

1115

PASTS

BOOK

No. 385 F



11-14  
N.E. Cor N. & 16th B.P. 1252  
" " " 16th " 1664

Book # 1115

MICROFILMED

0EG 2 1 1964

115

F/Stockton 202.48 SE B.P.

Hickory NW. B.P. 201.03

58.46  
21.67  
80.13

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**THE FREDERICK POST CO.**  
**ENGINEERING and DRAFTING SUPPLIES**  
**IRVING PARK STATION**  
**CHICAGO, ILL.**

**92 FIFTH ST.**  
**PORTLAND, ORE.**

**79 NEW MONTGOMERY ST.**  
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AGENTS FOR

"BERGER" TRANSITS and LEVELS  
"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS  
"CHICAGO" STEEL TAPES, etc.



- 1-11 — 16th & Logan
- 12- Tie at Sta 107+69<sup>3</sup>
- 12- " " 115+89<sup>3</sup>
- 13- Levels, Hunter & Arbor Dr.
- 14- " , Hawk
- 15- " , Arbor Dr.
- 17- Tie at Sta 53+80
- 18- Line below Arbor Dr.
- 22- Line from 115 to M.L.
- 25- Levels, Goldfinch & Hawk.
- 27- " Jackdaw
- 28- Canon Line Nat Montecito
- 29- Levels "
- 30 Tie Sta 139+47<sup>3</sup>, 117+42<sup>3</sup>
- 30 " " 121+91.16
- 31- Tie at Smith St
- 31- " " Hickory
- 32- Court Way
- 33- Arcadia
- 34- "
- 35- "
- 36- "
- 40- Tie, Goldfinch & Barr

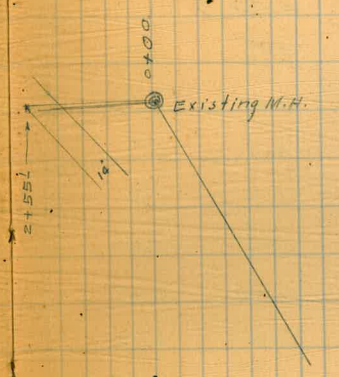
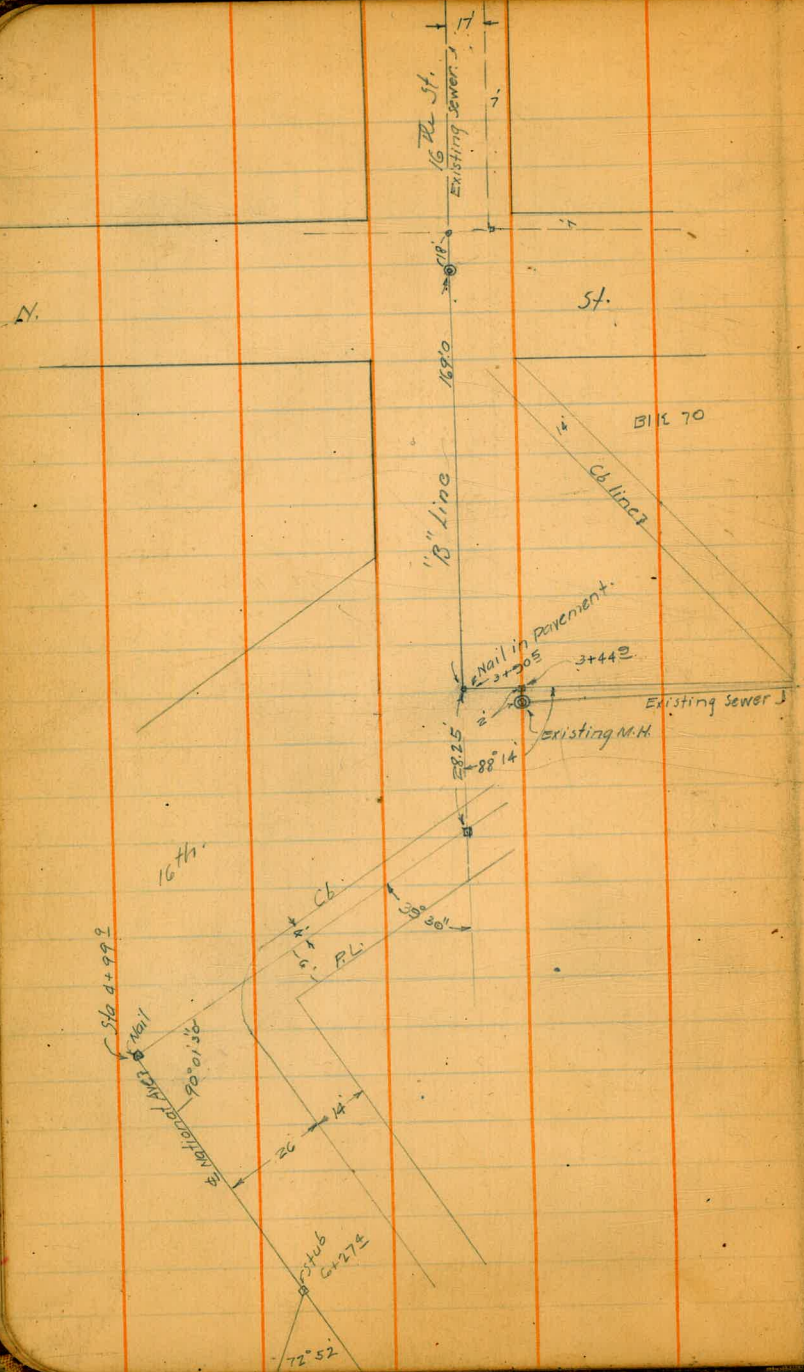


