7.1	
#	0.12	215.30 ✓	12.76	215.18 ✓
+82			3.0	

2		8.9	
	+22 on old RR Dump:	12.7	
#	0.53	202.98 ✓	12.85
+50			2.0
+62 = S. Edge dump;			2.7
3+01.40 = N.L. Laurel St (80' wide)			9.0
#	0.31	190.41 ✓	12.78
± Laurel St			3.0
0			5.14
00 = S.L. Laurel St			9.7
#	-0.02	177.54 ✓	12.85
+27			3.3
+50			4.1
+100			5.2
+150			7.5
2			10.7
+08 } waterway of Snotzer canyon			11.4
+12			8.8
+50			9.7
3+01.16 = N.L. Katmia St (80' wide) at S. Edge trail:			11.4
#	"	"	12.0
0			12.11
00 = S.L. Katmia St			9.2
+50			9.4
#	11.36	180.34 ✓	9.56
1			10.3

	+	π 180.34	-
1+2 = N.L. of Alley (30' wide)			12.8
00 = S.L. Alley - Mon = P.L.			13.7
+15			13.4
+50			11.7
+73			9.3
1			7.6
1+48 = N.L. Juniper St. 30' wide			2.3
#	5.87	185.85	0.38
4 Juniper St.			2.3
S.L. "			2.4
+50			2.5
1+00			2.7
+50			4.2
+82			6.0
2+00			7.8
+04			8.6
+20			21.0
+22			20.0
+30			18.0
+50			11.1
#	11.59	197.25	0.00
3+10 = N.L. IVY St. (60' wide)			2.7
#			2.7
S.L. IVY St.			6.2
0+50			2.0
	7.29	206.09	0.72
			186.70 = 13' Mon IVY St.

	+	π 206.09	-	24
0+70			1.2	
1			2.2	
+15			3.9	
#	0.36	153.41	13.04	153.05
+50			2.1	
+75			10.0	
#	7.37	187.86	12.72	180.49
2			10.2	
+10			11.6	
+18			11.3	
+37			2.5	
+50			5.7	
+65			11.4	
+75			11.2	
+87			9.5	
3			6.3	
#	12.92	100.79	0.01	187.85
3+20 = N.L. HANTHORNE (60' wide)			11.9	
4			2.3	
#	12.32	213.93	0.18	200.61 = 13' Mon Hawthorne
00 = S.L. Hawthorn St			8.2	
#	12.32	226.04	0.23	213.70
0+50			11.0	
+72			5.9	
1+00			3.9	
#	8.92	234.78	0.00	226.04

230.98 ✓

1+50

8.9

2

6.7

+50

4.9

3

4.4

+08⁶ = N. L. Grape St.

4.6

#

2.30

232.68 = 232.90 B.M.

25

1/4/23
Gregory
Moore
Miller
Shaw

Levels on Various ALLEYS IN MISSION BEACH FOR WATER MAINS

1.37	10.89	9.52
4.19	9.99	5.09 5.80
10.73	9.74	10.98 -0.99

BR 11E
Voltaire +
Beacon

sph 52 BKT
Mission + P. 1st

Alley BIK 179-178

EL Mission	(9.7)	10.2	- .5
50' E		9.9	- .2
100' ✓		9.9	- .2
150' ✓		9.9	- .2
200' ✓		10.2	- .5
6 Bay Side Lane (+ 1 + m)		10.5	- .8
260' E		9.6	+ .1
T.P.	4.70	9.47	4.97 4.77

Alley 3 184-185

11.47	11.71	9.23	0.24
EL Mission		11.6	0.2
50' E		11.6	0.1
100' ✓		11.6	0.2
150' ✓		11.6	0.1
200' ✓		11.4	0.2
6 Bay Side		12.5	-0.8
315' E of Mission		11.9	-0.2

42
6.2

123
6.2

128
6.2

26

9.74

Alley BIKS 180-181

W.L. Mission	(9.7)	9.80	-0.1 X
50' W		9.3	+0.4 X
90' ✓		8.7	+1.0 X
150' ✓		4.2	+5.5 X
6 Strand Way		1.5	+8.2 X
255 West		4.0	+5.7 X
T.P.	4.70	9.47	4.97 4.77

Alley 3 183-182

11.47	11.71	9.23	0.24
247' W of Mission	(11.7)	5.7	+6.0 X
6 Strand		3.5	+8.2 X
150' W of Mission		6.5	+5.2 X
100' ✓		10.6	+1.1 X
50' ✓		11.6	+0.1 X
W.L. Mission		11.7	0.0 X

Alley 3 188-189

W.L. Mission	11.6	+0.1 ✓
50' W	11.2	+0.5 ✓
90' ✓	10.6	+1.1 ✓
150' ✓	6.2	+5.5 ✓
6 Strand	3.9	+7.8 X
10 W of	3.7	+8.0 ✓
35' ✓	4.7	+7.0 ✓

35' ✓ = Bath house

11.71

Alleys 187-186

EL Mission		12.1	-0.4	✓
50' E		12.1	-0.4	✓
100' ✓		12.2	-0.5	✓
150' ✓		12.1	-0.4	✓
200' ✓		12.2	-0.5	✓
& Bayside		12.2	-0.5	✓
300' E of Mission		11.6	+0.1	✓
T.P.	4.33	10.53	5.51	620

Alleys 192-193

E.L. Mission		11.0	-0.5	✓
& Bayside		11.2	-0.7	✓
70' E of ✓		10.8	-0.3	✓

Alleys 191-190

60' W of & Strand		4.2	+6.3	✓
& Strand		2.4	+8.1	✓
10' E of ✓		2.6	+7.9	✓
50' - - -		6.1	+4.4	✓
90' - - -		8.5	+2.0	✓
W.L. Mission		10.5	0.0	✓
T.P.	9.63	9.75	10.41	0.12

Alleys 195-194

EL Mission		10.0	-0.3	✓
& Bayside		10.5	-0.8	✓
65' E of ✓		9.9	-0.2	✓

9.75

27

Alleys 196-197

W.L. Mission		9.4	+2.3	✓
75' W		6.1	+2.6	✓
& Strand		1.8	+7.9	✓
60' W of & Strand		3.5	+6.2	✓

Alleys 199-198

60' W of & Strand		3.6	+6.2	✓
& Strand		2.9	+6.8	✓
50' E of ✓		5.7	+4.0	✓
90' - - -		9.0	+0.7	✓
W.L. Mission		9.0	+0.7	✓

Alleys 200-201

65' E of & Bayside		10.6	-0.9	✓
& Bayside		10.6	-0.9	✓
EL Mission		9.5	+0.2	✓

Alleys 203-202

E.L. Mission		9.4	+0.3	✓
& Bayside		10.5	-0.8	✓
65' E of ✓		9.7	0.0	✓

Alleys 204-205

W.L. Mission		9.0	+0.7	✓
75' W of ✓		5.7	+4.0	✓
& Strand		3.0	+6.7	✓
60' W of ✓		4.2	+5.5	✓
T.P.	9.75	9.98	9.52	0.23

9.98

ok Strand Way

ok Seagirt Crt. (102) 30 + 7.0 ✓

✓ Alley 206-207 4.0 + 6.0 ✓

25' N. ok ✓ 2.7 + 7.3 ✓

ok Sunset Court 4.0 + 6.0 ✓

ok Alley 212-213 2.8 + 7.2 ✓

ok Tangiers 3.2 + 6.8 ✓

✓ Alley 215-214 4.8 + 5.2 ✓

✓ Toulon 3.5 + 6.5 ✓

✓ Alley 220-221 4.0 + 6.0 ✓

✓ Vanitie 4.0 + 6.0 ✓

✓ Alley 222-223 4.1 + 5.9 ✓

TP. 644 8.95 7.47 + 2.51 ✓

ok San Rafael 1.8 + 7.1 ✓

ok Alley 228-229 2.2 + 6.7 ✓

✓ Venice 2.0 + 6.9 ✓

✓ Alley 230-231 2.3 + 6.6 ✓

✓ Yerong 3.6 + 5.3 ✓

✓ Alley 235-236 4.3 + 6.6 ✓

9.98

28

Alleys 207-206

N.L. Mission (102) 8.9 + 1.1 ✓

50' W. 7.2 + 7.8 ✓

85' ✓ 4.0 + 6.0 ✓

ok Strand 4.0 + 6.0 ✓

45' N. ok 1.6 + 8.4 ✓

60' - - 4.3 + 5.7 ✓

Alleys 211-210

E.L. Mission 9.7 + 0.3 ✓

ok Bayside 10.3 - 0.3 ✓

60' E. ok ✓ 9.8 + 0.2 ✓

Alleys 212-213

60' W. ok Strand 4.0 + 6.0 ✓

30' N. ok Strand 2.0 + 8.0 ✓

- - 2.8 + 7.2 ✓

50' E. - - 4.2 + 5.8 ✓

80' - - - 8.8 + 1.2 ✓

N.L. Mission 9.8 + 0.2 ✓

Alleys 215-214

N.L. Mission 9.9 + 0.1 ✓

25' N. 9.1 + 0.9 ✓

75' ✓ 3.8 + 6.2 ✓

40' W. L. Strand 2.8 + 7.2 ✓

60' - - 10.1 + 0.1 ✓

E.L. Mission - 9.0 + 1.0 ✓

130' W. L. Bayside } NB 10.7 - 0.7 ✓

100' W. L. Bayside } 11.2 - 1.2 ✓

50' W. L. Bayside } 10.5 - 0.5 ✓

ok Bayside } 9.9 + 0.1 ✓

60' E. 9.9 + 0.1 ✓

998

Alley 220-221

60' W & Strand	(100)	3.6	+6.4	✓
40' ✓ ✓		2.1	+7.9	✓
✓ ✓		4.0	+6.0	✓
50' E ✓		6.8	+3.2	✓
W.L. Mission		9.5	+0.5	✓

