

1101

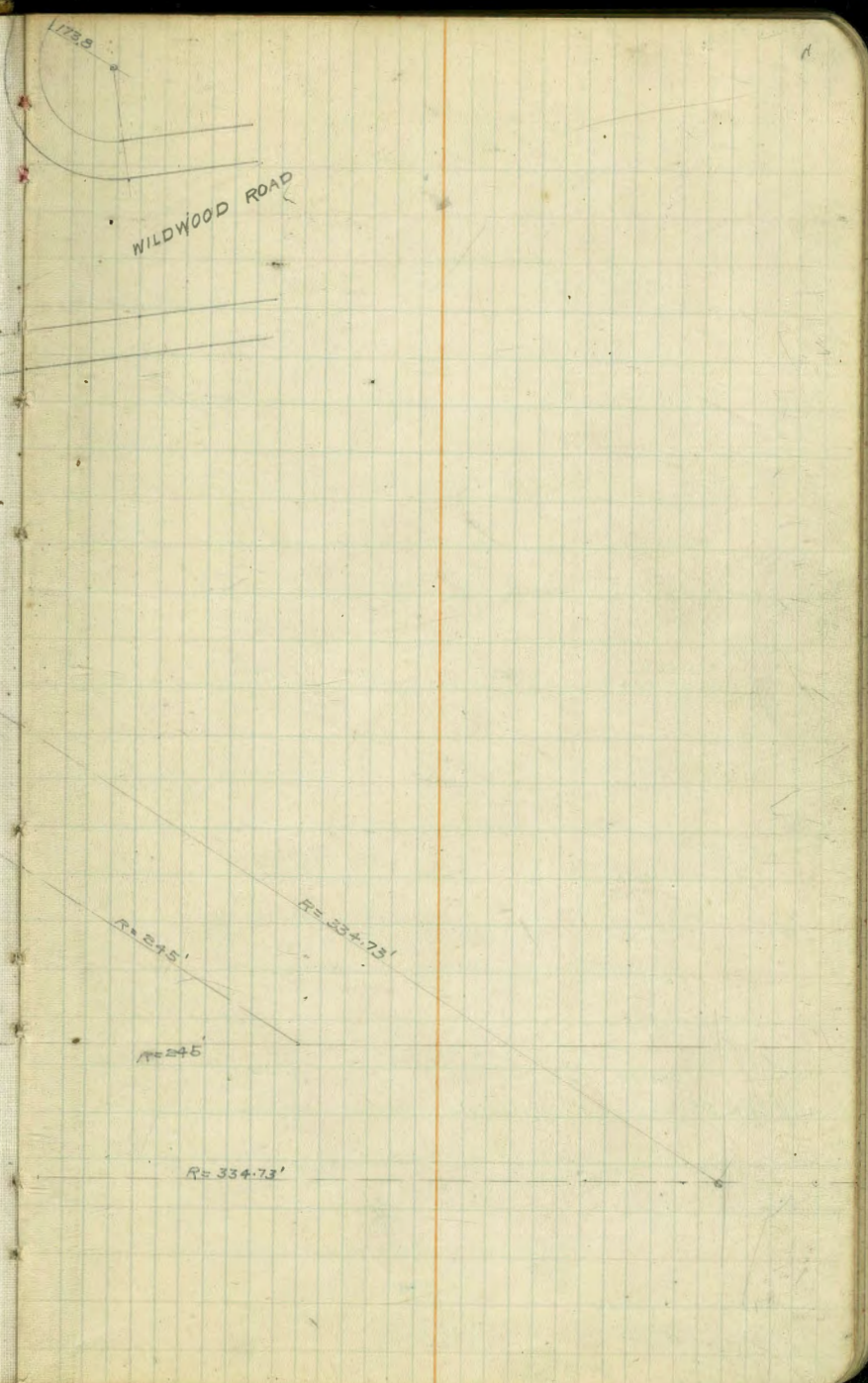
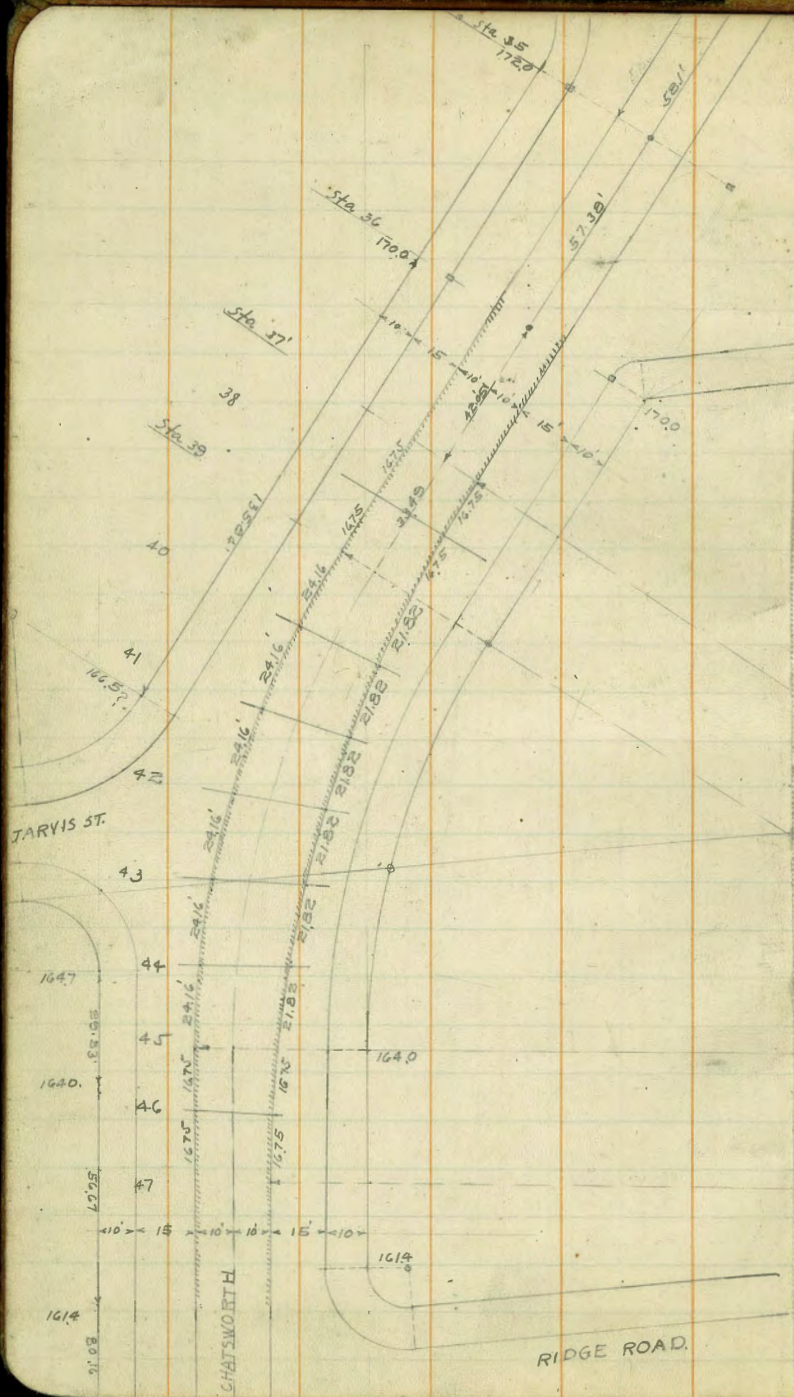
FIELD BOOK

385

MICROFILMED

DEC 21 1964

1101



CHAISWORTH

25  
29  
30  
31

Sta 32  
180.4

+0.23

+0.02

180.4

Sta 33  
177.5

5576

176.88

Sta 34

GARRISON ST.

519

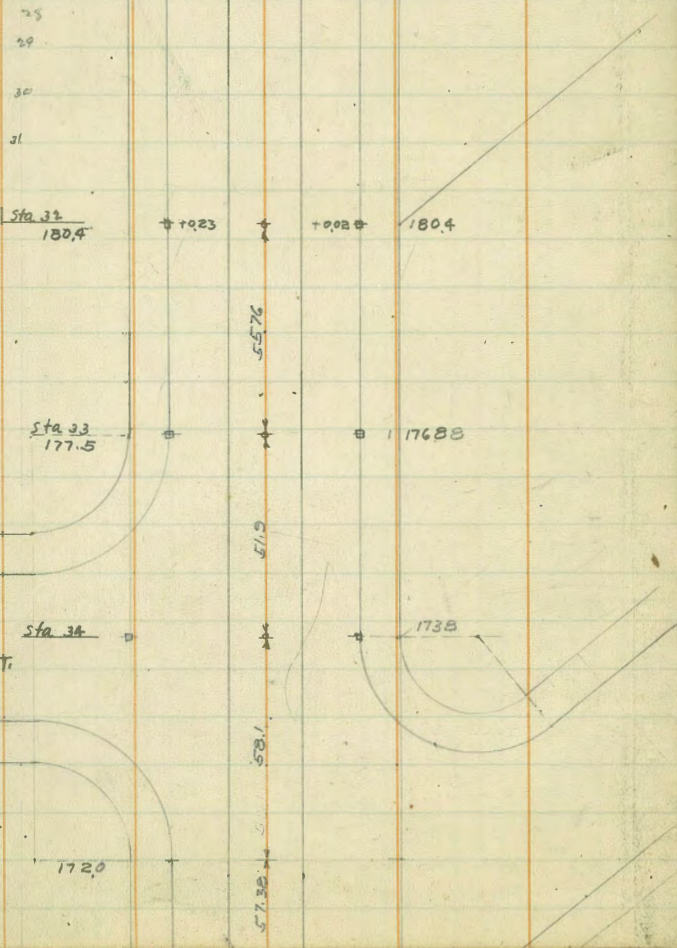
173.8

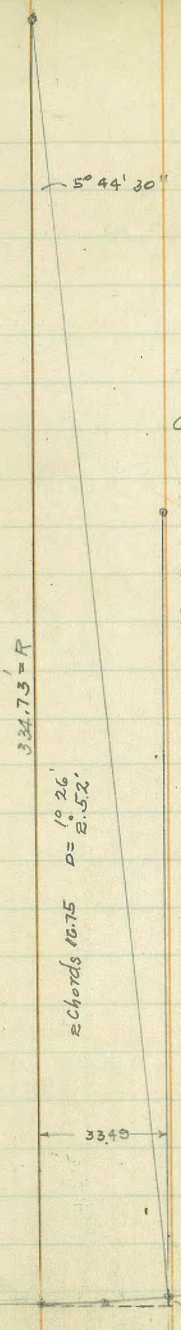
Sta 35

172.0

581

57.82





5° 44' 30  
 11° 29'  
 1 = 33° 55  
 11 29  
 22° 26'

d = 1° 52' 10" ✓  
 3 44 20 ✓  
 5 30 30 ✓  
 7 28 40 ✓  
 9 20 50  
 11 13 00

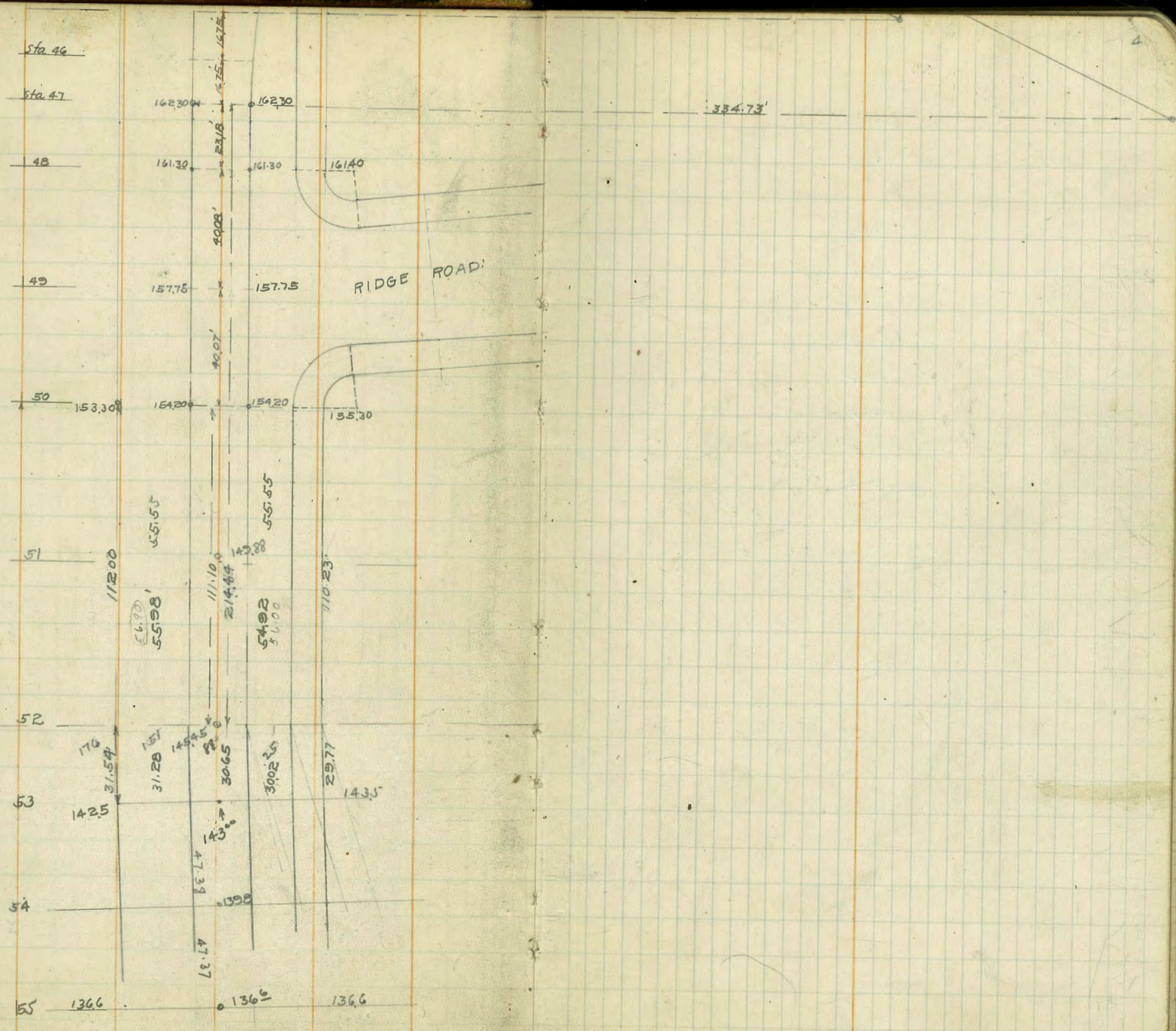
C = 21.825

A = 22° 26'  
 5 44 30  
 5 44 30  
 33° 55' 00 ✓

Tangent = 102.07'

R = 245.00  
 A = 33° 55'  
 T = 74.71'

2° 49' 35"  
 5° 39' 10"  
 8° 28' 45"  
 11° 18' 20" C = 24.16'  
 14° 07' 55"  
 16° 57' 30"  
 33° 55'



€

55.98'			
31.28'	52	145.45	54.62' P.L.
47.38'	53	148.00	30.02'
47.37'	54	139.8	
40.02	55	186.40	
40.03	56	134.70 ✓	
36.61	57	132.80 ✓	
36.62	58	130.53 ✓	
50.1	59	138.24 ✓	
30	60	125.12 ✓	P.L.
40.7	61	123.4 ✓	
40.7 ✓	62	120.95 ✓	
60 ✓	63	118.5 ✓	
49.88 ✓	64	116.00 ✓	
49.88 ✓	65	113.33	
49.88 ✓	66	110.67	
49.88 ✓	67	108.00	
49.88 ✓	68	105.33	
49.88 ✓	69	102.67	
60 ✓	70	100.00	
55 ✓	71	98.00	
55 ✓	72	95.7	
55 ✓	73	93.4	
55 ✓	74	91.1	
55 ✓	75	88.8	
60 ✓	76	86.5	
	77	84.5	

117.98-BM Chatsworth a La Cresta S.W. Cor. B.R

130.68 X							
-12.70							
117.98 BM							
+0.60							
118.58 X	E 58 W	E 59 W	E 60 W	E 61 W			
130.43	130.43	128.14	128.14	125.02	123.40	123.40	
-12.93	2.25	0.25	2.54	2.54	5.66	5.66	7.28
105.65	1.38	0.40	3.70	2.90	6.27	6.31	7.73
+0.94							7.28
106.49 X							7.28
-12.95							7.28
93.54	E 62 W	E 63 W	E 64 W	E 65 W			
+1.98	120.75	120.95	118.50	118.50	116.00	113.33	113.33
95.52 X	9.73	9.73	0.08	0.08	2.58	2.58	5.25
-12.54	9.73	11.04	0.09	1.47	3.15	3.14	5.25
82.58							5.25
+2.78							5.25
85.36 X	E 66 W	E 67 W	E 68 W	E 69 W			
8.25	110.67	110.67	108.00	108.00	105.33	102.67	102.67
77.11 ✓	7.91	7.91	10.35	10.35	1.16	1.16	3.82
77.14 = BM	8.55	8.48	11.21	11.15	1.90	1.75	4.54
	-0.64	0.57	-0.63	-0.87	-0.74	-0.59	4.42
							-0.60
	E 70 W	E 71 W	E 72 W	E 73 W			
	122.22	122.22	98.00	98.00	95.70	95.70	93.40
	6.54	7.03	2.49	2.49	10.75	10.75	2.12
	-0.05	-0.54	-1.06	-0.65	-0.75	-0.62	2.81
							2.69
							-0.32
							-0.57
	E 74 W	E 75 W	E 76 W	E 77 W			
	91.10	91.10	88.80	88.80	86.50	84.50	84.50
	4.42	4.42	6.72	6.72	9.02	9.02	11.02
	5.05	5.01	7.25	7.24	9.11	9.54	11.53
	-0.63	-0.59	-0.57	-0.52	-0.09	-0.52	-0.51
							0.51
	E 78 W	E 79 W	E 80 W	E 81 W			
	82.20	82.20	80.00	80.00	77.70	75.70	75.70
	12.22	12.22	3.26	3.26	4.46	4.46	5.66
	12.94	12.70	4.06	3.05	5.38	4.83	6.60
	-0.72	-0.48	-0.80	-0.43	-0.92	-0.37	-0.94
							-0.22
	E 82 W	E 83 W	E 84 W	E 85 W			
	78.50	78.50	77.50	77.50	77.31	77.31	77.13
	6.36	6.36	7.86	7.86	8.05	8.05	8.23
	7.31	6.46	3.56	3.00	9.20	8.12	9.61
	-0.45	-0.40	-0.70	-0.14	-1.15	-0.07	-1.38
							-0.01
	E 86 W	E 87 W					
	76.04	76.04					
	8.42	8.42					
	10.45	8.35					
	-2.03	+0.07					

S.W. Webster Drive

BM 77.14 Ring curb Chatsworth E of Car tracks.

12.10  
85.24 x

55'		83.3
55'	78	82.1
55'	79	80.7
55'	80	79.7
55'	81	78.5
60'	82	77.5
44.79	83	77.31
44.79	84	77.13
44.79	85	76.94
AS 2.99	86	
9.36	E 77 <sup>22</sup>	
43.47		77.51
34.65	87	78.84
60	88	80.43
43.56	89	82.35
43.56	90	84.90
43.56	91	87.45
43.56	92	90.00
50.39	93	92.55
50.38	94	94.25
60	95	96.00
22.83	96	96.55
22.83	97	96.73
22.83	98	96.91
22.83	99	97.09
22.83	100	97.27
	101	97.45

	E 87	W	E 88	W	E 89	W	E 90	W
	78.24	78.24	80.43	80.47	82.35	82.35	84.90	84.90
	10.40	10.40	8.81	8.81	6.89	6.89	4.34	4.34
BP 96.65 94.3	10.26	10.50	8.48	9.99	7.61	7.96	4.68	6.28
	+0.44	-0.10	+0.33	-1.18	-0.72	-0.97	-0.34	-1.94
97.08 x +10.93								
96.75 +10.69								
107.44 x +1.30								
107.14 +13.03								
120.17 x +0.34								
119.83 119.90								
	E 91	W	E 91	W	E 92	W	E 93	W
	87.45	87.45	87.45	87.45	90.00	90.00	92.45	92.45
	1.79	1.79	9.63	9.63	7.08	7.08	4.63	4.63
	2.36	3.62	10.21	11.47	7.73	8.77	4.53	5.75
	-0.57	-1.23	-0.58	1.84	-0.65	-1.29	+0.10	-1.12
	E 94	W	E 95	W	E 96	W	E 97	W
	94.15	94.15	95.90	95.90	96.45	96.45	96.63	96.63
	2.93	2.93	1.18	1.18	0.63	0.63	10.81	10.81
	2.68	2.96	1.12	1.57	-0.33	1.63	10.32	11.73
	+0.25	-0.03	+0.06	-0.39	+0.30	-1.00	+0.45	-0.92
	E 98	W	E 99	W	E 100	W	E 101	W
	96.81	96.81	96.99	96.99	97.17	97.17	97.35	97.35
	10.63	10.63	10.45	10.45	10.27	10.27	10.09	10.09
	10.17	11.40	10.15	11.12	10.49	10.91	10.20	10.63
	+0.46	-0.77	+0.30	-0.67	+0.22	-0.64	-0.11	-0.54
	E 102	W	E 103	W	E 104	W	E 105	W
	97.56	97.56	97.93	97.93	98.30	98.30	98.70	98.70
	5.28	5.28	5.51	5.51	5.14	5.14	8.74	8.74
	5.81	10.45	9.62	10.07	9.72	9.90	8.95	8.71
	+0.07	-0.57	-0.11	-0.56	-0.58	-0.76	-0.21	+0.03
	E 106	W	E 107	W	E 108	W	E 109	W
	99.10	99.10	99.50	99.50	99.90	99.90	101.21	101.21
	8.34	8.34	7.94	7.94	7.54	7.54	6.23	6.23
	8.34	7.91	7.63	7.11	6.86	6.63	6.54	5.54
	0.00	+0.43	+0.31	+0.83	+0.68	+0.91	-0.31	+0.69
	E 110	W	E 111	W	E 112	W	E 113	W
	102.07	102.07	104.92	104.92	106.78	106.78	108.64	108.64
	4.37	4.37	2.52	2.52	-0.66	0.66	11.53	11.53
	6.28	4.57	2.83	3.95	3.22	2.35	11.92	12.64
	-1.91	-0.20	-0.31	-1.43	-2.56	-1.69	-0.39	-4.11
	E 114	W	E 115	W	E 116	W		
	110.50	110.50	112.35	112.35	114.21	114.21		
	9.67	9.67	7.82	7.82	5.96	5.96		
	10.59	11.44	8.65	10.19	6.49	7.89		
	-0.92	-1.77	-0.83	-2.37	-0.53	-1.93		

RR=76.75

BM 77.14  
+0.31  
82.05 x

78.07	78.11
3.98	3.94
3.48	3.44
70.05	70.05

2 stakes for curb at Culvert No 6

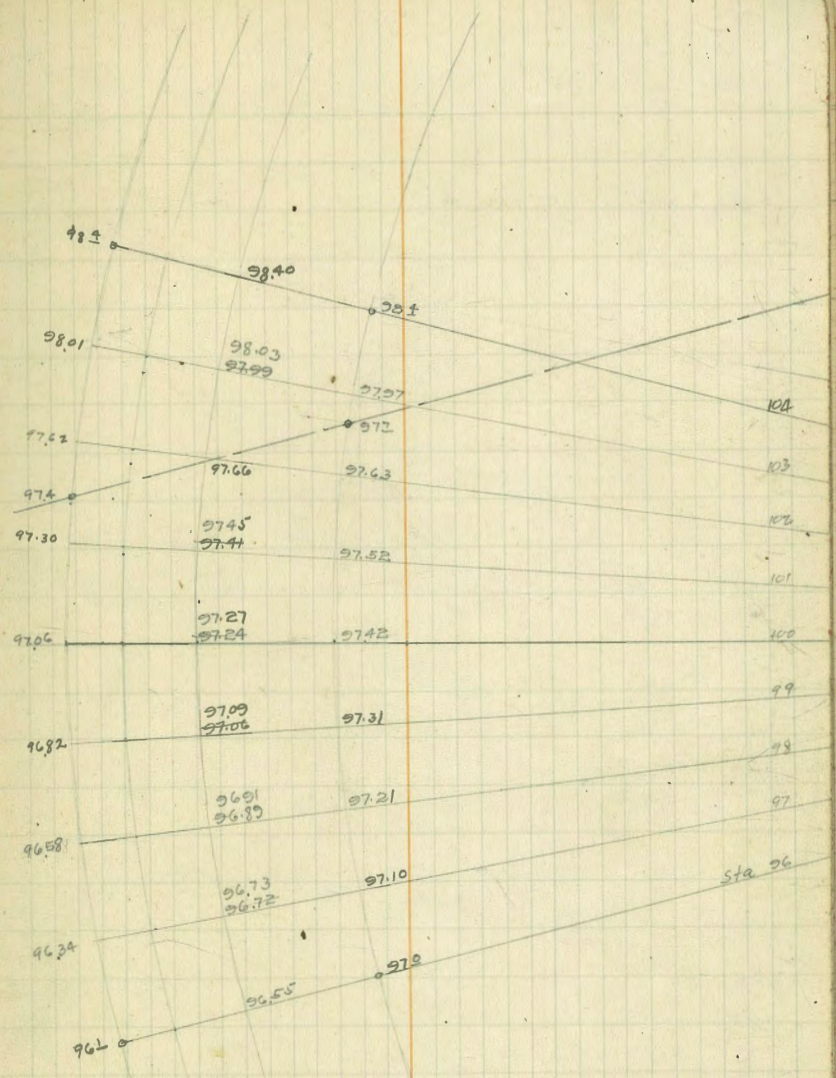


$\Delta = 28^{\circ} 49' 30''$

$R = 363' \quad C = 22.83' \quad LC = 180.82'$

$R = 403' \quad C = 25.35' \quad LC = 200.74'$

	1°	48'	6"
	3	36	12
	5	24	18
Chords:	7	12	24
	9	00	30
	10	48	36
	12	36	42
	14	24	48