Dannan.  
Kelly.  
Steck.  
July 1921

Sta	5.58	16.72	11.14 B.P. Logan 50' S of Int Curbs on Logan and 16th.	
00 = flow line:				
00 = Flow line:			8.97	7.75
00 = Top of M.H.			3.56	13.16
00 = Ground.			3.9	12.8
+50			4.7	17.0
1+00			5.4	11.3
1+50			5.9	10.8
1+75			4.1	17.6
2+00			3.1	13.6
2+55 <sup>1</sup> = N.E. Cb on Logan Av. (on Cement)			4.98	11.74
2+55 <sup>1</sup> = Pavement			5.66	10.06
2+90 <sup>4</sup> = S. D. E. R.R. North track (Pavement)			5.42	11.30
3+06 <sup>8</sup> = " " " South " "			5.49	11.23
3+39 <sup>3</sup> = Edge Pavement no curb:			7.65	9.07
3+44 <sup>2</sup> = Old M.H. E' S of line:			6.88	9.84
3+44 <sup>2</sup> = Ground.			7.0	9.7
3+72 <sup>5</sup> = Edge of Pavement - no Curb.			8.02	8.70
3+90 <sup>5</sup> = Intersection of 16 <sup>th</sup> St line: (Pavement)			7.76	8.96
#		5.58	"	11.14
3+90 <sup>5</sup> = 1469 <sup>00</sup> A line:				

