

1102

FIELD BOOK

385

MICROFILMED

DEC 21 1964

1102

Moore
10/27/23

Area in sq. ft. of Xings on 12th St
thru Balboa Park

Balboa Nursery Xing 1001.35

N. S. D. Elec. RR Xing 1430.41

S. " " " " 1490.01

Levels on Wood Lane (40' wide): Imperial Ave to Rst.

Highway Commission B.M. No 6 boat Spk Tel pole 156.873 see the page 9:

City 151.80
 0.99 157.86 (Note) Equation Page 9: -6.06

21' North of S.L. of Imperial Ave = S.L. Concrete Road:

EL	3.50	148.31
±	3.94	147.86
W.L.	4.40	147.4
0.00 = S.L. Imperial Ave:		
W.L.	5.8	146.01
±	5.0	146.8
E.L.	4.2	147.6
+50 E.L.	5.7	146.1
±	6.0	145.8
+18	6.3	145.5
W.L.	7.2	144.6
W.L. +5	7.0	144.8
1+00 W.L. -10	8.9	142.9
W.L. -5	8.3	143.5
W.L.	6.2	145.6
±	5.8	146.0
E.L.	6.0	145.8
1+50 E.L.	5.4	146.4
±	5.0	146.8
W.L.	5.7	146.1
W.L. +5	8.3	143.5
W.L. +10	8.8	143.0

Documents:
 Miller
 5/14/18
 Walbreck

11-21-22
 (City Datum = 750.813)

City 151.80
 157.86

WOOD LANE.

2+00 W.L.	4.3	147.5
±	4.2	147.6
E.L.	3.0	148.8
±	4.11	155.01 161.07 ✓
2+25 E.L.	4.5	150.90 156.96 ✓
+13	4.4	150.6
+18	7.1	147.9
±	6.9	148.1
W.L.	7.2	147.8
2+50 W.L.	6.0	149.0
+3	6.5	148.5
±	6.2	148.8
+2	6.4	148.6
+8	4.8	150.2
E.L.	4.3	150.7
2+75 E.L.	1.3	153.7
+12	2.3	152.7
+17	5.9	149.1
±	5.6	149.4
W.L.	5.5	149.5
2+00 W.L.	5.4	149.6
±	5.2	149.8
+2	5.3	149.7
+8	1.8	153.2
E.L.	2.0	153.0

Platted 12/11/18

City - 155.01
161.07 ✓

File

3+50 E.L	2.7	152.3 ✓
+12	3.4	151.6
+17	4.6	150.4
±	4.5	150.5
W.L	4.9	150.1
3+75 W.L	4.4	150.6 ✓
±	4.0	151.0
±+4	3.8	151.2
+9	1.0	154.0
E.L	0.3	154.7 ✓
4+20 E.L	3.0	151.5 ✓
±	4.1	150.9 ✓
W.L	4.8	150.2
4+50 W.L	4.9	150.2 ✓
±	4.6	150.4 ✓
+4	4.5	150.5
+9	2.7	152.3
E.L	2.2	152.8 ✓
4+70 E.L	2.3	152.7 ✓
+10	2.5	152.5
+17	4.7	150.3
±	4.8	150.2 ✓
W.L	5.4	149.6
+80 W.L	5.4	149.6 ✓
±	4.9	150.2
E.L	3.9	151.2 ✓

?

City - 155.01
161.07 ✓

WOOD LANE 2

5+00 E.L	4.5	150.5
±	5.1	149.9
W.L	5.2	149.8
5+50 W.L	5.8	149.2
+4	6.9	148.1
±	6.8	148.2
E.L	6.2	148.8
6+00 E.L	8.0	147.0
±	8.2	146.8
W.L	8.4	146.6
6+32 ³⁰ = N.L. Q. St. W.L (Q st so wide)	8.6	146.4
+5	9.0	146.0
±	8.9	146.1
E.L	8.8	146.2
00 = S.L. Q. St. E.L 6+6 ³⁰	8.4	146.6
±	9.4	145.6
+18	10.0	145.0
W.L	10.7	144.3
+60 W.L	11.0	144.0
+5	10.4	144.8
±	9.7	145.3
E.L	9.2	145.8
1+00 E.L	9.0	146.0
±	9.2	145.8
+15	10.0	145.0
W.L	10.7	144.3

Plotted 12/1/72
HRS.

7+12²

7+6²

City 15501
161.07 ✓

City 1474.37
155.43

WOODLANE

#		149.37 ✓ 155.43	8.78	146.23 152.27 ✓	4+50 W.L.	1147.2	11.0	138.4 ✓
1+50 W.L.	8+13.3		3.4	146.0	+3		11.8	137.6
E			3.0	146.4	E		11.6	137.8 ✓
E.L.			2.9	146.5	+6		12.4	137.0
2+00 E.L.	8+62.3		1.8	147.6 ✓	E.L.		13.7	135.7 ✓
+13			11.6	147.8	#	0.48	137.06 ✓ 143.12	136.58 142.64 ✓
+15			2.4	147.0	4+75 E.L.	11+37.3	12.79	133.8 ✓
E			2.3	147.1	+10		3.4	133.7
+18			2.6	146.8	E		2.2	134.8 ✓
W.L.			2.0	147.4	+17		2.4	134.7
2+50 W.L.	9+10.3		2.2	147.2	W.L.		0.9	136.2 ✓
E			1.6	147.8	4+80 W.L.	11+42.3	1.1	136.0 ✓
+2			1.7	147.7	+4		2.6	134.5
+9			0.9	148.5	E		2.6	134.5 ✓
E.L.			0.5	148.9	+2		2.8	134.3
3+00 E.L.	9+62.3		1.1	148.3	E.L.		6.7	130.4 ✓
E			2.3	147.1	5+00 E.L.	11+62.3	8.4	128.7 ✓
W.L.			2.5	146.9	+10		7.0	130.1
3+50 W.L.	10+11.3		3.4	146.0	+17		4.9	132.2
+3			3.7	145.7	E		4.7	132.4 ✓
E			3.0	146.4	+15		4.8	132.3
E.L.			3.0	145.9 ✓	W.L.		2.9	134.2 ✓
4+00 E.L.	10+62.3		8.0	141.4	5+50 W.L.	12+12.3	8.4	128.7 ✓
+15			6.7	142.7	+4		9.8	127.3
E			6.6	142.8 ✓	E		9.5	127.6 ✓
+15			6.7	142.7	+2		9.7	127.4 ✓
W.L.			5.4	144.0 ✓	+8		11.2	125.9 ✓

Plotted 12-1-22
H.P.B.

+ City - 1370.6
143.12

Rst 60' Wide +
10 Cbs
10' 1/2"

City - 1370.6
136.12 Note: See Wood Lane:

Rst 4

E.L.		12.1	124.0
#	1216.5 472	11.72	121.90
6+02.3 = N.L. of Rst (60' Wide)	130.06 136.12	10.7	119.4
+10		9.2	120.9
±		6.9	123.2
+18		5.9	124.2
W.L.		5.0	125.1

See plan on 6+02.3, take add. dist.

E.L. Wood Lane: 0-40

N.L.	10.7	119.4
Cb	11.2	118.9
1/4	11.5	118.6
±	11.6	118.6
1/4	12.3	117.8
Cb	13.3	116.8
S.L.	14.9	115.2

± Wood Lane 0-20

S.L.	11.4	118.7
cb	11.3	118.8
1/4	10.3	119.8
±	8.8	121.3
1/4	8.2	121.7
Cb	8.0	122.1
N.L.	6.9	123.2

W.L. Wood Lane: = 00

N.L.	5.0	125.1
+5	6.0	124.1
cb	6.0	124.1
1/4	6.5	123.6
±	6.9	123.2
1/4	7.4	122.6
cb	8.0	122.1
S.L.	8.5	121.6

Planted 12/1/22
JEB.

+ City - 130.06 136.12		- City - 130.06 136.12		+ City - 130.06 136.12		- City - 130.06 136.12	
							Rst
+50 S.L	5.0	125.1	±			6.4	123.7
CB	4.0	125.1	1/4	+		6.6	123.5
1/4	+	125.6	CB			6.3	123.8
±	3.3	126.8	S.L			6.5	123.6
+2	3.1	127.0	1+50 S.L			12.1	118.0
+5	2.5	127.6	CB			11.0	119.1
1/4	2.0	128.1	1/4	+		9.3	120.8
CB	1.5	128.6	±			8.3	121.8
N.L	0.9	129.2	1/4			6.6	123.5
+75 N.L	0.8	129.3	CB			5.2	124.9
CB	0.9	129.2	N.L			3.5	126.6
1/4	1.5	128.6	1+85 N.L			9.8	120.3
±	2.7	127.4	CB			10.9	119.2
1/4	3.4	126.7	1/4			11.9	118.2
CB	3.7	126.4	±			12.3	117.8
S.L	4.2	125.9	1/4	+		12.9	117.2
+95 S.L	4.4	125.6	CB			13.2	116.9
CB	3.7	126.4	S.L			12.8	117.3
1/4	3.0	127.1	2+100 S.L			10.4	119.7
±	3.0	127.1	CB			11.2	118.9
1/4	2.9	127.2	1/4	+		12.1	118.0
CB	2.8	127.3	±			12.0	118.1
N.L	2.2	127.9	1/4			11.7	118.4
1+25 N.L	3.4	126.7	CB			11.9	118.2
CB	4.7	125.4	N.L			11.3	118.8
1/4	5.7	124.4					

Plotted 12-1-22
HBB

+ City - 13.706 136.12		-	+ City - 148.79 106.98		-	Rst.	6
2125 N.L.		8.4	121.7	1/4		5.3	135.5
Cb		8.7	121.4	Cb		5.4	135.4
1/4		8.8	121.3	N.L.		5.6	135.2
±		8.0	122.1				
1/2	+	5.9	124.3	± Monte Vista N.L.	3139.3	1.5	139.3
Cb		4.9	125.2	±		1.7	139.1
S.L.		4.4	125.7	Cb		4.2	136.6
#	11.22	140.79 146.35 ✓	159.56 135.62 ✓	1/2		4.2	136.6
2150 S.L.		9.4	131.4	±		4.1	136.7
Cb		9.7	131.1	±		2.2	138.6
1/4	+	11.4	129.4	±		1.0	139.8
±		12.9	127.9	1/4	+	1.2	139.6
1/4		13.6	127.2	Cb		2.2	138.6
Cb		13.2	127.6	S.L.		3.2	137.6
N.L.		14.0	126.8	OO = W.L. Monte Vista St.	S.L.	1.5	139.3
3100 N.L.		6.0	134.8	Cb		1.8	139.0
Cb.		5.7	135.1	1/4	+	1.8	139.0
1/4		6.0	134.8	±		1.1	139.7
±		5.4	135.4	±		3.0	137.8
1/4	+	4.3	136.5	1/4		3.0	137.8
Cb		4.0	136.8	±		2.9	137.9
S.L.		3.7	137.1	Cb		2.1	138.7
3109 ± = E.L. Monte Vista St.	S.L.	3.0	137.8	±		1.0	139.8
Cb		3.1	137.7	N.L.		1.0	139.8
1/4	+	4.0	136.8				
±		4.8	136.0				

Plotted 12-1-22
HBB

+ City - 140.79 - 146.81			City - 140.79 146.80			Rst.	7
+50 N.L.	4+19 ³	0.3	140.5	1/4		2.0	138.5
+6		0.5	140.3	+3		1.9	138.9
C6		1.9	138.9	C6		0.4	140.4
1/4		2.1	138.7	N.L.		0.0	140.8
±		1.7	139.1	#	1.76	1.59	139.70 145.26
1/4	+	1.5	139.3	2+25 N.L.	5+94 ³	0.0	141.0
C6		1.6	139.2	C6		0.3	140.7
S.L.		2.0	138.8	+5		0.4	140.6
1400 S.L.	4+169 ³	4.0	136.8	+8		1.6	139.4
C6		2.8	138.6	1/4		1.8	139.2
1/4	+	1.9	138.9	±		2.1	138.9
±		1.5	139.3	1/4	+	2.05	138.5
1/4		2.4	138.6	C6		2.6	137.4
C6		2.2	138.6	S.L.	6+34 ³	4.2	136.8
+2		1.5	139.3	2+65 = E.L. Ocean View 60' Wide:	S.L.	5.0	136.0
N.L.		1.6	139.2	C6		4.5	136.5
1+50 N.L.	5+119 ³	1.6	139.2	1/4	+	4.0	137.0
C6		2.0	138.8	±		3.9	137.1
1/4		2.2	138.6	1/4		4.0	137.0
±		2.4	138.4	+2		4.0	137.0
1/4	+	2.9	137.9	+5		2.7	138.3
C6		3.9	136.9	C6		2.3	138.7
S.L.		4.5	136.3	N.L.		2.1	138.9
2 S.L.	5+169 ³	4.1	136.7	± Ocean View St	N.L.	4.2	136.7
C6		3.0	137.8	C6		4.8	136.2
1/4	x	2.2	138.6	1/4	+	5.7	135.3
±		1.9	138.9				

Plotted 12-1-22
H.P.

