

1099

FIELD BOOK

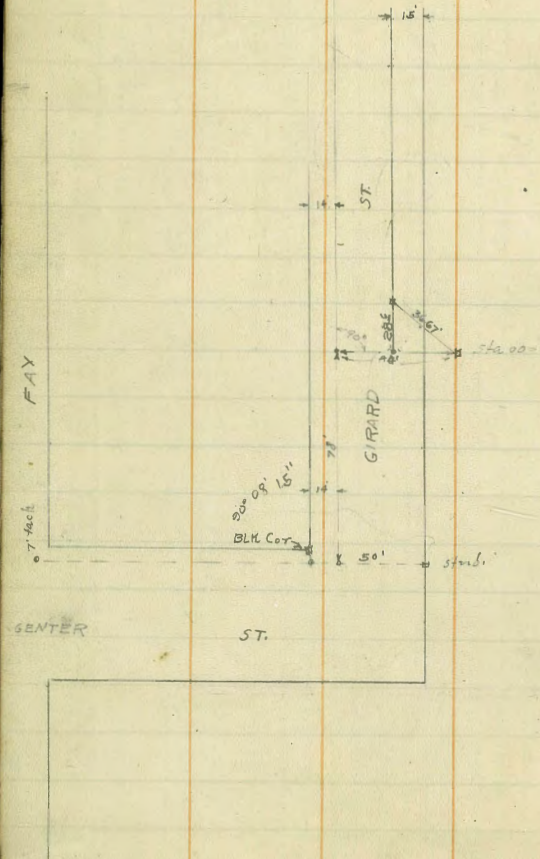
385

MICROFILMED

DEC 21 1964

1099

100
21.12
78.83



$A = 38^{\circ}48'$ RT
 $R = 100'$
 $T = 35.22'$
 $L = 67.72'$

Sta 00

P.C. 0+145

P.T. 0+69.7

P.O.T. 2+01.98

P.C. 2+06.50

$A = 27^{\circ}43'$ LT
 $R = 100'$
 $T = 24.67'$
 $L = 48.37'$

P.T. 3+148.7

6+82.65 P.C.

7+31.20 P.T.

31°
 7+31.20 P.T. Note: This tangent is S.W. of E.L. of Arroyo.

$A = 27^{\circ}44'$ RT
 $T = 24.69'$
 $L = 48.40'$
 $R = 100'$

10+57.05
 11+01.25 = S.L. Pearl St.

16+10.55
 17+20.25 P.C.

46.92
 17+26.25 = C.C.

13.11
 18+32.4 P.T.

$A = 75^{\circ}47'$
 $R = 100'$
 $T = 77.93'$
 $L = 132.26'$
 $E_x = 267.8'$

21 + 82⁵
 22 + 32⁵ P.C.

08⁴⁹
 22 + 58⁴⁹ E.C.

$\Delta = 14^\circ 16' L^+$
 100'

L 2592
 T 1251

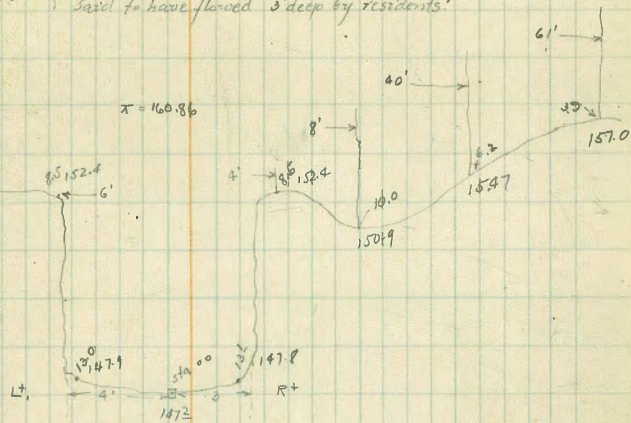
39¹²
 21 + 89¹² POT. = W. T. DRAPER 90° off this line; 36.36' from hub
 at SW. Coy as shown on tie point sheets.

	+	x	-	
10.02	155.24		145.22	NW FAYE CENTER
12.07	164.15	3.16	152.08	5th fence Cor Girard
177	160.86	5.06	159.09	9. Center NW.
00		12.7	147.2	
C.C		12.9	146.0	
0+60		15.2	145.7	
0+62		10.4	150.5	
0+69 ² EC.		10.1	150.8	
1+00		9.3	151.6	
1+13		9.3	151.6	
1+20		9.7	151.2	
1+30		12.8	148.1	
1+50		14.2	146.7	
#	0.29	149.22	11.92	148.23
2+00		5.2	144.0	
+17		5.3	143.9	
+50		4.6	144.6	
+65		4.2	145.0	
2+96 ⁵⁰ RC		6.0	143.2	
C.C		9.8	139.5	
3+44 ¹⁷ PT. #	0.42	138.66	10.98	stub 138.24
+60		1.0	137.7	
+66		2.1	134.6	
+90		2.5	134.2	
+92		6.8 (5?)	131.9	
4		6.5	132.2	



fall of ditch = 2.4 in 80'

said to have flooded 3' deep by residents:



	+	7 138.66	-	
4+04			6.6	132.1
+08			4.4	137.3
+45			6.6	132.1
+46	bottom Channel		8.8	129.9
+50	"	"	9.0	129.7
+63			7.7	131.0
5			9.0	129.7
5+27			10.5	128.2
+50			10.6	128.1
+97			11.6	127.1
6			11.1	127.6
+05			10.8	127.9
+50			13.0	125.7
#	1.10	127.26	12.55	126.11 on 6+50 stake
6+57			3.3	124.0
6+75			4.4	122.9
6+82.60 RC.			2.7	124.6
C.C.			3.3	124.6
7+31.00 E.C.			5.2	122.1
+50			5.4	121.9
8			7.1	120.2
+50			8.2	119.1
9			9.7	117.6
+50			11.2	116.1
10			13.0	114.3 Top stake 10"
#	1.00	118.81	12.45	114.81

10+63			2.5	112.3	
+50			4.2	111.6	
S gutter Pearl			5.4	110.4	
"			5.1	110.7	
"			5.5	110.3	
N gutter Pearl			7.0	108.7	
+37			6.5	109.3	
+50			7.0	108.8	
+60			7.9	107.9	
+75			10.7	105.1	
12			12.4	103.4	
#	0.06	103.93	11.95	103.86	On sta 12
+50			2.5	101.4	
12			3.9	100.0	
+50			5.2	98.7	
14			6.6	97.3	
+50			8.5	95.4	
15 1' L			9.0	94.9	
15 2' R			5.1	98.8	
+50			10.6	93.3	
16			13.1	90.8	
#	2.47	93.84	12.55	91.37	Top 16
+30			3.3	90.5	
+50			3.8	90.0	
16+80 ⁸⁵ PC			4.3	89.5	
17			5.0	88.8	

93.84

17+20			6.2	87.6
17+46 ⁹³ C.C.	bottom	Channel	6.5	87.3
	B.M. P.I. Hub		4.04	89.80 B.M.
18			6.9	86.9
18+10 ¹¹ EC.			7.0	86.8
+50			7.2	86.6
19	on cement	sidewalk.	6.9	86.9
+10	"	curb	7.1	86.7
+10	"	gutter	7.8	86.0
Flow line	Cal. intake:		10.27	83.47
+50			8.1	85.7
+63	gut		8.3	85.5
+65	curb		8.5	86.3
+78	Prop.		7.8	86.0
+85			10.0	83.8
Outfall	flow line	Culvert	13.15	80.69
20			9.0	84.8
+12			9.2	84.6
#	3.91	86.68	11.07	82.77 Onhead wall Cul.
+28			5.7	81.0
+50	Bottom		6.2	80.5
21			7.4	79.3
+15			5.7	81.0
+32			4.4	82.3
+50			4.6	82.1
RC 21+82 ⁵⁷			5.4	81.3

	+	86.68	-	
BM Bl Hub			6.19	80.49 BM.
C.C			6.9	79.8
22			6.7	80.0
+02 bottom old flume			9.7	77.0
22+08+9 EC " " "			10.0	76.7
+20 " " "			10.1	76.6
+22			7.4	79.3
+30			7.1	79.6
23			9.5	77.2
bottom flow line Culvert intake:			12.80	73.88
+30 ± street			10.3	76.4
+50			11.5	75.2
+52 gutter			11.8	74.9
+52 cement curb			10.8	75.9
+65 = Appe prop:			10.7	76.0
# E.14 77.47			11.35	75.00 on headwall
Outfall Culvert			6.0	72.0
+75 bottom channel			5.9	71.6
24			7.3	70.2
+10 bottom channel			8.0	69.5
+18 " "			8.1	69.4
+39			4.2	73.3
+50			4.3	72.2
+94			4.7	72.8
25			6.0	71.5
+25			5.0	72.0

+50		9.0	69.5
+54	Bottom Channel	9.5	68.0
+65	"	9.8	67.7
+80	"	7.8	69.7
+90	"	8.3	69.2
26	"	8.5	69.0
+15	"	9.9	68.6
+25	Bottom Channel	11.5	66.0
+30	"	11.7	65.8
+50	"	11.7	65.8
	Flow line intake Culvert	13.70	63.8
+70	Appx Prop line:	5.9	71.7
+80	= Curb	6.0	71.5
+81	= gut	6.6	70.9
27		6.1	71.4
27+32	= gutter	6.9	70.6
+24	= Curb	6.0	71.5
#	0.92	72.31	6.08
			71.30 = hub 27+32 ¹⁰
+45	= Appx prop line	0.8	71.5
+61		9.5	62.8
+83		10.7	61.6
+88		12.4	59.9
28+15	Bottom Channel;	14.9	57.4
	Flow line outfall culvert:	14.00	58.3

Spk N.E. Cov Fay & Rautner

87.04
+ 3.70
90.74
- 4.48
86.26
+ 1.03
87.29
77.46
+ 2.53
79.99
81.44
71.45 = 71.37

Assumed Ele bottom Culvert outfall = 40.00
 at La Jolla Blvd.

+17.86
57.86
0.00
57.86
+ 3.92
60.74

5	66.74	24'	66.74	24'	66.74
	4.90		5.40		4.90
	61.84		61.34		61.84

Survey for 36" Storm Drain Pipe from
30" Culvert on Pearl St to proposed Open Conduit
at Ravina & Girard

6+32.72 P.T

$\Delta = 20^{\circ}10' Lt$ $R=104$ $T=18.99$ $L=36.67$

5+96.05 P.C

5

4

3

2

+55.05 P.T. Δ

$\Delta = 14^{\circ}59' Lt$ $R=100$ $T=13.15$ $L=26.15$

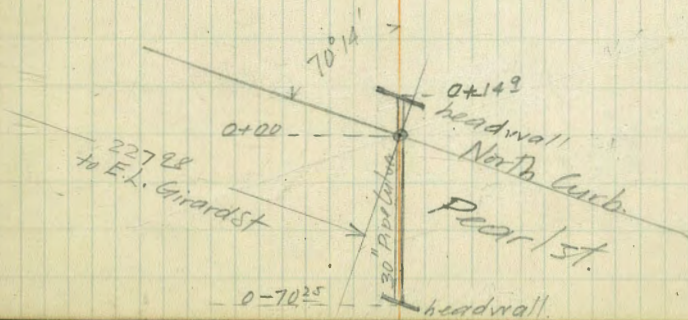
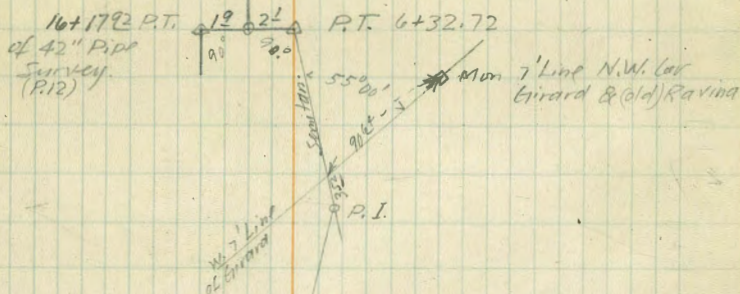
+28.90 P.C Δ

1

0+00

Sept 28-22 Com. by
Deanna
Miller
Sights
Wahlbreck

10



Survey for Storm Drain from Genter
and Girard Sts. to Draper & Ravina Sts.

11

10

9

8

7

6

5

4

3

2

1 + 00

+69.17 RT Δ
+50
+01.45 RC Δ
0 + 00

T = 35.22
Δ = 38° 48' RT R = 100'
L = 67.72

Sept 26, 22

11

Gentry
Dunn
Miller
Sights
Wahlbreck

ST.

10 ± 80 ±

PEARL ST.

> 35' < 65' >

P.L. line

GIRARD

> 35' < 15' >

Genter St
N. Genter
0 + 00
58'
78'

23

22

21

20

19

+77.50 PTA

R18 + 30.78 PCA

R18

$\Delta = 26^{\circ}46'44''$ R=100' T=23.79 L=46.72

"R' 17

16 + 17.92 PTA } offset 1.9 Rk.

+69.93 ctr.

+26.93 PCA

$\Delta = 55^{\circ}00'44''$ R=100'

T=52.06 L=95.99

15

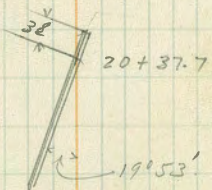
14

13

12

Tack on 7' Line Fay 20+29.93
6315

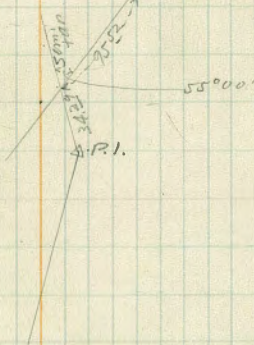
Tack on 7' Line Fay 20+29.93



24" Corrug Iron Pipe
across Fay.

