

1104

LEVEL BOOK

373

1104

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

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MICROFILMED

	.1	.2	.3	.4	.5	.6	.7	.8	.9		
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

1104

ENGINEERING DEPARTMENT,
CITY OF
SAN DIEGO,
CALIFORNIA.

Cross Section of
Imperial Ave
thru Escante
continued from book 1080-26

on B.M.	682	236.34	229.52	N Tie hub Sta 68+00	-2	+80	Narrow berms from Here to Bridge
		68+00			N	6.6	229.7
-2		6.3	230.0		+4	6.5	229.8
N		6.2	230.1		C	6.6	229.7
+1		6.6	229.7		+9	6.4	229.9
+4		6.6	229.7		S	5.8	230.5
C		6.5	229.8		+2	6.0	230.3
+9		6.4	229.9				
S		6.4	229.9		S+3	7.1	229.2
+2		6.0	230.3		+1	6.7	229.6
		+40			C	6.7	229.6
-2		5.3	231.0		+9	6.7	229.6
S		5.6	230.7		+10	7.1	229.2
+4		5.8	230.5				
C		5.9	230.4		N+4	7.0	229.3
+9		6.2	230.1		C	6.9	229.4
N		5.9	230.4		+9	7.0	229.3
+2		6.3	230.0				
					-2	8.8	227.5

Plotted by Tolman

69+00 W Line of Bridge
Deck of Bridge Elev = 228.2

Top of
Corner Wing

Top of
Corner Wing

+22 E Line of Bridge

Narrow berms
from Bridge
to here

S	8.2	228.1
+3	7.4	228.9
+4	7.4	228.9
0	7.2	229.1
+9	7.2	229.1
+10	7.3	229.0
N	7.9	228.4
+2	8.5	227.8

+65

-7	9.4	226.9
-2	8.8	227.5
N	7.2	229.1
+4	7.3	229.0
C	7.8	229.0
+9	7.7	228.6
S	7.8	228.5
+2	9.0	227.3
+7	9.3	227.0

70+00

-2	8.1	228.7
----	-----	-------

S	7.4	228.9
+1	7.9	228.4
+4	7.7	228.6
E	7.4	228.9
+9	7.5	228.8
N	7.6	228.7
+2	8.8	227.5
+7	9.2	227.1

+50

-2	7.4	228.9
N	7.2	229.1
+4	7.4	228.9
C	7.3	229.0
+9	7.6	228.7
S	7.5	228.8
+2	7.9	228.4

71+00

-2	7.2	229.1
S	7.5	228.8
+4	7.4	228.9

						+50	
C	7.1	229.2		-2	5.8	230.5	
+9	7.2	229.1		N	5.7	230.6	
N	7.0	229.3		+4	6.1	230.2	
+2	7.0	229.3		C	6.0	230.3	
		+50		+9	6.3	230.0	
-2	6.8	229.5		S	6.4	229.9	
N	6.9	229.4		+2	6.4	229.9	
+4	7.0	229.3					
					73+00		
C	7.0	229.3		-2	5.5	230.8	
+9	7.2	229.1		S	5.4	230.9	
S	7.3	229.0		+4	5.2	231.1	
+2	7.1	229.2		C	5.1	231.2	
				+9	5.2	231.1	
-2	6.7	229.6		N	4.7	231.6	
S	7.0	229.3		+2	4.6	231.5	
+4	6.9	229.4					
					+50		
C	6.7	229.6		-2	4.3	232.0	
+9	6.7	229.6		N	4.3	232.0	
N	6.3	230.0		+4	4.4	231.9	
+2	6.5	229.8		C	4.3	232.0	

+9	4.4	221.9
S	4.6	221.7
+2	4.6	221.7

74+00

-2	3.4	232.9
S	3.8	232.5
+4	3.6	232.7
C	3.4	232.9
+9	3.5	232.9
N	3.5	232.8
+2	3.6	232.7

+50

-2	2.6	233.7
N	2.8	233.5
+4	2.7	233.6
C	2.6	233.7
+9	2.8	233.5
S	2.3	234.0
+2	2.3	234.0

75+00

-2	1.6	234.7
S	1.5	234.8
+4	1.6	234.7
C	1.8	234.5
+9	1.8	234.5
N	1.8	234.5
+2	1.8	234.5

+50

-2	1.0	235.3
N	1.0	235.3
+4	0.8	235.5
C	0.9	235.4
+7	1.3	235.0
+9	0.9	235.4
S	1.0	235.3
+2	1.6	234.7

76+00

-2	1.8	234.5
S	1.8	234.5
+4	1.3	235.0

236.34

c			0.6	235.7	N		6.7	237.7
+9			0.2	236.1	+2		6.7	237.7
N			0.2	236.1		+81		
+2			0.2	236.1	-2		6.3	238.1
T.P	8.24	✓ w4436	0.22	236.12	N		6.3	238.1
		+45			+4		6.6	237.8
-2			7.1	237.3	+10		6.9	237.5
N			7.1	237.3	+11		6.1	
+4			7.2	237.2	C		6.1	238.3
C			7.5	236.9	+6		6.4	238.0
+9			8.8	235.6	+9		8.7	235.7
S			9.2	235.2	S		10.1	234.3 ✓
+2			9.5	234.9	+2		11.0	233.4
		+70			+11		14.8	229.6
-2			7.7	236.7	+16		16.5	227.9
S			7.3	237.1 ✓	+27		15.7	228.7
+4			7.0	237.4		77+00		
C			6.4	238.0	-13		13.3	231.1
+2			7.2	237.2	-8		16.5	227.9
+9			6.8	237.6	-2		16.0	228.4

S	16.0	228.4	✓	+2	16.3	228.1
+2	14.6	229.8		+7	13.1	231.3
+9	12.7	231.7		+15	12.0	232.4
C	5.6	238.8			+40	
+3	5.5	238.9		-15	12.4	232.0
+4	6.4	238.0		-10	15.8	228.6
+9	6.2	238.2		-2	16.0	228.4
N	5.9	238.5		S	16.1	228.3
+2	5.9	238.5		+4	15.2	229.2
	+ 25			+9	5.5	238.9
-2	5.5	238.9		C	4.9	239.5
N	5.5	238.9		+2	5.7	238.7
+4	5.5	238.9		+9	5.2	239.2
+9	5.9	238.5		N	5.1	239.3
+10	4.9	239.5		+2	5.1	239.3
C	5.3	239.1			+53	
+2	12.7	231.7		-2	4.9	239.5
+5	16.4	228.0		N	4.9	239.5
+9	16.3	228.1		+4	4.8	239.6
S	16.3	228.1	✓	+12	5.5	238.9

c	4.9	239.5
+4	5.0	239.4
+9	7.9	236.5
S	9.8	234.6 ✓
+v	10.1	234.3
+10	15.7	228.7
+20	15.7	228.7

+66

-2	5.6	238.8
S	5.6	238.8 ✓
+4	4.8	239.6
+8	4.5	239.9
c	5.2	239.2
+9	4.7	239.7
N	4.7	239.7
+2	4.7	239.7

78+00

-2	4.0	240.4
N	4.0	240.4
+4	4.1	240.3

c	4.0	240.4
+7	4.4	240.0
+9	3.7	240.7
S	4.7	239.7
+2	4.7	239.7
+30		

-2	4.1	240.3
S	3.5	240.9
+4	3.1	241.3
+5	3.5	240.9
c	3.3	241.1
+9	3.6	240.8
N	3.5	240.6
+2	3.8	240.6

+60

-2	3.3	241.1
N	3.3	241.1
+4	2.9	241.5
c	2.7	241.7
+9	2.7	241.7

244.36

S			3.6	240.8	C		8.9	245.3
+v			4.0	240.4	+9		9.2	245.0
			19+00		N		9.4	244.8
-v			1.7	242.7		80+50		
S			1.7	242.7	N		8.2	246.0
+4			1.6	242.8	+4		7.9	246.3
C			1.7	242.7	C		7.7	246.5
+9			2.0	242.4	+9		7.6	246.6
N			2.3	242.1	S		7.4	246.8
+v			2.6	241.8		81+00		
T.P.	10.55	254.17	0.74	243.62	S		6.1	248.1
			79+50		+4		6.6	247.6
N			10.7	243.5	C		6.7	247.5
+4			10.5	243.7	+9		7.2	247.0
C			10.2	244.0	N		7.5	246.7
+9			10.1	244.1		81+50		
S			9.5	244.7	N		7.1	247.1
		80			+4		6.8	247.4
S			7.9	246.3	C		6.2	248.0
+4			8.7	245.5	+9		6.1	248.1
					S		5.7	248.5

Pole 70173
Apr light pole
NW cor.

246.5

25417

82+00

S	5.3	248.9
+4	5.3	248.9
C	5.6	248.6
+9	6.3	247.9
N	6.6	247.6

82+50

N	5.7	248.5
+4	5.4	248.8
C	5.1	249.1
+9	5.0	249.2
S	5.1	249.1

83+00

S	4.4	249.8
+4	4.4	249.8
C	4.6	249.6
+9	5.1	249.1
N	5.5	248.7

83+50

N	5.1	249.1
---	-----	-------

+4

C	4.7	249.5
+9	4.2	250.0
S	4.0	250.2
S	4.0	250.2

84+00

S	2.6	251.6
+1	3.3	250.9
+4	3.3	250.9
C	3.5	250.7
+9	4.2	250.0
N	4.4	249.8

84+50

N	3.7	250.5
+4	3.5	250.7
C	3.0	251.2
+9	2.6	251.6
+12	2.5	251.7
S	2.2	252.0

85+00

S	2.1	252.1
---	-----	-------

254.17

+4	2.0	252.2
C	2.1	252.1
+9	2.6	251.6
N	2.8	251.4

85+50

N	2.0	252.2
+4	1.7	251.5
C	1.2	253.0
+9	1.1	253.1
S	1.3	252.9

86+00

S	0.9	253.3
+4	0.7	253.5
C	0.8	253.4
+9	1.2	253.0
N	1.4	252.8

86+50

N	1.1	253.1
+4	0.9	253.3
C	0.5	253.7

10

+9	0.3	253.9
S	0.2	254.0
T.P.	8.92	262.76
	0.33	253.84

87+00

S	7.9	254.9
+3	8.5	254.3
+4	8.6	254.2
C	8.6	254.2
+9	9.2	253.6
N	9.4	253.4

87+50

N	8.5	254.3
+4	8.7	254.1
C	8.2	254.6
+9	8.1	254.7
+11	8.2	254.6
S	7.8	255.0

88+00

S	7.2	255.6
+4	7.8	255.0

262.76

11

C		81	254.7	+11		5.8	257.0
+9		86	254.2	5		5.2	257.6
N		82	254.6		90+00		
	88+50			5		4.6	258.2
N		81	254.7	+2		5.3	257.5
+4		80	254.8	+4		5.3	257.5
C		76	255.2	C		5.5	257.3
+9		73	255.5	+9		6.2	256.6
5		70	255.8	N		6.5	256.3
	89+00				90+50		
5		64	256.4	N		5.7	257.1
+4		66	256.2	+4		5.3	257.5
C		68	256.0	C		4.7	258.1
+9		75	255.3	+9		4.4	258.4
N		77	255.1	+12		4.6	258.2
	89+50			5		3.9	258.9
N		71	255.7	on County BM.		4.04	258.72
+4		70	255.8		91+00		
C		60	256.8	5		3.5	259.3
+9		59	256.9	+1		4.2	258.6

spk to left
 at 90+85
 Co Elev 262.96
 258.04 258.72
 6.24
 should be 6.12

46276

+4	42	258.1
C	44	258.4
+9	51	259.7
N	52	257.6

91+50

N	44	258.4
+4	48	258.0
C	41	258.7
+9	39	258.9
S	40	258.8

92+00

S	37	259.1
+4	37	259.1
C	38	259.0
+9	43	258.5
N	37	259.1

92+50

N	31	259.7
+4	40	258.8
C	33	259.5

12

+9	30	259.8
S	30	259.8

93+00

S	30	259.8
+4	30	259.8
C	32	259.6
+9	34	259.4
N	47	260.1

93+50

N	42	260.6
+4	31	259.7
C	27	260.1
+9	26	260.4
S	28	260.3

94+00

S	2.6	260.2
+4	2.3	260.5
C	2.1	260.7
+9	2.3	260.5
N	1.5	261.3

262.76

94+50

N	1.4	261.4
+4	1.9	260.9
C	1.7	261.1
+9	1.9	260.9
S	1.9	260.9
T.P.	942 27023 ✓	1.95 26081

95+50

S	88	261.4
+4	8.7	261.5
C	8.5	261.7
+9	8.7	261.5
N	8.1	262.1

95+50

N	7.3	262.9
+2	8.0	262.2
+4	8.0	262.2
C	8.3	261.9
+9	8.4	261.8
S	8.4	261.8

13

96+00

S	7.8	262.4
+4	7.7	262.5
C	7.3	262.9
+9	7.4	262.8
+11	7.4	262.8
N	6.7	263.5

96+50

N	6.8	263.4
+4	6.7	263.5
C	6.6	263.6
+9	6.9	263.3
+11	7.0	263.2
S	6.2	264.0

97+00

S	6.1	264.1
+2	6.9	263.3
+4	6.3	263.9
C	5.9	264.3
+9	6.0	264.2
N	6.1	264.1

270.23

97+50

N	56	264.6
+4	54	264.8
C	53	264.9
+9	58	264.4
+12	60	264.2
S	56	264.6

98+00

S	53	264.9
+4	52	265.0
C	46	265.6
+9	49	265.3
N	50	265.2

98+50

N	45	265.7
+4	43	265.9
C	41	266.1
+9	47	265.5
S	48	265.4

14

99+00

S	43	265.9
+4	41	266.1
C	36	266.6
+9	38	266.4
N	39	266.3

99+50

N	35	266.7
+4	33	266.9
C	32	267.0
+9	36	266.6
S	37	266.5

100+00

S	2.6	267.6
+2	3.0	267.2
+4	3.0	267.2
C	2.7	267.5
+9	2.9	267.3
#12	2.9	267.3
N	2.4	267.8

270.23

15

100 + 62.64

N

1.9 2 68.3

+4 = Edge of parking

1.67 268.56

C

✓

1.59 268.64

+9 Edge of ✓

1.74 268.49

S

1.8 268.4

0.43

269.80

✓ Mon Pt. at
Road at Boundary

X sections of Relocation Paring 18 mbs
on Imperial Ave Berms 4' v

for alignment see book 1080-69

10+30

4.05	15179	147.74	spt via pole W. West Holman 3 side road	N	3.8	148.0
	9+39.74 = old PC			+4	3.9	147.9
S		4.6		+9	4.8	147.0
+v		4.8		C	4.7	147.1
+d		5.9		+9	4.7	147.1
+B=C		5.4		S	4.7	147.1