Alley 222-223

W.L. Mission		9.6	+0.0	✓
65' W.		7.0	+3.0	✓
85' ✓		3.9	+6.1	✓
& Strand		4.1	+5.9	✓
40' W ✓		2.2	+7.8	✓
60' ✓ ✓		4.0	+6.0	✓
T.P. 644 896		7.47	2.51	✓

Alley 228-229

60' W & Strand		1.8	+7.1	✓
& ✓		2.2	+6.7	✓
10' E ✓		2.1	+6.8	✓
40' ✓ ✓		6.8	+2.1	✓
100' ✓ ✓ ✓		9.0	+0.0	✓
W.L. Mission		8.5	+0.4	✓

998

(100)

29

Alley 219-218

E.L. Mission		9.7	+0.3	✓
& Bayside		10.8	-0.8	✓
60' E ✓		10.6	-0.6	✓

Alley 224-225

60' Exd Bayside		9.9	+0.1	✓
& Bayside		10.2	-0.2	✓
E.L. Mission		10.2	-0.2	✓

T.P. 644 896 (90) 7.47 2.51

Alley 227-226

E.L. Mission		9.2	-0.2	✓
10' Exd E.L. Mission		9.4	-0.4	✓
50' ✓ ✓ ✓		10.6	-1.6	✓
& Bayside		10.1	-1.1	✓
60' E ✓		9.9	-0.9	✓

Alley 232-233

E.L. Mission		9.7	-0.7	✓
50' ✓ ✓		10.1	-1.1	✓
& Bayside		10.0	-1.0	✓
60' E ✓		9.6	-0.6	✓

Alley 234

E.L. Mission		9.7	-0.7	✓
& Bayside		9.8	-0.8	✓
60' E ✓		9.5	-0.5	✓

8.95 - 90

Alley 231-230

W.L. Mission 91 - 0.1 ✓

50' W. of W.L. Mission 10.0 - 1.0 ✓

100' - - - 7.2 + 1.8 ✓

2. Strand 2.3 + 6.3 ✓

25' W ✓ 4.3 + 4.7 ✓

15' - - - 1.7 + 7.3 ✓

60' - - - 3.7 + 5.3 ✓

Alley 236-235

60' W. 2 Strand 1.1 + 7.9 ✓

20' - - - 0.5 + 8.5 ✓

2 ✓ 4.3 + 4.7 ✓

75' E - - - 9.2 - 0.2 ✓

60' W of W.L. Mission 7.3 + 1.7 ✓

15' - - - 10.5 - 1.5 ✓

W.L. Mission 9.2 - 0.2 ✓

3/24/23

Gregory
Moore
MillerCROSS SECTION OF
GLENWOOD DRIVE
End to End.WIDTHS OF STREET
AS SHOWN ON SKETCH
SIDEWALKS 5' Wide
Curb is 1' too far S. on both side of

13.02

83.08

70.058

E.L. India

N	0+00	6.2	76.9	
cb		6.48	76.6	on curb
1/4		6.3	76.8	on paving
C	0+00	6.2	76.9	
1/4		6.0	77.1	
+6		5.7	77.4	
cb		5.20	77.88	on curb
S	0+00	4.9	78.2	

13.59' E on N 00' E on S = Sec. A.

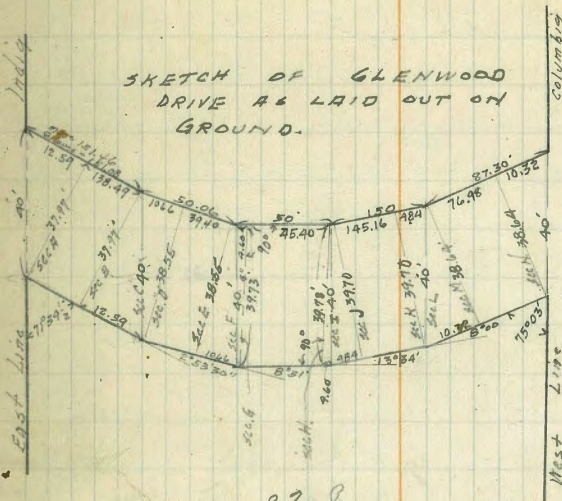
S	0+00	4.9	78.2	
cb		5.1	78.0	
+1		5.6	77.5	
1/4		6.0	77.1	
C	0+62.9	6.2	76.9	
1/4		6.4	76.7	
cb		6.1	77.0	
N	0+77.59	5.7	77.4	

50' E of Sec. A

N	0+62.59	5.2	77.9	
cb		5.5	77.6	
1/4		5.5	77.6	
C	0+56.29	5.3	77.8	
1/4		4.7	78.4	

70.02

31

SKETCH OF GLENWOOD
DRIVE AS LAID OUT ON
GROUND.

83.08

cb		5.1	77.7	
S	0+50	5.7	77.4	
		100' E of Sec. A		
S	1+00	4.8	78.3	
cb		4.3	78.8	
1/4		4.4	78.7	
C	1+06.29	4.6	78.5	
1/4		4.6	78.5	
cb		4.7	78.4	
N	1+12.6	4.2	78.9	

138.49' E = Sec. B

N	1+51.08	3.9	79.2	
cb		4.0	79.1	
1/4		4.2	78.9	
C	1+44.28	4.2	78.9	

Plotted May 15 1923
G.P.M.

$\frac{1}{4}$ 83.08 3.9 79.7
 cb 3.6 79.5
 S 1+38.49 3.6 79.5
 12.59' E of Sec B
 S 1+51.05 3.2 79.9
 cb 3.2 79.9
 $\frac{1}{4}$ 3.8 79.3
 C 1+51.08 4.1 79.0
 $\frac{1}{4}$ 4.0 79.1
 cb 3.9 79.2
 N 1+51.05 3.9 79.2
 10.66' E of Sec C
 N 1+61.24 3.4 79.7
 cb 3.6 79.5
 $\frac{1}{4}$ 3.9 79.7
 C 1+56.01 4.0 79.1
 $\frac{1}{4}$ 3.6 79.5
 cb 3.2 79.9
 S 1+51.08 3.2 79.9
 39.40' E of Sec D = Sec E
 S 1+90.48 2.7 80.4
 cb 2.7 80.4
 $\frac{1}{4}$ 3.4 79.7
 C 1+95.81 3.4 79.7
 $\frac{1}{4}$ 3.3 79.8
 cb 3.1 80.0
 T.P. 12.05 9209 3.04 80.04 ✓

9709 32
 N 2+01.14 11.7 80.4
 10.66' E of Sec E
 N 2+01.14 11.7 80.4
 cb 12.1 80.0
 $\frac{1}{4}$ 12.3 79.8
 C 2+01.14 12.4 79.7
 $\frac{1}{4}$ 12.3 79.8
 cb 11.2 79.9
 S 2+01.14 10.6 81.5
 4.60' E of Sec F
 S 2+01.14 10.6 81.5
 cb 11.4 80.7
 $\frac{1}{4}$ 12.3 79.8
 C 2+03.44 12.3 79.8
 $\frac{1}{4}$ 12.2 79.9
 cb 11.9 80.2
 N 2+05.74 11.7 80.4
 11' E of Sec G
 N 2+16.74 11.4 80.7
 cb 11.7 80.4
 17' E of Sec G
 N 2+22.74 9.5 82.6
 +3 11.1 81.0
 cb 11.1 81.0
 41' E of Sec G
 N 2+46.74 9.3 82.8 ✓

92.09

+ 2	10.7	81.4
cb	10.8	81.3

45.4' E of Sec 6 = Sec. H.

N 2+51 ¹⁴	10.3	81.8
cb	11.0	81.1
1/4	11.3	80.8
C 2+48 ²⁴	11.3	80.8
1/4	11.1	81.0
cb	10.6	81.5
S 2+44 ⁵⁴	10.5	81.6

4.6' E of H on S 00' E of N = I

S 2+51 ¹⁴	10.1	82.0
cb	10.5	81.6
1/4	11.0	81.1
C 2+51 ¹⁴	11.2	80.9
1/4	11.1	81.0
cb	10.9	81.2
N 2+51 ¹⁴	10.3	81.8

4.84' E of Sec I on S 00' E of N = Sec J.