W 7' Line Girard

Hub 100'
ctr of Arc
"Radius"



27+93.60 = Δ 27+39.19 of old line (p.2)

27

26

25

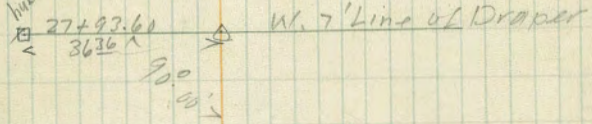
24 + 75.42 P.T. not set.

$\Delta = 8^{\circ}15' R=100 T=7.21 L=14.40$

24 + 61.02 P.O. not set

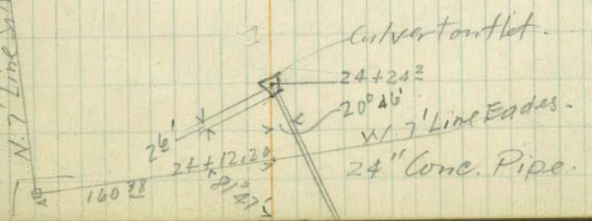
24

Hub of S.W. Cor. Roving & Draper
21 shown on tie of sheets



P.I. set:

N. 7' Line Silver St.



	6.38	144.62		138.24 = old RT
2496 ⁵ = old P.C.			1.5	143.1
3			1.9	42.7
+50			7.6	37.0
4			9.0	35.6
+50			6.9	37.7
+70			7.5	37.1
5			9.2	35.4
+50			12.0 ⁵	32.1
#	0.89	132.14	12.97	131.65
6			2.2	129.9
7			6.1	26.0
8			10.0	22.1
#	0.54	119.77	12.91	119.23
9*			1.6	118.2
10			5.5	114.6
+50			6.8	113.0
11			8.7	111.1
12			12.2	107.6
#	0.16	106.91	12.02	106.75
13			3.2	103.7
14			7.0	99.9
15			10.7	96.2
15+2139 P.C.L [†]			11.6	95.3
15+6993 = middle of curve			13.3	93.6
#	0.29	94.37	12.83	94.08

	+	T	-			
				92.37		
15+85	Appe	(Cement Curb	Gutter full:	0.93	93.44	
16+17	PT.			1.1	93.3	
17				3.1	91.3	
+7				3.6	90.8	
+8		= bottom	channel	6.6	87.8	
+20		"	"	6.1	88.3	
+24				4.0	90.4	
+28				5.3	89.1	
+70				6.1	88.3	
+75				5.0	89.4	
18				5.3	89.1	
18+30	78 = PC			5.3	89.1	
		middle	curve	6.3	88.1	
15+77	80 = P.T.	= bottom	channel	7.4	87.0	
19		"	"	7.7	86.7	
+69	= Cement	Curb:		7.61	86.76	
+69	=	Gutter:		8.6	85.8	
20	=			8.4	86.0	
#	on	culvert	575	88.58	11.54	82.80
+21				3.1	85.5	
+24				2.4	86.2	
Grating	on	culvert	7' H	3.63	84.95	
Curb	for	culvert	7' H	2.60	85.98	
+34				2.6	86.0	
+42	=	Appe	top	5.7	82.9	

	+	π	-	
		88.58		
+82 = Appe - bottom Cut			8.2	80.4
+46 = bottom Channel			8.1	80.5
21			7.8	80.8
+40			5.6	83.0
22			6.6	82.0
+65			7.0	81.6
23			7.7	80.9
+50			11.2	77.4
24			12.8	75.8
#	1.30	77.25	12.63	75.95
+4 = Gutter			1.7	75.5
+6 = Curb,			1.2	76.0
on grating 6' R ⁺			2.3	74.9
on Curb for grating			1.3	75.9
+17			1.3	75.9
+21 ⁷ = top of parapet wall.			1.30	75.9
+21 ² = flow line			5.25	72.00
+27 ² = End apron;			5.25	72.00
+27 ² = bottom Channel;			6.8	70.4
24+68 ²³ A L ^t = bottom channel;			7.8	69.4
+81 = " "			7.7	69.5
+90			3.9	73.3
25 ⁵			3.8	73.4
75 ⁰			5.0	72.2
26			7.1	70.1

16

292⁹⁸ along North curb line of Pearl St 10 + 742 to sta
 00 at end of end pipe;

	+	71	-	
		77.25		
+15 = Bottom Channel			9.7	67.5
+35			7.0	69.7
+50			7.8	69.4
+70			8.6	68.4
+95 = Bottom Channel			11.6	65.6
27			11.3	65.9
+5			10.8	65.4
+21			5.7	71.5
+35 = Dirt curd.			5.9	71.3
+36 = Gutter			6.3	70.9
+50			6.0	71.2
+87 = Cutter } Earth:			6.6	70.6
+88 = Curb }			5.8	71.4
#1			5.80	71.42 = 71.39 on old line.

	9.33	116.08		106.75	
Flow time intake pipe Culvert Pearl st:			5.80	110.58	
+00 = Gutter			2.41	113.67	
+00 = Curb Cement			1.49	114.59	
+16 = Top of retaining wall:			11.25	114.83	
+16 = Flow line outfall pipe Culvert			7.34	108.76	
+25			6.9	109.2	
1			8.7	107.4	
+28 ⁹⁰ = PC			9.2	106.9	
+35 ⁹⁰ = PT			9.5	106.6	
2			10.7	105.4	
#	0.57	105.98	10.67	105.41 on sidewalk	stake sta 2
3			3.3	102.7	
+50			5.5	100.5	
4			6.2	99.8	
+85 = Earth Curb.			8.4	97.6	
+90 = Gutter			9.3	96.7	
5			9.4	96.6	
+100			10.8	95.2	
+96 ⁰⁰ = PC Lt.			12.4	93.6	
Appe 6+02 = Cement curb			12.8	93.2	
6+37 ⁷² = PT = End line			12.7	93.3	
#			11.89 =	94.09 = 94.08	

Conly
Nov. 1922. 19

30th St Bridge

Diagram Showing Stringer Renewals
Stringers represented by single longitudinal lines. Caps and floor-beams shown by transverse double lines.

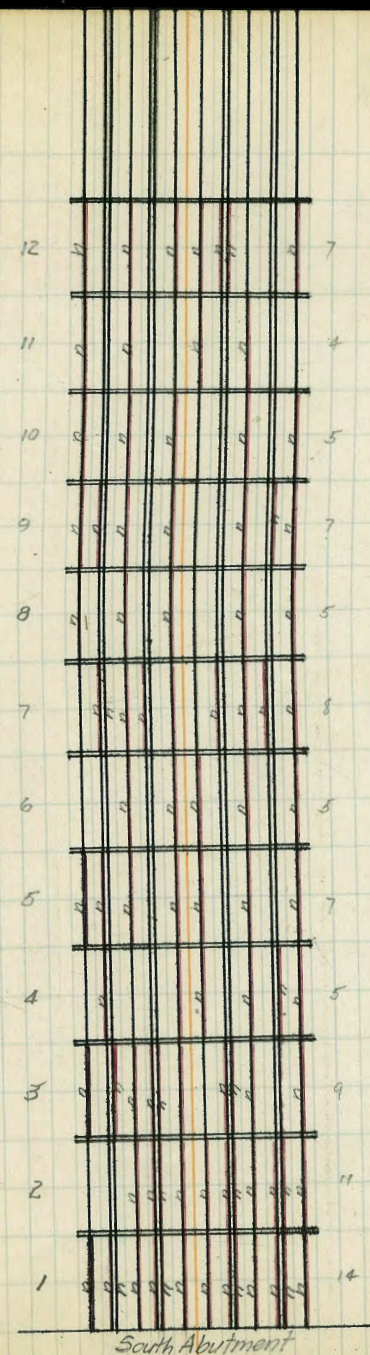
New Stringers indicated by letter "n"

new stringers 219.

100'
TRUSS

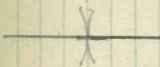
100'
TRUSS

100'
TRUSS



South Abutment

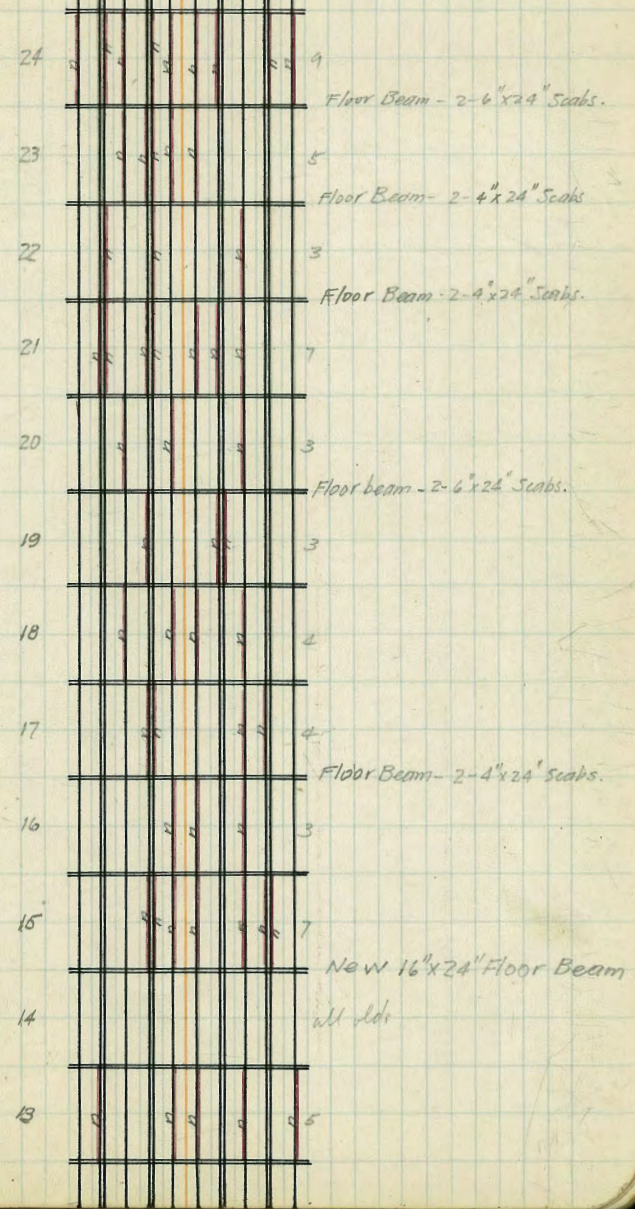
100'
Truss



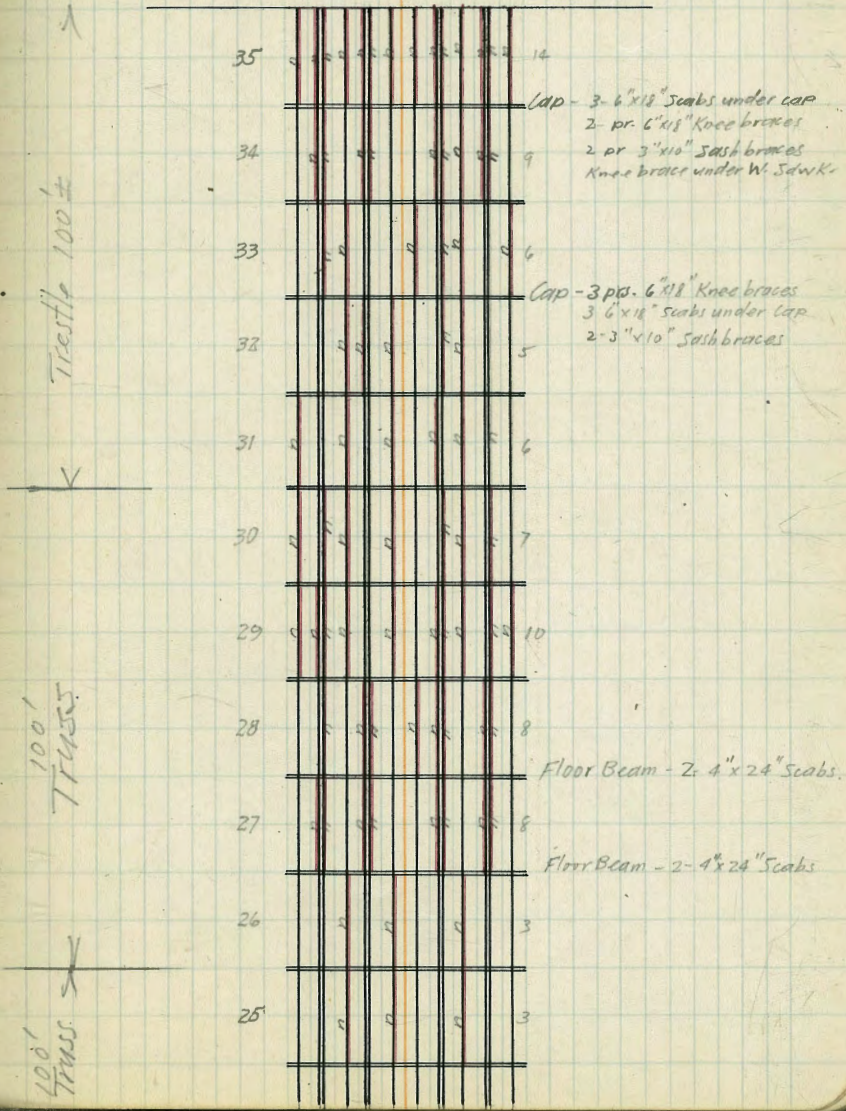
100'
Truss



100'
Truss



North Abutment.