10+50

+9		5.4				
+B=N		5.6		S	4.7	147.1
	9+50			+4	4.7	147.1
N		5.4		C	4.8	147.0
+4		5.3		+6	3.8	148.0
C		5.3		+9	5.0	146.8
+9		5.5		N	6.1	145.7
S		3.7		+5	6.6	145.2

Plotted by Tolman

10+75

	9+80					
S		5.3		-16	11.8	140.0
+d		5.4		-5	12.0	139.8
C		5.0		N	6.4	145.4
+9		5.0		+4	6.4	145.4
N		5.1				

+10	5.9	145.9
C	4.5	147.3
+9	4.9	146.9
S	4.9	146.9
	10+80	
S	4.8	147.0
+4	4.8	147.0
C	4.9	146.9
+4	6.3	145.5
+9	11.3	140.5
N	11.9	139.9
+14	11.3	140.5
	10+90	
-13	8.4	143.4
N	11.4	140.4
+4	11.5	140.3
+7	11.6	140.2
C	8.3	143.5
+2	4.9	146.9
+9	4.9	146.9

S	4.9	146.9
	11+20	
S	5.1	146.7
+4	5.1	146.7
C	5.6	146.2
+6	7.7	144.1
+9	9.1	142.7
+11	10.5	141.3
N	10.5	141.3
+12	9.2	142.6
	11+37.18 = PC.	
-15	10.2	141.6
-7	10.2	141.4
-4	7.3	144.5
N	7.1	144.7
+4	6.3	145.5
C	5.6	146.2
+9	5.2	146.6
S	4.8	147.0

14
A
113
119
113
17

151.79

11+50

S	4.5	146.3
+4	5.0	146.8
C	5.6	146.2
+9	5.8	146.0
N	5.8	146.0
+7	7.3	144.5

11+88

-5	5.7	146.1
N	5.5	146.3
+4	5.4	146.4
C	4.9	146.9
+9	4.3	147.5
S	4.3	147.5

12+38.98 = E.C.

S	4.8	47.0
+4	4.4	47.4
C	4.4	47.4
+9	4.5	47.0
N	4.9	46.9

18

6/7/23 Gregory

CROSS SECTION OF 18' Roadway
IMPERIAL AVE RELOCATION H. Bents
SEC. book 1080-64 for alignment ^{26' wide}

72.72

19

						8+00		
	8.09	156.59	148.50	Co. H. signal BM #10 3.0 x P.C.	N		11.1	145.5
		6+74.57 P.C.			+4		11.1	145.5
S		8.7	147.9		C		11.1	145.5
+4		8.7	147.9		+9		11.5	145.1
C		8.7	147.9		S		11.4	145.2
+9		9.1	147.5			Culvert somewhere here to be extended		
N		9.3	147.3			8+50		
		7+10.93 C.C.			S		11.3	145.3
					+4		12.2	144.4
N		9.9	146.7		+10		12.4	144.2
+4		9.9	146.7		C		11.4	145.2
C		9.8	146.8		+9		11.2	145.4
+9		9.8	146.8		N		11.2	145.4
S		10.0	146.6			9+00		
		7+47.29 = P.T.			N		10.9	145.7
S		10.6	146.0		+4		10.9	145.7
+4		10.5	146.1		C		11.0	145.6
C		10.5	146.1		+9		11.2	145.4
+9		10.4	146.2		+10		9.8	146.8
N		10.4	146.2		S		9.5	147.1

Plotted by Tolman 6-13-23

9+32

S	6.8	149.8
+L	7.8	148.8
+7	9.8	146.8
C	10.8	145.8
+9	10.3	146.3
N	10.3	146.3

9+41

N	10.1	146.5
+4	10.1	146.5
C	10.6	146.0
+2	9.6	147.0
+9	8.2	148.4
S	7.1	149.5

9+50

S	5.2	151.4
+4	5.4	151.4
C	9.9	146.7
+2	10.5	146.1
+9	10.1	146.5

N

10.0 146.6

9+67

N	10.0	146.6
+4	10.0	146.6
+12	10.4	146.2
C	8.6	148.0
+4	5.0	151.6
+9	3.5	153.1
S	2.5	154.1

9+82

S	0.0	156.6
+4	5.0	151.6
C	10.4	146.2
+9	9.8	146.8
N	9.8	146.8

10+00

N	9.7	146.9
+L	9.7	146.9
C	10.1	146.5
+3	10.0	146.6

+4 91 147.5

+9 8.1 148.5

S 7.5 149.1

10+25

S 8.7 147.9

+4 9.4 147.2

+6 10.0 146.6

C 9.9 146.7

+9 9.5 147.1

N 9.3 147.1

10+50

N 9.5 147.1

+4 9.4 147.2

C 9.7 146.9

+9 9.9 146.7

+10 9.3 147.3

S 8.9 147.7

11+10.89 P.C.

S 9.3 147.3

+4 9.3 147.3

C 9.4 147.2

+9 10.0 146.6

N 10.0 146.6

11+61.69 = CC

N 10.2 146.4

+4 9.9 146.7

C 9.2 147.4

+9 9.3 147.3

S 9.3 147.3

12+12.50 = P.T.

S 9.2 147.4

+4 9.2 147.4

C 9.2 147.4

+9 9.8 146.8

N 9.8 146.8

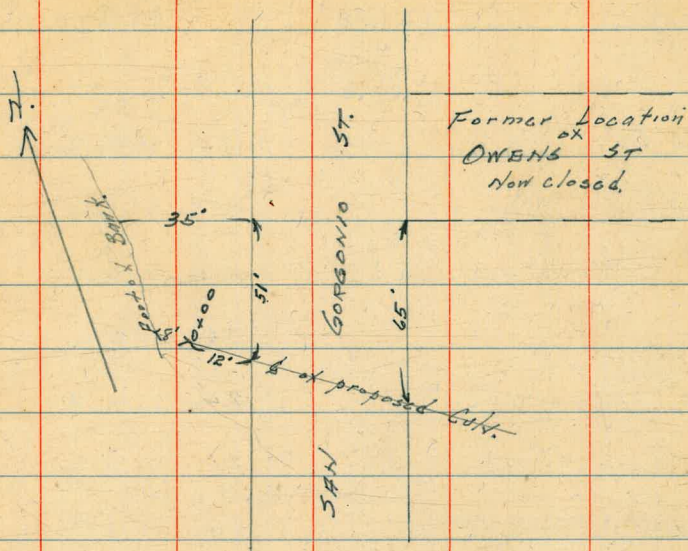
chk BM 8.85 147.74

8/6/23 Gregory and party.

Levels on proposed Culvert on San Geronimo and OWENS ST.

12.60	
12.50	0.15
12.87	0.01
12.56	0.00
12.93	0.00
0.07	11.47
3.22	0.84
-10	1.2
-8	2.2
0.0	3.5
0+30	6.1
0+45	7.5
0+51	10.2
0+54	14.3
0+60	17.4

Top Corb
SE Owens St
San Francisco



2/9/23

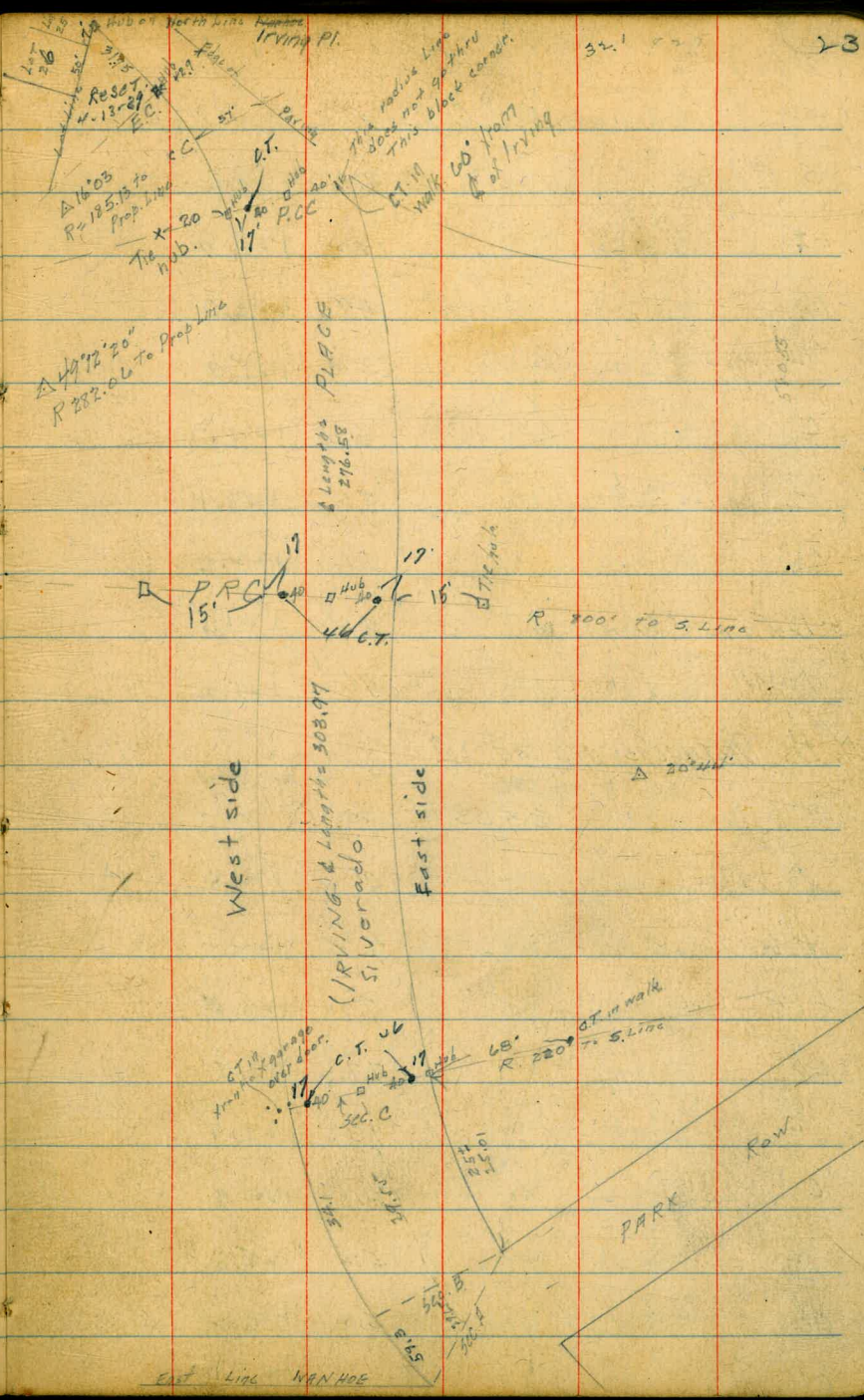
Graphic

CROSS SECTION OF 80 wide 14' x 65 13' quarters
 IRVING PLACE
 PARK Row TO EXCHANGE PL.

Top of Curve
 51' 3" from
 2' markers

BM	627	131.17	125.00
SEC. A			
± E	3.4	127.8	
cb	4.7	126.5	
1/4	6.3	124.9	
C	7.6	123.6	
1/4	8.4	122.8	
+ 8	8.6	122.6	
+ 10	7.5	123.7	
cb	7.9	123.3	
+ 4	8.1	123.1	
+ 6	8.9	122.3	
NW	10.0	121.4	
SEC. B			
NW	9.8	121.4	
cb	8.5	122.7	
1/4	7.5	123.7	
C	7.0	124.2	
1/4	6.4	124.8	
cb	5.2	126.0	
± E	3.4	127.8	

Plotted by Tolman
 11-C-23



32.1

23

Sec. C

SE

14 129.8

SE	16	127.6
+2	42	127.0
cb	49	126.3
1/4	52	125.8
C	65	124.7
1/4	76	123.6
cb	86	122.6
+12.5 front of garage	94	121.9
NW	96	121.6

48.25 on S 50.66 E of C 53.07 on N

SE	07	130.5
+4	40	127.2
cb	47	126.5
1/4	52	125.8
C	61	125.1
1/4	70	124.2
cb	82	123.0
+11	90	122.2
NW	92	121.8

N.B. Distances are on C

24.12 on SE

26.54 on NW

25.33 E of C

74.39 on S 76 E of C 79.62 on N

NW	98	121.4
+6	92	122.0
+12	77	123.5
cb	77	123.5
1/4	73	123.9
C	64	124.8
1/4	52	125.8
cb	50	126.2
+9	41	127.1

NW	94	121.8
+5	96	121.6
+6	90	122.2
cb	85	122.7
1/4	71	124.1
C	59	125.3
1/4	49	126.3
cb	39	127.3