116  
 117  
 118  
 119

1285	1285	1285	123
1240	1240	1285	122
12176	1240	1285	121
		1285	120
		11998	119
		11767	118
		11678	117
		11617	116

1285  
 1285  
 1285  
 1240  
 1240  
 12176  
 11998  
 11767  
 11678  
 11617

1896 28.65'  
 2001 29.28'  
 2001 30.74'  
 2009 20.02' 30.59'  
 21.07' 31.63'

1240  
 3.72%

4.36%

57.54  
 50'  
 63.23  
 64.23

25.93'				
25.93'	128	135.71	27.04'	
25.93'	129	137.15	27.04'	
25.93'	130	138.59	27.04'	
25.93'	131	140.03	27.04'	
25.93'	132	141.47	27.04'	
25.93'	133	142.91	27.04'	
25.93'	134	144.36	27.04'	
25.93'	135	145.80	27.04'	
25.93'	136	146.53	27.04'	
25.93'	137	147.95	27.04'	
25.93'	138	149.37	27.04'	
25.93'	139	150.79	27.04'	
25.93'	140	152.21	27.04'	
25.93'	141	153.63	27.04'	
25.93'	142	155.05	27.04'	
50'	143-PT.	156.46		
20'	144	159.13		
20'	145	160.14		
20'	146	161.03		
20'	147	161.78		
20'	148	162.44		
20'	149	162.93		
20'	150	163.31		
20'	151	163.57		
20'	152	163.70		
	153	163.71		

BM 11003 H26

+4.05

123.88 π

-0.20

123.68

+12.20

135.88 π

-0.41

135.47

+12.54

148.01 π

-0.54

147.47

+12.94

160.41 π

-0.32

160.09

+7.27

167.36

-5.88

161.48 =

161.58 BR

161.58 BM 200's Abott:

+0.09

167.67 π

E 116 W E 117 W E 118 W E 119 W

114.21 114.21 116.07 116.07 117.57 117.57 118.89 118.89

9.67 9.67 7.81 7.81 6.31 6.31 5.00 5.00

11.60 11.60 9.01 9.01 6.74 6.74 4.72 4.72

-0.93 -1.20 -0.99 -0.53 -1.27 +0.88 -1.22

E 120 W E 121 W E 122 W E 123 W

121.60 121.60 124.40 124.40 126.26 126.26 128.40 128.40

2.22 2.22 11.44 11.44 9.62 9.62 7.48 7.48

2.34 2.34 12.00 12.20 10.39 10.28 8.88 7.99

-0.12 -1.33 -0.52 -0.72 -0.77 -1.20 -1.35 -0.51

E 124 W E 125 W E 126 W E 127 W

129.84 129.84 131.28 131.28 132.72 132.72 134.16 134.16

6.04 6.04 4.60 4.60 3.16 3.16 1.72 1.72

8.17 7.03 5.58 5.64 3.95 3.96 4.11 2.77

-2.13 -0.99 -0.98 -1.04 -0.79 -0.80 -2.30 -1.08

E 128 W E 129 W E 130 W E 131 W

135.61 135.61 137.05 137.05 138.49 138.49 139.93 139.93

2.27 2.27 10.54 10.56 9.58 9.58 8.08 8.08

2.75 1.19 12.54 11.94 11.04 10.39 10.08 9.17

-2.48 -0.92 -1.58 -0.98 -1.52 -0.87 -2.00 -1.09

E 132 W E 133 W E 134 W E 135 W

141.37 141.37 142.81 142.81 144.26 144.26 145.70 145.70

6.04 6.04 5.20 5.20 3.75 3.75 2.65 2.65

8.31 7.40 6.52 6.16 5.14 4.65 3.67 3.36

-1.67 -0.74 -1.32 -0.96 -1.30 -0.90 -1.02 -0.71

E 136 W E 137 W E 138 W E 139 W

146.43 146.43 147.85 147.85 149.27 149.27 150.69 150.69

1.58 1.58 2.14 2.16 1.14 1.14 9.72 9.72

2.50 1.71 1.19 0.54 11.87 11.33 10.40 10.18

-0.92 -0.13 -1.03 -0.38 -0.73 -0.19 -0.68 -0.44

E 140 W E 141 W E 142 W E 143 W

152.11 152.11 153.53 153.53 154.95 154.95 156.36 156.36

8.20 8.30 6.88 6.88 5.40 5.40 4.05 4.05

9.18 8.71 7.22 7.44 6.43 6.22 5.40 5.10

-0.88 -0.41 -0.94 0.76 -0.97 -0.76 -0.44 -1.05

E 144 W E 145 W E 146 W

158.26 158.26 159.68 159.68 161.10 161.10 162.53 162.53

11.20 11.20 8.63 8.63 7.62 7.62 6.73 6.73

12.65 12.26 10.45 10.14 9.41 9.38 8.10 8.07

-1.35 -0.96 -1.28 -1.51 -1.29 -1.19 -1.37 -1.34

E 147 W E 148 W E 149 W E 150 W

161.68 161.68 163.10 163.10 164.52 164.52 165.94 165.94

5.08 5.08 4.83 4.93 5.32 5.32 4.35 4.35

7.17 7.24 5.90 5.62 6.45 6.38 5.44 5.06

-1.12 -1.28 1.07 -0.79 -1.13 -1.06 -0.99 -0.61

E 151 W E 152 W E 153 W E 154 W

162.47 162.47 163.90 163.90 165.32 165.32 166.74 166.74

4.19 4.19 4.06 4.06 4.05 4.05 4.17 4.17

4.09 4.81 4.74 4.52 4.60 4.45 4.58 4.46

-0.39 -0.62 -0.68 -0.26 -0.55 -0.40 -0.41 -0.20

E 155 W E 156 W E 157 W

168.95 168.95 170.37 170.37 171.79 171.79 173.21 173.21

4.71 4.71 4.93 4.95 5.13 5.13 5.39 5.39

4.80 5.24 4.91 5.66 4.80 6.03 4.94 6.10

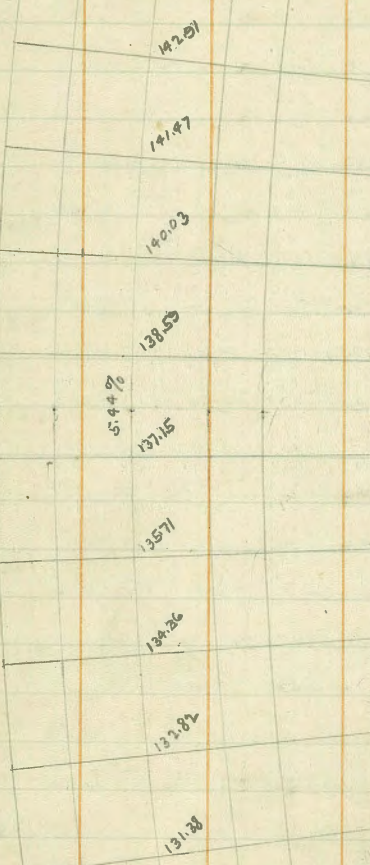
-0.15 -0.53 1.02 -0.71 1.03 1.06 1.27 -0.89

E 158 W E 159 W

162.25 162.25 163.67 163.67 165.09 165.09 166.51 166.51

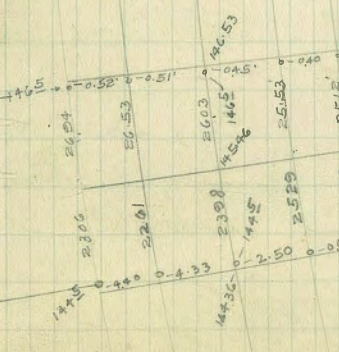
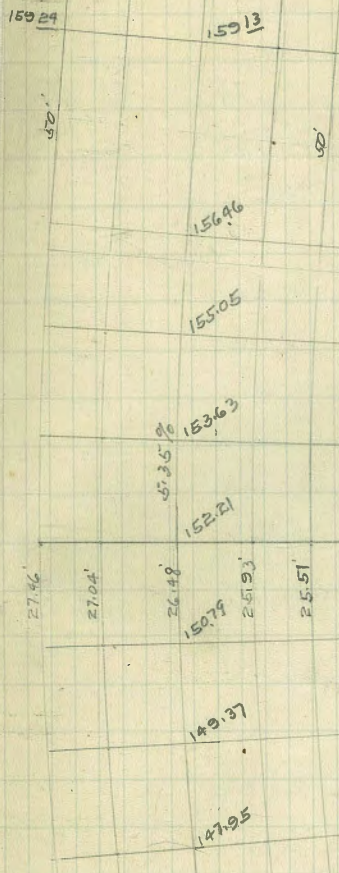
5.41 5.41 5.62 5.62 6.12 6.12 6.87 6.87

4.15 4.27 -0.19 -0.75



136  
135  
134  
133  
132  
131  
130  
129  
128  
127  
126  
125  
124  
PC. 123

r 31° 48'  
R e = 954'  
L.C. 533.67  
C { 27.04'  
25.04'



159.02	Sta. 144	0°	47'	42"	
		1	35'	24"	
		2	23'	06"	
		3	10'	48"	
		3	58'	30"	P.T. 143
		4	46'	12"	142
		5	33'	54"	
		6	21'	36"	141
		7	08'	18"	
		7	57'	00"	140
		8	44'	42"	
		9	32'	24"	139
		10	20'	06"	
		11	07'	48"	138
		11	55'	30"	
		12	43'	12"	137
		13	30'	54"	
		14	18'	36"	136
		15	06'	18"	135
		15	54'	00"	

134

20'					
60'	154	163.59			
60'	35.68' 155	162.73	163.95	162.71	
	24.32'				21.76'
24.32'	156 PC	162.53	162.51	162.28	
24.32'	157	162.45	162.30	161.95	
24.32'	158	162.25	162.10	161.75	
24.32'	159	162.04	161.89	161.54	
24.32'	160	161.84	161.69	161.34	
24.32'	161	161.63	161.48	161.13	
24.32'	162	161.42	161.27	160.92	
24.32'	163	161.22	161.07	160.72	
24.32'	164	161.01	160.86	160.51	
24.32'	165	160.80	160.65	160.30	
63.61'	166 EG	160.46	160.44	160.22	
	24.32'	160.23		160.24	21.76
63.62'	167		159.87		41.85
44.92'	168		159.30		
44.91'	169		159.16		
10.17'	170		159.93		
49.83'	171		159.00		
60'	172		157.25		
50'	173		156.00		
50'	174		154.00		
50'	175		152.00		
60'	176		150.00		
60'	177		148.55		
60.76'	178		147.10		
60.77'	179		147.33		

BM 16158 B.P. 200.5 Alcott.

+ 3.39  
1650.8 π

E 160 W	E 161 W	E 162 W	E 163 W
161.94	161.34	161.63	161.13
3.24	3.74	3.85	3.95
3.12	4.41	3.27	4.64
+0.12	-0.67	+0.18	-0.69
+0.24	-0.63	+0.24	-0.63
+0.01			-0.58

E 164 W	E 165 W	E 166 W	E 167 W
161.01	160.51	160.80	160.30
4.07	4.57	4.28	4.78
3.80	5.15	4.23	5.26
+0.18	-0.58	+0.05	-0.48
+0.06	-0.54	+0.06	-0.54
-0.04			-0.57

E 168 W	E 169 W	E 170 W	E 171 W
159.77	159.77	159.20	159.20
5.31	5.91	5.88	5.88
5.22	5.95	5.83	6.42
+0.09	-0.64	+0.05	-0.54

NE Alcott.

E 168 W	E 169 W	E 170 W	E 171 W
159.20	159.20	159.06	159.03
1.45	1.45	1.89	1.89
1.40	1.29	1.19	0.30
+0.05	-0.54	+0.40	+1.20
-0.27	-0.55	-0.27	-0.43
-0.43			1.24

E 172 W	E 173 W	E 174 W	E 175 W
157.85	157.85	155.20	155.20
2.90	2.90	4.75	4.75
3.01	3.42	5.91	5.39
-0.21	-0.62	-0.76	-0.64
-0.73	-0.63	-0.71	-0.62

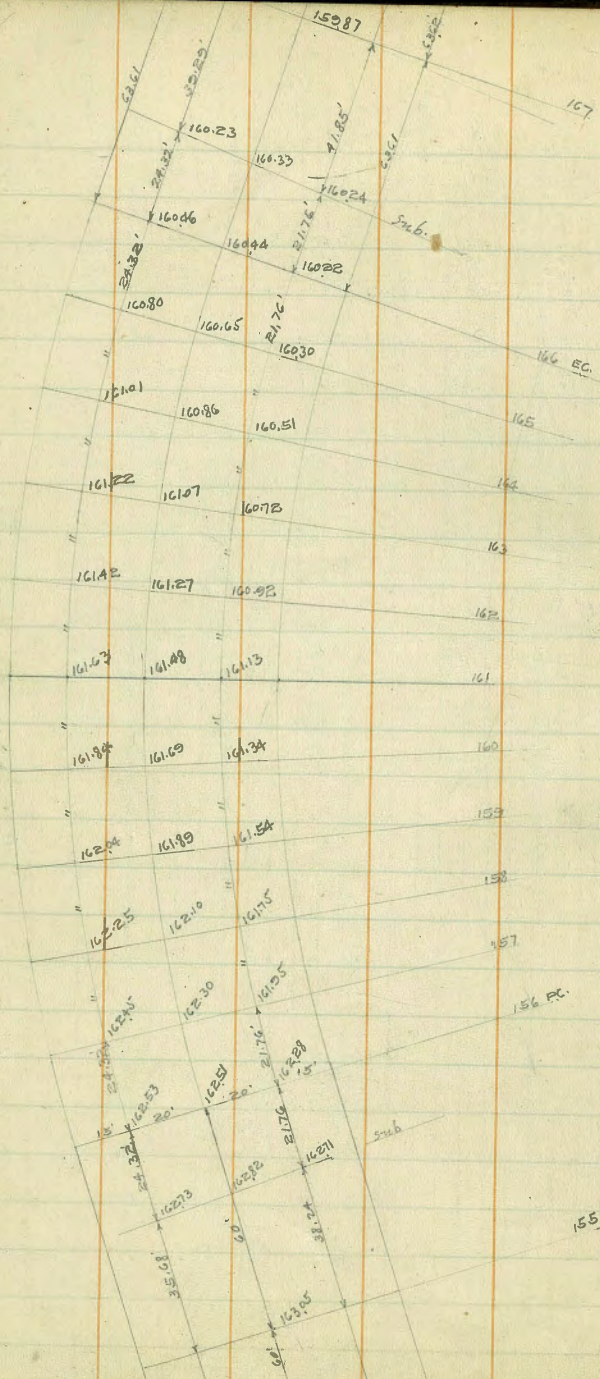
  

E 176 W	E 177 W	E 178 W	E 179 W
149.20	149.20	148.45	148.45
7.75	10.75	13.09	3.09
11.42	11.44	4.33	4.47
-0.67	-0.69	-1.24	-1.38
-1.31	-0.13	-1.31	-0.13
-1.10			-0.10

BM Chertiss

E 180 W	E 181 W	E 182 W
147.47	147.47	147.27
4.07	4.07	4.27
5.27	4.17	5.17
-1.20	-0.10	-0.00
+1.32	-0.50	+1.16
-0.46		+0.65



$\angle A = 360'$

$R = 340'$

$R = 380'$

$\Delta 36^\circ 40'$

$L.C. = 239.05'$

$C \begin{cases} = 1.76' \\ = 24.32' \end{cases}$

$1^\circ 50'$

$3^\circ 40'$

$5^\circ 30'$

$7^\circ 20'$

$d = 9^\circ 10'$

$11^\circ 00'$

$12^\circ 50'$

$14^\circ 40'$

$16^\circ 30'$

$18^\circ 20'$

168  
1592

159.30

1553

44.8

165

159.55

159.16  
159.34

159.7

Alcott.

159.170

171

159.49

159.03  
159.32

1582

159.15  
159.28

43.83

BROWNING

172

157.9

157.95

1582

60'

173

1562

156.00

1562

174

60'

154.00

175

60'

152.00

176

1502

60'

150.00

1502

CURTIS.

150°

50' 150.00

176  
1502

14

CURTIS

148.35

148.50

177

148.75

146.2

147.0

178

147.5

60.76

146.82

147.33

179

147.85

60.77

146.24

147.57

180

148.2

60.47

147.0

147.37

181

60.01

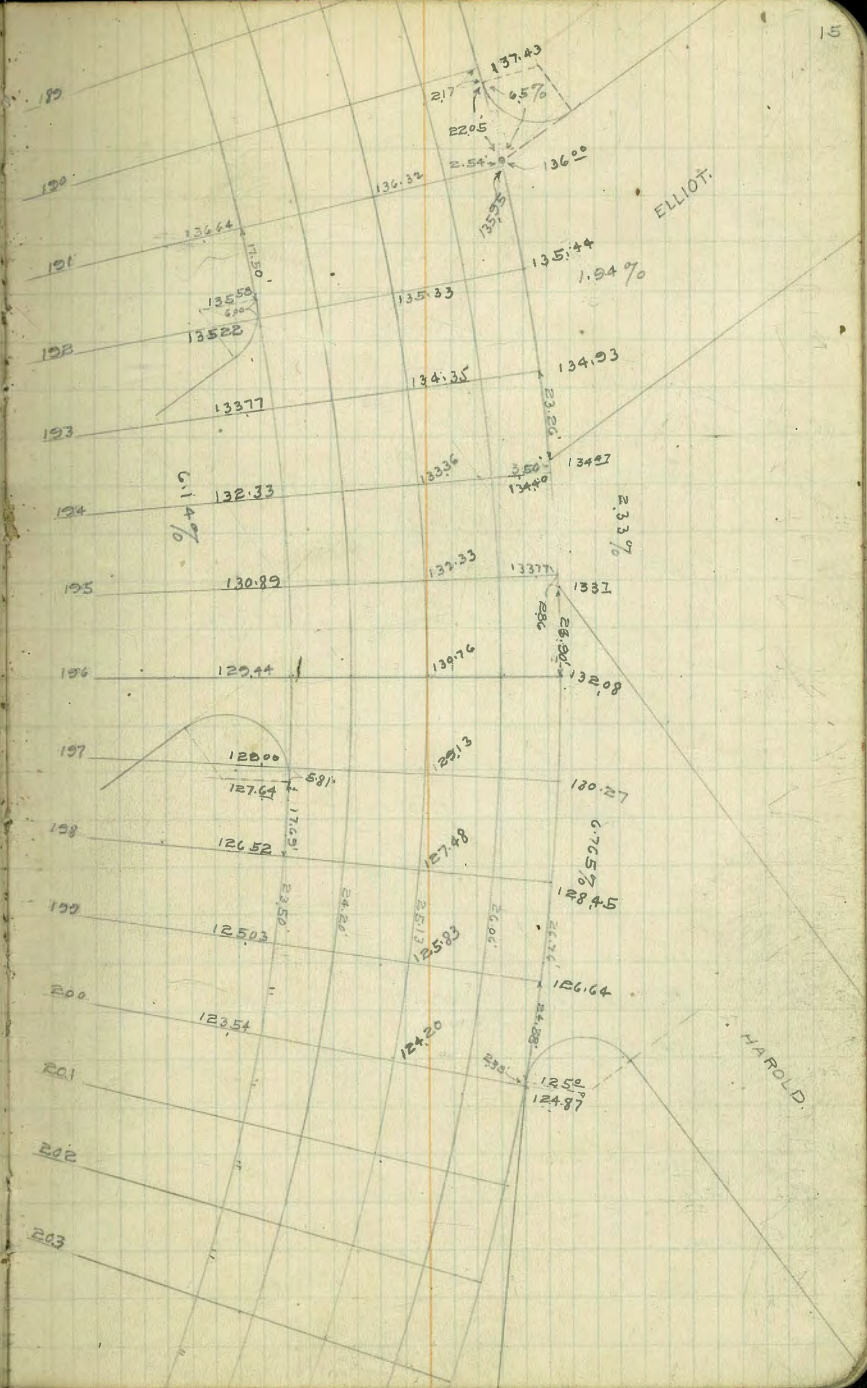
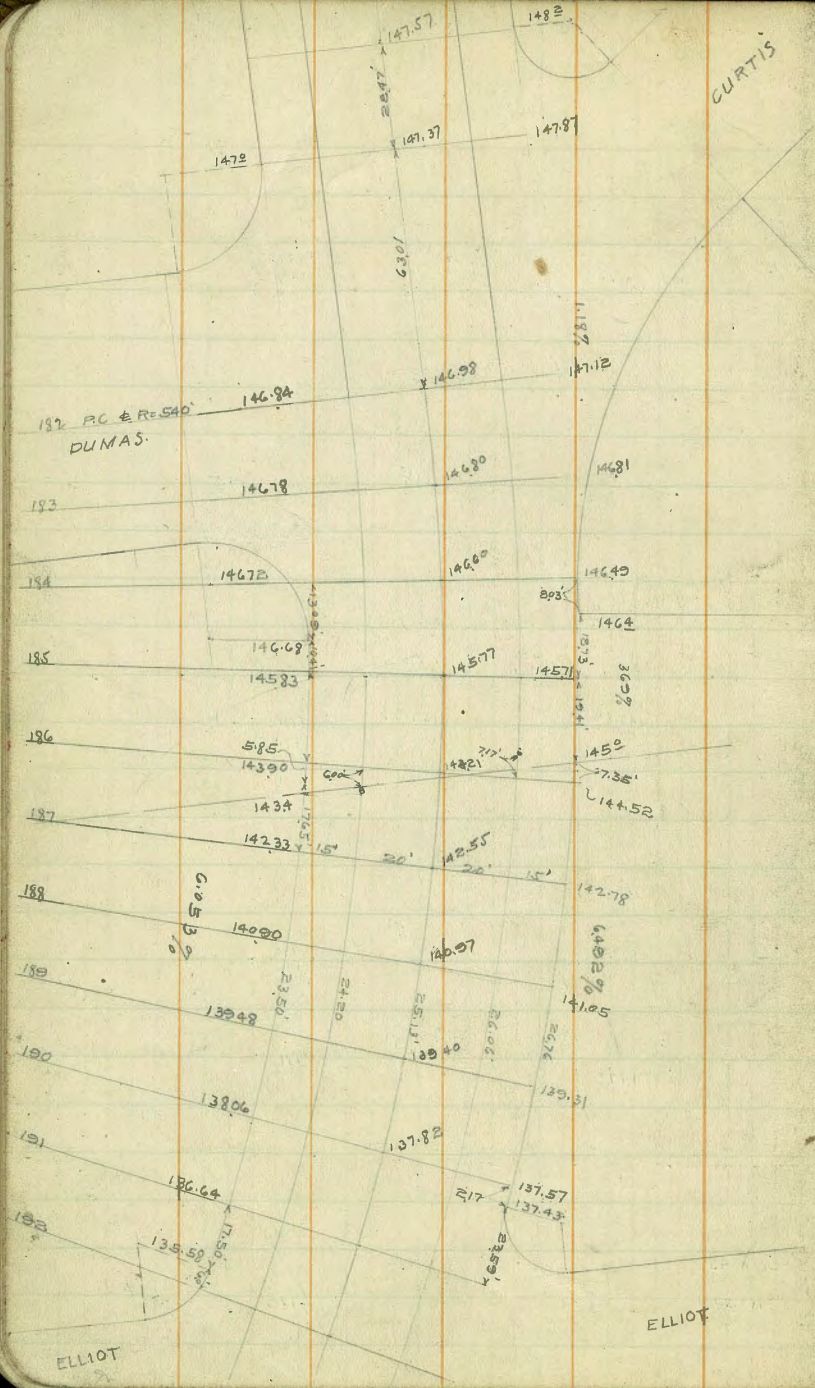
DUMAS