Truss 100'

100'
TRUSS

100'
TRUSS

12/26/22

Carpenter
11/00/22
E/1/23CROSS SECTION OF
HOITT ST 60' wide -
from S.L. I to N.L. K

CO. BM	957	107.60	98.03	B.P. 3W 28+4 + I
		S.L. I	ST	
W	104.25	3.5	104.1	↓
cb	104.0	4.1	103.5	
1/4		3.6	104.0	
C	104.75	3.5	104.1	
1/2		3.5	104.1	
+9.9		4.0	103.6	
cb	105.5	5.0	102.6	
E	105.75	8.0	99.6	↓
+5		3.1	104.5	
		5.5		
-10		5.5	102.1	
-5		5.8	101.8	
E	105.44	7.5	100.1	
+5		8.9	98.7	
cb	105.19	7.1	100.5	
1/4		7.4	100.2	
C	104.44	7.0	100.6	
1/4		4.9	102.7	
cb	103.69	4.5	103.1	
W	103.94	3.9	102.7	↓
		15.5		
W	103.33	5.8	101.8	↓
cb	103.08	6.2	101.4	
1/6		7.9	99.7	

1076

22

C	108.63	11.6	96.6
1/4		13.2	94.2
cb	104.58	12.9	94.7
E	104.67	13.5	94.1
+5		13.8	93.8
+10		11.9	95.7
		20.5	
-20		8.6	99.0
-10 =	flow line of outlet	13.20	94.4
-5		15.8	91.6
E	104.52	16.0	91.6
cb	104.27	13.8	93.8
1/4		14.1	93.5
C	103.52	12.5	98.1
1/4		8.5	94.1
cb	102.77	6.9	100.7
W	103.04	6.6	101.0
+5		6.2	101.4
T.P.	1.92	100.71	88.1
		39.5	100.7
-5		1.9	98.8
W	101.85	2.2	98.5
cb	101.60	2.7	98.0
1/4		5.7	95.0
C	102.35	8.3	92.4
1/4		8.6	92.1

100.71

100.7

cb	103.10	9.2	91.5
E	103.35	9.0	91.7
+3		5.4	95.3
+15		4.1	96.6
	41'5		
-15		4.1	96.6
E	102.73	5.4	95.3
+1.99		5.5	95.2
+W		9.3	91.4
cb	104.98	9.4	91.3
1/4		8.5	92.2
E	102.23 w. cont 101.73	8.3	92.4
	50'5		
-15		3.3	97.4
E	102.68	5.2	95.5
cb	102.43	5.8	92.9
+3		6.2	92.5
1/4		9.9	90.6
C	101.68	8.8	91.9
(on Manhole)		(7.87)	(92.84)
1/4		7.8	92.9
+9.99		5.2	95.5
cb	100.93	4.2	96.5
+5		3.9	96.8
W	101.18	3.8	96.9

H. 1.57

23

100.7

		75'5	
-10		6.4	92.3
W	99.85	6.7	92.0
cb	99.60	8.1	92.6
+8		8.5	92.2
+8.1		9.5	91.2
1/4		10.0	90.7
C	100.4	9.2	91.5
1/4		9.1	91.6
+5		8.7	92.0
cb	101.20	5.3	95.4
E	101.45	4.0	96.7
+15		3.1	97.6
		100'5	
-15		1.9	96.8
E	100.75	2.8	97.9
+5		3.1	97.6
cb	100.5	4.6	96.1
+5		6.6	92.1
1/4		7.2	93.5
+6		9.3	91.4
C	99.75	10.0	90.7
+5		10.5	90.2
1/4		9.3	91.4
+3		8.4	92.3
cb	99.0	8.6	92.1

	100.71		(100.7)
W	99.55	8.5	94.2 ✓
+15		8.0	92.7
	125'5		
-15		9.0	91.7
W	99.52	9.2	91.5 ✓
cb	99.27	10.7	90.0
1/4		11.1	89.6
+5	100.04	10.0	90.7
C	100.02 ✓	8.0	92.7
1/4		6.7	95.0
cb	100.77	3.6	97.1
+5		1.8	98.9
E	101.02 ✓	1.3	99.0 ✓
+15		0.6	100.1
	145'5		
-10		+0.2	100.9
E	101.44	0.0	100.7 ✓
+7		0.5	100.2
cb	101.19	1.8	98.9
1/4		6.1	94.6
C	100.44	7.1	93.6
1/4		7.9	92.8
+5		8.5	92.2 ✓
cb	99.70	10.1	90.6
W	99.95	11.7	89.0 ✓
+20		9.6	91.1

	160'5		(100.7)	HOITT.	24
-20		9.7	91.0		
-10		12.2	88.5 ✓		
W	100.56	9.1	91.6 ✓		
cb	100.31	7.6	92.1		
1/4		6.8	93.9		
C	101.02	6.2	94.5		
1/4		4.1	96.3		
cb	101.74	0.2	100.5		
T.P.	112.22 112.69	0.24	100.47		(112.7)
+5		10.9	101.8		
E	101.99	10.8	101.9 ✓		
+10		10.6	102.3		
	175'5				
-10		8.4	104.3		
E	102.55	9.4	103.3 ✓		
cb	102.30	10.4	102.3		
1/4		14.2	98.5		
C	101.61	15.6	97.1		
1/4		17.9	94.8		
cb	100.92	19.0	93.7		
W	101.17	19.2	93.5 ✓		
+10		17.5	95.2		
+20		24.1	89.5		
	200'5				
-20		20.9	91.8		

112.69

112.7

W	10217	18.7	94.0
cb	101.94	17.4	95.3
1/4		15.9	96.8
c	102.59	13.3	99.4
1/4		11.7	101.0
cb	103.24	7.0	105.7
E	103.49	6.7	106.0
+10		6.0	106.7
		275' S	
-10		2.5	110.2
E	104.48	3.9	108.8
cb	104.18	4.8	107.9
1/4		6.8	105.9
c	103.57	9.6	103.1
1/4		12.6	100.1
cb	102.96	12.4	98.3
W	103.21	16.1	96.2
+25		20.7	92.0
		250' S	
-25		20.2	92.5
-10		17.3	95.4
W	104.22	14.6	98.1
cb	103.97	11.7	101.0
1/4		9.4	103.3
c	104.54	7.3	105.4
1/4		5.2	107.5

HOITT

25

cb	105.12	23	110.4
TP	9.33	121.71	0.31
E	105.37	93	112.38
+10		82	113.5
		275' S	
E	106.31	61	115.6
cb	106.06	61	115.6
1/4		10.0	111.7
c	105.52	13.1	108.3
1/4		15.0	106.7
cb	104.99	16.2	105.5
W	105.24	19.0	102.7
+25		27.8	93.9
		300' S = NL J	57 80 wide 14' cbs 13' 1/4 S
-25		23.2	98.5
W	106.25	17.1	104.6
cb	106.00	15.3	106.4
1/4		12.9	108.8
c	106.50	9.9	111.8
1/4		6.6	115.1
cb	107.00	4.2	117.5
E	107.25	3.7	118.0
		N. Curb	
E		27	119.0
cb		32	118.5
1/4		51	116.3

121.71

121.7

c	80	113.7
1/4	10.8	110.9
cb	13.6	108.3
W	15.9	105.8
+10	166	105.1

N 1/4

-10	176	104.1
W	15.3	106.4
cb	120	109.7
1/4	9.4	114.7
c	7.0	114.7
1/4	5.0	116.7
cb	25	119.2
E	22	119.5

Center J

E	106.75	1.2	120.5
cb		20	119.7
1/4		4.4	117.3
c	106.25	6.5	115.2
1/4		8.3	113.4
cb		10.5	110.9
W	105.75	14.1	107.6
+15		18.4	103.3

S 1/4

-15	17.7	104.0
W	13.6	108.1

121.7

26

121.7

cb	93	112.4
1/4	73	114.4
c	58	115.9
1/4	36	118.1
cb	1.9	119.8
E	0.2	121.5

S Curb

E	0.6	121.1
cb	26	119.1
1/4	36	118.1
c	50	116.7
1/4	69	114.8
cb	96	112.1
W	133	108.4
+15	17.4	104.3

S L J

-15	17.7	104.0	
W	105.25	15.0	108.7
cb	105.00	9.6	112.1
1/4		7.5	114.2
c	105.50	6.0	115.7
1/4		3.3	118.4
cb	106.00	3.9	117.8
E	106.25	1.9	119.8

25'S

E	104.02	5.3	116.4
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	121.71		121.7
cb	103.77	65	115.2
+3		7.8	113.9
1/4		81	113.6
c	103.31	9.2	112.5
1/4		10.5	111.2
cb	102.56	12.2	109.3
W	103.11	14.8	106.9
+15		18.1	103.6
		50.3	
-10		20.0	101.7
W	100.97	18.8	102.9
cb	100.7	17.0	102.7
1/4		15.3	106.4
c	101.63	14.1	107.6
1/4		13.2	108.5
cb	101.54	12.0	109.7
E	101.79	11.2	110.5
TP	0.77	12.48	109.23
		110.00	
		75.5	
-10	on sidewalk to house	4.4	105.6
E	99.56	5.1	102.9
cb	99.31	5.5	104.5
1/4		6.4	103.6
c	98.94	6.5	103.5
1/4		6.7	103.3
	98.58	7.3	102.7

			Holt	27
W	98.83	9.2	100.8	✓
+10		10.8	99.2	
		90.5		
-10		12.2	97.6	
W	97.54	11.5	98.5	
cb	97.29	10.2	99.8	
1/4		9.2	100.8	
c	97.62	9.0	101.0	
1/4		9.4	100.6	
cb	97.97	9.1	100.9	
E	98.22	9.0	101.0	
+10	= on driveway	9.2	100.8	
		100.5		
-10		9.5	100.5	
E	97.33	9.9	100.1	✓
cb	97.08	10.1	99.9	
1/4		10.3	99.7	
c	96.75	10.3	99.7	
1/4		10.2	99.6	
cb	96.43	11.2	98.6	
W	96.68	12.2	97.6	✓
+10		13.0	97.0	
TP	0.30	12.94	97.06	
		12.5		
-10	on lawn	11.3	95.1	✓
W	94.54	11.5	95.9	✓

(97.4)

cb	9429	2.0	95.4
1/4		1.2	96.2
c	9457	07	96.7
1/4		0.5	96.9
cb	9485	0.5	96.9
E	9510	0.6	96.8
+10		0.5	96.9
		150' S	
-10		31	94.3
E	9316	31	94.3
cb	9291	33	94.1
1/4		34	94.0
c	9270	35	93.9
1/4		38	93.6
cb	9250	41	93.3
W	9275	44	93.0
+10	on/ann.	43	93.1
		175' S	
-10		59	91.5
W	9150	61	91.3
cb	9125	58	91.6
1/4		59	91.5
c	9134	57	91.7
1/4		57	91.7
cb	9143	58	91.6
E	9168	58	91.6

(97.4) 28

		300	5
E	9020	77	89.7
cb	8995	76	89.8
1/4		74	90.0
c	8997	70	90.4
1/4		70	90.4
cb	9000	72	90.4
W	9025	73	90.1
		garage floor 3' West of SWL	
		225' S	
W	8900	80	89.4
cb	8875	81	89.3
1/4		83	89.1
c	8866	82	89.2
1/4		85	88.9
cb	8847	88	88.6
E	8874	89	88.5
		250' S	
E	8724	95	87.9
cb	8699	96	87.8
1/4		94	88.0
c	8724	92	88.2
1/4		91	88.3
cb	8750	92	88.2
W	8735	93	88.1
		495' S	
W	8650	101	87.3

97.36

97.4

29

cb	8625	11.0	86.0
1/4		10.6	86.8
c	8586	10.5	86.9
1/4		10.5	86.9
cb	8551	10.5	86.9
E	8576	10.2	87.2
295.5			
E	8457	10.4	87.0
cb	8432	10.3	85.1
1/4		12.8	84.6
c	8478	12.1	85.3
1/4		12.2	85.2
cb	8525	12.2	85.2
W	8550	10.7	86.7
300.8 = N.L. K 35			
W	8525	11.7	85.7
cb	8500	12.5	84.9
1/4		12.3	85.1
c	8450	12.3	85.1
1/4		12.6	84.8
cb	8400	12.5	84.9
E	8425	12.4	85.0
chk cb. NW K + Heitt		12.7	84.89

12/16/22
Gregory
Moore
Ellis

Levels 1' S of N. Curb of
Douglas St. from E. CB Line of
Eagle St to

30

	0.00	263.06		263.06	BR NE Walt - Eagle Flow line of present pipe
0+00 - Ecb Line of Eagle			6.3	56.8	
0+00			5.1	58.0	= top of pipe
0+52			5.3	57.8	
0+59			7.8	55.3	
T.P.	0.83	251.51	12.36	250.68	
0+70			2.3	49.3	
+73	Hollow under this		5.0	46.5	
+73.2	Hole here is 45 high		12.3	39.2	
+85			15.9	35.6	
1+00			21.3	30.2	
+10			22.0	29.5	

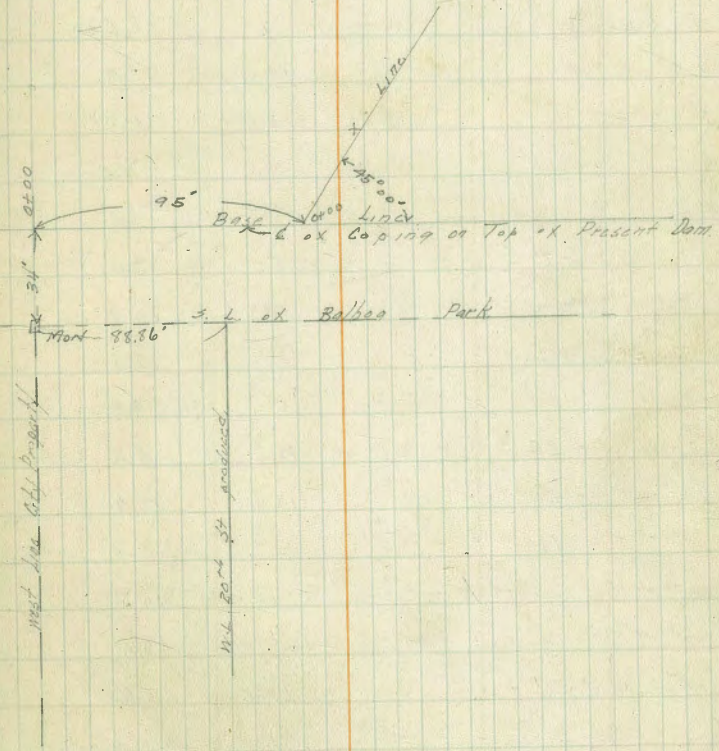
1/3/23

Gregory Moore Miller Show.