+ City - 14896 ✓
147.02

+ City 14896 ✓
147.02

Rst. 8

±	5.8	135.4 ✓	H50 N.L.	$8+44^3 = 8+64^{12}$	10.5	130.5
1/4	6.0	135.0	Cb		11.3	129.7
Cb	6.5	134.5	1/4	+	11.9	129.1
S.L.	7.4	133.6	±		11.8	129.2
00 = W.L. of Ocean View St			1/4		12.1	128.9
S.L.	8.7	132.3	Cb.		12.4	128.6
Cb	8.3	132.7	S.L.		12.3	128.7
1/4	7.6	133.4	#	394	12.09	128.87 134.93 ✓
±	7.2	133.8	2400 S.L.	$8+94^3 = 9+14^{12}$	4.8	128.0
1/4	7.3	133.7	Cb		4.2	128.6
Cb	6.3	134.7	1/4		4.0	128.8
N.L.	6.1	134.9	±		3.9	128.9
0+50 N.C.	8.4	132.6	1/4	+	4.1	128.7
Cb	9.0	132.0	Cb		3.5	129.3
1/4	9.4	131.6	N.L.	$9+59^3 = 9+79^{12}$	3.3	129.5
±	9.6	131.4	265 = EH Escuela St (60' wide)			
1/4	10.0	131.0	N.L.		6.0	126.8
Cb	10.5	130.5	Cb		5.8	127.0
S.L.	10.8	130.2	1/4	+	6.3	126.5
1+00 S.L.	12.9	128.1	±		6.0	126.8
Cb	12.1	128.9	1/4		5.6	127.2
1/4	11.3	129.7	±		4.7	128.1
±	11.0	130.0	Cb		3.7	129.1
1/4	11.0	130.0	S.L.		2.7	130.1
Cb	10.0	131.0	#	11.70	4.7	128.64 ✓ 134.70 ✓
N.L.	9.9	131.1				

Note flow here on Profile plotted to conform to 60' start and not 30' start
 $7+44^3 = 7+64^{12}$

Plotted 12-1-22
HBB

N.E. Cor of Concrete manhole S.E. G&E Co Alley between Escuela & Ocean View St.

		146.39 ✓ 146.45 ✓			
#	12.79	153.10 ✓ 159.16 ✓ 157.56 ✓	0.08	140.31 ✓ 146.37 ✓	
#	5.59	158.02 ✓ 151.80 ✓	6.13	146.97 ✓ 153.03 ✓ 147.35 ✓	
#	9.45	157.86 ✓	10.21	148.91 ✓	
			1.03	150.77 = 150.813 = City Datum	
				156.83 = 156.87 Initial BM	
				V 004	

B. P. Church Step 39th & Rst (Gregory)

101.43
+ 11.29
112.71
- 3.84
108.87
+ 6.96
115.83
- 6.06
109.77 = 115.83 Equation = -6.06

County Highway Commission's line of precise level BM's N^o 1 near west end of paving.

Note Highway Commission's level Datum
corresponds to U.S.G.S Datum. Correct Equation = 6.12
24.23.

Levels for Cross Streets Cont.
Page 13.

✓ 24.23.

Levels on proposed Columbia St sewer extension from Upas to Glenwood Drive;
See page 12 for sketch:

DONNAN
MILLER
SIGHTS
WALBRECK
NOV 23-22

See page 17 for grades

	+	π	-	
B.M. N.W. Cor Willow & India B.F.			70.06	Manhole (side to Bay road)
	12.92	82.78	2.16	80.82 = + on
	13.3A	93.16		
Flow line at manhole			17.44	75.72
0+67			11.7	81.5
0+50			5.6	87.6
0+30			0.5	92.7
#	12.45	105.61	0.00	93.16
0+25			11.7	94.4
0+05			6.5	99.1
00 N.L. of Vine St.			3.4	102.7
#	12.45	117.68	2.38	105.23
14' N of ± of Vine St			6.1	111.6
± Vine St:			5.9	111.8
3+05 ⁹⁸ = S.L. of Vine St:			5.6	112.1
Check on Curb S.E. Cor Vine & Columbia			4.65	113.03
" " B.M. Spoke Electric light pole S.W. Cor. Vine & Columbia (Gregory)			5.19	112.49
3+00			5.0	112.7
2+50			4.4	113.3
2+00			4.0	113.7
1+50			3.5	114.2
1+00			3.2	114.5
0+50			2.7	115.0
00 = N.L. Upas St.			1.5	116.2

Bench Line on Catalina Blvd.

+ + -

DENNAN
MILLER
SIGHTS
WALBRECK

11

NW Cor Verona & Catalina B.P. 250.17

NOV 23-22:

10.15 260.32[✓] 250.17

7th TEL Pole North from Cañon Road to Catalina intersection.

2 1/2 miles East side of Road: 2 nails 1.25 259.07 B.M. nails

3.27 262.67[✓] 0.92 259.40[✓]

0.92 262.37[✓] 1.22 261.45[✓]

Mon B.P. Appx 12' West of Auto Club sign post
Cañon Road: West side Catalina Blvd: 0.74 261.63 B.M. Mon:

0.48 253.45[✓] 9.40 252.97[✓]

4.71 255.51[✓]

highest rock in headwall of Culvert 9.65 243.80 B.M. Rock

Appx 600' West Cañon Road: Over pipe: West side Catalina:

11.78 267.16[✓] 0.13 255.38[✓]

West B.M. in 10' x 10' opposite Main entrance
Theosophical gate on East side road: 5.68 261.48 = 261.41 West B.M.

12.20 277.81[✓] 1.55 265.61[✓]

2 miles in a Go Slow Look out for pedestrians sign-
post; E side of road, Appx 500' S of Main gate to
Theosophical grounds:

5.13 272.68[✓] 2 nails

12.88 290.39[✓] 0.30 277.51[✓]

8.23 298.35[✓] 0.27 290.12[✓]

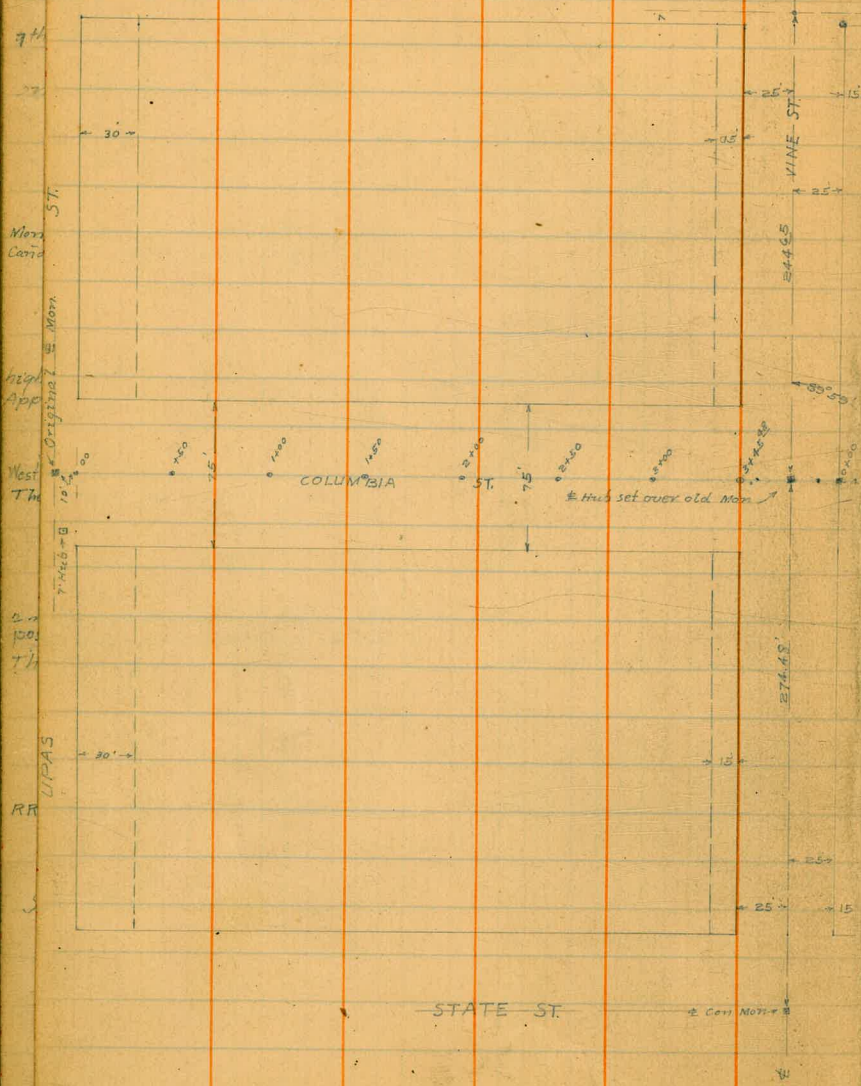
RR Sph South past of Egyptian Gate: 2.35 296.00 2nd West B.M.

See also Book 1072 page 75:

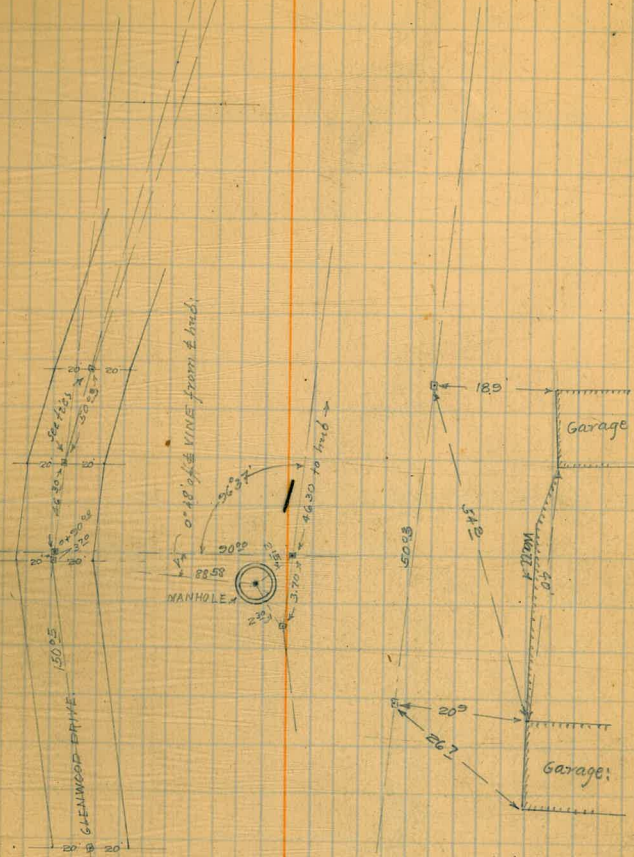
SURVEY FOR EXTENSION OF SEWER ON COLUMBIA FROM LIPAS TO
 GLENWOOD DRIVE! See page 10 for level notes.

DOXMAN
 MILLER
 SIGHTS
 WALBYECK.

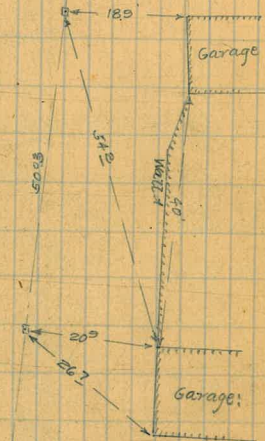
INDIA ST. NOV 23-22



74
 ST.
 Mon
 Carr
 High
 App
 West
 Th
 7
 100
 74
 LIPAS
 RR



0.18' 1/2' VINE from 2' bed.



Q Street

± Q St. 20' Wide.

EI.

Station	Offset	Height	Distance	Elevation
	0.48	151.27 [✓]		150.81
	3.50	153.04 [✓]	1.75	149.54 [✓]
00 = W.L. Wood Lane			7.7	145.8
+ 25			7.6	145.4
+ 50			5.8	147.2
1+00			5.6	147.4
1+75			7.7	145.3
2+00			7.7	145.3
2+50			8.5	144.5
3+00			8.3	144.7
3+09 ⁰⁰ = E.L. Monte Vista St. (60' wide)			8.1	144.9
±	2.37	148.40 [✓]	6.96	146.08 [✓]
± Monte Vista St	3+39 ³		2.5	146.0
00 = W.L. Monte Vista St	3+69 ³		1.8	146.7
+ 50	4+19 ³		1.2	147.3
1+00	4+69 ³		2.3	145.2
1+50	5+19 ³		4.5	144.0
2+00	5+69 ³		6.2	142.3
2+65 = E.L. Ocean View St (60' wide)	6+34 ³		10.4	138.1
± Ocean View	6+64 ³		12.3	136.2

✓

13

EI 150813

Highway Commission BM # 6 U.S.G.S. EI = 156873 = City Datum

See page 2 for Levels on Wood Lane.

Plotted
Dec 13 1922

\pm Ocean View St (across).
 \pm Ocean View St.

	+	π 148.45	-	
00 = S.L. Q St.		148.45	12.0	136.5
+50			11.4	137.1
1+00			11.7	136.8
1+50			11.7	136.8
2+00			11.5	137.0
#	3.30	140.26	11.49	136.96
2+50			9.0	136.3
3+00			4.6	135.7
+50			5.3	135.0
4+00			6.0	134.3
+50			5.3	135.0
5			4.7	135.6
+50			4.0	136.3
6+00 = N.L. R st			4.5	135.8
#	5.90	134.55	11.61	128.65 = 128.64

going East.

see Enl. Page 8

00 = S.L. Rst \pm of Ocean View to the North produced South.

00	6+67 ³	1.0	133.6
+50	7+17 ³	3.4	131.2
1	7+67 ³	5.6	129.0
+50	8+17 ³	6.3	128.3
2	8+67 ³	7.6	127.0
+50	9+17 ³	8.1	126.5
3	9+67 ³	8.7	125.9
+50	10+17 ³	10.3	124.3
4	10+67 ³	13.0	121.6

✓

14

	+	π 134.55	-	
#	1.68	123.46	12.77	121.78
4+50	11+17 ³		6.0	117.5
5	11+67 ³		8.3	115.2
+50	12+17 ³		9.5	114.0
6+00 = N.L. Urban St.	12+67 ³		9.3	114.2

Plotted
Dec 13, 1928
J.B.

Monte Vista St

	+	+	± Monte Vista St (60' wide)	
	12.94	123.46	0.21	123.25
00 = N.L. Urban St 12+64.9		136.17		
+50	12+14.9		10.0	126.2
+70	11+94.9		7.9	128.4
1+00	11+64.9	11+60	5.3	130.9
+50	11+14.9		4.4	131.8
2	10+64.9	11+10	2.9	133.3
+50	10+14.9		0.8	135.4
3	9+64.9		2.0	134.2
+50	9+14.9		2.5	133.7
+75	8+89.9		4.6	131.6
4	8+64.9		3.5	132.7
+50	8+14.9		4.2	132.0
5	7+64.9		3.9	132.3
#	12.30	148.40	1.6	134.6
			0.07	<u>136.10</u>
+50	7+14.9		11.2	137.2
6 = S.L. Rst	6+64.9		10.9	137.5
00 = N.L. Rst	6+04.9		9.5	138.9
+50	+54.9		10.0	138.4
1+00	5+04.9		8.8	139.6
1+50	+54.9		9.2	139.2
2+00	4+04.9		8.6	139.8
+50	+54.9		6.9	141.5
3	3+04.9		5.5	142.9
+50	+54.9		5.0	145.4
4	2+04.9		2.2	146.2

148.40

15

+50	1+54.9	1.7	146.7
5	1+04.9	3.3	145.1
+50	+54.9	3.7	144.7
6+ ⁰⁰ = S.L. Rst	00	1.1	147.3
#		2.40	146.00 = 146.09

Plotted
Dec 13, 1974

Rst along Division Line.