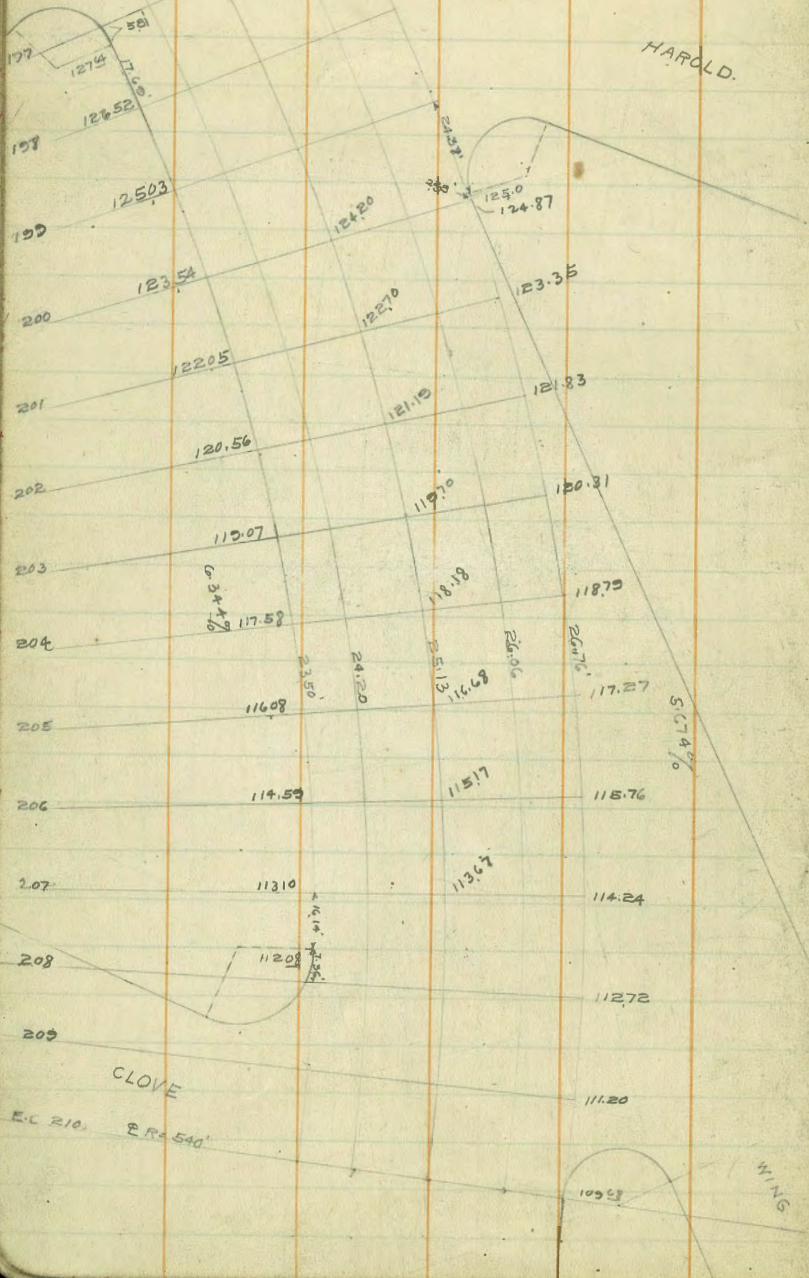
ER=540'

182

CURTIS







$A = 74^{\circ} 40'$   
 $e = 540'$   
 $LC = 675.22$      $M = 114.73'$   
 $C \text{ for } 37^{\circ} 20' = 353.48'$      $M = 29.46'$

50.5	23.50'
520'	24.20'
$R = 540'$	$C = 25.13'$
560'	26.06'
575'	26.76'

1	20
2	40
4	00
5	20
6	40
8	00
9	20
10	40
12	00
13	20
14	40
16	00
17	20
18	40
20	00
21	20
22	40
24	00
25	20
26	40
28	00
29	20
30	40
32	00
33	20
34	40
36	00
37	20

dl =

60.77'				
28.47'	180	147.57		
63.01	181	147.14	147.37	147.15
24.20'	182 PC	146.75	146.98	147.00
24.20'	183	146.45	146.80	146.95
24.20'	184	145.85	146.20	146.35
24.20'	184	145.05	145.40	145.55
24.20'	186	143.85	144.20	144.35
24.20'	187	142.57	142.92	143.07
24.20'	188	141.29	141.64	141.79
24.20'	189	140.01	140.36	140.51
24.20'	190	138.73	139.08	139.23
24.20'	191	137.45	137.80	137.95
24.20'	192	135.90	136.25	136.40
24.20'	193	134.36	134.71	134.86
24.20'	194	132.81	133.16	133.31
24.20'	195	131.27	131.62	131.77
24.20'	196	129.73	130.08	130.23
24.20'	197	128.18	128.53	128.68
24.20'	198	126.64	126.99	127.14
24.20'	199	125.09	125.44	125.59
24.20'	200	123.55	123.90	124.05
24.20'	201	122.10	122.45	122.60
24.20'	202	120.66	121.01	121.16
24.20'	203	119.21	119.56	119.71
24.20'	204	117.77	118.12	118.27
24.20'	205	116.33	116.68	116.83

BM 148.86  
+2.68  
151.54 x

17

E 183 W	E 184 W	E 185 W	E 189 W	E 190 W	E 191 W	E 192 W	E 193 W
146.45	146.95	145.85	146.35	145.05	145.55		
5.09	4.59	5.09	5.19	6.49	5.99		
5.85	4.62	6.79	5.61	7.51	6.41		
-0.76	-0.03	-1.10	-0.42	-1.02	-0.42		
149.55	144.35	142.57	143.07	141.29	141.79	140.01	140.51
7.76	7.26	9.04	8.54	10.32	9.82	11.60	11.10
8.63	7.56	9.74	8.83	11.04	10.18	12.41	11.46
-0.87	-0.30	-0.70	-0.29	-0.72	-0.36	-0.81	-0.36
138.76							
+0.34							
139.10							
-12.89							
126.21							
1.37							
127.58							
-13.00							
114.58							
+0.05							
114.63							
138.73	139.23	137.95	137.95	135.99	136.40	134.36	134.86
0.37	+0.13	1.65	1.15	3.20	2.70	4.74	4.24
1.28	0.35	2.68	0.39	4.24	2.10	4.97	3.96
-0.91	-0.48	-1.03	+0.76	-1.04	+0.60	-0.23	+0.28
132.81	133.31	131.27	131.77	129.73	130.23	128.19	128.68
6.29	5.79	7.83	7.33	9.37	8.87	10.92	10.42
6.60	6.95	8.55	7.04	10.24	12.31	11.45	13.20
-0.31	-1.16	-0.72	+0.29	-0.87	-3.44	-0.53	-2.78
126.64	127.14	125.09	125.59	123.65	124.05	122.10	122.60
0.94	0.44	2.49	1.99	4.03	3.53	5.48	4.98
1.42	0.25	3.06	4.66	4.37	5.43	5.78	6.74
-0.48	+0.19	-0.51	-2.67	-0.34	-1.90	-0.30	-1.76
120.66	121.16	119.21	119.71	117.77	118.27	116.33	116.83
6.92	6.42	8.37	7.87	9.81	9.31	11.25	10.75
7.26	8.08	8.71	9.05	10.17	9.79	11.62	10.92
-0.34	-1.66	-0.34	-1.18	-0.36	-0.48	-0.37	-0.17
114.88	115.38	113.44	113.94	111.99	112.49	110.67	110.92
12.70	12.20	11.19	0.69	2.64	2.14	3.96	3.71
13.05	12.26	11.52	0.79	2.66	2.74	3.22	4.45
-0.35	-0.06	-0.33	-0.10	-0.02	-0.60	+0.44	-0.74

24.20'					
24.20'	206	114.88	115.23	115.38	
24.20'	207	113.44	113.79	113.94	
24.20'	208	111.99	112.34	112.49	
24.20'	209	110.67	110.90	110.92	
24.38'	210 PC.		110.10		
24.38'	211	109.88	109.38	109.08	
24.38'	212	108.96	108.66	108.16	
24.38'	213	108.24	107.94	107.44	
24.38'	214	107.53	107.23	106.73	
24.38'	215	106.81	106.51	106.01	
PC. 57.10'	216	105.90	105.80	105.50	
51.48'	217		103.30		
51.47'	218		100.85		
51.47'	219		98.40		
51.47'	220		95.90		
50.63'	221		93.90	0	
50.62'	222		92.41		
50.62'	223		90.93		
50'	224		89.45		
50'	225		88.93		
50'	226		87.16		
50'	227		85.76	85.70 0	
50.63'	228		84.90		
50.62'	229		84.46		
50.62'	230		83.66		
50.62'	231		82.86		

108.78 = Sta 6  
 4387  
 11865 X  
 -12.85  
 99.80  
 +0.55  
 100.35 X  
 -12.81  
 87.54  
 0.77  
 88.31 X  
 -9.43  
 78.88  
 +2.49  
 81.37 X  
 7.44  
 73.93 = B.M.  
 James:

110.67	209	110.92			
1.98		1.73			
1.26		2.49			
+0.72		-0.76			
+0.72		-0.74			
E 210 W		E 211 W	E 212 W	E 213 W	
110.00	112.00	109.48	109.08	109.96	108.24
2.65	2.65	3.17	3.57	3.69	4.41
2.39	3.44	3.01	4.12	4.2	4.77
-10.35	-0.73	4.016	-0.55	-0.52	-0.28
E 214 W	E 215 W	E 216 W	E 217 W		
107.73	106.73	106.81	105.90	103.20	103.20
5.13	5.92	5.94	6.44	6.75	7.15
5.22	6.07	6.03	6.75	6.92	7.40
-0.10	-0.15	-0.10	-0.11	-0.07	-0.25
E 218 W	E 219 W	E 220 W	E 221 W		
100.75	100.75	98.30	95.80	93.80	93.80
11.50	11.90	28.5	20.5	4.58	4.58
12.34	12.19	25.4	24.7	5.07	4.95
-0.44	-0.29	-0.42	-0.42	-0.52	-0.40
E 222 W	E 223 W	E 224 W	E 225 W		
22.31	22.31	20.83	22.55	22.35	22.55
8.24	8.04	9.52	9.52	11.00	11.82
8.02	8.54	9.70	10.06	11.40	11.52
-10.02	-0.50	-0.18	-0.54	-0.40	-0.52
E 226 W	E 227 W	E 228 W	E 229 W		
27.05	27.06	25.66	25.66	24.90	24.90
1.25	1.25	2.65	2.65	3.51	3.51
1.75	1.75	3.12	3.12	4.35	4.41
-0.50	-0.54	-0.47	-0.54	-0.34	-0.30
E 230 W	E 231 W	E 232 W	E 233		
23.56	23.56	22.76	22.76	21.96	21.14
4.75	4.75	5.55	5.55	6.35	6.35
5.16	5.64	6.08	6.48	7.27	7.31
-0.41	-0.29	-0.53	-0.53	-0.92	-0.92
E 234 W					
20.37	20.37				
7.99	7.99				
8.67	8.96				
-0.68	-0.97				

85.288  
 1.58%



15' 20' 20' 15' 212 PATH

51.43  
51.47  
51.47  
51.47  
47.65  
50.63  
50.62  
50.62  
50.62  
50.62

212

220

221

88.38'  
88.32'

222

223

224

225

GOLDSMITH.

20' 50' 50' 50' 27.80' 50.63' 50.62' 48.62' 48.62'

225

226

227

88.38'

228

229

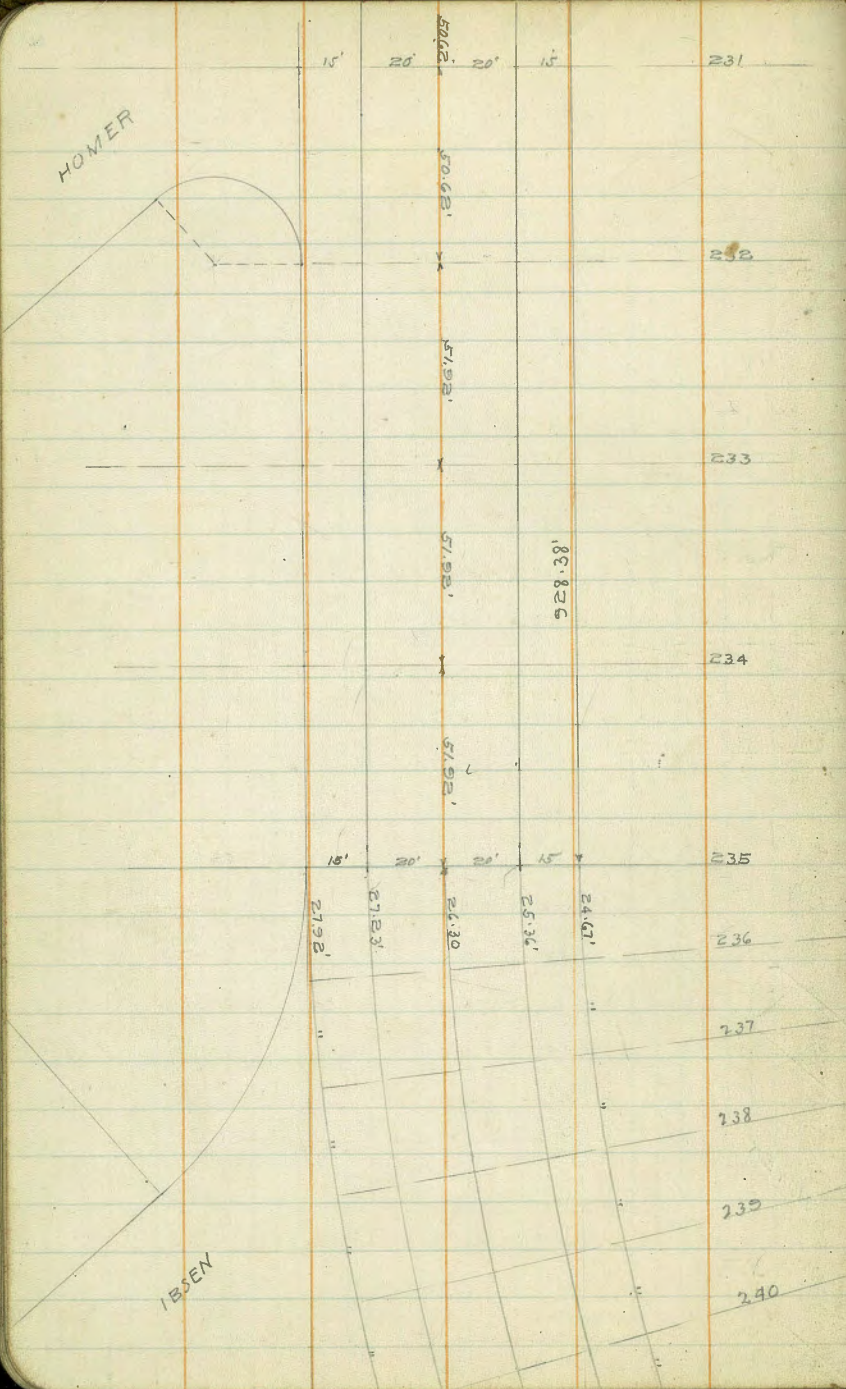
230

231

232

HOMER

HOMER



- 1° 20" ✓
- 2 40 ✓
- 4 00 ✓
- 5 20 ✓
- 6 40 ✓
- 8 00 ✓
- 9 20 ✓
- 10 40 ✓
- 12 00 ✓
- 13 20 ✓
- 14 40 ✓
- 16 00 ✓
- 17 20 ✓
- 18 40 ✓
- 20 00 ✓
- 21 20 ✓
- 22 40 ✓
- 24 00 ✓
- 25 20 ✓
- 26 40 ✓
- 28 00 ✓

21 chords:

P.C.  $\frac{1}{2}$  R = 565' A = 56°

C  $\begin{cases} 530' = 24.67' \\ 565' = 26.30' \\ 600 = 27.92' \end{cases}$

L = 545.28'  
M = 68.47'

BM 73.03  
 + 6.25  
 80.18 X  
 - 8.20  
 71.98  
 + 0.32  
 72.30 X

E 234 W  
 80.32 80.32  
 0.14 -0.14  
 0.56 -0.56  
 -0.70 -0.57  
 0.68 -0.57

E 235 W  
 79.93 79.93  
 0.25 -0.25  
 0.25 1.31  
 -0.67 -1.02

E 236 W  
 79.31 78.81  
 0.18 1.37  
 1.50 2.21  
 -0.63 -0.84

E 237 W  
 78.87 78.37  
 1.31 1.81  
 1.46 2.65  
 -0.15 -0.84

E 238 W  
 78.42 77.92  
 1.76 2.26  
 1.50 3.17  
 +0.26 -0.91

E 239 W  
 77.98 77.48  
 2.20 2.70  
 1.50 3.59  
 +0.30 -0.85

E 240 W  
 77.54 77.04  
 2.64 3.14  
 2.78 4.07  
 -0.14 -0.93

E 241 W  
 77.09 76.59  
 3.09 3.59  
 3.86 4.48  
 -0.77 -0.85

E 242 W  
 76.65 76.15  
 3.53 4.03  
 4.41 5.36  
 -0.88 -0.89

E 243 W  
 75.67 75.17  
 4.01 4.51  
 4.20 5.36  
 -0.92 -0.85

E 244 W  
 75.70 75.20  
 4.48 4.98  
 5.44 5.79  
 -0.96 -0.81

E 245 W  
 75.22 74.72  
 4.96 5.46  
 5.07 6.18  
 -1.01 -0.78

E 246 W  
 74.74 74.24  
 5.44 5.94  
 6.40 7.04  
 -1.02 -0.65

E 247 W  
 73.76 73.26  
 5.92 6.42  
 6.95 7.04  
 -1.07 -0.62

E 248 W  
 73.78 73.28  
 6.40 6.90  
 6.75 7.45  
 -0.95 -0.55

E 249 W  
 72.31 71.81  
 6.87 7.37  
 6.94 7.88  
 -0.07 -0.51

E 250 W  
 72.23 71.73  
 7.35 7.85  
 8.09 8.27  
 -0.74 -0.42

E 251 W  
 72.35 71.85  
 7.85 8.33  
 9.15 8.65  
 -1.32 -0.32

E 252 W  
 72.05 71.55  
 8.13 8.63  
 9.36 9.02  
 -1.23 -0.59

E 253 W  
 71.75 71.25  
 8.55 9.05  
 1.72 1.72  
 -1.24 -0.41

E 254 W  
 71.45 70.95  
 8.85 9.35  
 2.08 1.72  
 -1.23 -0.37

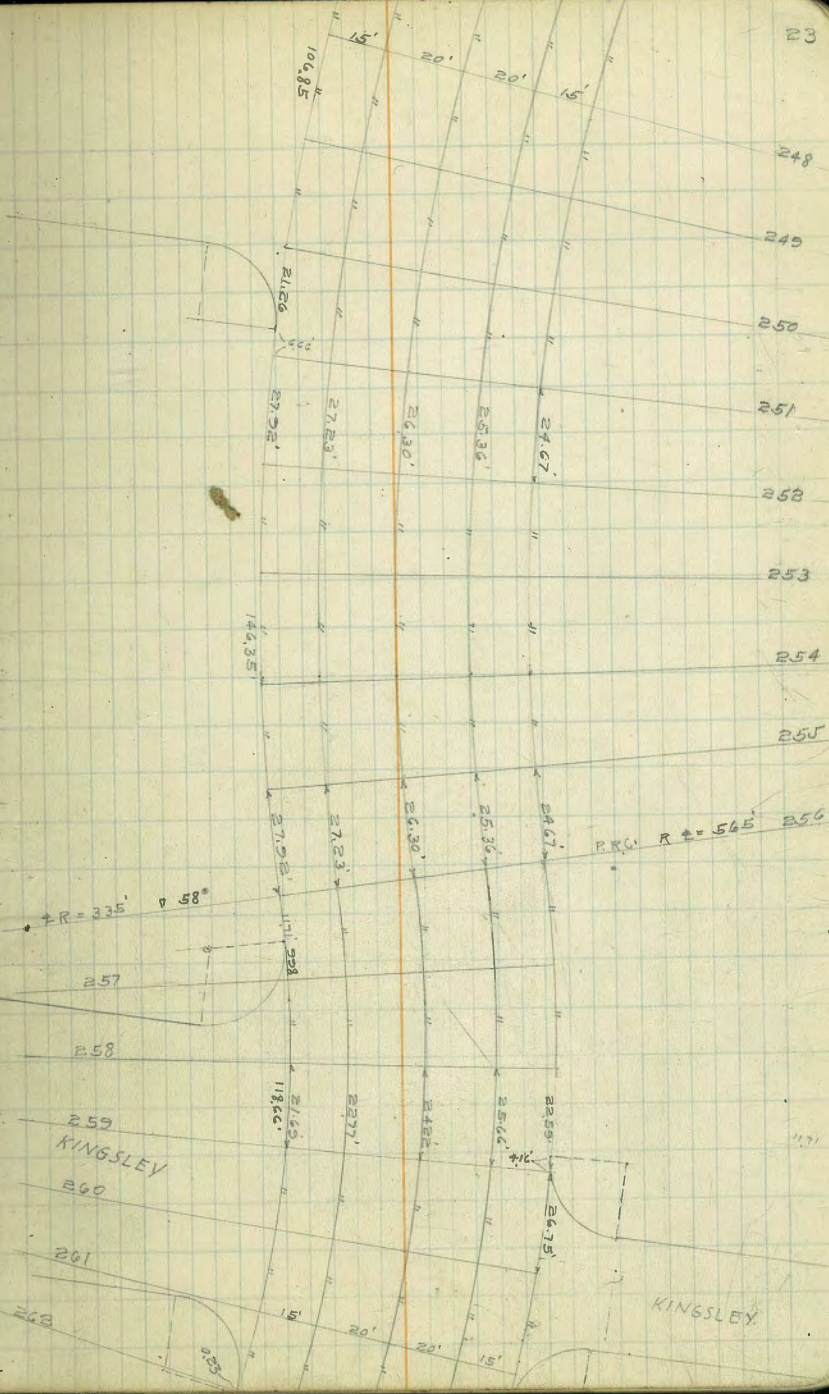
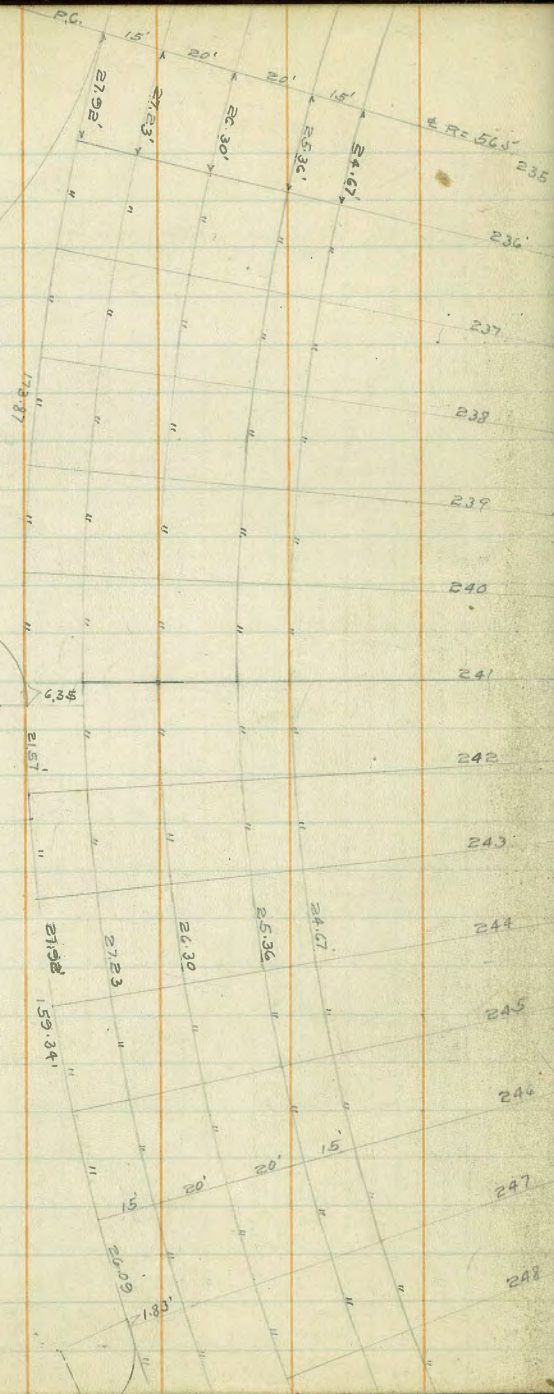
E 255 W  
 71.03 70.53  
 9.17 9.67  
 2.45 2.03  
 -1.18 -0.50

E 256 W  
 70.60 70.10  
 9.70 1.70  
 2.74 2.27  
 -1.04 -0.57

50.62'			82.06		
57.92'	232		81.24	79.82	25.36'
57.92'	233		80.42	79.38	25.36'
51.92'	234	79.98	80.03	79.82	25.36'
P.C.	235	79.63	79.60	79.38	25.36'
27.23'	236	79.31	79.16	78.81	25.36'
27.23'	237	78.87	78.72	78.37	25.36'
27.23'	238	78.42	78.27	77.92	25.36'
27.23'	239	77.98	77.83	77.48	25.36'
27.23'	240	77.54	77.39	77.04	25.36'
27.23'	241	77.09	76.94	76.59	25.36'
27.23'	242	76.65	76.50	76.15	25.36'
27.23'	243	76.17	76.02	75.67	25.36'
27.23'	244	75.70	75.55	75.20	25.36'
27.23'	245	75.22	75.07	74.72	25.36'
27.23'	246	74.74	74.59	74.24	25.36'
27.23'	247	74.26	74.11	73.76	25.36'
27.23'	248	73.78	73.63	73.28	25.36'
27.23'	249	73.31	73.16	72.81	25.36'
27.23'	250	72.83	72.68	72.33	25.36'
27.23'	251	72.35	72.20	71.85	25.36'
27.23'	252	71.85	71.90	71.55	25.36'
27.23'	253	71.45	71.60	71.25	25.36'
27.23'	254	71.15	71.30	70.95	25.36'
27.23'	255	71.03	71.00	70.77	25.36'
P.R.C.	256		70.70	70.50	25.36'
27.23'	257	70.10	70.40	70.50	25.36'



IBSEN.