+10		3.8	127.4	+7		4.3	126.9
SE		0.6	130.6	SE		0.0	131.2
96.50 on SE	101.37' E of C.		106.14 on NW	192.99 on SE	202.64' E of C.		212.29 on NW
SE		0.5	130.7	SE		1.5	129.7
+4		4.2	127.0	+10		4.4	126.8
cb		4.6	126.6	cb		4.6	126.6
1/2		5.3	125.9	1/4		4.7	126.5
C		5.8	125.4	C		5.5	125.7
+10		6.3	124.9	1/4		6.1	125.1
1/4		7.0	124.2	cb		7.2	124.0
cb		7.8	123.4	NW		8.0	123.2
NW		9.1	122.1	217.11 on SE	227.97' E of C.		238.83 on NW
144.74 on SE	^{50.66} 151.98' E of C. _{45.53}		159.22 on NW	NW		8.0	123.2
NW		8.7	122.5	cb		6.8	124.4
+8		8.2	123.0	1/4		5.2	125.9
cb		7.1	124.1	C		5.3	125.9
1/4		6.9	124.5	1/4		4.5	126.4
C		5.6	125.6	cb		4.7	126.5
1/4		5.2	126.0	+7		3.4	127.8
cb		4.6	126.6	SE		1.7	129.5

(241.20 on S) 253.30' E of C (265.36 on N)

TP 3.61 131.06 3.72 127.45

SE 1.5 129.6

t3 2.8 128.3

cb 4.3 126.8

1/4 4.4 126.7

C 5.1 126.0

1/4 5.5 125.6

cb 6.8 124.3

NW 7.8 123.3

265.36 on S 278.63' E of C 291.90 on N
25.22

NW 7.4 123.7

cb 6.0 125.1

1/4 5.7 125.4

C 5.2 125.9

1/4 4.8 126.3

cb 3.3 127.8

SE 2.0 129.1

289.50 on S 303.97' E of C = P.R.C. 318.44 on N

SE 0.4 130.7

t1 2.0 129.1

cb 3.6 127.5

1/4 4.3 126.8

C 5.1 126.0

1/4 5.4 125.7

cb 5.5 125.6

NW 6.7 124.4

341.33 on S 350.07' E of C 358.81 on N
26

NW 6.6 124.5

cb 5.3 125.8

1/4 5.4 125.7

C 5.0 126.1

1/4 4.3 126.8

cb 3.5 127.6

t8 2.4 128.7

t11 0.6 130.5

SE 0.5 130.6

393.16 on S 396.17' E of C 399.18 on N

SE 1.3 129.8

t4 1.6 129.5

7	30	128.1	1/4	66	124.5
cb	31	128.0	cb	72	123.9
1/4	43	126.8	NW	79	123.2
C	52	125.9	496.812 on S	488.37 E of C	479.93 on N
1/4	60	125.1	NW	80	123.1
cb	64	124.7	cb	77	123.4
NW	67	124.4	1/4	73	123.8
419.07 on S	419.22 E of C	419.37 on N	C	67	124.4
NW	72	123.9	1/4	62	124.9
cb	66	124.5	cb	53	125.8
1/4	62	124.9	SE	35	127.6
C	58	125.3	548.64 on S	534.47 E of C	520.30 on N
1/4	45	126.6	SE	52	125.9
cb	33	127.8	cb	60	125.1
SE	24	128.7	1/4	70	124.1
444.98 on S	442.27 E of C	439.56 on N	C	75	123.6
SE	26	128.5	1/4	80	123.1
cb	38	127.3	cb	83	122.8
1/4	50	126.1	NW	87	122.4
C	62	124.9			

560.67 on W

IRVING

51328

600.44 on E

580.55 E of C = P.C.C

+ 2.90 = Edge of paving

131.04
987 121.22

NW

9.5 121.6

31.75' E of End of Curve

cb

9.0 122.1

47.9' N. of 3 Line produced
Edge paving

11.42 119.64

1/4

8.7 122.4

N 1/4

11.0 120.1

C

8.4 122.7

cb

11.4 119.7

1/4

7.6 123.5

N

11.5 119.6

cb on cement.

131.06
6.95 124.11

83.05' E. of End of Curve = End of Curve on tree

SE

6.6 124.5

N

13.1 118.0

612.02 E of C
Center of Curve580.6 on W.
see sketch.

cb on cement

13.83 117.23

23' N. of St. = Edge of paving

8.48 122.58

5 1/4

8.7 122.4

C

9.0 122.1

1/4

9.4 121.7

cb

9.7 121.4

N

9.6 121.5

643.61 E of C
End of Curve

612.53 on W

N

10.7 120.4

cb

10.5 120.6

1/4

10.1 121.0

C

10.2 120.9

++ for Imperial Ave thru French to
cuts on S. side 10' offset from Paving

29

224.96
~~258.72~~
6.24

				Sta 90+65		
91+30.74 EC	8.64	267.36	258.72	-Co. BM 266.96		
92 -		7.70	259.06	259.01	+ 0.05 ✓	
93 -		7.63	259.73	259.91	- 0.18 ✓	
94 -		6.98	260.38	260.50	- 0.42 ✓	
95 -		5.83	261.53	261.68	- 0.15 ✓	
95 +25 BK		5.51	261.85	261.90	- 0.05 ✓	
96 -		4.96	262.40	262.83	- 0.43 ✓	
97 -		2.34	265.02	264.06	+ 0.96 ✓	
98 - TP	4.10	270.96	0.50	266.86	265.30	+ 1.56 ✓
99 -		3.66	267.30	266.53	+ 0.77 ✓	
100 -		1.70	269.26	267.76	+ 1.50 ✓	
+62.64 Paving Co. Line		2.34	268.62	268.53	+ 0.09 ✓	

++ for S. edge of Pavement 040 Super. Elv.

Ave hole

1025 253.87 248.62 BM #70173

79+18 ⁹⁰ BC		11.30	242.57	242.06	- 0.49 ✓	
+ 50		9.72	244.15	243.85	+ 0.30 ✓	
80 -		8.13	245.74	245.10	+ 0.64 ✓	
+ 50		7.20	246.67	246.35	+ 0.32 ✓	
81 - Brk		5.94	247.95	247.60	+ 0.35 ✓	

+50		5.07	248.80	248.11	+ 0.69 ✓			
82 -		4.53	249.34	248.62	+ 0.72 ✓			
+50		4.86	249.01	249.14	- 0.13 ✓			
83 -		4.07	249.80	249.65	+ 0.15 ✓			
+50		3.64	250.23	250.17	+ 0.06 ✓			
84 -		4.33	249.54	250.68	- 1.14 ✓			
+50 Brk.		4.95	248.92	251.20	- 2.28 ✓			
85 -		3.27	250.60	251.85	- 1.25 ✓			
+50 T.P. 8.83	260.62	2.08	251.79	252.50	- 0.71 ✓			
86 -		5.82	254.80	253.15	+ 1.65 ✓			
+50 Brk		6.90	253.72	253.80	- 0.08 ✓			
87 -		8.54	252.08	254.32	- 2.24 ✓			
+50		8.84	251.78	254.85	- 3.07 ✓			
88 -		7.80	252.82	255.37	- 2.55 ✓			
+50		7.77	252.85	255.90	- 3.05 ✓			
89 -		4.28	256.34	256.42	- 0.08 ✓			
+50		4.73	255.89	256.95	- 1.06 ✓			
90 -		3.37	257.25	257.47	- 0.22 ✓			
+50 Brk		1.21	259.41	258.00	+ 1.41 ✓			
91 -		1.85	258.77	258.44	+ 0.33 ✓	190	258.72	258.72
+30.74 EC.		2.0	258.62	258.71	- 0.09 ✓			

Imperial Hvc + 4 - 0+00
Thru Encanto

N

S

642
51

31

ch									
28.7	0+51.14 Paving		164.48						
	+79.84	+1.39	164.49 5.51 4.33	164.29 163.42	164.09 5.91 5.21	+0.10	163.15 8.26 171.41	673 623 713 164.98	
	1+08.54	+0.19	164.30 5.70 5.24	164.10 163.2	163.90 6.1 5.43 5.21	+1.37	163.53 6.23 170.46 12.83	171.41	405 163.95
	1+37.27 EL.	+1.13	164.12 5.88 4.71 1.18	163.20 162.20	163.72 6.28 4.73 +1.55	+1.55	157.63 0.24 158.47 12.13 146.34 4.64 150.98		163.15 685 170.00 10.08 159.92 0.00 160.52 1.201 148.51 6.50 155.01
	2 -	+4.31	163.81 4.24 4.31	163.52	163.52 6.28 4.73 +1.55 4.55 3.54	+3.02	171.41		
	+50	+3.78	31 5.78	163.20	6.90	+6.45	5.53 65.88	662 647.7	615 5.26
	3 - Brk	+4.20	7.22 3.02	162.88 162.58	2.77	+4.45	6.92 64.49	613 63.28	612 63.28
	+25 "	+4.10	3.45	162.55 162.40	7.55 2.60	+4.25			4.26 66.45 5.24 2.92
	+50	+3.39	7.93 4.54	162.17 162.02	4.95	+5.18	6.73 65.27		
	+75	+2.66	5.22	161.62 161.47	8.46 0.85	+7.63			
	4 - "	+1.94	7.30	160.76	7.24 0.20	+8.39			
	+25 "	+1.75	8.24	159.81	10.19 2.14	+8.05			
	+50 Brk	+1.93	4.37	158.70	11.80 2.30	+7.50			
	5 -	-0.38	4.22 4.60	156.30	0.21	+3.91			
	+50	-5.18	11.80 11.2	153.90	6.64 1.80	-1.02			
	6 +00	-6.32	11.2	152.10	7.68	-1.68			
	6+25 Brk	-5.65	13.2	150.30	10.22 11.00	-0.98			
	+50	-4.05	14.23 1.95 6.90	149.23	14.09 11.71	-0.62			
	6+74.57 B.C.	-3.95	14.83 7.65 6.20	148.43	14.73 7.25 7.20	-0.95			
	7+00	-3.27	14.72 5.14 2.2	147.99	14.19 6.82 8.10	-1.28			

		N	S	
7+25 Brk	-1.62	^{147.51} 17.50 912	147.41	^{147.91} 4.10 810
+47.29 EC	-0.68	^{147.39} 7.02 830	147.59	^{147.79} 7.22 862
8 -	-1.68	^{7.82} 0.50	147.19	^{8.25}
+50 Brk	-1.72	^{8.53} 8.11	146.9	^{9.23}
9 -	-1.50	^{7.89} 7.39	147.12	^{7.57}
+50	-0.78	^{7.67} 4.49	147.34	^{7.93}
10 -	-0.51	^{147.57}	147.57	^{147.57}
+50	-0.08	^{147.49}	147.79	^{148.09}
10 + 72.14	-0.81	^{147.40}	147.94	^{148.49}
11 + 10.89 BC	-2.81	^{147.36}	148.06	^{148.76}
+36.29	-3.08	^{147.48}	148.18	^{148.88}
+61.69	-1.74	^{147.59}	148.29	^{148.99}
+87.09	-1.86	^{147.71}	148.41	^{149.11}
12+12.5 EC	-1.24	^{147.82}	148.52	^{149.22}
+50	-1.66	^{148.31}	148.71	^{149.11}
13 -	-1.19	^{148.93}	148.93	^{149.11}
+50	-2.22	^{149.15}	149.15	^{149.15}
14 -	-2.22	^{149.36}	149.36	^{149.36}
+25	-2.06	^{149.55}	149.55	^{149.55}
+50	-1.75	^{149.88}	149.88	^{149.88}
+75	-2.15	^{150.35}	150.35	^{150.35}

0.07 51 1.00 1 5
0.07 0.07 0.07
22 5 0x7 55 32
60 11 51 710

150.98 NO
346
147.54
155.01 NO
819
146.82
524
152.06

12 12

222
146.79

5 11 32
10 23
15 35
20 47 +

6

+93.49 PC.	-	156	¹¹⁸¹ 150.70	150.90	150.70	-0.94
15	-	2.71	¹⁰⁵⁹ ₁₃₂ 151.32	151.07	150.82	^{11.09} _{12.0} -0.91
+25	-	3.05	¹¹⁷⁸⁵ ₉₃₃ 152.08	151.83	151.58	^{11.27} _{10.28} -1.14
+50	-	3.09	¹²⁰⁰ ₂₉₁ 153.0	152.75	152.50	^{10.63} _{9.41} -1.22
+75	-	2.57	¹⁰⁰⁰ ₇₇₃ 153.98	153.73	153.48	^{8.60} -1.07
16	-	0.66	⁷⁶⁵ 154.96	154.71	154.46	^{8.80} _{7.45} -0.85
+25	+	0.77	⁵⁹⁷ ₉₁₈ 155.94	155.69	155.44	^{7.45} _{6.47} -0.96
+50	-	0.06	⁵⁹⁷ ₇₉₉ 156.92	156.67	156.42	^{6.64} _{5.69} -1.15
+75	+	0.16	⁴⁴⁴ ₃₂₈ 157.90	157.65	157.40	^{5.43} _{4.51} -0.92
17	-	1.26	⁴⁸⁷ ₃₁₁ 158.80	158.55	158.30	^{4.82} _{3.61} -0.92
+25	+	0.50	²³⁷ ₁₈₁ 159.54	159.29	159.04	^{3.11} _{2.87} -0.24
+50	+	0.55	175 160.16	159.91	159.66	^{2.25} -0.02
+75	+	0.16	131 160.60	160.35	160.10	^{1.81} _{1.77} +0.44
18	+	0.37	¹⁰¹ ₂₂ 160.90	160.65	160.40	^{1.51} _{1.64} +0.87
+25	+	0.77	⁰⁸⁷ ₂₀ 161.04	160.79	160.54	^{1.27} _{2.70} +0.62
+34.17 EC	+	0.88	⁴¹¹ ₂₅₃ 161.00	160.81	160.60	^{4.81} _{3.6} +0.45
19	+	1.51	⁴⁵³ ₃₀₄ 162.88	162.98	162.88	^{2.22} +2.31
+60	-	1.01	^{587161.03}	161.73		^{4.38} _{5.00} +0.88
20	-	1.74	⁶¹² ₄₂₈ 161.13	161.23		^{4.07} 0.0
+50	-	1.85	^{415161.76}	161.36		-0.62