N 2+51 ¹⁴	10.3	81.8
cb	10.9	81.2
1/4	11.1	82.0
C 2+53 ⁵⁶	11.1	81.0
1/4	11.0	81.1
cb	10.5	81.6
S 2+55 ²²	9.7	82.4

94.09

73

25' E of Sec. J

S 2+80 ⁹⁸	7.5	84.6
cb	9.3	82.8
1/4	10.2	81.9
C 2+78 ⁵⁶	10.4	81.7
1/4	10.2	81.9
cb	9.5	82.6
N 2+76 ¹⁴	9.0	83.1

65' E of Sec. J

N 3+16 ⁷⁴	6.6	85.5
cb	6.8	85.3
1/4	7.3	84.8
+ 2	8.3	83.8
C 3+18 ⁵⁶	8.2	83.9
1/4	8.1	84.0
cb	7.8	84.3
+ 2	8.0	84.1
S 3+20 ⁹⁸	5.2	86.9

100' E of Sec. J

S 3+55 ⁹⁸	3.4	88.7
+ 1	6.2	85.9
cb	5.7	86.4
1/4	5.7	86.4
C 3+53 ⁵⁶	5.5	86.6
1/4	5.5	86.6
cb	4.1	88.0
N 3+51 ¹⁴	3.7	88.4

9409

125' E of Sec. J

N	3+76 ¹⁴	1.8	90.3
+1		2.8	89.3
cb		2.9	89.2
+5		3.1	89.0
1/4		4.2	87.9
c	3+78 ⁵⁶	3.7	88.4
1/4		3.7	88.4
cb		3.6	88.5
+4		4.0	88.1
S	3+80 ⁹⁸	1.3	90.8
T.P.	12.15 102.85	1.39	90.90
145.16' E of Sec. J = Sec. K.			
S	4+01 ¹⁴	10.7	92.2
+1		13.0	89.9
cb		12.5	90.4
1/4		12.6	90.3
c	3+98 ²²	12.4	90.5
1/4		13.0	89.9
+2.5		13.3	89.6
+4		12.2	90.7
cb		11.9	91.0
N	3+96 ³⁰	11.7	91.2
484' E of Sec. K on N 00° E on 5 = Sec. L.			
N	4+01 ¹⁴	11.3	91.6
cb		11.5	91.4

02.85

GLENWOOD 24

+3		11.6	91.3
+4		12.6	90.3
1/4		12.4	90.5
c	4+01 ¹⁴	12.2	90.7
1/4		12.4	90.5
cb		12.3	90.6
+4		13.0	89.9
5	4+01 ¹⁴	10.7	92.2

10.32' E of Sec. L on S 00° E on N = Sec. M.

S	4+11 ⁴⁶	10.1	92.8
+1		12.1	90.8
cb		11.8	91.1
1/4		11.7	91.2
c	4+06 ³⁰	11.7	91.2
1/4		12.5	90.4
+3		12.5	90.4
cb		11.5	91.4
N	4+01 ¹⁴	11.3	91.6

40' E of Sec. M.

N	4+41 ¹⁴	7.3	95.6
cb		7.4	95.5
+3		7.7	95.2
+4		8.9	94.0
1/4		9.2	93.7
c	4+46 ³⁰	8.6	94.3
1/4		8.4	94.5

0285

cb	8.6	94.3
+2	9.3	93.6
5 4+81 ⁴⁶	6.8	96.1

65' E of Sec. M.

3 4+76 ⁴⁶	4.4	98.5
+4	5.1	97.8
cb	7.1	95.8
1/4	5.7	97.2
C 4+71 ³⁰	5.7	97.2
1/4	6.4	96.5
+4	6.2	96.7
+6	4.6	98.3
cb	4.6	98.3
N 4+66 ¹⁴	4.2	98.7

76' E of Sec. M.

N 4+77 ¹⁴	2.7	00.2
+1	4.6	98.3
cb	4.9	98.0

76.98' E of Sec. M. = Sec. N

N 4+78 ¹²	4.5	98.4
cb	4.9	98.0
1/4	4.6	98.3
C 4+83 ²⁸	4.4	98.5
1/4	4.7	98.2
+4	5.6	97.3
+5	3.8	99.1

0285

GLENWOOD

35

cb	3.0	99.9
5 4+88 ⁴⁴	0.0	02.9

10.32' E of Sec. N on N. 00' E on S - Mt. Columbia

3 4+88 ⁴⁴	0.0	02.9
cb	2.6	00.3
+2	3.7	99.2
+3	5.3	97.6
1/4	4.3	98.6
C 4+88 ⁴⁴	3.8	99.1
1/4	3.8	99.1
cb	3.8	99.1
N 4+88 ⁴⁴	3.7	99.2

4/15/23

Gregory
Mingo
Mingo
ShawCROSS SECTION OF
POLK AVE

from E.L. 32nd to W.L. Boundary

80' wide
14' Cb's
13' 1/2's

5.28

358.32

353.04

BP SE.
Polk + 32nd

E.L. 32nd.

S	5.0	353.3
C	5.5	52.8
1/4	5.3	53.0
C	5.2	53.1
1/4	5.1	53.2
+4	6.2	52.1
+12	6.1	52.2
cb	5.5	52.9
N	4.5	53.8
10'E		
N	4.7	53.6
cb	3.7	54.6
+3	6.3	52.0
+11	6.3	52.0
1/4	4.6	53.7
C	4.3	54.0
1/4	3.7	54.6
cb	3.7	54.6
+2	4.3	54.0
S	4.4	53.9
20'E		
S	4.6	53.7
cb	4.6	53.7
+4	3.5	54.7

36

1/4

+4

C

1/4

+2

+3

+10

cb

+1

+4

N

N

+5

+12

cb

+6

+7

1/4

C

1/4

+8

+12

cb

S

3.8

4.5

4.6

4.8

4.8

6.4

6.5

4.4

3.6

3.6

5.4

45'E

6.5

5.6

5.8

8.0

8.2

5.9

5.7

5.5

5.4

5.0

5.6

6.2

6.1

354.5

53.8

53.7

53.5

53.5

51.9

51.8

53.9

54.7

54.7

52.7

51.8

52.7

52.5

50.3

50.1

52.4

52.6

52.8

52.9

53.3

52.7

52.1

52.3

= PLOTTED =

See Book 1055 for additional Polk St

358.32

65'E

S	70	51.3
cb	73	51.0
+6	59	52.4
1/4	60	52.3
C	64	51.9
1/4	67	51.6
+3	67	51.6
+5	10.0	48.3
+9	10.7	47.6
cb	10.7	47.6
+4	9.7	48.6
+8	7.0	51.3
N	7.5	50.8

82'E

N	8.0	50.3
+11	7.5	50.8
+12	9.2	49.1
cb	11.0	47.3
+10	10.7	47.6
1/4	7.4	50.9
C	7.1	51.2
+10	7.3	51.0
1/4	6.6	51.7
+8	6.4	51.9
cb	7.9	50.4

POLK

39

+1	8.5	349.8
S	8.2	50.1

100'E

S	10.5	47.8
+7	10.5	47.8
+11	8.3	50.0
cb	7.4	50.9
1/4	7.7	50.6
C	7.9	50.4
1/4	7.6	50.7
+1	7.6	50.7
+12	11.8	46.5
cb	11.3	47.0
+3	7.7	50.6
N	9.4	48.9

115.84'E - W.L. Boundary on N.

N	10.9	47.4
+9	8.9	49.4
+10	11.8	46.5
cb	12.4	45.9
+4	12.4	45.9
+9	8.2	50.1
1/4	8.0	50.3
C	8.5	49.8
+10	8.7	49.6
1/4	8.2	50.1
cb	8.8	49.5

+8	358.32	13.2	45.1
5		13.5	44.8
+10		12.8	45.5
	115.84 E on N } = W. L. Boundary St 132.71 - - - - -		
-10		14.5	343.8
5		14.5	44.0
+5		14.1	44.2
cb		10.6	47.7
+7		9.1	48.2
1/4		9.1	47.9
c		9.2	49.1
1/4		8.0	50.3
+3		8.2	50.1
+9		12.8	45.5
cb		12.8	45.5
+3		11.8	46.5
+2		9.6	48.9
N		10.9	47.4
+10		12.8	48.0
	W. cb Boundary		
N		11.4	46.9
+11		10.9	47.4
+12		12.8	45.5
cb		12.8	45.5
+9		12.2	46.1
+12		8.5	49.8
1/4		8.5	49.8
c		8.9	49.4
1/4		10.1	48.2

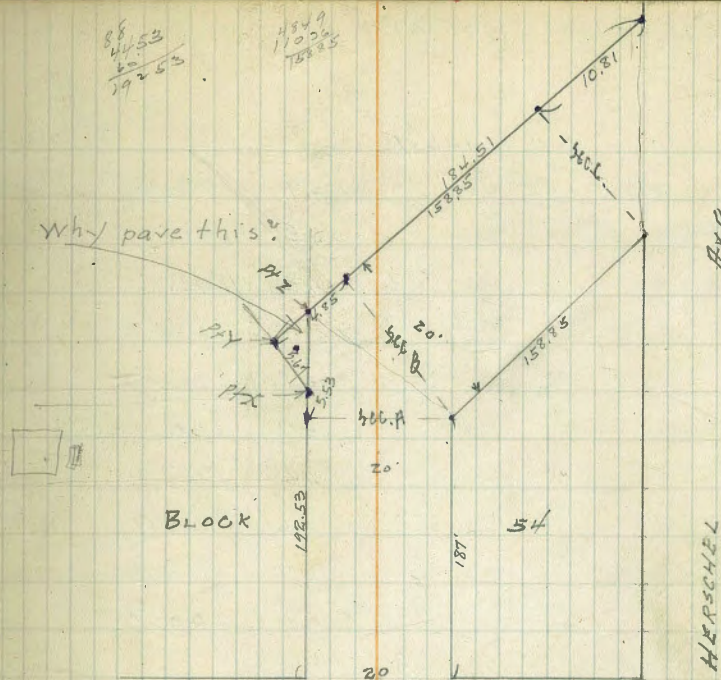
POLK.

38

+7	10.5	347.8
cb	11.2	47.1
+9	13.7	44.6
5	13.7	44.6

20' wide

Why pave this?



WALL

ST

	120' N	105' 37" 41
W	4.2	101.1
C	4.0	101.3
E	4.0	101.3
129' N = door of public garage on E		
E = Floor of Public garage	2.77	102.50
E	3.1	102.2
+7	4.0	101.3
C	4.1	101.2
W = center of door wood garage	4.3	101.0

105.77

146' N

W	4.7	100.6
C	4.3	101.0
E	4.2	101.1

787' N = Sec. A

E	4.8	100.5
C	4.7	100.6
W	4.6	100.7
PT X	4.6	100.7
PT Y	6.7	98.6
PT Z	5.1	100.2

Sec. B.