$P R = 144.03'$   
 $S R = 129.03'$   
 $\Delta = 47^\circ$   
 $c = 19.08'$   
 $C = 17.63'$   
 $\pm R = 102.03'$   
 $14.90'$

$3^\circ 51'$   
 $7 \quad 50$   
 $11 \quad 45$   
 $d = Gc$   
 $15 \quad 40$   
 $19 \quad 35$   
 $23 \quad 30$

$\Delta = 53^\circ 31' 22''$

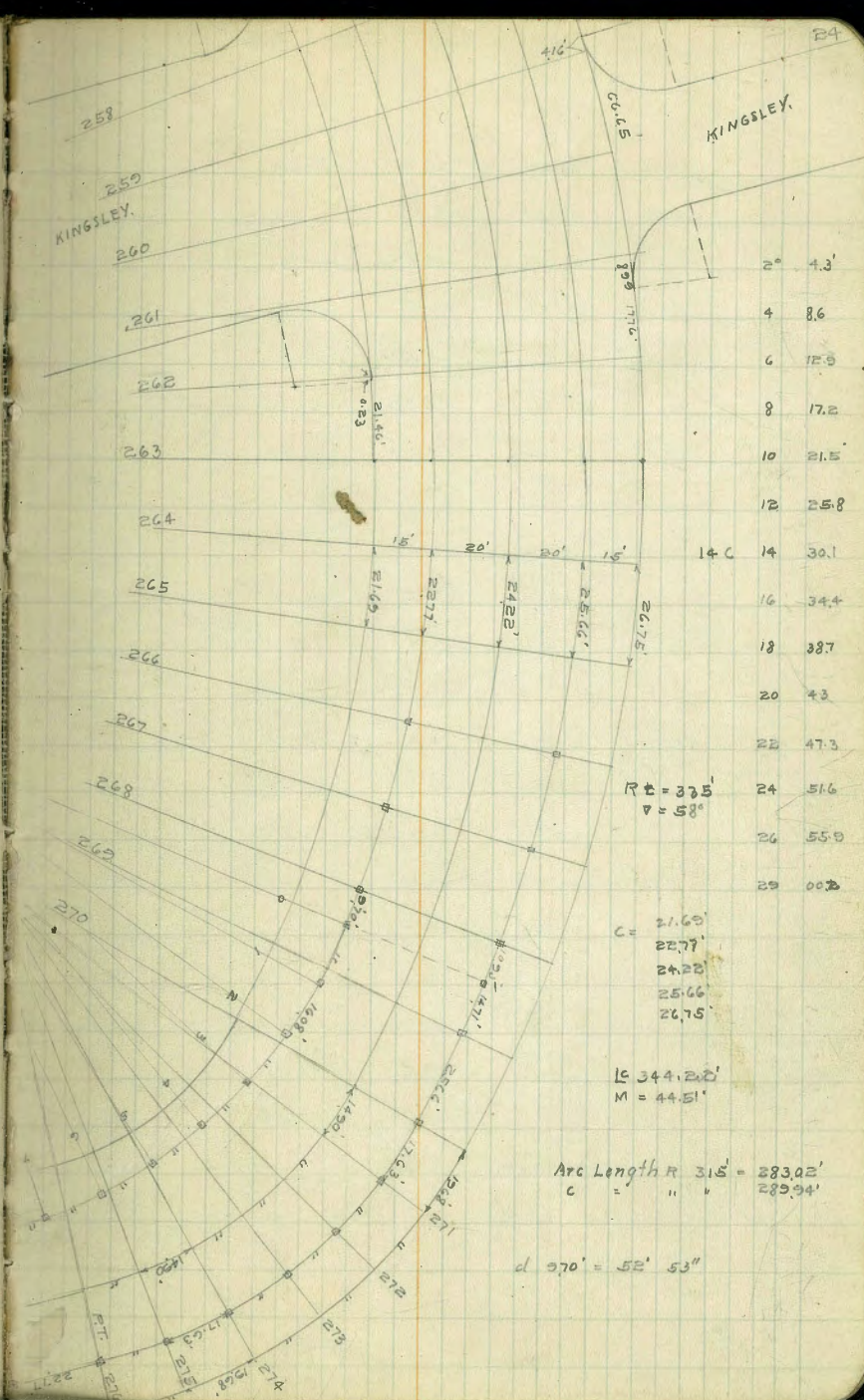
R to paving = 147.70'

R to Stake line = 137.73'

$c \begin{cases} 17.25' \\ 16.08' \end{cases}$

$3^\circ 20' 43'$   
 $6 \quad 41 \quad 25$   
 $10 \quad 02 \quad 09$   
 $d g c = 13 \quad 22 \quad 50$   
 $16 \quad 43 \quad 33$   
 $20 \quad 04 \quad 16$   
 $23 \quad 24 \quad 58$   
 $26 \quad 45 \quad 41$

27 W. L. E. GREEN A  
 ON SOUTH



$R = 325'$   
 $\Delta = 58^\circ$

$C = \begin{cases} 21.60' \\ 22.77' \\ 24.22' \\ 25.66' \\ 26.75' \end{cases}$

$15 344.22'$   
 $M = 44.51'$

Arc Length R 315' = 283.02'  
 C = " " 289.94'

$d 970' = 52' 53''$

72.30π Sec page 22

-10.37  
61.53 = T.P.  
+3.62  
65.55 π

E 257 W	E 258 W	E 259 W	E 260 W
70.10	70.50	69.60	70.40
2.20	1.80	2.70	1.90
2.93	2.49	2.53	2.62
-0.73	-0.69	+0.07	-0.72
+0.32	-0.62	+0.94	-0.44

E 261 W	E 262 W	E 263 W	E 264 W
68.51	69.31	68.02	68.22
3.79	2.99	4.28	3.48
4.35	3.55	5.10	4.00
-0.56	-0.56	-0.82	-0.52
-0.88	-0.56	-0.56	-0.50

E 265 W	E 266 W	E 267 W	E 268 W
66.55	67.35	66.06	66.26
5.75	4.95	6.24	5.44
6.63	5.47	7.17	5.99
-0.88	-0.52	-0.93	-0.55
-0.98	-0.98	-0.55	-0.96

269 W	270 W	271 W	272 W
65.59	65.20	65.02	64.73
6.71	7.10	7.28	7.57
7.39	7.88	8.30	8.70
-0.68	-0.78	-1.02	-1.13

273 W	274 W	275 W	276 W
64.45	64.17	63.82	63.42
7.85	8.13	8.42	8.82
9.17	9.54	10.01	10.40
-1.32	-1.41	-1.59	-1.52

0E	1E	2E	3E	4E	5E	6E	7E	8E
64.73	64.36	63.90	63.41	63.01	62.62	62.25	62.11	62.05
7.57	7.94	8.40	8.89	9.29	9.68	10.05	10.18	10.25
8.55	9.00	9.35	9.57	9.77	9.95	10.23	10.52	10.71
-0.98	-1.06	+0.65	+0.32	+0.52	+0.73	+0.82	+0.67	-0.46

E 277 W	E 278 W	E 279 W
62.05	62.72	61.87
3.50	2.77	3.68
3.96	4.02	4.53
-0.46	-1.25	-0.85
-0.88	-0.28	-0.70

- 0 = 64.73
- 1 = 64.36
- 2 = 63.90
- 3 = 63.41
- 4 = 63.01
- 5 = 62.62
- 6 = 62.25
- 7 = 62.11
- 8 = 62.05 = Sta. 277

2277	258	69.60	70.10	70.40	25.66'
2277	259	69.30	69.80	70.10	25.66'
2277	260	69.00	69.50	69.80	25.66'
2277	261	68.51	69.01	69.31	25.66'
2277	262	68.02	68.52	68.82	25.66'
2277	263	67.53	68.03	68.33	25.66'
2277	264	67.04	67.54	67.84	25.66'
2277	265	66.55	67.05	67.35	25.66'
2277	266	66.06	66.56	66.86	25.66'
2277	267	65.57	66.07	66.37	25.66'
2277	268	64.98	65.58	65.98	25.66'
PC. on E	269	64.39	65.09	65.59	25.66'
PC. on W	270	63.80	64.60	65.30	17.63'
	271	63.42	64.32	65.02	17.63'
	272	63.13	64.03	64.73	17.63'
	273	62.85	63.75	64.45	17.63'
	274	62.57	63.47	64.17	17.63'
	275	62.29	63.18	63.88	17.63'
PT. on E	276	62.05	62.9	63.42	22.77'
PT. on W	277	62.05	62.52	62.78	32.57'
40	278	61.87	61.97	61.87	40'
	279	W.E. EVERGREEN ON S.	61.30		

2 chains 1 to 8

PT. on E  
PT. on W  
40

278 15' 20' 20' 15'

279 61.30

EVERGREEN

280 60.57

281 59.63

282 58.47

283 57.32

284 56.17

285 55.02

286 53.86

287 15' 20' 20' 15'

LOCUST

LYTTON ST.

61.53 T.P. See page 25

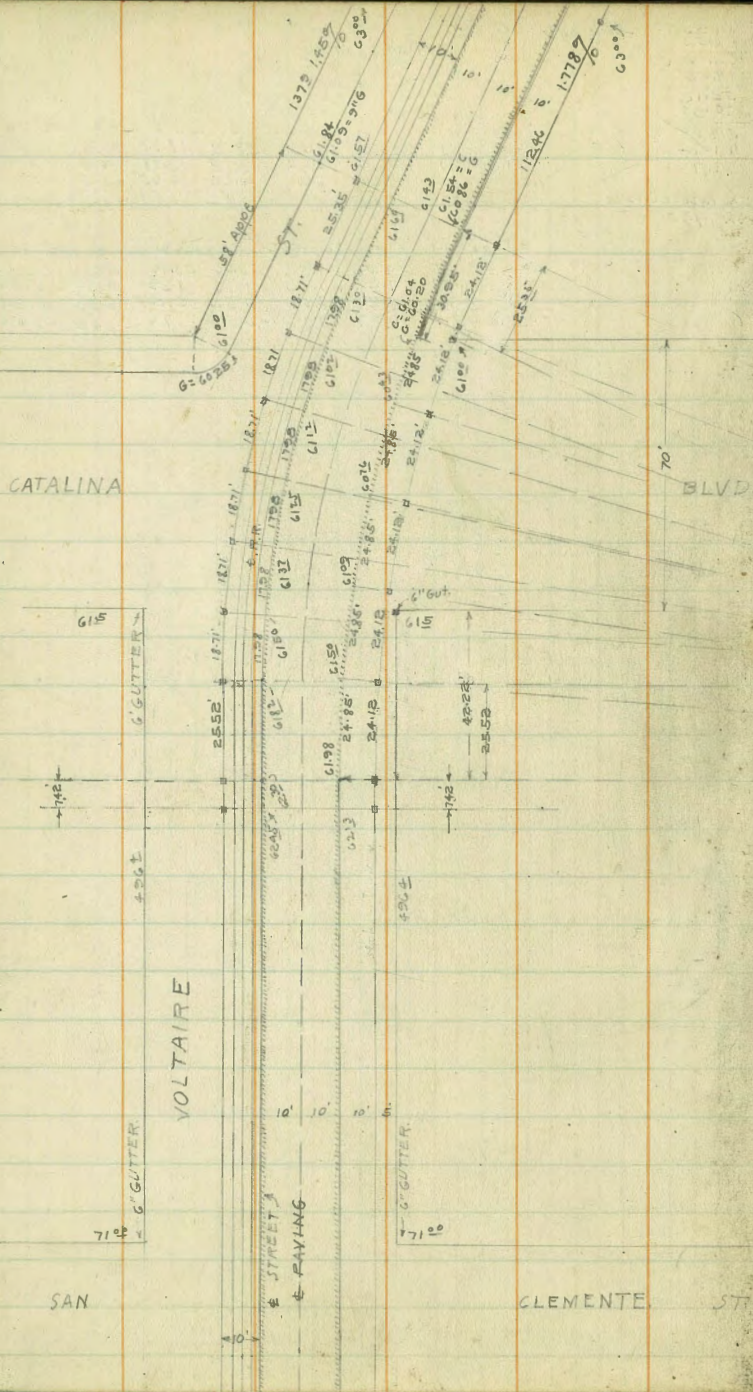
+ 8.22  
62.15 X  
- 1.03  
52.12  
10.58  
53.10 X  
11.34  
41.76 =

West BM Rosecrans Ex  
LYTTON 41.75

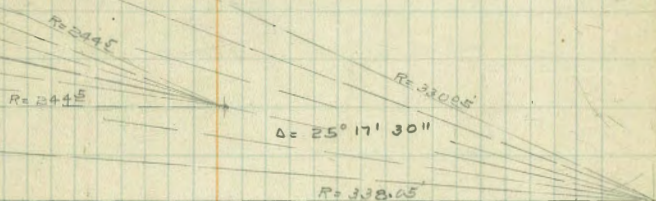
E 279 W  
61.20 61.20  
0.54 0.55  
11.24 11.24  
-0.30 -0.65  
-0.28 -0.70

E 280 W E 281 W E 282 W E 283 W  
60.87 60.87 59.53 59.53 58.37 58.37 57.22 57.22  
1.28 1.28 2.62 2.62 3.78 3.78 4.93 4.93  
1.60 2.07 2.66 2.91 4.60 4.65 5.80 5.79  
-0.32 -0.79 -0.04 -0.29 -0.82 -0.87 -0.87 -0.86

E 284 W E 285 W E 286 W E 287 W  
56.07 56.07 54.22 54.22 53.76 53.76 52.61 52.61  
6.08 6.08 7.23 7.23 8.39 8.39 9.54 9.54  
6.99 6.93 8.20 8.04 9.32 9.15 10.23 10.24  
-0.91 -0.85 -0.97 -0.81 -0.93 -0.76 -0.49 -0.70



$$\begin{aligned} \Delta &= 25^\circ 17' 30'' & L &= 25.58' = 348.45' & 2' 6' 25'' \\ R &= 338.05' & & = 624.85' & 4' 12' 50'' \\ R &= 328.05' = T 73.58' = 624.17' & & & 6' 19' 15'' \\ & & L_c &= 143.52' & 8' 25' 40'' \\ & & & & 10' 32' 5'' \\ & & & & 12' 38' 30'' \end{aligned}$$



$$\begin{aligned} \Delta &= 25^\circ 17' 30'' & L_c &= 111.34' \\ R &= 244.5 & & \text{c 18.71 stake} \\ R &= 254.5 & & \text{c 17.98 PAVING} \\ & & T &= 57.08' \end{aligned}$$

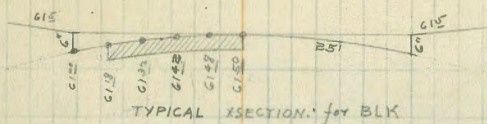
Staco-E.L. of

Catalina Blvd	0 615	61.50	61.18	615
+ 49.64	1	62.45	62.13	
+ 49.28	2	63.40	63.08	
+ 48.92	3	64.35	64.03	
+ 48.56	4	65.30	64.98	
+ 48.20	5	66.25	65.03	
+ 47.84	6	67.20	66.88	
+ 47.48	7	68.15	67.83	
+ 47.12	8	69.10	68.78	
+ 46.76	9	70.05	69.73	
+ 46.40 = W.L. SAN CLEMENTE BLVD	10 7100	71.00	70.68	7100
		71.50	71.18	

10 EQUAL STATIONS OF 4966'

S.L. PAYING

M.L. PAYING



72.42 B.M. RR Spk San Cle Monte:

72.42														
+ 10.20														
72.62														
- 10.53														
62.09	Spk Catalina													
+ 11.76														
73.85	S	0	N	S	1	N	E	2	W	S	3	N		
73.85	61.50	61.18	62.45	62.13	63.40	63.08	64.35	64.03						
- 0.35	11.18	11.50	10.23	10.55	9.28	9.60	8.33	8.65						
73.46	10.85	11.62	10.60	11.00	10.67	10.10	9.68	9.40						
+ 7.83	+ 0.33	- 0.12	- 0.37	0.45	- 0.79	- 0.50	+ 1.35	- 0.75						
81.29	S	4	N	S	5	N	S	6	N	S	7	N		
81.29	65.30	64.03	66.25	65.03	67.20	66.88	68.15	67.83						
- 8.32	7.38	7.70	6.43	6.75	5.48	5.80	4.53	4.85						
78.97	8.04	8.73	7.27	6.86	5.36	4.91	3.93	3.50						
79.00	1.56	- 1.03	- 0.84	- 0.11	+ 0.12	+ 0.99	+ 0.60	+ 1.35						
	S	8	N	S	9	N	S	10	N	S	0	N		
	69.10	68.78	70.05	69.73	71.00	70.68	71.50	71.18						
	3.58	3.90	2.63	2.55	1.68	2.00	1.18	1.50						
	2.85	2.40	2.30	1.89	1.71	1.28	1.20	0.82						
	+ 0.73	+ 1.50	+ 0.33	+ 1.06	- 0.03	+ 0.72	- 0.11	+ 0.68						

62.10 Spk above:  
10.58 corrected:  
72.68

4175 BM. ROSECRANS

+11.38  
53.13 πE 287 W  
52.61 52.61  
0.52 0.52  
110.2 110.2  
-0.52 -0.72  
-0.42 -0.70

E 288 W		E 289 W		E 290 W		E 291 W	
51.76	51.76	50.52	50.52	49.36	49.36	47.80	47.80
1.37	1.37	2.81	2.21	3.77	3.77	5.33	5.33
1100	212	240	319	4.54	416.2	6.15	6.18
+0.37	-0.75	-0.19	-0.58	-0.77	-0.85	-0.82	-0.85

E 292 W		E 293 W	
46.24	46.24	44.68	44.68
6.89	6.89	8.45	8.45
7.75	7.71	9.29	11.00
-0.86	-0.82	-0.86	-0.84
		-0.90	-0.77

287

20'

50'  
52.71

20'

50'

51.86

LOCUST

P.

288

50'

289

51.02

50'

290

49.64

Stake Line

50'

291

47.00

LYTTON

50'

292

46.34

Stake Line

50'

293

44.78

50'

294

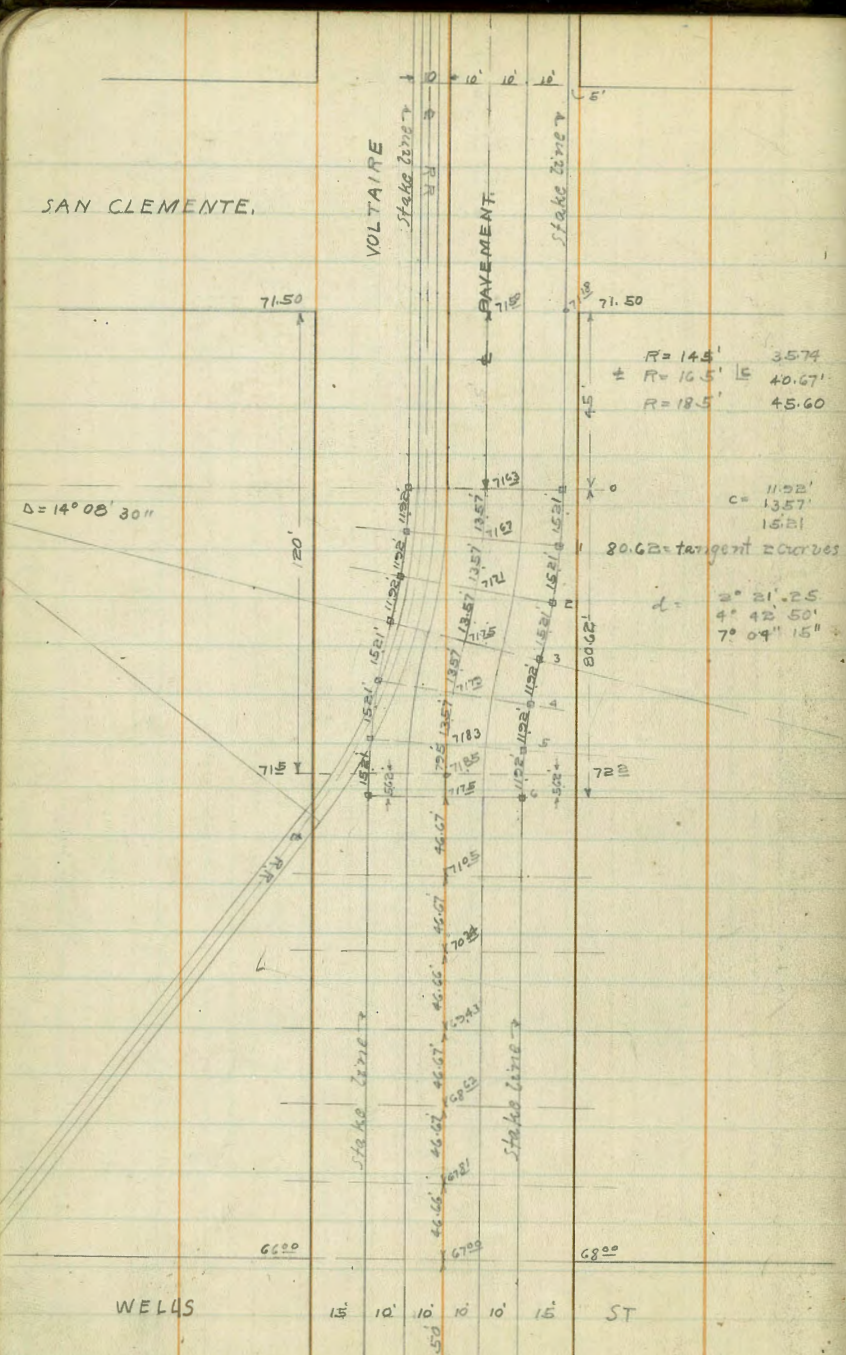
20'

43.13

47'

41.65

SAN CLEMENTE.