CROSS SECTION OF SWITZER CANYON DAM

	9.09	82.29	73.20	Map on 11.34 NW cor of bridge
T.P.	8.99	86.75	453	77.76
T.P.	14.75	98.42	1.18	85.57 B.M.
	100' W. of 0+00			
Base Line		8.3		90.1
30' S. of B.L.			11.0	87.4
30' N. " "			4.9	93.5
60' " "			4.1	96.3
73' " "			4.4	96.0
	50' W. of 0+00			
30' S. of B.L.			10.4	88.0
Base Line			8.0	90.4
30' N. of " "			5.5	92.9
50' " "			4.3	94.1
65' " "			2.4	96.0
78' " "			1.8	96.6
	0+00 = W.L. of City Property			
83.5' N. of Base = Edge pavement.				
10' N. of Base L			1.9	96.5
70' " "			2.4	96.0
50' " "			4.1	94.3
25' " "			5.9	92.5
Base Line			7.9	90.5
40' S. of " "			10.2	88.2
25' " "			10.8	87.6
50' " "			13.4	85.0
" " " "			14.1	84.3

75' S. of B.L.	16.2	82.2
" " " " + 8' E of 0+00	16.4	82.0 = Edge of Cut
" " " " "	18.3	80.1
" " " " + 9' E of 0+00	18.7	79.7 = Edge of Cut
120' " " " "	21.1	77.3 = " " "



98.42

25' E. of 0+00

25' N. of B.L.	2.0	96.4
75' - - - -	2.5	95.9
50' - - - -	4.6	93.8
75' - - - -	6.6	91.8
Base Line	9.0	89.4
25' S. of - - -	15.2	83.2
45' - - - -	13.9	84.5
T.P. 0.57 2614	14.85	85.57
50' S. of B.L.	27.	77.4
✓ ✓ ✓ ✓ + 27' E. of 0+00	13.7	72.4
✓ ✓ ✓ ✓ + 32' - - - -	17.7	68.7
34' ✓ ✓ ✓ ✓ + 50' - - - -	18.0	68.1
50' ✓ ✓ ✓ ✓ + 50' - - - -	18.9	67.2
52' ✓ ✓ ✓ ✓ + 25' - - - -	12.7	73.4
75' ✓ ✓ ✓ ✓ + 25' - - - -	17.2	68.9
75' ✓ ✓ ✓ ✓ + 16' - - - -	16.8	69.3
95' - - - - + 25' - - - -	19.8	66.3
95' - - - - + 14' - - - -	18.0	68.1
95' - - - - + 50' - - - -	20.5	65.6
120' ✓ ✓ ✓ ✓ + 50' - - - -	21.0	65.1
140' ✓ ✓ ✓ ✓ + 29' - - - -	18.4	67.7
50' 75' E. of 0+00		
28' S. of B.L.	3.8	82.3
15' - - - -	5.8	80.3
Base Line	6.2	79.9

9.2
9.0

9.6

13.8

4.3 11.5

79.32

15' N. of Base Line

25' - - - -	4.6	21.5
25' - - - -	1.8	84.3
25' - - - -	4.8	81.3
50' - - - -	+ 6.0	92.1
75' - - - -	+ 7.9	94.0
101' - - - -	+ 9.7	95.8
121' - - - -	+ 9.2	95.3
92' - - - -	+ 9.0	95.1
75' - - - -	+ 7.4	93.5
81.3' - - - -	+ 0.1	86.2
75' - - - -	+ 4.5	90.6
50' - - - -	2.9	83.2
25' - - - -	6.9	79.2
Base Line	7.8	78.3
13' S. of - - -	5.2	80.9
21' - - - -	18.3	67.8
50' - - - -	20.2	65.9
50' - - - -	20.2	65.9
21' - - - -	19.0	67.1
8' - - - -	6.7	79.4
Base Line	7.3	78.8
25' N. of - - -	7.6	78.5
50' - - - -	3.1	83.0
75' - - - -	+ 4.0	90.1
75' - - - -	+ 1.0	87.1
75' - - - -	+ 4.9	96.0

App. Edge Pav.

Edge Pav.

on fill

Flow Line

= Outlet at 2+00

20

98' N. of B.L. 104.5' E. of 0+00	+8.4	94.5	Edge of Road.
117.5' - - - 104.5' - - -	+9.0	95.1	Edge of Pav.
0+35 on X Base Line			
X Line	8.3	77.8	
25' West of - -	5.1	81.0	
0+39.7 on X Base			
25' West of X Line	3.8	82.3	
4' - - - = End of Dam coping	10.12	76.02	Top of Concrete
X Line = Edge	10.12	76.02	- - -
X - - -	12.0	74.1	Facing
0+47 on X Base			
X Line	14.5	71.6	
15' West - -	13.0	73.1	
25' - - -	6.2	79.9	
0+59 on X Base			
35' West of X Base	4.3	81.8	
27' - - -	6.9	79.2	
24' - - -	11.5	74.6	
15' - - -	12.9	73.2	
X Line	14.6	71.5	
10' E. of - -	17.0	69.1	
T.P. 157	78.16	105.5	73.59
0+70 on X Base			
15' E. of X Line	5.7	69.5	
X Line	7.3	70.9	
West - -	3.0	75.2	

27' W. of X Line	+1.5	79.7	
(- - - and 65' N. of 0+00)	2.5	75.6	
35' - - -	0.8	77.4	
(35' - - - and 65' N. of 0+00)	+3.0	81.2	
38' - - -	+3.3	81.5	
45' - - -	+3.9	82.1	
46' - - -	+7.9	86.1	
51' - - -	+9.3	87.5	
0+75 on X Line			
50' W. of X Line	+10.4	88.6	
43' - - -	+6.6	84.8	
27' - - -	+2.7	80.9	
5' - - -	7.2	71.0	
X Line	7.7	70.5	
13' E. of - -	8.3	69.9	✓
1+00 on X Line			
50' E. of X Line	13.3	64.9	
43' - - -	15.3	62.9	
42' - - -	18.0	60.2	creak bottom
37' - - -	18.1	60.1	" "
25' - - -	11.9	66.2	
X Line	10.5	67.7	
3' West - -	10.0	68.2	
10' - - -	6.4	71.8	
27' - - -	+2.6	80.8	
35' - - -	+6.7	84.9	

50' W. of X Line	+12.8	91.0	
56' " " "	+16.3	94.5	Edge of Road
74' " " "	+17.1	95.3	" - Pav.
1+25 on X Line			
70' W. of X Line	+16.9	95.1	Edge of Pav.
51' " " "	+15.7	93.9	" Road
40' " " "	+9.9	88.1	
32' " " "	+5.3	83.5	
25' " " "	+0.4	78.6	
20' " " "	3.8	74.4	
12' " " "	6.7	71.5	
5' " " "	11.2	67.0	
X Line	11.4	66.8	
27' E. of " "	11.9	66.3	
35' " " "	15.0	63.2	crack bottom
45' " " "	15.1	63.1	" "
47' " " "	13.7	64.5	
55' " " "	12.2	66.0	
60' " " "	11.3	64.9	
1+50 on X Line			
75' E. of X Line	12.1	66.1	
60' " " "	10.6	67.6	
47' " " "	15.4	62.8	crack bottom
38' " " "	15.1	63.1	" "
27' " " "	12.1	66.1	
10' " " "	12.2	66.0	

X Line	11.1	67.1	
7' W. of " "	9.7	68.4	
10' " " "	7.6	70.6	
25' " " "	0.0	78.2	
31' " " "	+3.6	81.8	
38' " " "	+8.3	86.5	
46' " " "	+15.3	93.5	Edge of Road
63' " " "	+15.6	93.8	
68.5' " " "	+16.5	94.7	Edge of Pav.
1+75 on X Line			
67' W. of X Line	+16.3	94.5	Edge of Pav.
62' " " "	+15.2	93.4	
42' " " "	+14.9	93.1	
32' " " "	+7.3	85.5	
27' " " "	+1.6	79.8	
21' " " "	0.0	78.2	
13' " " "	4.9	73.3	
X Line	11.0	67.2	
2' E. of " "	11.8	66.4	
25' " " "	11.6	66.6	
39' " " "	14.8	63.4	crack bottom
50' " " "	14.3	63.9	" "
58' " " "	11.8	66.4	
75' " " "	12.0	66.2	
2+00 on X Line			
75' E. of X Line	11.9	66.3	

52' E. of X Line	11.8	66.4	
45' " " "	14.1	64.1	erect bottom
39' " " "	14.8	63.3	
32' " " "	13.6	64.6	
24' " " "	10.5	67.7	
6' " " "	11.6	66.2	
X Line	10.4	67.8	
6' N. of " "	6.2	72.0	
9' " " "	5.1	73.1	
12' " " "	1.2	77.0	
25' " " "	+8.4	86.6	
31' " " "	+10.4	88.6	
36' " " "	+14.6	92.8	Edge of Road
65' " " " Edge Pavp	80'		
	+115' E of 0+00		Coping Line
20' N. of Base	0.3	77.9	
5' " " "	0.0	78.2	
Base Line	2.8	75.4	
3' S. of " "	4.7	73.5	
20' " " "	10.3	67.9	
30' " " "	11.2	67.0	
	115'		
	+140' E of 0+00		
23' S. of Base	10.5	67.7	
20' " " "	8.4	69.8	
7' " " "	2.0	76.2	
Base Line	1.2	77.0	
6' N. of " "	1.0	77.2	

13'± N. of Base	2.3	76.9	Top Coping
13'± " " "	4.3	73.9	bottom ✓
36' " " "	10.3	67.9	
	128.9		
	+53.9 E. of 0+00 = Angle in coping		
32.5' N. of Base	13.4	64.8	at Top of road
Base Line	4.3	73.9	bottom Coping
" " "	2.45	75.71	Top ✓
	143.6		
	+68.6 E of 0+00		
28' N. of Base	15.8	62.3	
17.7' " " " = Top of Handwall	11.65	66.51	= Center of Handwall
(17.7' " " " = Flow Line 5' C.P.)	(17.9)	60.3	
Base Line	4.3	73.9	Bottom Coping
" " "	2.4	75.8	✓ ✓
14' S. of Base	3.1	75.1	
24' " " "	10.3	67.9	
	175		
	+100' E of 0+00		
73' S. of Base	11.0	67.2	
12' " " "	4.9	75.3	
Base	2.2	76.0	Top coping
" " "	4.2	74.0	bottom ✓
15' N. of " "	14.2	64.0	
24' " " "	12.0	66.2	
	225		
	+50' E of 0+00		
35' N. of " "	12.4	65.8	
11.6' " " "	11.8	66.4	Top of road
Base	4.3	73.9	

Base Line		2.3	75.9	
13.5 - ✓		3.1	75.1	
20 - ✓ ✓		9.6	68.6	
T.P.	734	7829	2.21	75.95
		^{275'} 300' E of 0+00		
21.5. of Base		8.6	69.7	
12 - ✓ ✓		2.5	75.8	
7 - ✓ ✓ ✓		1.1	77.2	
Base		2.3	76.0	Top Coping
		4.3	74.0	bottom ✓
10' N. of ✓		10.9	67.4	Toe of Apron
15 - ✓ ✓ ✓		11.4	66.9	
30 - ✓ ✓ ✓		10.1	68.2	
80 - ✓ ✓ ✓		11.9	66.4	
		^{325'} 350' E of 0+00		
30' N. of Base.		10.4	67.9	
40 - ✓ ✓ ✓		10.8	67.5	
45 - ✓ ✓ ✓		9.9	68.4	
9.8 - ✓ ✓ = Toe of Apron		10.5	67.8	
13.5 - ✓ ✓		3.1	75.2	
24 - ✓ ✓ ✓		7.8	70.5	
		^{375'} 400' E of 0+00		
28.5. of Base		9.2	69.1	
15 - ✓ ✓ ✓		3.2	74.8	
Base		2.3	76.0	Top
		4.3	74.0	Bottom