R^o Sta from Wood Lane East.

See T.P. Page 15

	1.96	138.06	136.10		
#	1.42	126.74	127.9	125.32	
00 = EL. Wood Lane Ave.			7.6		119.1
150				16.0	110.7
175				16.9	109.9
182				21.8	104.9
190				16.9	109.9
1400				12.4	114.3
1440				5.9	120.8
1465				3.4	123.3
2100				0.0	126.7

✓

Plotted
Doc
3/1

1/4/23 Gregory
Miller
Moore
Shaw

Sewer Construction
to Columbia
from 40' N. of N.L. Ugas to
M.H. & Glenwood Drive
see page 10 for preliminary

330
11358
24358

91.00
27.00

17

Grade

	4.58	117.07		112.49		
0+00 D.E. 40' N. of Ugas			1.53	115.24	108.50	+6.74
+30			2.48	114.59	108.04	+6.55
1			2.77	114.30	107.59	+6.71
+50			3.78	113.79	107.13	+6.66
2			3.80	113.27	106.68	+6.59
+50			4.30	112.77	106.22	+6.55
3			4.88	112.19	105.77	+6.42
+30 M.H. & Ugas Δ 0°28'R.			5.13	111.94	105.50	+6.44
+50	0.28	106.27	11.08	105.99	99.29	+6.70
	0.41	93.88	12.80	93.87		
4			4.40	89.48	83.78	+5.70
+18.58 break			10.83	83.05	78.0	+5.05
+43.58 M.H. & Glenwood.					75.72	

6/8/73 Gregory
 CROSS SECTION OF
 CENTER 30' dx LAMONT ST
 FROM SL GRAND S.

51.44 18.

N.B. { E = 15' E dx C
 W = 15' W dx C dx Lamont

1.05 51.42 50.37
 S. L. GRAND. Produced from the West

W	3.7	47.7
+5	3.8	47.6
C	4.3	47.1
+10	4.3	47.1
E	4.4	47.0

25' S

E	5.3	46.1
+5	5.8	45.6
C	5.6	45.8
+10	5.6	45.8
W	5.5	45.9

65' S

W	6.9	44.5
+5	6.5	44.9
C	6.3	45.1
+10	6.6	44.8
E	6.0	45.4

100' S

E	6.6	44.8
+5	7.0	44.4
C	6.6	44.8
+10	7.0	44.4
W	7.1	44.3

150' S

W	7.6	43.8
+5	7.5	43.9
C	7.2	44.2
+10	7.6	43.8
E	8.1	43.3

200' S

E	9.1	42.3
+5	8.1	43.3
C	7.9	43.5
+10	8.1	43.3
W	8.2	43.2

T.P. 27.5 45.34
 271' S = N.L. Thomas 80' wide

W	3.0	42.3
+5	2.7	42.6
C	2.4	42.9
+6	2.8	42.5
+10	3.1	41.9
E	4.0	41.3

311' S Thomas

E	4.0	41.3
+5	3.6	41.7
+10	3.0	42.3
C	2.8	42.5
+10	3.2	42.1
W	3.5	41.8

45.34

S. L. Thomas

W	4.0	41.3
+5	3.6	41.7
C	3.3	42.0
+5	3.5	41.8
+10	4.1	41.2
E	4.7	40.6

50' S

E	5.5	39.8
+5	4.9	40.4
+10	4.1	41.2
C	4.0	41.3
+10	4.3	41.0
W	4.7	40.6

100' S

W	4.7	40.6
+5	4.6	40.7
C	4.5	40.8
+5	4.6	40.7
+10	5.6	39.7
E	6.0	39.3

150' S

E	6.4	38.9
+5	5.5	39.8
+10	4.9	40.4
C	4.6	40.7

45.34

LAMONT

19

+10	4.7	40.6
W	4.8	40.5

200' S

W	4.8	40.5
+5	4.6	40.7
C	4.4	40.9
+5	4.6	40.7
+10	5.3	40.0
E	6.3	39.0

270' S = N.L. Reed 80' wide

E	6.1	39.2
+5	5.4	39.9
+10	4.5	40.8
C	4.4	40.9
+10	4.7	40.6
W	5.0	40.3

d Reed

W	5.0	40.3
+5	4.7	40.6
C	4.1	41.2
+7	4.4	40.9
+10	4.9	40.4
E	5.2	40.1

S.L. Reed

E	5.0	40.3
+5	4.5	40.8

4534

+10	4.0	413
C	4.1	412
+10	4.6	407
W	5.0	403
50' S		
W	5.0	403
+5	4.5	408
C	3.8	415
+5	3.9	414
+10	4.4	409
E	5.1	402
100' S		
E	4.8	405
+5	4.3	410
+10	4.0	413
C	4.0	413
+10	4.4	406
W	5.1	402
150' S		
W	5.1	402
+5	4.7	406
C	4.2	411
+5	4.2	411
+10	4.7	406
E	5.2	40.1
		✓

4534

LAMONT 70

300' S		
E	5.2	40.1
+5	4.7	40.6
+10	4.3	41.0
C	4.3	41.0
+5	4.9	40.4
W	5.3	40.0
270' S = NL OLIVER 80' wide		
W	5.6	39.7
+5	4.9	40.4
C	4.5	40.8
+5	4.5	40.8
+10	4.9	40.4
E	5.5	39.8
TP	0.22 4103	4.53 40.81
OLIVER		
E	0.9	40.1
+5	0.5	40.2
+10	0.3	40.7
C	0.3	40.7
+5	0.5	40.5
+10	0.9	40.1
W	1.2	39.8
S. L. OLIVER		
W	1.9	39.1
+5	1.5	39.5
		✓

41.03

+10	1.0	40.0
C	0.8	40.2
+7	0.9	40.1
+10	1.3	39.7
E	1.6	39.4
50' S		
E	2.5	38.5
+5	1.9	39.1
+8	1.5	39.5
C	1.5	39.5
+10	2.0	39.0
W	2.6	38.4
95' S		
W	3.3	37.7
+5	3.0	38.0
C	2.4	38.6
+7	2.3	38.7
+10	2.6	38.4
E	3.0	38.0
100' S		
E	3.1	37.9
+5	2.8	38.2
+8	2.5	38.5
C	2.5	38.5
+10	3.2	37.8
+14	3.3	37.7

4103

LAMONT.

21

W	4.5	36.5
+2	4.6	36.4
+3	3.1	37.9
150' S		
-2	4.8	36.5
-1.5	5.3	35.7
W	5.5	35.5
+1	4.5	36.6
+5	4.0	37.0
C	3.6	37.4
+7	3.7	37.3
+10	4.0	37.0
E	4.4	36.6
200' S		
E	5.4	35.6
+5	5.1	35.9
+10	4.8	36.2
C	4.9	36.1
+8	5.1	35.9
+10	5.4	35.6
+13.5	5.8	35.2
W	6.5	34.5
+2	5.8	35.2
250' S = NL Pacific ^{on East} 60 mids		
-2	7.3	33.7
W	7.7	33.3

4103

+5	6.8	34.2
+7	6.5	34.5
C	6.1	34.9
+8	6.4	34.6
+10	7.0	34.0
E	7.0	34.0

Pacific

E	7.7	33.3
+5	7.3	33.7
+8	6.8	34.2
C	6.9	34.1
+7	7.2	33.8
+10	7.6	33.4
W	8.0	33.0

5 L Pacific on East = 0+00

W	8.8	32.2
+5	8.6	32.4
+7	8.2	32.8
C	7.7	33.3
+6	7.7	33.3
+10	8.2	32.8
E	8.4	32.6

50' S

E	9.5	31.5
+5	9.5	31.5
+7	9.1	31.9

4103

LAMONT.

72

E	9.2	31.8
+10	9.6	31.4
W	9.7	31.3

100' S

W	11.0	30.0
+5	10.9	30.1
C	10.4	30.6
+7	10.1	30.9
+10	10.8	30.2
E	11.1	29.9

150' S

E	12.5	28.5
+5	12.2	28.8
+9	11.6	29.4
C	11.8	29.2
+10	12.4	28.6
W	14.5	28.5
T.P.	12.6 30.08	12.21 28.82

200' S

W	3.1	27.0
+5	3.1	27.0
C	2.6	27.5
+10	2.6	27.5
E	3.3	26.8

250' S

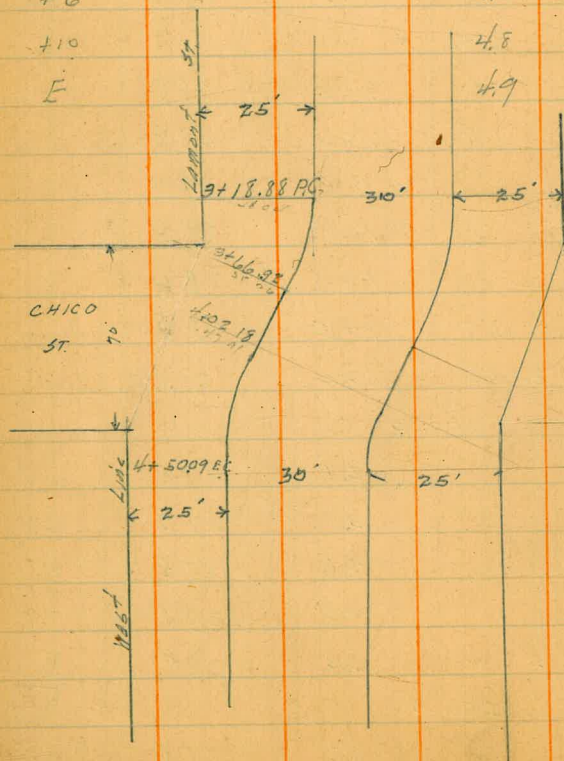
E	4.6	25.5
---	-----	------

3008

+5	3.7	26.4
C	3.8	26.3
+7	3.8	26.3
+10	4.0	26.1
W	4.0	26.1

318.88 S = PC see sketch

W	5.2	24.9
+5	5.1	25.0
C	4.5	25.6
+6	4.4	25.7
+10	4.8	25.3
E	4.9	25.2

35010
3421
340
1823

3008

LAMONT 23

3 + 42.90 = Cox Curve

E	5.4	24.7
+5	5.3	24.8
+10	5.0	25.1
C	5.1	25.0
+10	5.4	24.7
W	5.4	24.7

3 + 66.92 = EC

W	5.6	24.5
+5	5.6	24.5
C	5.7	24.4
+10	5.7	24.4
E	6.1	24.0

4 + 02.18 = PC

E	6.1	24.0
+5	6.0	24.1
C	6.0	24.1
+10	6.0	24.1
W	6.1	24.0

4 + 26.13 = CC

W	6.5	23.6
+5	6.5	23.6
C	6.3	23.8
+10	6.2	23.9
E	6.4	23.7

30.08

4450.09 = EC ✓

E			6.5	23.6	
+5			6.6	23.5	
C			6.9	23.2	
+10			6.9	23.2	
W			6.8	23.3	
21 B.M.	1.12	2613	5.07	25.01	sw chico. + Lamont. 436
		5400			
W			3.6	22.5	
+5			3.6	22.5	
C			3.5	22.6	
+10			3.1	23.0	
E			3.0	23.1	
		5450			
E			3.8	22.3	
+5			4.0	22.1	
C			4.4	21.7	
+10			4.6	21.5	
W			4.4	21.7	
		6400			
W			5.2	20.9	
+5			4.9	21.2	
C			4.5	21.6	
+10			4.4	21.7	
E			4.3	21.8	✓

76.13

LAWMONT 6.11.93

24

6+25.93 = NL. Sunset Ave 75 St. ✓

E			4.6	21.5	
+5			4.7	21.4	
C			4.9	21.2	
+10			5.5	20.6	
W			5.8	20.3	
		6+63			
W		center	Sunset.		
		37.5			
		70093			
W			6.3	19.8	
+5			5.8	20.3	
C			5.7	20.4	
+10			5.5	20.6	
E			5.6	20.5	
		7400	5.1	Sunset.	-0+00
E			6.2	19.9	
+5			6.3	19.8	
C			6.3	19.8	
+8			6.0	20.1	
+10			6.3	19.8	
W			6.7	19.4	
		0+50			
W			7.6	18.5	
+5			7.4	18.7	
+10			6.8	19.3	
C			6.9	19.2	
+5			6.8	19.3	
E			6.6	19.5	✓

26.13

1+00

E	6.8	19.3
+5	7.0	19.1
C	7.5	18.6
+10	7.8	18.3
W	7.9	18.2

1+50

W	7.8	18.3
+5	7.5	18.6
C	7.3	18.8
+10	6.9	19.2
E	6.8	19.3

2+00

E	6.1	20.0
+5	6.0	20.1
C	6.7	19.4
+10	7.1	19.0
W	7.5	18.6

2+50

W	6.2	19.9
+5	6.0	20.1
C	5.6	20.5
+10	5.4	20.7
E	5.4	20.7

26.13

LAMONT

25

3+00

E	4.6	21.5
+5	4.7	21.4
C	5.0	21.1
+10	5.4	20.7
W	5.9	20.2

3+50

W	5.2	20.9
+5	4.5	21.6
C	4.1	22.0
+10	3.9	22.2
E	3.8	22.3

4+00

E	3.5	22.6
+5	3.5	22.6
C	3.6	22.5
+10	4.4	21.7
W	4.9	21.2

4+50

W	4.3	21.8
+5	3.8	22.3
C	3.4	22.7
+10	3.6	22.5
E	3.7	22.4

36.13

5+00

E	3.7	22.4
+5	3.6	22.5
C	3.5	22.6
+10	3.8	22.3
W	4.2	21.9

5+50

W	4.4	21.7
+5	4.1	22.0
C	3.7	22.4
+10	3.6	22.5
E	3.5	22.6

6+00 = N.L. Roosevelt Ave 75' wide

37.5

E	3.9	22.2
+5	3.9	22.2
C	4.1	22.0
+10	4.3	21.8
W	4.5	21.6

6+37.5 center Roosevelt

W	4.8	21.3
+5	4.5	21.6
C	4.4	21.7
+10	4.3	21.8
E	4.3	21.8
T.P.	3.16	23.74
		5.55
		20.58

23.74

LAMONT

26

6+75 S.L. Roosevelt = 0+00

E	2.2	21.5
+5	2.2	21.5
C	2.4	21.3
+10	2.7	21.0
W	3.0	20.7

0+50

W	3.3	20.4
+5	3.0	20.7
C	2.8	20.9
+10	2.6	21.1
E	2.6	21.1

1+00

E	3.1	20.6
+5	3.1	20.6
C	3.3	20.4
+10	3.6	20.1
W	3.9	19.8

1+50

W	4.8	18.9
+5	4.5	19.2
C	3.9	19.8
+10	3.9	19.8
E	3.8	19.9

23.74

2400

E	4.9	18.8
+5	4.6	19.1
C	4.8	18.9
+10	5.1	18.6
W	5.6	18.1

see paring plans for curve 2 + 23.35 = PC.

