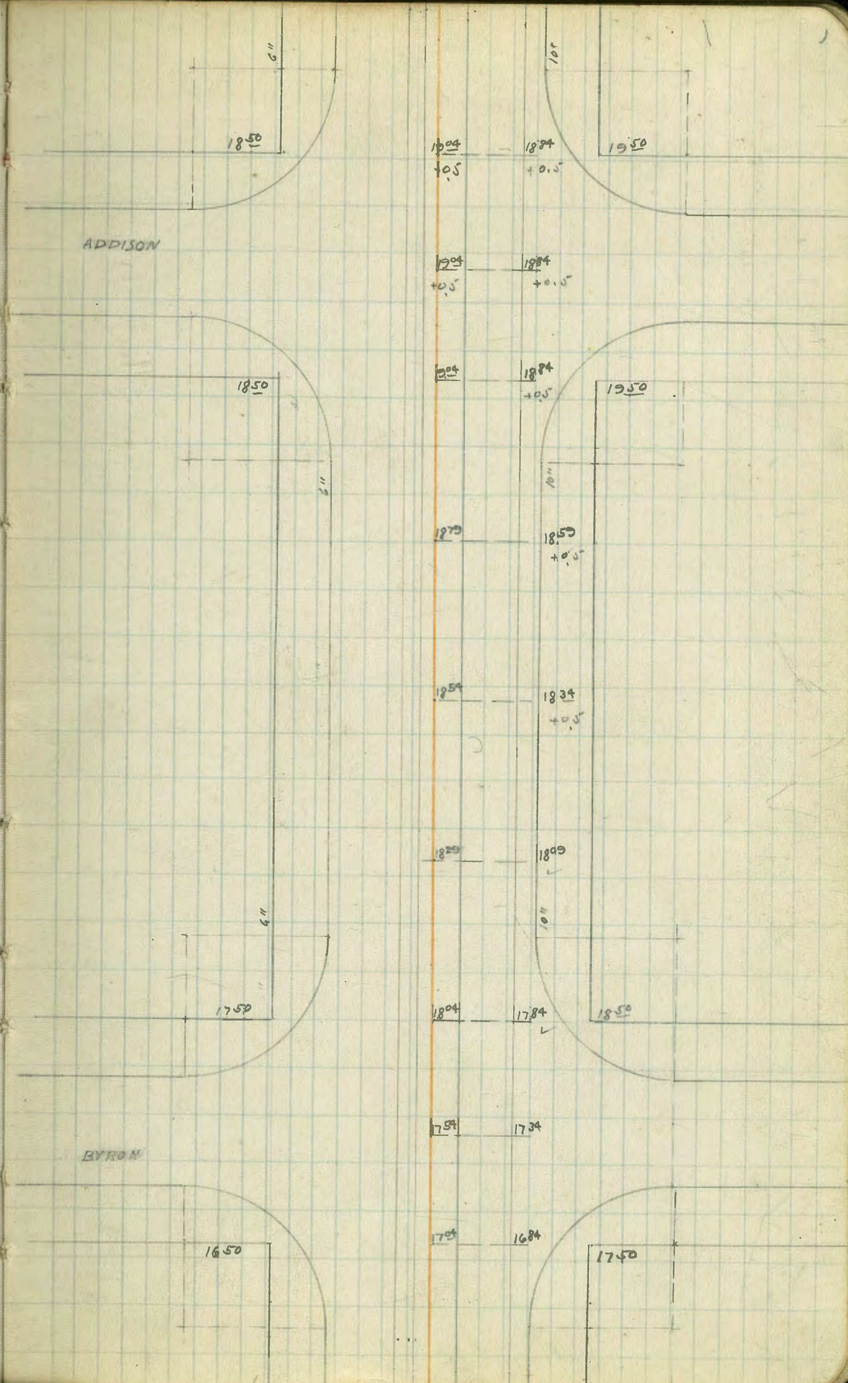
1097

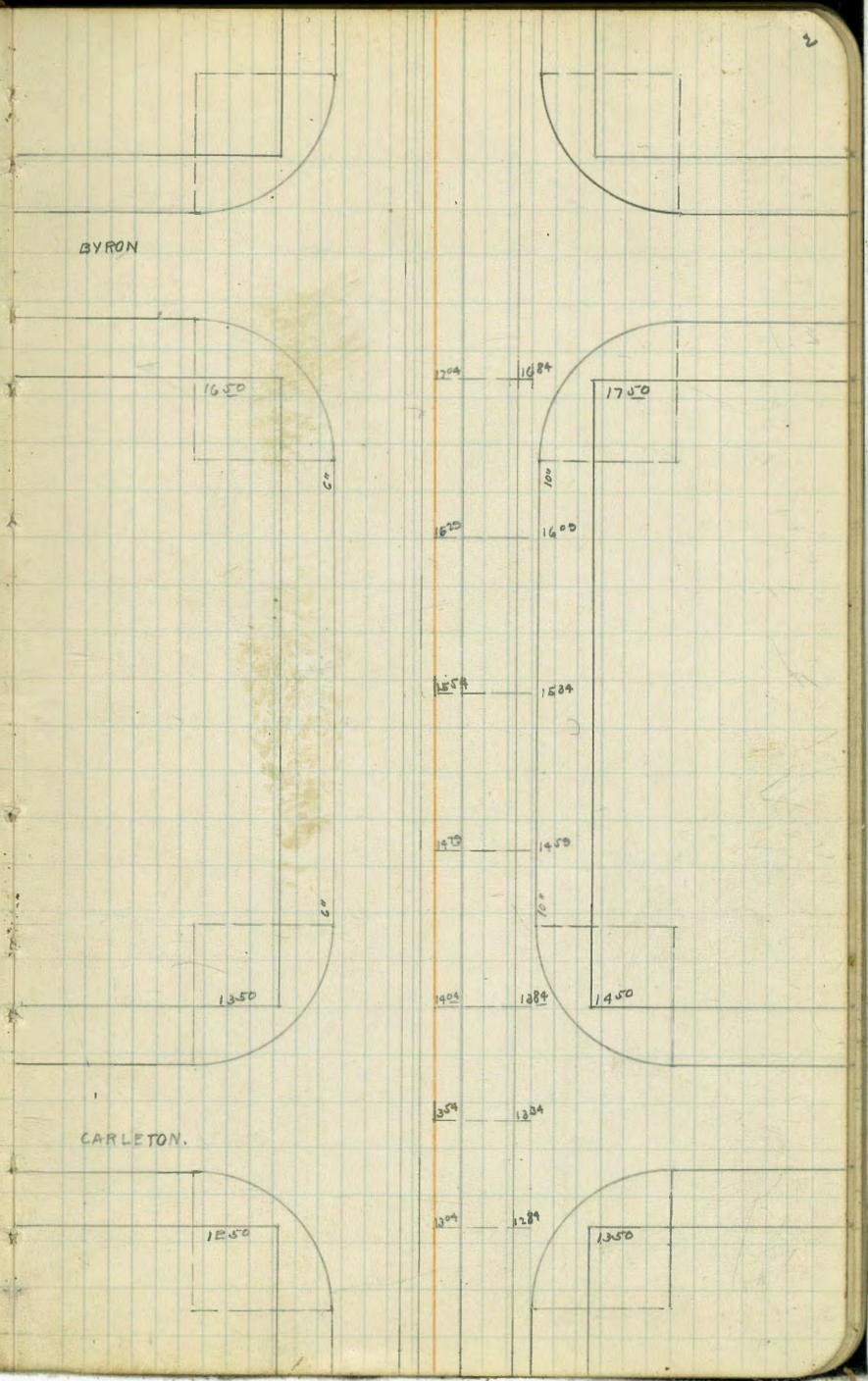
FILE BOOK

1097


6"
18 50
10"
19 50
19 04 +0.5
18 84 +0.5
ADDISON
19 04 +0.5
18 84 +0.5
19 04
18 84 +0.5
18 50
19 50
6"
10"
18 79
18 59 +0.5
18 54
18 34 +0.5
18 29
18 09
6"
10"
17 50
18 04
17 84
18 50
17 54
17 34
BYRON
17 04
16 84
16 50
17 50

21.33
17.04
4.29

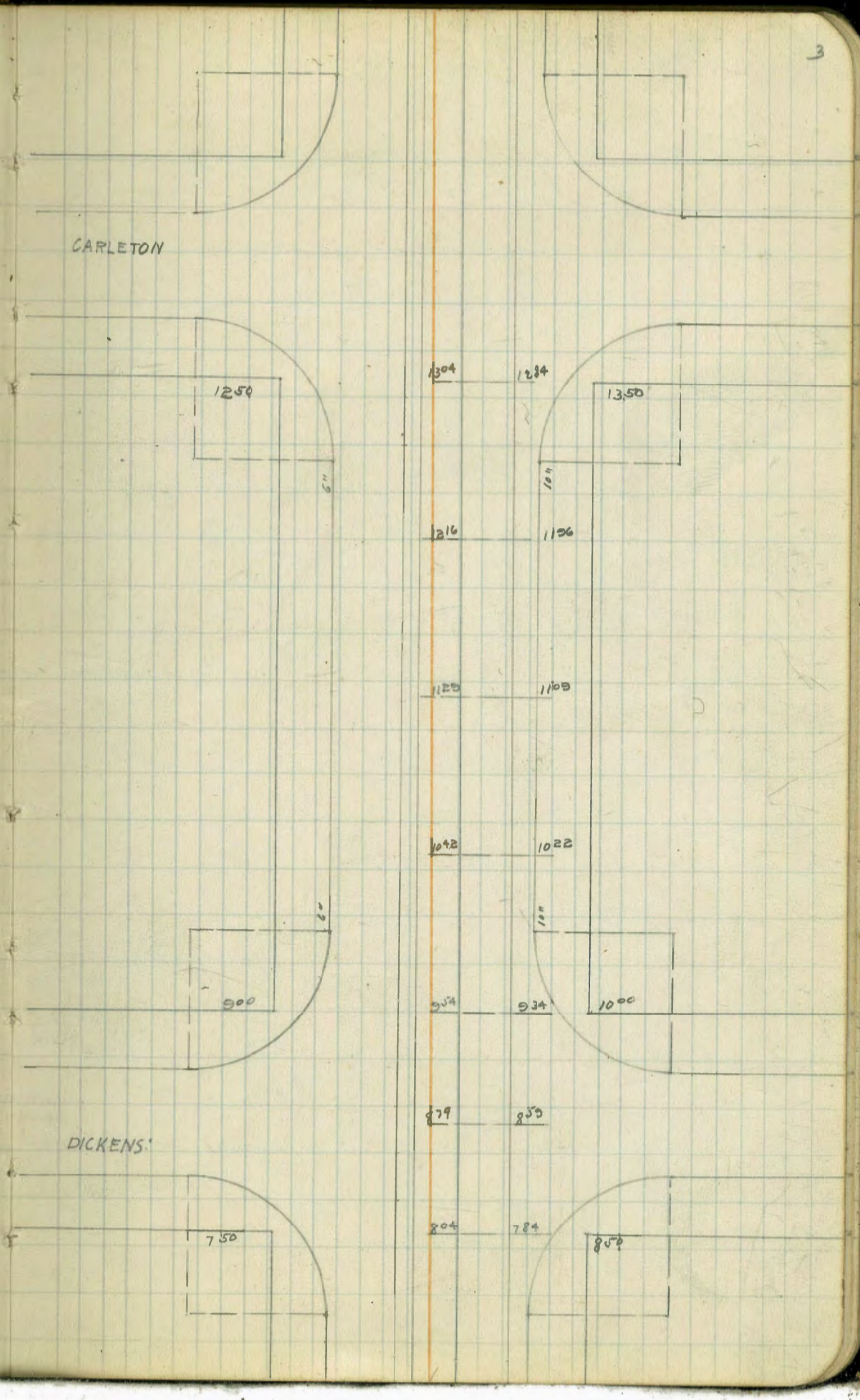
BM 16.55	21.33	21.33	21.33	21.33	21.33	21.33
6.78	17.04	15.29	15.54	14.79	14.04	13.54
21.33 ℄	4.29	6.04	5.79	6.54	7.29	7.79
	+0.5	+0.5	+0.5	(6.24)	(6.99)	
	4.49	6.24	5.99	6.74	7.49	7.99



16.12
12.04
2.08
2.78

14.55 BM
1.07
16.12 π

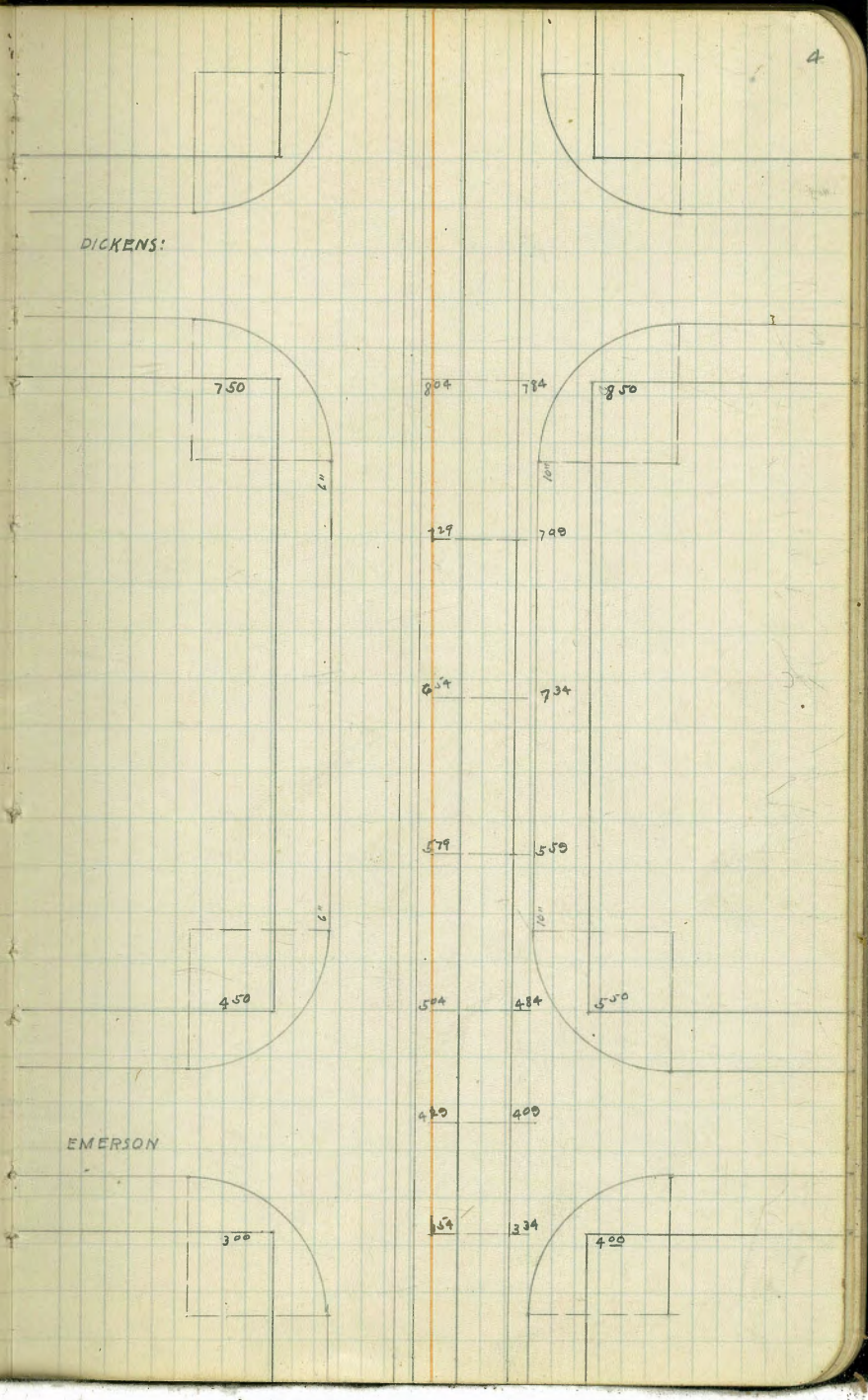
16.12	16.12	16.12	16.12	16.12	16.12	16.12
13.04 ✓	12.16 ✓	11.29 ✓	10.42 ✓	9.54 ✓	8.79 ✓	8.04
3.08 ✓	3.96 ✓	4.83 ✓	5.70 ✓	6.58 ✓	7.33	8.08
3.28 ✓	4.16 ✓	5.03 ✓	5.90 ✓	6.78 ✓	7.53	8.28



9.34 = grade stake
+0.28
9.62 ✕

9.62	9.62	9.62	9.62	9.62	9.62	9.62	9.62
8.79 ✓	8.04 ✓	7.29 ✓	6.54 ✓	5.79 ✓	5.04 ✓	4.29 ✓	3.54 ✓
0.83	1.58	2.33 ✓	3.08	3.83 ✓	4.58 ✓	5.33 ✓	6.08 ✓

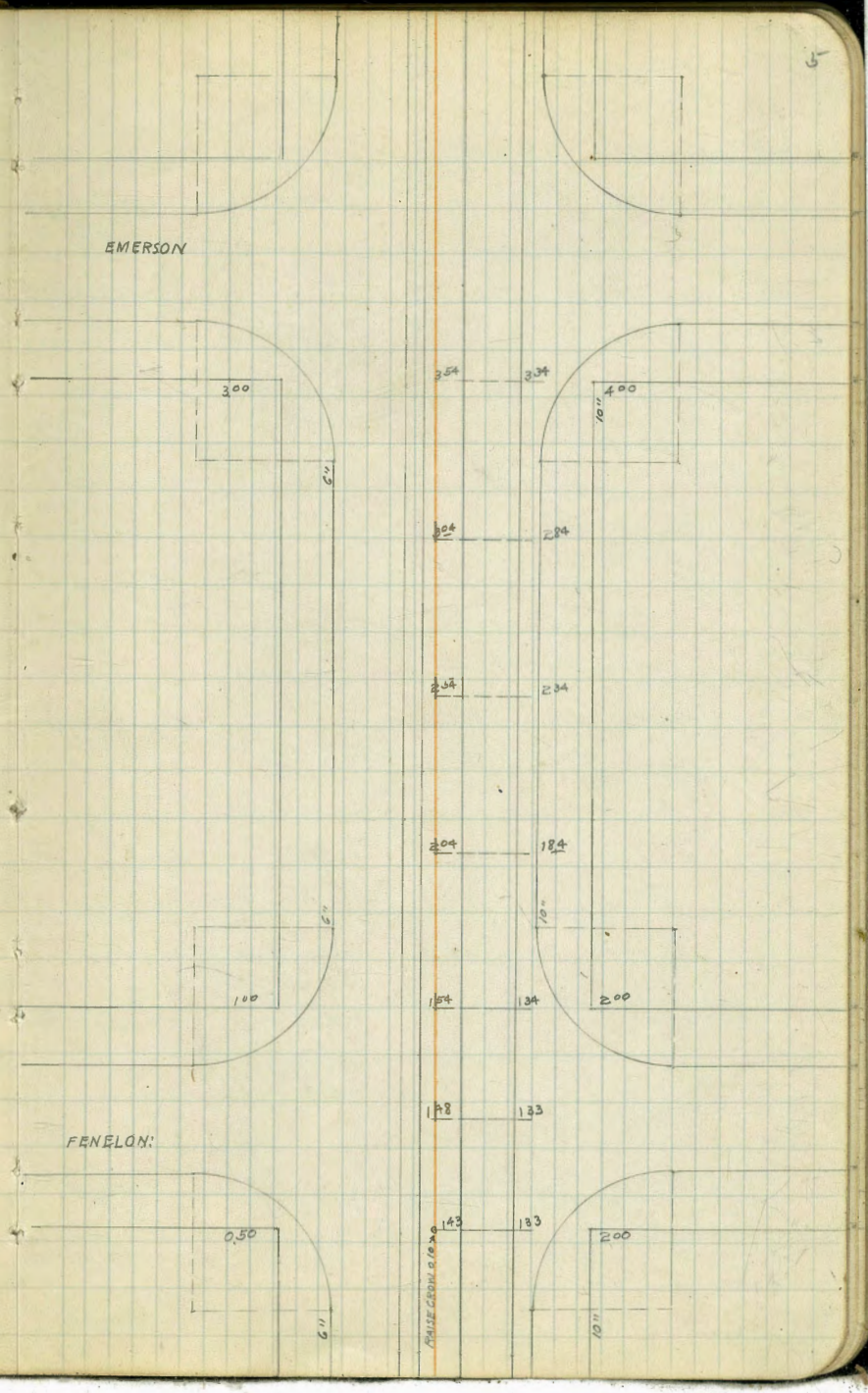
10.3 ✓ 1.78 ✓ 2.53 ✓ 3.28 ✓ 4.03 ✓ 4.78 ✓ 5.53 ✓ 6.28 ✓