1265
1337

15206
220
149.76
1715
161.91
76
161.16
425
76541

5) 490
98 33

N				S					
31			-2.48	⁶¹⁵ 402	161.39	161.49	283	-2.81	
+50			-2.25	³⁸⁹ 617	61.52	161.62	89 607	-2.72	
22			-1.98	³⁷⁶ 572	61.65	161.75	610	-2.34	
+50			-0.37	³⁶³ 450	61.78	161.88	438	-1.75	
23			-0.88	³⁵⁸ 450	61.83		500	-1.42	
	10.82	Elev stake = 161.86 174.28	-0.04	³⁵¹ 355	61.90	162.00	423	-0.72	
+50			12.15	-0.42	162.13	162.55	161.72	1256	-0.83
24			11.27	-0.19	163.01	163.20	162.63	1165	-0.57
+50			10.52	-0.09	163.76	163.85	163.44	1084	-0.41
25	Bk		9.65	+0.13	164.63	164.50	163.53	1075	-0.97
+50			8.80	-0.46	165.48	165.94	164.90	938	-1.04
26			7.12	-0.22	167.16	167.38	166.18	810	-1.20
+50			5.27	+0.19	169.01	168.82	170.54	3.74	+1.72
27			3.92	+0.10	170.36	170.26	172.67	1.61	+2.41
+50			2.60	-0.02	171.68	171.70	174.12	0.16	+2.42
28	T.P.N. Hub 9.85	18358	0.55	+0.59	173.73	173.14	174.91	9.67	+4.77
+50			8.70	+0.30	174.88	174.58	174.93	8.65	+0.35
+75	Bk		8.37	+0.03	175.21	175.30	175.23	8.35	+0.05
29	P.O.T.		8.00	+0.04	175.58	175.54	176.38	7.20	+0.14
+50			7.20	+0.35	176.38	176.03	177.18	6.40	+1.15
30			6.55	+0.51	177.03	176.52	177.62	5.96	+1.10

16541
165
163.76 = BM opposite yellow house

175.20
175.16
175.58
175.06
175.06

+50		620 +0.37	177.38	177.01	179.58	+2.57	4.00	
31		555 +0.53	178.03	177.50	179.23	+1.73	4.35	
+50		517 +0.41	178.41	178.00	180.54	+2.54	3.04	
32		467 +0.42	178.91	178.49	181.08	+2.59	2.50	
+50		462 -0.02	178.96	178.98	181.08	+2.10	2.50	
33		486 -0.25	178.72	179.47	179.15	-0.32	4.43	
+50		472 -1.16	178.86	179.96	178.58	-1.38	5.00	
34		500 -1.87	178.58	180.45	179.13	-1.32	4.45	
+50		570 -2.06	177.88	180.94	178.53	-2.41	5.25	
35		316 -1.01	180.42	181.43	179.46	-1.97	4.12	
+50		294 -1.28	180.64	181.92	179.58	-1.34	4.00	
36		250 -1.33	181.08	182.41	180.35	-2.06	3.23	
+50		190 -1.22	181.68	182.90	181.37	-1.53	2.21	
37	TP N hub Brk 13.00	195.75	0.83 -0.66	182.75	183.41	182.36	-1.05	1.22
+25		1232 -0.30	183.43	183.73	183.18	-0.55	12.57	
+50		1152 0.0	184.23	184.23	183.90	-0.33	11.85	
+75		1070 +0.16	185.05	184.89	184.52	-0.37	11.23	
38	Brk	981 +0.15	185.88	185.73	185.37	-0.36	10.38	
+50		820 0.0	187.55	187.56	187.45	-0.11	9.30	
39		643 +0.02	189.32	189.30	188.85	-0.45	6.90	

19575 Rd N

\$ Rd

+25 Brk	530 + 0.15	190.45	190.30	190.08	- 0.22	567	
+50	400 + 0.25	191.75	191.50	193.70	+ 2.20	205	
40 TPN tub 12.20	20588	207 - 0.22	193.68	193.90	198.06	+ 4.16	7.82
+50	✓ 997 - 0.39	195.91	196.30	201.58	+ 5.28	430	
+75 Brk	✓ 696 + 1.42	198.92	197.50	203.76	+ 6.26	212	
41	✓ 542 + 1.96	200.46	198.50	204.34	+ 5.84	154	
+50	✓ 478 + 0.60	201.10	200.50	205.16	+ 4.66	072	
TP tub							
+75 Brk 10.30	21166	454 - 0.16	201.34	201.50	205.28	+ 3.78	0.60
42	✓ 1007 - 0.59	201.59	202.18	206.36	+ 4.18	530	
+50	✓ 893 - 0.81	202.73	203.54	206.62	+ 3.08	504	
43 Brk	800 - 1.24	203.66	204.90	207.34	+ 2.44	432	
+50	625 - 0.16	205.41	205.57	208.01	+ 2.44	365	
44	515 + 0.28	206.51	206.53	207.18	+ 0.65	448	
+50	375 + 1.01	207.91	207.35	210.61	+ 3.26	105	
011'20" L			207.33				
+8857 Δ	363 + 0.72	208.03	207.97	211.28	+ 3.31	038	
45			207.57				
+75 Brk			208.17		+ 3.42		
+50	+ 0.99		208.23		+ 2.10		
+75	+ 0.35		208.59		+ 2.31		
46	- 0.12		208.72		+ 1.95		

Co. BM #12
 Rod 780 = 203.86
 210.00
 6.14
 209.98

11.38
 9.72
 3.62
 203.86
 9.09
 212.95

20957 538
 196
 3.42

20823 472
 202
 270

20859 436

20872 423
 228

375
 0.94

Item	Change	Balance	Notes	Balance	Change	Balance	Notes
46 + 25 Bk	- 0.23	208.65	212.96 163	212.96	+ 1.36	214.32	853 430 442 480
+ 50 Bk	- 0.53	208.53	211.32 13.04	211.32	+ 1.45	212.77	608 7.77 5.18 4.40
47	- 0.64	208.15	224.36	208.15	+ 1.08	209.23	357 10.22 2.63
+ 50	- 0.90	207.77		207.77	+ 0.78	208.55	1.58 1.40
48 Bk	- 0.67	207.40		207.40	+ 0.32	207.72	581 7.97 4.98 4.41
+ 50	- 0.87	207.97		207.97	+ 0.47	208.44	854 3.86 4.07
49	- 1.06	208.54		208.54	+ 0.37	208.91	530 206.02
+ 50 Bk	- 0.85	209.10		209.10	+ 1.10	210.20	
50 -	- 0.94	210.32		210.32	+ 1.00	211.32	
+ 50	T.P. on this day = 2/1/32 - 0.23			211.55	+ 1.00	212.55	
51	- 0.51	212.77	11.59 12.1 - 0.51	212.77	+ 1.12	213.89	11.59
+ 50	- 0.71	214.0		214.0	+ 1.21	215.21	10.36
52	- 1.39	215.22		215.22	+ 1.29	216.51	9.14
+ 50	- 0.51	216.45		216.45	+ 1.63	218.08	7.91
53	- 0.2	217.67		217.67	+ 1.53	219.20	6.49
+ 50 Bk	- 0.26	218.90		218.90	+ 1.62	220.52	5.46
54	- 0.26	219.43		219.43	+ 1.84	221.27	4.93
+ 50	- 0.43	219.96		219.96	+ 1.78	221.74	4.40
55	- 0.85	220.49		220.49	+ 1.72	222.21	3.97
+ 50	- 0.23	220.02		220.02	+ 1.57	221.59	3.94

	+75 Brk	-0.2	221.3	3.06	+1.58	224.36	
56		00	221.23	3.13	+1.86	222.72	
	+50	+0.35	221.10	3.26	+2.66	218.23	
57		-0.05	220.98	3.38	+2.56	214.68	
	+50	-0.80	220.85	3.51	+2.34	218.23	P.N. stub sta. 6100
58		-5.66	220.72	3.64	+2.30	214.68	
	+50	-4.94	220.6	3.76	+2.12	218.23	
59		-3.39	220.47	3.89	-0.10	214.68	
	+50	-2.36	220.34	4.04	+1.91	218.23	
60		-2.14	220.22	4.16	+1.11	214.68	
	+50	-1.91	220.09	4.39	+0.51	218.23	
61		-1.73	219.96	4.72	+0.34	214.68	
	+25 Brk	-1.71	219.9	4.56	+0.86	218.23	
	+50	-1.26	220.0	4.46	+0.56	214.68	
62		-2.69	222.20	4.26	-0.1	218.23	
	+50	-2.84	222.40	4.06	-0.19	214.68	
63		-2.91	222.60	3.86	-0.22	218.23	
	+25 Brk	-3.24	220.90	3.76	+0.56	214.68	
	+50	-3.80	220.85	3.61	+1.20	218.23	
	+75	-3.50	221.03	3.43	+1.55	214.68	

1/24/63
2667
2

224.68
7.40
217.24
1.12
223.36

224.68
1.64
222.72
1.96
224.68
6.45
218.23
6.23
214.68

64		-4.13	221.49	2.97	+1.51	224.46
+25 Brk		-3.42	221.98	2.48	+0.98	1.48
64+50	1.94	-1.51	222.52	9.84	+2.42	222.98
65 0		-0.61	223.60	8.36	+1.76	8.98
+50		-0.82	224.68	7.28	+1.55	231.96
66		-0.71	225.75	6.21	+1.78	2.40
+50 Brk.		-1.0	226.82	5.14	+1.41	229.56
+75 ✓		-0.78	227.31	4.65	+1.52	T.P. N.T. Hub Sta 68+00
67 ✓		-0.23	227.69	4.27	+1.72	242.62
+25 ✓		-0.2	227.98	3.98	+1.81	0.27
+50 ✓		+0.46	228.15	3.81	+1.98	243.89
68		+1.44	228.40	3.56	+2.26	243.89
+50		+0.55	228.65	5.19	+3.69	+2.00
69 = bridge		+1.0	228.90	4.94	+1.0	231.89
+50		-2.11	229.15	4.69	-2.33	1.25
70		-2.23	229.40	4.44	-1.68	233.84
+50		-1.39	229.65	4.19	-1.07	4.30
71		-0.66	229.90	3.94	-0.57	229.54
+50		-1.7	230.15	3.69	-0.91	
72 ✓		-1.49	230.40	3.44	-0.44	


+50				-0.46	230.65	3.39	-0.12
73 Brk.				+0.09	230.90	2.94	+0.33
+50				+0.17	231.72	12.17	+0.27
74				+0.41	232.55	11.34	+0.64
+50				+0.32	233.57	10.52	+0.82
75				+0.45	234.19	9.70	+0.95
+50				+0.15	235.01	8.88	-1.12
76				+0.06	235.83	8.06	-2.34
+50				+0.08	236.65	7.24	-2.26
77				+0.9	237.48	6.41	-1.76
+25 Brk.				+0.72	237.90	5.99	-1.7
+50				+0.39	238.52	5.37	-1.84
78				+0.24	239.77	4.12	-0.3
+50 Brk.	00	2.86	241.03		So Side = 241.03	2.86	-0.65
79	+1.03	2.68	141.21		So. Side = 242.76	1.13	-0.8
+18.9 P.C.		1.23	242.66		✓ ✓ = 243.06	0.83	