W = door of garage dirt floor	5.0	100.3
C	4.8	100.5
E	4.8	100.5

27' N = X B

E	3.6	101.7
+4	4.7	100.6
C	4.8	100.5
W = center of garage dirt floor	4.8	100.5

45' N

W	5.2	100.1
C	4.8	100.5
E	4.3	101.0

105.27

75' N

-6 = front of garage dirt floor	3.4	101.9
E	3.9	101.4
C	4.4	100.9
W	4.7	100.6

100' N

W	4.1	101.2
C	3.9	101.4
E	3.1	102.2
+8 = front of dirt floor	2.9	102.4

118' N

E	3.1	102.2
C	3.8	101.5
W	3.8	101.5
+5 = front of dirt floor	3.9	101.4

142'

-3 front of dirt floor	2.9	102.4
W	2.8	102.4
C	2.6	102.7
E	2.2	103.1

158.85 on E

169.66 on W

} = W.L. Herschel.

E	2.0	103.3
C	2.5	104.8
W	2.3	103.0

105.77

11.3 W. of W. Cb of Herschel = Inside Edge sidewalk

W	on Edge of walk.	2.40	102.87
E	- - -	2.05	103.22
E	on cement ab Ft. Allen produced 2.23		103.04
W	- - - Wt. - -	2.70	102.57

7/19/23

Gregory
1700 ft
Miller
ShawCROSS SECTION OF
19th St
from N.L. Broadway to
32nd St80' wide
14' cbs
13' / 1/2

44

7.42

96.46

89.04

BP 3W
19th St

60' N

N.L. BROADWAY

W

5.8

90.7

-10

E

12.7

84.8

cb

6.2

90.3

cb

11.3

85.2

1/4

6.8

89.7

+9

9.5

87.0

c

7.2

89.3

1/4

8.9

87.6

1/4

7.1

89.4

c

7.3

89.2

cb

6.60

89.86 encasement

1/4

7.1

89.4

E

6.6

89.9

cb

6.5

90.0

5' N

+7

5.5

91.0

E

7.6

88.9

W

4.8

91.7

cb

6.5

90.0

1.8

94.7

1/4

6.8

89.7

W

95' N

2.2

94.3

c

6.5

90.0

cb

5.8

90.7

1/4

5.1

91.4

1/4

7.1

89.4

cb

3.3

93.2

c

8.4

88.1

W

3.1

93.4

1/4

8.4

88.1

26' N

+4

8.6

87.9

W

1.1

95.4

cb

10.8

85.7

+9

3.3

93.2

E

11.8

84.7

cb

3.8

92.7

+5

13.0

83.5

1/4

5.1

91.4

W

103' N

3.6

92.9

c

6.3

90.2

cb

6.1

90.4

1/4

6.5

90.0

-5

125' N

14.8

81.7

cb

7.0

89.5

E

9.8

86.7

+15

12.0

84.5

96.46

E	14.4	82.1
cb	11.8	84.7
+10	9.7	86.8
1/4	9.7	86.8
C	9.8	86.7
+5	8.9	87.6
1/2	9.0	87.5
+10	9.2	87.3
cb	8.2	88.3
+9	5.7	90.8
W	3.2	93.3

155' N

W	5.2	91.3
cb	10.8	85.7
1/4	10.9	85.6
C	11.8	84.7
1/4	12.0	84.5
+3	12.2	84.3
cb	14.0	82.5
E	16.3	80.2
+5	16.4	80.1

175' N

-5	17.4	79.1
E	17.8	78.7
+7	17.4	79.1
co	16.2	80.3

1974

43

+9	13.6	82.9
1/4	13.8	82.7
C	13.5	83.0
1/4	12.8	83.7
cb	12.4	84.1
W	5.7	90.8

200' N

W	8.0	88.5
cb	14.9	81.6
1/4	15.6	80.9
C	16.4	80.1
+3	17.2	79.3
1/4	17.2	79.3
+3	17.0	79.5
cb	20.3	76.2
+10	20.1	76.4
E	18.9	77.6

225' N

E	19.2	77.3
+5	22.3	74.2
cb	22.3	74.2
+8	21.9	74.6
1/4	20.7	75.8
C	19.8	76.7
1/4	18.8	77.7
+9	18.3	78.2

96.46

cb			16.6	79.9
W			10.4	85.1
T.P.	0.02	8383	12.65	83.81
		250' N		
W			2.9	80.9
cb			8.6	75.2
+5			9.7	74.1
1/4			9.5	74.3
C			10.0	73.8
+4			11.6	72.2
1/4			11.2	72.6
cb			12.0	71.8
+9			11.5	72.3
E			9.5	74.3
		275' N		
E			13.0	70.8
T.P.	4.51	75.71	12.93	70.90
+4			5.8	69.9
cb			6.2	69.5
1/4			5.7	70.0
C			6.6	69.1
+3			6.0	69.7
1/4			6.3	69.4
+10			6.3	69.4
cb			4.5	71.2
W			0.0	75.71

1974.5

W

295' N

W			5.1	70.6
cb			8.5	67.2
+5			9.3	66.4
1/4			9.3	66.4
C			8.7	67.0
1/4			8.5	67.2
cb			7.9	67.8
+10			7.4	68.3
E			6.0	69.7
		300' N = SLC 5+		
E			8.0	67.7
cb			8.7	67.0
on cement cb			8.97	66.74
+3			9.4	66.3
1/4			9.5	66.2
C			9.7	66.0
1/4			10.2	64.5
cb on cement			10.75	64.96
+10			10.6	65.1
W			8.4	67.3

11/8/23

Level 3 10' 5.0' & 0' of
 Palomar from 25' E of
 W. of Electric Arc.
 to 10' E of Vista Del Mar.

0+0 Q - 25' E of W. of Electric Arc	306	83.81	80.75	Cor. of Rd. NE. Pavement to B.
+25'		1.4	82.4	
+50		1.3	82.5	
1		1.7	82.1	
+50		2.8	81.0	
2		4.0	79.8	
+40' = E. La Jolla Blvd.		5.1	78.7	
2+80' = E. edge paving		6.4	77.4	
3+01' wedge paving =		6.40	77.40	
+05		6.43	77.38	
+10		6.4	77.4	
+20		10.5	73.3	
+27.5		12.0	71.8	
+34		11.8	72.0	
+50		8.6	75.2	
4		8.8	75.0	
+50		10.1	73.7	
5		11.3	72.5	
T.P.	0.51	12.5	71.3	
+35		12.85	70.96	
+40		1.4	70.1	
+85		3.5	68.0	
6		4.4	67.1	
+50		3.8	67.7	
		4.7	66.8	

7147

45

7		7.2	64.3
+63		10.2	61.3
8		14.3	57.2
T.P.	031	12.59	58.88
+50		9.6	49.6
T.P.	075	13.03	46.16
9		5.7	42.6
+50' = 10' E. of L. of Vista Del Mar		9.5	36.8

Plotted Nov. 17, 1923
 See L 1387
 J.B.

11/8/23

Levels 10' E of L of
Vista Del Mar from 25.5 x
N.L. of Palomar to 5.5 x
L of Playa Del Sur.

46.31 HD. from page 45

0+00 = 25.5 x N.L. Palomar	9.5	36.8
+25	11.6	34.7
+50	12.8	34.1
1	13.2	33.1
TP 0.83 34.36	12.78	33.53
+50	1.7	32.7
2	1.8	32.6
+55 ± = 10.5 x L of Rosemont	2.4	32.0
3	3.0	31.4
+50	3.8	30.6
4	4.0	30.4
+50	4.6	29.8
5	4.8	29.6
+20 ± = 10.5 x L of Holmar	4.8	29.6
+50	4.8	29.6
6	5.8	28.6
+50	6.3	28.1
7	7.0	27.4
+50	7.4	27.0
+85 ± = 10.5 x L of Gravelly	6.7	27.7
8	7.0	27.4
+50	7.3	27.1
9	7.4	27.0
+50	7.6	26.9
10	7.6	26.8

7.5
2.5
10.0

2.5
2.5
2.5
34.36

46

+25 ± = 5.5 x L of Playa Del Sur 7.7 26.7

Plotted Nov 15/1923
see L 1382
N.R.B.

11/8/43 Gregory

Levels to top of
Rosemont from 10' E
at d of Vista Del Mar
to the paving on La Jolla Blvd
34.36 Ad from page 48

0+00 = 10' E of
d of Vista Del Mar

			2.4	37.0
T.P.	1292	47.01	0.07	34.29
+20			14.2	32.8
+50			11.2	35.8
1			5.8	41.2
T.P.	1258	58.94	0.65	46.36
+50			11.5	47.4
2			6.1	52.8
+50			0.1	58.8
T.P.	1291	71.50	0.15	58.79
+75			10.7	60.8
3			9.6	61.9
+50			7.3	64.2
4			5.3	66.2
+50			3.3	68.2
5			1.2	70.3
T.P.	1138	82.68	0.20	71.30
+50			10.0	72.7
6			7.6	75.1
+40 = W La Jolla Blvd			5.7	77.0
+60			4.9	77.8
+82 = Edge of paving			3.33	79.35
chk BM			1.93	80.75

plotted
11/14/43
H.R.B.
see 1319 L

✓

11/16/23

Levels 10' S. & E. of
KOLMAR ST
ST is graded & curbed

	8.87	77.73	68.86
40' E. of 0+00 = W edge of paving		1.99	75.74
0+00 = W.L. of La Jolla Blvd.		3.9	73.8
1+00		7.7	70.0
2+00		12.2	65.5
T.P.	0.23	65.12	12.84 64.89
3		3.4	61.7
4		6.8	58.3
+50		8.8	56.3
+65		10.1	55.0
T.P.	0.06	52.28	12.90 52.22
5		2.0	50.3
T.P.	0.37	40.06	12.59 39.69
6		2.9	37.2
+60± = EL Vista Del Mar		9.7	30.4
+80± = 10' E. of 60±		10.5	29.6
T.P.	12.67	41.83	10.90 29.16

Plotted
Nov 21 1923
See L 1382
H.P.B.