$\Delta = 14^\circ 08' 30''$

71.50

71.50

71.5

72.0

66.00

68.00

WELLS

15' 10' 10' 10' 15' ST

VOLTAIRE

PAVEMENT

Stake Corner

Stake Corner

$R = 145'$  35.74  
 $R = 165'$  40.67  
 $R = 185'$  45.60

$c = 11.02'$   
 $c = 13.57'$   
 $c = 15.21'$

80.62 = tangent to curves

$\Delta = 2^\circ 21' 25''$   
 $\Delta = 4^\circ 42' 50''$   
 $\Delta = 7^\circ 04' 15''$

BM 72.42 West's Sph:  
 3.84  
 76.26 X

EX. L. SAN CLEMENTE:

76.26	N	76.26
71.50	N	71.18
4.76	S	5.08
4.86	S	4.38
-0.10	+	+0.70
-0.11	+	+0.68
S	O	N
S	N	S
71.83	71.53	71.57
4.73	4.73	4.69
4.63	4.64	4.56
+0.10	+0.09	+0.13
		-0.35
		+0.20
		-0.59
		+0.17
		-2.86
		+0.10?
S	4	S
76.69		71.73
4.57		4.53
4.55		4.12
+0.02		+0.41
		71.65
		71.65
		4.67
		4.61
		16.08
		11.70
		-1.47
		-7.99

72.42  
 2.30  
 74.72 X

74.72	74.72	74.72	74.72	74.72	74.72	74.72	74.72	74.72	Furnish Stakes
71.65	71.85	71.05	72.24	69.43	68.62	67.81	67.00	67.65	
3.07	2.87	3.67	4.48	5.29	6.10	6.91	7.72	7.72	
4.52									
-1.45									
-1.47									

74.72 X See page 37

71.25  
 66.90  
 7.35

72.21 BM  
 1.90  
 74.31 X

74.31  
 71.65  
 2.66

$\Delta = 14^\circ 08' 30''$

72.42  
 3.84  
 76.26 X

B.M. 72.42  
 +3.90  
 76.32 X

71.65	71.73	71.69	71.65	71.61
4.67	4.59	4.63	4.67	4.71



WORDEN

25' 25' 25' 25' 25' 25' 25' 25' 25' 50'

10' 23.5  
10' 29.4  
24.4  
24.28  
24.25  
23.52  
22.94  
22.2  
20.52  
87°  
10' 23.5  
10'

77.34 TR ELE from Chatsh  
+12.25  
89.59 x  
0.02  
89.57  
+0.40  
89.97 x  
-5.52  
94.45  
+8.66  
103.11 x  
-0.34  
102.77 = BM WORDEN  
+0.34  
103.11 x  
-12.83  
90.28  
+0.48  
90.77 x  
-12.50  
78.27  
+0.22  
78.49 x  
-12.91  
65.58  
+11.39  
76.97 x  
-4.56  
72.41 = BM West Spk  
72.42

Finish:

99.97	99.97	99.97	99.97	99.97	99.97	99.97	31	
20.50	22.36	22.24	23.60	24.25	24.48	24.44		
9.47	7.61	7.03	6.28	5.72	5.49	5.53		
103.11	103.11	stakes						
9.11	9.61							

102.77 BM.  
+0.39  
103.16 x  
-12.59  
90.57  
+6.95  
97.52 x

27.52	27.52	27.52	27.52	27.52	27.52	27.52
23.80	24.11	24.44	24.98	24.25	23.67	22.94
4.02	3.41	3.08	3.04	3.27	3.83	4.58

Reset finish:

27.52	27.52	27.52				
22.36	20.50	21.00				
5.16	7.02	10.52				

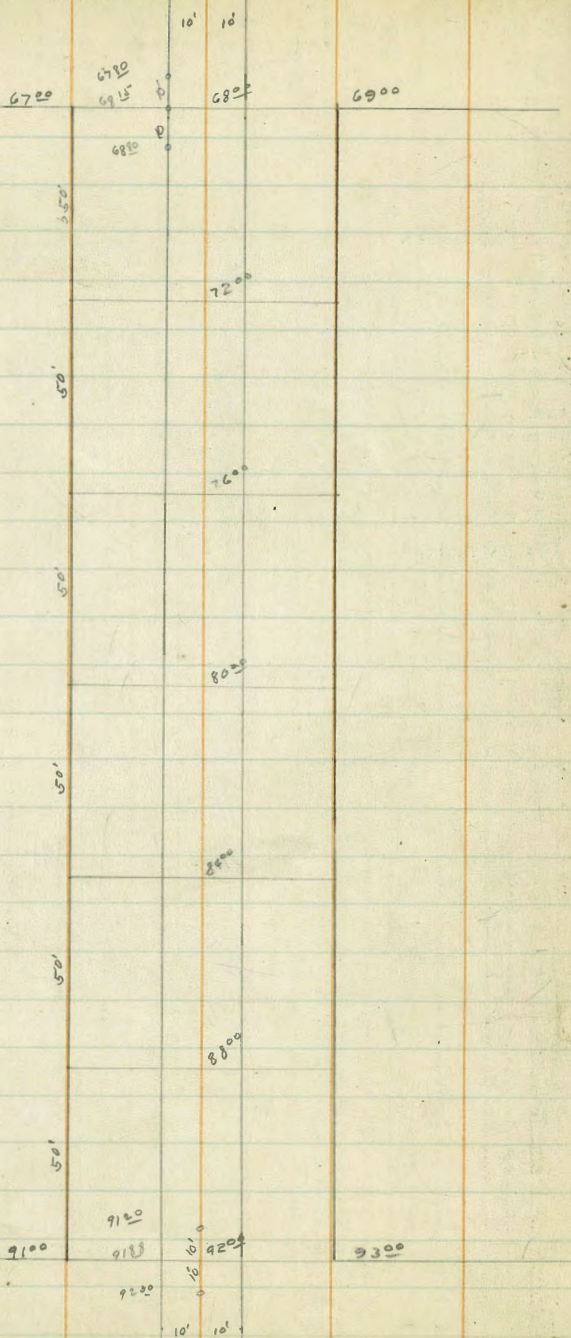
95.40 x see page 46:

95.40	95.40	95.40	95.40	95.40	95.40	95.40
86.90	90.40	92.26	92.84	93.09	94.14	94.28
8.50	5.00	3.14	2.56	1.91	1.26	1.02

95.40	95.40	95.40				
94.24	94.01	93.40				
1.16	1.39	2.00				

WARRINGTON

WELLS



WORDEN

103.11 x See page 31

$\begin{array}{r} 90.77 \\ 78.49 \end{array}$

$\begin{array}{r} 103.11 \\ 22.00 \\ 78.49 \end{array}$

stakes ±

32

93.50 E Worden;

70.00

79.16 x

24.16

92.00

2.16

94.16

88.00

6.16

72.92 BM West

2.30

74.72 x

-6.71 x

68.01

+12.92

80.93 x

-4.3

80.00

+12.45

92.45 x

-2.45

92.00 check on stake 277

74.72

68.00

6.72

80.93

72.00

12.93

80.45

80.00

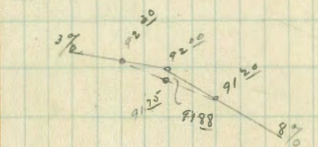
0.45

Reset

92.45

88.00

4.45



92.77

8.59

103.36 x

9.91

93.45

90.25

93.70 x

12.99

80.71

80.26

80.97 x

12.92

68.04

+4.10

72.25 x

92.70

92.10

1.60

93.70

91.78

1.92

93.70

91.10

2.60

92.70

87.40

5.30

92.70

83.90

8.80

90.97

90.90

0.07

80.77

79.90

0.87

80.97

71.70

9.27

80.97

68.70

12.27

80.97

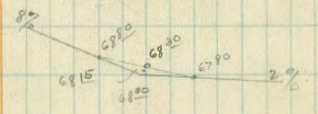
68.00

12.97

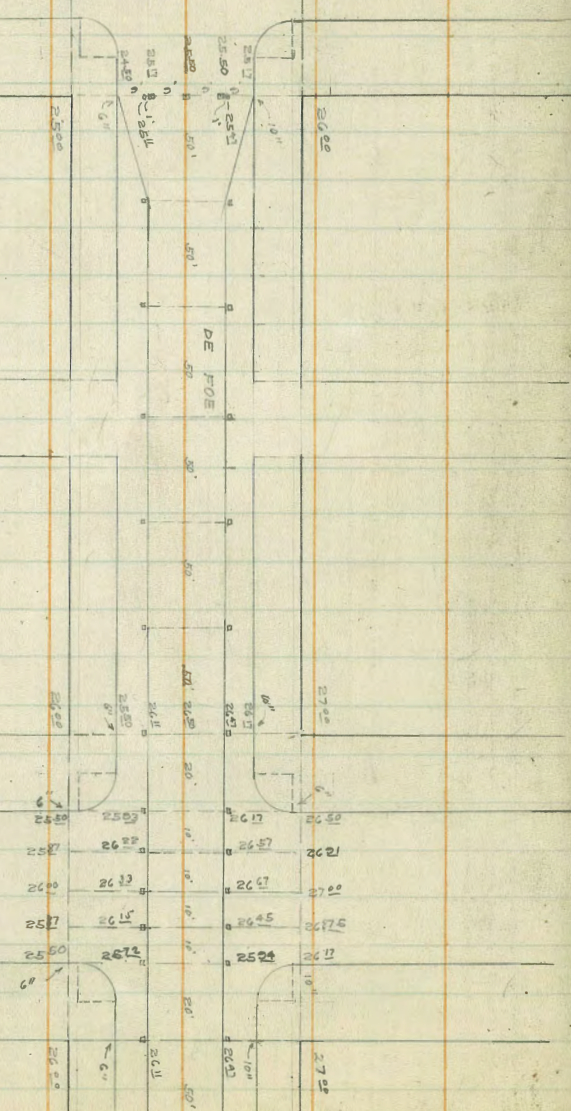
74.25

67.70

6.55



NEWPORT



B.M. 25.04  
 5.48  
 30.52 π

29.52	30.52	30.52	30.52	30.52	30.52	30.52
24.50	25.17	25.50	25.50	25.17	25.47	25.11
6.02	5.35	5.02	5.02	5.35	5.05	5.41

25.92  
 4.96  
 30.95 π

30.95	30.95	30.95	30.95	30.95	30.95	30.95	30.95
26.11	26.47	25.83	26.17	26.23	25.67	26.15	26.45
4.84	4.48	5.12	4.78	4.62	4.28	4.80	4.50

30.95  
 5.23  
 30.95  
 5.01

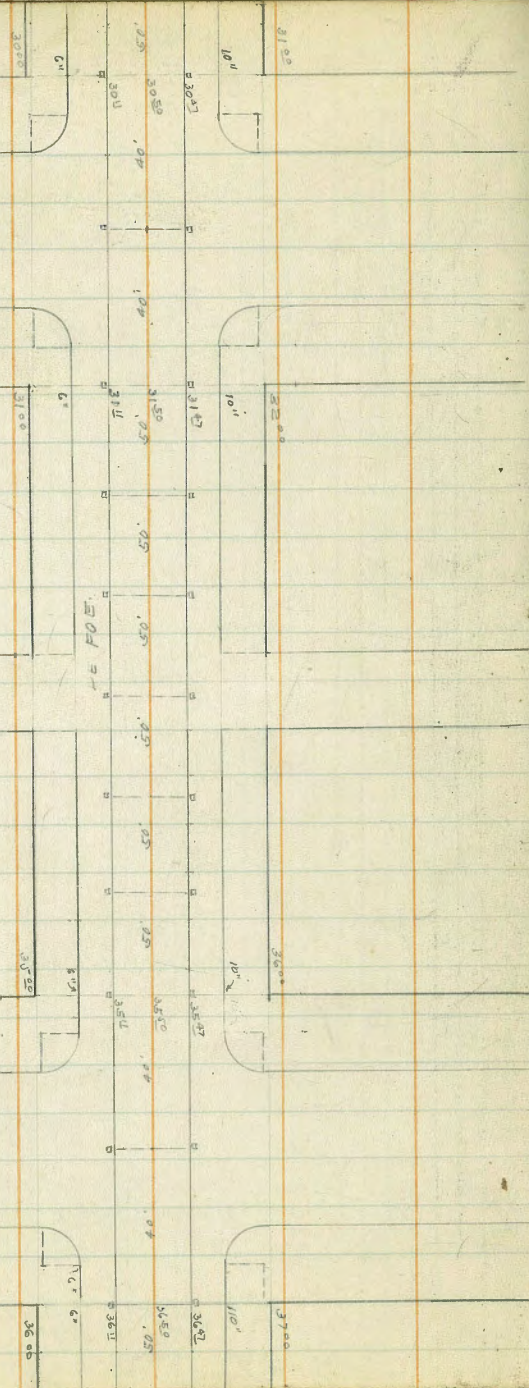
NIAGARA

BM. 12.04  
 3 2 2  
 35.33 X

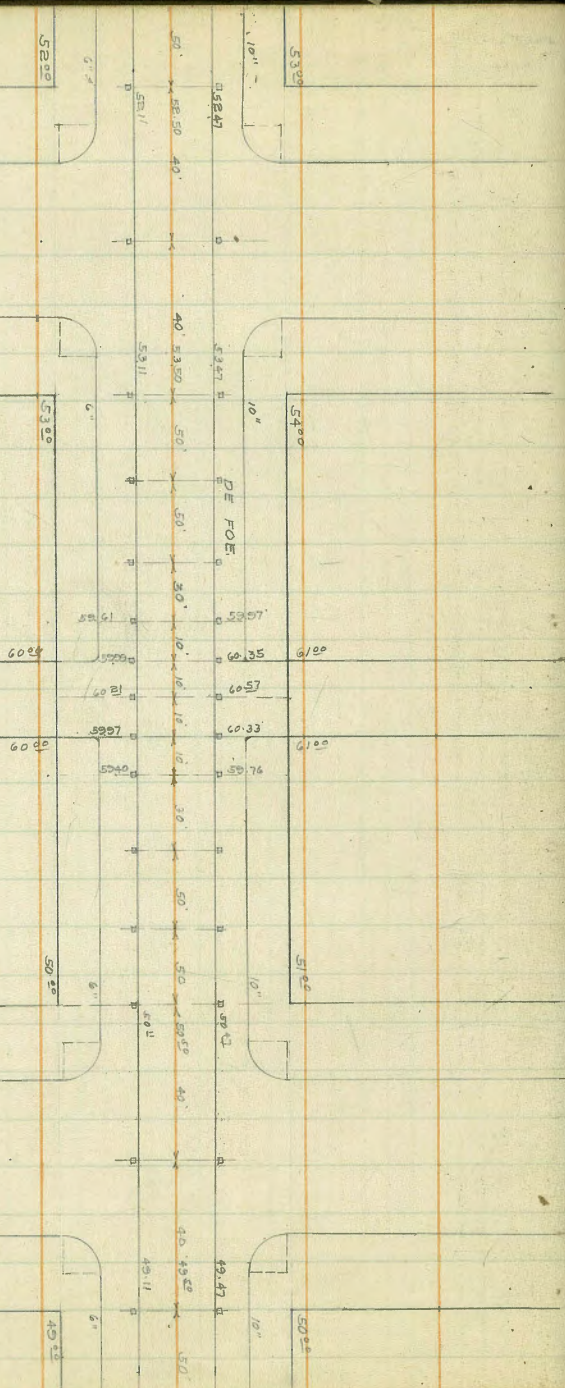
35.33	35.33
30.47	30.11
4.86	5.22
3.86	4.22

NARRAGANSETT

DEL MONTE



SANTA CRUZ



CORONADO

MAT. 54.10  
8.50  
62.69 x

62.69	62.69	62.69	62.69	62.69	62.69	62.69
52.11	62.47	59.97	60.35	60.57	60.33	59.76
10.58	10.22	2.72	2.34	2.12	2.36	2.93
9.52	9.22	3.02	2.70	2.48	2.72	3.29

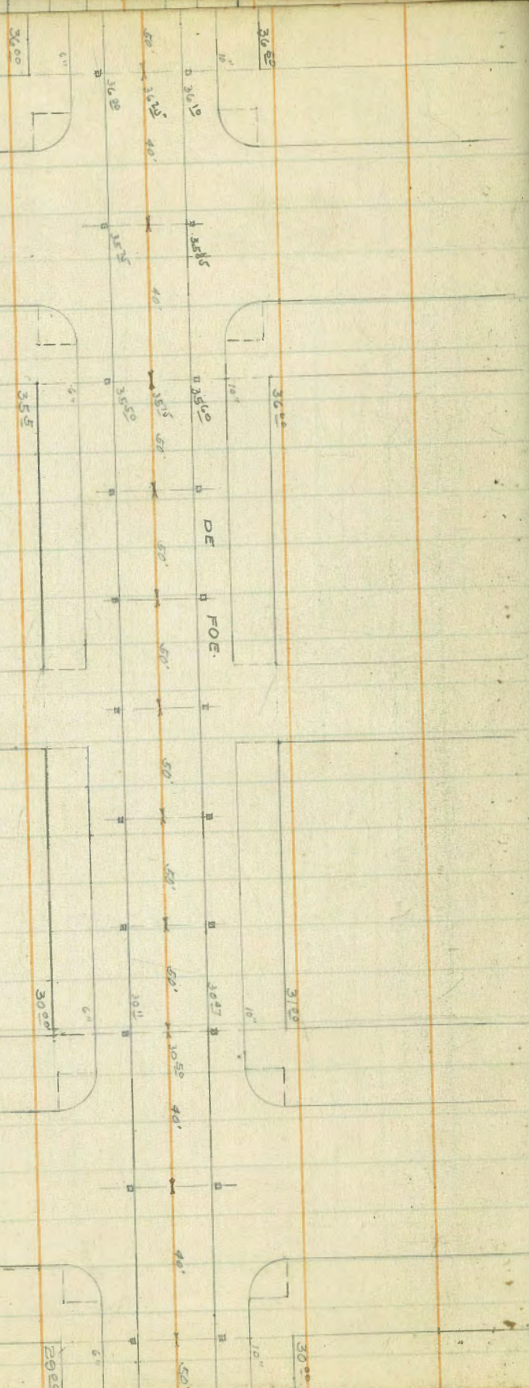
50.00 B.M.  
54.17  
54.17 x

54.17	54.17
52.11	50.47
4.06	3.70
5.06	4.70

DEL MAR.

COR

ORCHARD.



42.00 42.00  
 36.00 36.10  
3.97  
 40.00 X

42.00	42.00
36.00	36.10
4.00	3.95
4.34	4.24
4.80	4.40

33.66	33.66
37.11	37.47
3.55	3.14

15.00 PESCADERO.

4.50  
 30.60 X

33.53	33.53
36.11	36.47
3.4	3.06

33.53 X

PESCADERO



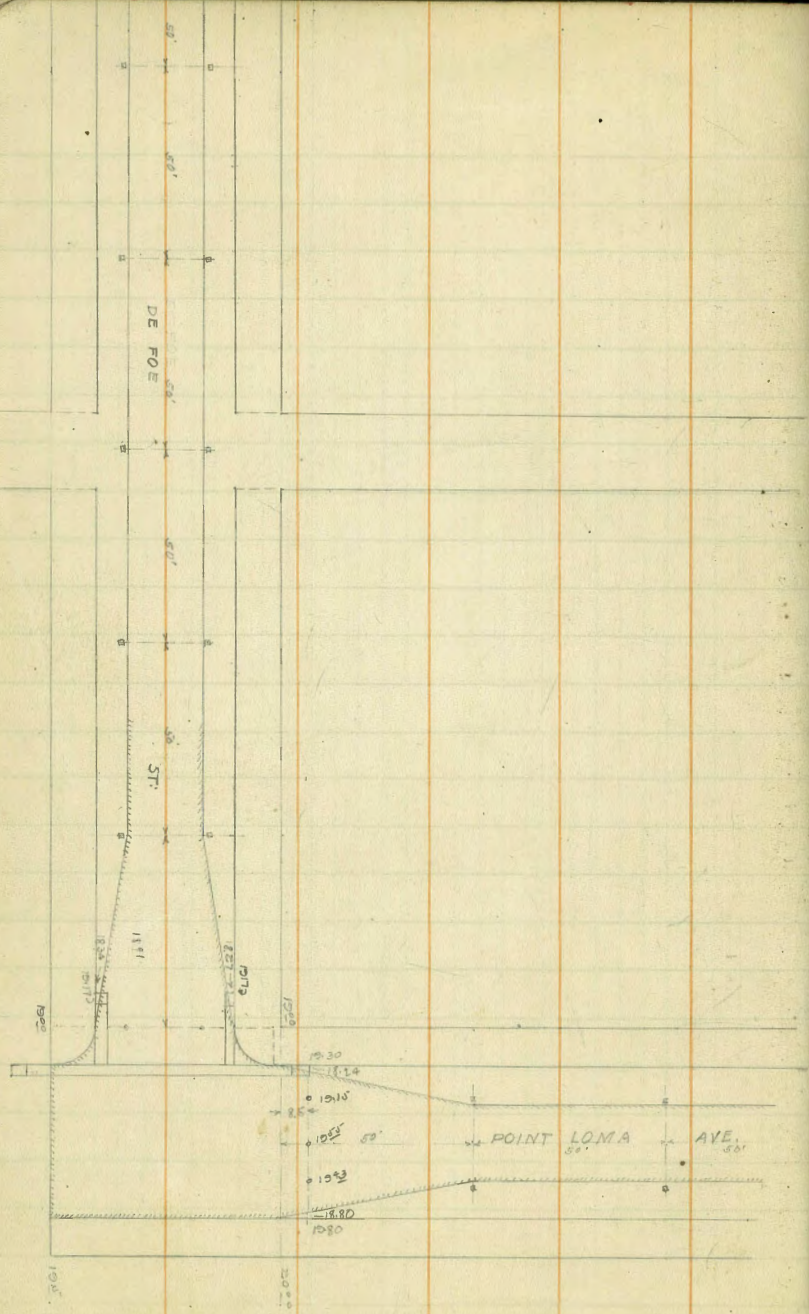
BERMUDA

B.N. 21.11  
 2.90  
 24.01 x

24.01	24.01
10.59	20.81
9.12	34.0
4.14	44.0

33.53	33.53
27.89	27.81
5.04	5.72

38.06  
 54.7  
 33.59 x



21.11  
 0.22  
 21.33

24.56  
 19.15  
 5.41

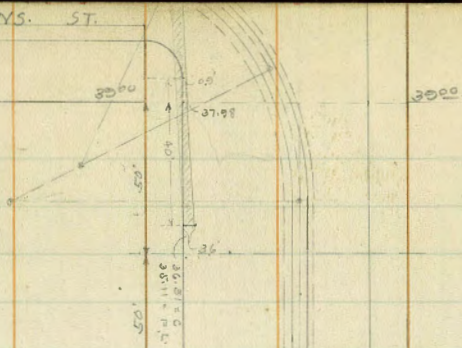
24.56  
 19.93  
 5.13

21.11  
 0.27  
 21.38





ROSECRANS. ST.



30.00

1180  
20°

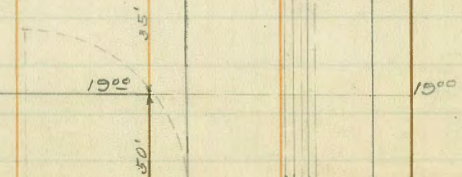
50'  
50'  
50'  
50'  
50'  
50'

21.00

LYTTON

21.00

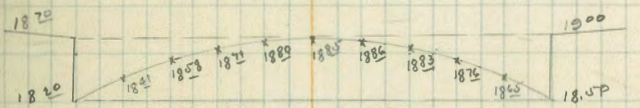
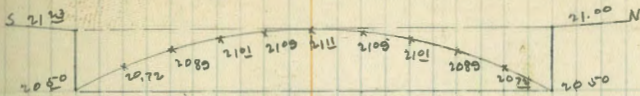
SCOTT ST.



19.00

50'

30.00



SCOTT ST

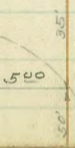


3.5'  
50'  
50'  
50'  
50'  
50'  
50'  
50'  
50'  
50'  
50'

LYTTON



SHAFTER ST

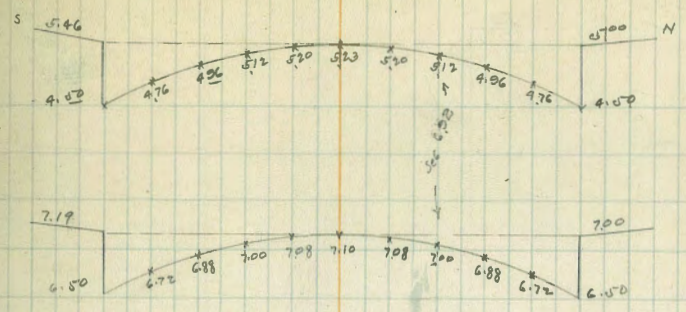


1000

700

500

100' BRACK. 100' PASEL 77



SHAFTER

500

500

Cal. 1844.82

Cal. 1837.38

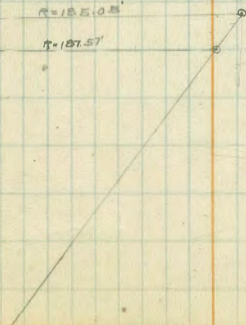
2777.07

170

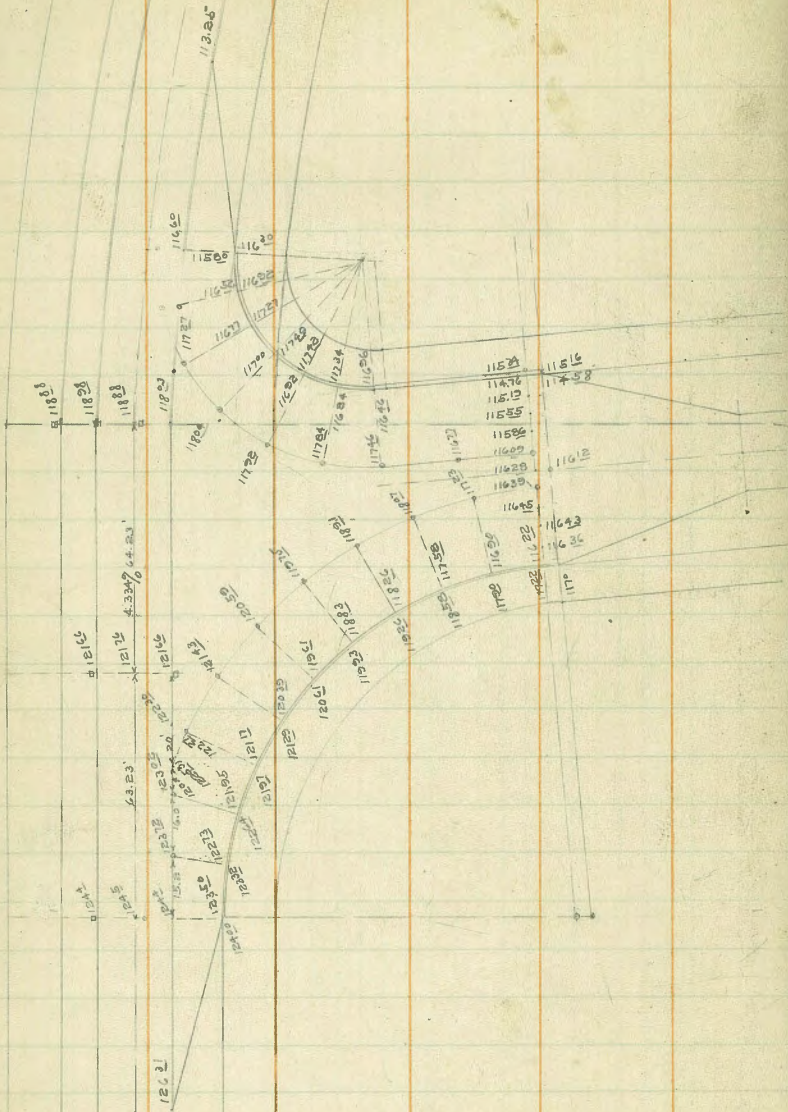
200

r=185.08'

r=187.57'