x 9.62

9.62	9.62	9.62	9.62
3.04	2.54	2.04	1.54
6.58	7.08	7.58	8.08

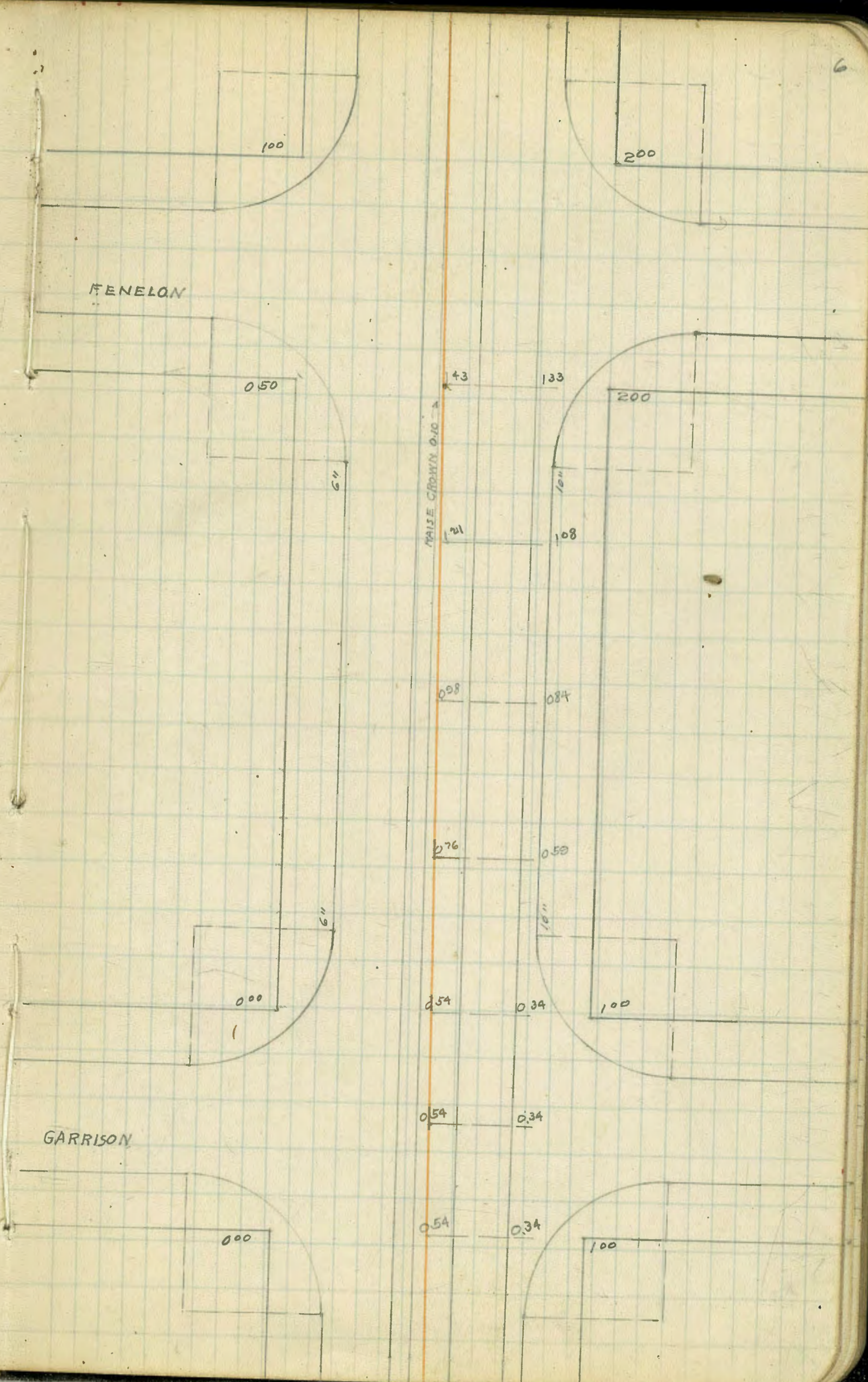
6.78 7.28 7.78 8.28



B.M. 1.15 GARRISON
5.36
6.51 T
5.18
1.33 = 1.34 check stk

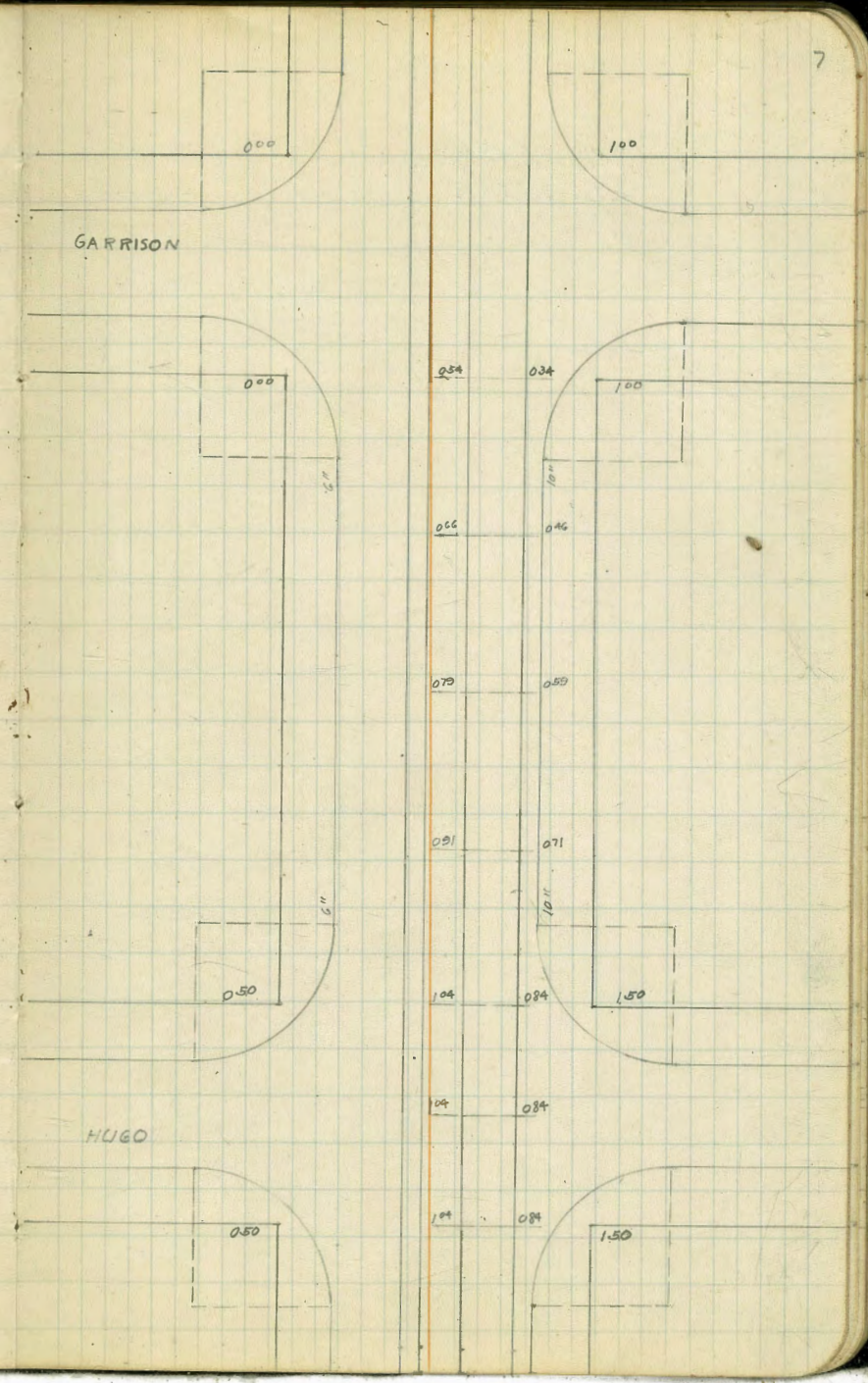
6.51	6.51	6.51	6.51	6.51	6.51
1.48	1.43	1.21	.98	.76	54
5.03	5.08	5.30	5.53	5.75	5.97
				(5.25)	(5.47)

6.51	6.51	6.51	6.51	6.51	6.51
1.33	1.33	1.08	84	.59	.34
5.18	5.18	5.43	5.67	5.92	6.17
				(5.42)	



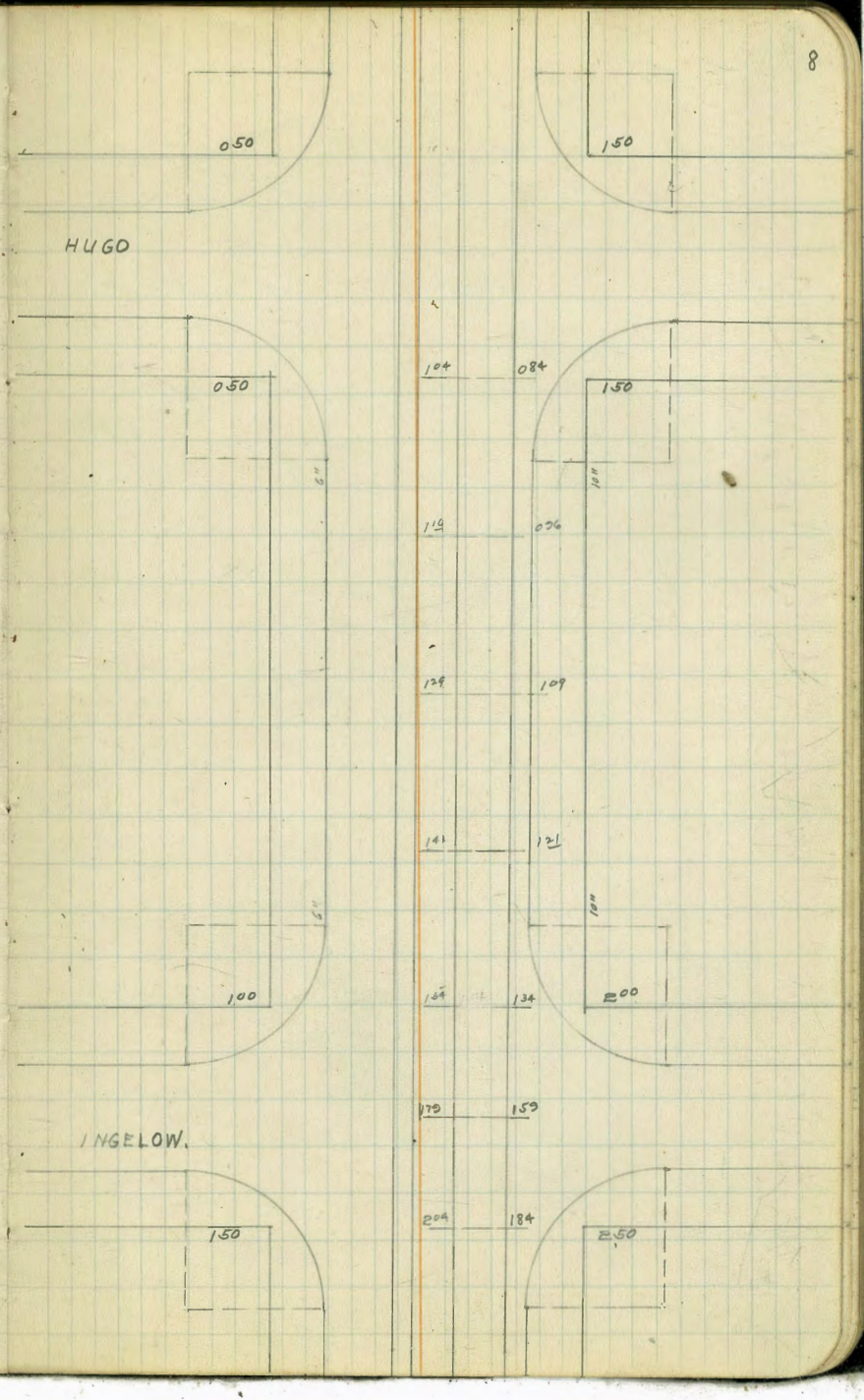
BM. 115
+5.04
6.19 ✗

E	6.19	6.19	6.19	6.19	6.19	6.19	6.19
	0.54	.54	.66	.79	.91	1.04	1.04
	5.65	5.65	5.53	5.40	5.28	5.15	5.15
		(5.1)	+0.5	+0.5	+0.5	+0.5	+0.5
W	5.85	5.85	5.73	5.60	5.48	5.35	5.35
	+1.0	+1.0	+1.0	+0.5	+0.5	+0.5	+0.5



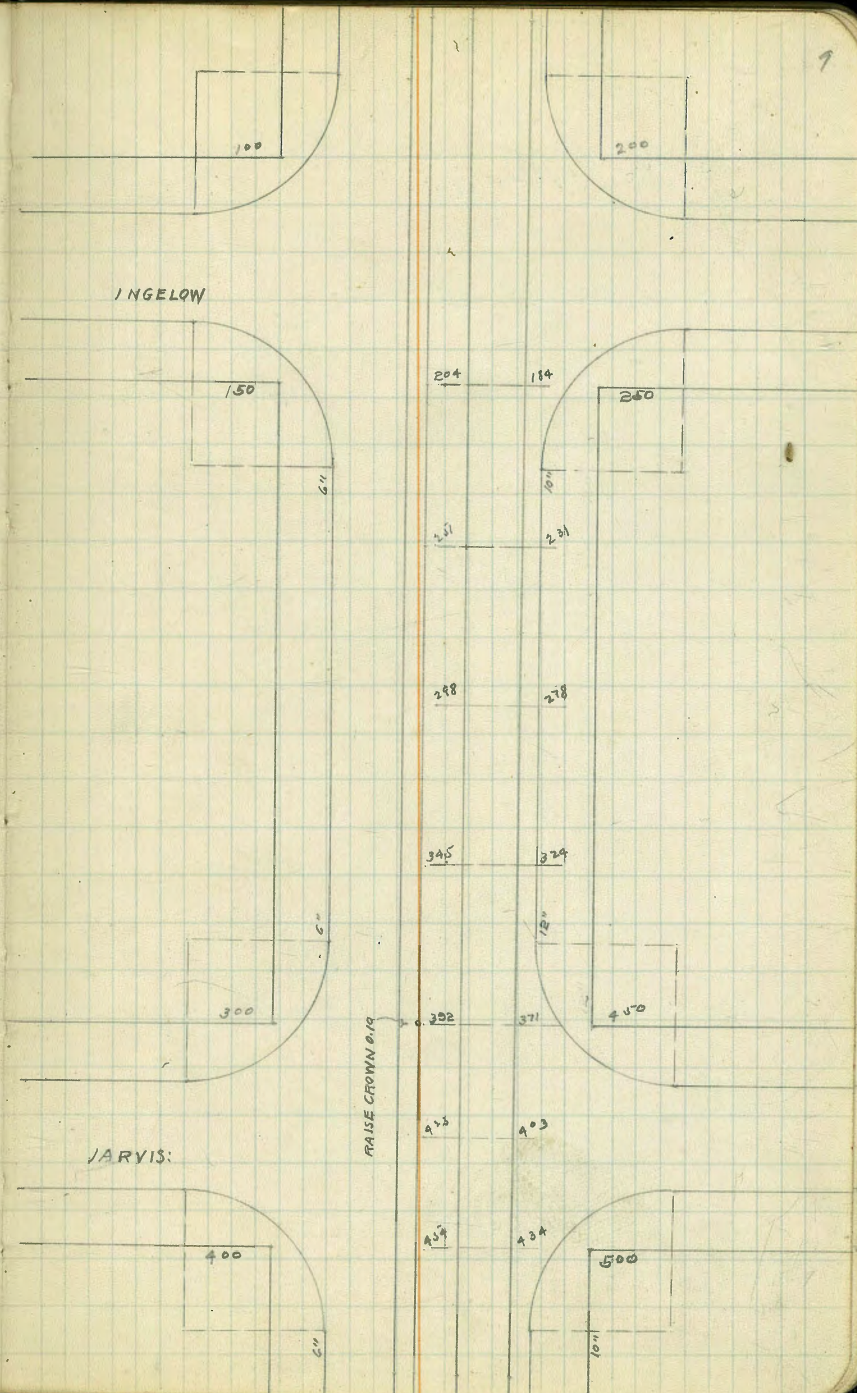
6.19 K

E	6.19 1.09	6.19 1.16	6.19 1.29	6.19 1.41	6.19 1.54
	5.45 +0.5	5.03 +0.5	4.90 +0.5	4.78 +0.5	4.67 +0.5
W	5.35 +0.5	5.23 +0.5	5.10 +0.5	4.98 +0.5	4.85 +0.5



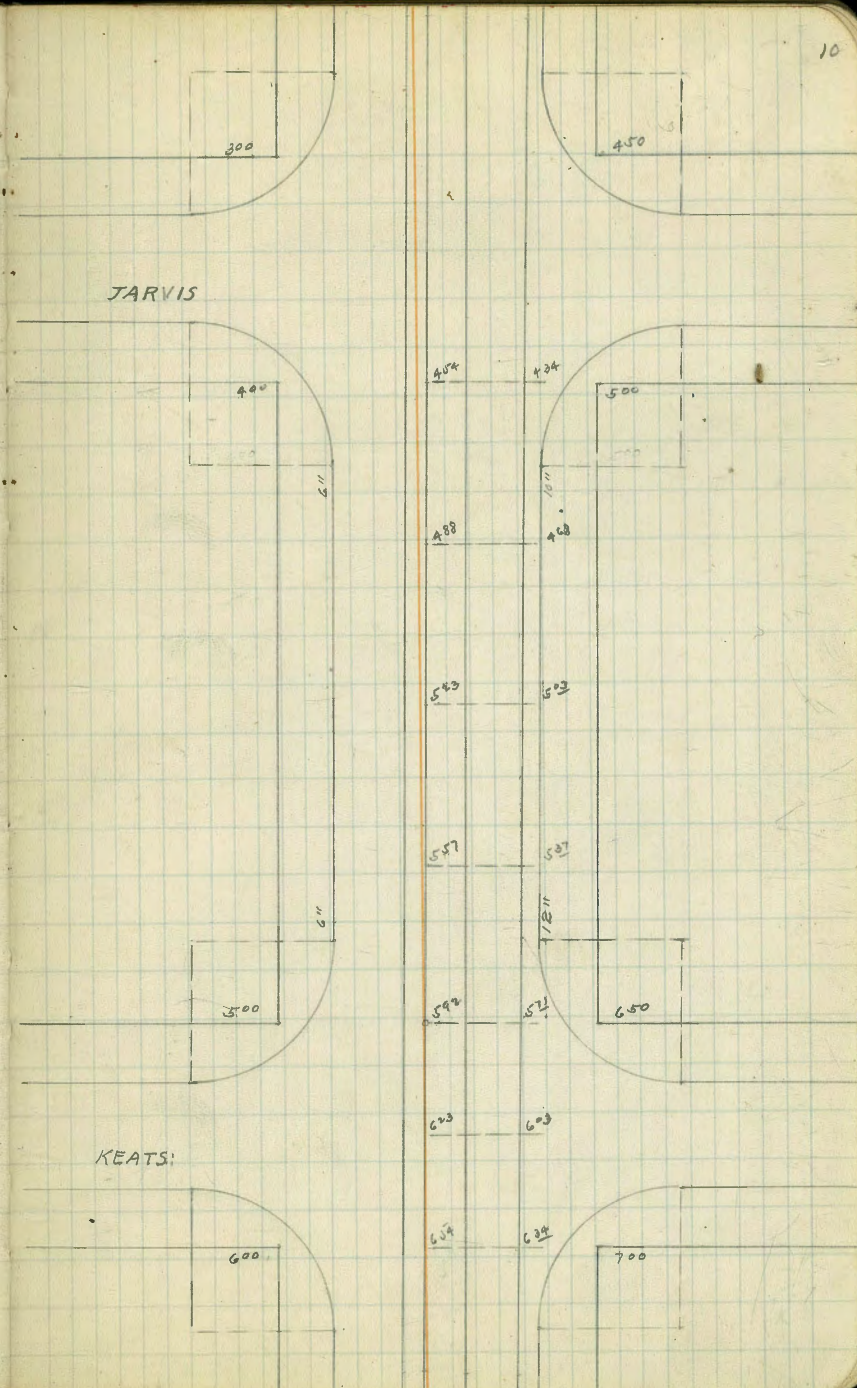
8.06 B.M
4 13
12.19
-5.20
6.99
+ 2 47
9.46

E	9.46	.946	946	9.46	9.46	9.46	9.46	9.46
	7.79	2.04	2.51	2.98	3.45	3.92	4.23	4.54
	7.67 ✓	7.42 ✓	6.95 ✓	6.48 ✓	6.01 ✓	5.54 ✓	5.23 ✓	4.92 ✓
W	7.87	7.62	7.15 ✓	6.68 ✓	6.21 ✓	5.74 ✓	5.43 ✓	5.12 ✓
	+05	+05						



9.46 π

E	9.46 4.88 4.58 ✓	9.46 5.23 4.23 ✓	9.46 5.57 3.89 ✓	9.46 5.92 3.54 ✓
W	4.78 ✓	4.43 ✓	4.09 +0.5	3.74 +0.5

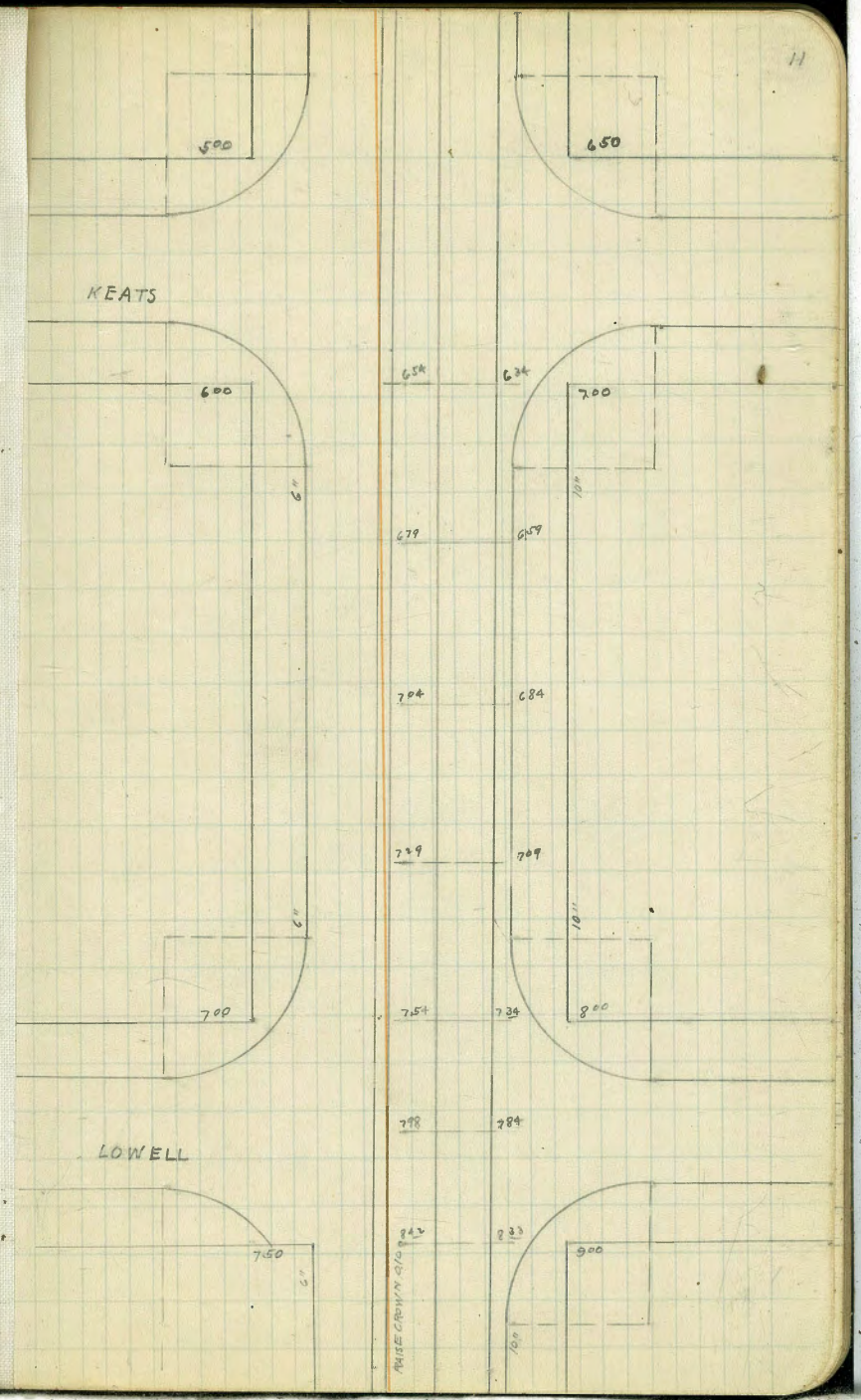


BOG - B.M. Lowell
388
11.91 π

E	11.91	11.91	11.91	11.91	11.91	
	6.23 ✓	6.54 ✓	6.79 ✓	7.04	7.29	
	5.68	5.37 ✓	5.12	4.87 ✓	4.62	
W	5.88	5.57 ✓	5.32	5.07	4.82	
	+0.5		+0.5	+0.5		