9' N. of Base = Toe Apron		9.9	68.4	
30 - - -		9.7	68.6	
20 - - -		9.7	68.6	
		^{425'} 450' E of 0+00		
80' N. of Base		9.4	69.9	
7' N. of Base = Toe Apron		9.0	69.3	
Base				
20.5. of ✓		4.4	73.9	
35 - - -		9.0	69.3	
		^{475'} 500' E of 0+00		
34.5. of Base		8.4	69.9	
27.5. of Base		4.8	73.5	
Base		2.3	76.0	
4.3 N. of ✓ = Toe of Apron		7.1	71.2	
70 - ✓ ✓ ✓		8.4	69.9	
		^{525'} 550' E of 0+00		
70' N. of Base		8.4	69.9	
3.5 - - - = Toe Apron		6.4	71.9	
27.5 - ✓ ✓		4.4	73.9	
34 - ✓ - -		6.4	71.9	
T.P.	795	8339	2.35	75.94
		^{550'} 575' E of 0+00		
26.5. of Base		9.8	74.1	
Base		9.0	74.9	= ground
		8.0	75.9	Top Coping
3' N. of ✓ = Toe Apron		11.9	72.0	

70' N. of Base	10.0	73.9	
30' ✓ ✓ ✓	11.4	72.5	
60' - - -	13.0	70.9	
	558' E. of 0+00		
60' N. of Base	12.4	71.5	
45' - - -	11.3	72.6	
35' ✓ ✓ ✓	11.3	72.6	
13' ✓ - -	8.4	75.5	
10' - - -	11.7	72.2	
3' - ✓ ✓ = Top. Mean	11.7	72.2	
	565.4' E. of 0+00 = End of Coping		
75' S. of Base	9.0	74.9	
Base	9.0	74.9	on ground
	5.0	75.9	Top Coping
3' N. of Base	11.4	72.5	
33' ✓ ✓ ✓	11.0	72.9	
38' ✓ ✓ ✓	8.9	75.0	
45' ✓ - -	10.8	73.1	
60' - - -	11.8	72.1	
	575' E. of 0+00		
60' N. of Base	9.8	74.1	
38' ✓ ✓ ✓	9.2	74.7	
28' - - -	8.0	75.9	
70' - - -	11.2	72.7	
5' - - -	11.2	72.7	
Base	9.0	74.9	

20' S. of Base	8.5	75.4	
	600' E. of 0+00		
20' S. of Base	5.5	78.4	
Base	7.1	76.8	
3' N. of ✓	6.9	77.0	
6' - ✓ ✓	9.4	74.5	
12' - - -	6.5	77.4	
55' - - -	4.1	79.8	
	625' E. of 0+00		
55' N. of Base	3.5	80.4	
25' - - -	4.7	79.2	
Base	3.6	80.3	
15' S. of ✓	1.5	82.4	
TP. 13.02	96.16 ✓	0.75	73.1 ✓
	660' E. of 0+00		
Base	7.4	88.8	
70' N. of Base	10.3	85.9	
35' ✓ - -	11.9	84.3	
68' ✓ ✓ ✓	12.1	84.1	
80' - - -	15.4	80.8	
100' ✓ ✓ ✓	14.7	81.5	

N. 9579

0+67 on Base Line

32' S of Base		12.3	83.5
19' " " "		14.6	81.2
9' " " "		15.0	80.8
Base		13.7	82.1
15' N of X		10.5	85.3
35' " " "		4.4	91.4
50' " " "		3.1	92.7
85' " " "		0.4	95.4
T.P.	277	98.17	0.39 95.40
88' N		2.0	93.8
98' " = edge parking		2.1	93.7
			15.57 B.M.
T.P.	0.86	86.43	8.70 77.73
	1.63	79.36	

X 2+25

20' E of X		11.6	67.8
5' E		11.9	67.5
0		10.7	68.7
10' W		3.5	75.9
20' W		+4.7	84.1
25' W		+6.4	85.8
36' W		+13.6	93.0 Top

X 2+50

36' W of Base X	+13.0	92.4 Top
25' " " "	+5.4	84.8
18' " " "	+1.8	81.2
12' " " "	+1.5	74.9
3'	10.7	68.7
X Base	10.9	68.5
17' E	11.8	67.6
	75.9	Top Curve
T.P.	12.05	87.95 4.23
	0.23	87.72 T.P.
	9.57	97.29

7+05 (old station)

15' S	+3.9	101.2
Base	+0.4	97.7
20' N	-4.4	92.9
40' N	8.6	88.7
40' N 6+96 E old	12.0	85.3
53' N	11.4	85.9
85' N	12.2	85.1

	0.50	7640	75.9	Elv. top of Copper
		2+25		
E of Baseline +20			8.7	67.2
" " +29			13.5	62.4
+43			11.8	64.6
+50			8.7	67.7
+75			8.3	68.1
		2+50		
" " +75			7.8	68.6
+50			8.7	67.7
+43			12.8	63.6
+35			12.6	63.8
+32			10.9	65.5
+17			8.7	67.7

4/2/23 Gregg. Cross SECTION OF 60' ST
 32nd ST 10' cbs
 from N.L. Market to S.L.F.

6.50 88.76 82.26 Max 32nd St

N.L. Market

W	73	81.5
cb	76	81.2
1/4	82	80.6
c	82	80.6
1/4	80	80.8
cb	80	80.8
E	74	81.4
E	6.0	82.8
+3	6.0	82.8
+5	7.5	81.3
cb	8.0	80.8
1/4	8.0	80.8
c	8.0	80.8
1/4	8.1	80.7
+6	7.3	81.5
+7	6.1	82.7
cb	6.1	82.7
W	54	83.4

Plotted on off Cr Sheet 5-25-23 Tolman

30' N

W	52	83.6
cb	57	83.1
+3	6.0	82.8

+6	7.1	81.7
1/4	7.3	81.5
c	7.2	81.6
1/4	7.2	81.6
cb	7.0	81.8
E	59	82.9
E	6.0	82.8
cb	6.0	82.8
1/4	6.3	82.5
c	6.2	82.6
1/4	6.4	82.4
+4	6.4	82.4
+7	5.1	83.7
cb	5.2	83.6
W	49	83.9
W	46	84.2
cb	47	84.1
+4	48	84.0
+7	6.1	82.7
1/4	6.2	82.6
c	6.3	82.5
1/4	6.4	82.4
+4	6.4	82.4
+6	5.2	83.6

65' N

100' N

88.76

32nd

41

cb		5.2	83.6
E		5.1	83.4
	160' N		
E		5.5	83.3
cb		5.0	83.8
+2		5.1	83.7
+6		6.2	82.6
1/4		6.2	82.4
C		6.2	82.4
1/4		6.2	82.6
+3		5.8	83.0
+5		4.9	83.9
cb		4.5	84.3
W		4.2	84.6
	200' N		
W		3.9	84.9
+3		4.4	84.4
cb		4.7	84.1
+7		5.8	83.0
+9		6.5	82.3
1/4		6.5	82.3
C		6.9	81.9
1/4		7.1	81.7
cb		7.2	81.6
+5		7.7	81.1
E		8.6	80.2
+10		9.1	79.7

223' N

-10		9.7	79.1
E		9.2	79.6
cb		7.7	81.1
1/4		7.6	81.2
C		7.4	81.4
1/4		7.0	81.8
+3		5.5	83.3
cb		5.2	83.4
W		4.2	84.6

270' N

W		6.9	81.9
cb		7.1	81.7
+1		7.7	81.1
1/4		8.2	80.6
C		8.5	80.3
1/4		8.6	80.2
+8		8.6	80.2
cb		9.3	79.5
E		9.7	79.1
+10		10.2	78.6

300' N = 5L G 54 80' st 10' cks

-10		10.2	78.6
E		9.8	79.0
cb		9.2	79.6
+1		8.7	80.1

1/4		8.9	79.9
c		8.8	80.0
1/4		8.7	80.1
cb		8.6	80.2
W		8.7	80.1
	S. Curb		
W		8.7	80.1
cb		8.8	80.0
1/4		8.6	80.2
c		8.7	80.1
1/4		8.9	79.9
+8		8.6	80.2
cb		9.5	79.3
E		9.9	78.9
+10		10.1	78.7
	5 1/4		
-10		10.3	78.5
E		10.0	78.8
cb		9.3	79.5
+1		8.5	80.3
1/4		8.9	79.9
c		8.7	80.1
1/4		8.5	80.3
cb		8.8	80.0
W		8.5	80.3

Center G 5T			
W		8.5	80.3
cb		8.7	80.1
1/4		8.5	80.3
c		8.7	80.1
1/4		8.8	80.0
+9		8.6	80.2
cb		9.7	79.1
E		10.0	78.8
+10		10.1	78.7
	N 1/4		
-10		10.0	78.8
E		9.7	79.1
cb		9.0	79.8
1/4		8.7	80.1
c		8.5	80.3
1/4		8.3	80.5
cb		8.5	80.3
W		8.3	80.5
	N. Curb		
W		8.2	80.6
cb		8.5	80.3
1/4		8.4	80.4
c		8.2	80.4
1/4		8.6	80.2
cb		8.6	80.3
E		8.5	80.3

88.76

NL G ST

E	7.9	80.9
cb	8.2	80.6
1/4	8.5	80.3
C	8.3	80.5
1/2	8.2	80.6
cb	8.2	80.6
W	8.1	80.7
35°N		
W	7.3	81.5
cb	7.6	81.2
1/4	7.7	81.1
C	7.7	81.1
1/2	7.9	80.9
cb	7.5	81.3
E	7.5	81.3
80°N		
-5	7.6	81.2
E	7.5	81.3
cb	7.1	81.7
+5	7.4	81.4
1/4	7.3	81.5
ctr	6.9	81.9
1/4	6.8	82.0
cb	6.6	82.3
W	5.3	83.5

32nd

W. 25 43

+2 45
46

110°N

W	5.3	83.5
cb	6.1	82.7
1/2	6.4	82.4
C	6.4	82.4
1/2	6.8	82.0
cb	6.4	82.4
+2	7.1	81.7
E	7.6	81.2
+10	7.7	81.1
140°N		
-10	9.3	79.5
E	8.8	80.0
+6	8.3	80.5
cb	5.9	82.9
1/2	6.1	82.7
C	6.0	82.8
1/2	5.8	83.0
cb	5.2	83.6
W	4.8	84.0
160°N		
W	4.4	84.4
cb	4.8	84.0
1/2	5.0	83.8
C	5.5	83.3
1/2	5.5	83.3

8876

cb		5.3	83.5
+5		7.3	81.5
E		7.7	81.1
+10		8.1	80.7
	163'N		
W		3.5	85.3
+N		4.5	84.3
cb		4.6	84.2
	200'N		
-10		5.5	83.3
E		4.6	84.2
cb		3.7	85.1
1/4		3.7	85.1
C		3.8	85.0
+3		3.8	85.0
1/4		4.4	86.4
+5		1.8	87.0
cb		1.9	86.9
W		2.4	86.4
T.P.	9.20 9609	1.89	86.89
	235'N		
W		7.0	89.1
cb		7.3	88.8
1/4		8.2	87.9
+8		9.0	87.1
C		9.7	86.4

82nd

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1/4		9.8	86.3
cb		9.8	86.3
E		9.7	86.4
+2		10.1	86.0
+10		10.7	85.4
	270'N		
-10		8.3	87.8
E		7.3	88.8
cb		8.1	88.0
1/4		7.8	88.3
46		7.7	88.4
C		7.2	88.9
1/4		6.0	90.1
cb		4.8	91.3
W		4.0	92.1
	295'N		
W		2.1	94.0
cb		2.6	93.5
+2		3.0	93.1
+5		4.5	91.6
1/4		5.1	91.0
C		5.6	90.5
1/4		6.1	90.0
cb		6.6	89.5
+5		5.7	90.4
E		5.7	90.4

96.09

300' N. = S.L. F St.

E	57	90.4
+5	57	90.4
cb	65	89.6
1/4	59	90.2
c	54	90.7
1/2	51	91.0
cb	42	91.7
W	39	92.2
cut on dirt curb SE F + 32nd	6.0	90.1

1.89

94.20 = 94/16
Non SW
32nd St

358
9151

32nd St

45

5/18/23

Gregory
Moore
Miller
CWCROSS SECTION OF
RESERVOIR SITE
South of El Cajon
West Idaho

	6.45	379.46	373.01
		395' S. of El Cajon = Toe of Slope Large Reservoir	
W.L. Idaho		5.5	374.0
20' W		5.3	374.2
40' ✓		5.6	374.0
60' ✓		5.2	374.3
80' ✓		5.1	374.4
100' ✓		5.1	374.4
120'		4.8	374.7
132' ✓		4.7	374.8
		375' S. of El Cajon	
132' W. of W.L. Idaho.		4.5	375.0
120' ✓ - - -		4.5	375.0
100' - - - -		4.7	374.8
80' - - - -		4.6	374.7
60' - - - -		4.9	374.6
40' - - - -		5.0	374.5
20' - - - -		5.3	374.2
W.L. Idaho		5.9	373.6
		355' S. of El Cajon.	
W.L. Idaho		5.9	373.6
20' W		5.1	374.4
40' ✓		4.9	374.6
60' ✓		4.8	374.7
80' ✓		4.7	374.8
100' ✓		4.7	374.8

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	120' W	4.5	375.0
	132' ✓	4.5	375.0
		335' S. of El Cajon = angle pt. of slope on old res.	
	132' W. of W.L. Idaho	4.7	374.8
	120' - - - -	4.7	374.8
	100' - - - -	4.8	374.7
	80' - - - -	5.0	374.5
	60' - - - -	4.9	374.6
	40' ✓	4.9	374.6
	20' - - - -	5.4	374.1
	5' ✓	5.7	373.8
	W.L. Idaho	6.1	373.4
	4' N. of W.L. Idaho & 323' S. of El Cajon = Palm Tree.		
		315' S. of ✓ ✓	
	W.L. Idaho	6.0	373.5
	5' N.	5.7	373.8
	20' ✓	5.3	374.2
	40' ✓	5.1	374.4
	60' ✓	5.0	374.5
	80' ✓	4.9	374.6
	100' ✓	4.9	374.6
	120' ✓	4.6	374.9
	132' ✓ = Tree slope.	4.3	375.2
	4' N. of W.L. Idaho & 302' S. of El Cajon = Palm Tree.		