2 N. 119.90 14.6  
 6.96  
 136.867  
 11.77  
 115.107

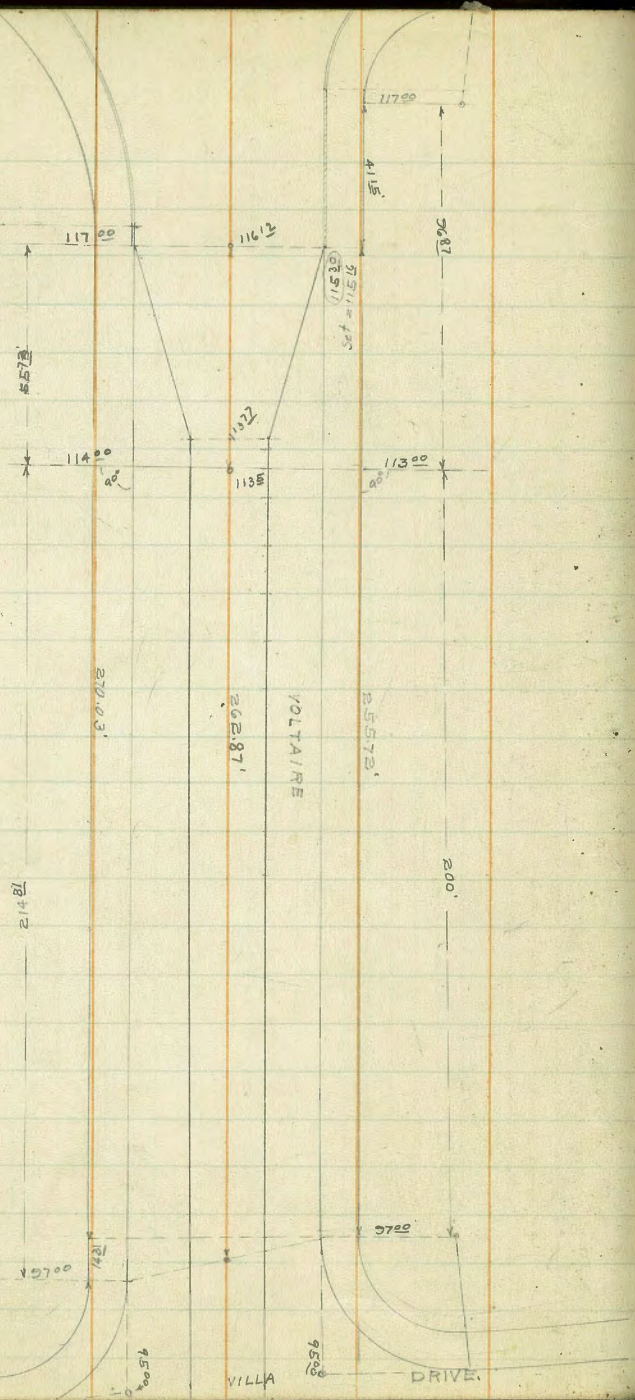


126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86
115.80	16.82	16.77	17.00	16.42	16.84	16.96	12.76	14.58	
11.06	10.34	10.09	9.86	9.94	10.02	10.40	12.10	12.23	

126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86
16.09	16.77	17.46	17.84	17.92	18.04	18.03	17.27	16.60	113.61
10.77	10.09	9.90	9.02	8.94	8.82	8.83	9.57	10.26	13.26

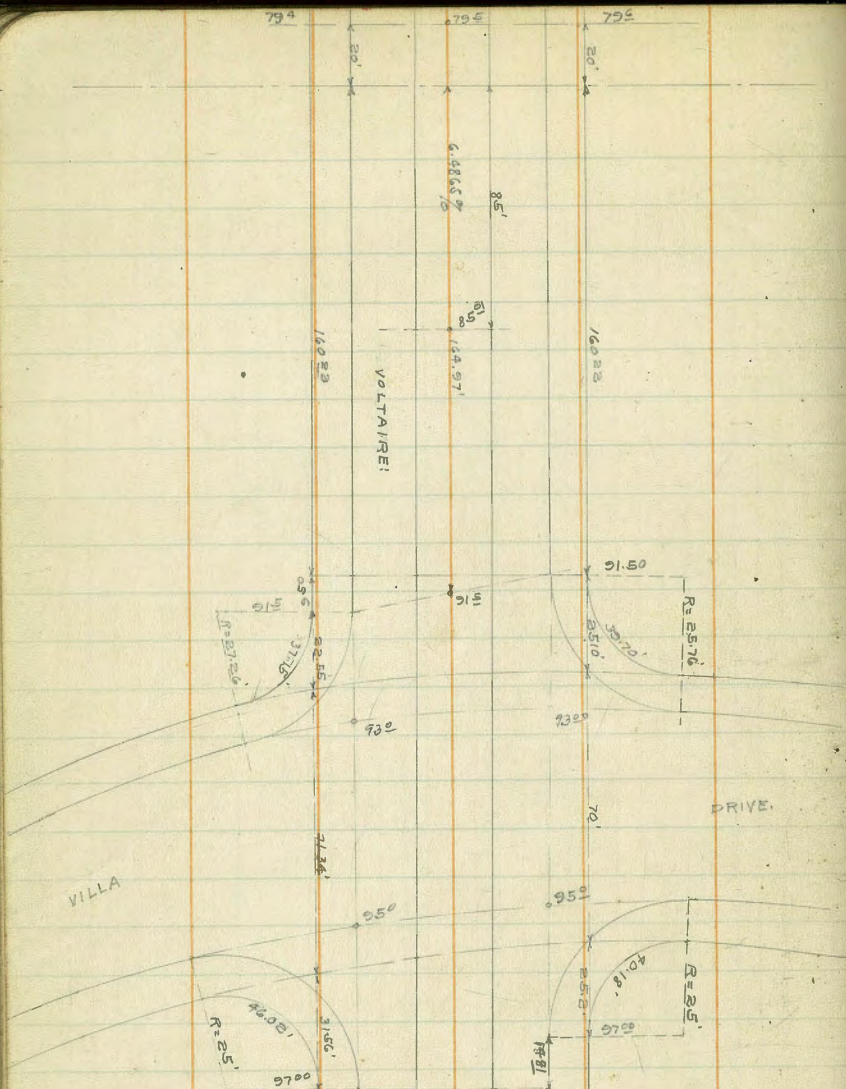
126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86
16.31	16.50	22.73	21.95	21.17	20.39	19.61	18.83	18.26	17.08
08.00	3.36	4.13	4.91	5.69	6.47	7.25	8.03	8.60	9.28

126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86	126.86
16.39	17.23	18.07	18.91	19.75	20.59	21.43	22.27	23.02	23.72
10.47	9.63	8.79	7.95	7.11	6.27	5.43	4.59	3.84	3.14



116.15 T.P.  
 + 0.60  
 115.80 T  
 12.80 T  
 0.25  
 0.14  
 103.09 T  
 - 6.19  
 96.9 ft = stake

115.80	115.80	103.09
113.77	113.50	97.00
+ 2.03	2.30	+ 6.09
2.13	2.40	6.19



20.50 = finish stake 100' W of Warrington.  
 70.12  
 90.62 π

90.62  
 87.00  
 3.62 = finish stake 50' W of Warrington.

20.62 20.62  
 78.50 85.01  
 11.12 5.61

96.90 = stake  
 + 0.35  
 97.25 π  
 72.67  
 84.58  
 91.96  
 85.54 π

97.20 97.20 97.25 85.54  
 78.00 95.00 91.40 79.40  
 4.20 2.20 6.80 6.14  
 4.35 2.35

WARRINGTON

83.5	84.2 83.7 83.0	83.5	83.5
83.5	83.5 82.0	83.5	83.5
80.0	80.0	80.0	80.0
78.46	78.45	78.45	78.45
77.34	77.35	77.35	77.35
76.63	76.64	76.64	76.64
76.35	76.37	76.37	76.37
76.48	76.52	76.52	76.52
77.04	77.09	77.09	77.09
78.01	78.09	78.09	78.09
79.4	79.50	79.50	79.50

VOLTAIRE:

90.50 E.M. finish stake 100' W of Warrington:

70.12  
 90.62  
 18.17  
 78.45  
 +9.00  
 87.54 π

90.62  
 87.00  
 3.62 ✓ 50' W of War'n

90.62  
 83.50  
 7.12  
 5.42  
 +1.70 e +3.80 OS

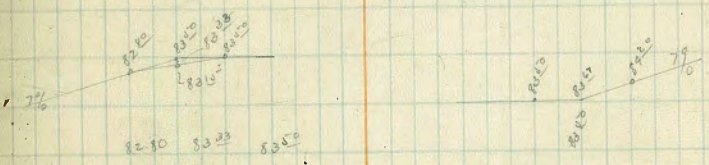
90.62	90.62	90.62	87.54	87.54	87.54	87.54	87.54
83.50	80.00	78.45	77.35	76.64	76.37	76.52	77.10
7.12	90.62	18.17	10.13	10.50	11.17	11.02	10.44

Finish stakes:

87.54 87.54  
 78.08 79.50  
 9.46 8.04

80.54 see preceding  
 1.12 Page:  
 83.00 T.M.W.S.  
 7.10  
 85.40

80.54	80.54	80.54	80.54	80.54	80.54	80.54	80.54	80.54
79.40	77.98	77.00	76.43	76.27	76.09	77.00	78.30	78.30
6.14	7.86	8.54	9.12	9.27	9.00	8.29	7.19	7.19
80.54	80.54	80.54	80.54	80.54	80.54	80.54	80.54	80.54
79.90	83.40	82.70	83.23	83.40	83.40	83.57	84.10	84.10
0.64	2.14	1.70	1.27	1.20	1.20	1.83	1.30	1.30





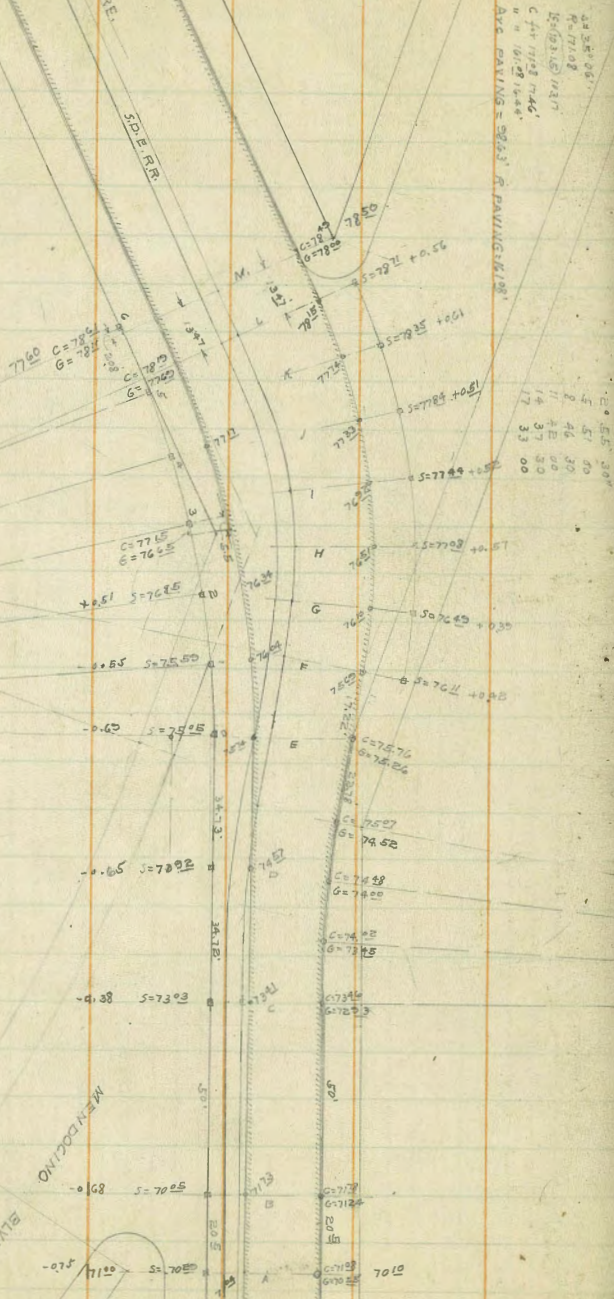
VOLTAIRE

S.D.E. RR.

MENDOZINO BLVD.

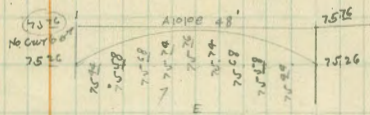
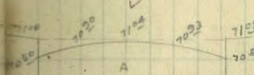
$A = 5^{\circ} 57' 12''$   
 $R = 2815$   
 $C = 113.88$   
 $L = 113.88$   
 $H = 574.6$   
 $E = 250'$   
 $C = 1825$   
 $L = 10350'$   
 $E = 57' 33''$

4 11 36  
 6 14 30  
 8 23 00  
 10 27 50  
 12 33 00



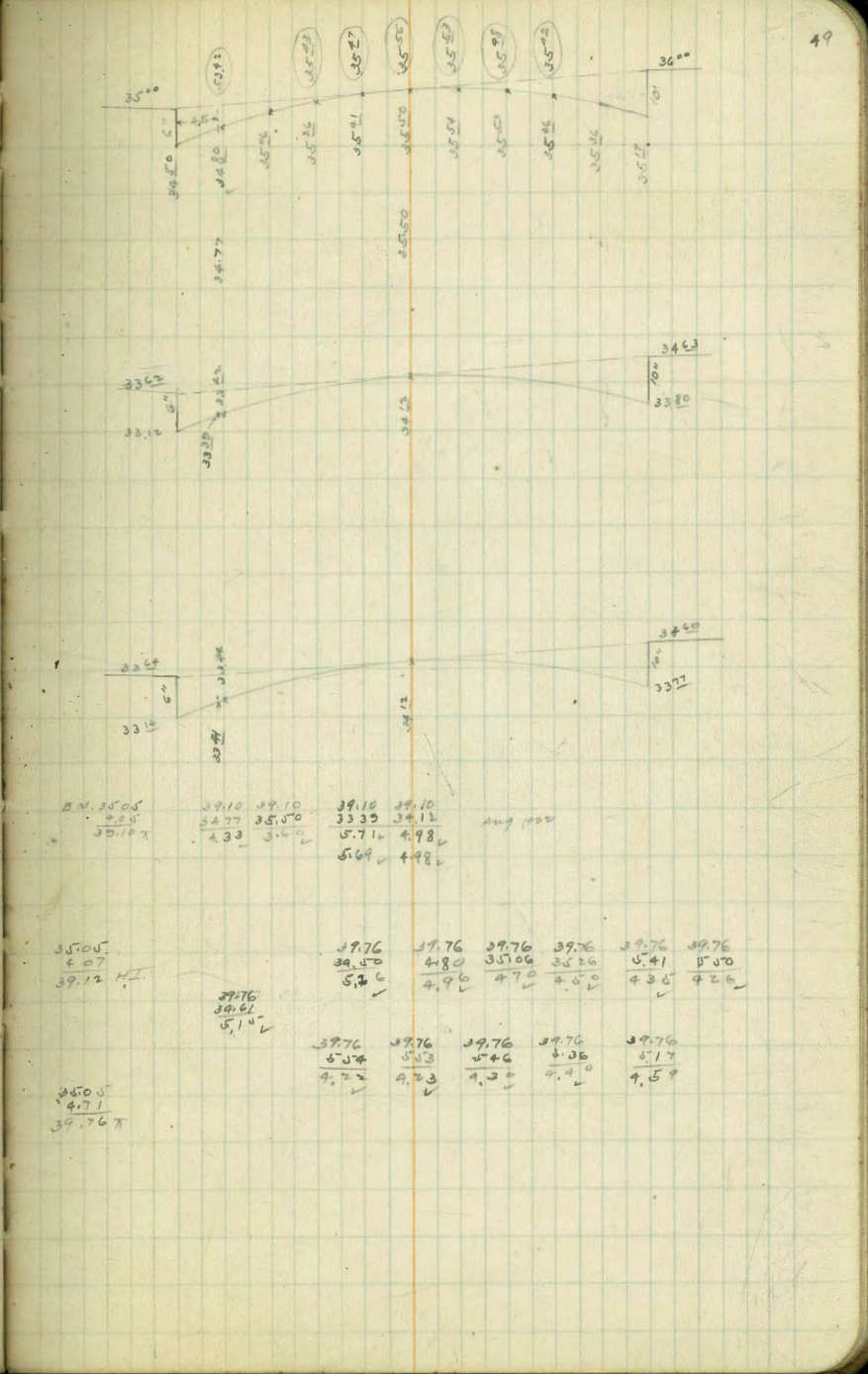
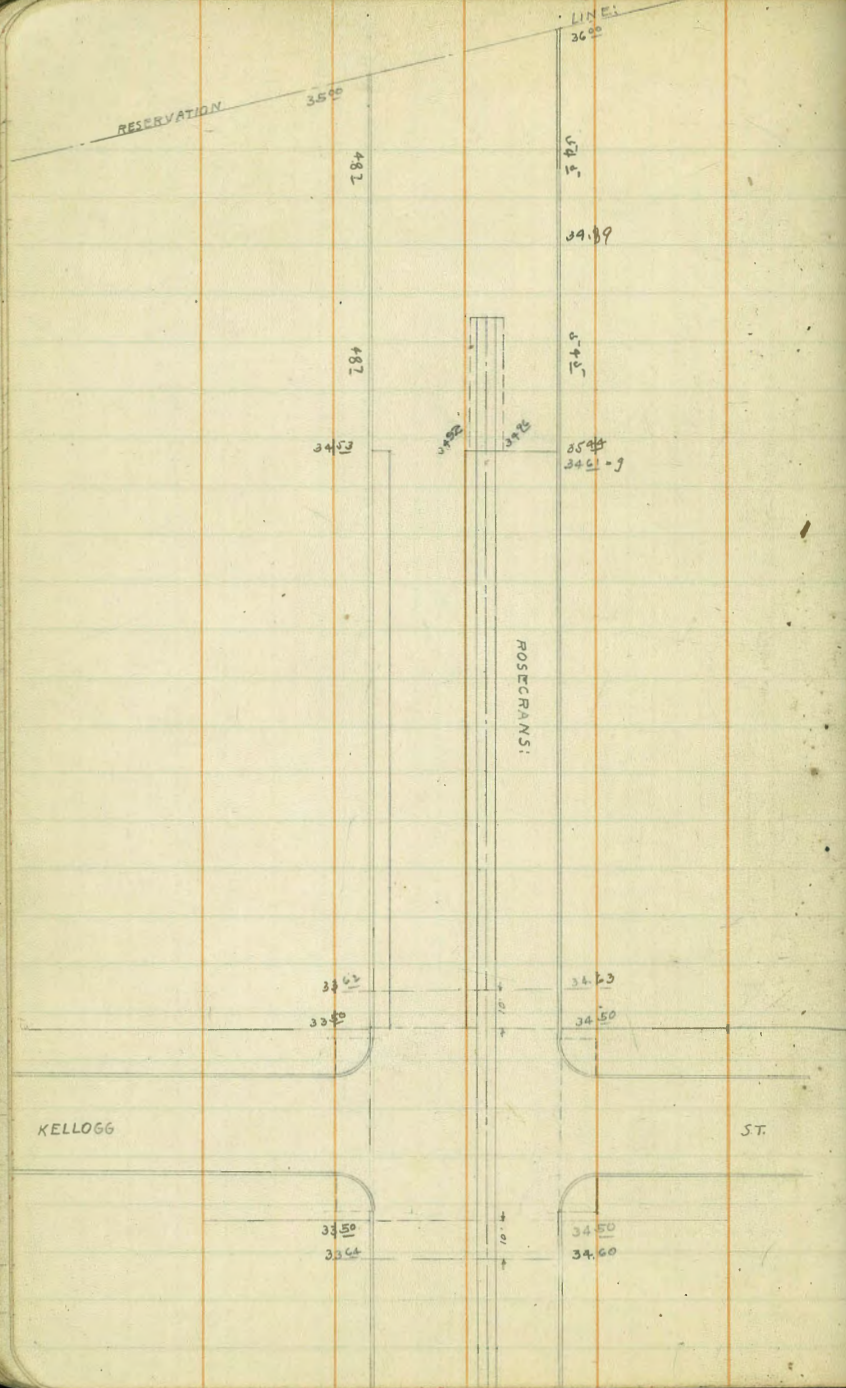
$23.5^{\circ} 06'$   
 $R = 171.03$   
 $C = 103.10$   
 $L = 103.10$   
 $H = 51.55$   
 $E = 25.77$   
 $C = 182.5$   
 $L = 103.50'$

$23.5^{\circ} 30'$   
 $R = 171.03$   
 $C = 103.10$   
 $L = 103.10$   
 $H = 51.55$   
 $E = 25.77$



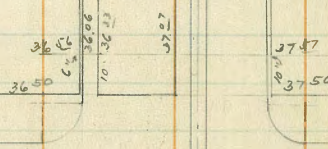
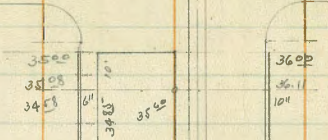
$A = 5^{\circ} 57' 30''$   
 $R = 2815$





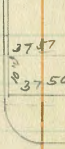
LAWRENCE

ST.



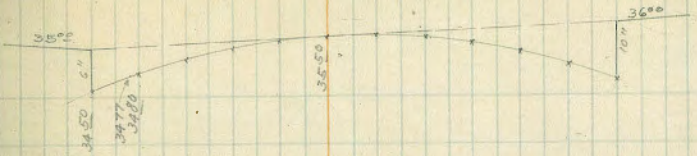
MCCALL

ST.



ROSECRANS

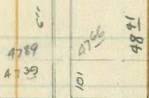
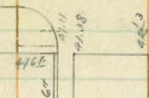
2



42.07	42.07	42.07	42.07	42.07	40.89	40.89	40.89	40.89
36.33	37.07	36.81	37.61	34.88	35.60	34.77	35.50	
6.74	5.52	5.78	4.98	6.04	5.29	6.12	5.39	

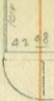
38.10  
 37.0  
 40.89

NICHOLS



OWEN

ROSECRANS



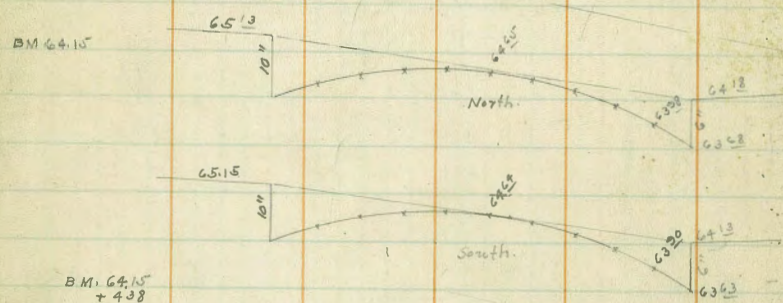
BAR 4163  
4140  
AC 108 T

46.08	46.08	46.08	46.08	46.08
41.38	41.08	40.80	41.48	42.12
4.70	4.80	5.28	4.60	3.96

B.M. 45.07  
5.21  
58.28 X

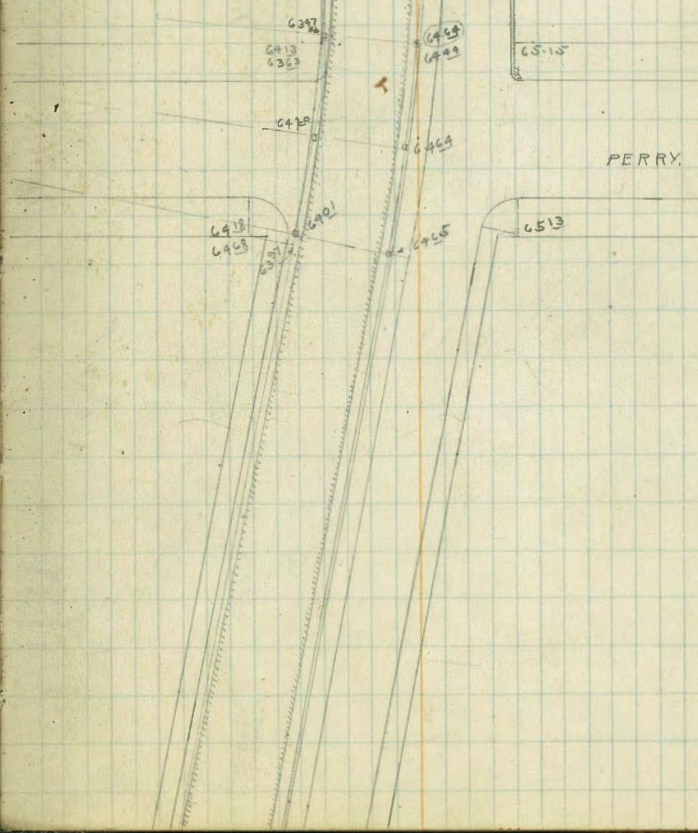
58.28	58.28	58.28	58.28
47.66	48.81	49.35	50.14
5.62	4.87	3.93	3.14