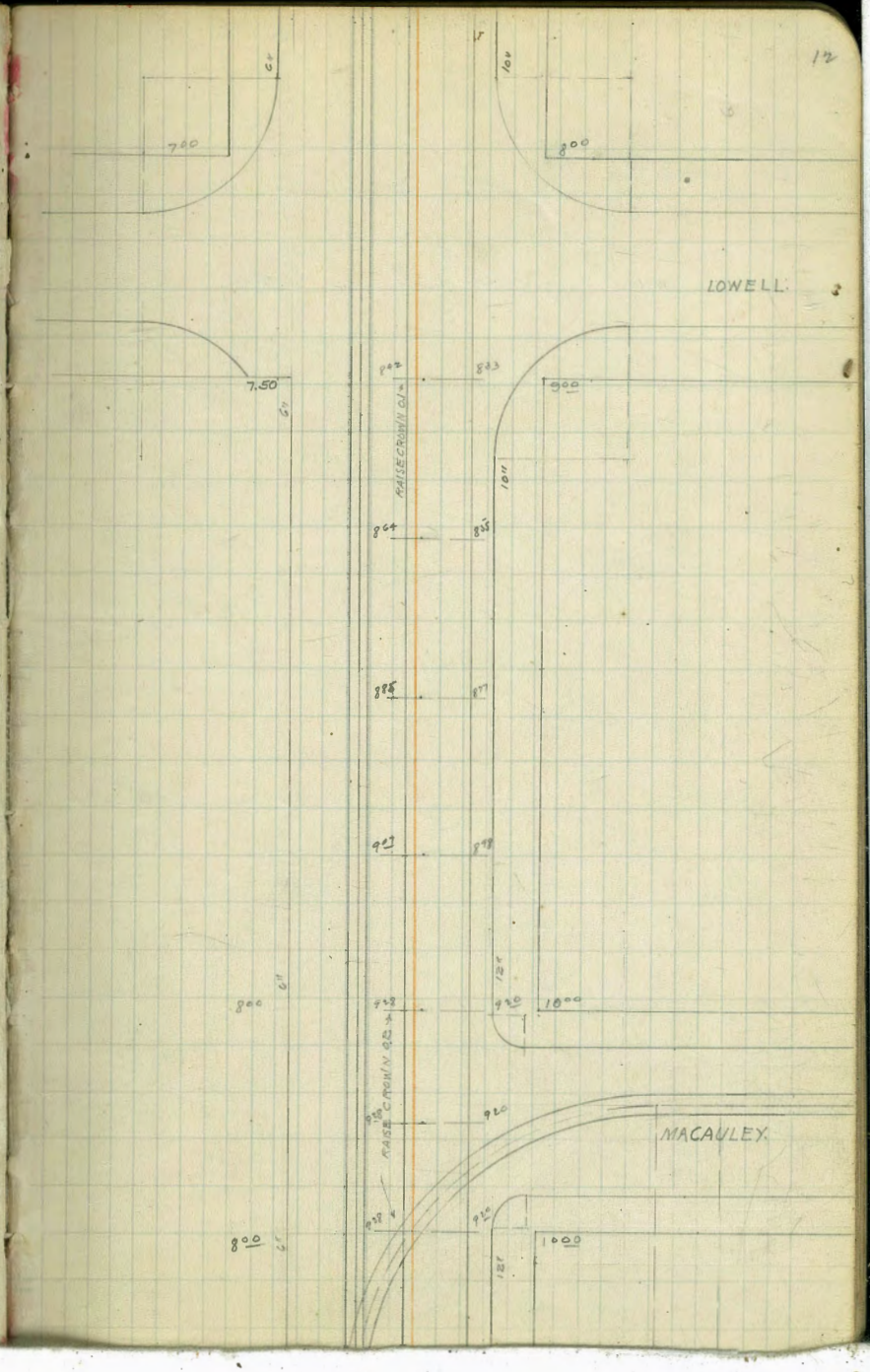
8.06
6.05
14.11 π

E	14.11	14.11	14.11	14.11	
	7.29	7.54	7.98	8.42	
	6.82	6.57	6.13	5.69	
		+0.5	+0.5	+0.5	
W	7.02 ✓	6.77 ✓	14.11 884	14.11 8.33	
	+0.5	+0.5	6.27	5.78 ✓	
			+0.5		



14.11 π

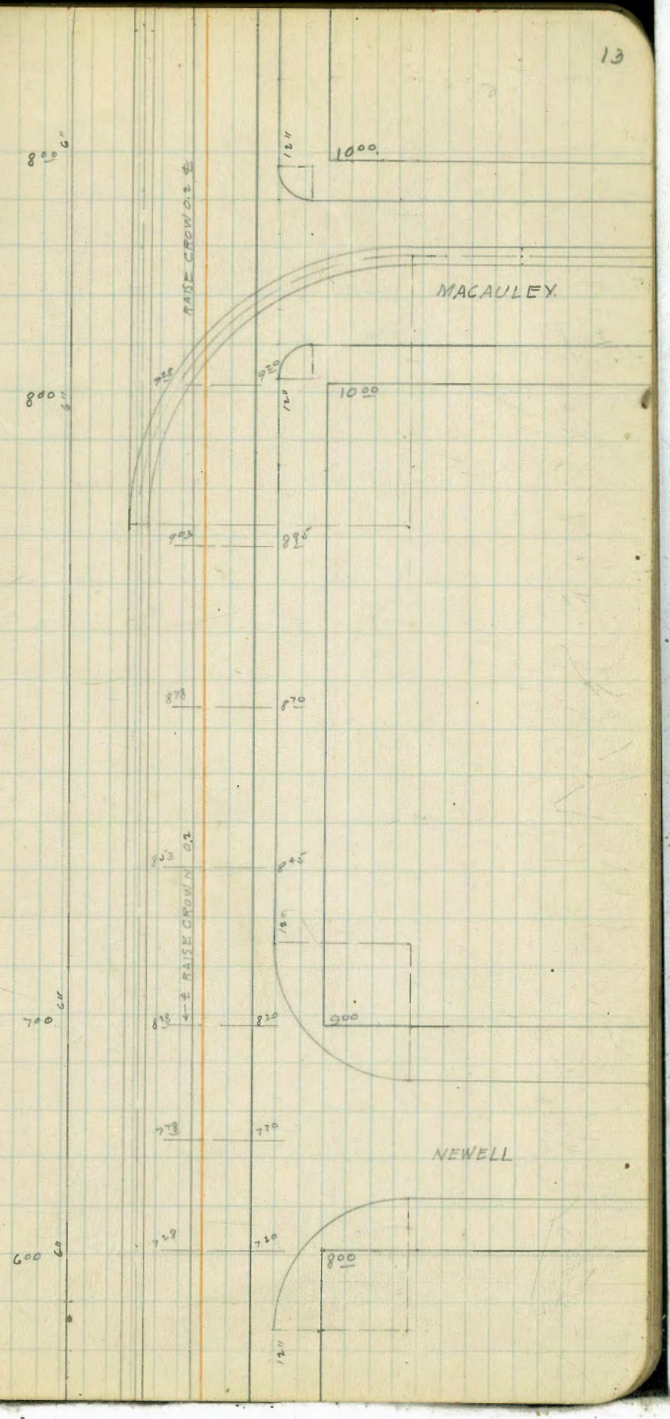
E	14.11	14.11	14.11	14.11
	8.64	8.85	9.07	9.38
	5.47	5.26	5.04	4.83
	+0.5	+0.5	+0.5	+0.5
W	14.11	14.11	14.11	14.11
	8.85	8.77	8.98	9.20
	5.56	5.34	5.13	4.91
	+0.5	+0.5	+0.5	+0.5



8.03
5.09
13.62 ft

	13.62	13.62	13.62	13.62	13.62	13.62
	9.03	8.78	8.03	8.28	7.78	7.28
	+4.59	4.84	5.09	5.34	5.84	6.34
	+0.5	+0.5	+0.5	+0.5	+0.5	+0.5

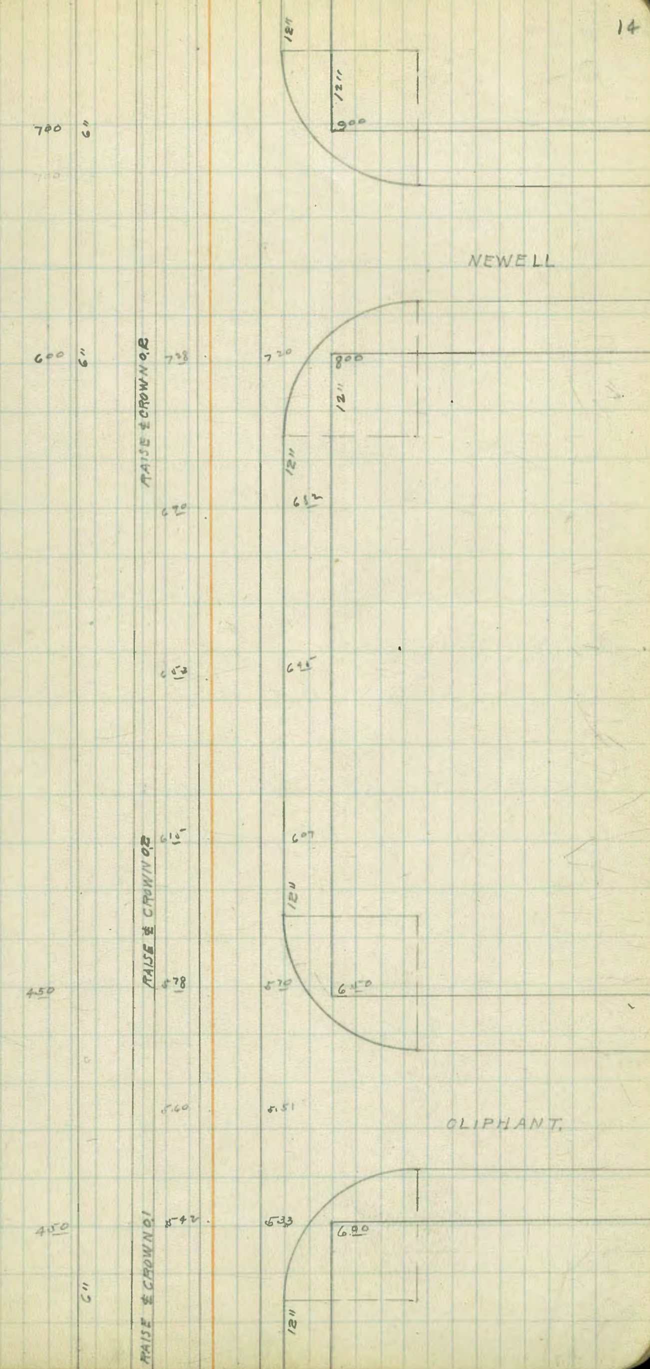
W 4.67 4.92 5.17 5.42 5.92 6.42



13.62 π

E 13.62 / 6.90 / 6.72 +0.5 — 13.62 / 6.55 / 7.07 ✓ — 13.62 / 6.15 / 7.47 — 13.62 / 5.78 / 7.84 ✓

W 6.80 ✓ 7.17 ✓ 7.55 ✓ 7.92 ✓



5.78 stk
4.30
10.08 π

E 10.08 − 5.60 = 4.48 ✓ | 10.08 − 5.42 = 4.66 +0.5 | 10.08 − 5.26 = 4.82 ✓ | 10.08 − 5.10 = 4.98 ✓

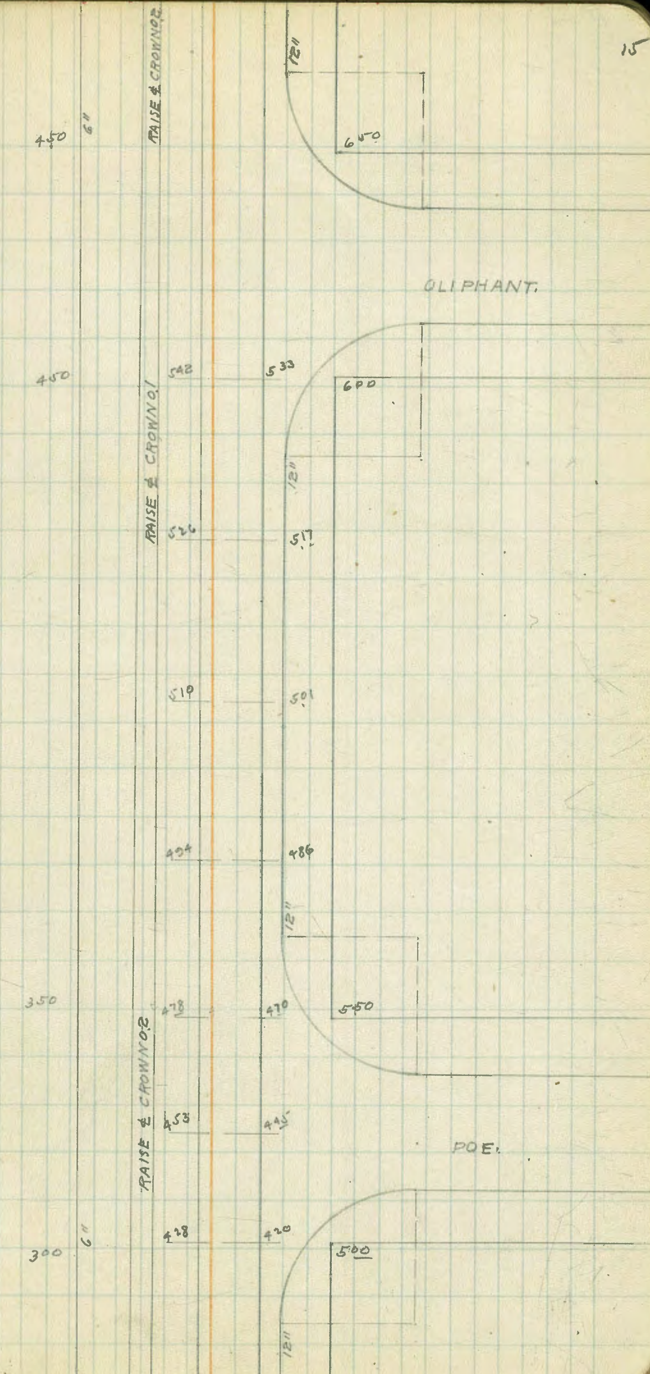
W 10.08 − 5.51 = 4.57 +0.5 | 10.08 − 5.33 = 4.75 +0.5 | 10.08 − 5.17 = 4.91 +0.5 | 10.08 − 5.02 = 5.06 +0.5

5.78 stk
3.61
9.39 π

E 9.39 − 5.60 = 3.79 ✓ | 9.39 − 5.42 = 3.97 ✓ | 9.39 − 5.26 = 4.13 ✓ | 9.39 − 5.10 = 4.29 ✓ | 9.39 − 4.94 = 4.45 | 9.39 − 4.78 = 4.61 ✓ | 9.39 − 4.53 = 4.86 | 9.39 − 4.28 = 5.11 ✓

check

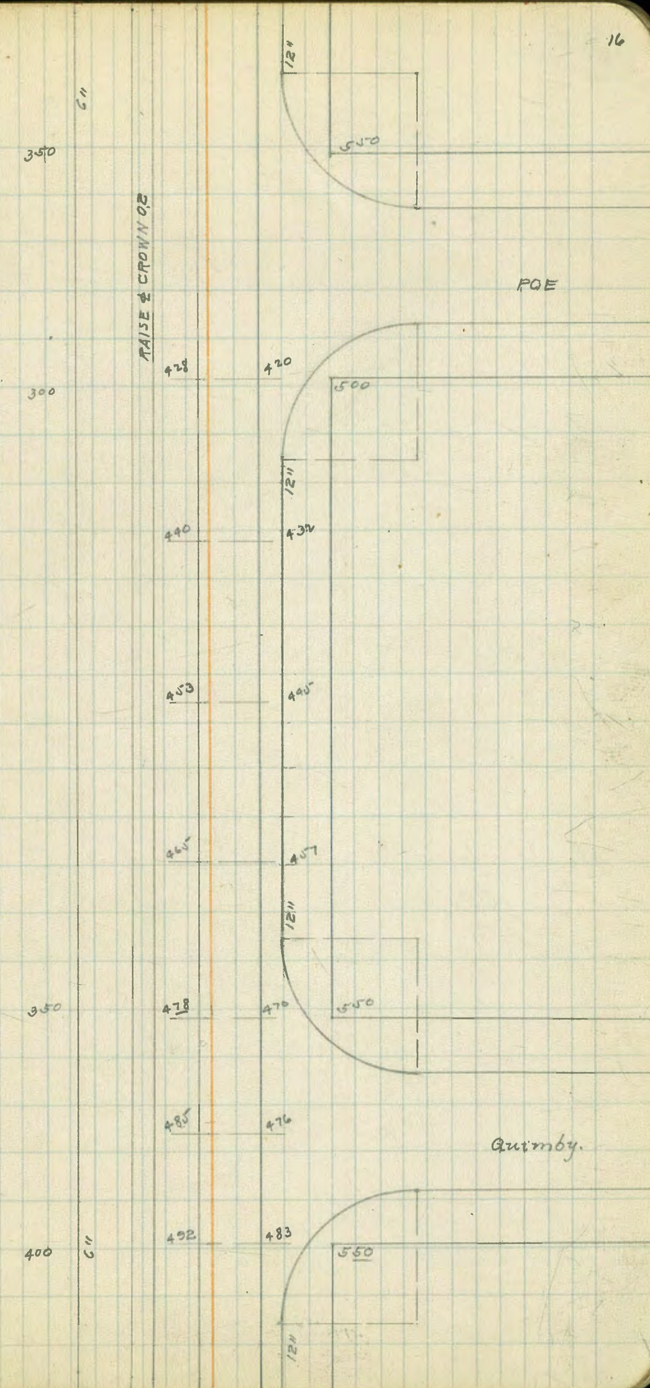
W 3.88 ✓ | 4.06 ✓ | 4.22 ✓ | 4.38 ✓ | 4.53 +0.5 | 4.69 +0.5 | 4.94 ✓ | 5.19 +0.5



9.39 +

	9.39	9.39	9.39	9.39
E	4.40	4.53	4.65	4.78
	4.99	4.86	4.74	4.61

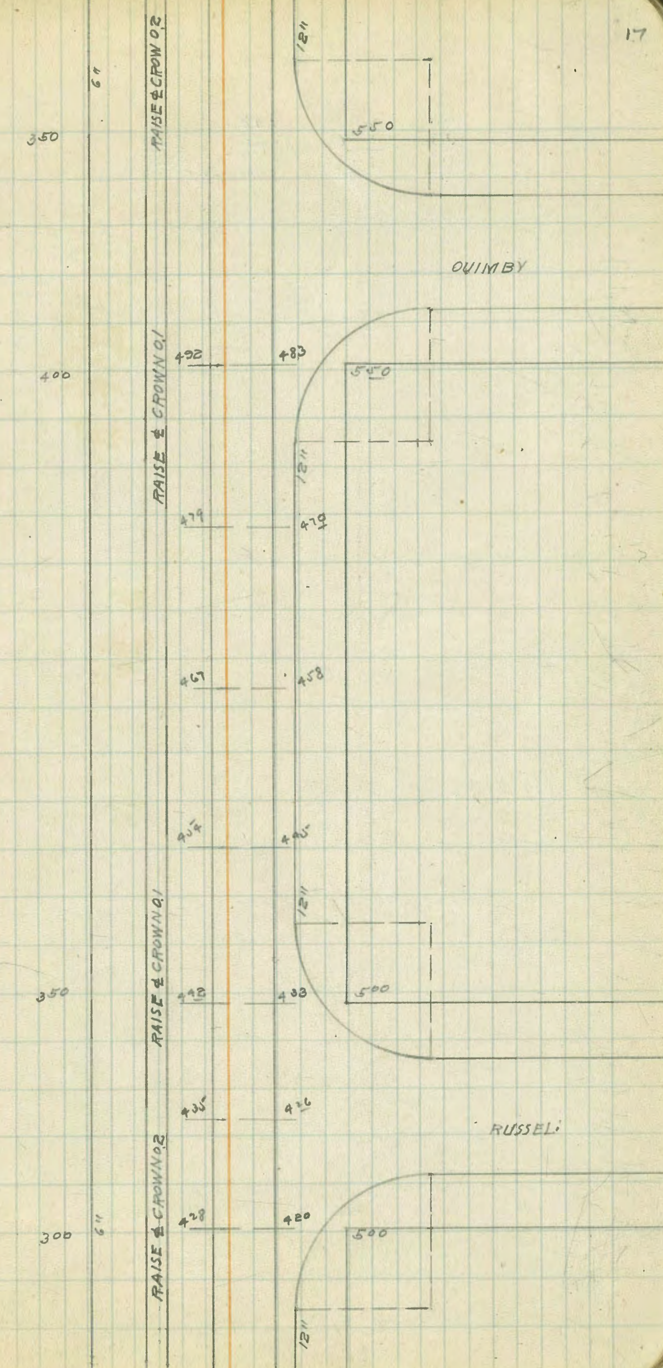
W	5.07	4.94	4.82	4.69
	+0.5	+0.5		



4.78 stk
4.70
9.48 ⊼

E	9.48	948	9.48	9.48	9.48	9.48	948	9.48
	4.85	492	4.79	4.67	4.54	4.42	4.35	4.28
	4.63	4.56	4.69	4.81	4.94	5.06	5.13	5.20
				+0.5	+0.5	+0.5	+0.5	+0.5