Old Town Contours

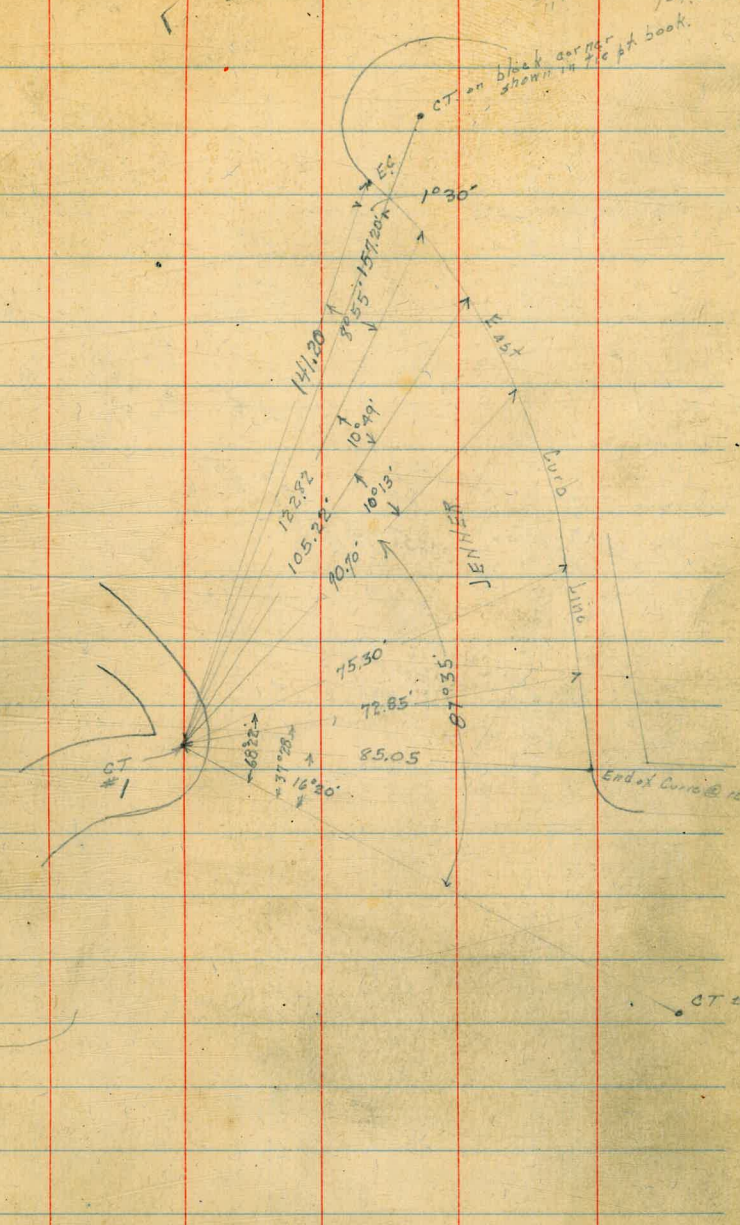
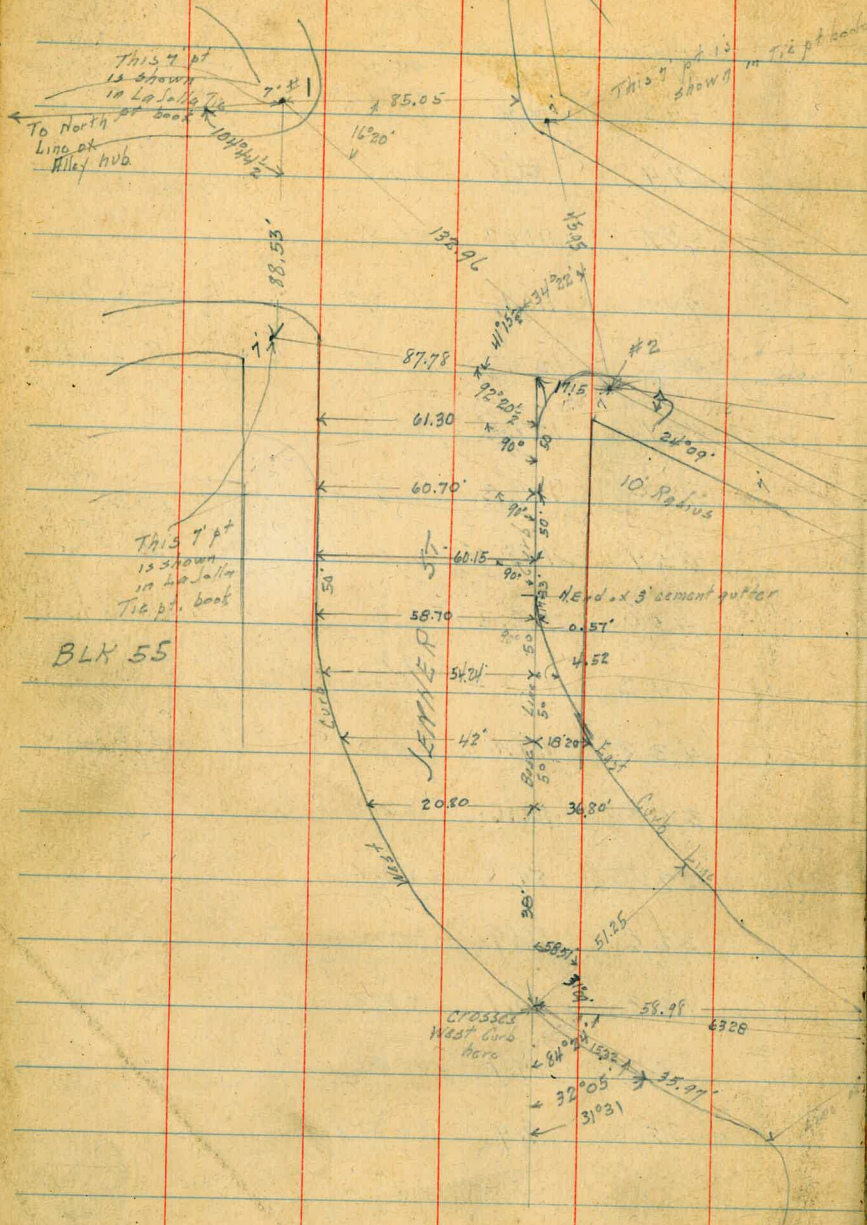
	W. Intersection	Az	V. Angle	Upper	Lower	Hor Dist	Verl Dist	Red	HI	Ed.
A	Dis. from <i>Q. Man</i> Church + <i>Mason</i> 18323	132° 30'						5.0	143.06	143.4 138.06
1		137° 40'	-21° 15'	519	39	481	34.0	13.2	124.9	El. v
2		✓ ✓	-20° 05'	533	66	467	58.0	21.2	116.9	
3		✓ ✓	-21° 04'	550	100	450	87.0	32.4	105.8	
4		✓ ✓	-21° 28'	570	140	430	122	47.5	90.6	
5		- ✓	-22° 10'	581	162	419	140	56.5	71.7	
6		- ✓	-22° 19'	587	174	413	148	61.1	77.0	
7		- ✓	-21° 44'	597	198	401	173	68.0	65.9	ground 5' lower
8		✓ ✓	-22° 28'	633	266	317	228	94.7	41.4	--- 2' "
9		✓ ✓	-22° 20'	660	320	340	272	112.5	25.6	
10		✓ ✓	-22° 13'	670	342	320	280	119.0	19.1	
11		✓ ✓	-21° 31'	681	362	317	314	123.5	14.6	Sedge road
12		✓ ✓	-20° 29'	692	387	308	338	125.9	12.2	N " "
13		149° 08'	-20° 22'	697	386	307	340	125.2	12.9	N " "
14		✓ ✓	-21° 23'	685	320	315	320	125.6	12.5	S " "
15		✓ ✓	-21° 11'	678	285	312	309	120.0	18.1	T. b bank
16		- ✓	-21° 42'	680	300	350	259	103.1	35.0	
17		- ✓	-21° 17'	630	260	370	224	87.8	50.3	
18		✓ ✓	-21° 47'	607	214	392	185	72.8	65.3	

change elevations

	Hz	✓ Angle	Upper	Lower						
19	149° 08'	-20° 31'	575	150	425	Hor Dist	Vert Dist	13800		
						133	492	88.9	942	
20	-	-20° 58'	564	125	436	112	432	94.9	100.2	
21	-	-18° 56'	545	70	455	81	27.6	110.5		
22	165° 20'	-17° 35'	522	84	458	77	24.3	113.8	119.1	
23	✓	-19° 06'	559	118	441	106 133	358	102.3		
24	✓	-18° 47'	571	142	424	127	43.3	94.8		
25	✓	-20° 04'	642	284	358	252	91.5	46.6		
26	✓	-19° 33'	656	312	344	278	98.4	39.7		
27	✓	-19° 12'	693	376	307	343	119.9	18.2		top bank
28	✓	-19° 26'	702	409	298	360	126.8	11.3		↓ Road
29	✓	-18° 28'	712	429	288	383	127.4	10.7		N Road
30	174° 00'	-17° 12'	723	446	277	408	126.0	12.1		N "
31	✓	-18° 12'	717	434	285	392	128.8	9.3		↓ "
32	✓	-17° 48'	711	422	289	384	122.8	15.3		top bank
33	✓	-19° 02'	622	244	378	218	75.2	62.9		
34	✓	-18° 14'	585	170	415	156	50.5	87.6		
35	✓	-18° 05'	563	126	437	117	37.2	100.9		
36	✓	-16° 58'	543	86	457	78	23.8	114.3		
37	183° 02'	-15° 12'	525	50	475	47	12.7	125.4		
38	✓	-16° 14'	548	96	452	89	25.8	112.3		

	Azi	V. Angle	upper	Lower						
39	183° 0'	-16° 50'	577	1.54	423	Hor Dist	Vert Dist	13806		
						143	42.9	95.4		
40	-	-17° 19'	633	2.66	367	243	75.6	62.5		
41	-	-17° 21'	652	3.09	348	274	86.5	50.6		
42	-	-16° 17'	707	4.14	293	371	111.43	26.5		
43	-	-16° 15'	716	4.32	284	400	116.1	22.0		Top bank
44	-	-16° 43'	726	4.48	276	410	123.7	14.4		E road
45	-	-16° 05'	740	4.80	260	441	127.8	10.3		N "
46	189° 52'	-15° 06'	757	5.14	243	480	129.3	8.8		" "
47	✓	-15° 49'	745	4.80	255	454	128.5	9.6		Sl "
48	-	-15° 44'	742	4.84	258	450	126.3	11.8		N road to 
49	✓	-15° 35'	738	4.76	262	443	123.2	9.9		ground 5' lower sl " " "
50	✓	-15° 40'	736	4.60	270	438	119.8	18.3		Tab bank
51	✓	-	699	3.86	307	358	100.6	37.5		
52	-	-16° 17'	657	3.14	343	290	84.5	53.6		
53	✓	-16° 28'	623	2.46	377	226	66.9	71.2		
54	✓	-16° 10'	575	1.50	425	138	40.1	98.0		
55	✓	-15° 48'	546	.92	454	85	24.1	114.0		
56	✓	-14° 21'	520	.40	480	38	9.4	128.7		

3/6/1914 Gregory JENNER ST CURBS



54.30
20
58.70

74.45
97.48
78.3
11

179.60
74.10
104.40
24.4

97.28
108.37
97.48

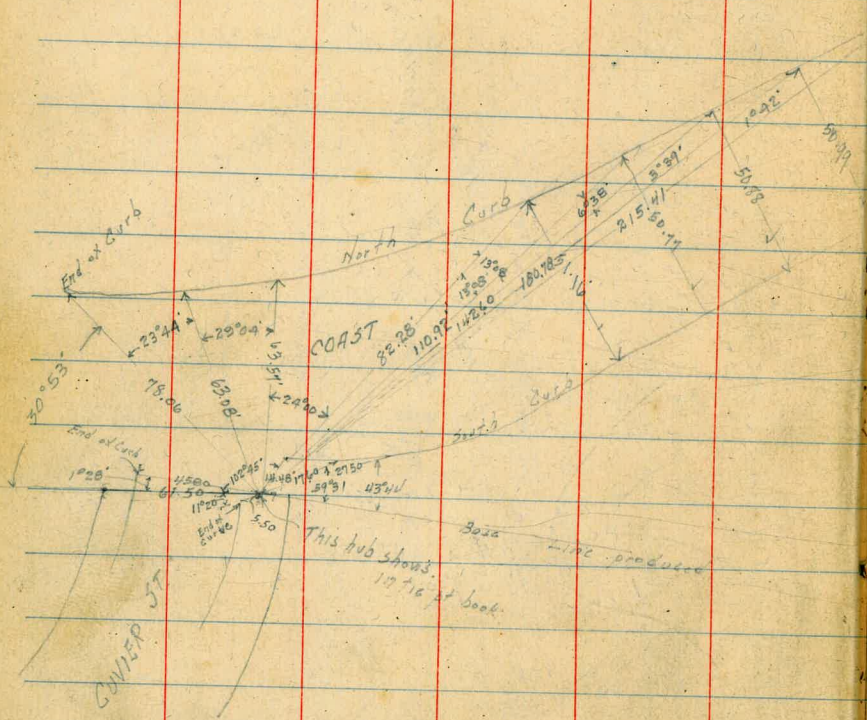
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100.9

114.32
116.40
103.8
23

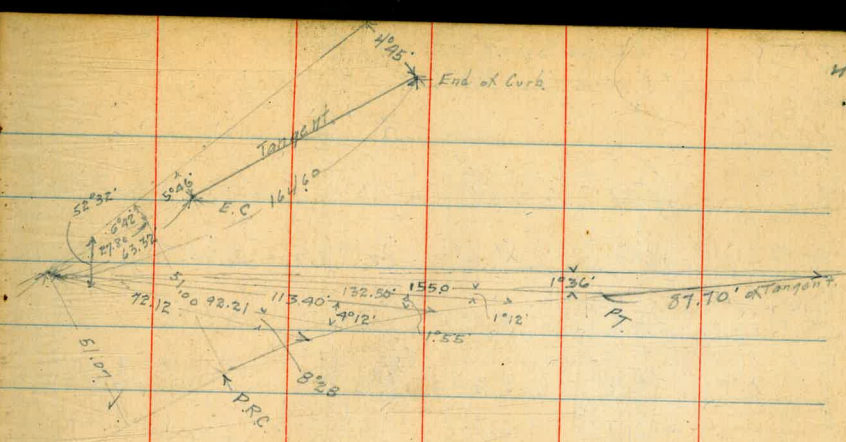
116.02
1.30

3/6/20

CUVIER & COAST BLVD CURBS



45



53.77	82.101	107.43	179.30	24.60	148.45	147.66	31.03	3.20	5.20	43.60	88.17	37.57	35.09
50.53	53.27	82.46	170.27	126.16	87.40	148.93	120.00	3.00	2.00	33.00	27.57	36.44	12.00
30.55	78.06	63.08	43.57	20.00	13.09	148.00	100.00	1.00	1.00	33.00	1.55	1.00	1.00

4/8/24

Cross Section of Canyon St 70' wide
from W.L. of Shaft to E To Bay. 10' s/w

5.55

46

					1/4	2.8	2.8
	0.31	20.98	20.67	SW Canyon Reservoirs	C	2.4	3.4
TP	1.62	9.67	12.93	8.05	+10	2.6	3.0
TP	3.08	5.55	7.20	2.47	1/4	3.1	2.5
		W.L. Shaft	✓	70' wide 10' s/w	+2.5	3.7	1.9
N			2.4	3.4	cb	3.3	2.3
cb			3.2	2.4	N	2.8	2.8
+9			3.5	2.1		1/4 ✓	
1/4			3.1	2.5	N	3.1	2.5
C			2.5	3.1	cb	3.3	2.3
1/4			2.8	2.8	+9	3.9	1.7
+11			3.3	2.3	1/4	3.1	2.5
cb			2.5	3.1	+3	2.5	3.1
+9			2.5	3.1	C	2.5	3.1
S			1.6	4.0	+10	2.7	2.9
		W.L. cb	✓		1/4	3.2	2.4
S			1.9	3.7	+11	3.7	1.9
+1			2.6	3.0	cb	2.8	2.8
cb			2.7	2.9	S	2.2	3.4
+5			3.5	2.1			

5.55 C+K. ✓

S	2.4	3.7
cb	2.8	2.8
+5	4.0	1.6
1/4	3.2	2.4
c	2.3	3.3
1/4	3.1	2.5
+2	4.1	1.5
+8	4.1	1.5
+9	3.3	2.3
cb	3.0	2.6
N	2.8	2.8
	E 1/4 ✓	
N	3.7	1.9
cb	3.8	1.8
+10	4.3	1.3
1/4	3.3	2.3
c	2.8	2.8
1/4	3.2	2.4
+11	4.1	1.5
cb	3.0	2.6