296

49

11/16/23 Lopez

Levels 10.5 and 6.4
Gravilla 54
X from Vista Del Mar to Blvd
Graded & Curbed
4183 x comp page 48

19

0+00 = 10' E of 6.4 Vista Del Mar	14.5	27.3
+20 = EL - - -	13.5	28.3
+65	9.7	32.1
1	6.8	35.0
T.P. 12.58 54.20 ✓	0.21	41.62
2	8.7	45.5
+59	4.0	50.2
3	2.3	51.8
T.P. 12.75 66.63 ✓	0.32	53.28
4	9.9	56.7
+40	8.0	58.6
5	5.8	60.8
6	2.2	64.4
T.P. 12.73 78.89 ✓	0.47	66.16
7	11.1	67.8
+18 ± = WL La Jolla Blvd	10.3	68.6
+58 = W. edge of paving	8.95	69.94
25		
+83		✓

Plotted
Nov 21 1923
500 L 1383
H.P.B.

11/16/23 Gregory Levels 25' E of W.L. of
Electric Ave.
from N.L. of Gravelly to Box 411

78.89 from page 49

0+00 = N.L. of Gravelly St.	2.2	76.7	3' deep
+45	2.4	76.5	
1	6.1	72.8	Grade probably 5/3' higher
+20	10.4	68.5	
+30	10.9	68.0	
+50	6.2	72.7	
+75	6.0	72.9	
2	6.6	72.3	Grade probably 3.0' higher
+50	9.4	69.5	
+80	10.2	68.7	
3	11.0	67.9	Grade probably 7' higher
+50	10.7	68.2	
4	5.6	73.3	probable grade
+10	5.0	73.9	
+35	4.9	74.0	
+80	9.6	69.3	
5	9.9	69.0	Grade probably 3.5' higher
+50	5.7	73.2	
6+00. A	4.5	74.4	
+26 = over 16" Main on Blvd.	4.8	74.1	
T.P.	1268	6621	

Plotted
Nov 19 1923
505 L 1380
XPRB.

11/10/23

Levels 5' 3.0 x 6' at
Playa Del Norte also

084	67.05	66.21	TP 2.00 m page 50
0400 = W. edge of Parking on Blvd = 15' 12" x 32' Playa Del Norte prod. E	3.33	63.72	
+4.50	3.4	63.7	
+23.0	14.6	52.5	
+32	16.4	50.7	
+40 = W. 40' 1/2' Blvd - P.C. = 15' 12" x 32' Playa Del Norte	13.4	53.7	
+50	11.6	55.5	
+65 = Graded St	5.5	61.6	
+80	6.0	61.1	
1+09.34 = P.R.C.	7.0	60.1	
+50	3.3	58.8	
2	10.7	56.4	
+23.64 = E.C.	11.5	55.6	
+58.64 = P.C.	12.6	54.5	
T.P. 0.20 54.22	13.03	54.02	
3	1.4	52.8	
+50	2.4	51.8	
4	4.1	50.1	
+05.91 P.R.C. 3+11.71	4.2	50.0	
+50	5.6	48.6	
5	6.8	47.4	
+17	7.5	46.7	
+32.01 = E.C.	9.3	44.9	6' 1/2" 1.6' higher 1' 2" 4.4' lower 3' 1/2" 6.0' V 6' 1/2" 2.0' higher
+55	9.1	45.1	
6 + 00.01 = P.C.	8.6	45.6	
+50	10.4	43.8	
7 + 00	12.5	41.7	

Note
Profile to be
taken from here
ice pool 100 ft. 75-

TP 04.4	42.11	12.55	41.67
7+06.39 = E.C.		0.6	41.5
7+76.39 = P.C.		4.0	38.1
+95		3.4	36.7
8		6.2	35.9
+16		11.2	30.9
T.P. 004	29.47	12.68	29.43
+30		5.8	23.7
+50		6.0	23.5
+92.43 = E.C.		7.0	22.5
TP 438	30.82	3.03	26.42
9+18 = 6" Sewer pipe H=5		5.98	24.84
+15		9.6	21.2
(+15 20' Hot Line		1.1)	29.7
+34.93 = P.C.		9.2	21.6
+55		9.9	20.9
+65		6.3	24.5
+76 = Wall of Bldg.		5.9	24.9
10 13 under Bldg			
+13.8 = Wall of Bldg.		5.7	25.1
+40.05 = E.C.		6.2	24.6
+80.05 = P.C.		10.2	20.6
11		11.0	19.8
+50		12.5	18.3
T.P. 9.83	28.20	12.45	18.37
12		10.9	17.3

See New Notes

10' N =
3.5' higher20' N =
11.5' higher30' N =
10' higherTop of pipe
groundgrade
= approx 1

2820 ✓

+05	10.9	17.3
+15	15.1	13.1
+25	11.1	17.1
+47.72 = E.C. = 12 + 13.52	10.8	17.4
13+06	10.5	17.7
+20 control wash bad one	19.2	9.0
+38.07 = P.C. = 13 + 05.87	13.3	14.9
+46 = another wash	17.2	11.0
+50	10.3	17.9
14	8.8	19.4
+36 ± = E.C. = 14 + 04.04	8.0	20.2
+63.5 = P.C. = 14 + 31.54	7.1	21.1
15 16	5.5	22.7
+50 → 15 + 18.61	3.0	25.2
+83 ± = 10' E. of d. of Vista Dell'Ar	1.6	26.6
	0.27	27.93

See New Notes

✓

11/16/23

Levels 5' 5.0x 2.0x
Playa Del Sur from
10' E of 2 Del Mar to
La Jolla Blvd
Graded & Curbed

53

	1245	40.38	27.93	T.P. on page 54
0 to 10' E of 2 Del Mar		13.8	26.6	
+20		13.5	26.9	
+43.5 [±] = P.C.		12.1	28.3	
1		7.2	33.2	
+50		2.9	37.5	
T.P.	1280	52.49	0.49	39.89
2		12.6	40.1	
+50		9.9	42.8	
3		7.8	44.9	
+50		5.9	46.8	
4		4.7	48.0	
+50		3.4	49.3	
5		1.7	51.0	
+50		0.0	52.7	
	1284	64.76	0.77	51.92
6		10.3	54.5	
+50		8.1	56.7	
7		5.5	59.3	
+50		2.8	62.0	
8		0.2	64.6	
T.P.	5.47	70.16	0.07	64.69
+20		3.7	66.5	
+26 [±] = W Edge Pav		3.84	66.32	
25 C.M. B.M.		1.24	68.92	786
8+51				

Platted
Nov 22 1923
500' L
M.R.B.

54

5 + 55.48

5 + 20.48

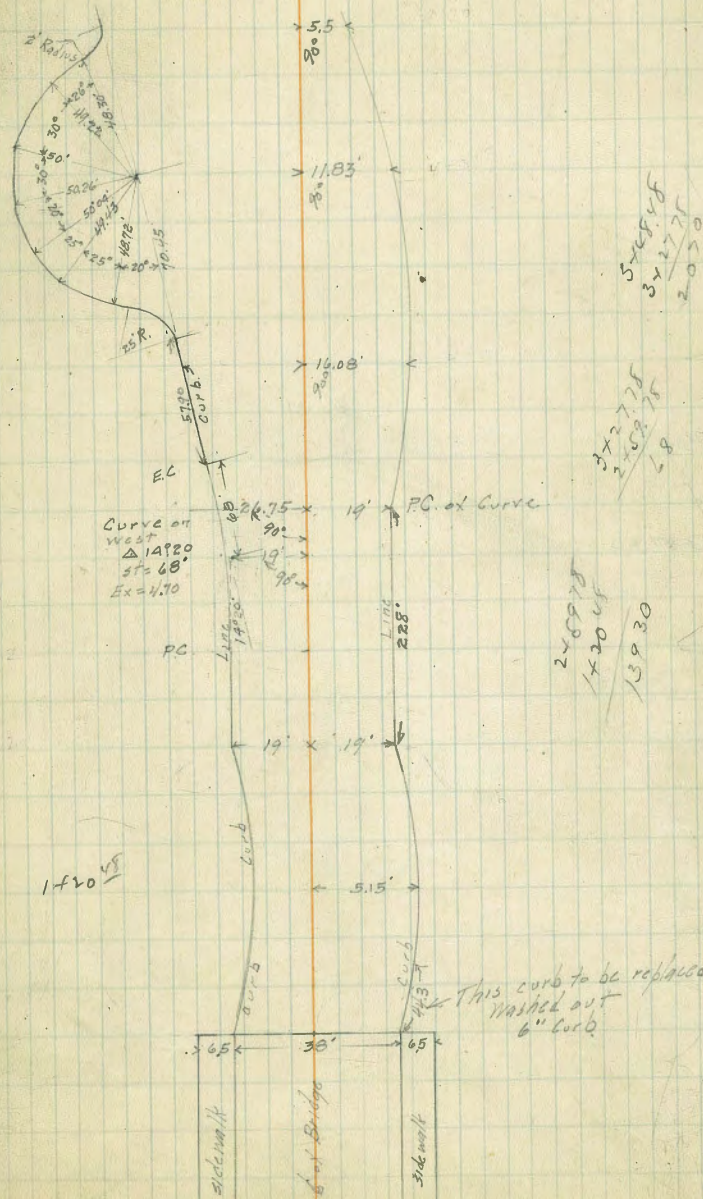
 $4 + 68.96 = PC \text{ of Curve on East Curb}$

4+48.26 PI on West Curb.