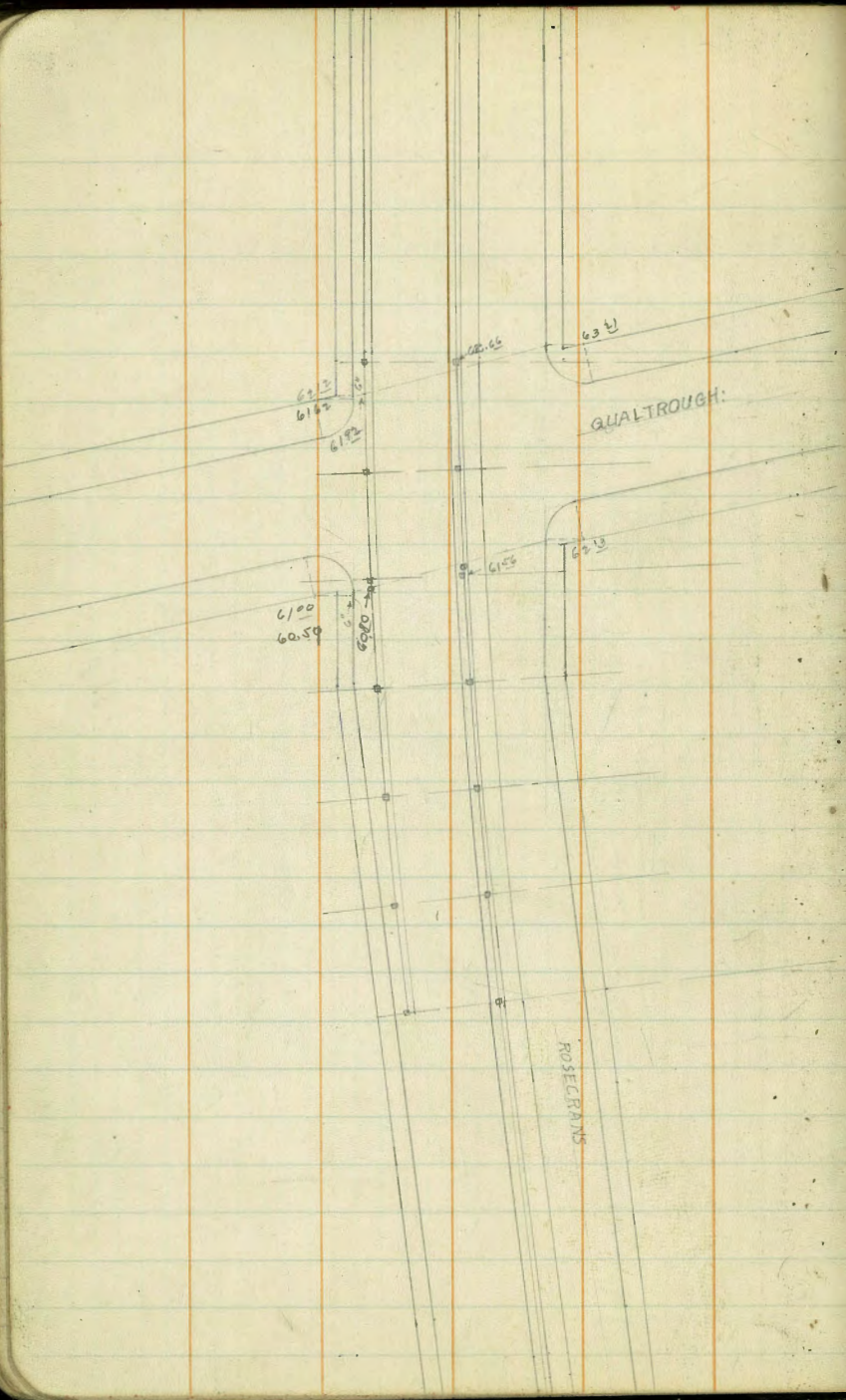
$\Delta = 10^{\circ} 54'$   $T = 52.40'$  Chords;  $1^{\circ} 21' 45''$   
 Rem stake line = 546.25  $C = 26.97'$   $2^{\circ} 43' 30''$   
 " " " " = 572.25  $C = 27.11'$   $4^{\circ} 05' 15''$   
 $5^{\circ} 27' 00''$



B.M. 6415  
 + 4.38  
 -----  
 6853

68.53	68.53	68.53	68.53
64.64	63.90	63.93	64.60
3.89	4.63	4.55	3.88
4.09			





66.27  
 +4.38  
 66.45 X

60.45	60.45	66.45	66.45
61.92	62.60	61.56	60.80
4.53	3.79	4.89	5.65

- 0° 25'
- 0° 50'
- 1° 15'
- 1° 40'
- 2° 05'
- 2° 30'

$A = 5^{\circ} 0'$   
 $T =$   
 Stake Line  $R = 1915'$   $C = 27.85'$   
 " " "  $= 1937'$   $T = 84.60'$   $C = 28.19'$

Sta + 45.99

45.99  
46.77

46.69

47.20

ROGERS

45.00

46.4  
45.0

46.22

ROSECRANS

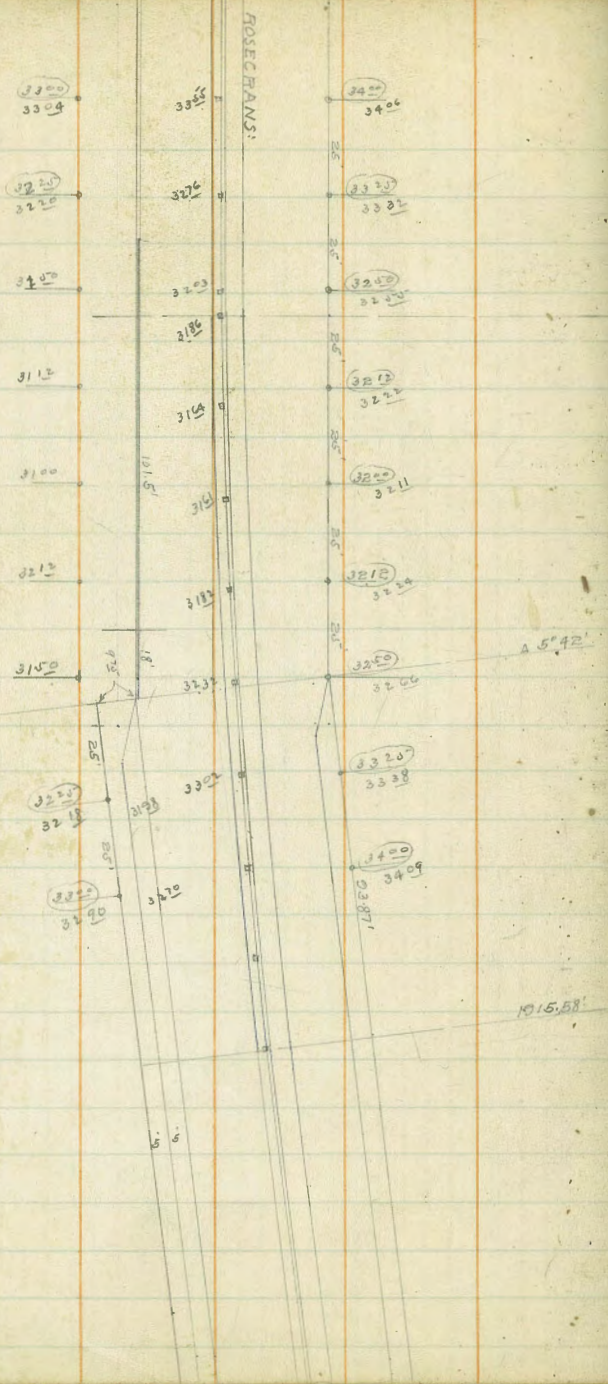
BM. 62.07  
+ 0.23  
62.30  
- 12.89  
49.41  
+ 1.25  
50.66  
- 3.34  
47.32 BM. Spk Pole

50.66  
+ 5.79  
48.7  
50.66  
16.60  
4.06

47.32  
+ 0.64  
47.96  
- 12.82  
35.14  
1.81  
36.35

47.36  
45.00  
2.36  
4.08 5184





B.M.	41.25	42.69	42.69	42.69	42.69	42.69
	+1.44	31.50	31.12	31.12	31.50	32.20
	42.69	11.49	11.57	11.69	11.19	10.44
	41.25					
	290					
	+3.74					

$\Delta = 15^{\circ} 42'$   $T = 95.81$   $C = 23.92'$

- 0' 21' 30"
- 0 43 00
- 1 04 30
- 1 26 00
- 1 47 30
- 2 09 30
- 2 30 30
- 2 52'

ROSECRANS:

BM. 51.57  
 2.89  
 54.40 X

59.40	59.40	59.40	59.40	59.40
2.83	3.47	4.11	4.75	5.39
51.57	50.93	50.29	49.65	49.01

$R = 135^{\circ}00'$   $\Delta = 36^{\circ}56'$   $C = 21.73'$   $T = 45.08'$

9  
 51.57

4° 37' 50.93

9 14 50.29 5 stakes

13 5' 49.65

18.28' 49.01

$\Delta = 36^{\circ}56'$   $R = 172.5'$   $C = 22.29$

$T = 57.61'$   $R = 196.5'$   $C = 25.34$

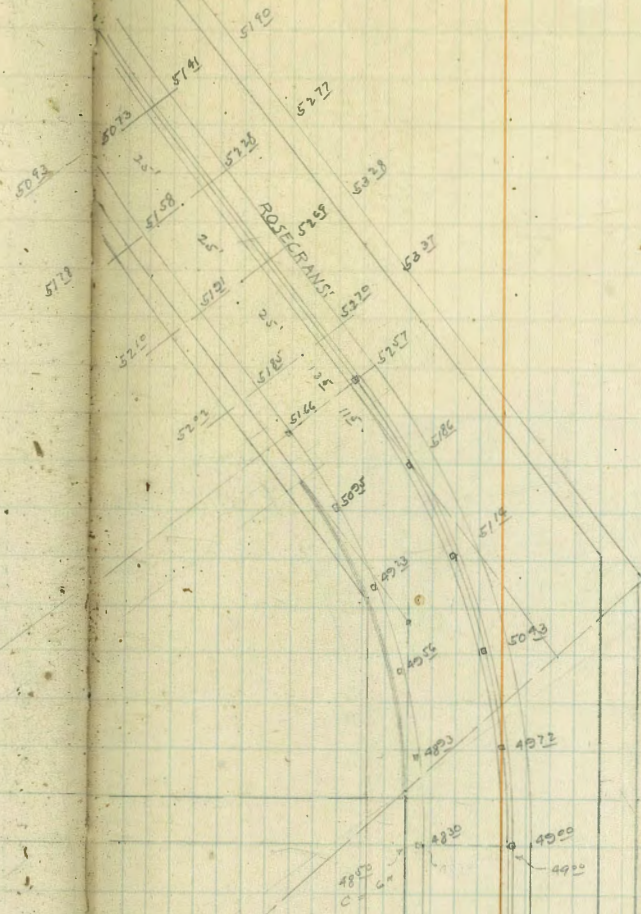
2° 41' 36"

7 23 12

11 04 48

14 46 24

18 28 00



BM. 25.05	23.61	23.61	23.61	23.61
4.56	27.55	28.60	26.97	27.64
33.61.7	5.66	5.01	6.63	5.97

23.61	23.61
5.66	6.93
28.10	27.19

ROSECRAUS.

2800 6" 2795 2800 10" 2900 2900

2810  
2760

BESSEMER.

2609 2719 2700 2699 2764 2810 2800

BM 2805 BESSEMER.

210  
30.10 X  
- 6.83

23, 32 = B.N. TALBOT.

2805  
968  
32.73 X

32.73    32.73  
26.93    27.61  
5.78     5.12

2800

2805

BESSEMER.

27 15

26 25

27 01

28 00

28 08

RAKED:

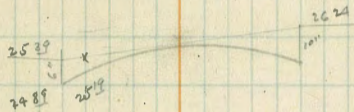
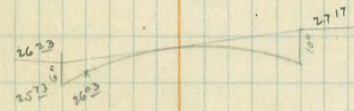
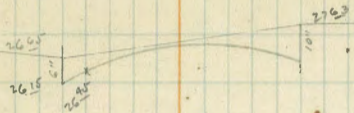
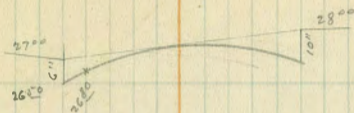
HOISCHRAUM.

50

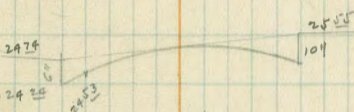
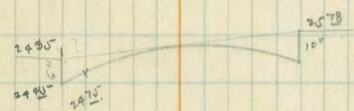
50

50

50



N.G. RAKED.



ROSECRANS!

RAKED!



23°

BM 28.32  
5.15  
28.47 T

28.47 28.47  
5.20 4.60  
C = 23.22 23.87 = C  
E = 20.54

G = 22.72 22.96

28.47 28.47  
23.54 22.96  
4.93 5.51 ✓

23.32  
3.11  
26.43 T

26.43 26.43  
21.30 22.00  
5.13 4.43 ✓

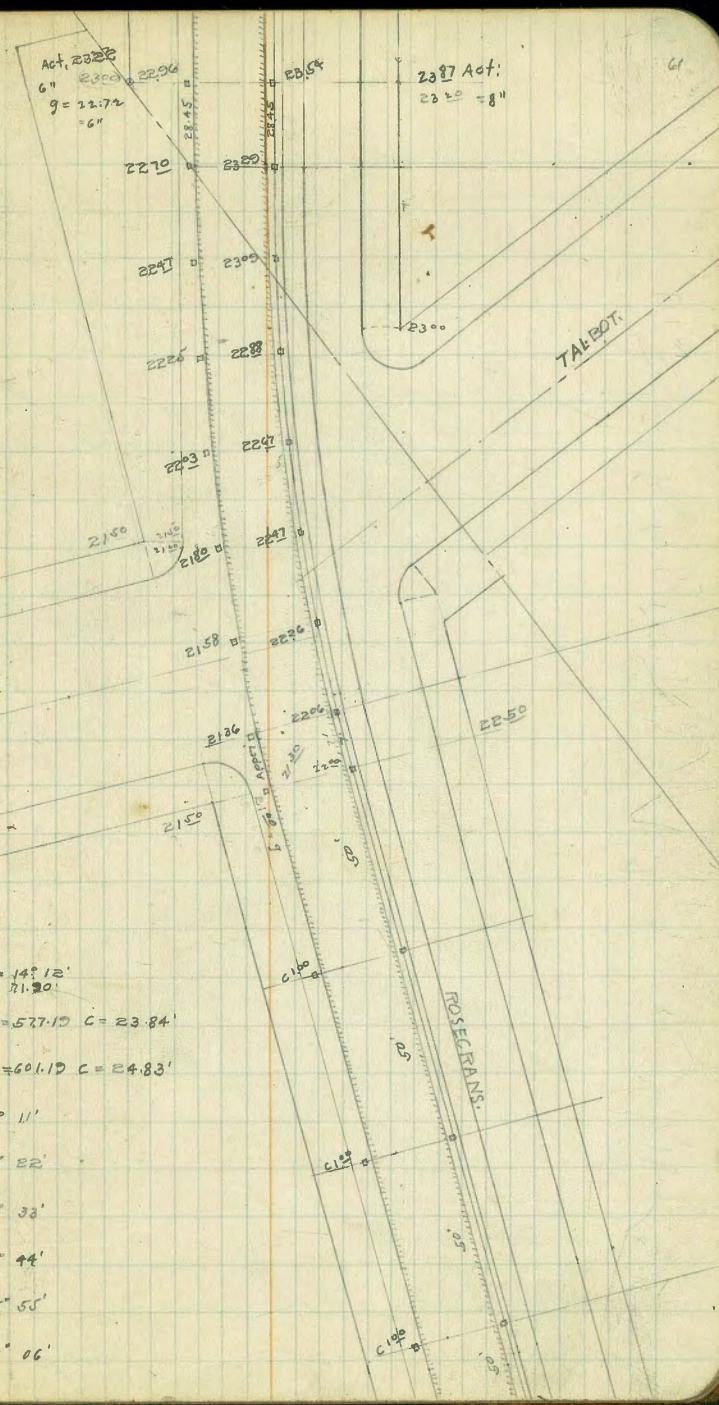
BM 20.67 SW Canyon Road

.08032%

26.43	26.43	26.43	26.43	26.43	26.43	26.43	26.43	26.43
22.00	22.00	22.26	22.47	22.67	22.95	23.09	23.27	23.54
4.43	4.43	4.17	3.96	3.76	3.55	3.34	3.14	2.89

.009%

26.43	26.43	26.43	26.43	26.43	26.43	26.43	26.43	26.43
21.30	21.30	21.08	21.80	22.03	22.24	22.47	22.70	22.96
5.13	5.07	4.85	4.63	4.40	4.19	3.96	3.73	3.47



Δ = 14° 12'  
T = 71° 30'

R = 57.17 C = 23.84'

R = 60.17 C = 24.83'

1° 11'

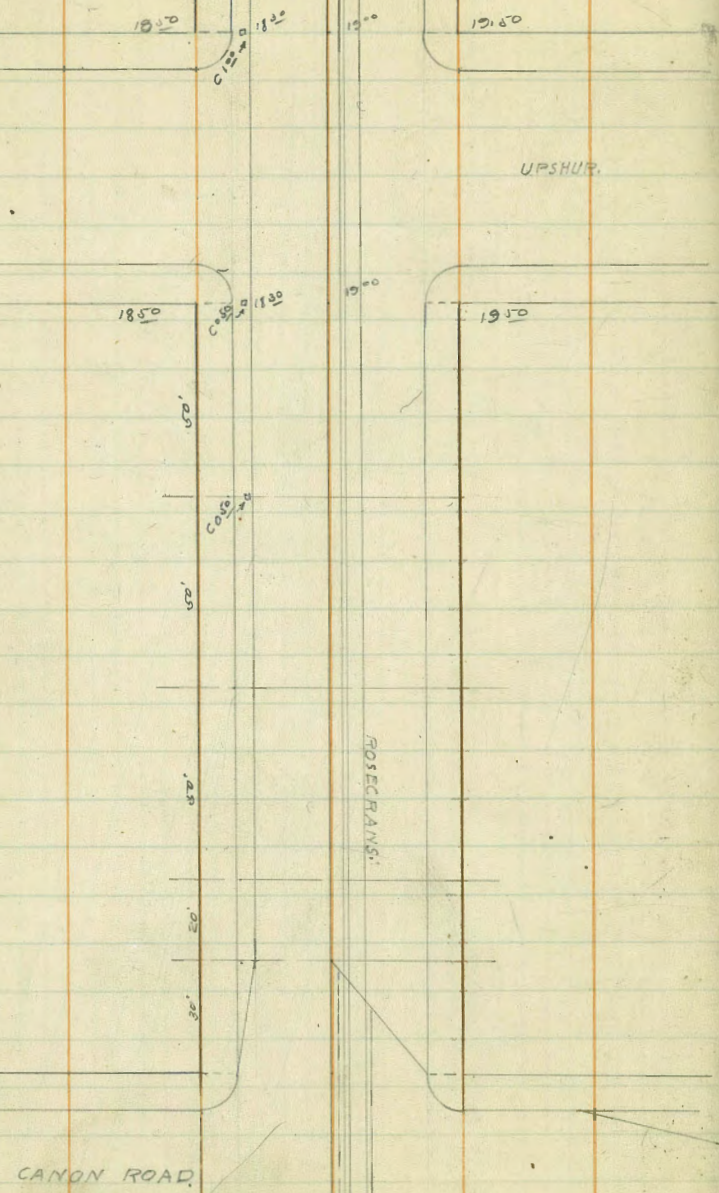
2° 22'

3° 33'

4° 44'

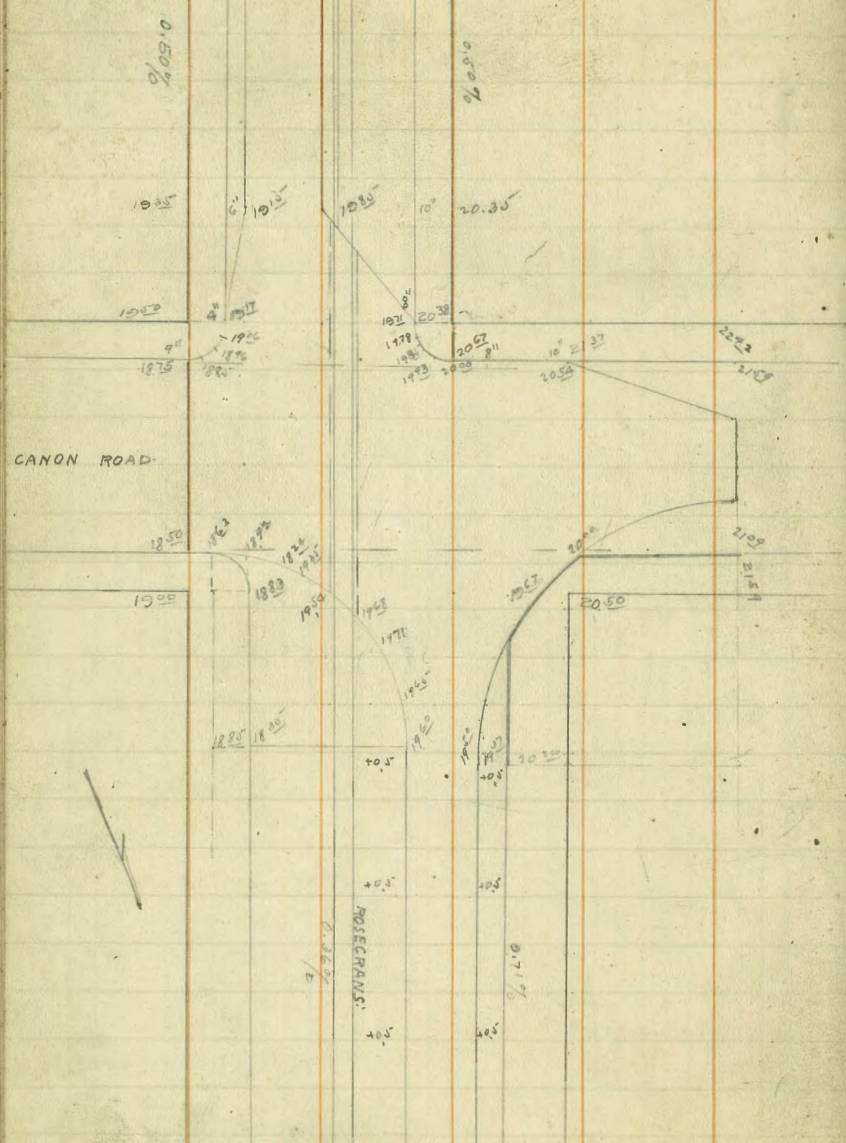
5° 55'

7° 06'



BM. 20.67	23.97	23.97	6.34 of Rod	5.19 Rod
3.30	18.30	19.00		4.64
23.97	5.67	4.97		





20.67 27.01  
 +2.96 6.34  
 23.63 27.01  
 23.63 19.00  
 8.01

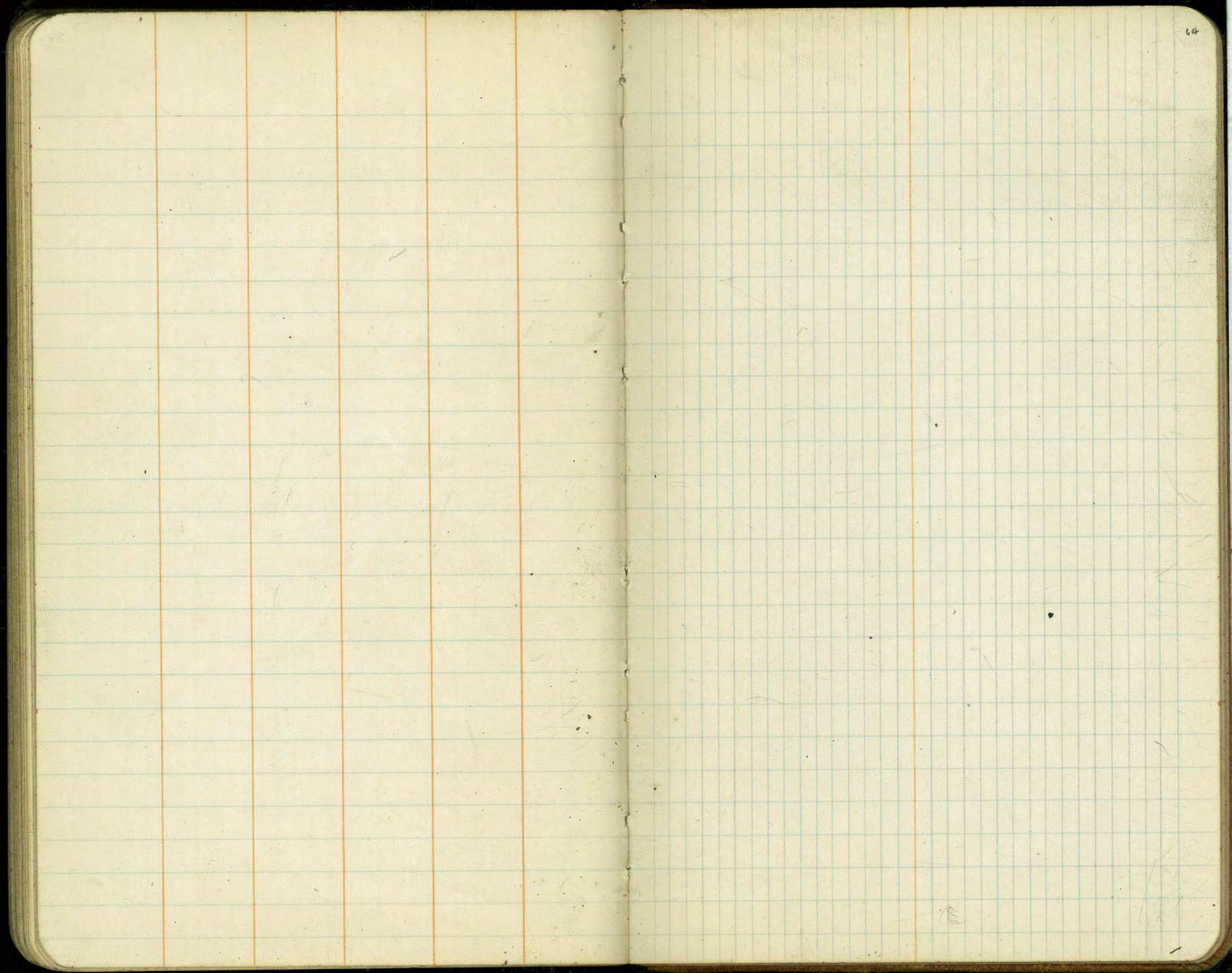
20.67 23.63 23.63  
 +2.96 19.10 19.88  
 23.63 4.48 3.78

	W	E
20.67	20.67	20.67
+2.96	19.50	19.60
	6.23	6.13
	5.73	5.63
	+0.50	+0.40
	6.56	6.41

20.67 20.67  
 +2.96 19.10  
 23.63 4.48

	W	E
20.67	20.67	20.67
+2.96	19.50	19.60
	6.23	6.13
	5.73	5.63
	+0.50	+0.40
	6.56	6.41

- ✓ 18.83 19.09 19.22 19.50 19.65 19.75 19.81 19.84 19.82 19.77 19.67
- ✓ 20.00 20.29 20.53 20.73 20.86 20.99 20.92 20.94 20.88 20.72 20.52
- ✗ ✓ 18.50 18.36 18.20 19.10 19.20 19.25 19.25 19.20 19.10 18.90 18.70
- ✓ 18.35 18.69 18.77 19.21 19.39 19.52 19.60 19.62 19.58 19.50 19.37
- ✓ 19.17 19.40 19.60 19.75 19.87 19.94 20.05 20.03 19.96 18.86 19.71
- ✓ 18.85 19.15 19.40 19.60 19.75 19.85 19.89 19.87 19.80 19.68 19.52
- ✗ 21.09 21.37 21.61 21.81 21.93 22.00 22.03 21.99 21.91 21.77 21.59



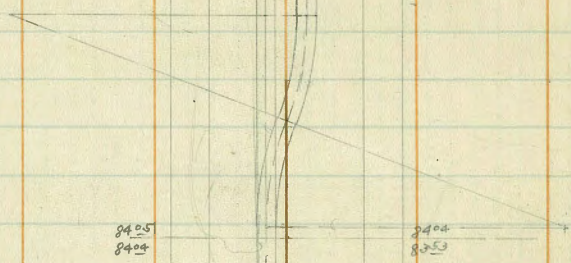
17.24  
86.74

87.12  
86.27  
86.23  
86.23  
87.23  
86.27  
86.53

BOLINAS ST.