5.55

Canyon St 47

S	2.6	3.0
	E cb ✓	
S	2.9	2.7
cb	3.1	2.5
+2	3.9	1.7
1/4	2.8	2.8
c	2.9	2.7
1/8	2.9	2.7
+8	4.1	1.5
1/4	4.4	1.4
+4	3.8	1.8
cb	4.0	1.6
N		
	✓ EL of Shafter. ✓	
N	4.0	1.6
cb	4.1	1.5
+2	4.6	1.0
+8	4.5	1.1
1/4	3.8	1.8
c	3.1	2.5
1/4	3.1	2.5

5.55			5.55			Canon St. 4E		
+10		3.8	1.8	N		3.9	1.7	
cb		3.3	2.3	cb		4.1	1.5	
+9		3.1	2.5	+6		5.5	0.1	
S		3.5	2.1	1/4		4.5	1.1	
+2		3.3	2.3	U		4.1	1.5	
	30' E ✓			+5		3.8	1.8	
-2		3.9	1.7	1/4		4.5	1.1	
S		3.9	1.7	+10		4.9	0.7	
+1		3.4	2.2	cb		4.1	1.5	
cb		3.3	2.3	+9		3.9	1.7	
+2		4.3	1.3	S		5.0	0.6	
1/4		3.1	2.5	+4		5.0	0.6	
C		3.5	2.1		100' E ✓			
1/4		4.3	1.3	-5		5.9	-0.3	
+9		4.9	0.7	S		5.3	0.3	
cb		4.2	1.4	+3		4.3	1.3	
N		3.9	1.7	cb		4.6	1.0	
	42' E ✓			+4		5.3	0.3	
N	Cr of door to Cannery	3.86	1.69	1/4		4.6	1.0	
	65' E			C		4.3	1.3	

5.55

1/4	4.9	0.7
+8	5.6	0.0
+11	4.6	1.0
cb	4.6	1.0
N	3.9	1.7

135' E ✓

N	4.7	0.9
cb	4.6	1.0
+3	5.9	-0.3
+7	6.1	-0.5
1/4	5.2	0.4
c	4.6	1.0
1/4	5.2	0.4
cb	6.0	-0.4
+2	4.4	1.2
+8	4.6	1.0
S	6.2	-0.6
+7	6.6	-1.0

158' E ✓

-7	6.7	-1.1
----	-----	------

5.55

CANON ST 49

-1	6.4	-0.8
S	5.5	0.1
+2	4.8	0.8
cb	5.1	0.5
+4	6.5	-0.9
+9	5.2	0.4
1/4	5.4	0.7
c	4.9	0.7
1/4	5.2	0.4
+4	5.2	0.4
cb	6.7	-1.1
+2	5.0	0.6
N	4.9	0.7

163' E

N	5.0	0.6
+7	5.2	0.4
cb	6.9	-1.3
+8	5.2	0.4
1/4	5.1	0.5
c	4.9	0.7

5.55

+9	5.6	0.0
1/4	4.9	0.7
+7	7.1	-1.5
cb	7.3	-1.7
S	6.9	-1.3
+8	7.0	-1.4

175' E

-8	8.3	-2.7
S	8.0	-2.4
cb	7.2	-1.6
1/4	6.4	-0.8
c	5.1	0.5
1/4	5.6	0.0
+8	7.2	-1.6
cb	6.8	-1.2
+5	5.4	0.2
N	5.6	0.0

190' E

-5	6.8	-1.2
N	6.8	-1.2

5.55

Canon St 50

cb	7.1	-1.5
1/4	7.8	-2.2
c	8.1	-2.5
1/4	8.5	-2.9
cb	8.9	-3.3
S	9.1	-3.5
+10	9.5	-3.9

200' E

-10	10.2	-4.6
S	10.0	-4.4
cb	9.8	-4.2
1/4	9.2	-3.6
c	8.9	-3.3
1/4	8.5	-2.9
cb	8.4	-2.8
N	8.3	-2.7
+5	8.3	-2.7

See page 55 for interpolation of
180' E.

4/8/24

Sewer Grades on Sea Lane Moor
Electric Ave to Montevista Ave

51

	13.12	84.98	71.86		
380.7' Exp. EL La Jolla Blvd	4.65	88.42	1.21	83.77	
= DE: 0.00			1.08	87.34	81.50
					+5.84
+47.14			341	85.01	79.57
					+5.44
+94.28			544	82.98	77.64
					+5.34
1+47.42			735	81.07	75.71
					+5.36
1+88.56			931	89.11	73.78
					+5.33
2+35.70			1095	77.47	71.85
					+5.62
2+82.85	027	75.96	1283	75.59	69.92
					+5.67
3+30.00			187	73.99	68.00
= M.H.					+5.99
3+77.14			521	70.65	66.14
					+4.51
4+24.29	on paving		637	69.49	64.28
					+5.21
4+71.43			834	67.52	62.42
					+5.10
5+13.57			1044	65.42	60.56
					+4.86
5+25.71	086	64.49	1225	63.61	58.70
					+4.91
6+12.85			296	61.52	56.85
					+4.67
6+60 =			434	60.13	55.00
Drop M.H.					+5.13
			434	60.13	52.00
					+8.13
7+05.16			607	58.40	50.58
					+7.82
+50.32			795	56.52	49.16
					+7.36
+95.48			991	54.56	47.75
					+6.81

8+40.66	358	5611	1194	5253	4633	+620
---------	-----	------	------	------	------	------

8+8583			537	5074	4492	+582
--------	--	--	-----	------	------	------

9+31 = 6	Monte Vista					
MH		7.01	49.10	43.50		560

4/3/24

Sewer Construction
to Olivetas from dot
Sea Lane to 240' N.
6.47 from preceding page.

dot Sea Lane				Grade	
= 0+00				52.0	
+48	3.80	60.67	52.3	+8.37	
+96	3.62	60.85	52.6	+8.25	
1+44	4.12	60.35	52.9	+7.45	
+92	4.86	59.61	53.2	+6.41	
2+40 DE	4.73	59.74	53.5	+6.24	

4/23/24 Grapery Sewer Construction from
 M.H. 380.7' E of EL La Jolla Blvd
 off of San Lane, to 680.7' E

M.H. Sta	0+00 page 51			see page 51	Grades	
= 0+00	10.48	97.82		87.34	81.50	
0+50			1087	8695	84.0	+ 2.95
1			565	9217	86.50	+ 5.67
+50			3.36	9446	89.00	+ 5.46
2	663	103.14	1.31	96.51	91.50	+ 5.01
+50			4.31	9883	94.00	+ 4.83
3			2.56	100.58	96.50	+ 4.08

+33. = W.L. ~~Graper~~ Draper



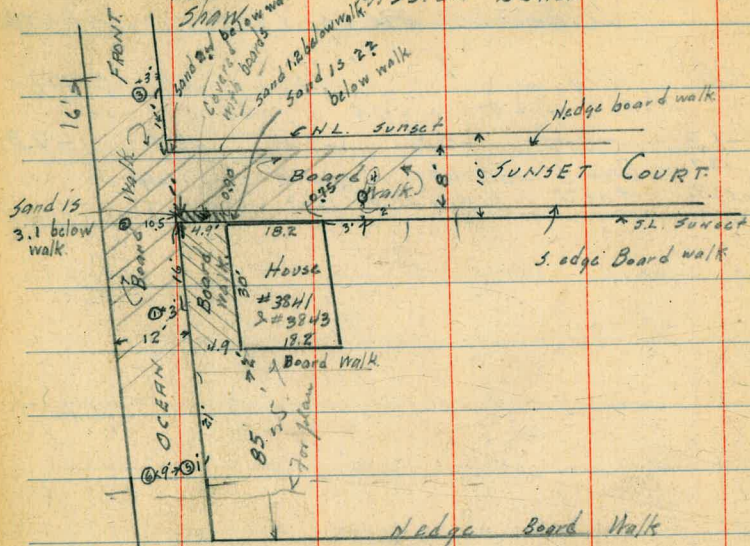
55

Canyon St.
180' E. of E. li Shafter St.
Ground Elevs. (Interpolated)

N.P.L.	0	$\frac{1}{4}$	$\frac{1}{2}$	$\frac{3}{4}$	0	S.P.L.	
	-10-	-12.5-	-12.5-	-12.5	-12.5-	-10-	
-0.4	-1.3	-0.7	-0.5	-1.5	-2.1	-2.8	
Ground at 1+75	13.7	Ground at 1+75	-0.5	14.7	Ground at 1+75	-1.7	10.9
	-0.7	-13.9	-17.7	-17.7	-17.1		

11/21/24

Gregory Miller
Walker
Spartan
Survey of House etc.
Location on Lot c BLK 206
MISSION BEACH



⊙ indicates where pictures were taken

11/21/21. Gregory		CROSS SECTION OF ALLEY BLK 55 LA JOLLA		66.13 6'5" x N.L. of Eads	260 493 1353 1027 2041			57
	Instr	Rod	Elv. (ft)		E		4.6	68.95
B.M.	0.14	8805	87.91	SE Fall + Prospect		35' N		
TP	0.32	75.33	1304	75.01	E		3.9	69.65
Curb runs across Alley on Eads N.L. of Eads								
					+3		4.1	69.45
E		10.88	64.45	on walk	+5		5.5	68.05
C		12.20	63.13	✓ -	C		5.7	67.85
W		13.53	61.8	✓ -	+3		5.6	67.95
TP	8.58	73.55	10.36	64.97	+5		6.6	66.95
		1' N.			W		7.5	66.05
W			61.9			70' N		
C			63.2		W		7.7	65.85
E			64.5		+6		6.2	67.35
		4' N			+7		5.2	68.35
E			7.1	66.45	C		5.2	68.35
C			8.1	65.45	+5		4.7	68.85
W			9.1	64.45	+7		3.5	70.05
		2.5' N			E		3.2	70.35
W			8.6	64.95		7.5' N		
+7			5.8	67.75	E		3.1	70.45
C			5.6	68.05	C		5.0	68.55

7355

W		76	65.95
	95° N		
W		8.1	65.45
C		56	67.95
E		35	70.05
	125° N		
E		20	71.55
+7		33	70.25
C		44	69.15
+3		59	67.65
W		8.53	65.02 <small>on cement walk</small>
	135° N		
W		8.53	65.02 <small>on walk</small>
+1		7.5	66.05
+7		6.2	67.35
C		44	69.15
+5		3.1	70.45
E		2.2	71.35
	150° N		
E		24	71.15

58

C		5.3	68.25
+3		5.7	67.85
W		8.4	65.15
	170° N		
W		7.4	66.15
E		4.5	69.05
E		2.1	71.45
	200° N		
E		2.6	70.95
C		5.0	68.55
W		7.8	65.75
	210° N		
W		7.7	65.85
+7		5.9	67.65
C		4.5	69.05
E		2.6	70.95
	220° N		
E		2.2	71.35
+5		2.9	70.65
C		3.9	69.65

+8 73.55 6.2 67.35
W 7.5 66.05

245°N

W 6.9 66.65
+4 5.0 68.55
C 3.6 69.95
E 2.1 71.45

255°N

E 2.1 71.45
C 3.0 70.55
+4 3.9 69.65
W 6.6 66.95

264° Lot Line 280°N

W 7.5 66.05
C 4.9 68.65
E 2.9 70.65

300°N

E 3.3 70.25
C 4.9 68.65
W 6.9 66.65

59

-5

W

+2

C

E

E

C

+0.30

+8.0

W

W

+2

+9.7

C

E

315°N

7.3

6.9

5.8

4.9

2.4

340°N

1.1

3.0

3.9

4.5

5.3

364°N = end of Alley

5.1

3.9

2.6

1.7

+0.4

66.25

66.65

67.75

68.65

71.15

72.45

70.55

69.65

62.05

68.25

68.45

69.65

70.95

71.85

74.0

12/31/24 Gregory Curb & Sidewalk Elevations
Thorn + Gregory

60

on B.M. 4.57 324.37 314.80 SW 33rd
+ Thorn

6.35 318.02 = Elevation of Curb NW cor. Thorn + Gregory

6.35 318.02 = ✓ ✓ ✓ SW ✓ - - ✓

6.27 318.10 = ✓ - outside edge walk NW cor. Thorn + Gregory

6.17 318.20 = ✓ - inside ✓ - - ✓ - -

100' wide
14' CBS
17' 1/4

X Sec. Rosecrans St from W. Line A.T.S.F. R. of W. 1/6/25
To E. Line MURTZ.