W	5.8	17.9
+5	5.2	18.5
+10	4.9	18.8
C	5.0	18.7
+10	4.9	18.8
E	✓ 4.9	18.8

2 + 96.43 = CC

E	6.0	17.7
+5	6.3	17.4
+13	6.6	17.1
C	6.0	17.7
+10	5.2	18.3
W	✓ 5.4	18.3

3 + 29.52 = FC

W	5.5	18.2
+5	5.7	18.0
+12	5.7	18.0
C	6.1	17.6
+10	5.7	18.0

23.74

27

E	5.9	17.8
3 + 50		
E	5.7	18.0
+5	5.6	18.1
C	5.7	18.0
+10	5.7	18.0
W	5.2	18.5

4400

W	4.9	18.8
+5	5.1	18.6
C	5.2	18.5
+10	5.1	18.6
E	✓ 5.0	18.7

4 + 40.18 = PC

E	4.8	18.9
+5	4.8	18.9
C	4.9	18.8
+10	4.9	18.8
W	4.5	19.2

2 + 46.38 = CC

W	4.5	19.2
+5	4.3	19.5
C	4.5	19.2
+10	4.2	19.5
E	4.3	19.4

See page 51 for Antipodal Sections on paring plans

See pages 50-53 for interpolated Sections

4374

5+52.58 = E.C.

E	2 19.53	40	19.7
+5	7.2	40	19.7
C		39	19.8
+10		40	19.7
W		38	19.9
TP	7.63	37.71	36.6
		6+00	20.08 on hub E.C.
W		7.6	20.1
+5		7.5	20.2
C		7.5	20.2
+10		7.9	19.8
E		7.8	19.9
		6+50	
E		7.6	20.1
+5		7.3	20.4
C		7.1	20.6
+10		7.5	20.2
W		7.4	20.3
		6+62.5 = curb	
W-16		6.75	20.96
		7+00	
W-16 = curb		6.26	21.45
W		7.0	20.71
+5		6.9	20.81
C		6.7	21.0

27.71

LAMONT.

28

+10		6.7	21.0
E		7.1	20.6
		7+50	
E		6.5	21.2
+5		6.3	21.4
C		6.2	21.5
+5		6.5	21.2
+10		6.1	21.6
W		6.2	21.5
+18 = curb.		5.51	22.20
		7+72.13 = P.C.	
-1.9 = curb. Top		5.16	22.55
W		5.6	22.1
+5		6.2	21.5
C		5.8	21.9
+10		6.2	21.5
E		6.4	21.3
		8+09.65 = E.C.	
E		5.8	21.9
+5		5.5	22.2
C		5.6	22.1
+10		5.7	22.0
W		5.6	22.1
		8+50	
W		5.3	22.4
+5		5.3	22.4

See pages 50-53 for Corrected Stations + Interpolated Sections

2771

29

C		4.8	229
+10		5.2	225
E		5.2	225
	9+00		
E		4.6	231
+5		4.5	232
C		4.3	234
+10		4.1	236
W		4.3	234
	9+50		
-20		3.5	242
-10		3.5	242
W		3.9	238
+5		4.0	237
C		3.9	238
+10		4.0	237
E		4.0	237
	(9+75.4 = E.L. Kendall.)		
-59 (-25)	= edge of curb	4.3	234
E		4.1	236
+5		3.5	242
C		3.7	240
+10		3.6	241
W		3.6	241
(+15)		3.2	245
(+25)		2.8	249
	= Top Curb N.W. Kendall.	2.95	2476

See pages 50-53 for corrected
Stations + Interpolated Sections

✓

6/12/23

Gregory
P. Miller

Survey of
12th St. Paving in
Balboa Park

30

12

14.5 38.5

11

433.58

15' 23'

10

20' 20'

9

7' 30'

8

Δ 36°45' R.

18.5
26
26
19' 40'
35'

7

5' 35'

6

477.1

18' 21'

5

20' 20'

3+25 Δ 19°36' L.

Platted
June 16 1923
G.P.M.

Edge of Road → 31' 12' ← Edge of Road

325'

0+00 = Edge of Paving East Entrance Exposition

See page 54 for Paving N. of 0+00

24

✓

23

22 $\Delta 25^\circ 12' L$

21

20

19 + 7.53

18 + 06.5
 $\frac{1}{2}$ 926

17

16

15

14

13

12 + 33.85 $\Delta 48^\circ 27\frac{1}{2}' R$

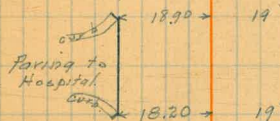
1' 35'

12 22.5

34' $\frac{1}{2}$ 1' $\frac{1}{2}$ to 1/2

20.5 14.5

18' 14'



18.20 19'

18.5 19

18.5 18'

15.5 21.5

6' 32'

12 36.5

Edge of Road

36 Δ 17° 15' R.

35

34

816 90'

33

32

31

30

29

$26 + 83.10 =$
 $27 + 83.10 \Delta 30^\circ 15' L$ } Equation

26

483 10

25

37
33

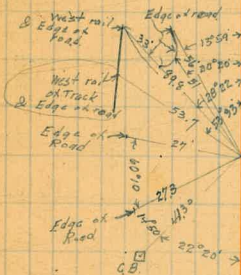
32 ✓

Edge of Road \rightarrow 0.0 \leftarrow 34' \leftarrow Edge of Road

36 47
14 47

22 44
07 16
37 03
6 009

10.5 \leftarrow Edge of Road



20 \leftarrow Edge of Road

17

18

18

19.5

18

19.5

18

19.5

20

14.5

35 Δ

0.0

13

21.5

1'

34'

45

44

43

41 + 87.5

40 + 77 A 28'48" R

40

39 + 41

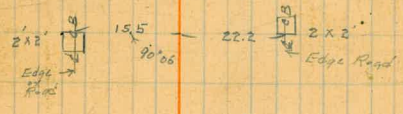
38

37

Edge → 20.5 16.5 ← Edge

Edge → 17.5 19.5 ← Edge

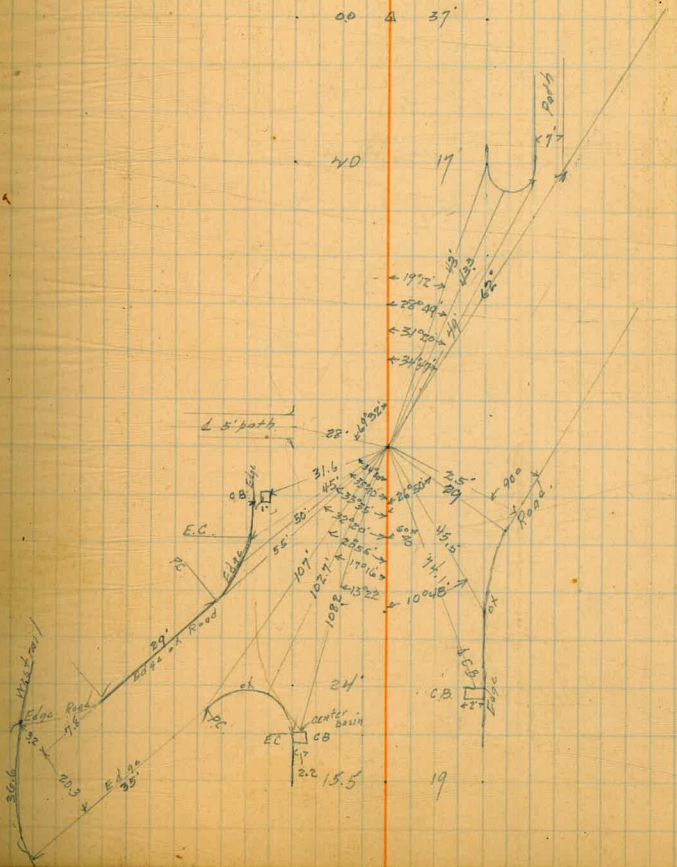
Edge → 18.5 18.5 ← Edge



00 37

40

17



53

52 + 56

52 + 50

52

51 + 44 Δ $32^{\circ}25'$ L

51

50

49

48 + 23.5

48 + 18

47

46 + 19 Δ $27^{\circ}38\frac{1}{2}'$ LEdge \rightarrow 20' 17' Edge
 \leftarrow 15.5 $\begin{matrix} 22 \\ \square \\ 3 \times 2 \text{ CB} \end{matrix}$ \leftarrow Edge cross
 3x2 CB
Edge \times $\begin{matrix} 26 \\ \square \\ 2 \times 2 \text{ CB} \end{matrix}$ 20.3Edge \rightarrow 25' 12' \leftarrow EdgeEdge \rightarrow 37' 00' \leftarrow EdgeEdge \rightarrow 26.5' 11' \leftarrow EdgeEdge \rightarrow 8' 29' \leftarrow EdgeEdge \rightarrow 0.5' 36'
 \leftarrow 34' $\begin{matrix} 13.5 \\ \square \\ 2 \times 2 \text{ CB} \end{matrix}$
 $\begin{matrix} 2 \times 2 \text{ CB} \\ \square \\ 2' \end{matrix}$ \times $\begin{matrix} 19.5 \\ \square \\ 2' \end{matrix}$

18' 19.5

Edge \rightarrow 38' 00' \leftarrow Edge

FOR LAYOUT OF 12th ST
INTERSECTION SEE NEXT PAGE

55+00.23 Δ 7°41' R. to Line 30' E. of W. L. 12th St.

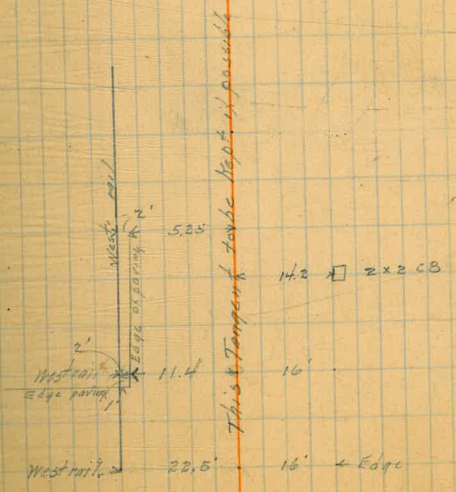
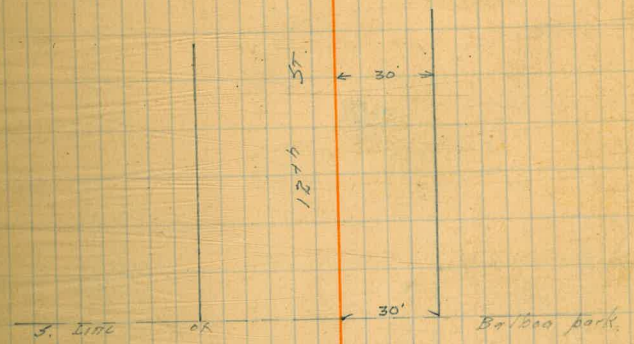
54+50

54+22

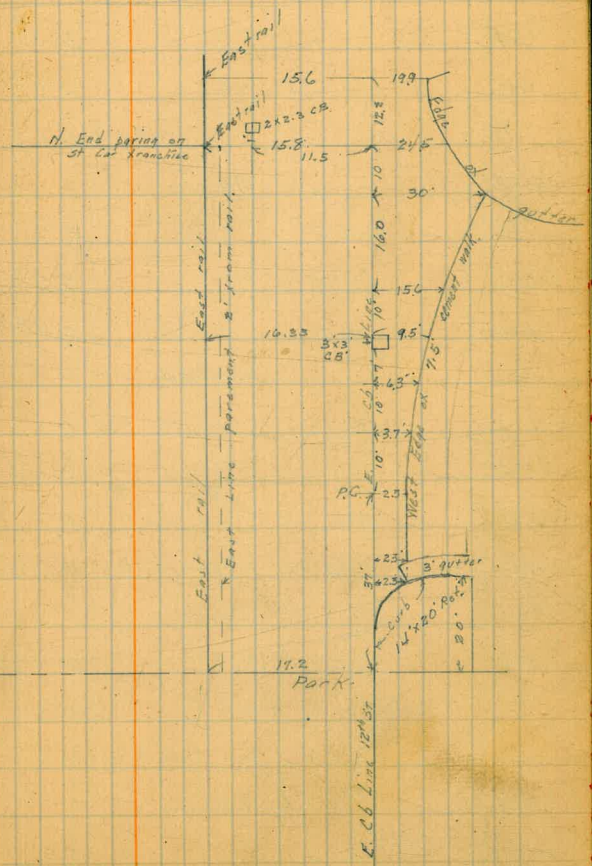
54

53+35 Δ 3°51' L

Platted June 16 1913
H.C.B.