$3 + 80.26 =$ P.C. of Curve on West Curb

$1 + 20.48 \Delta 31^{\circ}00$ Left. $\left\{ \begin{array}{l} P = \\ st = 120.48 \\ G = \end{array} \right.$

0400



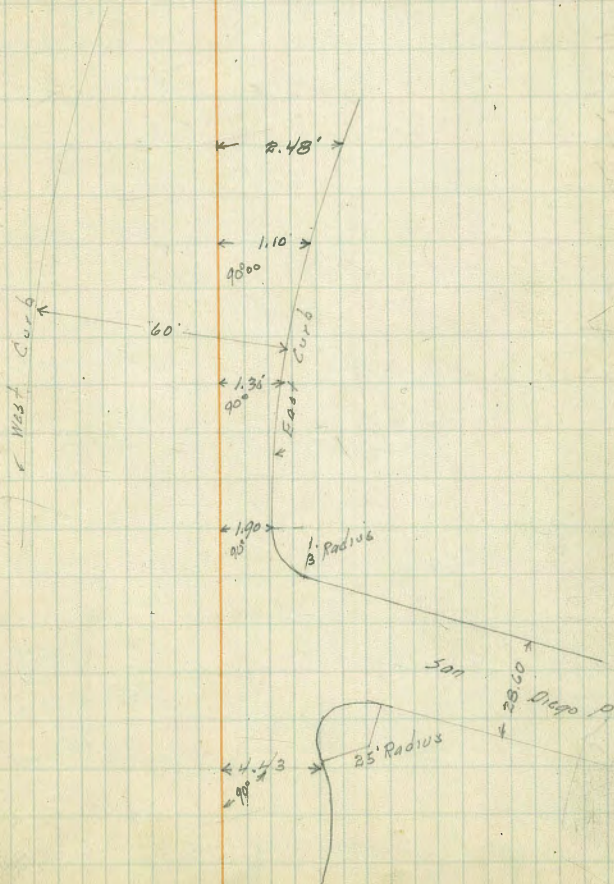
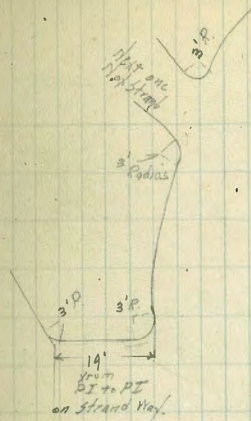
8+20.48

7+70.48

7+20.48

6+97.78

6+37.78 = PC into St. on East San Diego Place.



1/7/24 Gregory, CROSS SECTION OF
The Rock Fill on
MISSION Blvd
N. of Bridge

Distances are all taken on E. Curb Line

1.44 7.94
N. end of Bridge = 0+00

E. cb Line 1.4 6.5
0.5' E 2.4 5.5
6.5' = wood bulkhead 4.0 3.9

0+26

E cb Line (Curb gone) 2.1 5.8
0.2' E 3.1 4.8
1' ✓ 5.1 2.8
6.5 ✓ 6.8 1.1
20 ✓ 10.3 -2.4
29.5 ✓ = wood bulkhead 13.4 -5.5

0+50

E cb Line on cement 2.7 5.2
1' E 4.2 3.7
7' ✓ 7.4 0.5
20 ✓ 10.5 -2.6
30.6 ✓ = wood bulkhead 16.3 -8.4

0+75

E cb Line on Cement 3.5 4.4
1' E 4.0 3.9
7' ✓ 6.9 1.0
20 ✓ 11.4 -3.5
30.3 ✓ = wood bulkhead 18.2 -10.3

on cb at
N. end Bridge

6.5

E cb Line (on cement)

7' E

12' ✓

19' ✓

22' ✓

29.5' = wood bulkhead

0+85

3.8 4.1

4.6 3.3

5.0 2.9

10.4 -2.5

11.4 -3.5

15.8 -7.9

1+00

E cb Line (on cement)

10' E

17' ✓

23' ✓

30.7' = wood bulkhead

4.3 3.6

4.3 3.6

7.4 0.5

12.1 -4.2

16.2 -8.3

1+25

E cb Line (on cement)

8' E

18' ✓

26' ✓

30.5' = wood bulkhead

5.0 2.9

5.8 2.1

11.5 -3.6

13.5 -5.6

16.1 -8.2

1+50

E cb Line (on cement)

5' E

16' ✓

wood bulkhead gone

5.7 2.2

6.1 1.8

11.3 -3.4

14.3 -4.4

Plotted Jan 8 1924

ARB

340
1357
1697

7.94

1+75

E cb Line (on cement)	6.2	1.7
3.5' E	6.6	1.3
8' ✓	9.9	-7.0
16' ✓	12.3	-4.4
30' ✓	14.5	-6.6

2+00

E cb Line (on cement)	6.6	1.3
5' E	9.4	-1.5
8' ✓	7.8	+0.1
15' ✓	12.3	-4.4
25' ✓	14.3	-6.4

2+25

E cb Line (on cement)	6.7	+1.2
6' E	8.4	-0.5
7' ✓	7.3	+0.6
15' ✓	12.0	-4.1
26' ✓	14.3	-6.4

2+50

E cb Line (on cement)	6.8	+1.1
6' E	8.9	-1.0
8' ✓	8.3	-0.4
15' ✓	12.3	-4.4
23' ✓	13.6	-5.7
30' ✓	18.0	-10.1
T.P.	3.99	6.85 + 10.9

2.90

3.99

6.85 + 10.9

399

57

3+00

E cb Line (on cement)	3.2	+0.8
8' E	5.7	-1.7
15' ✓	9.1	-5.1
25.3' ✓ = wood bulkhead	12.9	-8.9

3+50

E cb Line (on cement)	3.6	+0.4
8' E	3.7	+0.3
9' ✓	5.0	-1.0
16' ✓	8.5	-4.5
26' ✓ = wood bulkhead	10.0	-6.0

4+00

E cb Line on cement	3.8	+0.2
8' E	3.8	+0.2
13' ✓	7.0	-3.0
20' ✓	8.1	-4.1
27' ✓ = wood bulkhead	10.4	-6.4

4+50

E cb Line (on cement)	4.2	-0.2
14' E	3.9	+0.1
18' ✓	7.6	-3.6
29' ✓ = wood bulkhead	9.1	-5.1

5+00

E cb Line (on cement)	4.4	-0.4
12' E	4.2	-0.2
17' ✓	7.3	-3.3
31.5' ✓ = wood bulkhead	11.1	-7.1

399

5+35 This section is on shore line
PTok₁

Ecb Line (on cement)	4.6	- 0.6
10' E	4.7	- 0.7
13' ✓	7.2	- 3.2
32.5' ✓ = wood bulkhead	7.6	- 3.6

5+50

Ecb Line (on cement)	4.7	- 0.7
4' E	4.7	- 0.7
16' ✓	3.0	+ 1.0
18' ✓	6.4	- 2.4
32.8' ✓ = wood bulkhead	7.2	- 3.2

5+75

Ecb Line (on cement)	4.9	- 0.9
8' E	4.6	- 0.6
17' E	6.0	- 2.0
33.4' ✓ = wood bulkhead	6.5	- 2.5

6+00

Ecb Line (on cement)	5.0	- 1.0
6' E	4.9	- 0.9
26' ✓	4.4	- 0.4
28' ✓	5.9	- 1.9
35' ✓ = wood bulkhead	6.4	- 2.4

shore line

Jan. 9. 1924
H.B.

Plotted



58

Additional sections
at Bridge on 65th St.

4.34

217.14

21280

1 + 90.3 = 1/2 side of S. bulkhead

4' No. 1

8.7

8.4

8' - - -

8.2

8.9

10' - - -

5.5

11.6

15' - - -

5.8

11.3

80' wide Sec 5th St from S. Line of Arbor Drive 1/5/25
 14' Ck 235' South to Canon
 13' 1/4

B.M.	5.59	294.62	289.03	SE. 7 th Ark 4 th Arbor
I.P.	2.95	293.48	4.09	290.53 B.P. N.W. cor 5 th 4 th Arbor
00 = S. line Arbor Drive				
E		3.7	289.8	
eb		4.1	289.4	
1/4		3.7	289.8	
e		3.1	290.4	
1/4		3.5	290.0	
cb		3.3	290.2	
w		3.1	290.4	
2' S				
w		2.7	290.8	
+12		2.4	291.1	
eb		3.3	290.2	
1/4		3.5	290.0	
c		3.1	290.4	
1/4		3.7	289.8	
cb		4.1	289.4	
+12		3.7	289.8	
E		3.0	290.5	
30' S				
E		3.3	290.2	
+1		3.3	290.2	
+3		4.4	289.1	
cb		4.4	289.1	
+6		4.4	289.1	

293.48

60

44	3.6	289.9
c	3.4	290.1
1/4	3.7	289.8
cb	3.9	289.6
+2	2.2	291.3
w	2.6	290.9
50' S		
w	3.3	290.2
+11	3.3	290.2
cb	4.3	289.2
1/4	4.1	289.4
c	3.9	289.6
1/4	4.2	289.3
cb	4.4	289.1
+10	4.4	289.1
+13	3.5	290.0
E	3.5	290.0
67' S		
E	2.5	291.0
+1	2.5	291.0
+3	4.2	289.3
cb	4.6	288.9
1/4	4.3	289.2
c	4.3	289.2
1/4	4.4	289.1
cb	4.8	288.7