379.46

295' S. of El Cajon.

132' W. of W.L. Idaho	4.2	375.3
120' - - - - -	4.7	374.8
100' - - - - -	4.9	374.6
80' - - - - -	4.9	374.6
(80' - - - - - pit = 10' square in bottom of pit)	12.3)	367.2 - hard pan.
60' - - - - -	5.1	374.4
40' - - - - -	5.0	374.5
20' - - - - -	5.3	374.2
5' - - - - -	5.2	374.1
W.L. Idaho	5.8	373.7

4' W. of W.L. Idaho and 279' S. of El Cajon = Palm Tree
275' - - - - -

W.L. Idaho	5.6	373.9
5' W	5.3	374.2
20' -	5.3	374.2
40' -	5.0	374.5
60' -	4.8	374.7
80' -	4.8	374.7
100' -	4.8	374.7
120' -	4.7	374.8
132' -	4.4	375.1

4' W. of W.L. Idaho and 257' S. of El Cajon = Palm Tree
255' S. of El Cajon

132' W. of W.L. Idaho	4.8	374.7
120' -	4.8	374.7

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100' W	4.9	374.6
80' -	4.7	374.8
60' -	4.9	374.6
40' -	5.0	374.5
20' -	5.1	374.4
5' -	5.1	374.4
W.L. Idaho	5.1	374.1

235' S. of El Cajon.

W.L. Idaho	5.2	374.3
20' W	5.1	374.4
40' -	5.1	374.4
60' -	4.8	374.7
80' -	4.9	374.6
100' -	5.0	374.5
120' -	4.8	374.7
132' -	4.6	375.0

4' W. of W.L. Idaho & 234' S. of El Cajon = Palm Tree.

215' S. of El Cajon.

135' W. of W.L. Idaho	4.5	375.0
120' - - - - -	4.7	374.8
100' -	4.7	374.8
80' -	4.7	374.8
60' -	4.6	374.9
40' -	4.8	374.7
20' -	5.0	374.5
W.L. Idaho	5.0	374.5

379.46

48

4' W. of W.L. Idaho ^{and 212} S. of El Cajon - Palm Tree

195' - - -

W.L. Idaho	4.9	374.6
30 W	4.8	374.7
40 -	4.8	374.7
60 -	4.7	374.8
80 -	4.5	375.0
100 -	4.6	374.9
120 -	4.8	374.7
134' -	4.5	375.0

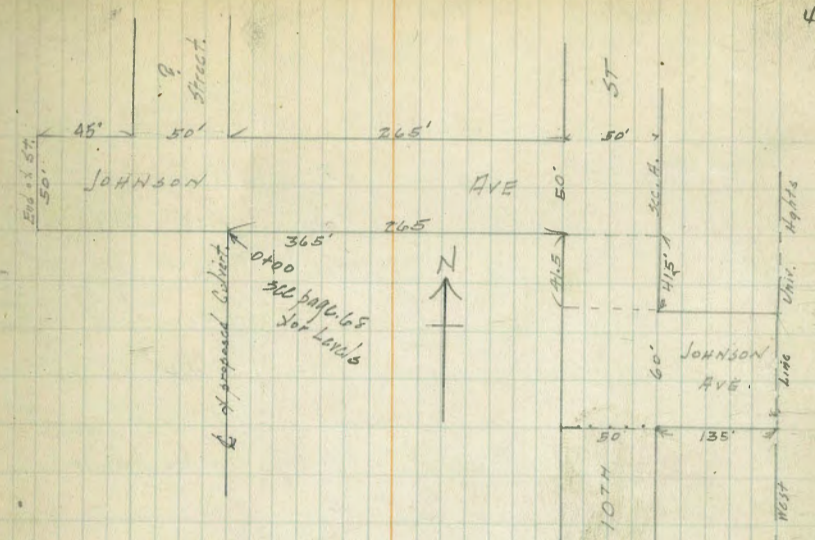
4' W. of W.L. Idaho ^{and 190} S. of El Cajon - Palm Tree

6/6/23 Gregory
 CROSS SECTION OF 60' wide 50' str
 JOHNSON AVE 10' cbs
 from the W.L. of University Heights
 to West End of Johnson

1.10 289.43 288.33 ^{5pk in pole}
 5.20c at 2.00c

W. L. Univ. Heights.

S	1.3	288.1	✓
cb	1.3	288.1	✓
+10 = cement cb of Johnson to East	1.39	289.0	
1/4	1.6	287.8	✓
+1	2.1	287.3	✓
C	1.9	287.5	✓
1/4	2.1	287.3	✓
cb	2.2	287.2	✓
N	2.2	287.2	✓
35' W			
N	2.2	287.2	✓
cb	2.3	287.1	✓
1/4	2.3	287.1	✓
C	2.2	287.2	✓
1/4	2.5	286.9	✓
cb	2.4	287.0	✓
S	2.3	287.1	✓
55' W			
S	2.3	287.1	✓
cb	2.6	286.8	✓
1/4	2.9	286.5	✓
C	2.9	286.5	✓
1/2	3.2	286.2	✓
cb	3.2	286.2	✓
N	3.4	286.0	✓



N	4.3	285.1	✓
cb	3.6	285.8	✓
1/4	3.8	285.6	✓
C	3.6	285.8	✓
1/4	2.7	286.7	✓
cb	2.8	286.6	✓
S	3.2	286.0	✓
135' W = E.L. 10th St 50' wide 10' cbs			
S	5.9	283.5	✓
cb	5.8	283.6	✓
1/4	5.8	283.6	✓
C	5.6	283.9	✓
1/4	5.3	284.1	✓
cb	5.4	284.0	✓
N	5.2	284.2	✓

E. Curb

N	59	✓83.5 ✓	
cb	6.0	✓83.4 ✓	
1/4	6.2	✓85.2 ✓	
c	6.3	✓83.1 ✓	
1/2	6.5	✓82.9 ✓	
cb	6.4	✓83.0 ✓	
3	6.2	✓83.2 ✓ ✓	

E. Quarter

3	6.8	✓87.6 ✓	
cb	6.8	✓87.6 ✓	
1/4	7.0	✓87.4 ✓	
c	7.1	✓87.3 ✓	
1/2	6.8	✓87.6 ✓	
cb	6.4	✓83.0 ✓	
N	6.2	✓83.2 ✓ ✓	

Center 10th

N	6.6	✓87.8 ✓	
cb	6.9	✓87.5 ✓	
1/4	6.9	✓87.5 ✓	
c	7.3	✓87.1 ✓	
1/2	7.3	✓87.1 ✓	
cb	7.0	✓87.4 ✓	
3	6.9	✓87.5 ✓ ✓	

W. Quarter

3	7.3	✓87.1 ✓	
---	-----	---------	--

cb	7.6	✓81.8 ✓	
1/4	8.0	✓81.4 ✓	
c	8.3	✓81.1 ✓	
1/2	8.0	✓81.4 ✓	
cb	7.1	✓84.3 ✓ ✓	
N	6.8	✓87.6 ✓	

W. curb

N	7.6	✓81.8 ✓	
cb	8.3	✓81.1 ✓	
1/4	8.9	✓80.5 ✓	
c	9.3	✓80.1 ✓	
1/2	9.0	✓80.4 ✓ ✓	
cb	8.2	✓81.2 ✓	
3	8.0	✓81.4 ✓	

W. Line 10th St

-10	8.3	✓81.1 ✓	
3	9.1	✓80.3 ✓	
cb	9.7	✓79.7 ✓	
1/2	10.5	✓88.9 ✓	
c	10.8	✓88.6 ✓	
1/4	10.5	✓88.9 ✓	
cb	9.4	✓80.0 ✓	
+3	10.1	✓79.3 ✓ ✓	
N	9.3	✓80.1 ✓	

10th W.

N	10.7	✓78.7 ✓	
---	------	---------	--

cb	11.2	178.2 ✓
1/4	13.0	176.4 ✓
c	13.2	176.2 ✓
1/4	12.8	176.6 ✓
cb	11.8	177.6 ✓
S	10.4	179.0 ✓

cb	5.2	184.1 ✓
1/4	5.0	184.4 ✓
c	4.8	184.6 ✓
1/4	4.9	184.5 ✓
cb	5.0	184.4 ✓
S	4.8	184.6 ✓

Section across 10th St 10' N. of N.L. Johnson

E. Quarter

-10	8.3	181.1 ✓ steps on house
W	8.1	181.3 ✓
cb	7.1	181.3 ✓
1/4	6.6	181.8 ✓
c	6.2	183.2 ✓
1/4	6.2	185.1 ✓
cb	5.3	184.1 ✓
E	5.0	184.4 ✓

S	5.3	184.1 ✓
cb	5.3	184.1 ✓
1/4	5.0	184.4 ✓
c	5.0	184.4 ✓
1/4	5.2	184.2 ✓
cb	4.9	184.5 ✓
N	5.1	184.3 ✓

Center

JOHNSON AVE AGAIN 50' wide this time

• FL. 10th ST. = Sec. A, 10' cbs

S	5.0	184.4 ✓
cb	4.7	184.7 ✓
1/4	4.7	184.7 ✓
c	4.3	185.1 ✓
1/4	4.8	184.6 ✓
cb	5.0	184.4 ✓
N	5.2	184.2 ✓

N	5.0	184.4 ✓
cb	5.1	184.3 ✓
1/4	5.3	184.1 ✓
c	5.3	184.1 ✓
1/4	5.4	184.0 ✓
cb	5.4	184.0 ✓
S	5.6	183.8 ✓

W Quarter

E cb		
N	5.2	184.2 ✓

S	5.8	183.6 ✓
cb	5.5	183.9 ✓
1/4	5.4	184.0 ✓

c	5.5	✓83.9	✓
1/2	5.4	✓84.0	✓
cb	5.3	✓84.1	✓
N	5.1	✓84.3	✓

1/2 curb

N	5.3	✓84.1	✓
cb	5.5	✓83.9	✓
1/2	5.7	✓83.7	✓
c	5.7	✓83.7	✓
1/4	5.7	✓83.7	✓
cb	5.8	✓83.6	✓
S	5.9	✓83.5	✓

1/2 L 10+4

S	6.7	✓84.7	✓
+3	5.9	✓83.5	✓
cb	6.3	✓83.1	✓
1/2	6.1	✓83.3	✓
c	6.0	✓83.4	✓
1/2	6.0	✓83.4	✓
cb	5.9	✓83.5	✓
N	5.4	✓84.0	✓

50' West

N	6.5	✓81.9	✓
+2	6.6	✓81.8	✓
+5	7.6	✓81.8	✓
cb	7.7	✓81.7	✓

1/2	8.2	✓81.1	✓
c	8.4	✓81.0	✓
1/2	8.7	✓80.7	✓
cb	8.8	✓80.6	✓
+5	8.9	✓80.5	✓
S	10.0	✓79.4	✓
+10	10.4	✓79.0	✓

100' West

-10	13.5	✓75.9	✓
S	12.1	✓77.3	✓
+4	10.5	✓78.9	✓
cb	10.4	✓79.0	✓
1/2	10.4	✓79.0	✓
c	10.4	✓79.0	✓
1/2	9.8	✓79.6	✓
cb	9.5	✓79.9	✓
+5	8.3	✓81.1	✓
N	8.2	✓81.1	✓

115' W

N	8.4	✓81.0	✓
cb	9.9	✓79.5	✓
1/2	10.5	✓78.9	✓
c	10.8	✓78.6	✓
1/2	10.8	✓78.6	✓
cb	11.1	✓78.3	✓
S	11.6	✓77.8	✓
+5 = front of garage	11.7	✓77.7	✓

150' W

-5	12.3	✓77.1	✓
5	12.1	✓77.3	✓
cb	11.6	✓77.8	✓
1/4	11.7	✓77.7	✓
c	11.5	✓77.9	✓
1/4	11.4	✓78.0	✓
cb	11.1	✓78.3	✓
+3	10.8	✓78.6	✓
+7	8.8	✓80.6	= lawn
N	8.7	✓80.7	= ✓

182.5' W

N = on cement walk to house	9.93	✓79.4	
+3 = end of "	10.10	✓79.3	✓
+6	11.9	✓77.5	
cb	12.3	✓77.1	✓
1/4	12.3	✓77.1	✓
c	12.5	✓76.9	✓
1/4	12.4	✓77.0	✓
cb	12.4	✓77.0	✓
5 = edge lang	12.7	✓76.7	✓
+5	12.8	✓76.6	✓
T.P.	✓77.4	✓77.54	12.63
		✓76.80	✓

300' W

-5	3.7	✓75.8	✓
5	3.6	✓75.9	✓

cb	3.5	✓76.0	✓
1/4	3.4	✓76.1	✓
c	3.4	✓76.1	✓
1/4	3.2	✓76.3	✓
cb	2.8	✓76.7	✓
1/4	2.5	✓77.0	✓
+7 = lawn	1.0	✓78.5	✓ ✓
N =	0.9	✓78.6	✓ ✓