65

87.00 87.04  
86.53

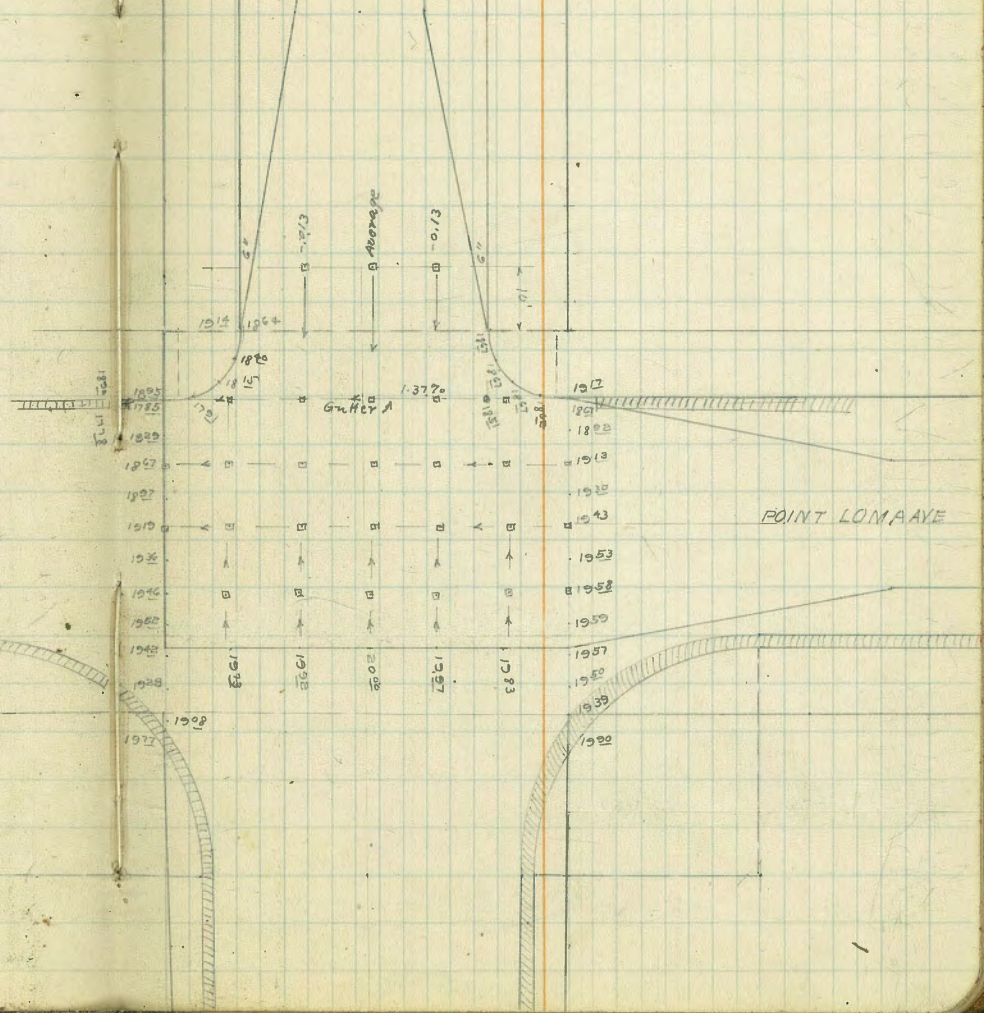


78.60 78.11  
78.11

78.48  
78.00

M. ZINBOCINO.

DE FOIE ST



POINT LOMAYE

1921  
1922  
1923  
1924  
1925  
1926  
1927  
1928  
1929  
1930  
1931  
1932  
1933  
1934  
1935  
1936  
1937  
1938  
1939  
1940  
1941  
1942  
1943  
1944  
1945  
1946  
1947  
1948  
1949  
1950  
1951  
1952  
1953  
1954  
1955  
1956  
1957  
1958  
1959  
1960

EBERS ST.

36.2  
 36.25  
 36.5  
 36.7  
 36.16  
 36.3

34.98  
 35.24  
 34.91  
 34.7  
 34.5  
 34.05

POINT LOMA AVE.

23.15  
 23.21  
 23.2  
 23.19  
 23.2  
 23.19  
 23.15

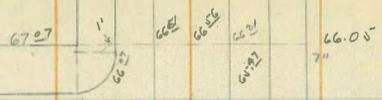
34.04  
 22.21  
 36.24 X

36.25    36.25  
 36.16    36.69  
 1.09    0.86

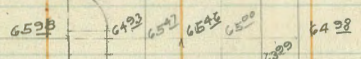
34.04  
 87  
 34.91 X

34.91    34.91  
 34.47    34.05  
 0.44    0.86

34.91    34.91  
 22.23    22.28  
 11.08    11.03



FROUDE ST.



POINT LOMA

AVE

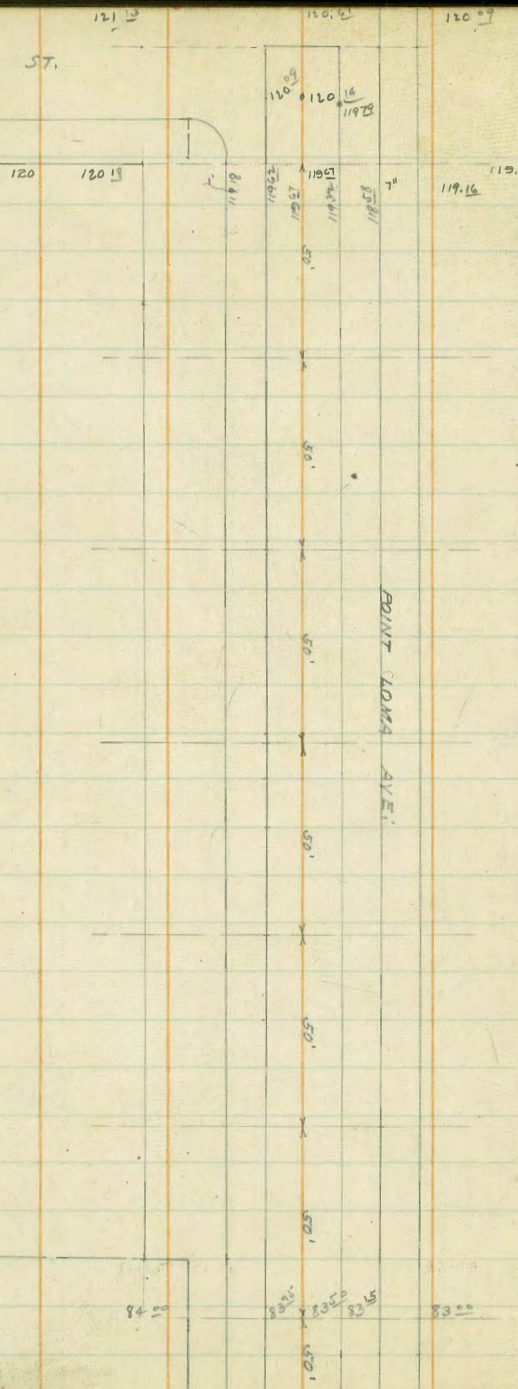
B.M. 64.90  
 + 5.22  
 70.12 X

70.12	70.12
<u>65.47</u>	<u>65.00</u>
4.65	5.12

64.90  
 18.60  
 77.90 X  
 0.67  
 77.23  
 91.47  
 86.70 X

77.90	77.90
<u>60.21</u>	<u>60.21</u>
11.39	11.69

GULF LOT ST.



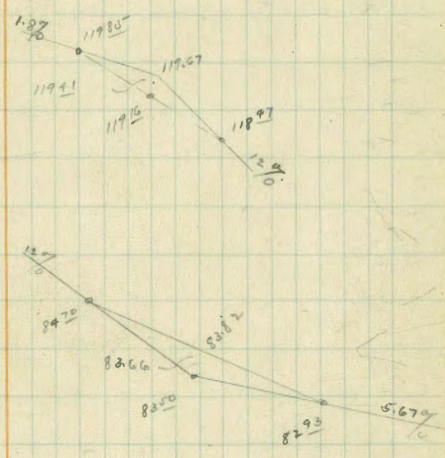
BANK 11/2/13	124.31	124.31	124.31	124.31	124.31	124.31
518	120.09	119.79	119.80	119.50	119.36	119.06
124.31 X	4.22	4.52	4.51	4.81	4.95	5.25

124.31	124.31
118.42	118.16
5.89	6.15

86.70 x Sea Measuring Jodge	86.70	86.70	86.70	86.70	86.70	86.70
	82.85	82.58	83.61	83.31	84.65	84.35
	3.85	4.12	3.09	3.39	2.05	2.35



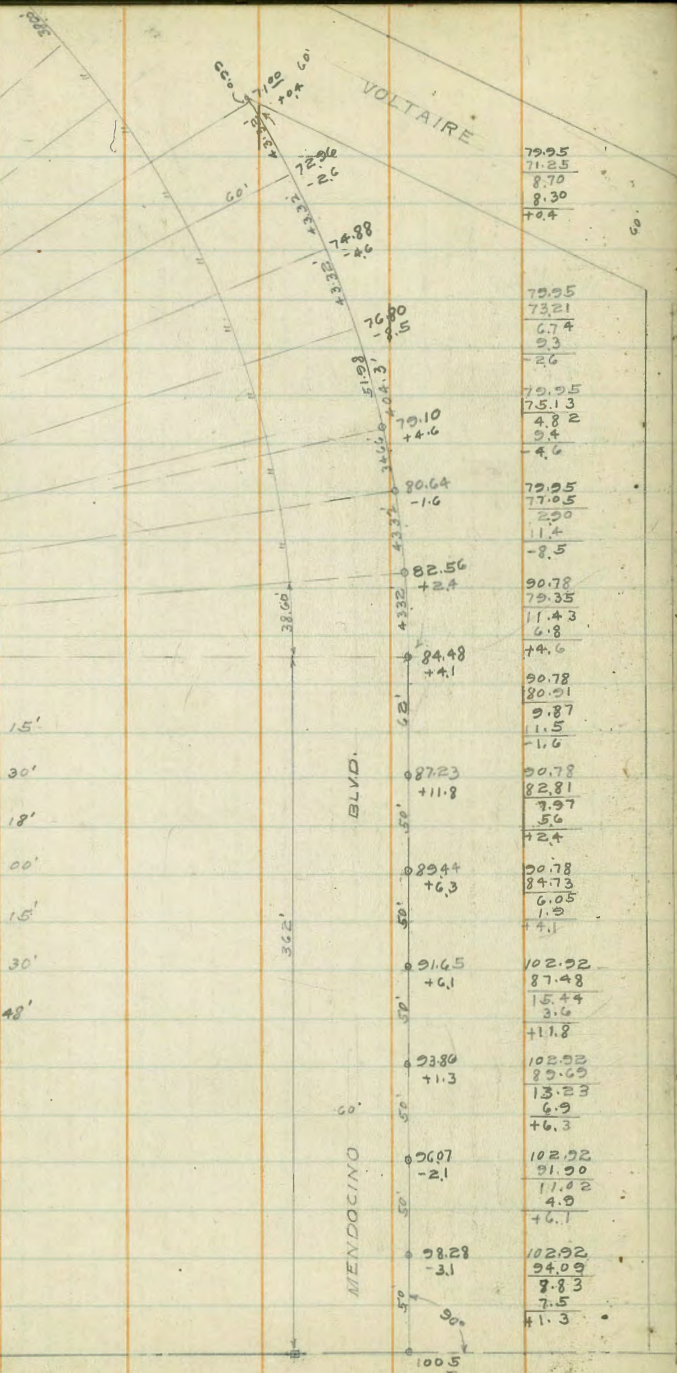
			grade
00		82.14 82.00	69.80
+50	82.14 69.57 12.57 7.68 +4.89	82.14 18.14 -9.55 +3.59	69.57
1			
1+50	82.14 70.72 11.42 6.03 +5.39	82.14 71.30 10.84 5.39 +5.50	70.15
2			
2+60 = M H	82.14 72.77 9.37 2.71 +6.66	82.14 72.00 10.14 4.26 +5.88	70.72
3			
3+50	82.14 72.77 9.37 2.71 +6.66	82.14 73.73 8.41 2.59 +5.82	71.30
4			
4+50	82.14 75.65 6.49 0.96 +5.53	82.14 72.00 10.14 4.26 +5.88	72.10
5			
5+32	82.14 75.65 6.49 0.96 +5.53	82.14 73.73 8.41 2.59 +5.82	72.77
5+72 = N, H	82.14 75.65 6.49 0.96 +5.53	82.14 74.69 7.45 1.69 +5.76	73.73
6+12			
6+50	82.14 75.65 6.49 0.96 +5.53	82.14 74.69 7.45 1.69 +5.76	74.69
7			
7+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	75.65
8			
8+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	76.61
9			
9+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	77.25
0			
0+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	78.00
1			
1+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	78.68
2			
2+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	79.32
3			
3+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	80.16
4			
4+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	81.01
5			
5+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	81.86
6			
6+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	82.70
7			
7+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	83.54
8			
8+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	84.39
9			
9+50	82.14 75.65 6.49 0.96 +5.53	82.14 76.61 17.53 11.37 +6.16	85.20

B. M. 87.60 - With Draper & Pearl. N  
 + 4.43  
 92.03 x  
 - 2.69  
 79.34  
 + 2.80  
 82.14 x  
 - 0.56  
 81.58  
 + 12.96  
 94.54 x  
 2.30  
 97.84 = Subs B.M. 71.88

Top stakes July 19th 22  
 Bonmart  
 Miller  
 Seyferts  
 Walbrecht

B.P. S.E. Cor Pearl & Gerard. 115.05





79.95  
 71.25  
 8.70  
 8.30  
 +0.4

79.95  
 73.21  
 6.74  
 9.3  
 -2.6

79.95  
 75.13  
 4.82  
 9.4  
 -4.6

79.95  
 77.05  
 2.50  
 11.4  
 -8.5

82.56  
 90.78  
 79.35  
 11.43  
 6.8

84.48  
 90.78  
 80.21  
 9.87  
 11.5  
 -1.6

87.23  
 90.78  
 82.81  
 7.97  
 5.6  
 +2.4

89.44  
 90.78  
 84.73  
 6.05  
 1.9  
 +7.1

91.65  
 102.92  
 87.48  
 15.44  
 3.6  
 +11.8

93.80  
 102.92  
 89.69  
 13.23  
 6.9  
 +6.3

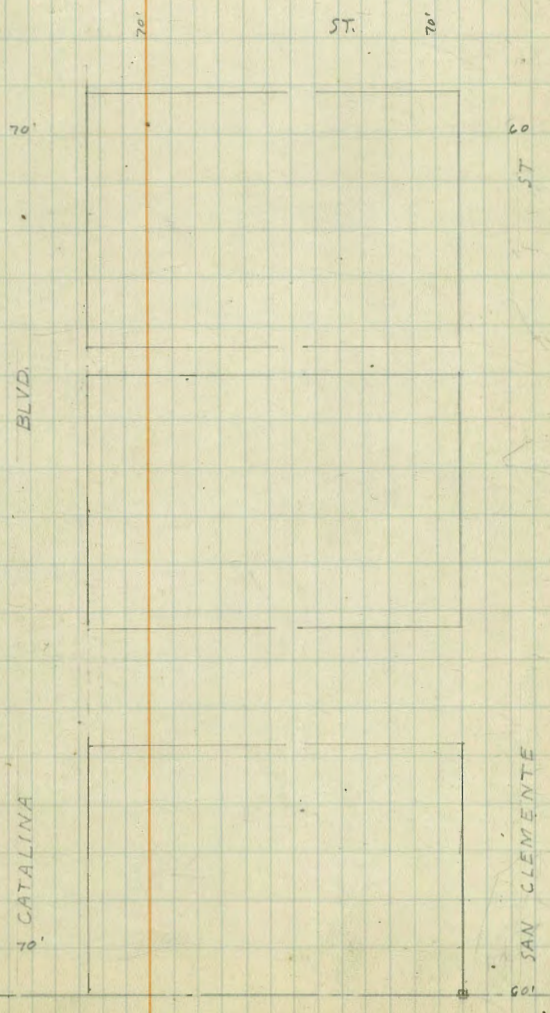
96.07  
 102.92  
 91.90  
 11.02  
 4.9  
 +6.1

98.28  
 102.92  
 94.09  
 8.83  
 7.5  
 +1.3

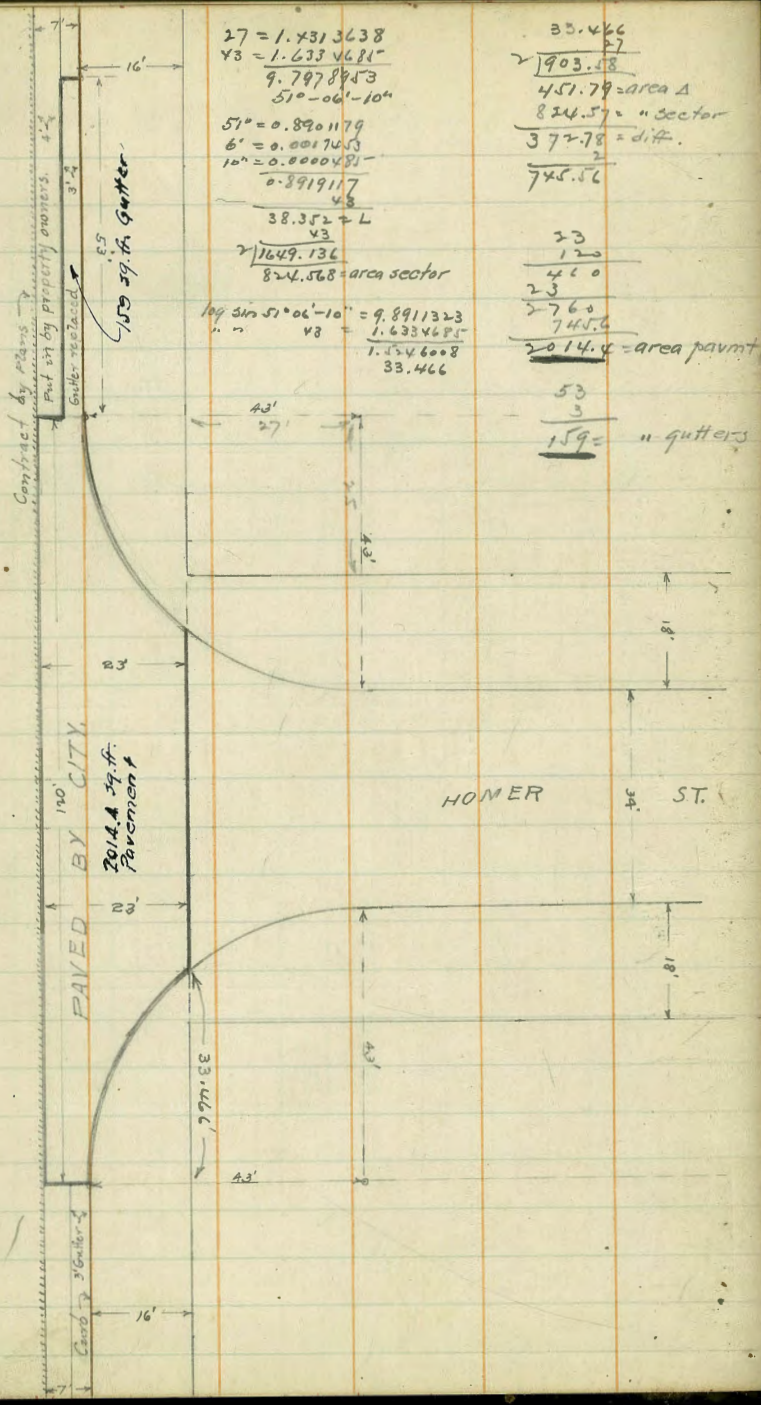
B.M. 7500  
 + 0.95  
 75.95 X  
 0.00  
 75.95  
 + 10.83  
 90.78 X  
 - 0.08  
 90.70  
 + 12.22  
 102.92 X

102.92  
 96.32  
 6.60  
 8.7  
 -2.1

102.92  
 98.53  
 4.39  
 7.5  
 +3.1



ROSCREANS ST.



$$\begin{aligned}
 27 &= 1.4313638 \\
 43 &= 1.6334681 \\
 \hline
 &9.7978943 \\
 51^\circ - 06' - 10'' & \\
 51^\circ &= 0.8901179 \\
 6' &= 0.0017653 \\
 10'' &= 0.0000481 \\
 \hline
 &0.8919117 \\
 &43 \\
 \hline
 &38.352 \rightarrow L
 \end{aligned}$$

$$\begin{aligned}
 104 \sin 51^\circ 06' 10'' &= 9.8911323 \\
 43 &= 1.6334681 \\
 \hline
 &1.2576608 \\
 &33.466
 \end{aligned}$$

$$\begin{aligned}
 33.466 \\
 27 \\
 \hline
 903.48 \\
 451.79 = \text{area } \Delta \\
 824.57 = \text{sector} \\
 \hline
 372.78 = \text{diff.} \\
 75.56
 \end{aligned}$$

$$\begin{aligned}
 23 \\
 120 \\
 \hline
 460 \\
 23 \\
 \hline
 760 \\
 744.6 \\
 \hline
 2014.10
 \end{aligned}$$

area pavement = 2014.10

DIRECTIONS FOR USE OF TABLES

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in both of table in same row and column gives distance level estimate the distance in elevation between the side stake and slope stake. Lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at end and find distance in table. Add cut target. If it does not make the sight adjustment

IMPROVED TABLES AND INFORMATION

TABLE No. 2

To find Tangent and External for curve of any other degree, divide by degree of curve and add connection found in column of connections. Degree of curve with a given L may be found by dividing tangent (or external), opposite L by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

$$\begin{array}{r} 113.30 \\ 1.30 \\ \hline 112.00 \end{array}$$
$$\begin{array}{r} 32.72 \\ 52.73 \\ \hline 85.45 \\ \hline 37.15 \end{array}$$
$$\begin{array}{r} 26.43 \\ 3.23 \\ \hline 23.20 \end{array} \quad \begin{array}{r} 26.43 \\ 2.61 \\ \hline 23.82 \end{array}$$
$$\begin{array}{r} 67.80 \\ 2.36 \\ \hline 70.16 \\ \hline 77.2 \end{array}$$
$$\begin{array}{r} 67.80 \\ 1.72 \\ \hline 69.52 \end{array}$$
$$\begin{array}{r} 2.36 \\ 1.72 \\ \hline 4.08 \\ 1.72 \\ \hline 5.80 \\ 1.72 \\ \hline 7.52 \end{array}$$