Plotted June 11, 1933
S.H.S.



S. L. Balboa

14.2 Park

6/21/23

CROSS SECTION OF

12th St

Roadway in Balboa Park

Roadway taken 30' wide i.e. E = 15' East 80' NW
W = 15' West 12th + 4'

27

B.M.

12.97

118.44

705.47

12th + 4'

W

8.3

144.8

+3.5

8.5

144.6

0+00 = S.L. Balboa Park.

16' W. of L

109.54

8.90

109.54 on paving

3+00

L

110.63

7.77

110.63

-3.5

125.1

6.5

144.6

2' E

110.73

7.67

110.73 next rail

W

125.2

6.1

145.0

0+50

C

125.5

5.6

145.5

5.4 E of L

110.75

5.13

113.31 edge paving

E

125.2

6.2

144.9

L

110.75

5.3

113.1

+3.5

125.1

6.5

144.6

W

6.1

114.3

3+50

115.4

1+00

-3.5

127.35

4.3

144.8

W

115.5

3.5

114.9

E

127.45

4.1

146.0

C

115.75

2.7

115.7

C

127.75

3.5

147.6

11.4 E

116.0

3.45

115.99 edge paving

W

127.45

4.1

147.0

1+50

+3.5

127.35

4.4

146.7

15' E of L

118.35

0.3

118.1

4+00

C

118.37

0.1

118.3

-3.5

129.6 - 2

2.1

149.0

15' W of L

118.1

0.8

117.6

W

129.7 + 1

1.7

149.4

T.P.

12.82

131.12

0.14

118.30

C

130.0 + 4

1.1

130.0

2+00

120.6

E

129.7 + 1

1.7

149.4

W

120.7

10.7

120.4

+3.5

129.6 + 1

1.8

149.3

C

121.0

10.1

121.0

T.P.

127.4 143.61

0.25

130.87

E

120.7

10.5

120.6

4+50

120.6

2+50

-3.5

11.9

131.7

-3.5

8.5

144.6

E

11.6

132.0

E

8.2

144.9

C

11.1

132.5

C

7.7

143.4

W

11.7

131.9

+3.5

11.9

131.7

143.61

5+00

-3.5		9.7	133.9
W		9.2	132.4
C		8.7	134.9
E		9.2	132.4
+3.5		9.5	132.1

5+50

-3.5		7.3	136.3
E		7.0	136.6
C		6.4	137.3
W		6.9	136.7
+3.5		7.2	136.4

6+00

-3.5		5.1	138.5
W		4.7	138.9
C		4.1	139.5
E		4.5	139.1
+3.5		4.8	138.8

6+50

-3.5		2.6	141.0	
E		2.3	141.3	
C		1.8	141.8	
W		2.2	141.4	
+3.5		2.4	141.4	
T.P.	12.70	156.16	0.15	143.46

12+00

38

7+00

-3.5		13.1	143.0
W		12.7	143.4
C		12.0	144.1
E		12.5	143.6
+3.5		12.8	143.3

7+50

-3.5		10.6	145.5
E		10.1	145.0
C		9.7	146.4
W		10.2	145.9
+3.5		10.7	145.4

8+00

-3.5		8.4	147.7
W		7.9	148.4
C		7.3	148.8
E		7.9	148.4
+3.5		8.2	147.9

8+50

-3.5		5.7	150.4
E		5.5	150.6
C		5.0	151.1
W		5.6	150.5
+3.5		6.0	150.1

9+00

-3.5		3.6	151.5
------	--	-----	-------

156.16

W			3.0	153.1
C			2.4	153.7
E			3.0	153.1
+3.5			3.3	154.8
		9+50		
-3.5			0.8	155.3
E			0.6	155.5
C			0.0	156.1
W			0.5	155.6
+3.5			0.9	155.5
T.P.	12.91	168.81	0.26	155.90
		10+00		
-3.5			11.3	157.5
W			10.9	157.9
C			10.4	158.4
E			11.0	157.8
+3.5			11.2	157.6
		10+50		
-3.5			8.7	160.1
E		✓	8.4	160.4
C			8.0	160.8
W			8.5	160.3
+3.5			8.9	159.9
		11+00		
-3.5			6.4	164.4
W			6.0	164.8

12th St. 39

C			5.5	163.3
E			6.0	164.8
+3.5			6.4	164.4
		11+50		
-3.5			3.9	164.9
E			3.5	165.3
C			3.1	165.7
W			3.6	165.4
+3.5			3.9	164.9
		12+00		
-3.5			1.2	167.6
W			0.9	167.9
C			0.4	168.4
E			0.9	167.9
+3.5			1.3	167.5
T.P.	12.76	181.47	0.10	168.71
		12+50		
-3.5		✓	11.4	170.0
E			11.0	170.4
C			10.6	170.8
W			11.1	170.3
+3.5			11.3	170.1
		13+00		
-3.5			8.4	173.0 = CB
W			8.3	173.1
C			8.1	173.3

181.47

E	8.5	174.9	
+3.5	8.6	174.8	= C.B.
	13+50		
-3.5	6.6	174.8	
E	6.3	175.1	
C	5.7	175.7	
W	6.2	175.1	
+3.5	6.4	175.0	
	14+00		
-3.5	4.5	176.9	
W	4.1	177.3	
C	3.7	177.7	
E	4.2	177.1	
+3.5	4.5	176.9	
	14+50		
-3.5	2.8	178.6	
E	2.2	179.1	
C	1.9	179.5	
W	2.3	179.1	
+3.5	2.5	178.9	
	15+00		
-3.5	0.9	180.5	
W	0.7	180.7	
C	0.2	181.1	
E	0.5	180.9	
+3.5	0.8	180.6	

12th St.

40

T.P.	12.57	193.95	0.09	181.38
		15+50		
-3.5			11.7	181.1
E			11.5	181.4
C			11.3	181.6
W			11.8	181.1
+3.5			11.9	181.0
		16+00		
-3.5			10.7	183.1
W			10.5	183.4
C			10.0	183.9
E			9.9	184.0
+3.5			10.0	183.9
set B.M.			9.70	184.25
		16+50		
-3.5			8.9	185.0 on C.B.
E			8.8	185.1
C			8.7	185.1
W			9.2	186.7
+3.5			9.6	186.3
		17+00		
-3.5			7.8	186.1
W			7.4	186.5
C			7.1	186.8
E			7.5	186.1
+3.5			7.8	186.1

193.95

17+50

-3.5	6.1	187.8
E	5.7	188.1 ✓
C	5.6	188.3
W	5.9	188.0
+3.5	6.3	187.6

18+00

-3.5	4.4	189.5
W	4.0	189.9
C	3.7	190.2 ✓
E	4.1	189.8
+3.5	4.5	189.4

18+50

-3.5	2.7	191.2 ✓
E	2.2	191.7
C	2.0	191.9
W	2.5	191.2 ✓
+3.5	2.9	191.0

19+00

-3.5	1.4	192.5 ✓
W	0.8	193.1
C	0.3	193.6
E	0.4	193.5 ✓
+3.5	0.7	193.2 ✓
T.P.	13.27	209.13
	0.09	193.86

12+4 ST

41

19+50

-3.5	12.1	195.0
E	11.8	195.3
C	11.6	195.5
W	12.0	195.1
+3.5	12.4	194.7

20+00

-3.0	10.4	196.7
W	10.0	197.0
C	9.6	197.5
E	9.7	197.2 ✓
+3.0	9.9	197.2 ✓
at BM	7.77	199.36

20+50

-2.5	7.7	199.4
E	7.7	199.4
C	7.7	199.4
W	8.3	198.8
+2.5	8.7	198.2

21+00

-2.0	6.5	✓ 100.6
W	6.1	✓ 101.0
C	5.7	✓ 101.4
E	5.8	✓ 101.3
+2.0	5.8	✓ 101.3

207.13

21+50

-2.0	4.5	✓0.6
E	4.0	✓0.3.1
C	3.8	✓0.3.3
W	4.3	✓0.8
+2.0	4.7	✓0.1.2

22+00

-2.0	3.0	✓0.1
W	2.6	✓0.4.5
C	2.1	✓0.5.0
E	2.2	✓0.4.9
+2.0	2.5	✓0.4.6

22+50

+2.	0.9	✓0.6.✓		
E	0.7	✓0.6.4		
C	0.5	✓0.6.6		
W	1.0	✓0.6.1		
+2	1.5	✓0.5.6		
T.P	12.95	219.69	0.41	206.72

23+00

-2	12.2	✓0.7.2
W	11.9	✓0.7.7
C	11.5	✓0.8.1
E	11.6	✓0.8.0
+2	11.8	✓0.7.8

12+45

12

23+50

-2	10.4	✓0.9.✓
E	10.2	✓0.9.4
C	9.9	✓0.9.7
W	10.8	✓0.8.8
+2	11.1	✓0.8.5

24+00

-2	9.2	✓1.0.4
W	8.9	✓1.0.7
C	8.4	✓1.1.✓
E	8.8	✓1.0.8
+2	9.1	✓1.0.5

24+50

-2	7.5	✓1.1.1
E	7.5	✓1.1.1
C	7.0	✓1.1.6
W	7.5	✓1.1.1
+2	7.8	✓1.1.8

25+00

-2	6.7	✓1.1.9
W	6.4	✓1.3.✓
C	6.1	✓1.3.5
E	6.4	✓1.3.✓
+2	6.5	✓1.3.1

25+50

-2	5.4	✓1.4.✓
----	-----	--------

21967

E	5.4	✓14.✓
C	5.1	✓14.5
W	5.6	✓14.0
+Z	5.8	✓13.8

26+00

-Z	4.8	✓14.8
W	4.7	✓14.9
C	4.3	✓15.3
E	4.6	✓15.0
+Z	4.7	✓14.9

26+50

-Z	4.0	✓15.0
E	4.0	✓15.0
C	3.6	✓16.0
W	4.2	✓15.✓
+Z	4.4	✓15.✓

27+00

-Z	3.5	✓16.1
W	3.3	✓16.3
C	2.8	✓15.8
E	3.2	✓16.✓
+Z	3.3	✓16.3

27+50

-Z	2.6	✓17.0
E	2.4	✓17.✓
C	1.9	✓17.7

127757
v3

W	2.4	✓17.✓
+Z	2.6	✓17.0

28+00

-Z	1.8	✓17.8
W	1.5	✓18.1
C	1.2	✓18.✓
E	1.6	✓18.0
+Z	1.7	✓17.9

28+50

-Z	0.6	✓19.0
E	0.5	✓19.1
C	0.2	✓19.✓
W	0.4	✓19.✓
+Z	0.6	✓19.0

T.P. 12.40 231.73 034 219.33

29+00

-Z	11.8	✓19.9
W	✓11.4	✓10.3
C	11.0	✓10.7
E	11.4	✓10.3
+Z	11.5	✓10.✓

29+50

-Z	10.1	✓11.6
E	9.9	✓11.8
C	9.5	✓11.✓
W	10.1	✓11.6
+Z	10.✓	✓11.3

231.73

12th ST
47

30+00

-Z	9.0	✓✓2.7
W	8.7	✓✓3.0
C	8.1	✓✓3.6
E	8.4	✓✓3.3
+Z	8.5	✓✓3.2

30+50

-Z	7.0	✓✓4.7
E	6.8	✓✓4.9
C	6.4	✓✓5.3
W	7.1	✓✓6.6
+Z	7.3	✓✓4.2

31+00

-Z	5.5	✓✓6.2
W	5.2	✓✓6.5
C	4.6	✓✓7.1
E	5.0	✓✓6.7
+Z	5.2	✓✓6.5

31+50

-Z	3.6	✓✓8.3
E	3.2	✓✓8.5
C	2.9	✓✓8.8
W	3.5	✓✓8.2
+Z	3.8	✓✓7.9

32+00

-Z	1.9	✓✓9.8
W	1.6	✓✓9.1
C	1.3	✓✓9.4
E	1.6	✓✓9.1
+Z	1.9	✓✓9.8

T.P. 11.72 2/3.26 0.19 231.54

32+50

-Z	11.6	✓31.6
E	11.4	✓31.8
C	11.1	✓31.1
W	11.6	✓31.6
+Z	11.9	✓31.3

33+00

-Z	9.8	✓32.4
W	9.6	✓33.6
C	9.4	✓33.8
E	9.9	✓33.3
+Z	10.1	✓33.1

33+50

-2.5	8.5	✓34.7
E	8.1	✓35.1
C	7.6	✓35.6
W	7.9	✓35.3
+2.5	8.2	✓35.0

243.46

34+00

-2.5	6.2	✓37.0
W	5.9	✓37.3
C	5.8	✓37.4
E	6.3	✓36.9
+2.5	6.6	✓36.6

34+50

-2.5	4.7	✓38.5
E	4.6	✓38.7
C	4.0	✓39.2
W	4.3	✓38.9
+2.5	4.4	✓38.8

34+99.4 = Nest and Hospital parking

-4	2.8	✓40.4
W	2.5	✓40.7
C	2.2	✓41.0
E	2.8	✓40.4
+4 = Edge paving	2.90	✓40.300 paving

35+50

-3	0.35	✓41.91 - -
E	1.0	✓41.2
C	0.6	✓41.6
W	1.0	✓41.2
+3	1.0	✓41.2

35+ 68.2

3.2 E of E.L. = Edge paving 0.35 ✓41.91 on paving

45

TP 12.03 255.18 0.11 243.15

36+00

-3.5	11.5	✓43.6
W	11.2	✓43.9
C	10.8	✓44.3
E	11.2	✓43.9
+3.5	11.5	✓43.6

36+50

-3.5	9.8	✓45.3
E	9.4	✓45.7
C	9.0	✓46.1
W	9.5	✓45.6
+3.5	9.7	✓45.4

37+00

-3.5	8.0	✓47.1
W	7.7	✓47.4
C	7.2	✓47.9
E	7.4	✓47.7
+3.5	7.6	✓47.5

37+50

-3.5	5.9	✓49.2
E	5.8	✓49.3
C	5.5	✓49.6
W	6.0	✓49.1
+3.5	6.2	✓48.9

38+00

-3.5	4.6	√50.6
W	4.4	√50.7
C	3.9	√51.2
E	4.3	√50.8
+3.5	4.5	√50.6

38+50

-3.5	2.6	√51.5
E	2.5	√51.6
C	2.1	√53.0
W	2.6	√51.5
+3.5	2.7	√51.4
set BM	1.23	√53.95