225' W

N	4.1	✓75.4	✓
cb	4.4	✓75.1	✓
1/4	4.6	✓74.9	✓
c	4.6	✓74.9	✓
1/4	4.7	✓74.8	✓
cb	4.9	✓74.6	✓
5	5.2	✓74.3	✓
+5 = cement walk	4.7	✓74.8	✓

250' W

-5	6.6	✓72.9	✓
5	6.4	✓73.1	✓
cb	5.9	✓73.6	✓
1/4	6.0	✓73.5	✓
c	5.7	✓73.8	✓
1/4	5.6	✓73.9	✓
cb	5.6	✓73.9	✓
N	5.8	✓73.7	✓

299.54

JOHNSON

54

265' W. = E.L. 2 57 50' wide 10' cbs

N	6.7	✓ 71.8 ✓
cb	6.3	✓ 73. ✓ ✓
1/4	6.2	✓ 73.3 ✓
c	6.1	✓ 73.4 ✓
1/4	6.0	✓ 73.5 ✓
cb	6.0	✓ 73.5 ✓
S	6.5	✓ 73.0 ✓
+5	6.6	✓ 74.9 ✓

E. cb.

-5	6.7	✓ 71.8 ✓
S	6.6	✓ 72.9 ✓
cb	6.0	✓ 73.5 ✓
1/4	5.9	✓ 73.6 ✓
c	6.2	✓ 73.3 ✓
1/4	6.3	✓ 73.2 ✓
cb	6.6	✓ 74.9 ✓
N	6.8	✓ 74.7 ✓

E Quarter

N	6.7	✓ 71.8 ✓
cb	6.5	✓ 73.0 ✓
1/4	6.5	✓ 73.0 ✓
c	6.0	✓ 73.5 ✓
1/4	5.9	✓ 73.6 ✓
cb	6.1	✓ 73.4 ✓
S	6.7	✓ 71.8 ✓
+5	6.6	✓ 74.9 ✓

center

-5	6.6	✓ 71.9 ✓
S	6.6	✓ 72.9 ✓
cb	6.2	✓ 73.3 ✓
1/4	6.1	✓ 73.4 ✓
c	6.1	✓ 73.4 ✓
1/4	6.5	✓ 73.0 ✓
cb	6.6	✓ 74.9 ✓
N	6.8	✓ 74.7 ✓

W Quarter

N	6.7	✓ 71.8 ✓
cb	6.4	✓ 73.1 ✓
1/4	6.3	✓ 73. ✓ ✓
c	6.2	✓ 73.3 ✓
1/4	6.2	✓ 73.3 ✓
cb	6.4	✓ 73.1 ✓
S	6.7	✓ 74.8 ✓

W. Curb

S	6.8	✓ 74.7 ✓
cb	6.6	✓ 74.9 ✓
1/4	6.4	✓ 73.1 ✓
c	6.4	✓ 73.1 ✓
1/4	6.4	✓ 73.1 ✓
cb	6.4	✓ 73.1 ✓
N	6.4	✓ 73.1 ✓

279.54

55

W. Line ~ St

H	6.1	✓73.4	✓
cb	6.6	✓72.9	✓
1/2	6.4	✓73.1	✓
c	6.4	✓73.1	✓
1/2	6.5	✓73.0	✓
cb	6.7	✓72.8	✓
S	6.9	✓72.6	✓

45° W. = End of St.

S	6.6	✓72.9	✓
cb	6.3	✓73.2	✓
1/2	6.2	✓73.3	✓
c	6.0	✓73.5	✓
1/2	5.7	✓73.8	✓
cb	5.5	✓74.0	✓
H	5.2	✓74.3	✓

6/6/23 Gregory. CROSS SECTION OF
WITHERBY ST
from NL SUNSET TO
NL Whitman

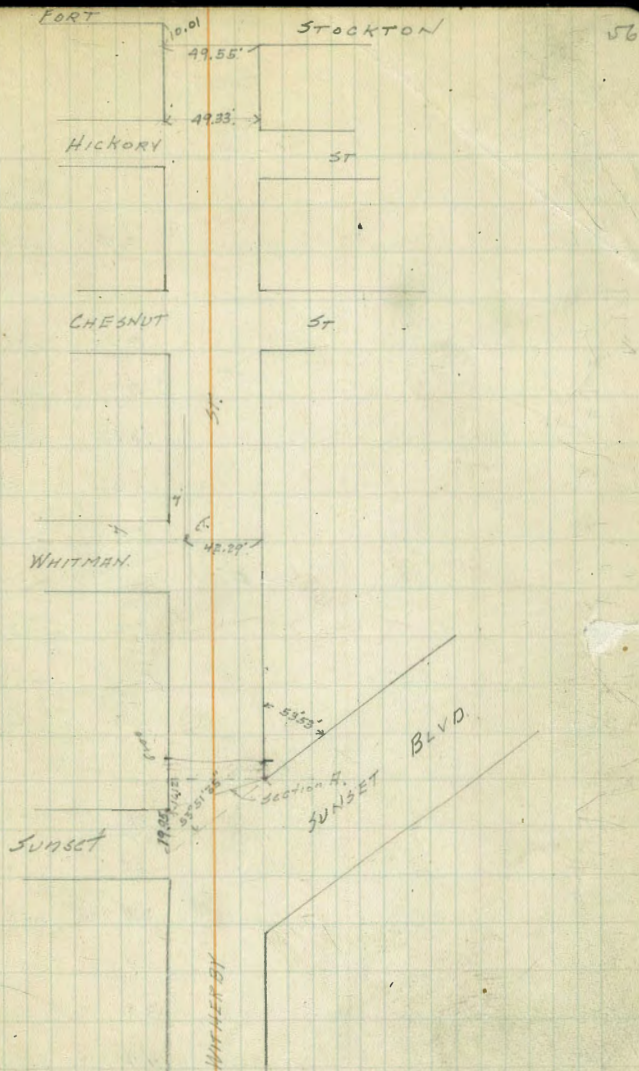
odd widths
10' cbs

1.62 262.24

261.02 B.P.N.E.
Whitman 155.

SECTION A.

W	1.3	261.3
cb	1.8	260.8
1/2	2.2	260.4
c	2.6	260.0
1/4	2.8	259.8
cb	2.9	259.7
E	2.5	260.1
25' N of Sect A on W. 888' - - - E = 0+00		
E	2.2	260.4
cb	3.0	259.6
1/2	3.2	259.4
c	2.9	259.7
1/4	3.0	259.6
cb	2.4	260.2
W	2.0	260.6
0+15		
W	3.3	259.3
cb	3.1	259.2
1/2	3.2	259.4
c	3.3	259.3
1/4	3.3	259.3
cb	3.0	259.6
E	2.4	260.2



	0+44		
E	4.9	259.5	
cb	3.5	259.1	
+1	3.8	258.8	
1/4	3.7	258.9	
C	3.7	258.9	
1/4	3.6	259.0	
cb	3.5	259.1	
W	3.6	259.2	
	0+48		
W	1.9	260.7	
cb +3	3.6	259.2	
cb	3.9	258.7	
	0+70		
W	2.8	259.8	
+7	3.5	258.8	
cb	3.8	258.8	
1/4	3.9	258.7	
C	3.8	258.8	
1/4	4.2	258.4	
+6.5	4.1	258.5	
cb	3.7	258.9	
E	3.1	259.5	
	0+95		
E	3.5	259.1	
cb	3.9	258.7	

+1	4.4	258.2
1/4	4.4	258.2
C	4.1	258.5
1/4	3.7	258.9
cb	8.1	254.5
W	9.6	253.0
+20	12.8	249.8
	1+10	
-20	14.1	248.5
W	11.0	251.6
cb	8.3	254.3
+5	7.4	255.2
1/4	5.7	256.9
+5	3.6	259.0
C	4.2	258.4
1/4	4.6	258.0
+6.5	4.6	258.0
cb	3.9	258.7
E	3.5	259.1
	cb = walk in on E side from here, north.	1+40
	E curb line	5.0
	1/4	5.0
	C	4.5
	+2	4.5
	1/4	8.2
	cb	10.9

W	13.5	249.1
+15	16.1	246.5
+25	19.9	242.7
	1465	
-35	27.9	232.7
-10	17.9	244.7
W	15.3	247.3
cb	12.9	249.7
1/4	8.7	253.9
+5	4.8	257.8
c	4.8	257.8
1/4	5.3	257.3
cb	5.1	257.5
	1485	
E cb line	5.6	257.0
1/4	5.4	257.2
c	5.2	257.4
+2.5	5.2	257.4
1/4	8.8	253.8
cb	13.3	249.3
+5	17.7	244.9
W	18.6	244.0
+7	20.3	242.3
+38	29.8	232.8
+45	34.4	228.2

15 c. of next one.

	1492	
60' W. of W.L.	42.2	220.4
40' ✓ ✓ ✓	34.2	228.4
W.L.	19.1	243.5
	2407	
-40	27.2	235.4
-25	24.6	238.0
W	19.7	242.9
+3	18.3	244.3
cb	14.1	248.5
1/4	9.5	253.1
+6	5.5	257.1
c	5.5	257.1
1/4	5.7	256.9
cb	5.9	256.7
	1435	
E cb	6.1	256.5
1/4	6.0	256.6
c	5.7	256.9
+2	5.4	257.2
1/4	9.5	253.1
cb	13.9	248.7
W	16.0	246.6
+20	15.9	246.7

+90.

	w+65		
-20	14.7	247.9	
W	13.0	249.6	
cb	12.0	250.6	

w+75 = 5L Whitman St 50' wide roads Ecb Line

-20	14.8	247.8	
W	12.9	249.7	
cb	11.5	251.1	
1/2	7.1	255.5	
+4	6.2	256.4	
c	6.3	256.3	
1/2	6.6	256.0	
cb	6.3	256.3	

3. Curb

E cb Line	6.4	256.2	
1/2	6.6	256.0	
c	6.4	256.2	
1/2	6.3	256.3	
cb	11.0	251.6	
W	12.2	250.4	
+15	14.0	248.6	
	S Quarter		
-15	13.2	249.4	
W	11.3	251.3	
cb	9.5	253.1	
1/2	6.1	256.5	

c	6.4	256.2
1/2	6.7	255.9
cb	6.4	256.2

Center

Ecb Line	6.5	256.1
1/2	6.8	255.8
c	6.3	256.3
1/2	5.9	256.7
cb	6.4	256.2
W	6.8	255.8

Graded privately from the north.

6/15/23

Gregory/

CROSS SECTION OF
DWIGHT ST 60' wide 10' cbs
E.L. Alabama to W.L. Mississippi

266.69

60

	10.73	266.69	255.96	BRNE Ala. + Dwight
	E.L. Alabama			
N		10.0	256.7	
cb		10.6	256.1	
1/4		10.4	256.3	
c		10.7	256.0	
1/4		10.7	256.0	
cb		10.6	256.1	
S		10.2	256.5	
	10' E			
S		9.4	257.3	
cb		9.4	257.3	
1/4		9.4	257.3	
c		9.2	257.5	
1/4		9.1	257.6	
cb		9.0	257.7	
N		8.9	257.8	
	40' E			
N		5.3	261.4	
+5		7.0	259.7	
cb		7.2	259.5	
1/4		7.2	259.5	
c		7.1	259.6	
1/4		7.7	259.0	
cb		8.1	258.6	
S		7.8 (1)	258.9	
+6		6.1	260.6	

	50' E	
	6.0	260.7
	7.2	259.5
cb	7.8	258.9
1/4	7.7	259.0
c	7.3	259.4
1/4	6.7	260.0
cb	6.7	260.0
+6	6.5	260.2
+8	5.5	261.1
N	+2.3	269.0
	75' E	
N	+3.5	270.2
+2	+3.5	270.2
+3	5.9	260.8
cb	6.5	260.2
1/4	6.7	260.0
c	7.0	259.7
1/4	6.7	260.0
cb	6.9	259.8
S	6.1	260.6
+1	+3.4	270.1
	85' E	
-1	+3.5	270.5
S	5.4	261.3
7.4	6.5	260.2

26669

cb	6.7	260.0
1/4	6.5	260.2
c.	6.4	260.3
1/4	6.5	260.2
cb	6.4	260.3
+9	5.7	261.0
N	+4.0	270.7
	85'E	
-1	+4.0	270.7
N	5.7	261.0
cb	6.4	260.3
1/4	6.5	260.2
c	6.5	260.2
1/4	6.5	260.2
cb	6.7	260.0
+6	6.4	260.3
S	5.4	261.3
+1	+3.8	270.5
	93'E	
-1	+4.3	271.0
S	5.3	261.4
cb	6.5	260.2
1/4	6.1	260.6
c	6.1	260.6
1/4	6.0	260.7
cb	6.1	260.6

DIVIGHT 61

91
26
25

N	55	261.2
+1	+4.5	271.2
	100'E	
-1	+5.0	271.7
N	5.1	261.6
cb	5.6	261.1
1/4	5.7	261.0
c	5.7	261.0
1/4	6.0	260.7
cb	6.3	260.4
+8	5.3	261.4
S	+4.8	271.5
	122'E	
S	+5.9	272.6
+5	+5.9	272.6
+6	4.1	262.6
cb	5.4	261.3
1/4	5.2	261.5
c	4.9	261.8
1/4	4.8	261.9
cb	4.1	262.6
N	4.0	262.7
+2	+6.5	273.2
	123'E	
N	+6.6	273.3
+1	2.6	264.1