293.48

67'S (con)

+4	3.5	290.0
W	3.6	289.9

90'S

W	4.1	289.4
+10	4.3	289.2
cb	4.7	288.8
1/4	4.5	289.0
C	4.5	289.0
1/4	4.6	288.9
cb	4.6	288.9
+9	4.7	288.8
E	4.1	289.4

115'S

E	4.0	289.5
cb	4.3	289.2
1/4	4.4	289.1
C	4.3	289.2
1/4	4.7	288.8
cb	4.8	288.7
W	4.7	288.8

140'S

W	5.9	287.6
cb	5.7	287.8
1/4	5.1	288.4
C	4.7	288.8
1/4	4.8	288.7

293.48

5th ST

61

cb	4.7	288.8
E	4.6	288.9

170'S

E	5.5	288.0
cb	5.3	288.2
1/4	5.3	288.2
C	5.4	288.1
1/4	5.7	287.8
cb	6.0	287.5
W	6.1	287.4

200'S

W	6.8	286.7
cb	6.7	286.8
1/4	6.3	287.2
C	6.2	287.3
1/4	6.3	287.2
cb	6.4	287.1
E	6.4	287.1

222'S

E-5	9.9	283.6
E	7.2	286.3
cb	7.1	286.4
1/4	7.1	286.4
C	7.4	286.1
1/4	7.4	286.1
cb	7.2	286.3
W	7.3	286.2

293.48

228'S

W-5	7.8	285.7
W	8.1	285.4
cb	7.8	285.7
1/4	4.6	284.9
C	8.7	284.8
1/4	8.9	284.7
+7	7.8	285.7
cb	7.6	285.9
+11	7.9	285.6
E	9.8	283.7
+5	11.5	282.0

235'S

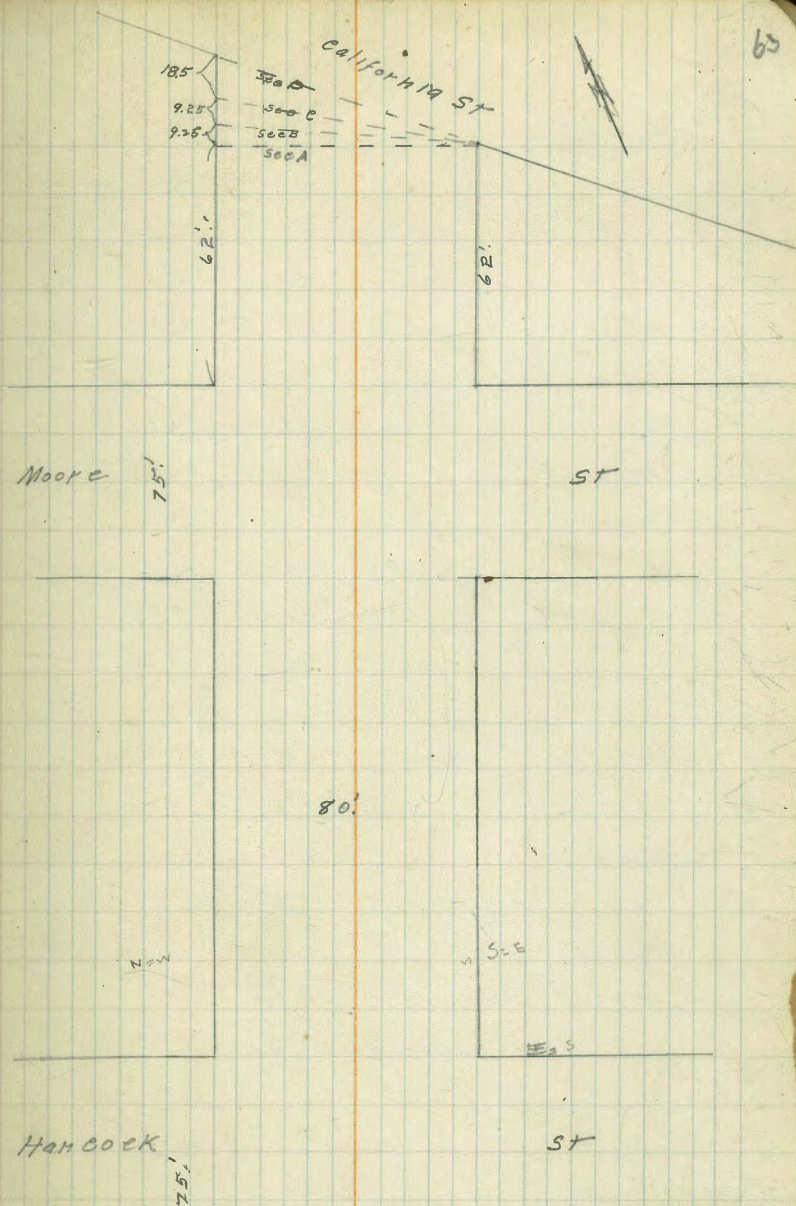
-5	14.7	278.8
E	11.6	281.9
+10	10.4	283.1
cb	10.8	282.7
1/4	11.9	281.6
C	12.6	280.9
1/4	11.6	281.9
+7	11.0	282.5
cb	9.8	283.7
W	10.0	283.5
+5	11.2	282.3

535T

62

80' wide & See Clayton St from E. line of Hancock 1/3/26
14' c/s To W. line California Miller
13' $\frac{1}{4}$ Shaw
Ch

B.M.	2.55	41.27 00 = E. Line Hancock	38.72
S		10.0	31.27
cb		11.0	30.3
1/4		10.8	30.5
C		10.7	30.6
1/4		10.7	30.6
cb		10.9	30.4
N		10.7	30.6
		4'E	
N		10.5	30.8
cb		10.3	31.0
1/4		10.4	30.9
C		10.5	30.8
1/4		10.6	30.7
+7		10.6	30.7
+10		12.8	28.5
cb		11.8	29.5
+2		8.9	32.4
S		8.1	33.2
		13'E	
S		8.2	33.1
+11		8.5	32.8
cb		9.9	31.4
1/4		10.1	31.2
C		10.0	31.3
1/4		9.6	31.7



	41.27	
	13'E @ 0W	
cb	10.0	31.3
N	10.1	31.2
	50'E	
N	8.1	33.2
cb	8.0	33.3
1/4	7.4	33.9
c	7.7	33.6
1/4	7.7	33.6
cb	8.0	33.3
+3	6.5	34.8
S	6.1	35.2

	100'E	
S	2.9	38.4
cb	2.9	38.4
1/4	4.3	37.0
c	4.0	37.3
1/4	4.3	37.0
cb	4.5	36.8
N	4.9	36.4

	115'E	
N	2.7	38.6
cb	3.2	38.1
1/4	3.0	38.3
c	2.8	38.5
+10	3.1	38.2
1/4	2.5	38.8

	46.27	
cb		1.6 39.7
S		1.6 39.7
	135'E	
S		0.2 41.1
cb		0.3 41.0
1/4		0.5 40.8
c		1.1 40.2
1/4		1.4 39.9
cb		1.9 39.4
N		1.8 39.5
T.P	12.85 53.86	0.26 41.01

	165'E	
N		11.8 42.1
cb		11.9 42.0
1/4		11.5 42.5
c		11.3 42.6
1/4		10.9 43.0
cb		10.5 43.4
S		10.2 43.7

	200'E = W. Line Moore 75' wide 12' cbs 12.75' 1/4	
S-S		5.8 46.1
S		7.3 46.6
cb		7.7 46.2
1/4		7.8 46.1
c		7.6 46.3
1/4		8.3 45.6

Clayton St

64

53.86

200 W (con)

cb	8.5	45.4
N	8.7	45.2
+5	8.8	45.1
	9'E	
N-5	7.8	46.1
N	7.8	46.1
cb	7.7	46.2
1/4	7.5	46.4
c	6.5	47.4
1/4	6.9	47.0
cb	5.7	48.2
S	5.5	48.2
	W. cp.	
S	5.0	48.9
cb	5.4	48.5
1/4	6.2	47.7
c	6.2	47.7
1/4	7.0	46.9
cb	7.1	46.8
N	6.5	47.4
	W 1/4	
N	6.0	47.9
cb	5.9	48.0
1/4	6.0	47.9
c	5.7	48.2
1/4	5.4	48.5

Clayton St.