Top Hydrant
8.66 Waitman & Taylor

1331.54
71.03
48-55

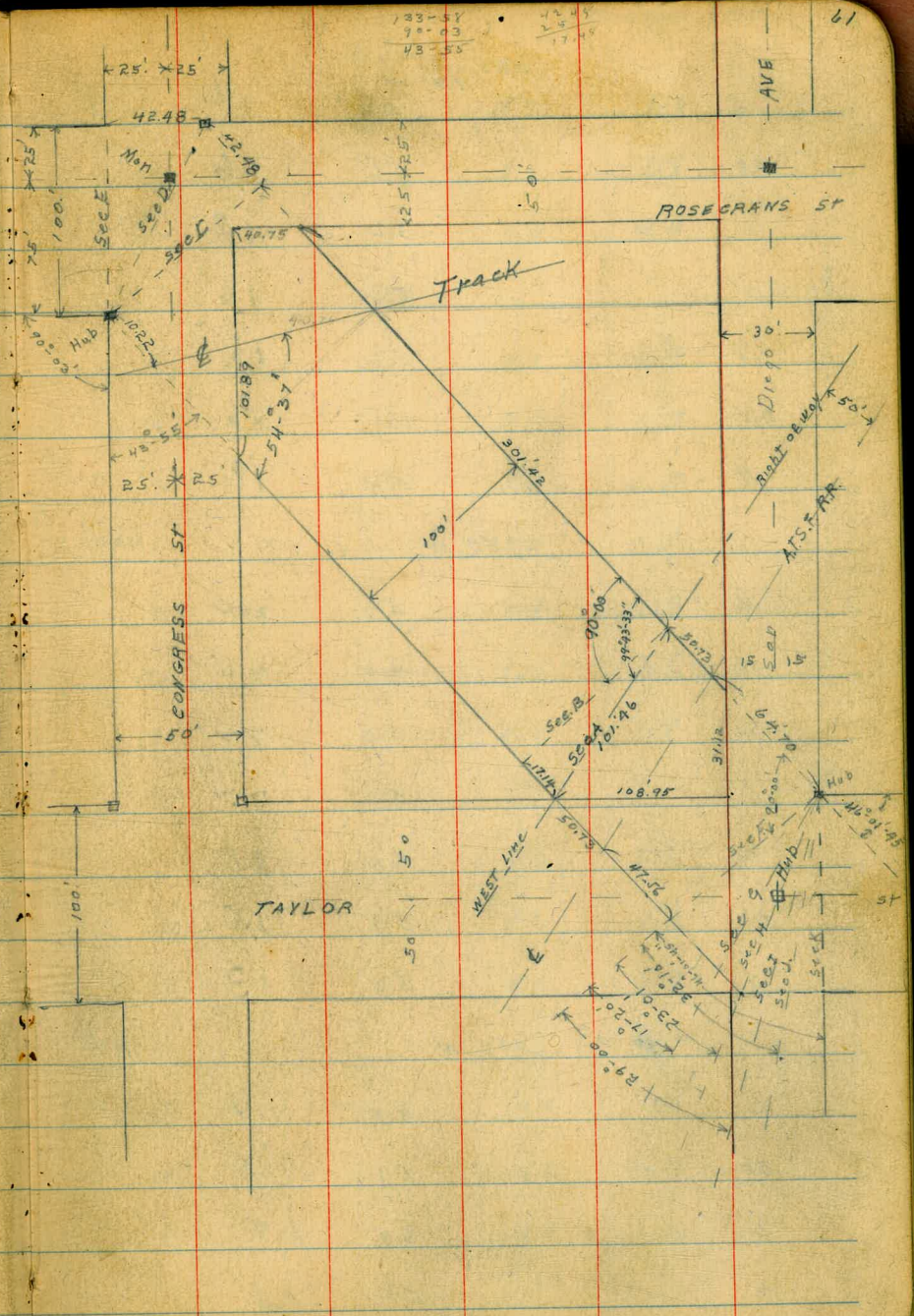
B.M.	1.52	10.18 ↓		
T.P.	4.03	8.60 ↓	5.61	4.57
T.P.	5.35	7.23 ↓	6.72	1.98

Sec A = W. Line S.F. R. of Way

S		4.7	2.5
cb		5.4	1.8
1/4		5.7	1.5
C		5.7	1.5
1/4		6.1	1.1
cb		5.8	1.4
N		5.3	1.9

Sec B. = 00

H		5.3	1.9
cb		5.6	1.6
1/4		5.5	1.7
C		5.4	1.8
1/4		5.2	2.0
cb		5.0	2.2
S		5.2	2.0



	7.23	40' W		2788		7.23		
S		5.8	14		1/4	5.4	1.8	
cb		5.6	16		cb	5.3	1.9	
1/4		5.4	18		N	4.8	4.4	
C		5.6	16			120' W		2708
1/4		5.6	16		N	5.3	1.9	
cb		5.6	16		cb	5.5	1.7	
N		5.4	18		1/4	5.9	1.3	
		80' W		2748	C	5.7	1.5	
N		5.0	22		1/4	5.4	1.8	
cb		4.8	24		cb	5.6	1.6	
1/4		5.0	22		S	5.5	1.7	
C		5.0	22			160'		1768
1/4		5.4	18		S	5.4	1.8	
cb		5.7	15		cb	5.6	1.6	
S		5.9	13		1/4	5.4	1.8	
		100' W		2728	C	5.0	4.4	
S		5.8	1.4		1/4	4.7	4.5	
cb		5.9	1.3		cb	4.9	4.3	
1/4		5.8	1.4		N	5.0	4.4	
C		5.7	1.5					

7.23 175'W			1+53			7.23					
N		5.0	4.4		1/4		5.4	1.8			
cb		5.1	4.1		c		5.2	4.0			
1/4		5.0	4.4	5.1	1/4		5.6	1.6			
c		5.4	1.8		+8		4.9	4.3			
1/4		5.5	1.7		cb		3.3	3.9			
cb		5.5	1.7		s		2.3	4.9			
+c		5.3	1.9			240'W				+88	
s		3.6	3.6		s		3.3	3.9			
	200'W			1+28	cb		2.5	4.7			
s		3.2	4.0		+9		2.7	4.5			
+10		3.3	3.9		1/4		4.6	4.6			
cb		5.2	4.0		+8		5.5	1.7			
1/4		5.6	1.6		c		5.2	4.0			
c		5.3	1.9		1/4		5.1	4.1			
1/4		5.4	1.8		cb		5.2	4.0			
cb		4.9	4.3		N		4.9	4.3			
N		5.0	4.4			255'W				+73	
	220			1+08	N		4.4	4.4			
N		5.0	4.4		cb		4.6	4.6			
cb		5.2	4.0		1/4		5.0	4.4			

7.23
255 (EOM)

E	5.6	1.6	
+4	5.7	1.5	
1/4	2.5	4.7	
cb	3.2	4.0	
S	3.0	4.4	
	268'W		+60
S	3.1	4.1	
cb	3.0	4.4	
1/4	3.3	3.9	
+1/4	3.3	3.9	
e	4.7	4.5	
1/4	4.2	3.0	
cb	5.0	4.4	
N	5.2	4.0	
	300'W		+70
N	5.1	4.1	
cb	5.0	4.4	
1/4	4.7	4.5	
c	3.7	3.5	
+10	5.1	4.1	

7.23

Rosecrans St 64

			1/4	3.8	3.4
			cb	3.9	3.3
			S	4.0	3.4
				328'W = Sec C	00
			S	4.5	4.7
			+7	4.0	3.4
			cb	4.0	3.4
			1/4	3.8	3.4
			c	3.6	3.6
			1/4	3.6	3.6
			cb	5.0	4.4
			N	5.3	1.9
				Sec D	
			N	4.6	4.6
			cb	4.0	3.4
			1/4	3.3	3.9
			c	3.1	4.1
			1/4	3.7	3.5
			cb	4.1	3.1
			S	4.5	4.7

7.23
 Sec E = 00 = W Line Congress St.

S	4.5	7.7
cb	4.1	3.1
1/4	3.8	3.4
C	3.1	4.1
1/4	3.4	3.8
cb	3.7	3.5
+11	3.8	3.4
N	3.2	4.0
50' W		
N	2.7	4.5
+9	3.5	3.7
cb	3.4	3.8
1/4	3.6	3.6
C	3.0	4.2
1/4	3.6	3.6
cb	3.9	3.3
S	3.8	3.4
100' W ↓		
S	3.7	3.5
cb	3.9	3.3

Rosecrans St 65

7.23

1/4	3.7	3.5
C	3.5	3.7
1/4	3.3	3.9
cb	3.0	4.4
N	3.4	3.8
150' W		
N	3.6	3.6
cb	3.6	3.6
1/4	4.1	3.1
C	3.9	3.3
1/4	4.2	3.0
cb	4.3	4.9
S	4.4	4.8
T.P.	3.75	7.93 ✓
175' W		
S	5.5	4.4
cb	5.3	4.6
1/4	4.4	3.1
C	4.5	3.4
1/4	4.6	3.3

7.93

175' W com

cb 4.3 3.6

N 4.1 3.8

200' W

N 4.7 3.4

cb 4.6 3.3

1/4 3.9 4.0

c 4.2 3.7

1/4 5.6 4.3

cb 5.3 4.6

s 4.9 3.0

225' W

s 4.0 3.9

cb 4.2 3.7

1/4 4.3 3.6

c 4.3 3.6

1/4 4.4 3.5

cb 4.5 3.4

N 4.2 3.7

7.93

249' W

N 4.2 3.7

cb 4.5 3.4

1/4 4.4 3.5

c 4.9 3.0

1/4 5.0 4.9

cb 4.9 3.0

s 4.7 3.4

255' W

s 4.1 3.8

cb 4.2 3.7

1/4 4.2 3.7

c 4.8 3.1

1/4 4.6 3.3

cb 4.4 3.5

N 4.3 3.6

300' W = E line JEFFERSON

N 4.7 3.4

cb 4.4 3.5

1/4 3.9 4.0

c 3.6 4.3

Rosecrans

66

7.93

300W(eon)

1/4	4.3	3.6
cb	4.7	3.4
S	4.4	3.5

00 = W Line Jefferson St

S	4.5	3.4
cb	4.5	3.4
1/4	4.4	3.5
c	3.9	4.0
1/4	4.6	3.3
cb	4.6	3.3
N	4.5	3.4

50'W

N	4.0	3.9
cb	4.4	3.5
1/4	4.7	3.4
c	4.0	3.9
1/4	4.6	3.3
cb	4.6	3.3
S	4.5	3.4

7.93

100'W

S	4.3	3.6
cb	4.3	3.6
1/4	4.3	3.6
c	4.1	3.8
1/4	4.4	3.5
cb	4.7	3.4
N	4.8	3.1

150'W

N	4.6	3.3
cb	5.5	4.4
1/4	5.4	4.5
c	4.2	3.7

1/4	4.5	3.4
cb	4.5	3.4
S	4.8	3.1

200'W

S	5.2	4.7
cb	4.8	3.1
1/4	4.7	3.4
c	4.0	3.9

ROSCOPANS

67

7.93

200' W 2011

1/4	5.4	4.5
c	5.2	4.7
N	4.4	3.5

250' W

N	4.3	3.6
cb	5.2	4.7
1/4	4.7	3.4
c	3.9	4.0

1/4	4.5	3.4
-----	-----	-----

cb	4.8	3.1
----	-----	-----

S	5.6	4.3
---	-----	-----

300' E Line Moore

S	4.2	3.7
---	-----	-----

cb	3.8	4.1
----	-----	-----

1/4	4.0	3.9
-----	-----	-----

c	4.1	3.8
---	-----	-----

1/4	4.8	3.1
-----	-----	-----

cb	5.0	4.9
----	-----	-----

N	4.6	3.3
---	-----	-----

7.93

00 = W. Line Moore St

Rosecrans 68

N	5.2	4.7
---	-----	-----

cb	4.7	3.4
----	-----	-----

1/4	4.5	3.4
-----	-----	-----

c	4.4	3.5
---	-----	-----

1/4	4.9	3.0
-----	-----	-----

cb	4.7	3.4
----	-----	-----

S	5.0	4.9
---	-----	-----

T.P.	4.41	7.34 ✓	5.00	2.93	Mon Moore & Rosecrans
------	------	--------	------	------	--------------------------

15' W

S	4.3	3.0
---	-----	-----

cb	4.1	3.4
----	-----	-----

1/4	4.2	3.1
-----	-----	-----

c	3.7	3.6
---	-----	-----

1/4	4.0	3.3
-----	-----	-----

cb	4.3	3.0
----	-----	-----

T11	4.3	3.0
-----	-----	-----

N	3.4	3.9
---	-----	-----

50' W

N	4.1	3.4
---	-----	-----

T10	4.4	4.9
-----	-----	-----

cb	4.7	4.6
----	-----	-----

7.34
50'W (EON)

1/4	4.2	3.1
e	3.7	3.6
1/4	4.4	4.9
cb	4.1	3.4
S	5.3	4.0

100'W

S	5.7	1.6
cb	4.3	3.0
1/4	4.3	3.0
e	3.8	3.5
1/4	4.3	3.0
cb	4.9	4.4
+5	5.0	4.3
+9	4.4	4.9
N	4.3	3.0

150'W

N	4.3	3.0
10	4.6	4.7
12	5.3	4.0
cb	5.0	4.3

7.34

Rosecrans 69

1/4	4.6	4.7
e	4.0	3.3
1/4	4.3	3.0
cb	4.7	4.6
S	5.8	1.5

200'W

S	5.0	4.3
cb	4.6	4.7
1/4	4.5	4.8
e	4.2	3.1
1/4	4.4	4.5
cb	5.0	4.3
+4	5.1	4.4
+6	4.7	4.6
N	4.4	4.9

250'W

N	4.6	4.7
+9	4.6	4.7
+11	5.2	4.1
cb	5.0	4.3

7.34

250' W (con)

1/4	4.4	4.5
C	4.4	4.9
1/4	4.4	4.5
eb	5.0	4.3
S	4.8	4.5

300' W = E. Line Hancock ST

S	4.7	4.6
eb	5.3	4.0
1/4	5.0	4.3
C	4.4	4.9
1/4	4.7	4.6
eb	4.8	4.5
+4	5.2	4.1
+6	4.6	4.7
N	4.3	3.0

00 = W. Line Hancock ST

N	4.4	4.9
+9	4.5	4.8
+11	5.1	4.4
eb	4.9	4.4

7.34

ROSECRANS 70

1/4	4.8	4.5
C	4.4	4.9
1/4	5.3	4.0
eb	5.4	1.9
S	5.1	4.4

50' W

S	5.1	4.4
eb	5.4	1.9
1/4	5.2	4.1
C	4.7	4.6
1/4	5.2	4.1
+13	4.8	4.5
eb	5.2	4.1
+6	5.5	1.8
+8	5.0	4.3
N	4.7	4.6

100' W

N	4.3	3.0
+11	4.9	4.4
+12	5.6	1.7

7.34
100W (con)

cb	5.7	1.6
+6	4.9	4.4
'14	4.9	4.4
+7	5.3	4.0
c	4.4	4.9
+10	5.0	4.3
'14	5.3	4.0
cb	5.7	1.6
S	5.2	4.1

150'W

S	5.4	1.9
cb	5.4	1.9
'14	5.4	1.9
c	5.0	4.3
+10	5.3	4.0
'14	4.8	4.5
cb	5.6	1.7
+6	5.7	1.6
+8	5.2	4.1
N	4.8	4.5