RAIL RR
2.124 2.127
38+50

39

-3.5	1.2	√53.9	
W	1.0	√54.1	
C	0.4	√54.7	
E	0.6	√54.5	
+3.5	0.4	√54.7	
T.P.	12.84	267.90	
		0.12	√55.06

39+50

-3.5	11.6	√56.3
E	√ 11.5	√56.4
C	11.3	√56.6
W	11.8	√56.1
+3.5	12.2	√55.7

40+00

-3.5	10.4	√57.5
W	10.1	√57.8
C	√ 9.7	√58.2
E	10.2	√57.7
+3.5	10.4	√57.5

40+50

-3.5	8.6	√59.3
E	8.4	√59.5
C	7.9	√60.0
W	8.4	√59.5
+3.5	8.7	√59.2

41+00

-3.5	7.1	√60.8
W	6.8	√61.1
C	6.1	√61.8
E	6.5	√61.4
+3.5	6.8	√61.1

41+50

-3.5	5.0	√62.9
E	4.8	√63.1
C	4.4	√63.5
W	5.1	√62.8
+3.5	5.4	√62.5

42+00

-3.5	3.7	√64.2
------	-----	-------

267.90

W		3.3	✓64.6
C		2.6	✓65.3
E		3.1	✓64.8
+3.5		3.5	✓64.1

42+50

-3.5		1.6	✓66.3
E		1.3	✓66.2
C		0.9	✓67.0
W		1.7	✓66.✓
+3.5		2.2	✓65.7

T.P.	13.26	281.07	0.09	267.81
------	-------	--------	------	--------

43+00

-3.5		13.0	✓68.0
W		12.9	✓68.1
C		12.4	✓68.6
E		12.7	✓68.3
+3.5		13.1	✓67.9

43+50

-3.5		11.4	✓69.6
E		11.1	✓69.9
C		10.7	✓71.3
W		11.1	✓69.9
+3.5		11.4	✓69.2

44+00

-3.5		9.8	✓71.2
W		9.4	✓71.6

46.50

12th St 47

C		8.9	✓71.1
E		9.2	✓71.8
+3.5		9.7	✓71.3

+50

-3.5		7.8	✓73.2
E		7.5	✓73.5
C		7.2	✓73.8
W		7.8	✓73.✓
+3.5		8.1	✓71.9

45+00

-3.5		6.6	✓74.4
W		6.2	✓74.8
C		5.6	✓75.4
E		5.8	✓75.✓
+3.5		6.1	✓74.9

+50

-3.5		4.9	✓76.1
E		4.5	✓76.5
C		4.0	✓77.0
W		4.7	✓75.3
+3.5		4.9	✓76.1

46+00

-3.5		3.7	✓77.3
W		3.6	✓77.6
C		2.7	✓78.3
E		3.2	✓77.8
+3.5		3.6	✓77.4

281.07

+50

-3.5	2.8	✓18.1
E	2.3	✓18.7
C	1.7	✓19.3
W	2.4	✓18.6
+3.5	2.6	✓18.4

47+00

-3.5	2.0	✓19.0
W	1.8	✓19.1
C	✓1.2	✓19.8
E	1.7	✓19.3
+3.5	2.1	✓18.9

+50

-3.5	1.7	✓19.3
E	1.4	✓19.6
C	0.9	✓20.1
W	1.6	✓19.4
+3.5	1.8	✓19.1

48

-3.5	1.4	✓19.6
W	1.2	✓19.8
C	0.7	✓20.3
E	1.1	✓19.9
+3.5	1.4	✓19.6

38.80
17.20
53.80

48

+50

-3.5	1.1	✓19.9
E	0.9	✓20.1
C	0.4	✓20.6
W	1.0	✓20.0
+3.5	1.2	✓19.8

TR 6.80 287.01 0.86 280.21

49

-3.5	6.8	✓20.1
W	6.4	✓20.6
C	6.0	✓21.0
E	6.5	✓20.5
+3.5	6.6	✓20.4

+50

-3.5	6.2	✓20.8
E	6.1	✓20.9
C	✓5.7	✓21.3
W	6.2	✓20.8
+3.5	6.5	✓20.5

50

-3.5	6.0	✓21.0
W	5.7	✓21.3
C	5.3	✓21.7
E	5.6	✓21.4
+3.5	5.6	✓21.4

50+50

-3.5	5.3	√81.7
F	5.3	√81.7
C	5.0	√81.0
W	5.4	√81.6
+3.5	5.6	√81.4

51+00

-3.5	5.3	√81.7
W	5.1	√81.9
C	✓ 4.7	√81.3
F	5.0	√81.0
+3.5	5.1	√81.9

+50

-3.5	5.0	√81.0
F	4.8	√81.4
C	4.5	√81.5
W	4.5	√81.4
+3.5	5.1	√81.9
+3.5	4.43	√81.58 on Top curb

52

-3.5	4.6	√81.4
-3.5	4.6	√81.4
C	4.3	√81.7
F	4.4	√81.6
+3.5	4.5	√81.5

52+50

-3.5	4.2	√81.8
F	4.2	√81.8
C	4.2	√81.8
W	4.1	√81.6
+3.5	4.1	√81.6

53

-3.5	4.4	√81.6
W	4.2	√81.6
C	4.0	√83.0
F	4.0	√83.0
+3.5	3.8	√83.4

31.6

53+55.07 = Edge of parking

E	3.85	√83.16	on parking
C	4.05	√81.96	✓ ✓
W	4.15	√81.86	✓ ✓
BM	4.43	√81.58	on curb Left of 51+50 + on Top.

Continued from page 27
Samond Interpolated Sections

50

4 + 29 $\frac{21}{PC}$

E	18.6
+5	18.8
C	18.7
+10	18.8
W	19.1

4 + 82 $\frac{79}{center of Curve}$

E	19.3
+5	19.3
C	19.1
+10	19.3
W	19.2

5 + 36 $\frac{38}{E.C.}$

E	19.6
+5	19.6
C	19.6
+10	19.6
W	19.8

6 + 00

W	20.1
+5	20.2
C	20.2

Lamont Str sections
Mission View Blvd Sections
Continued from page 27

2+23³⁵ PG ok

E	17.9
+5	17.7
C	17.9
+10	18.3
W	18.2

See page 27 2+76⁴³ Center of Curve @

3+16⁶ South Line Lamont produced.

E	17.8
+5	17.8
C	17.6
+10	18.1
W	18.2

3+29⁵ EC ok

3+50 @

4+00 @

4+29²¹ PC

See page 27

E	18.6
+5	18.8
C	18.7
+10	18.8
W	19.1

4+31¹¹ North line of Alley

E	18.6
+5	18.8
C	18.7
+10	18.8
W	19.1

4+48⁸¹ South Alley line

E	19.0
+5	19.0
C	18.9
+10	18.9
W	19.2

4+82²⁹ Center of Curve

E	19.3
+5	19.3
C	19.1
+10	19.3
W	19.2

5+36³⁸ E.C.

E	19.6
+5	19.6
C	19.6
+10	19.6
W	19.8

Mission View Blvd. Sections

5+89⁴ North line Sequoia St.

E 19.9
 +5 19.8
 C 20.1
 +10 20.1
 W 20.0

6+00 ok

6+50 ok See page 28

7+00 ok

7+05⁴⁰ South line Sequoia

E 20.6
 +5 21.0
 C 21.0
 +10 20.9
 W 20.8

7+50 ²⁰ See page 28

7+71¹³ BC

Top curb

E 21.3
 +10 21.5
 C 21.9
 +5 21.5
 W 22.1
 Top Curb
 +1.9 22.55

7+99⁵⁶ Center of curve

E 21.8
 +5 22.1
 C 22.1
 +10 21.9
 W 22.1

8+27⁹⁹ E.C.

E 22.2
 +5 22.3
 C 22.5
 +10 22.2
 W 22.2

8+38⁸² N Alley line

E 21.8
 +5 22.0
 C 22.3
 +10 22.4
 W 22.0

8+54⁶⁹ South Alley line

E 22.3
 +5 22.4
 C 22.5
 +10 22.3
 W 22.2

Mission View Blvd Sections

53

9400

E	231
+5	234
C	235
+10	233
W	233

9459¹⁰ = N Line Kendall

E	241
+5	243
C	242
+10	240
W	239

Levels on Survey
Shown on page 54

10.27	293.05	282.55
20' E of L	9.7	283.3
15' - - -	9.7	283.3
L	9.80	283.25
20' W of L	9.9	283.1
0+00		
20' W of L	7.2	285.8
18' - - -	7.6	285.4
15' - - -	7.6	283.4
9' - - - = curb	9.5	283.2
L	9.5	283.2
9' E of L	9.5	283.2
15' - - -	8.2	284.8
20' E of L	7.4	285.6
0+10		
20' E of L	7.2	285.8
15' - - -	7.7	285.3
9' - - - Top curb	9.07	283.98
- - - - gutter	7.61	283.44
L	9.4	283.6
9' W of L gutter	9.60	283.45
- - - - Top curb	9.06	283.99
15' - - -	9.2	283.1
18' - - -	7.5	285.5
20' - - -	7.0	286.0

293.05

0+11.0

20' W of L	5.1	287.9
15.5' - - -	9.1	283.9
9' - - - Top curb	9.04	284.01
9' - - - gutter	9.58	283.47
L	9.4	283.6
9' E of L gutter	9.60	283.45
- - - - Top curb	9.06	283.99
15' - - -	7.4	285.6
19' - - -	7.2	285.8
20' - - -	4.3	288.7
0+15		
20' E of L	3.6	289.4
15' - - -	7.4	285.6
9' - - - Top curb	8.92	284.13
- - - - gutter	9.43	283.62
L	9.25	283.80
9' W of L gutter	9.43	283.62
9' - - - Top curb	8.92	284.13
15' - - -	9.1	283.9
15.5' - - -	9.1	283.9
18' - - -	5.7	287.3
20' - - -	5.0	288.0
0+20.5		
Top of CB at	9.30	west curb 283.75

293.05

0+50

20' W of d.	40	289.0
18' " " "	47	288.3
15.5' " " "	76	285.4
15' " " "	76	285.4
9' " " " Top curb	732	285.73
9' " " " gutter	790	285.15
6	770	285.35
9' E of d gutter	791	285.14
" " " " Top curb	733	285.72
15' " " "	5.0	288.0
20' " " "	3.0	290.0

1+00

20' E of d.	1.7	291.3
15' " " "	3.3	289.7
9' " " " Top curb	4.93	288.12
9' " " " gutter	5.55	287.50
6	5.38	287.67
9' W of d gutter	5.54	287.51
" " " " Top curb	4.92	288.13
15' " " "	5.1	287.9
15.5' " " "	5.1	287.9
18' " " "	3.6	289.4
20' " " "	3.3	289.7

293.05

1+20

20' W of d	3.5	289.5
18' " " "	3.5	289.5
15' " " "	4.3	289.7
9' " " " Top curb	4.25	288.80
" " " " gutter	4.80	288.25
6	4.63	288.42
9' E of d gutter	4.82	288.23
" " " " Top curb	4.25	288.80
15' " " "	2.3	290.7
20' " " "	1.0	292.0

1+25

20' E of d	0.8	292.2
15' " " "	2.0	291.0
9' " " " Top curb	4.12	288.93
" " " " gutter	4.71	288.34
6	4.54	288.51
9' W of d =	4.74	288.31
12' " " "	4.77	288.28
" " " " Top curb	4.22	288.83
15' " " "	4.26	288.79
20' " " "	4.31	288.74
" " " " gutter	4.81	288.24

293.05

1+38.5

20' W of d	gutter	4.54	288.51
✓ - - -	Top curb	3.98	289.07
15' - - -	- -	3.85	289.20
✓ - - -	gutter	4.45	288.60
12' - - -	-	4.41	288.64
d		4.26	288.79
9' E of d		4.41	288.64
- - - -	Top curb	3.86	289.19
15' - - -		1.8	291.2
20' - - -		1.1	291.9

1+45

Top of E	Catch Basin	4.40	288.65
✓ - - -	W Catch Basin	4.40	288.65

1+60

16' W of d		3.8	289.2
9' - - -	Top curb	3.69	289.36
- - - -	gutter	4.27	288.78
d		4.07	288.98
9' E of d	gutter	4.28	288.77
- - - -	Top curb	3.68	289.37
12' - - -		3.2	289.8
15' - - -		1.9	291.1
17' - - -		1.3	291.7
20' - - -		1.0	292.0

293.05

2+00

20' E of d		1.0	292.0
17' - - -		1.2	291.8
15' - - -		1.8	291.2
11' - - -		3.4	289.6
9' - - -	Top curb	3.50	289.55
✓ - - -	gutter	4.07	288.98
d		3.86	289.19
9' W of d	gutter	4.07	288.98
- - - -	Top curb	3.50	289.55
15' - - -		3.7	289.3

2+50

15' W of d		3.4	289.6	
9' - - -	Top curb	3.24	289.81	
✓ - - -	gutter	3.80	289.25	
d		3.60	289.45	
9' W of d	gutter	3.80	289.25	
✓ - - -	Top curb	3.22	289.83	
11' - - -		3.0	290.0	
15' - - -		1.8	291.2	
18' - - -		1.2	291.8	
20' - - -		1.1	291.9	
T.P.	4.81	294.81	3.05	290.00

3+00

20' E of d		3.2	291.6
17' - - -		3.4	291.4
15' - - -		3.8	291.0

294.81

11' E of d		46	290.2
9' E of d	Top Curb	478	290.03
" " "	gutter	538	289.43
" " "	d	512	289.69
9' W of d	gutter	534	289.47
" " "	Top Curb	477	290.04
15' " "		50	289.8