266.69

cb		3.9	262.8
1/4		4.8	261.9
c		4.9	261.8
1/4		5.2	261.5
cb		5.4	261.3
+4		4.1	262.6
+5		+5.9	272.6
5		+5.9	272.6
	150' E		
5		+7.2	273.9
+6		+7.4	274.1
+8		3.8	262.9
cb		4.3	262.4
1/4		4.6	262.1
c		4.0	262.7
1/4		4.1	262.6
cb		4.0	262.7
+3		2.2	264.5
+4		+7.8	274.5
N		+7.8	274.5
T.P.	12.08	278.49	0.28 266.41
		175' E	
N		5.9	272.6
+0.3		15.2	263.3
cb		15.3	263.2
1/4		15.2	263.3

18.5

3.3

11.2

2.8

2.4

278.49

DWIGHT 62

c		15.4	263.1
1/4		15.9	262.6
cb		15.6	262.9
+2		3.3	275.2
5		3.3	275.2
	196' E		
5		2.6	275.9
4.9		2.4	276.1
cb		14.8	263.7
1/4		15.1	263.1
c		14.7	263.8
1/4		13.9	264.6
cb		12.9	265.6
+5		11.3	267.2
+6		2.1	276.4
N		2.3	276.2
	203' E		
N		2.0	276.5
+8		2.2	276.3
+9		9.7	268.1
cb		10.2	268.3
1/4		12.7	265.8
c		13.3	265.2
1/4		11.4	267.1
+6		9.0	269.5
+8		2.0	276.5

278.47

cb			2.2	276.3
S			2.2	276.3
		209'E		
S			2.1	276.4
cb			1.9	276.6
1/4			1.7	276.8
C			1.7	276.8
1/4			2.3	276.2
cb			2.3	276.2
N			2.0	276.5
T.P.	5.98	282.42	2.05	276.44
		242'E		
N			4.8	277.6
cb			5.2	275.2
1/4			5.1	275.3
C			4.8	277.6
1/4			4.7	277.7
cb			4.8	277.6
S			4.8	277.6
		273'E		
S			4.0	278.4
cb			4.0	278.4
1/4			4.1	278.3
C			4.3	278.1
1/4			4.4	278.0
cb			4.6	277.8

282.42

DWIGHT

63

N		4.3	278.1
	276'E = W.L	Mississippi	
N		7.1	275.3
cb		7.1	275.3
1/4		7.1	275.3
C		7.1	275.3
1/4		7.0	275.4
cb		6.4	276.0
S		6.9	275.5
cgk BM		6.9	275.48
			SE Miss Dwight

6/5/23

Gregory

CROSS SECTION OF A
PORTION OF 8th ST
from S.L. of Robinson

66 wide
13' cbs

276.46

8+7

64

151

276.46

274.75

82' N
5th St

+5

6.1

270.4

+8

12.3

264.2

Curb ENDS at S.L. Robt. produced east.

Return at S.W. cor Robt - 8th is 12.5 x 12.5

+11.5 = End of Iron pipe

S.L. Robinson on West.

E

13.5

263.0

+7

10.3

266.2

W

2.4

274.1

cb

2.8

273.7

+15

11.6

264.9

1/4

3.7

272.8

T.P.

7.99

272.03

12.42

264.04

C

4.0

272.5

29' 5"

1/2

4.2

272.3

-25

13.3

258.7

cb

4.4

272.1

-15

11.6

260.4

E

3.2

273.1

-2

9.9

262.1

11' 3"

E

5.8

266.2

E

4.9

271.7

+8

2.8

269.2

cb

5.0

271.5

cb

2.3

269.7

x

1/2

5.3

271.2

1/4

2.3

269.7

C

4.7

271.8

C

2.1

269.9

1/2

4.6

271.9

1/4

1.8

270.2

cb

3.9

272.6

cb

1.4

270.6

x

W

3.4

273.1

+4

1.1

270.9

16' 3"

W

1.4

270.6

W

4.1

272.4

40' 5"

cb

4.8

271.7

W

2.1

269.9

1/4

5.1

271.4

+9

1.8

270.2

C

5.2

271.3

cb

2.5

269.5

x

1/2

5.7

270.8

1/4

2.9

269.1

cb

5.5

271.0

C

2.9

269.1

272.03

1/4	3.0	269.0
cb	3.3	268.7
+3	3.6	268.4
E	8.7	269.3
+5	18.0	260.0
+20	17.6	254.4
+30	18.5	253.5
	47' S	
-35	21.4	250.6
-22	19.3	252.7
-10	15.3	256.7
E	10.0	262.0
+10	3.8	268.2
cb	3.6	268.4
1/4	3.1	268.6
C	3.3	268.7
1/2	3.3	268.7
cb	3.0	269.0
+4	2.1	269.9
+11	2.2	269.8
W	3.7	268.3
+5	7.9	264.1
+15	11.9	260.1
	65' S	
-22	18.4	253.6
-9	12.7	259.3

272.03

8th 57 127 65

W	6.7	265.3
+5	3.2	268.8
+10	2.6	269.4
cb	3.1	268.6
1/4	3.8	268.2
C	4.1	267.9
1/2	4.2	267.8
cb	4.1	267.6
+3	4.5	267.5
E	10.6	261.4
+15	20.7	251.3
+25	25.6	246.4
+45	28.0	244.0
	85' S = N.L. Robin on E. 60 wide 10 obs	
-45	29.4	242.6
-32	28.8	243.7
-17	20.8	251.2
E	10.0	262.0
+7	5.6	266.4
cb	5.6	266.4
1/2	5.2	266.8
C	4.8	267.2
1/2	4.5	267.5
+5	4.4	267.6
cb	3.0	269.0
+4	4.2	267.8

272.03

Inlet of 12" C.P. under 8th + 15th 8th
4.7' S. of H. Cb + 32' W. of W.L.

64

272.03

W	10.2	261.8
+17	19.3	252.7
+27	21.6	250.4
✓ N. Curb		
-35	24.2	247.8
-22	22.4	249.6
W	11.3	260.7
+9	4.4	267.6
cb	3.8	268.2
+5	4.7	267.3
1/4	4.9	267.1
c	5.2	266.8
1/4	5.5	266.5
cb	5.9	266.1
+11	7.5	264.5
E	8.5	263.5
+10	14.3	257.7
+22 + 6' 3" outlet of 10" C.P.	22.8	249.2
+30	24.2	247.6
✓ N. 1/4		
f10	10.4	261.6
E	9.5	263.5
cb	6.4	265.6
1/4	5.8	266.2
c	5.3	266.7
1/4	5.1	266.9

+4	5.0	267.0
cb	3.8	268.2
+3	4.2	267.8
W	11.2	260.8
+20	21.8	250.2
+30	23.8	248.2
✓ center		
-23	19.3	252.7
-13	18.1	253.9
W	10.4	261.6
+7	5.9	266.1
cb	4.5	267.5
+4	5.2	266.8
1/4	5.3	266.7
c	5.4	266.6
1/4	5.8	266.2
cb	6.6	265.4
E	9.0	263.0
+10	10.6	261.4
✓ S. 1/4		
-15	11.8	260.2
E	8.8	263.2
+9	6.8	265.2
cb	6.7	265.3
1/4	6.0	266.0
c	5.6	266.4

1/4	56	266.4
cb	55	266.5
+7	53	266.7
W	9.2	262.8
+22	15.2	256.8

✓ S. Curb

W	5.7	266.3
cb	5.8	266.2
1/4	5.7	266.3
C	5.7	266.3
1/4	6.1	265.9
+7	6.2	265.8
cb	6.7	265.3
E	8.1	263.9
+10	10.0	262.0

3L Robinson on E

E	6.2	265.8
+3	6.8	265.2
cb	6.7	265.3
N. End cement cb. on E	7.07	264.96
Inlet 10" C.P. here		
1/4	5.9	266.1
C	5.5	266.5
1/4	5.6	266.4
cb	5.7	266.3
W	5.5	266.5

N. end of curb on W. 105' S. of 3L Robin (on East)

5' - - - - - 255' - - - - -

Curb in on E Side 3L Robin (on East) to 185' S

- out - - - 185' S. of - - - to 235' ✓

- 17' - - - 235' - - - - - to 285' ✓

Permit out on 37.5' S. at last above but curb not in

Curb paved to 335' S. of 3L Robin (on E) on East Side

- - - - - 355' - - - - - West ✓

7/3/73 Gregory. Levels on proposed culvert (drain)
 Johnson Ave. W. of 10th St. ¹⁰²
 see page 49 for location ₂₇₅₅
 Jacobs is owner of property.

	0.66	275.40	274.5	on side walk
0+00 = S.L. Johnson Ave.			2.4	273.1 ✓
0+15			2.9	271.6 ✓
+18			5.2	270.3 ✓
+65			10.1	265.4 ✓
+68			12.7	264.8 ✓
+77			13.1	264.4 ✓
T.P.	-0.01	262.59	12.88	262.60
+79			2.3	260.3 ✓
+91			3.8	258.8 ✓
+93			6.0	256.6 ✓
1+00			6.7	255.9 ✓
1+01			8.2	254.4 ✓
1+35			13.6	249.0 ✓
T.P.	0.65	253.29	9.95	252.64
+36			9.5	243.8 ✓
+48			14.6	38.7 ✓
+67			20.3	233.0 ✓
+70			24.2	229.1 ✓

7/31/23

Levels on Curb
B 5th at 31st

Gregory.

	4.55	211.29	206.74
		WL 31 st	
S. Curb. no return at S.W. cor.	6.30	204.99	
N ✓	4.54	206.75	
		25' W	
N curb	5.07	206.77	
S ✓	6.91	204.38	
		50' W	
S curb	7.51	203.78	
N ✓	5.61	205.68	
		75' W	
N curb	6.43	204.86	
S ✓	8.14	203.15	
S gutter - Top of Down pipe.	97' W = CB on 7.90	201.39	
		100' W	
S curb	8.01	203.78	
N ✓	6.84	204.45	
N ✓ gutters - Top of C.B.	116' W = CB on 6.76	205.03	
		7.46	203.83
		125' W	
N curb	6.64	204.65	
S ✓	8.03	203.76	
		150' W	
S curb	7.47	203.82	
N ✓	6.01	205.98	
		175' W	
N curb	5.33	205.96	
S ✓	6.70	204.59	

BP. HW
31st + B.

7.11.29

200' W = break.

S curb	5.70	205.59
N ✓	4.42	206.87
No return on S.E. cor. E.L. 31 st		
S curb	5.29	206.00
	12.5' E	
S curb	5.01	206.78
	25' E	
S curb	4.63	206.66
	50' E	
S curb	4.03	207.46

Curb in on S. Side from E.L. Edgement to 95' E
 and 2' return
 Need 12' of curb for Alley return on S. Side B.W. side of alley
 Curb in on N. side from E.L. Edgement to 215' E
 Alley intersection on N. is paved.

Alley on S. bet 31st + Edgement needs 10' of curb ^{on each side} from Prop
 Line to H's of S Curb
 Alley on N. bet 31st + Edgement needs 12' of curb on each
 sides of Alley from N.L. of B to 2' H. of N. C.B. Line

200 Carb. H. 25N 50N

11:00 3.58 20.00 1.00

01:15 3.58 20.00 1.00

01:30 3.58 20.00 1.00

T-2 3.58 20.00 1.00

01:45 3.58 20.00 1.00

02:00 3.58 20.00 1.00

02:15 3.58 20.00 1.00

T-1 3.58 20.00 1.00

02:30 3.58 20.00 1.00

02:45 3.58 20.00 1.00

03:00 3.58 20.00 1.00

03:15 3.58 20.00 1.00

03:30 3.58 20.00 1.00

03:45 3.58 20.00 1.00

04:00 3.58 20.00 1.00

04:15 3.58 20.00 1.00

04:30 3.58 20.00 1.00

04:45 3.58 20.00 1.00

05:00 3.58 20.00 1.00

05:15 3.58 20.00 1.00

05:30 3.58 20.00 1.00

05:45 3.58 20.00 1.00

06:00 3.58 20.00 1.00

06:15 3.58 20.00 1.00

06:30 3.58 20.00 1.00

06:45 3.58 20.00 1.00

07:00 3.58 20.00 1.00

50N 100N

11:00 3.58 20.00 1.00

01:15 3.58 20.00 1.00

01:30 3.58 20.00 1.00

T-2 3.58 20.00 1.00

01:45 3.58 20.00 1.00

02:00 3.58 20.00 1.00

02:15 3.58 20.00 1.00

T-1 3.58 20.00 1.00

02:30 3.58 20.00 1.00

02:45 3.58 20.00 1.00

03:00 3.58 20.00 1.00

03:15 3.58 20.00 1.00

03:30 3.58 20.00 1.00

03:45 3.58 20.00 1.00

04:00 3.58 20.00 1.00

04:15 3.58 20.00 1.00

04:30 3.58 20.00 1.00

04:45 3.58 20.00 1.00

05:00 3.58 20.00 1.00

05:15 3.58 20.00 1.00

05:30 3.58 20.00 1.00

05:45 3.58 20.00 1.00

06:00 3.58 20.00 1.00

06:15 3.58 20.00 1.00

06:30 3.58 20.00 1.00

06:45 3.58 20.00 1.00

28-29

14m

35
41
60
70
75

19.0

Jaw w. 6

30 19.3

ELI A.

48

47.70

15.7
59.
74.7

110
40
50
75
83
85
100
123
150
175
196
203
208
211
242
273
296

15 + 21.93

48.

14.8

15 84.73 Cb.

15 + 21.93

95.99

16 + 17.92

77.25
1.89
75.36

14

16

~~16~~

29

40

47

65

85

21.7

30

27

19

33

16.3

17.3