7.34
200'W

Rosecrans 71

N	5.4	1.9
cb	5.7	1.6
'14	5.2	4.1
c	4.6	4.7
'14	5.3	4.0
cb	5.4	1.9
S	5.3	4.0

250'W

S	5.9	1.4
cb	5.9	1.4
+12	6.0	1.3
'14	5.1	4.4
c	4.8	4.5
'14	5.3	4.0
cb	5.9	1.4
+11	5.9	1.4
N	5.1	4.4

7.34
300' W = E Line Kurtz

Rosecrans 72

N 5.1 7.4

Ch 4.9 7.4

114 6.0 1.3

E 6.2 1.1

114 6.2 1.1

26 5.1 7.4

S 5.2 7.1

T.P. 5.92 8.85 4.41 2.93

T.P. 6.39 10.28 4.96 3.89

T.P. 1.60

8.68:866
Top Hydrant
Taylor Whitman

Top

Rosecrans ST X Sec
from Sec A Page 61 East

3/14/26

73

7.07
43' E. of Sec A = Top R.R. Embankment

Top Hd +
Taylor + White

BM	1.55	10.21		8.66	S	7.8	5.3		
TP	3.95	8.59	5.57	4.64	cl	1.8	5.3		
TP	2.64	7.07	4.16	4.43	1/4	1.8	5.3		
<p>(Page 61) 7' E. of Sec A 157' E. of W Line SE Right of Way Following sections parallel to E.R.R.</p>					C	1.8	5.3		
S			7.2	0.1	1/4	1.8	5.3		
cl			7.0	0.1	cl	1.8	5.3		
1/4			7.0	0.1	N	1.8	5.3		
C			7.0	0.1					
					50.73 E. of Sec A Track no yardage				
1/4			6.9	0.4	N	1.15	5.94	on E. rail	
cl			6.9	0.4	S	1.30	5.77	" "	
N			6.7	0.4					
					59' E. of Sec A = Top R.R. Embankment				
31' E. of Sec A					S	1.6	5.5		
X			7.0	0.1	cl	1.6	5.5		
cl			7.3	-0.2	1/4	1.6	5.5		
1/4			7.3	-0.2	C	1.6	5.5		
C			7.3	-0.2	1/4	1.6	5.5		
1/4			7.3	-0.2	cl	1.6	5.5		
cl			7.3	-0.2	N	1.6	5.5		
S			7.1	0.0					

7.07

70'E. of Sec H

7.07

Rosecrans

74

s	6.9	0.4	c	5.2	1.9
cl	6.7	0.4	14	5.9	1.7
14	6.4	0.7	cl	5.1	2.0
c	6.7	0.4	N	6.0	1.1
14	6.4	0.7			
cl	5.5	1.6	N	6.0	1.1
N	5.5	1.6	cl	5.1	2.0
	115.43 E. on N 98.29 S on S } Sec F (Page 61) 90°00		14	5.1	2.0
N	6.0	1.1	c	4.4	2.7
cl	5.1	2.0	14	3.2	3.9
14	5.6	1.5	cl	3.2	3.9
c	5.6	1.5	100.5	5.4	1.7
14	5.9	1.4	78 = S. Line Taylor	5.4	1.7
cl	5.6	1.5			
100'S	5.0	2.1			
	Sec G (Page 61)		S-4.4 = S. Line Taylor	2.0	5.1
S-13 = S. Line Taylor	5.7	1.4	s	2.2	4.9
100'S	5.6	1.5	cl	2.1	5.0
cl	5.6	1.5	14	2.2	4.9
14	4.7	2.4	c	3.1	4.0
			14	4.7	2.4

7.07

cl	5.1	7.0	
N	6.0	1.1	
	Sec J.		
N	6.0	1.1	
cl	5.1	7.0	
114	4.6	7.5	
C	2.6	4.5	
+9	2.1	5.0	
114	2.4	4.7	
cl	2.2	4.9	
S	2.4	4.7	
+35 = skina Taylor	2.40	4.63	on W. edge paving in San Diego Ave
	Sec K = E. Line San Diego Ave		
S = skina Taylor	3.8	3.3	
+5 = edge Paving	3.80	3.3	on inside curve
cl	3.65	3.47	on paving
114	3.25	3.84	" "
+10 edge Paving	2.75	4.37	on outside curve
C	2.5	4.6	
+10	2.9	4.4	

7.07

Rosecrans 75

114	4.9	4.7	
cl	6.8	0.9	
N	6.0	1.1	
	9' E of Sec K = 9' E. of E. Line S.D. Ave		
N	6.5	0.6	
cl	6.8	0.3	
+10	4.7	0.4	
114	4.4	7.7	
+9	2.5	4.6	
C	2.7	4.4	
114	3.60	3.5	on paving
cl	4.2	4.9	
S	3.9	3.7	
	15' E. of E. Line S.D. Ave.		
S	5.7	1.4	
+10	4.1	3.0	
cl	4.1	3.0	
114	3.9	3.7	on paving
C	3.0	4.1	" "
+10	2.7	4.4	

7.07

14	3.8	3.3
+3	6.2	0.9
cl	4.7	0.4
N	6.7	0.4

35' E. of E Line S.D. Ave

N	6.7	0.4
cl	6.7	0.4
+11	4.4	0.7

14	3.9	3.7
----	-----	-----

+3	2.5	4.6
----	-----	-----

cl	3.4	3.7
----	-----	-----

14	4.3	4.8
----	-----	-----

18	4.2	4.9
----	-----	-----

+14	5.5	1.6
-----	-----	-----

cl	6.0	1.1
----	-----	-----

S	6.4	0.9
---	-----	-----

50' E. of E Line S.D. Ave

S	6.2	0.9
---	-----	-----

cl	6.2	0.9
----	-----	-----

+6	6.2	0.9
----	-----	-----

7.07

+15	4.3	4.8
-----	-----	-----

14	4.1	3.0
----	-----	-----

cl	3.55	3.54	on paving
----	------	------	-----------

14	3.2	3.9
----	-----	-----

+9	6.4	0.7
----	-----	-----

cl	6.6	0.5
----	-----	-----

N	6.6	0.5
---	-----	-----

100' E of E Line S.D. Ave

N	6.2	0.9
---	-----	-----

cl	6.6	0.5
----	-----	-----

+9	4.3	0.8
----	-----	-----

14	3.7	3.4
----	-----	-----

cl	3.63	3.44	on paving
----	------	------	-----------

14	4.2	4.9
----	-----	-----

+8	6.3	0.8
----	-----	-----

cl	6.4	0.7
----	-----	-----

S	6.3	0.8
---	-----	-----

BM	5.56	8.69	3.13	Elev Spur at Rosecrans + Congress Ctr. Mon Congress & Reservoirs
----	------	------	------	--

S line	4.64	4.05	on rail
--------	------	------	---------

N "	5.60	3.09	" "
-----	------	------	-----

76

00 = south

2.75	8.65	5.90	TRK
		4.25	4.40
		6.05	2.60 TRK
		5.10	3.55 TRK

Top N. W.
Cuts - West

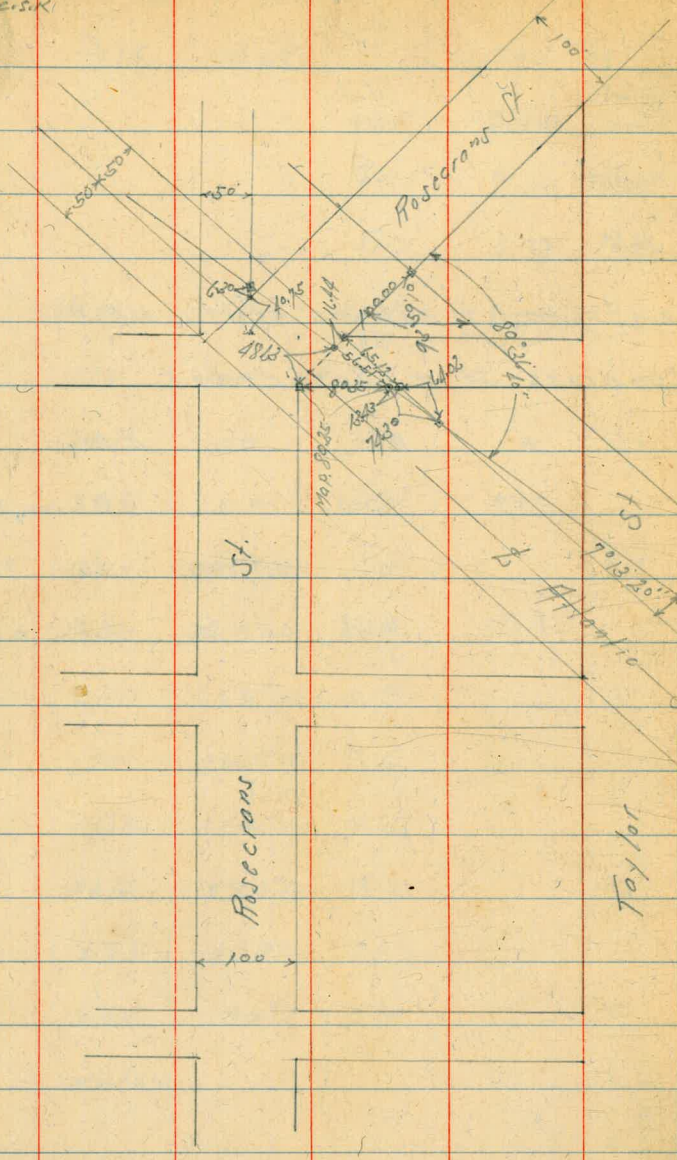
Dist	Az.	Rod
		5.2 at instrument
110	00	5.1
220	00	5.2
330	00	5.5
305	345° 30'	5.3
300	340° 00'	8.0
250	322° 00'	6.9
190	300° 00'	7.6
165	264° 00'	7.5
210	230° 00'	7.2
235	197°	7.5
330	30°	5.4

Water

instrument set 50' south NE cor
Congress St & Rose Crans

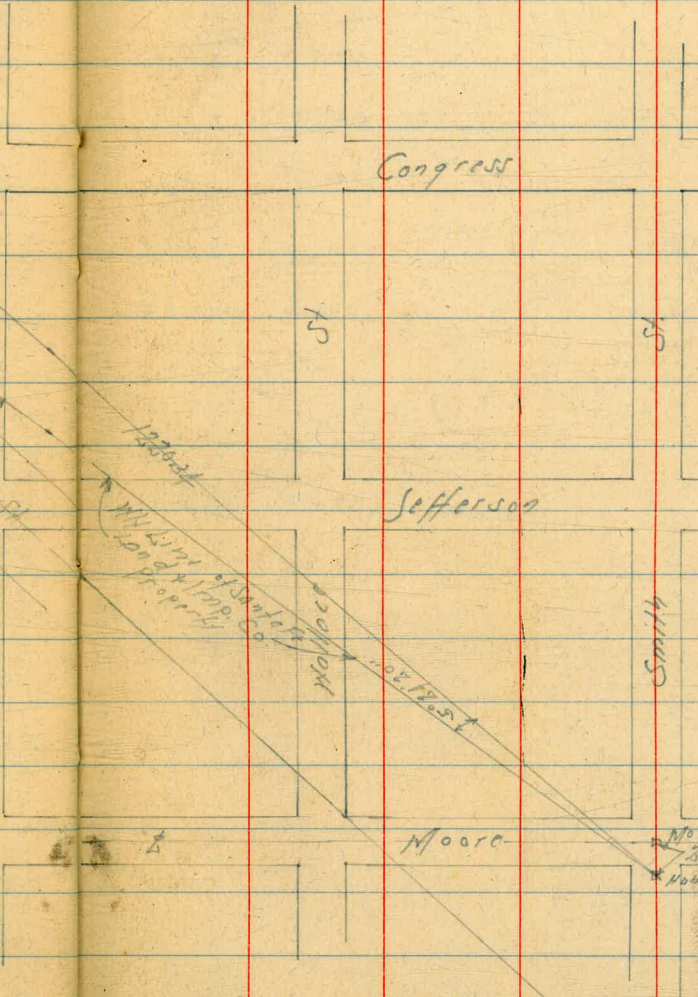
+	H. I	-	Elev
2.53	8.43		5.9 on track
		4.31	4.12 TP
5.57	9.69	1.13	8.56 = <u>8⁶⁶</u>

indexed
C.S.K.



Survey of Santa Fe &
Petroleum Products Co's property
South of Rosecrans

3-9-32 78
Moore
Sisson
Hartman



Congress

Jefferson

Moore

Smith

No. 7
5913
No. 4

Moore
Preston
Walker

Sewer Construction
Five to cherry

TRIAS ST

0+00 = DE	263.0	+6.25
+50.6	261.6	+6.56
101.2	260.2	+6.52
151.8	258.8	+6.12
202.4	257.1	+5.95
253.0 = M.M. 490 ft	256.0	+5.58
278.0 END-EL TRIAS	255.0	+6.08

267.06
7.09
274.75
12.19
262.56
6.07
268.63

1175	1315	1455	1595	1735	1263
<u>450</u>	<u>659</u>	<u>853</u>	<u>983</u>	<u>1148</u>	<u>705</u>
7625	+6.56	+6.52	+6.12	+5.95	+5.58
1362		975	1225	1475	
<u>755</u>		<u>502</u>	<u>661</u>	<u>860</u>	
+6.08		+4.71	+5.64	+6.15	

Lateral #1 PL.	265.0	+4.71
✓ #2 ✓	262.5	+5.64
✓ #3 ✓	260.0	+6.15

10.18
3.90
6.28 Top Hyd Taylor & Juan

7.23
4.10
3.13 Mon Conger & Rose

7.93
5.00
2.93 Mon Moore & Ros

7.34
4.82
2.52 Mon Hancock

ENGINEERING DEPARTMENT,
CITY OF
SAN DIEGO,
CALIFORNIA

1.55
10.71
5.57
4.64
3.95
8.59
4.10
4.43 x
2.64
7.07

4.4
1.7
27

46.02
28.42
17.20
46.02
17.02
29.00

16
35
50
100
13-50
17-00
23-01
28-40

78
34
43
59
72

20995 Co BM #10
7186 Sea Lane La Jolla Bl.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.
FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