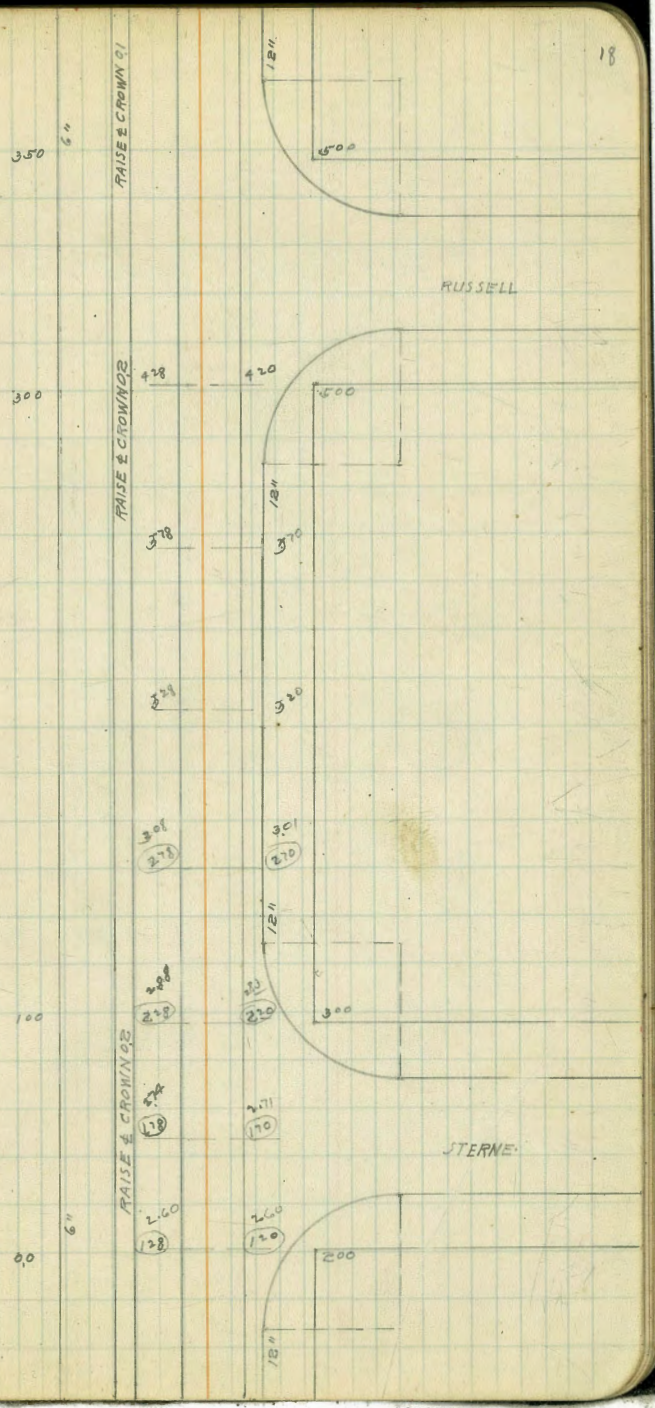
W	4.72 ✓	4.65 ✓	4.78 ✓	4.90 ✓	5.03 ✓	5.15 ✓ +0.5	5.22 ✓	5.28 ✓



	S	9.48 3.78 5.70 +0.5	9.48 3.28 6.20 +0.5	9.48 2.78 6.70 +0.5	9.48 2.28 7.20 +0.5
	W	5.78	6.28	6.78	7.28
3.14 5.16 8.30	E	8.30 2.28 6.02 +0.5	8.30 1.78 6.52 +0.5	8.30 1.28 7.02 +1.0	
	W	8.30 2.20 6.10 +0.5	8.30 1.70 6.60 +0.5	8.30 1.20 7.10 +1.0	

Change:

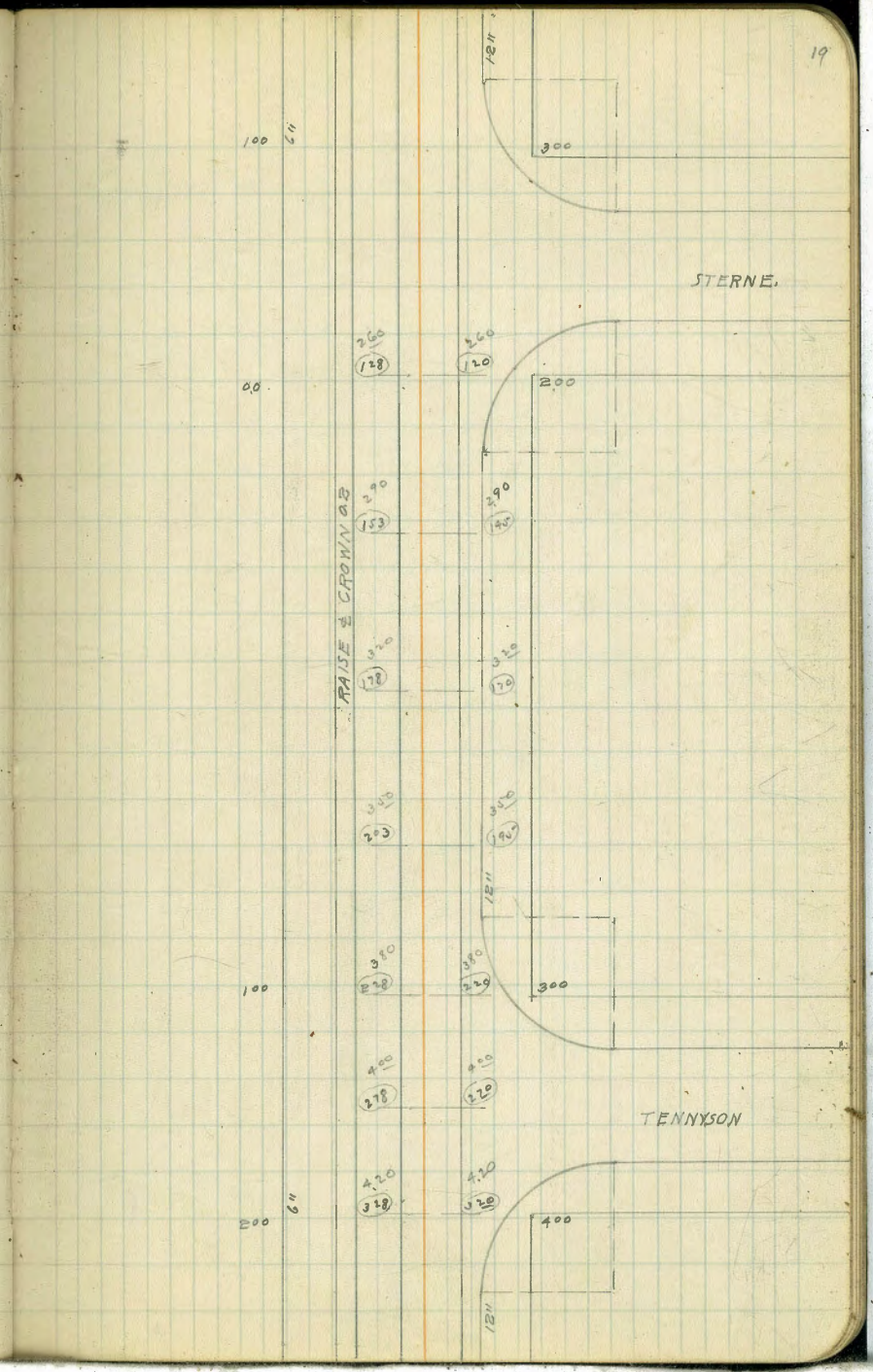
E	8.30 3.09 5.22	8.30 2.88 5.42	8.30 2.74 5.56 -0.5	8.30 2.60 5.70 -0.5
W	8.30 3.01 5.29	8.30 2.83 5.47 -0.5	8.30 2.71 5.59 -0.5	8.30 2.60 5.70 -0.5



change

8.30 π

E	8.30	8.30	8.30	8.30	8.30	8.30
	290	320	350	380	400	420
	5.4°	5.1°	4.8°	4.5°	4.3°	4.1° ✓
	-1.0	-1.0	-1.0	-0.5	-0.5	
W	8.00	8.30	8.30	8.30	8.30	8.30
	290	320	350	380	400 ✓	420
	5.4°	5.1°	4.8°	4.5°	4.3°	4.1°
	-0.5	-0.5	-0.5	-0.5		



π = 17.93

E 17.93 / 11.80 / 6.13 / −1.0 — 17.93 / 12.55 / 5.38 / −1.0

W 17.93 / 12.73 / 6.20 ✓ / −0.5 — 17.93 / 12.98 / 5.45 ✓ / −1.0

Changed.

17.99 π

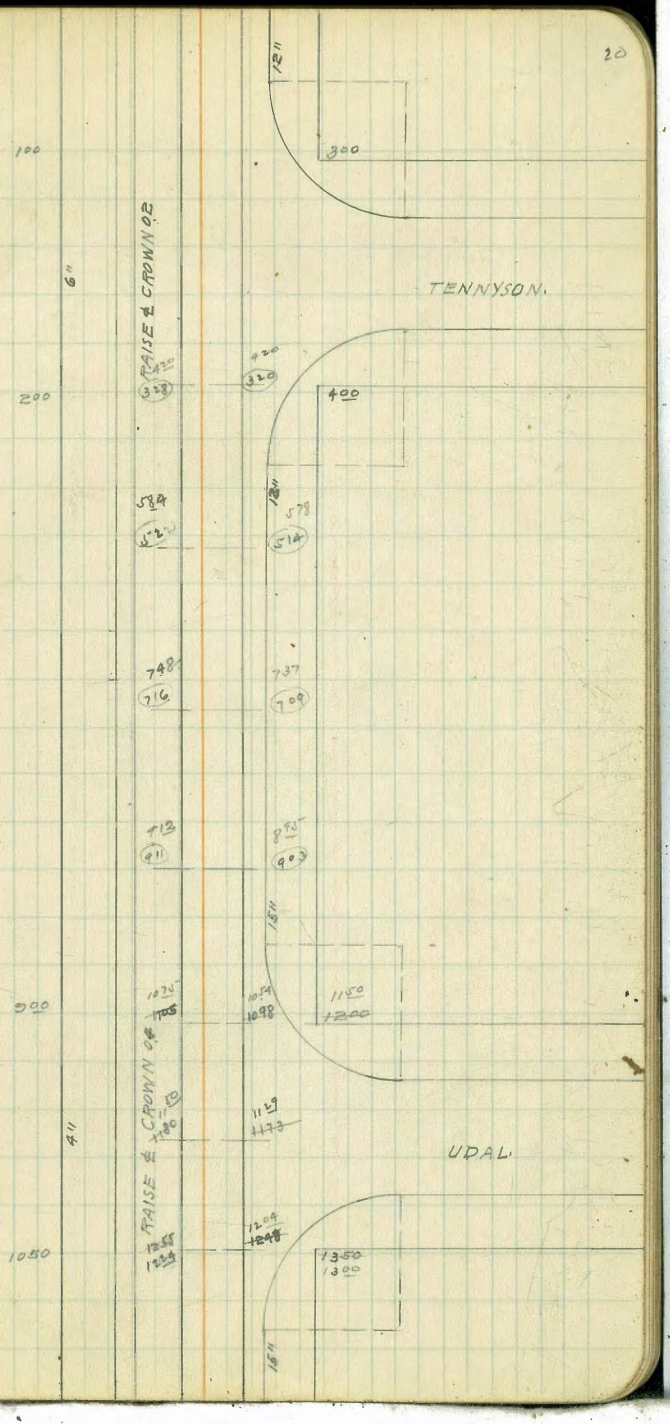
E 17.99 / 11.50 / 6.49 / −1.0 — 17.99 / 12.74 / 5.75 / −1.0 — 8:30 / 5.84 / 2.46 / −1.0 — 8.30 / 7.48 / 0.82 / −1.0

W 17.99 / 11.29 / 6.70 ✓ — 17.99 / 12.04 / 5.95 / −0.50 — 8:30 / 5.78 / 2.52 / −0.5 — 8:30 / 7.37 / 0.93 / −0.5

8.30
−1.48
6.87
+6.35
13.22 π

13.22 / 9.12 / 4.10 / −1.5 — 13.22 / 10.75 ✓ / 2.47 / −1.0

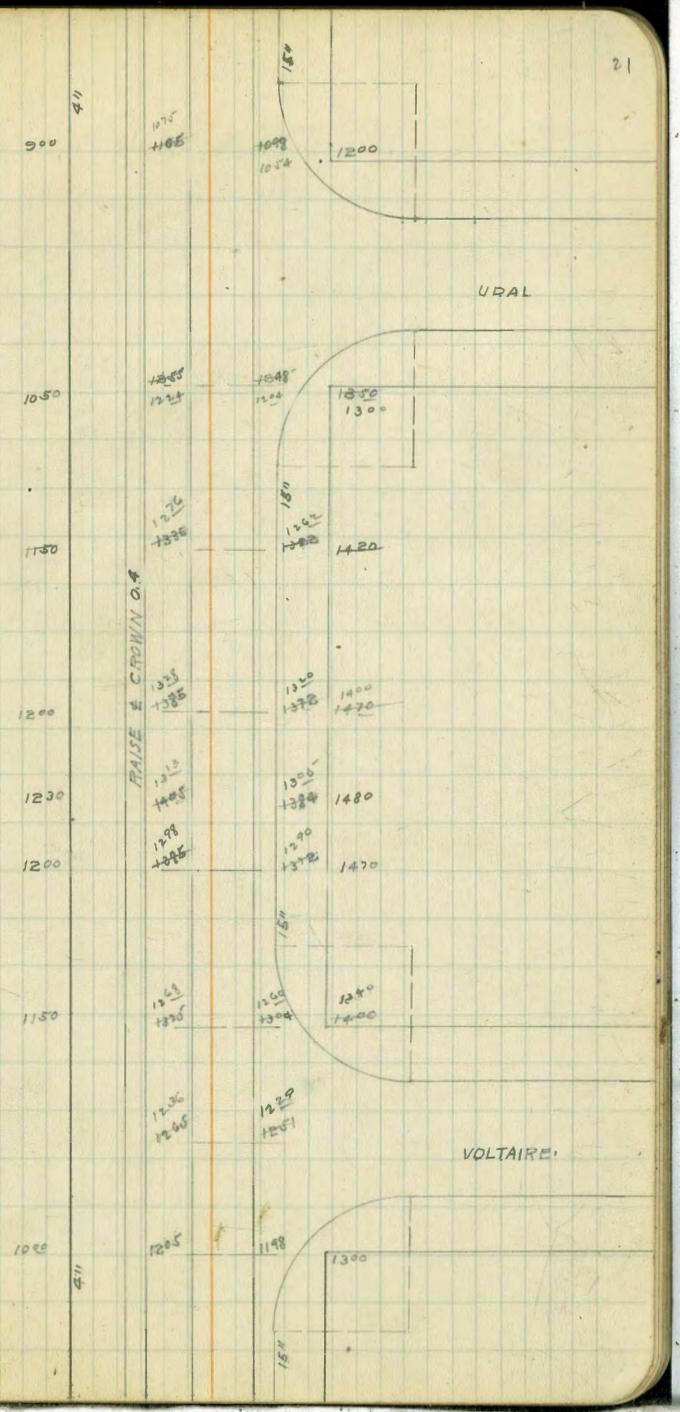
13.22 / 8.95 ✓ / 4.27 / −0.5 — 13.22 / 10.54 / 2.68



E	17.93	17.93	17.93	17.93	17.93	17.93	17.93
	1335	1385	14.05	1385	1320	1265	1206
	4.58	4.08	3.98	4.08	4.68	5.28	5.88
	-1.0	-0.5	-1.0	-0.5		+.05	+1.0
W	17.93	17.93	17.93	17.93	17.93	17.93	17.93
	1322	1377	1394	1377	1304	1205	1198
	4.71	4.21	4.09	4.21	4.89	5.42	5.95
	-1.0	-0.5	-0.5	-0.5	+05	+1.0	+1.5

change!

E	17.99	17.99	17.99	17.99	17.99	17.99
	1276	1328	1313	1298	1268	1206
	5.23	4.71	4.86	5.01	5.31	5.63
	-0.50				+0.50	
W	17.99	17.99	17.99	17.99	17.99	17.99
	1267	1320	1305	1290	1260	1229
	5.37	4.79	4.94	5.09	5.39	5.70
	0.50				+1.0	+1.0



Voltaire St to Whittier

17.93	E	17.93	17.93	17.93	17.93
		11.80	11.55	11.30	11.05
		6.13	6.38	6.63	6.88
		+1.0	+1.0	+1.0	+1.0
17.93	W	17.93	17.93	17.93	17.93
		11.73	11.48	11.23	10.98
		6.20	6.45	6.70	6.95
		+1.0	+1.0	+1.0	+1.0

Whittier to Xenophon

BM. 18.01
1.71
19.72 ✓

E

19.72	19.72	
11.25	11.45	
8.47	8.27	
+0.5		
19.72		
11.21		
8.51		
+1.0		

18.01
1.48
19.49 ✓

E

19.49	19.49	19.49	19.49	19.49
11.45	12.86	14.27	15.68	17.10
8.04	6.63	5.22	3.81	2.39
+1.5				

W

19.49	19.49	19.49	19.49	19.49
11.45	12.86	14.27	15.68	17.10
8.04	6.63	5.22	3.81	2.39
+1.0				

18.01 BM								
9.13								
27.14 T		27.14	27.14	27.14	27.14	27.14	27.14	27.14
BM	E	17.10	18.10	19.10	20.10	21.10	22.10	23.10
		10.04 ✓	9.04 ✓	8.04 ✓	7.04 ✓	6.04 ✓	5.04 ✓	4.04 ✓
	W	27.14	27.14	27.14				
		17.10	18.10	19.10				
		10.04 ✓	9.04 ✓	8.04	27.14	27.14	27.14	27.14
				-0.5 ✓	20.10	21.10	22.10	23.10
					7.04 ✓	6.04	5.04	4.04 ✓
						-0.5	-1.0	-1.0
18								
1								
19								

27.14 ✓

E

27.14	27.14	27.14	27.14	27.14	27.14
2328	2347	2390	2432	2476	2520
3.86	3.67	3.24	2.81	2.38	1.94
-0.2	-0.2				

W

27.14	27.14	27.14	27.14	27.14	27.14
2328	2347	2392	2437	2482	2528
3.86	3.67	3.22	2.77	2.32	1.86

25.19 10.25 35.44	E	35.44 25.29 10.16	35.44 25.28 10.16	35.44 26.06 9.38	35.44 26.84 8.60	35.44 27.62 7.82	35.44 28.40 7.04	35.44 29.34 6.10	35.44 30.28 5.16
	W	35.44 25.20 10.24 +0.5	35.44 25.20 10.24 +0.5	35.44 26.00 9.44	35.44 26.80 8.64	35.44 27.60 7.84	35.44 28.40 7.04	35.44 29.30 6.14	35.44 30.20 5.24

35.44 N

E

35.44	35.44	35.44	35.44
31.31 ✓	32.35 ✓	33.38 ✓	34.42 ✓
4.13	3.09	2.06	1.02

W

35.44	35.44	35.44	35.44
31.23 ✓	32.27	33.30	34.33 ✓
4.21	3.17	2.14	1.11
	-1.0	-0.5	

44.33 = BM
2.45
46.78 ✗

E

46.78	46.78	46.78	46.78	46.78	46.78
35.35	36.28	37.53	38.78	40.03	41.28
11.43	10.50	9.25	8.00	6.75	5.50

W/

46.78	46.78	46.78	46.78	46.78	46.78
35.26	36.20	37.45	38.70	39.95	41.20
11.52	10.58	9.33	8.08	6.83	5.58
	+1.0	+0.5	-1.0	-0.25	-1.0

46.78	46.78
41.78	42.28
5.00	4.50

46.78	46.78
41.70	42.20
5.08	4.58
	-0.5

46.78 N

E

46.78	46.78	46.78	46.78
43.28 ✓	44.28 ✓	45.28 ✓	46.28
3.50	2.50	1.50	0.50
			−0.5

W

46.78	46.78	46.78	46.78
43.20	44.20	45.20	46.20 ✓
3.58 ✓	2.58	1.58	0.58
	−0.5	−1.0	

BM 48.18		54.62	54.62	54.62	54.62	54.62	54.62
6.44	E	47.05	47.82	48.55	49.28	50.00	
54.62 ⊼		7.57	6.80	6.07	5.34	4.62	
	W	54.62					
		47.01					
		7.61	6.80	6.07	5.34	4.62	

54.62 T

E	54.62	54.62	54.62	54.62	54.62
	50.45 ✓	50.30 ✓	50.04 ✓	49.77 ✓	49.50 ✓
	4.17	4.32	4.58	4.85	5.12
W	4.17 ✓	4.32 ✓	4.58 ✓	4.85 ✓	5.12

9.14
2.33.
51.47

E

51.47	51.47	51.47	51.47	51.47	51.47	51.47
48.89	48.28	49.78	47.16	46.60	47.00	46.80
2.58	3.19	3.7	4.31	4.87	4.47	4.67
					-1.0	

W

51.47	51.47	51.47	51.47	51.47	51.47	51.47
48.89	48.28	47.78	47.16	46.60	47.00	46.80
2.58	3.19	3.7	4.31	4.87	4.47	4.67

A 51.47

51.47	51.47	51.47	51.47	51.47
47.57 ✓	48.34 ✓	49.10 ✓	49.97 ✓	50.74
3.90	3.13	2.37	1.55	0.78

51.47	51.47	51.47	51.47	51.47
47.57 ✓	48.34 ✓	49.10 ✓	49.97 ✓	50.74
3.90	3.13	2.37	1.55	0.73

8/22/43

Cross Section of 50' St
Spindrift Drive 10' curbs
from N.E. line of La Jolla Vista Tract-North

Mark number shown on Mel.