65

53.86

cb	5.1	48.8
S	5.1	48.8
	2.75'E of W 1/4 = W. Edge Pavement	
S	5.31	48.25 on paving
E	5.68	48.18 " "
N	5.92	47.94 " "
	8'E. of E. Moore St on wedge temporary Pavement Put down by Oil Station	
N	5.93	47.93 " "
E	5.68	48.18 " "
S	5.20	48.66 " "
	E 1/4	
S	4.8	49.1
cb	5.0	48.9
1/4	5.2	48.7
c	5.2	48.7
1/4	5.3	48.7
cb	5.6	48.3
N	5.7	48.2
	6'E. of E. 1/4	
N	5.2	48.7
cb	5.5	48.8
1/4	4.9	49.0
c	5.0	48.9
1/4	4.8	49.1
cb	4.5	49.4
S	4.1	49.8

53.86
E. Eb Moore St

S	3.4	50.5
cb	3.8	50.1
1/4	3.9	50.0
c	4.2	49.7
1/4	4.3	49.6
cb	4.7	49.2
+6	4.3	49.6
N	2.7	51.2

00=E Line Moore St

N	2.0	51.9
cb	3.2	50.7
1/4	2.9	51.0
c	2.5	51.4
1/4	1.4	52.5
cb	0.9	53.0
S	1.0	52.9

3'E

S	0.4	53.5
cb	0.4	53.5
1/4	0.7	53.2
c	2.2	51.7
1/4	2.8	51.1
cb	2.8	51.1
N	1.3	52.6
T.P.	8.55	61.39
	1.02	52.84

61.39
25'E

Clayton St

66

N	7.4	54.0
cb	8.3	53.1
1/4	8.2	53.2
c	7.9	53.5
1/4	7.7	53.7
cb	7.2	54.2
S	7.1	54.3

48'E

S	5.4	56.0
cb	5.7	55.7
1/4	6.0	55.4
c	5.5	55.9
1/4	6.0	55.3
cb	6.1	55.3
N	5.5	55.9

54'E

N	2.7	58.7
+9	3.7	57.7
cb	5.3	56.1
1/4	5.5	55.9
c	5.0	56.4
1/4	5.0	56.4
+5	5.7	55.7
cb	5.3	56.1
S	5.0	56.4

61.39

62.8 = Sec A sec P. 63

S	4.5	56.9
eb	5.0	56.4
1/4	4.4	57.0
e	4.3	57.1
1/4	4.7	56.7
eb	4.5	56.9
1/4	2.4	59.0
N	2.0	59.4

Sec B

N	1.1	60.3
1/4	2.3	59.1
eb	3.9	57.5
1/4	4.2	57.2
e	4.0	57.4
1/4	4.2	57.2
eb	4.8	56.6
S	4.5	56.9

Sec C

S	4.5	56.9
eb	4.6	56.8
1/4	3.9	57.5
e	3.4	58.0
1/4	3.5	57.9
eb	3.0	58.4
1/4	1.5	59.9
N	1.30	60.1

61.39

Sec D

N	1.2	60.7
eb	1.34	60.05 one element eb
1/4	2.1	59.3
1/4	2.6	58.8
e	3.0	58.4
1/4	3.6	57.8
eb	4.3	57.1
S	4.5	56.9
A.P.	0.83	60.56

Clayton St

M

Moore
Proctor
Walker
5/5/25

CROSS SECTION of 31 ST
S.L. of THORN to 350' South

65' wide
10' cbe
11.25 1/45

321.13

68

ON BHP NW 2.5 321.13 321.1 318.98 Thorn + 31.07

S.L. Thorn = 0 + 0.0

W on Cor. Return

cb cem. cb

+1

1/4

e

1/2

+10

cb concrete

E Cor Return

15' S

E

+ 2.5 E edge of S/W

+ 7.5 W edge of S/W

cb

1/2

1/2

1/2

cb

+ 2.5 E edge of S/W

+ 7.5

W on Lateral

25' S

W

+ 2.5 W edge of S/W

+ 7.5 E edge of S/W

cb

1/2

1/2

1/4

cb

+ 2.5 W edge of S/W

+ 7.5 E

E on Lateral

60' S

cb

+ 2.5 E edge of S/W

+ 7.5 W edge of S/W

cb

1/2

1/2

1/2

cb

+ 2.5 E edge of S/W

+ 7.5 W edge of S/W

W on Lateral

75' S

W

+ 2.5 W edge of S/W

+ 7.5 E

cb

321.1

3.55

3.7

3.1

2.7

2.8

2.1

2.60

2.50

1.1

3.2

3.75

3.96

3.1

3.6

3.8

4.3

5.1

4.93

4.85

4.7

5.1

5.25

5.55

6.0

317.58

317.4

318.0

318.4

318.3

318.7

318.33

318.6

319.7

317.9

317.38

317.17

317.7

317.5

317.3

316.8

315.9

316.20

316.28

316.4

316.0

315.68

315.58

315.1

constructed

S end of S/W on East - North

321.13

+5	5.2	315.9✓
1/2	4.8	316.3✓
c	4.4	316.7✓
1/2	4.2	316.9✓
cb	3.8	317.3✓
+3	3.3	317.8✓
+7	3.2	317.9✓
E	2.2	318.9✓

100' S = S end of slw on West ^{No cb} constructed
 55 wide
 E on S edge of Conn Drive to garage

cb	2.60	318.53✓
1/2	3.9	317.2✓
c	4.7	316.4✓
1/2	5.0	316.1✓
+6	5.5	315.6✓
cb	5.8	315.3✓
+2.5 E edge of slw	6.4	314.7✓
+7.5 W ✓ ✓ ✓	6.55	314.58✓
W on tower	6.42	314.71✓
	6.0	315.1✓

110'S

W	6.5	314.6✓
cb	6.3	314.8✓
1/2	5.6	315.5✓
c	5.2	315.9✓
1/4	4.8	316.3✓
cb	4.0	317.1✓

321.13

31.07

69

E	3.1	318.0✓
125'S		
E	3.6	317.5✓
cb	4.2	316.9✓
1/2	5.2	315.9✓
c	5.5	315.6✓
1/2	6.2	314.9✓
cb	6.9	314.2✓
W	6.8	314.3✓

150'S

W	7.5	313.6✓
cb	7.5	313.6✓
1/2	6.8	314.3✓
c	5.7	315.4✓
1/2	5.6	315.5✓
cb	5.0	316.1✓
E	4.0	317.1✓

175'S

E	4.8	316.3✓
cb	5.6	315.5✓
1/2	6.1	315.0✓
c	6.9	314.2✓
1/2	7.7	313.4✓
cb	8.2	312.9✓
W	8.2	312.7✓

321.13

200'S

W	8.8	312.3✓
Ob	8.6	312.5✓
1/4	8.4	312.7✓
C	7.8	313.3✓
1/4	6.8	314.3✓
Ob	6.1	315.0✓
E	5.4	315.7✓

216'S on W.L. = E of Cent steps to Residence

16' W Street on Lower step 8.62 312.51✓

225'S

E	5.9	315.2✓
Ob	6.8	314.3✓
1/4	7.5	313.6✓
C	8.5	312.6✓
1/4	9.2	311.7✓
Ob	9.2	311.7✓
W	9.1	312.0✓

250'S

W	10.2	310.9✓
Ob	10.3	310.8✓
1/4	10.1	311.0✓
C	9.2	311.7✓
1/4	8.3	312.8✓
Ob	7.2	313.7✓
E	6.8	314.3✓

321.13

275'S

E	7.1	314.0✓
Ob	8.1	313.0✓
1/4	8.9	312.2✓
C	9.9	311.2✓
1/4	10.6	310.5✓
Ob	10.8	310.3✓
W	11.0	310.1✓

283.35 E of Cent steps on W.L.

To Residence

47' W Street on Lower step 11.0 310.1✓

T.P. 421 314.72 10.65 310.48✓

300'S

-1E	13.8	300.9✓
W	5.9	308.8✓
Ob	5.2	309.5✓
1/4	4.6	310.1✓
C	4.2	310.5✓
1/4	3.2	311.5✓
Ob	2.4	312.3✓

+5 St. Cent Approx to Auto Drive 1.47 313.25✓

E Fly off at E.L. 0.52 314.20✓ 7' wide

E.L. 1.1 313.6✓ for yardage

320'S

E	2.0	312.7✓
Ob	2.8	311.9✓
1/4	3.4	311.3✓
C	4.2	310.5✓

314.72

1/4	4.9	309.8✓
cb	6.0	308.7✓
+5	6.0	308.7✓
W	9.1	305.6✓
+15	16.0	298.7✓

325'S

-15	17.8	296.9✓
-5	13.3	301.4✓
W	11.4	303.3✓
+5	8.3	306.4✓
cb	7.5	307.2✓
+6	5.8	308.9✓
1/4	4.8	309.9✓
C	4.1	310.6✓
1/4	3.6	311.1✓
cb	2.9	311.8✓
E	2.1	312.6✓

340'S

E	2.5	312.2✓
cb	3.2	311.5✓
1/4	4.0	310.7✓
C	4.6	310.1✓
1/4	6.9	307.8✓
cb	11.5	303.2✓
W	14.7	300.0✓
+20	23.6	291.1✓

314.72

31.07

71

350'S

-20	25.0	289.7✓
W	16.1	298.6✓
cb	12.3	302.4✓
+5	10.6	304.1✓
1/4	6.3	308.4✓
C	4.5	309.2✓
1/4	4.3	310.4✓
cb	3.4	311.3✓
E	2.7	312.0✓

T.P. 744

320.86

1.30

313.42

check to em.

1.88

318.98

318.98

For Note South SEC No 1141 Page 16

318.98

7788
850
8638

21280
434
217.14

5
26
60
95
117
125
150
180
200
220
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260
280
300

7139 30
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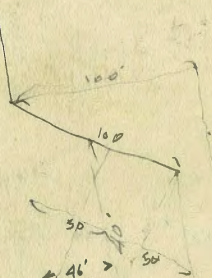
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923
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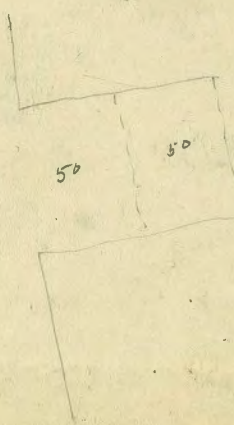
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847
847
923
923

419
839
22



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1053

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22800



51

37.5
10
27.5
24.75
2.75

1275
24

99
37
62

345
207
32778

25978
12045
38026
68
44826

86
83.9

53
81.1

37
82

34848
32778
12045
44826

80.04
1201
9209

869

92.1
80
83.1

61

81.8

81.2

455
81.83

5.1
81.3

46896

46890
12045

470
12045