3 + 33'

15' W of d		49	289.9
9' " "	Top Curb	455	290.26
" " "	gutter	513	289.68
" " "	d	495	289.86
9' E of d	gutter	517	289.64
" " "	Top Curb	458	290.23
15' " "		36	291.2
20' " "		32	291.6

3 + 37.3

20' E		390	290.91
15' "		45	290.3
9' "	gutter	515	289.66
" " "	d	49	289.9
9' W of d		510	289.71
" " "		45	290.29
15' " "		48	290.0

294.81

433.8
41.0

3 + 76

15' W of d		47	290.1
9' " "		435	290.46
" " "		490	289.91
" " "	d	48	290.0
9' E of d		492	289.89
15' " "		43	290.5
20' " "		38	291.0

3 + 92.8

20' E of d		36	291.2
15' " "		39	290.9
9' " "	Top Curb	432	290.49
" " "	gutter	489	289.92
" " "	d	478	290.03
9' W of d	gutter	485	289.96
9' " "	Top Curb	429	290.52
15' " "		46	290.2

4 + 33.8

15' W of d	Top cb	410	290.71
" " "	gutter	473	290.08
12' " "	gutter	469	290.12
12' " "	Top curb on return	408	290.73
" " "	d	474	290.07
12' E of d	gutter	473	290.08
12' " "	Top curb on return	410	290.71
15' " "		410	290.71
" " "	gutter	473	290.08

GRADES 12th ST EXTENSION

	W	E
0+00	109.5	
+ 50	112.5	
1	115.5	116.0
+ 50	118.4	118.4
+ 68 RC	119.09	119.26
OUT + 75	119.47	119.6
2	120.8	120.8
+ 25	121.93	121.93
+ 50	123.05	123.05
+ 75	124.18	124.18
3	125.30	125.30
+ 25	126.43	126.43
+ 50	127.56	127.55
+ 75	128.68	128.68
4+01.77 PCC	129.89	129.89
+ 25	130.99	130.99
+ 50	132.17	132.17
+ 76	133.35	133.35
5	134.55	134.55
+ 25	135.74	135.74
+ 50	136.93	136.93
+ 75	138.11	138.11
6	139.3	139.3
+ 25	140.45	140.45
+ 50	141.60	141.60
+ 75	142.75	142.75

4) 5'3"
1.32

53
12
41.4
4.3
91

10547 BP HW 12th A.

12.27
117.74
0.25
117.49
117.0
129.19

W 112.5 115.5 118.4 119.09 839 726 614
524 2.24 1105 7810 825 676 657
2.09 1060 861 4034 +0.50 -043
+0.15 4045 +0.49

E 118.4 119.26 120.8 121.93 120.8 121.93 123.05
10.99 9.93 8.37 7.26 6.14
0.0

W 5.01 3.89 2.76 1.64 0.51 10.33 0.0 0.0 0.0 0.0
5.44
-0.43

E 124.18 125.30 126.43 127.55 128.68 129.89 130.99 132.17 133.35 134.55
12.27 3.89 2.76 1.64 0.51 10.33 9.23 8.05 6.87 5.67
12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27
12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27
12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27 12.27

W 0.0 0.0 0.0 0.0 14.245 14.160 14.275
12.03 10.88 9.73
0.0 0.0

E 135.74 136.93 138.11 139.3 140.45 141.60 142.75
14.27 14.27 14.27 14.27 14.27 14.27 14.27
14.27 14.27 14.27 14.27 14.27 14.27 14.27
14.27 14.27 14.27 14.27 14.27 14.27 14.27
14.27 14.27 14.27 14.27 14.27 14.27 14.27

4/8
1.15
3.62
2.8
8.24

1.125
1.1875
0.4735
0.950

7	143.90	
+ 25	145.05	
+ 50	146.20	
+ 75	147.35	147.35
8	148.5	148.5
+ 25	149.71	
+ 50	150.92	
+ 75	152.13	
9	153.34	
+ 25	154.55	
+ 50	155.76	
+ 75	156.98	
10	158.2	158.2
+ 25	159.44	
+ 50	160.70	
+ 66.10 EC	161.49	
11	163.17	
+ 50	165.61	
12	168.1	168.1
+ 51.97 FC	170.64	
+ 75	171.80	
13	173.03	
+ 25	174.26	
+ 50	175.5	175.5
+ 75	176.55	
14	177.6	177.6

5/19/22 1.16 8/19/22 1.2

152.48	E	14290	14505	14620	14735	1485	14971	15092	15213
041		8.58	7.43	6.28	5.13	3.98	2.77	1.56	0.35
152.04		00	00	00	00	00	00	00	00
	W	00	00	00	00	00	00	00	00
148.1	E	1071	950	829	707	585	461	335	256
160.05		00	-0.35	0.63	-0.36	0.30	-0.47	0.37	-0.31
				-0.34		-0.45		-0.37	
	W	15334	15455	15576	15698	1582	15944	16070	16149
		10.71	9.50	8.29	7.07	5.85	4.61	3.35	2.56
			0.35	0.63	-0.36	0.30	-0.47	0.37	-0.31
				-0.34		-0.45		-0.37	
	F	088	16564	1681	16964	17180	17302	17426	1755
		117	1018	772	518	402	279	156	32
		-0.29	1045	790	511	396	272	150	50
			-0.27	-0.18	-0.03	0.06	0.37	0.07	-0.15
164.05	W	16317	1018	772	518	402	279	156	032
067		121	1059	797	533	00	272	150	062
16338		-0.33	-0.40	-0.25	-0.16		0.07	-0.24	-0.31
1244									
17582									
102									
51	E	17655	1776						
063		1085	98						
17519		1103	1805						
1221		018	-0.25						
18740									
	W	1085	98						
		-0.21	-0.20						

W

+ 25'	178.5
+ 50	179.4
+ 75'	180.14
15	180.88
+ 25'	181.52
+ 50	182.35
+ 75	183.09
16	183.83
+ 25	184.57
+ 54.73 EC	185.45
17 + 17.15 PC	187.40
+ 50	188.42
+ 75	189.21
18	190.0
+ 25'	190.91
+ 50	191.82
+ 75'	192.73
19	193.64
+ 25'	194.55
+ 50	195.46
+ 75	196.37
20	197.30
+ 25'	198.25
+ 50	199.20
+ 75'	200.15
21	201.10

187.40

178.5	80	726	652	588	505	431	357
19	805	730	660	588	496	442	352
90	-0.05	-0.04	-0.08	+0.02	+0.09	-0.11	-0.25
-0.10							

E	178.5	179.4	180.14	180.88	181.52	182.35	183.09	183.83
	89	80	726	652	588	505	431	357
	928	848	715	636	576	487	393	321
	-0.33	-0.28	+0.11	1016	+0.12	+0.18	+0.22	+0.66
							+0.98	

W	333	195	00	1170				
	337	275		1180				
187.40	-0.54	-0.20	+0.09	-0.10	1077	822	933	870
272					+0.14	+0.20	-0.12	-0.40
								304
								865

E	184.57	185.45	187.40	188.42	189.21	190.0	190.91	191.82	192.73
	233	195	00	1170	1091	1000	921	830	739
	212	196	026	1193	1089	1039	957	860	771
	+0.69	00	-0.25	-0.23	+0.24	-0.27	-0.36	-0.30	-0.32

W	19364	19455	19546	19637	19730	19821	19920	20015	20110
	648	557	466	375	282	189	92	124	129
	723	615	508	417	325	236	130	122	117
	-0.25	-0.58	-0.82	0.42	-0.26	00	-0.38	+0.04	00

E	638	558	445	330	221	096	19920	19920	19920
	+0.15	00	+0.60	+0.15	+0.61	+0.91	13.19	1224	1129
							1280	1170	75
							-0.37	+0.54	+0.34

205.29

W	20110	20015	19920
	4.19	5.14	6.09
	+0.11		0.15
			+0.30
E	419		
	383		
	+0.16		

	W
21 + 28.21 PF	202.16
+ 50	203.0
22	204.9
+ 50	206.42
23	207.92
+ 50	209.47
24	211.0
+ 50	212.4
25	213.5
+ 42.39 PC	214.21
+ 75	214.78
26	215.2
+ 20	215.58
+ 50	215.96
+ 75	216.33
27	216.7
+ 25	217.1
+ 50	217.5
+ 75	217.9
28	218.3
+ 25	218.85
+ 50	219.40
+ 75	219.95
29	220.5
+ 31.49 PCC	221.43
+ 50	222.00

212.89	W	202.16	2030	2049	20642	20794	20947	
0.02		1023	939	749	597	445	292	
212.86		730	961	787	653	478	355	
714		+0.03	-0.22	-0.38	-0.56	-0.30	-0.63	
	E							
		1023	939	749	597	445	292	
		1042	874	0.0	607	436	285	
		-0.19	+0.65		-0.10	+0.09	+0.07	
	W	211	212.4	213.5	214.21	214.78	215.2	
		139	.00	8.0	7.29	6.72	6.3	
		167	0.16	8.37	7.26	6.60	6.1	
		-0.28	-0.16	-0.37	+0.02	+0.12	+0.20	
221.50	E	139	.00	8.0	7.29	6.72	6.30	
0.01		150	-0.03	8.27	7.39	6.82	6.20	
221.49		-0.11		-0.27	-0.10	-0.10	+0.10	
12.11								
231.60								
	W	215.58	215.96	216.33	216.7	217.1	217.5	217.9
		592	554	517	480	442	404	366
		572	534	505	468	430	392	354
		-0.20	-0.30	-0.18	-0.75	-0.22	-0.71	-0.21
	E	592	554	517	480	442	404	366
		572	534	507	468	427	387	347
		.00	-0.09	+0.10	.00	-0.07	-0.11	+0.22
	W	218.3	218.85	219.40	219.95	220.5	221.13	222.0
		32	265	210	155	10	1017	960
		32	304	261	185	10	1075	1011
		-0.20	-0.44	-0.51	+0.20	-0.52	-0.58	-0.51
	E	32	265	210	155	10	1017	960
		32	304	205	175	10	1072	1005
		+0.20	+0.06	+0.05	-0.20	+0.10	-0.05	+0.05

19917
612
205.27

W 202.16
3.13
2.18
+0.25

W 313
305
+15

29 + 75 222.75

30 223.5

+ 25 224.36

+ 50 225.23

+ 75 226.09

31 226.95

+ 25 227.81

+ 50 228.67

+ 75 229.53

11

32 230.4

+ 25 231.26

+ 50 232.12

+ 75 232.99

33 233.85

+ 25 234.71

+ 52.7 EC. 235.67

34 237.3

+ 50 239.0

35 240.70

+ 50 242.45

36 244.20

+ 50 246.0

8/24/24

237.3

238.85

240.40 next day

242.00

244.00

245.77

250.25
250.25
250.25

54
1036
1310

29160	W	22275	2235	22436	22523	22609	22695	22781
019		885	81	724	637	551	465	379
23141		782	865	714	701	624	530	427
677		-098	-085	-050	-024	-074	-065	-048
23819								

051	F	885	610	724	637	551	465	379
23737		878	757	662	614	545	461	373
1235		+007	+053	+062	+023	+062	-30	-014

24972	W	22867	22953	2304	23126	23212	23299
844		293	207	112	24	052	519
24948		354	213	17	291		442
		-061	-066	-05	-057		-030

24948	F	293	207	112	24	052	519
		310	240	161	76	606	474
		-017	-023	-041	-042	-011	-078

	W	23285	23471	23567	2373	2390	24070
		433	347	251	088	1022	878
		453	361	238	081	1044	844
		-020	-054	+013	+007	+038	+034

	F	433	347	251	088	23885	
		477	392	200	134	4087	
		-044	-054	-049	-077	1680	
						+0.07	

24972	W	24245	24420	246			
497		703	528	348			
750		690	542	361			
420		+017	+0.06	-017			

	F		244	24577			
			548	371			
			533	377			
			+016	-006			

	W	24245	24420	246			
		703	528	348			
		690	542	361			
		+017	+0.06	-017			

	F		244	24577			
			548	371			
			533	377			
			+016	-006			

	W	24245	24420	246			
		703	528	348			
		690	542	361			
		+017	+0.06	-017			

	F		244	24577			
			548	371			
			533	377			
			+016	-006			

	W	24245	24420	246			
		703	528	348			
		690	542	361			
		+017	+0.06	-017			

345
43
1038
1380

345
43
1038
1380

24230

390

24250

$\frac{260}{270} \frac{650}{770}$
 $\frac{270}{280} \frac{770}{880}$
 $\frac{280}{290} \frac{880}{990}$
 $\frac{290}{300} \frac{990}{1100}$

44+	271.8	272.0
+25	272.65	272.8
+50	273.50	273.6
+75	274.35	274.4
45	275.2	275.2
+25	275.85	275.85
+50	276.5	276.5
+75	277.15	277.15
46	277.8	277.8
+25	278.2	
+50	278.6	
+75	278.9	
47	279.2	
+2465 EC	279.45	
+50	279.7	
48	280.1	
+50	280.45	
49	280.8	
+6726 PC	281.23	
50	281.45	
+25	281.62	
+50	281.80	
+75	281.95	
51	282.1	282.1
+1295 EC	282.15	282.15
+50	282.28	282.28