	0.65	HI 35.96		353'	BM on hub
		00 = E.B.			
-10			10.2	25.8	
W			10.0	26.0	
+4			9.9	26.1	
+5			10.8	25.2	
C/L			11.0	25.0	
1/4			10.5	25.5	
E			10.5	25.5	
+4			17.2	18.8	
1/4			18.2	17.8	
C			13.6	22.4	
+5			9.2	26.8	
E			8.6	27.4	
		10'N			
E			10.3	25.7	
C			17.8	18.2	
+6			17.5	18.5	
1/4			11.5	24.5	
C/L			11.8	24.2	
1/4			11.6	24.4	
C			12.0	24.0	
+5			11.2	24.8	
W			11.3	24.7	
+10			11.3	24.7	

H.I. 35.96

34

T.P.	.0.33	HI 24.12	12.17	23.79
		25'N		
-10			00	24.1
W			0.6	23.5
+7			0.8	23.3
C			1.5	22.6
1/4			1.3	22.8
E			1.4	22.7
1/4			1.2	22.9
+4			1.1	23.0
C			7.6	16.5
+3			8.7	15.4
E			4.0	20.1
+3			0.9	23.2
		45'N		
-9			3.5	20.6
E			9.1	15.0
+4			3.7	20.4
C			3.4	20.7
1/4			3.6	20.5
E			3.5	20.6
1/4			3.3	20.8
C			3.4	20.7
W			3.0	21.1

H.F. 24.12

62' N

W	5.2	18.9
C	5.3	18.8
1/4	5.2	18.9
C	5.3	18.8
1/4	5.2	18.9
C	5.3	18.8
+7	5.3	18.8
E	8.8	15.3
+4	10.2	13.9
+10	5.5	18.6

65' N

E	5.6	18.5
C	5.5	18.6

100' N

E	8.3	15.8
C	8.5	15.6
1/4	8.6	15.5
C	8.8	15.3
1/4	8.7	15.4
C	8.4	15.2
W	9.0	15.1

135' N

W	11.4	12.7
C	11.7	12.4
1/4	11.5	12.6

H I, 24.12

E			11,7	12.4
1/4			11.4	12.7
C			11.2	12.9
E			11.0	13.1
T.P.	1.43	13.22	12,33	11.79
		170' N		
E			2,5	10.7
C			2.5	10.7
1/4			2.4	10.8
C			2.6	10.6
1/4			2.5	10.7
E			2.4	10.8
W			1.9	11.3
		200' N		
-8			2.20	11.0
W			2.2	11.0
C			3.0	10.2
1/4			3.9	9.3
E			4.2	9.0
1/4			4.4	8.8
E			4.5	8.7
E			4.5	8.7
		R16N on N. Entrance to Spindrift		
8' W of W Line			2.32	10.9

on S. Entrance to Spindrift

H.I. 13.22

233 N
133 N

E		7.2	6.0
e		6.5	6.7
1/4		6.1	7.1
℄		5.6	7.6
1/4		4.7	8.5
e		4.0	9.2
W		2.9	10.3

250 N

-10		6.7	6.5
W		6.9	6.3
E		7.2	6.0
1/4		7.3	5.9
℄		7.4	5.8
1/4		7.1	6.1
C		7.2	6.0
E		7.25	6.0
+15		8.3	4.9

1N Traveled Road

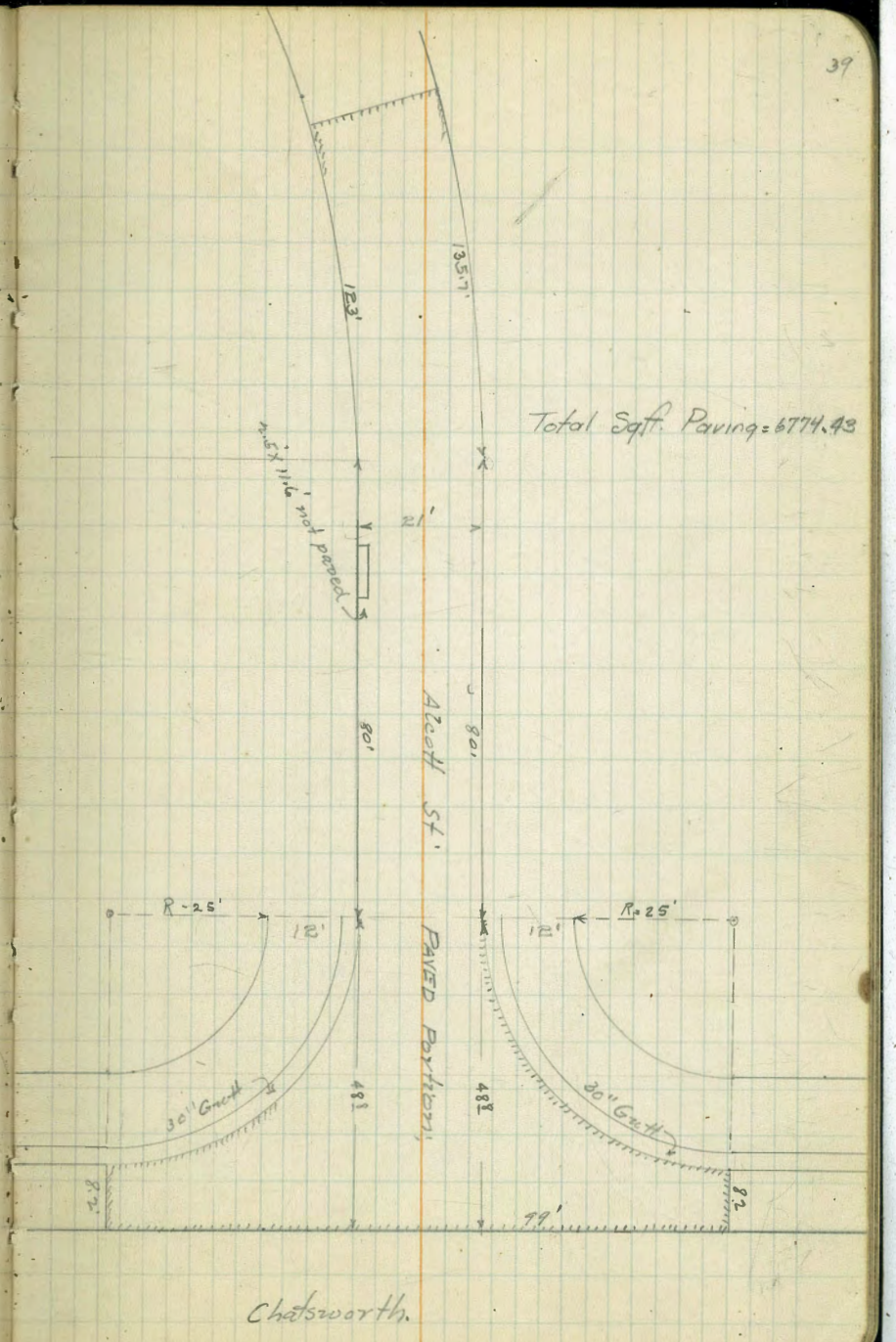
257.93 N = N End Spindrift Drive

-15		8.3	4.9
E		7.8	5.4
e		8.2	5.0
1/4		8.3	4.9
℄		8.3	4.9
1/4		7.9	5.3
C		7.5	5.7
W		7.3	5.9
+10		7.2	6.0

H.I 13.23

307.93 N

-10	10.4	2.8
W	10.6	2.6
C	11.0	2.2
1/4	11.0	2.2
E	11.2	2.0
1/4	11.5	1.7
C	11.5	1.7
E	11.2	2.0
+10	11.0	2.2



Total Sqft. Paving = 6774.48

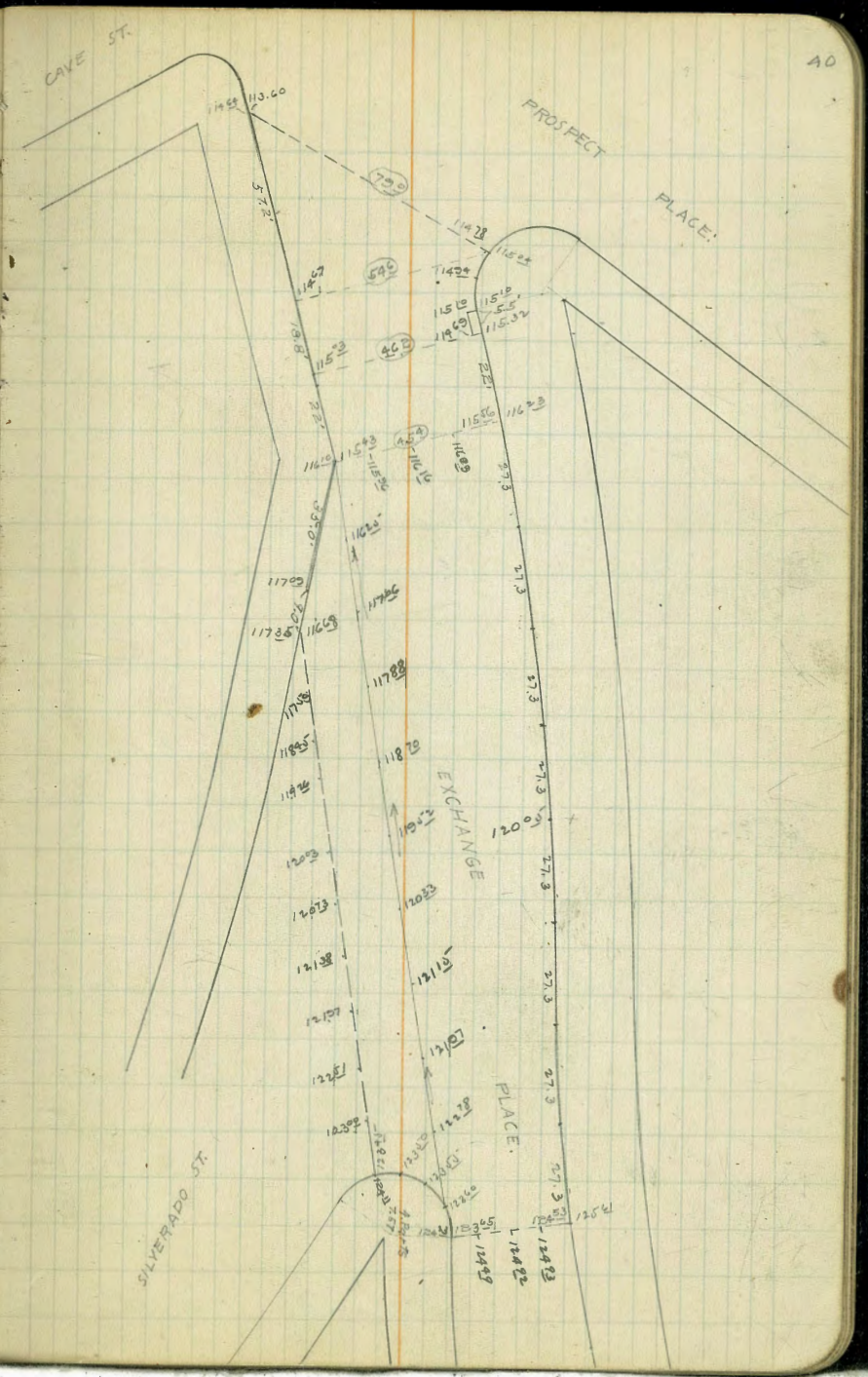
Chatsworth.

BM 113.11 PROSPECT & CAVE.

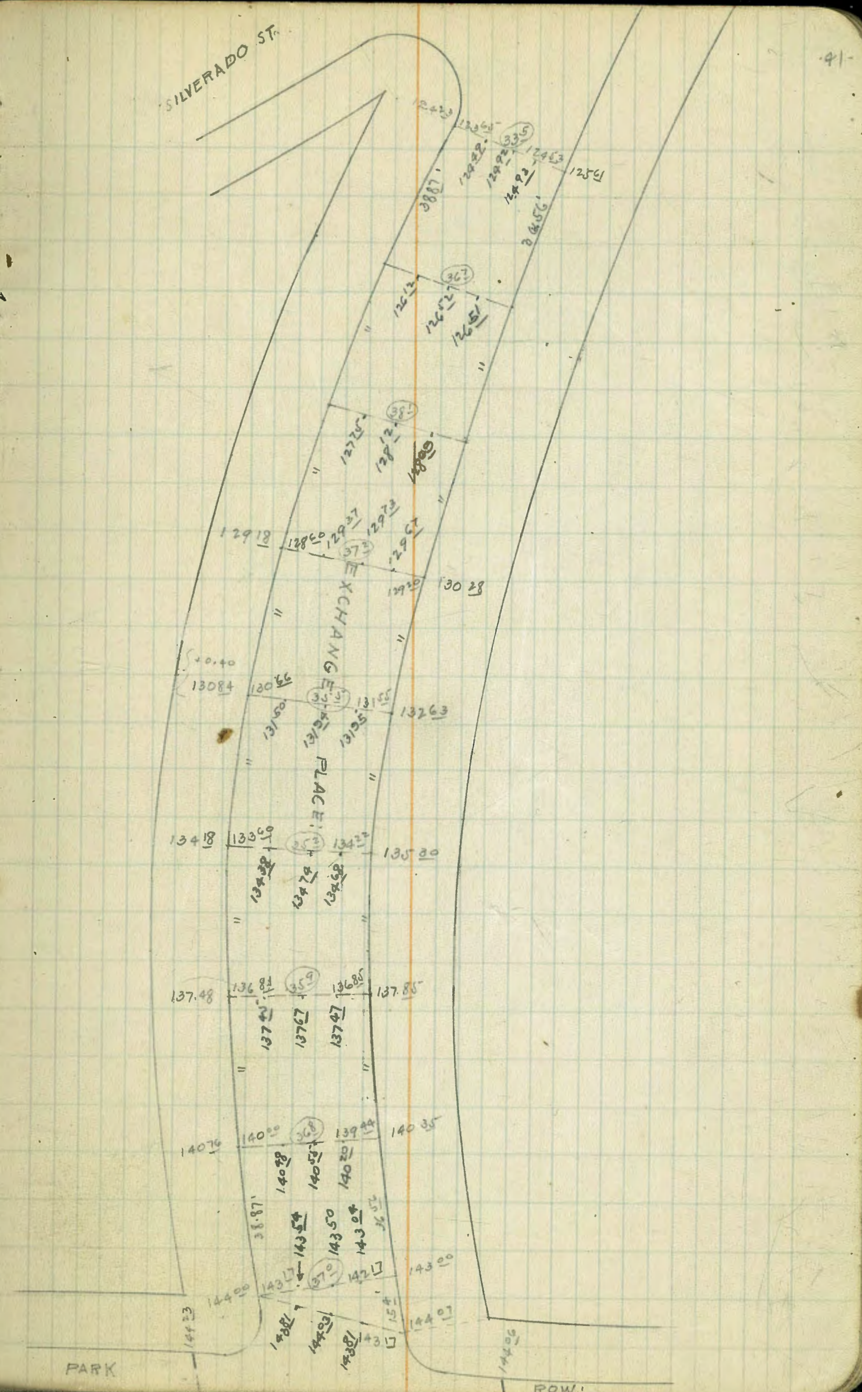
8.40

121.51 π
0.44
121.07
10.14
131.21 π

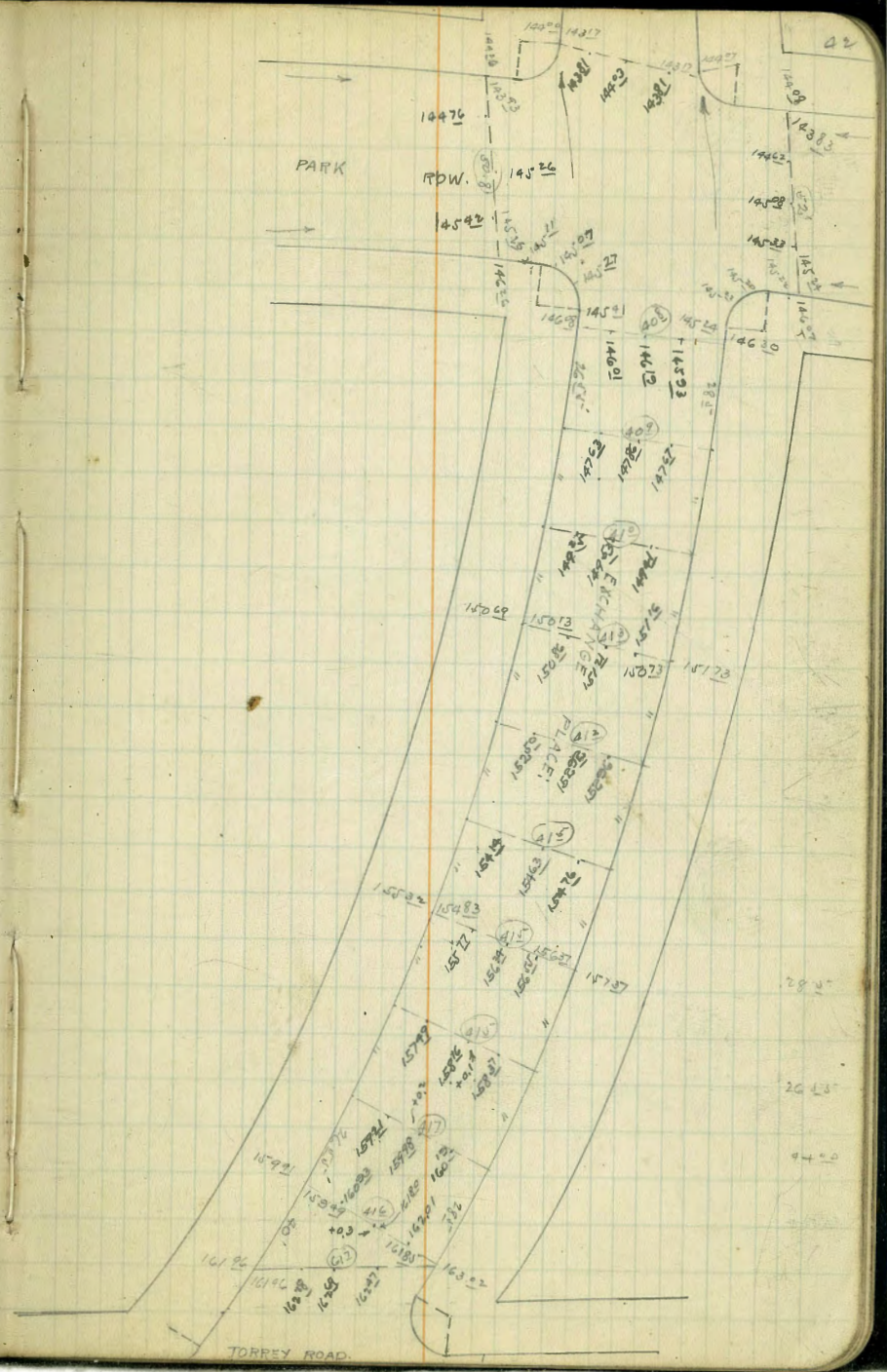
115.43
5.94
121.37
117.35
-.02



131.21 BM
0.07
131.14 on Cement walk.
+ 10.14
141.28
- 0.35
140.93
- 8.35
149.28
5.25
144.03 mails Tel pole Exchange S.W. Park Row.

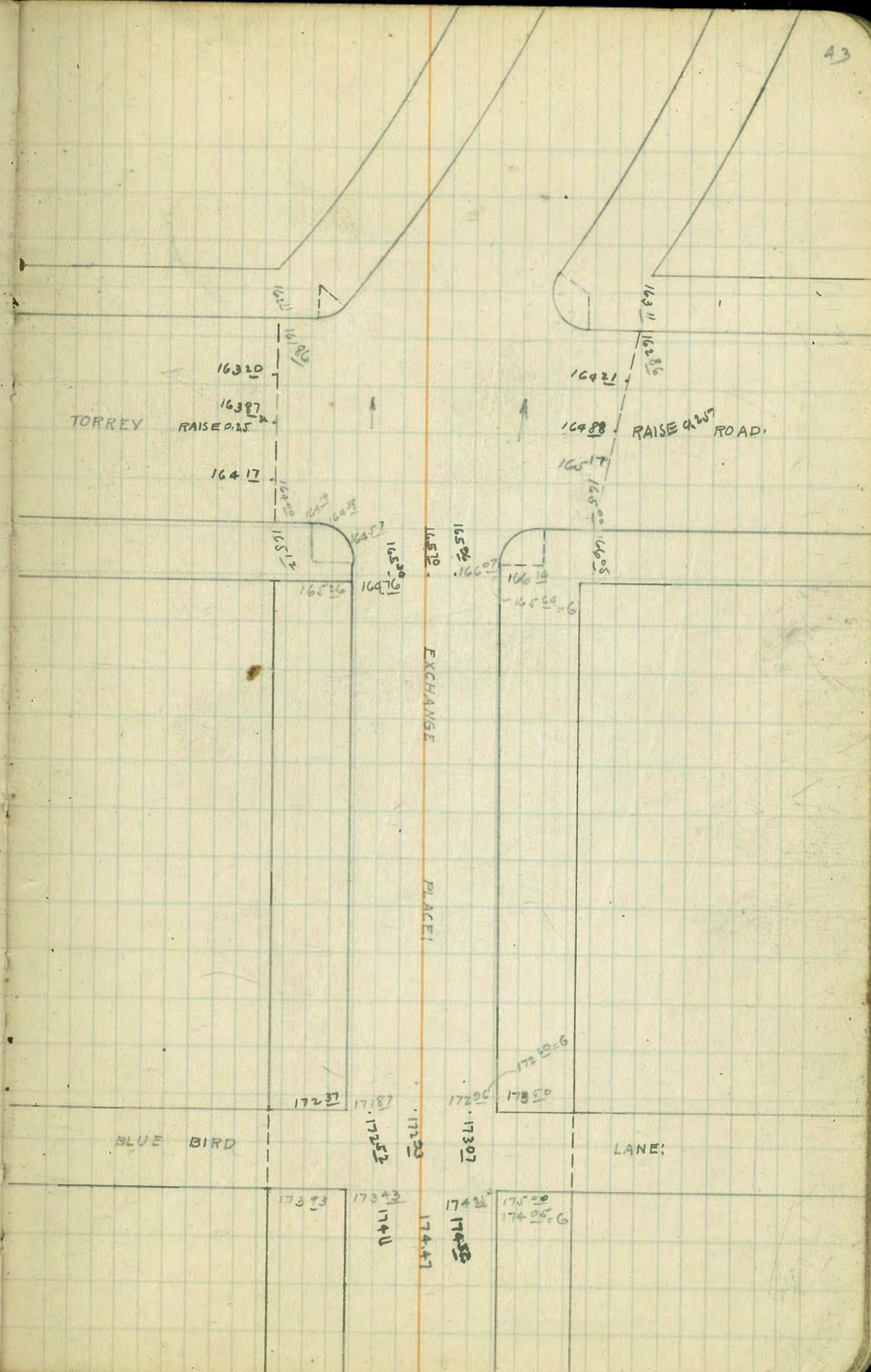


184.02
12.18
196.21
- 0.89
195.32
11.30
166.62
0.46
166.16 Hydrant.



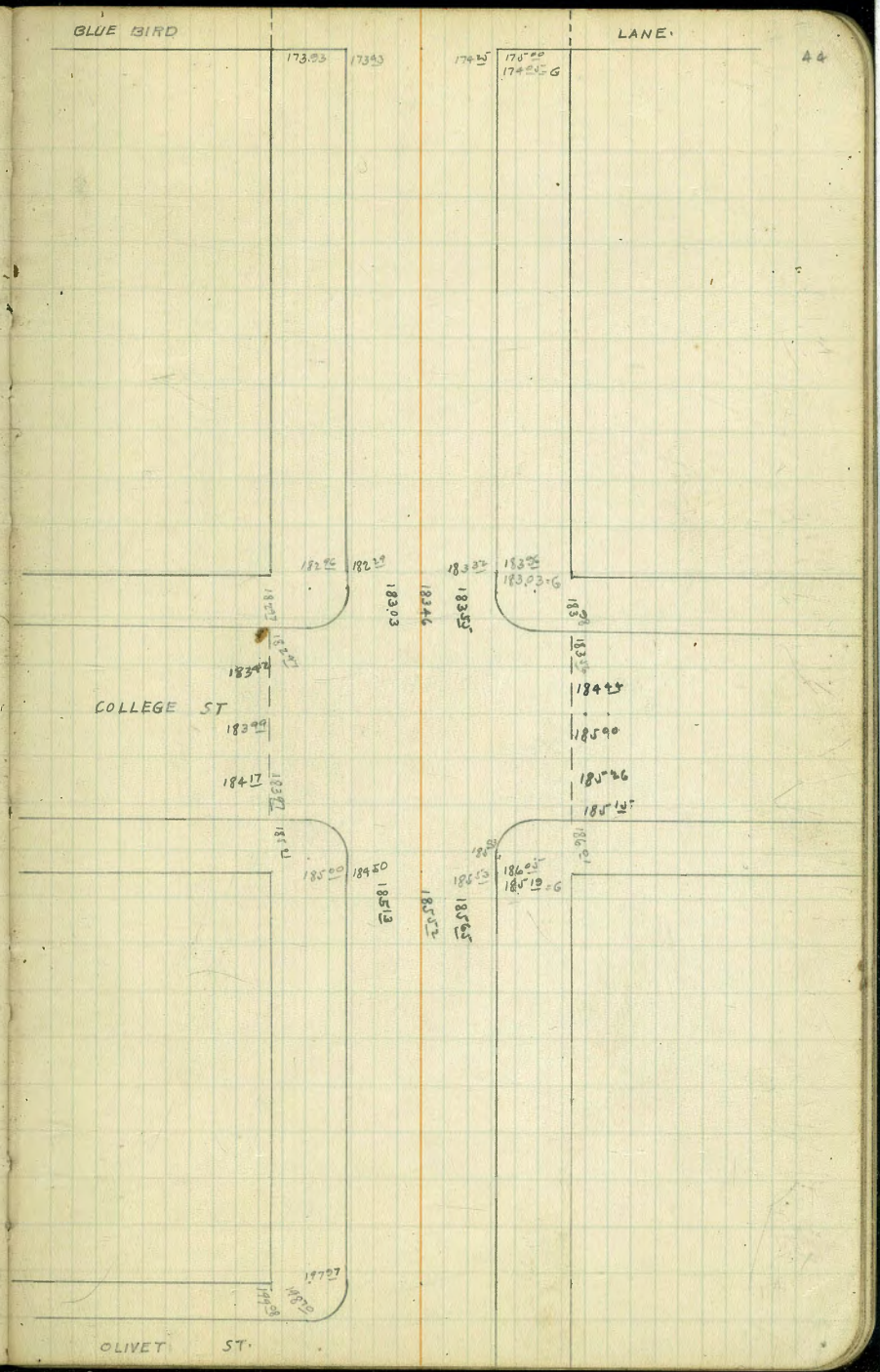
T.P. 166.16
9.87
176.03 ⊼
0.06
175.97

185.01 B.M. B.P.
+ 4.23
189.24 ⊼



189.24 A

185.01 BM.
+12.91
197.92
-0.17
197.75
+12.18
209.93 A



209.93 π
5.93
204.00 Tel pole Olivet st:

209.93
0.06
209.87
+13.06
222.93 π
.22
222.71 ~~Fire~~ hydrant: hydrant moved:
+4.80
227.51 π
-2.53
224.98
+11.80
236.78 π
-0.62
236.16 on wall:
+11.92
248.08 π

Floor. Grade lower end garage floor = 225.60
St " " " " " = 225.95
2.6 ⅝

St Grade upper end garage floor 225.35
Floor " " " " " 225.60

EXCHANGE PLACE

OLIVET ST

OLIVET LANE:

SOLEDAD AVE

MAR AVE.

C = 5.65 ~~D = 5~~ 2° 7½

A = 10.5° 2.7'
R = 76'
T = 7.976
E = 0.473'
L = 139.85
10 chords 13.98'

10°	32.7	
21°	05.4	
31	38.1	
42	10.8	
52	43.5	C = 67.49
62	16.2	
73	48.9	
84	21.6	
94	54.3	
105°	27.0	

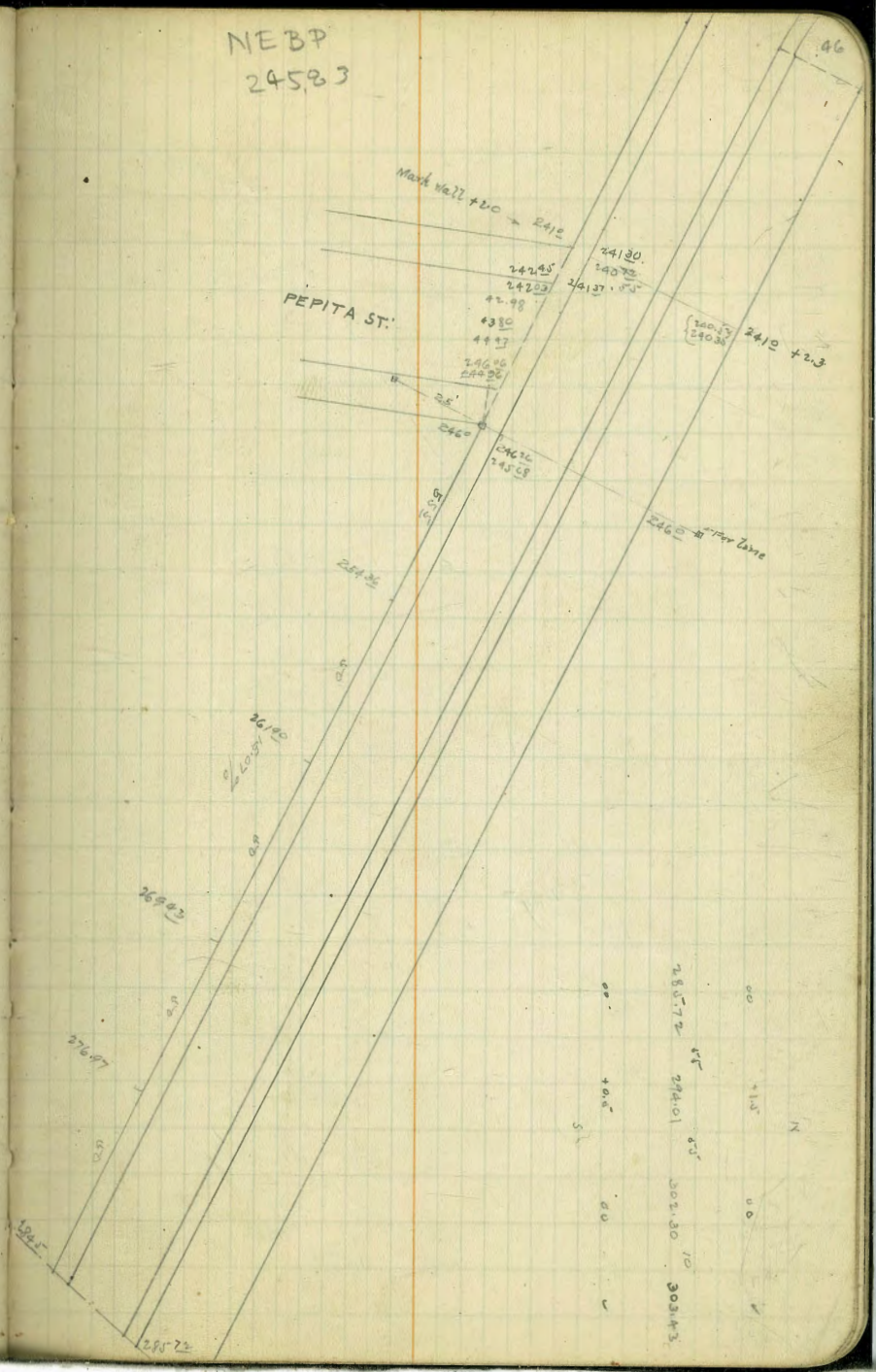
C = 13.37'

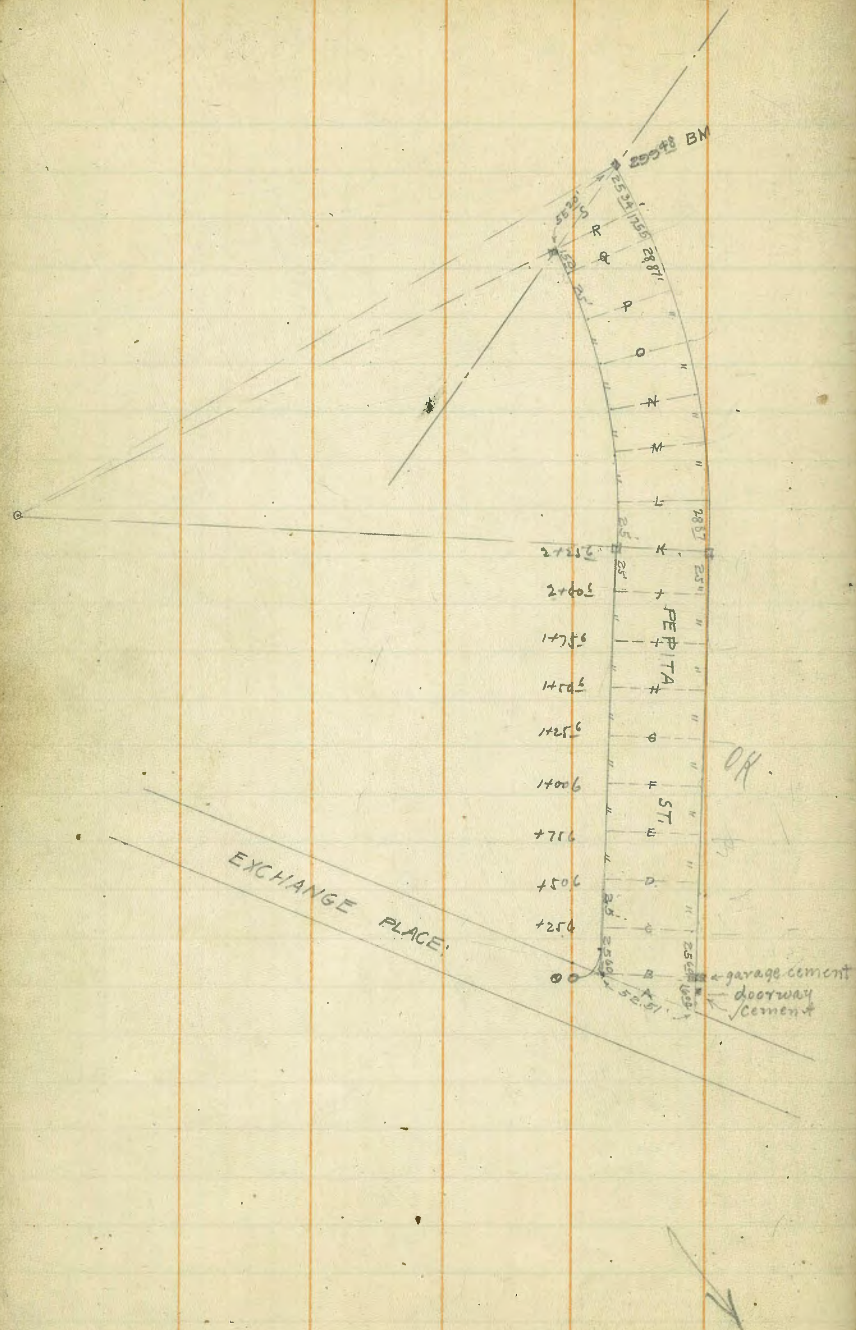
24808 T
- 030
247.78
12.35
260.13 T
0.05
260.08
+ 12.64
272.73 T
0.53
272.20
+ 12.64
284.84 T
0.43
284.41
+ 8.52
292.93 T
4.96
288.97 = Check Bobs BM Xsection notes Book 1080 Page 55 = 287.98

	W	E
	260.13	260.13
	246.25	246.25
	13.88	13.88
	10.85	7.60
	+3.03	+6.28
	260.13	260.13
	54.36	54.36
	5.77	5.77
	1.85	-0.33
	+3.92	+6.10
	272.73	272.73
	261.90	261.90
	10.83	10.83
	7.72	5.12
	+3.11	+5.71
	272.73	272.73
	269.43	269.43
	3.30	3.30
	1.29	0.77
	+2.01	+2.53
	284.84	284.84
	276.97	276.97
	7.87	7.87
	5.91	7.49
	+1.96	+0.38
	292.93	292.93
	284.50	285.72
	8.43	7.21
	6.97	6.40
	+1.46	+0.81

NEBP
24583

46




BM
PEPITA ST.
EXCHANGE PLACE
garage cement
doorway cement
OK

Sta		+	±	−	
		Xsection Pepita St 50' wide 10'Cbs 7½Q's			
		12.49	256.28 ✓		243.79 N.E. Cor Cement approach To Garage:
Sec: A	East P			8.5	47.8
	+5			8.1	48.2
	+7			9.0	47.3
+105'	cb			9.3	47.0
	+3			10.7	45.6
	+5			10.4	45.9
1838	¼			10.6	45.7
2625	℄			11.8	44.5
3403	¼			12.9	43.4
4191	cb			13.5	42.8
5000	W.L.			13.5	42.8
A+5 = ± door on Cement walk:				13.20	243.1
B	W.L. - ± Garage cement runway:			12.42	43.9
	cb = " " " "			12.43	43.9
	¼			11.8	44.5
	℄			11.0	45.3
	¼			10.1	46.2
	cb			9.0	47.3
	+2			9.1	47.2
	+5			7.3	49.0
	E.L.			8.5	47.8
C	E.L.			4.1	52.2
	+6			4.5	51.8
	+9			6.2	50.1 ✓

Platted Oct 1924 MRB. See 1437L

{ Denman, Miller, Sights, Walbrech } Oct 26-27 ✓

See sketch page 47:

Note: Plat profile each way from Sec'k to make even stations:

		+	T	−	
			256.28		
	cl			6.4	49.9
	1/4			7.1	49.2
	c			7.3	49.0
	1/4			8.1	48.2
	cl			8.7	47.6
	W.L			8.7	47.6
D	W.L			5.3	51.0
	cl			5.4	50.9
	1/4			4.5	51.8
	c			3.8	52.5
	1/4			3.2	53.1
	cl			2.8	53.5
	E.L.			1.6	54.7
#		12.46	268.29	0.95	255.83
E	E.L.			8.8	59.5
	cl			9.5	58.8
	1/2			10.5	57.8
	c			11.2	57.1
	1/4			11.8	56.5
	cl			12.5	55.8
	W.L			13.0	55.3
F	W.L			8.4	59.9
	cl			7.9	60.4
	1/2			7.4	60.9
	c			6.5	61.8
	1/2			6.0	62.3

		+	T	−	
			268.29		
	cl			5.1	63.2
	EL			5.7	62.6
#		12.38	279.95	0.72	267.57
G	E.L.			11.3	68.7
	cl			12.3	67.7
	1/4			13.0	67.0
	c			13.6	66.4
	1/4			14.8	65.2
	cl			15.1	64.9
	W.L.			15.8	64.2
H	W.L			10.8	69.2
	+9			10.3	69.7
	cl			10.9	69.1
	1/4			9.7	70.3
	c			8.8	71.2
	1/4			8.2	71.8
	+3			9.0	71.0
	cl			7.5	72.5
	+7			7.2	72.8
	E.L			5.9	74.1
I	E.L			2.4	77.6
	+4			3.5	76.5
	cl			4.2	75.8
	+3			5.9	74.1
	1/4			4.8	75.2
	c			5.1	74.9

		+	π 279.95	−	
	½			6.1	73.9
	+4			7.0	73.0
	cb			6.2	72.8
	W.L			6.5	73.5
#		12.53	292.13	0.35	279.60
J	W.L			14.8	77.3
	+9			14.4	77.7
	cb			15.7	76.4
	¼			14.4	77.7
	c			13.8	78.3
	½			13.4	78.7
	+5			14.8	77.3
	cb			12.8	79.3
	+8			12.2	79.9
	E.L.			10.9	81.2
K	=PC E.L.			9.3	83.8 Bob 83.5
	cb			9.3	82.8
	+4			10.9	81.2
	+5			10.2	81.9
	½			10.3	81.8
	c			10.6	81.5 Bob 81.4
	½			7.3	84.8
	cb			7.8	84.3
	W.L			12.0	80.1 Bob 80
L	W.L			9.1	83.0
	cb			8.6	83.5

Something wrong here see book 500.2 page 36

		+	π 292.13	−	
	+1			8.9	83.2
	¼			8.2	83.9
	c			7.5	84.6
	¼			7.2	84.9
	+5			7.7	84.4
	cb			6.3	85.8
	E.L.			5.4	86.7
M	E.W			2.5	89.6
	cb			3.2	88.9
	+2			4.2	87.9
	¼			4.2	87.9
	c			4.4	87.7
	½			5.2	86.9
	+6½			6.0	86.1
	cb			5.7	86.4
	W.L			6.0	86.1
N	W.W			3.1	89.1
	+8			2.9	89.2
	cb			3.2	88.9
	¼			2.3	89.8
	c			1.7	90.4
	½			1.5	90.6
	+6½			1.6	90.5
	cb			1.0	91.1
	EL			0.2	91.9
#		12.53	304.15	0.51	291.62

		+	π 304.15	−	
O	E.L.			9.3	294.9
	cl			9.8	294.4
	+2			10.6	293.6
	1/4			10.7	293.5
	C			10.9	293.3
	1/4			11.5	292.7
	cl			12.3	291.9
	+2			11.9	292.3
	W.L.			12.0	292.2
P	W.L			9.0	95.2
	+7			8.7	95.5
	cl			9.0	95.2
	1/4			8.4	95.8
	c			7.8	96.4
	1/4			7.7	96.5
	+5			7.9	96.3
	cl			6.7	97.5
	E.L.			6.3	97.9
Q	E.L			3.2	301.0
	cl			4.4	99.8
	1/4			4.9	99.3
	c			5.1	99.1
	1/4			6.0	98.2
	cl			6.4	97.8
	+4			5.9	98.3
	W.L			6.2	98.0 ✓

		+	π 304.15	−		
						51.
R	W.L			4.9	99.3	
	+5			4.6	99.6	
	+7			5.1	99.1	
	cl			5.0	99.2	
	1/4			3.9	300.3	
	c			3.3	300.9	
	1/4			3.0	01.2	
	cl			2.5	01.7	
	E.L			2.5	01.7	
S-P.L.	E.L			1.5	02.7	
	cl.			1.8	02.4	
	1/4			2.1	02.1	
	c			1.9	02.3	
	1/4			2.5	01.7	
	cl			3.7	01.0	
	W.L			3.9	300.4	
Hub; see sketch for B.M.				4.67		299.48 B.M.
		286	294.72	12.29		291.86
				6.75		287.97

Xsection of Exchange place from end of Contract to Golf Grounds:

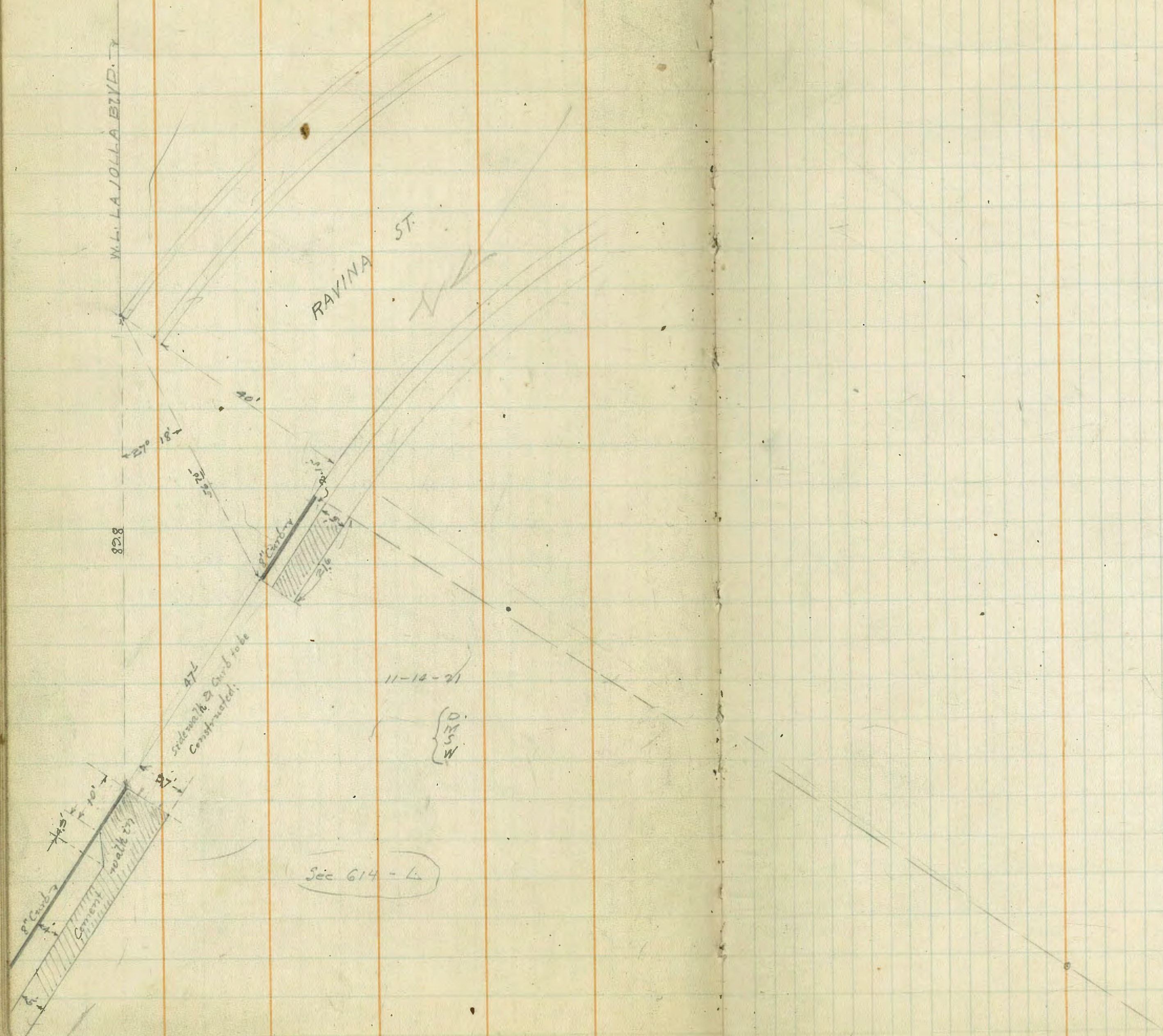
20' Road
5' Curbs

Nov 3-22
Dominant

+	T	−	
	12.98	300.95	287.97 B.M. Page 46
Along diagonal W.L.		14.6	286.4
ob		15.3	285.7
℄		15.9	285.1
cb		16.5	284.5
E.L.		16.3	284.7
00W 17.0 = Sta 00 E.L.		15.3	285.3
cb		15.6	285.4
℄		15.2	285.8
cb		15.3	285.7
W.L.		14.62	286.4
+25' W.L.		8.3	292.7
cb		8.7	292.3
+4		9.3	291.7
+6		11.0	290.0
℄		11.0	290.0
cb		11.0	290.0
E.L.		11.2	289.8
+50 E.L.		7.0	294.0
cb		6.6	294.4
℄		6.9	294.1
+3		4.0	29.2.0
cb		3.4	297.6
W.L.		3.6	297.4
+70' W.L.		1.0	300.0
cb		1.0	300.00