272.05

W	271.80	272.65	7350	7435	7520	7585
	+25	11.17	1022	847	862	877
	+29	11.42	1029	854	869	884
	-25	-0.23	-10	-38	-51	-17
E	272.0	7280	7360	7440	864	797
	+25	11.02	1022	942	864	797
	+25	10.80	1017	945	867	797
	-25	-0.19	+0.05	-0.03	+0.17	+0.14
W	7650	7715	7780	7820	7860	7890
	+25	6.67	6.02	5.62	5.22	4.82
	+25	6.70	6.02	5.50	5.10	4.70
	-0.03	-0.03	+0.02	+0.09	+0.05	+0.05
E	732	167	402	562	522	482
	+0.02	2.02	6.02	5.62	5.22	4.82
		-0.41	-0.05	+0.02	-0.05	+0.04
W	7945	7970	8010	8045	8080	8123
	+25	1.12	3.72	3.37	3.02	2.59
	+25	1.12	3.72	3.37	3.02	2.59
	+0.5	-0.36	+0.01	+0.08	+0.19	+0.44
E	437	412	372	337	302	259
	+0.13	4.09	0	2.67	2.62	2.13
		+0.03	0	+2.5	+0.40	+0.46
W	8145	8162	8180	8195	8210	8215
	+0.37	2.40	2.02	1.87	1.72	1.57
	+0.37	2.40	2.02	1.87	1.72	1.57
	+0.37	+0.03	+0.11	+0.04	-0.04	-0.12
E	237	220	202	187	172	157
	+0.27	1.91	1.77	1.62	1.47	1.32
		+0.27	+0.25	-0.03	+0.27	+0.27

	✓	£
52	282 41	282 45
+ 50	282 51	282 59
53	282 98	282 73
+ 29.6	282 86	283.76
	282.62	282.82

287.22

43

282.45	82.51	82.58
+ 77	4.71	+ 67
4.81	4.20	
- 1.04	82.59	
	4.63	
4.77	4.80	82.73
4.34	+ .83	4.49
+ .73		

289.11
0.50
 288.61

289.11
6.02
 283.07

289.11
5.99
 283.12

283.11
6.00
 289.11

289.11
5.16
 283.95

5000
5113
 217

0021
70
 125
 515
 121

0025
760
 1090

Location + Elev. of Sewer at County Hospital
at Front + Dickenson sts

	3.95	293.71	289.76	Top of Hydr SE Front + Dickenson
M.H. flow of Hospital from North		7.62	286.09	
M.H. flow of line = 0100 from Residence		7.40	286.31	
1 + 72.30 top of 1/2" pipe 28" long		4.40	289.31	
driven to flow line			$\frac{2}{33}$ 286.98	

70

st

Front st

○

M.H. 0100

Drive to Hospital

172.30'

1/2" pipe

Dickenson

Elevations Past Haven

	4.97	104.97	Assumed 100.00	SW Cor cement porch Bldg #1
Ground SW cor Bldg #1		5.30	99.6	
✓ NW - - - - #1		6.3	98.6	
25 W of - - - - #1		6.1	98.8	
25 N - - - - #1		6.2	98.7	
Ground NE - - - -		6.5	98.4	
✓ SE - - - -		5.8	99.1	
center of E Side - - -		7.1	97.8	
✓ NW cor Bldg #2		4.7	99.8	
Floor - - - -		3.7	101. ✓	
20 W of NW cor ✓ -		4.3	100.6	
20 - - SW - - - -		4.0	100.9	
Ground - - - -		4.1	100.8	
✓ SE ✓ - - -		4.7	100. ✓	
NE - - - -		4.7	100. ✓	
Floor ✓ - (3)		4.0	100.9	
Ground NW ✓ - ✓		5.4	99.5	
center of W side - - -		5.4	99.5	
Ground NE - - - -		7.0	97.9	
✓ SE - - - -		6.2	98.7	
✓ SW - - - -		4.4	100.5	
✓ SW - - - - #5		3.4	101.5	
✓ NW - - - -		3.6	101.3	
✓ NE - - - -		2.7	102. ✓	
✓ SE - - - -		4.9	100. ✓	

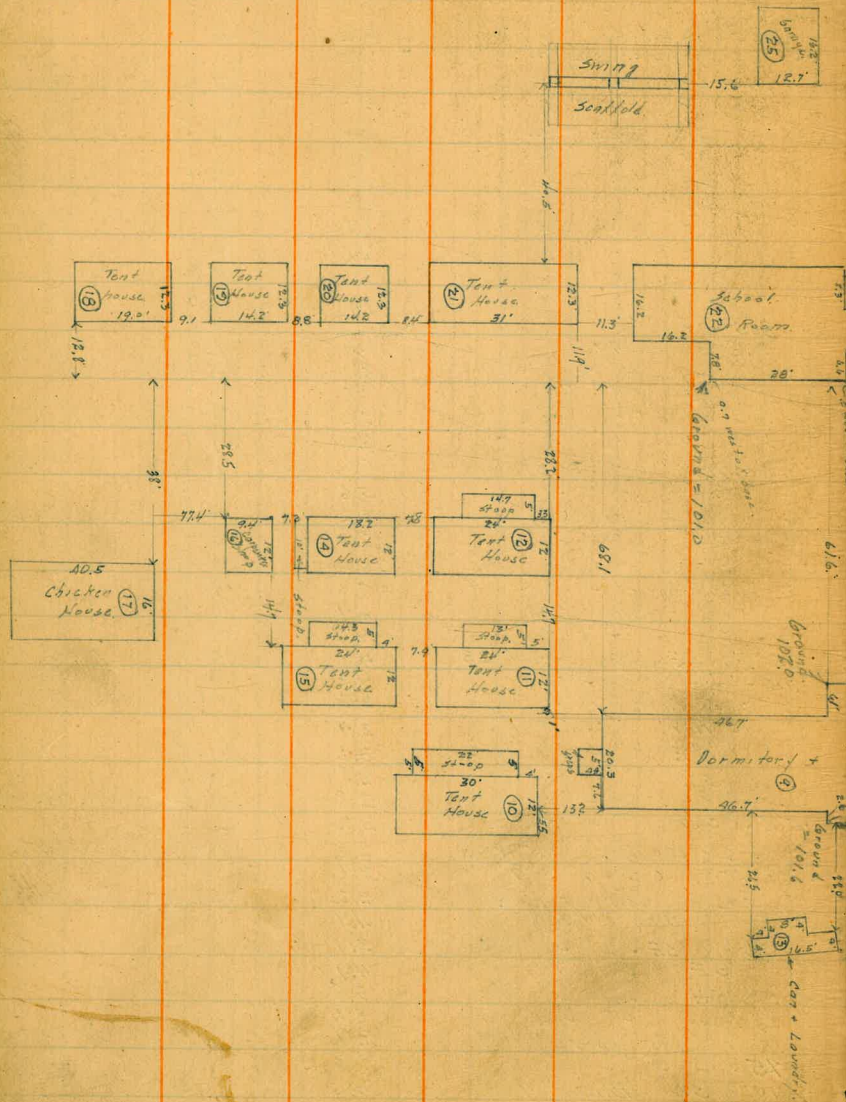
Ground SE Bldg #4	3.0	101.9
✓ NE	3.7	101. ✓
✓ NW	4.1	100.8
✓ SW	3.1	101.8
✓ 15 W of - - - -	3.4	101.5
✓ 25 - - - -	4.1	100.8
✓ 25 S ✓ - - - - #1	4.2	100.7
✓ 25 W ✓ - - - -	6.4	98.5
✓ 25 S of above	6.2	98.7
✓ 45 W of SW Bldg #4	4.5	100.4
✓ SE	5.3	99.6
✓ 80	6.7	98.2
✓ NW Bldg #24	9.4	94.5
✓ NE	8.1	96.8
✓ SE	8.6	96.7
✓ SW	9.3	95.6
✓ NE (25)	8.8	96.1
✓ NW	9.9	95.0
✓ SE	9.1	95.8
✓ SW	9.9	95.0
✓ 80 S	10.8	94.1
✓ N.E. end Swing	9.6	95.3
25 W of - - - -	8.1	96.8
25 E of NE Bldg (25)	7.8	97.1
15 - - - - (24)	7.2	97.7
30 - - - -	6.0	98.9
Ground NW ✓ (23)	5.6	99.3
✓ SW	5.6	99.3
✓ NW ✓ (22)	6.2	98.7
✓ SW	7.0	97.9
S. End of Swing -	10.0	94.9
✓ 23 E of - - - -	8.0	96.9
✓ NE Bldg (23)	4.9	100.0
✓ SE	4.9	100.0
25 E of NE of Main portion (23)	4.1	100.8
25 - - - - Washroom	4.3	100.6
20 N of last above	3.8	101.1
Ground NW Bldg #6	2.9	102.0
✓ NE	3.1	101.8
✓ SW	2.8	102.1
✓ SE	2.8	102.1
15 W of SW	3.2	101.7
SW cor of cement walk	2.6	102.4
Grd. NW cor Bldg #9	2.6	102.3
E. End of Cement walk	2.2	102.7
Grd. NE Bldg #9	4.1	100.8
✓ 23 N of SE ✓	3.1	101.8
✓ SE	4.1	100.8
✓ SW	3.8	101.1
✓ 23 NW ✓	2.6	102.3
✓ 15 W of last above	2.6	102.3
✓ 25 - - - -	3.8	101.1
✓ 10 - SW Bldg #9	4.0	100.9
✓ 25 - - - -	3.4	101.6
✓ 35 - - - -	3.4	101.6
✓ 45 - - - -	5.0	99.9
✓ - - - - at 23 N of SW Bldg #9	4.4	100.5

6/21/23

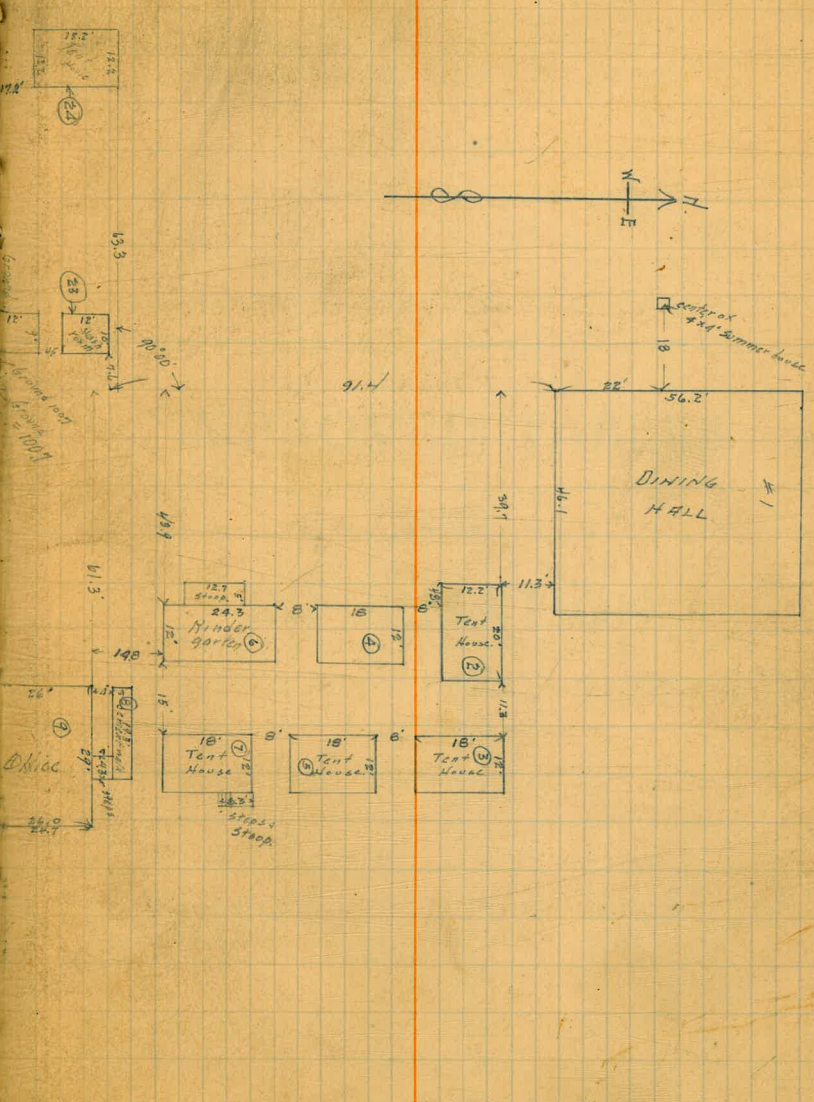
Gregory

REST HAVEN HOME Improvements

71



72



10497

35' W + 23' S. of NE Bldg #2

20

4.4
5.4

100.5
101.5

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in the table. The number in both

of table in same row and column gives distance level. The distance in inches between the side stake and slope stake, lower tangent by this amount if cut, else add. Add this amount to cut or fill and find distance in table. Set up rod at side stake and find distance in table. Set up rod at side stake and find distance in table. If it does not make the slight adjustment necessary.

**IMPROVED TABLES
AND
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external) opposite T by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the apsis of the tangent length divided by twice the radius.

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{7}{8}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{15}{16}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
1	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790''$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{4}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

$$\text{Horizontal Distance} = R - R \sin^2 a + C \cos a$$

$$\text{Vertical Distance} = R \frac{1}{2} \sin 2a + C \sin a$$

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

2955
135
1248
4338

B M Vine & Columbia

181.38
168.71
12.67

3916
1938
1939

120) 42
60
175

.038
254
76
1.564

4156
330
886
203.0

.038
12
76
1.564

677 52

19343
171

166) 570 81
498
720
664
560

11) 69
66
30
21
80
71

886) 275.0
2658
920
886
3400
15.50

.017
42
34
68
71

3104
20
62080

3104
156
18622
2432
3104
5773.00

16
2058
343
5488

4282.13
408355
21955

25
86
34
76

6/50
83

121) 690
875
1500
1.5360
767

4) 15
371
264
33

.033
280
212
28

84) 340
336
400
307
28
614
819

722
51

34
19
306
30
646

0401
18
3240
105
729

47
207
329
121
124
32

2) 165
53

34
19
306
30
646
68
32

762
740
440

172.30

180) 600
540

309.3
60
2600
9373

12.84
110

06666
3333
139996
80.82
1234
9316

4.10
36
27

270
14666
22335

2+23.35 = PC.
2+76.43 = CC
3+29.52 = EC.
4+40.18 = PC.
4+9.638 = CC
5+52.58 = EC.
7+72.13 = PC
7+9.89
8.07 65
975 39.

10617
5308

11066

11220
5020

3772
1876

16577

150) 740
600
1380
500
25451

1933
52
9566
21465
25451

247
120

17665

25.9999