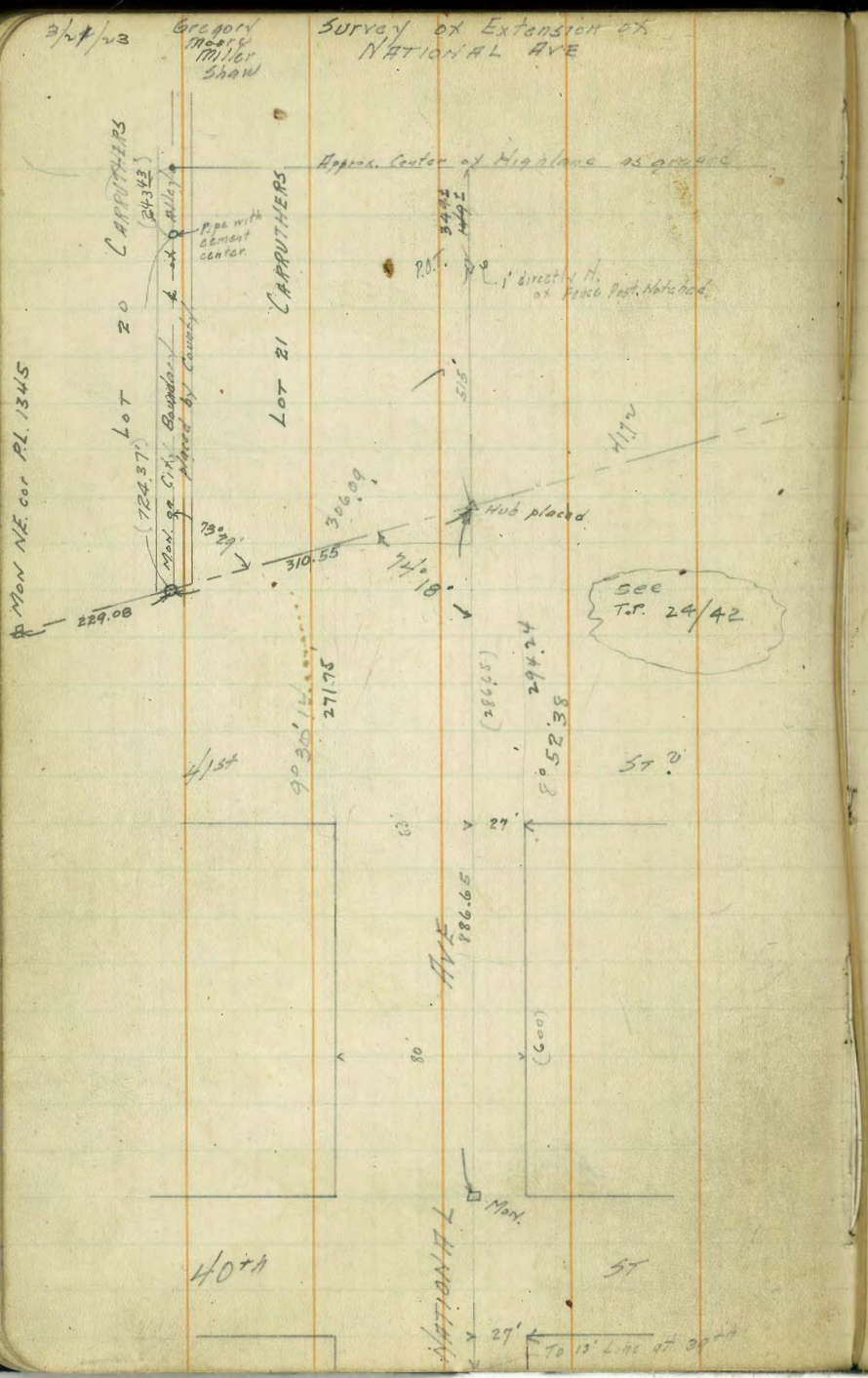
+	T 300.95'	−	
℄		1.5	299.5
+4		3.5	297.5
cb		3.0	298.0
E.L.		3.1	297.9
#	1+90	296.21	0.54 300.41
1+00 E.L.		1.0	301.3
cb		1.2	301.1
℄		1.8	301.5
cb		1.7	301.6
W.L.		1.5	301.8
1+30 = End work; W.L.		2.7	303.6
cb		2.9	303.4
℄		2.9	303.4
cb		2.8	303.5
E.L.		2.7	303.6

J.7


W.L. LAJOLLA BLVD.
RAVINA ST.
40'
27° 18'
828
8" Curb
Cement walk
47'
Sidewalk & Curb to be Constructed.
11-14-21
D M S W
Sec 614 - L

3/24/23 Gregory Moore Miller Shaw

Survey ox Extension ox NATIONAL AVE



54

4/17/23 Gregory Moore Miller

CROSS SECTION OF ALLEY BLK 1 Lynnhurst 15' wide

Dale - 30th Upas to Thorn

	5.11	331.03	325.92	BP NE 30th + Upas
		S.L. Upas		
E			4.63	326.40	on paving
C			4.90	326.1	" "
W			4.80	326.2	" "
		3' S		
W			4.5	326.5	
C			4.6	326.4	
E			4.9	326.1	
		50' S		
E			5.4	325.6	
C			5.5	325.5	
W			5.4	325.6	
		71' S		
W.			6.0	325.0	
C			5.9	325.1	
E = N. end cement pavement in yard			5.70	325.3	
		85' S		
E = S. end of above pavement.			5.81	325.22	
		105' S		
-6 = garage cement floor.			6.10	324.93	
E			6.3	324.7	
C			6.2	324.8	
W			6.2	324.8	

		150' S		
W			6.3	324.7
C			6.6	324.4
E			6.8	324.2
		175' S		
E			6.7	324.3
C			6.9	324.1
W			6.7	324.3
T.P.	3.83	327.83	7.03	324.00
		192' S		
4' E of E = cement apron.			4.00	323.83
		206' S		
W			3.8	324.0
C			4.1	323.7
E			4.1	323.7
+6.0 = garage cement floor			4.00	323.8
		242' S		
E			4.6	323.2
C			4.5	323.3
W			4.3	323.5
+6.5 = garage dirt floor.			4.4	323.4
		275' S		
W			4.8	323.0
C			4.7	323.1
E			4.7	323.1

327.83

305'S

-V = cement floor	5.18	322.65
E	5.0	322.8
C	5.0	322.8
W	5.0	322.8

350'S

W	5.4	322.4
C	5.4	322.4
E	5.4	322.4

400'S = center of double garage

-6.5 = garage dirt floor	6.1	321.7
E	6.2	321.6
C	6.2	321.6
W	6.0	321.8

450'S

W	6.3	321.5
C	6.5	321.3
E	6.3	321.5

500'S

E	6.7	321.1
C	6.8	321.0
W	6.6	321.2

550'S

W	7.1	320.7
C = Manhole.	6.80	321.03
E	7.0	320.8

590'S

E	7.9	319.9
C	8.2	319.6
+2	8.1	319.7
W	7.4	320.4

600'S. = N.L. Thorn.

W on cement curb.	8.33	319.50
C	8.8	319.0
+3	8.7	319.1
E	8.0	319.8
(E on cement curb)	8.30	319.53

4/28/23 Gregory X section of Intersection of Myrtle + Indiana
60' Wide 10' cbs
Indiana 80' - 20' - 10' 1/4s

3.35 297.40 294.05 NW Myrtle + Indiana

10" N. of NL Myrtle

W. L. Indiana	2.9	294.5
cb	3.38	294.02
gutter	3.9	293.5
1/4	3.8	293.6
+ 1.85	3.91	293.49 = west rail
c	3.8	293.6
+ 8.5	3.98	293.42
1/4	4.10	293.30 = East rail
E gutter	5.6	291.8
E cb = End of curb + Walk	4.40	293.0
E.L.	4.4	293.0

N.L Myrtle

E.L.	3.8	293.6
cb	3.5	293.9
1/4	3.9	293.5
c	3.8	293.6
1/4	3.9	293.5
W gutter	3.8	293.6
curb	3.42	293.98
W L	2.8	294.6

N curb

W L	2.95	294.45 on curb
+ 10	3.23	294.17
W cb	3.7	293.7

1/19 293

297.40

N gutter

W	3.3	294.1
cb	3.7	293.7
1/4	3.8	293.6
+ 1.4	4.03	293.37 = west rail
c	3.8	293.6
+ 9.3	3.99	293.41 = East rail
1/4	3.9	293.5
cb	3.9	293.5
E	4.1	293.3
+ 10	4.6	292.8
+ 17	4.8	292.6
+ 27	8.6	288.8
+ 35	10.1	287.3
+ 53	22.1	275.3 = natural grade

Platted Apr 30 1923 [initials]

N Quarter

E	4.1	293.3
cb	3.8	293.6
1/4	4.0	293.4
c	3.9	293.5
1/4	4.1	293.3
cb	3.6	293.8
W	2.6	294.8

Center

W	2.1	295.3
cb	3.5	293.9

	2974			
1/4		4.1	293.3	
c		4.0	293.4	
1/4		4.0	293.4	
cb		3.8	293.6	
E		3.4	294.0	
	S. Quarter			
E		4.2	293.2	
cb		3.8	293.6	
1/4		4.0	293.4	
c		3.8	293.6	
1/4		4.0	293.4	
cb		3.5	293.9	
W		2.5	294.9	
	S Curb			
(W Top Curb)		2.83	294.57	
W		3.5	293.9	
cb		3.7	293.7	
+9.6		4.05	293.35	W rail
1/4		4.1	293.3	
B		3.9	293.5	
1/4		4.0	293.4	
+0.3		3.97	293.43	E. rail
cb		4.0	293.4	
E		4.4	293.0	
+5		4.3	293.1	
+7		3.2	294.2	

	2974			
+18		2.6	294.8	
+26		5.6	291.8	
+34		11.0	286.4	
+48		18.0	279.4	
+58		22.2	275.2	= natural grd.

Plotted April 30 1933 H.P.B.

5/8/23 Gregory Moore Miller & W

Sewer Construction Blk B Prospect Park
& .x Alley E. ox La Jolla Blvd
from M.H. in E+W Alley 5 ox Westbourne
to

				spk 5E Westbourne +La Jolla	
M.H. ℄ ox E+W	7.68	88.99	81.22		
Alley ~0+00		8.90		80.0	
+50		5.87	83.03	80.37	+2.66
1		5.16	83.74	80.75	+2.99
+32 D.E.		3.46	85.44	80.99	+4.45

3.2
7.1
7.60
22.4
2.40

5/8/23 Gregory Moore Miller CW

CROSS SECTION OF PRINCESS ST 50' ST 10' cbs from Torrey Road to N.E. End

	5.86	89.65	83.79	nail in pole Sta 13+58

N. Edge Paving

E	4.40	85.25	on paving
cb	4.58	85.07	✓ ✓
1/4	4.71	84.94	✓ ✓
c	4.84	84.81	✓ ✓
1/4	4.94	84.71	
cb	5.02	84.63	
W	5.12	84.53	

6.8 N of Edge Paving on W / E } = 0+00 Sect

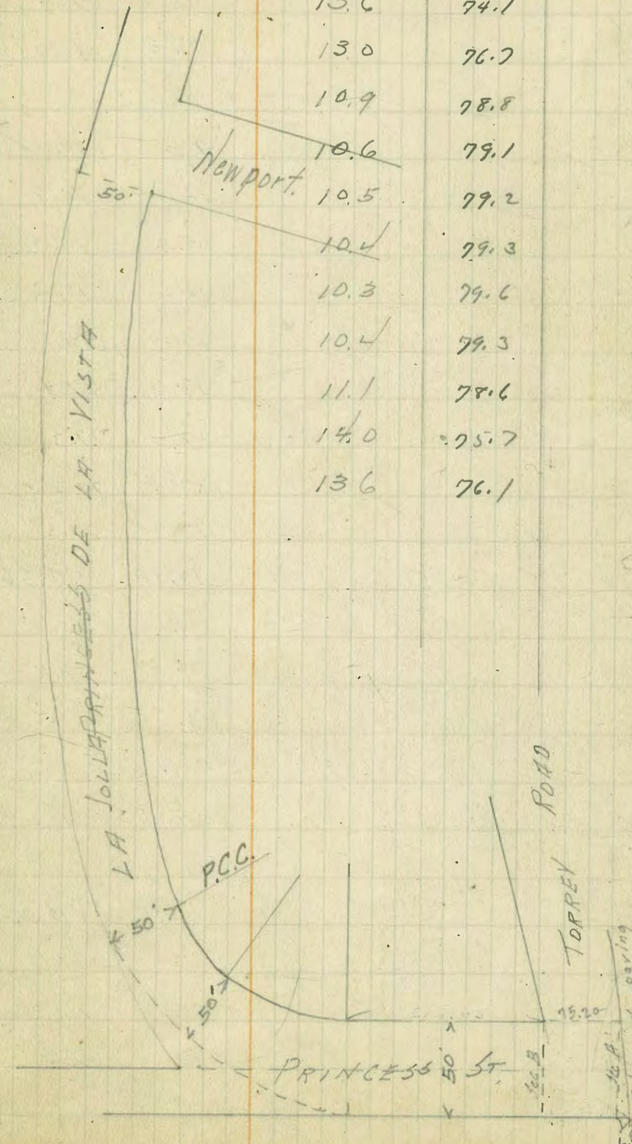
W	5.9	83.8
cb	5.8	83.9
1/4	5.7	84.0
c	5.5	84.2
1/4	5.0	84.7
cb	4.8	84.9
E	4.40	85.3

30' N of A

-15	9.7	80.0
E	8.2	81.5
cb	8.9	80.8
1/4	9.2	80.5
c	9.0	80.7
1/4	9.0	80.7
cb	9.3	80.4
W	9.3	80.4
+5	12.3	77.4

45' N 89.7

-15	17.0	72.7
-5	15.6	74.1
W	13.0	76.7
+4	10.9	78.8
cb	10.6	79.1
1/4	10.5	79.2
c	10.4	79.3
1/4	10.3	79.6
+5.5	10.4	79.3
cb	11.1	78.6
E	14.0	75.7
+15	13.6	76.1



		89.65		
		70' N		
-3			9.8	79.9
E			15.2	74.5
cb			14.3	75.4
		75.20' N = Sec B.		
-3			9.3	80.4
E			12.8	76.9
+2			15.3	74.4
cb			14.4	75.3
1/4			12.4	77.3
C			12.3	77.4
1/2			12.4	77.3
cb			12.4	77.3
+6			12.2	77.5
T.P.	2.05	79.41	12.29	77.36
W			4.00	75.4
+7			8.8	70.6
+20			11.8	68.6
		7.5' N + 9' W. of E Line =		
(Flow Line)		Inlet of 24" Conc. pipe	5.17	74.24
		25' N		
-25			15.1	64.3
-15			13.3	66.1
W			6.1	73.3
+5			3.5	75.9
cb			3.4	76.0

7.5 + 9 W
36' N + 11' W
13.40
15.40
10.20

7941

1/4		3.1	76.3
C		3.2	76.2
1/4		3.4	76.0
cb		5.5	73.9
+7		5.1	74.3
E		+1.9	81.3
	36' N + 11' W of W.L. = Outlet 24" pipe		
Flow Line =		10.2	69.21
	50' N		
E		0.3	79.1
+2.5		5.1	74.3
cb		5.8	73.6
1/4		4.7	74.7
C		4.5	75.0
1/2		4.2	75.2
cb		4.3	75.1
+7		4.4	75.0
W		6.6	72.8
+13		15.3	64.1
+25		15.5	63.9
	100' N		
-20		11.0	68.4
-12		9.8	69.6
W		6.1	73.3
cb		6.2	73.2
1/4		6.1	73.3

794/

c		6.2	73.2	
1/4		6.4	73.0	
cb		6.6	72.8	
E		5.8	73.6	
	120' N			
E		4.6	74.8	
+3		6.9	72.5	
cb		7.0	72.4	
1/4		7.0	72.4	
c		6.8	72.6	
1/4		6.7	72.7	
cb		6.8	72.6	
W		6.7	72.7	
	150' N			
W		8.3	71.1	
cb		8.0	71.4	
1/4		7.8	71.6	
c		7.7	71.7	
1/4		7.6	71.8	
cb		7.4	72.0	
E		7.0	72.4	
	157' N			
8 W o x W L = Garage		8.65	70.76	= Floor
	300' N			
E		9.1	70.3	
cb		9.5	69.9	

157 8.6'

PRINCESS

211.61'
56.46
268.11

1/4		9.4	70.0
c		9.7	69.7
1/4		9.6	69.8
cb		9.8	69.6
W		10.5	68.9
+10 = lawn + garden		10.4	69.0
	232.86' N on E		
	235.27' - - W		
-1		11.5	67.9
W		11.3	68.1
cb		11.3	68.1
1/4		11.4	68.0
+6 = Catch Basin		11.8	67.6
c		11.0	68.4
+3		10.2	69.2
1/4		10.2	69.2
cb		10.1	69.3
E		9.7	69.7
	272.11' N on E		
	280.92' - - W		
E		9.8	69.6
cb		10.1	69.3
1/4		10.1	69.3
c		10.3	69.1
+3.5		13.0	66.4
1/4		13.0	66.4
cb		12.7	66.7
W		13.1	66.3
+5		13.1	66.3

79.41

T.P	6.52	73.23	12.70	66.71
		313.64 N of E	PCC	
		347.36 ~ ~ W		
-15			9.1	64.1
W			8.5	64.4
cb			9.1	64.1
+4			9.1	64.1
1/4			6.6	66.6
C			3.8	69.4
1/4			3.8	69.4
cb			3.9	69.3
E			4.0	69.2
		347.71 N of E		
		375.95 ~ ~ W		
E			0.9	72.3
+5			4.2	69.0
cb			4.4	68.8
1/4			4.1	69.1
C			3.8	69.4
1/4			3.7	69.5
+3			4.0	69.2
cb			6.1	67.1
W			11.8	61.4
+15			11.8	61.4
+35			12.8	60.4
		364.71 N of E		
		400.19 ~ ~ W		
W			4.0	69.2
cb			3.9	69.3

26811
3407
30218

6607
D2
3407

63

H.I 73.23

1/4	3.7	69.5
C	3.6	69.6
1/4	3.9	69.3
cb	4.4	68.8
+5	3.1	70.1
E	2.8	70.4
	399.71 N on E = P.C.C.	
	450.11 ~ ~ W	
E	3.94	70.29 ~ on hub
cb	3.8	69.4
1/4	3.7	69.5
C	3.6	69.6
1/4	3.5	69.7
cb	3.8	69.4
W	4.2	69.0
	429.71 N on E 26/37	
	481.31 ~ ~ W	
W	4.6	68.6
cb	4.4	68.8
1/4	4.2	69.0
C	4.0	69.2
1/4	4.0	69.2
cb	4.2	69.0
+6	3.2	70.0
E	3.2	70.0
	479.71 N on E	
	533.31 ~ ~ W	
E	3.4	69.8
+3	4.4	68.8

73.23

cb			5.2	68.0
1/4			5.5	67.7
C			5.3	67.9
1/4			5.2	68.0
cb			5.1	68.1
W			5.5	67.7
		529.71 N on E		
		585.3 ✓ ~ W		
W			7.2	66.0
cb			7.0	66.2
1/4			7.0	66.2
C			7.3	65.9
1/4			7.3	65.9
cb			6.3	66.9
+2			6.3	66.9
+5			4.9	68.3
E			4.7	68.5
		579.71 N on E		
		637.49 ✓ ~ W		
E			6.4	66.8
cb			6.7	66.5
+4			8.4	64.8
1/4			8.7	64.5
C			9.5	63.7
1/4			9.5	63.7
cb			9.5	63.7
W			10.2	63.0
+5			10.5	62.7

579.71
15.06
594.77
50

H.I = 73.23

64

		609.71 N on E		
		668.5 ✓ ~ W		
W			11.7	61.5
cb			11.3	61.9
1/4			11.6	61.6
C			10.5	61.7 ✓
+5			10.0	63.2
1/4			8.5	64.7
cb			8.2	65.0
E			7.6	65.6
		644.77 N on E	40-42	
		704.97 ✓ ~ W		
E			9.2	64.0
cb			9.9	63.3
1/4			10.6	62.6
+4			11.0	62.2
C			12.5	60.7 ✓
1/4			12.8	60.4
+1			14.0	59.2
cb			13.9	59.3
W			13.9	59.3
+5			13.9	59.3
T.P.	0.72	61.41	12.54 ✓	60.69
		756.96 N on W		
		694.77 N on E	41-42	
-10			6.3	55.1
W			6.2	55.2
cb			6.0	55.4
1/4			4.8	56.6

61.41

+5			4.5	56.9	
c			3.1	58.3	
1/4			4.5	58.9	
cb			4.0	59.4	
E			1.5	59.9	
		744.71 N. on E 42.43 808.95 ~ W			
E			5.9	55.5	
cb			6.7	54.7	
1/4			7.2	54.2	
c			7.9	53.5	✓
1/4			8.7	52.7	
cb			10.1	51.3	
W			9.8	51.6	
+10			10.3	51.1	
		794.71 N. on E 48.44 860.94 ~ W			
-10			13.3	48.1	
W			12.8	48.6	
cb			13.0	48.4	
1/4			11.9	48.5	
c			10.7	50.7	✓
1/4			9.9	51.5	
cb			9.2	52.2	
E			8.3	53.1	
T.P.	0.53	51.02 844.71 N. on E 44.45 913.93 ~ W	10.92	50.49	
E			1.5	49.5	

H1 = 51.02

65

cb		2.1	48.9	
1/4		2.8	48.2	
c		3.5	47.5	✓
1/4		4.3	46.7	
cb		5.5	45.5	
W		5.3	45.7	
+10		5.7	45.3	
	894.71 N. on E 45.46 964.92 ~ W			
-10		8.8	42.2	
W		8.6	42.4	
cb		8.7	42.3	
1/4		7.2	43.8	
c		5.5	45.3	✓
1/4		5.1	45.9	
cb		4.6	46.4	
E		3.8	47.2	
	944.71 N. on E 46.47 1016.91 ~ W			
E		4.9	46.1	
cb		5.4	45.6	
1/4		6.5	44.5	
c		7.6	43.4	✓
1/4		9.1	41.9	
+4		12.0	39.0	
cb		12.1	38.9	
W		11.8	39.2	
+10		12.0	39.0	

TP	3.44	42.27	12.19	38.83	51.42
		996.16 N. on E = W.L. Newport Terrace			
		1070.47 ~ W			
-5			6.1	36.2	
W.			5.8	36.5	
cb			5.7	36.6	
1/4			5.7	36.6	
C			4.4	37.9 ✓	
1/4			5.1	37.2	
cb			5.0	37.3	
E			4.4	37.9	
+10			4.0	38.3	
		75.71' N. = L ox Newport Terrace			
E			4.6	37.7	
cb			4.7	37.6	
1/4			4.6	37.7	
C			5.0	37.3 ✓	
+4			6.4	35.9	
1/4			6.6	35.7	
cb			6.8	35.5	
W			7.1	35.2	
+10			7.8	34.5	
		75.71' N. ox Last Section = E.L. Newport			
-10			9.1	33.2	
W			8.2	34.1	
cb			7.7	34.6	
1/4			7.4	34.9	
C			7.1	35.2	
+2			5.1	37.2	
					1/4
					cb
					E
					+5
					E
					cb
					+5
					1/4
					+6
					C
					1/4
					cb
					W
					+10
					-10
					W
					cb
					1/4
					C
					+5
					1/4
					+5
					cb
					E

89.27
37.85
51.42
HI = 42.27

944.71
51.42
996.16

6C

4.9	37.4
4.7	37.6
4.8	37.5
4.4	37.9

37.85' N. ox E.L. ox Newport = PC

3.7	38.6
4.5	37.8
4.8	37.5
10.3	32.0
13.7	28.6
10.0	32.3 ✓
9.9	32.4
10.1	32.2
10.5	31.8
11.1	31.2

26' N on E
17.33 ~ W

11.8	30.5
11.8	30.5
11.5	30.8
11.5	30.8
11.2	31.1 ✓
14.8	27.5
14.0	28.3
5.0	37.3
4.7	37.6
3.3	39.0

4-2-27

63.65 N. on E } = E.L. La Jolla Vista
4-4.41 ✓ - W }

E	6.96	35.31	on hub
+8	7.9	34.4	
cb	9.8	32.5	
1/4	17.2	25.1	
+4	17.0	25.3	
C	13.8	28.5	
1/4	14.0	28.3	
cb	14.0	28.3	
W	14.05	28.3	
+10	14.4	27.9	

5/15/23 Gregory. CUTS FOR WATER LINE
La Solla Dela Vista Drive

	11.58	4689		35.31		
Stations on E.L. of 50' St.					GRADE	
W.L. Newport Terrace			9.50	39.39	34.75	+2.64
+51.45			1.7	45.2	37.79	+7.4
1+01.45	12.50	58.72	0.67	46.22	40.74	+5.5
+51.45			10.0	48.7	43.70	+5
2+01.45			6.7	52.0	46.65	5.4
+51.45			4.2	54.5	49.61	4.9
	17.96	70.77	091	57.81		
3+01.46			11.7	59.1	52.56	6.6
+51.45			7.6	63.2	55.52	7.7
4+16.57			5.4	65.4	59.36	6.0
+66.57			4.1	66.7	62.31	4.4
5+16.57			2.9	67.9	65.75	2.7
+30.68			2.1	68.7	65.40	3.3
+80.68			1.4	69.4	65.59	3.9
6+30.68			1.8	69.0	6588	3.1
6+P.+80.68	4.72	74.13	1.36	69.41	66.17	3.7
7+30.			4.7	69.4	66.46	3.0
7+80.68			4.7	69.4	66.75	2.6
			38.4	70.29		

7/24/23 Gregory. CROSS SECTION OF FERN ST 60' wide
Ivy to Juniper

	2.15	287.23		285.08
W cb on cement.	285.0		2.31	84.92
3' E = E. Edge C.B. (on top)			2.38	84.85
W 1/4 on pavement			3.11	84.12
C "	284.0		3.33	83.90
E 1/4 " "			3.83	83.40
+7 = W edge of C.B.			4.22	83.01
E. Cb on cement.	283.0		4.32	82.91

Cb is in on W side from SL Juniper to 5' S
" " " " E " " " " " NL Ivy.

28.8' S = S. End of 7' sidewalk on W side

E cb on cement.	282.9		4.39	82.84
" gutter			5.1	82.13
1/4			3.8	83.43
E rail			3.77	83.46
C	283.9		3.5	83.7
W rail			3.30	83.93
1/4			3.4	83.8
cb	284.9		2.5	84.7
+3.0 = Edge of sidewalk			2.26	84.97
W = W. " "			1.91	85.32

65 S

W			2.2	85.0
+9			2.7	84.5
cb	284.78		3.3	83.9

287.23

1/4			3.4	83.8
C	283.78		3.7	83.5
1/4			4.0	83.2
E gutter			5.1	82.1
" cb on cement.	282.78		4.45	82.78

105' S

E cb on cement	282.65		4.57	82.66
E gutter			5.0	82.2
1/4			4.0	83.2
E rail			3.92	83.31
C	283.65		3.6	83.6
W rail			3.46	83.77
1/4			3.5	83.7
cb	284.65		2.8	84.4
W			2.4	84.8

140' S = Approx. PC of car tracks

W			2.4	84.8
cb	284.53		3.0	84.2
+2			3.6	83.6
1/4			3.7	83.5
W. rail			3.67	83.56
C	283.53		3.9	83.3
E rail			3.98	83.25
1/4			4.2	83.0
+4			4.4	82.8
E gutter			5.2	82.0
" Eb on cement	282.53		4.65	82.58

287.73

165'5

E cb on cement	28245	4.80	824
~ gutter		5.5	81.7
+6		4.3	82.9
1/4		4.7	830
+3.7 = E rail.		3.91	833
c	28345	4.1	831
+9.97 = W rail		3.70	835
1/4		3.7	83.5
+8		3.5	83.7
cb	28445	2.8	844
W		2.6	84.6
	198.80 = where west rail intersects W cb		
W		2.7	84.5
cb for yardage	28434	3.1	84.1
✓ = W rail		3.37	8386
1/4		3.5	83.7
+7.5 E rail		3.70	835
c	28334	3.7	835
1/4		4.1	83.1
+4		4.5	82.7
E gutter		5.3	81.9
~ cb on cement	28134	4.88	8235

✓

287.73

218.70 = where west rail intersects W.L. of St.

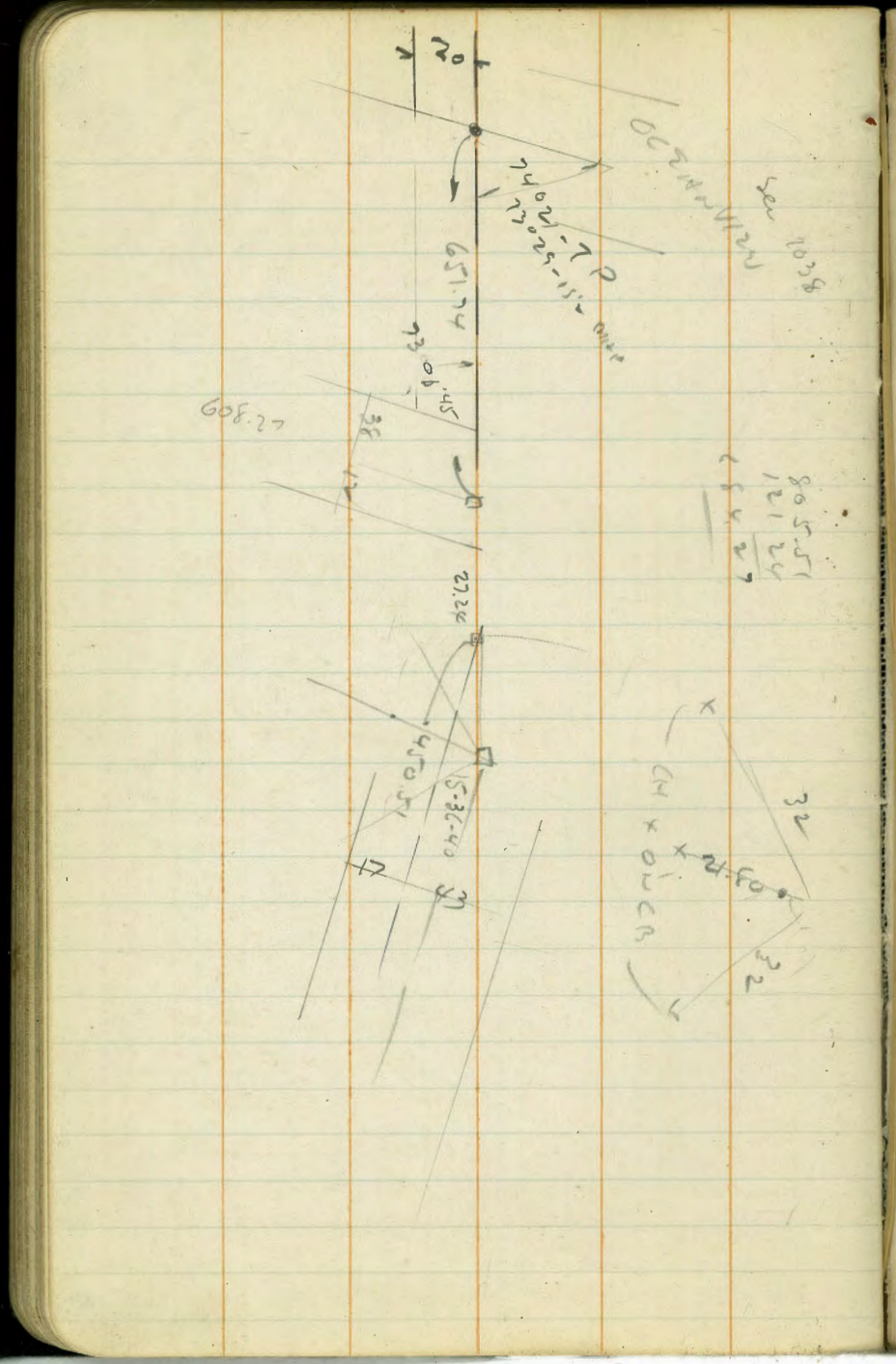
E cb on cement	28227	4.90	823
~ gutter		5.5	81.7
+6		4.6	82.6
1/4		4.4	82.8
c	28327	3.7	835
+10.1 = E rail		3.45	8378
cb	28427	3.0	842
W.L = W rail		3.00	84.2
	234.53 = where E rail intersects W cb		
W cb = E rail		3.17	8406
	240.3 = N. end of Cement Cb & Walk on W.		
W		3.1	84.1
W cb on cement	28427	3.12	8411
W. gutter		3.4	83.8
1/4		3.7	83.5
c	28327	4.1	83.1
1/4		4.4	82.8
+4		4.6	82.6
E gutter		5.5	81.7
~ cb on cement	28227	4.98	82.25
	246.95 = where E rail intersects W.L. of St.		
W.L. on E rail		2.85	84.38
	W.L. W.		
E cb on cement	28207	5.24	81.99
~ gutter		5.8	81.4

✓

28723

+6			5.0	84.2
1/4			4.9	82.3
C	283.0		4.6	82.6
1/4			4.2	83.0
W gutter			3.9	83.3
v cb on cement	284.0		3.22	84.01

✓



IMPROVED TABLES
AND
INFORMATION

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2	+	71°	4086.9	1308.2	+	81°	4893.6	1805.3	+
10′	3386.3	925.9	5° C.	10′	4099.5	1315.6	5° C.	10′	4908.0	1814.7	5° C.
20′	3397.5	931.6	T	20′	4112.1	1322.9	T	20′	4922.5	1824.1	T
30′	3408.8	937.3	.25	30′	4124.8	1330.3	.30	30′	4937.0	1833.6	.36
40′	3420.1	943.1	E	40′	4137.4	1337.7	E	40′	4951.5	1843.1	E
50′	3431.4	948.9		50′	4150.1	1345.1		50′	4966.1	1852.6	
62°	3442.7	954.8	.080	72°	4162.8	1352.6	.110	82°	4980.7	1862.2	.149
10′	3454.1	960.6		10′	4175.6	1360.1		10′	4995.4	1871.8	
20′	3465.4	966.5		20′	4188.5	1367.6		20′	5010.0	1881.5	
30′	3476.8	972.4		30′	4201.2	1375.2		30′	5024.8	1891.2	
40′	3488.3	978.3		40′	4214.0	1382.8		40′	5039.5	1900.9	
50′	3499.7	984.3		50′	4226.8	1390.4		50′	5054.3	1910.7	
63°	3511.1	990.2	10° C.	73°	4239.7	1398.0	10° C.	83°	5069.2	1920.5	10° C.
10′	3522.6	996.2	T	10′	4252.6	1405.7	T	10′	5084.0	1930.4	T
20′	3534.1	1002.3	.51	20′	4265.6	1413.5	.61	20′	5099.0	1940.3	.72
30′	3545.6	1008.3	E	30′	4278.5	1421.2	E	30′	5113.9	1950.3	E
40′	3557.2	1014.4	.159	40′	4291.5	1429.0	.220	40′	5128.9	1960.2	.299
50′	3568.7	1020.5		50′	4304.6	1436.8		50′	5143.9	1970.3	
64°	3580.3	1026.6		74°	4317.6	1444.6		84°	5159.0	1980.4	
10′	3591.9	1032.8		10′	4330.7	1452.5		10′	5174.1	1990.5	
20′	3603.5	1039.0		20′	4343.8	1460.4		20′	5189.3	2000.6	
30′	3615.1	1045.2		30′	4356.9	1468.4		30′	5204.4	2010.8	
40′	3626.8	1051.4		40′	4370.1	1476.4		40′	5219.7	2021.1	
50′	3638.5	1057.7	15° C.	50′	4383.3	1484.4	15° C.	50′	5234.9	2031.4	15° C.
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T
10′	3661.9	1070.2	.76	10′	4409.8	1500.5	.91	10′	5265.6	2052.1	1.09
20′	3673.7	1076.6	E	20′	4423.1	1508.6	E	20′	5281.0	2062.5	E
30′	3685.4	1082.9	.240	30′	4436.4	1516.7	.332	30′	5296.4	2073.0	.450
40′	3697.2	1089.3		40′	4449.7	1524.9		40′	5311.9	2083.5	
50′	3709.0	1095.7		50′	4463.1	1533.1		50′	5327.4	2094.1	
66°	3720.9	1102.2		76°	4476.5	1541.4		86°	5343.0	2104.7	
10′	3732.7	1108.6		10′	4489.9	1549.7		10′	5358.6	2115.3	
20′	3744.6	1115.1		20′	4503.4	1558.0		20′	5374.2	2126.0	
30′	3756.5	1121.7		30′	4516.9	1566.3		30′	5389.9	2136.7	
40′	3768.5	1128.2	20° C.	40′	4530.4	1574.7	20° C.	40′	5405.6	2147.5	20° C.
50′	3780.4	1134.8	T	50′	4544.0	1583.1	T	50′	5421.4	2158.4	T
			1.02				1.22				1.45
67°	3792.4	1141.4	E	77°	4557.6	1591.6	E	87°	5437.2	2169.2	E
10′	3804.4	1148.0	.321	10′	4571.2	1600.1	.445	10′	5453.1	2180.2	.603
20′	3816.4	1154.7		20′	4584.8	1608.6		20′	5469.0	2191.1	
30′	3828.4	1161.3		30′	4598.5	1617.1		30′	5484.9	2202.2	
40′	3840.5	1168.1		40′	4612.2	1625.7		40′	5500.9	2213.2	
50′	3852.6	1174.8		50′	4626.0	1634.4		50′	5517.0	2224.3	
68°	3864.7	1181.6		78°	4639.8	1643.0		88°	5533.1	2235.5	
10′	3876.8	1188.4	25° C.	10	4653.6	1651.7	25° C.	10′	5549.2	2246.7	25° C
20′	3889.0	1195.2	T	20′	4667.4	1660.5	T	20′	5565.4	2258.0	T
30	3901.2	1202.0	1.28	30′	4681.3	1669.2	1.53	30′	5581.6	2269.3	1.83
40′	3913.4	1208.9	E	40′	4695.2	1678.1	E	40′	5597.8	2280.6	E
50′	3925.6	1215.8		50′	4709.2	1686.9		50′	5614.2	2292.0	
69°	3937.9	1222.7	.403	79°	4723.2	1695.8	.558	89°	5630.5	2303.5	.756
10′	3950.2	1229.7		10′	4737.2	1704.7		10′	5646.9	2315.0	
20′	3962.5	1236.7		20′	4751.2	1713.7		20′	5663.4	2326.6	
30′	3974.8	1243.7		30′	4765.3	1722.7		30′	5679.9	2338.2	
40′	3987.2	1250.8		40′	4779.4	1731.7		40′	5696.4	2349.8	
50′	3999.5	1257.9		50′	4793.6	1740.8		50′	5713.0	2361.5	
70°	4011.9	1265.0	30° C.	80°	4807.7	1749.9	30° C.	90°	5729.7	2373.3	30° C.
10′	4024.4	1272.1	T	10′	4822.0	1759.0	T	10′	5746.3	2385.1	T
20′	4036.8	1279.3	1.54	20′	4836.2	1768.2	1.84	20′	5763.1	2397.0	2.20
30′	4049.3	1286.5	E	30′	4850.5	1777.4	E	30′	5779.9	2408.9	E
40′	4061.8	1293.6	.485	40′	4864.8	1786.7	.671	40′	5796.7	2420.9	.910
50′	4074.4	1300.9		50′	4879.2	1796.0		50′	5813.6	2432.9	

T = R tan ½ I E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	
10′	5847.5	2457.1	5° C.	10′	6971.3	3294.1	5° C.	10′	8362.7	4407.6	+
20′	5864.6	2469.3	T	20′	6992.0	3310.1	T	20′	8388.9	4429.2	5° C.
30′	5881.7	2481.5	.43	30′	7012.7	3326.1	.51	30′	8415.1	4450.9	T
40′	5898.8	2493.8	E	40′	7033.6	3342.3	E	40′	8441.5	4472.7	.62
50′	5916.0	2506.1		50′	7054.5	3358.5		50′	8468.0	4494.6	E
92°	5933.2	2518.5	.200	102°	7075.5	3374.9	.268	112°	8494.6	4516.6	.360
10′	5950.5	2531.0		10′	7096.6	3391.2		10′	8521.3	4538.8	
20′	5967.9	2543.5		20′	7117.8	3407.7		20′	8548.1	4561.1	
30′	5985.3	2556.0		30′	7139.0	3424.3		30′	8575.0	4583.4	
40′	6002.7	2568.6		40′	7160.3	3440.9		40′	8602.1	4606.0	
50′	6020.2	2581.3		50′	7181.7	3457.6		50′	8629.3	4628.6	
93°	6037.8	2594.0	10° C.	103°	7203.2	3474.4	10° C.	113°	8656.6	4651.3	10° C.
10′	6055.4	2606.8	T	10′	7224.7	3491.3	T	10′	8684.0	4674.2	T
20′	6073.1	2619.7	.86	20′	7246.3	3508.2	.103	20′	8711.5	4697.2	1.25
30′	6090.8	2632.6	E	30′	7268.0	3525.2	E	30′	8739.2	4720.3	E
40′	6108.6	2645.5	.401	40′	7289.8	3542.4	.536	40′	8767.0	4743.6	.721
50′	6126.4	2658.5		50′	7311.7	3559.6		50′	8794.9	4766.9	
94°	6144.3	2671.6		104°	7333.6	3576.8		114°	8822.9	4790.4	
10′	6162.2	2684.7		10′	7355.6	3594.2		10′	8851.0	4814.1	
20′	6180.2	2697.9		20′	7377.8	3611.7		20′	8879.3	4837.8	
30′	6198.3	2711.2		30′	7399.9	3629.2		30′	8907.7	4861.7	
40′	6216.4	2724.5		40′	7422.2	3646.8		40′	8936.3	4885.7	
50′	6234.6	2737.9	15° C.	50′	7444.6	3664.5	15° C.	50′	8965.0	4909.9	15° C.
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T
10′	6271.1	2764.8	1.30	10′	7489.6	3700.2	1.56	10′	9022.7	4958.6	1.93
20′	6289.4	2778.3	E	20′	7512.2	3718.2	E	20′	9051.7	4983.1	E
30′	6307.9	2792.0	.604	30′	7534.9	3736.2	.806	30′	9080.9	5007.8	1.09
40′	6326.3	2805.6		40′	7557.7	3754.4		40′	9110.3	5032.6	
50′	6344.8	2819.4		50′	7580.5	3772.6		50′	9139.8	5057.6	
96°	6363.4	2833.2		106°	7603.5	3791.0		116°	9169.4	5082.7	
10′	6382.1	2847.0		10′	7626.6	3809.4		10′	9199.1	5107.9	
20′	6400.8	2861.0		20′	7649.7	3827.9		20′	9229.0	5133.3	
30′	6419.5	2875.0		30′	7672.9	3846.5		30′	9259.0	5158.8	
40′	6438.4	2889.0	20° C.	40′	7696.3	3865.2	20° C.	40′	9289.2	5184.5	20° C.
50′	6457.3	2903.1	T	50′	7719.7	3884.0	T	50′	9319.5	5210.3	T
			1.74				2.08				2.52
97°	6476.2	2917.3	E	107°	7743.2	3902.9	E	117°	9349.9	5236.2	E
10′	6495.2	2931.6	.809	10′	7766.8	3921.9	1.08	10′	9380.5	5262.3	1.46
20′	6514.3	2945.9		20′	7790.5	3940.9		20′	9411.3	5288.6	
30′	6533.4	2960.3		30′	7814.3	3960.1		30′	9442.2	5315.0	
40′	6552.6	2974.7		40′	7838.1	3979.4		40′	9473.2	5341.5	
50′	6571.9	2989.2		50′	7862.1	3998.7		50′	9504.4	5368.2	
98°	6591.2	3003.8		108°	7886.2	4018.2		118°	9535.7	5395.1	
10′	6610.6	3018.4	25° C.	10′	7910.4	4037.8	25° C.	10′	9567.2	5422.1	25° C.
20′	6630.1	3033.1	T	20′	7934.6	4057.4	T	20′	9598.9	5449.2	T
30′	6649.6	3047.9	2.18	30′	7959.0	4077.2	2.61	30′	9630.7	5476.5	3.16
40′	6669.2	3062.8	E	40′	7983.5	4097.1	E	40′	9662.6	5504.0	E
50′	6688.8	3077.7		50′	8008.0	4117.0		50′	9694.7	5531.7	
99°	6708.6	3092.7	1.02	109°	8032.7	4137.1	1.36	119°	9727.0	5559.4	1.83
10′	6728.4	3107.7		10′	8057.4	4157.3		10′	9759.4	5587.4	
20′	6748.2	3122.9		20′	8082.3	4177.5		20′	9792.0	5615.5	
30′	6768.1	3138.1		30′	8107.3	4197.9		30′	9824.8	5643.8	
40′	6788.1	3153.3		40′	8132.3	4218.4		40′	9857.7	5672.3	
50′	6808.2	3168.7		50′	8157.5	4239.0		50′	9890.8	5700.9	
100°	6828.3	3184.1	30° C.	110°	8182.8	4259.7	30° C.	120°	9924.0	5729.7	30° C.
10′	6848.5	3199.6	T	10′	8208.2	4280.5	T	10′	9957.5	5758.6	T
20′	6868.8	3215.1	2.62	20′	8233.7	4301.4	3.14	20′	9991.0	5787.7	3.81
30′	6889.2	3230.8	E	30′	8259.3	4322.4	E	30′	10025.0	5817.0	E
40′	6909.6	3246.5	1.22	40′	8285.0	4343.6	1.63	40′	10059.0	5846.5	2.20
50′	6930.1	3262.3		50′	8310.8	4364.8		50′	10093.0	5876.1	

T = R tan ½ I E = R exsec ½ I

25
50
100
120
150
200

NON
4 40.83 E = EC = 0 + 0
2691 NW
4 10
4.25
45
62
65
1 —
35
70
2 —
33
50 to New RW Hub
57.93

15.2

67
66.5 66.5 66
66
29"

8.30

8.30
6.35
1.95

33
17
16

247
150
397

67
24
43