← See Book 199 pp 20 + 62 (7.44) ? 1/24/42

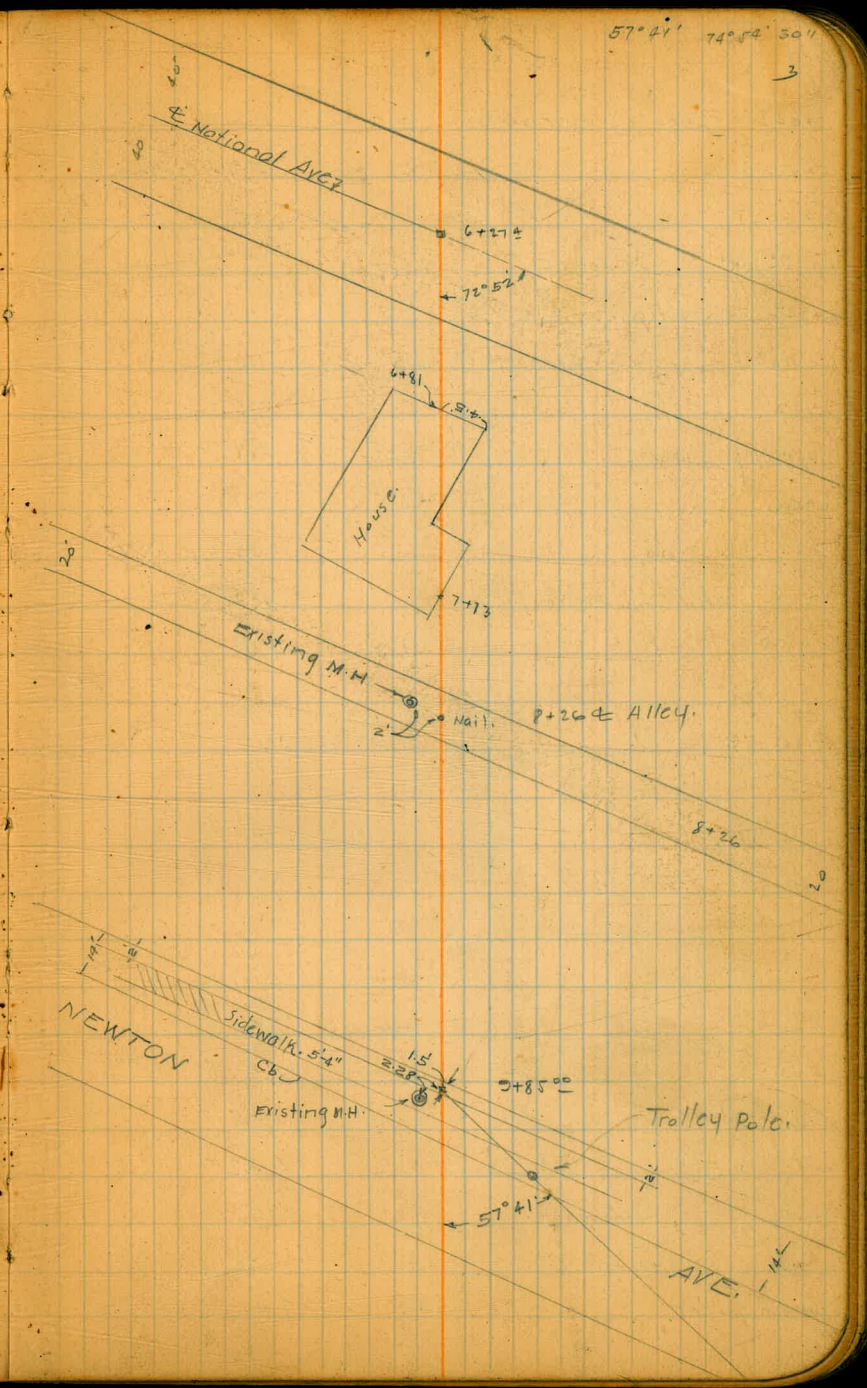






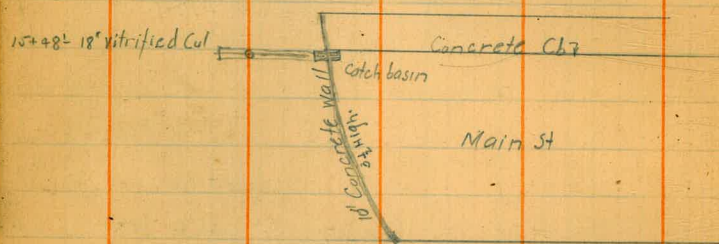
B line

Sta	2.25	12.39	11.14 B.P.E.M.	
0+00 = M.H. 25' S of the N.L. of N. St. (Flow line)			5.87	7.57
" " " " " " Ground			1.76	11.63
0+55 N. Rail of S.D. & A. R.R.			1.68	11.71
0+50			2.6	11.8
0+70 = N.R. of N. Track S.D. & A. R.R.			2.81	10.58
0+80 S.R. " " " " "			2.73	10.66
0+87 N.R. " S " " "			3.01	10.38
0+90 = S.R. " S " " "			2.94	10.45
1+20 on Pavement:			3.17	10.22
1+69 = Int of			4.42	8.97
1+91 = E.Cb line of 16th St. (Pavement)			5.16	8.73
1+91 <sup>91</sup> = on top of Cement Curb (No sidewalk)			4.67	8.72
1+97 <sup>25</sup> = $\Delta 39^\circ 30'$ Rt.			4.7	8.7
2+50 (No sidewalk)			5.6	7.8
3+00 = Alley Curb			5.99	7.4
3+00 = " Pavement			6.32	7.07
3+10 = $\pm$ Alley Pavement			6.65	6.74
3+20 = S.L. of Alley Pavement			6.62	6.87
3+20 = " " " " Cement Curb			6.37	7.02
3+50 Sidewalk			6.83	6.56
4+00 "			7.48	5.91
4+50 "			8.18	5.21
4+71.8 " = Edge of Return			8.46	4.93
4+71.8 Pavement " "			9.07	4.32
4992 A # 892 $\pm$ of National Ave	12.78		9.53	3.86

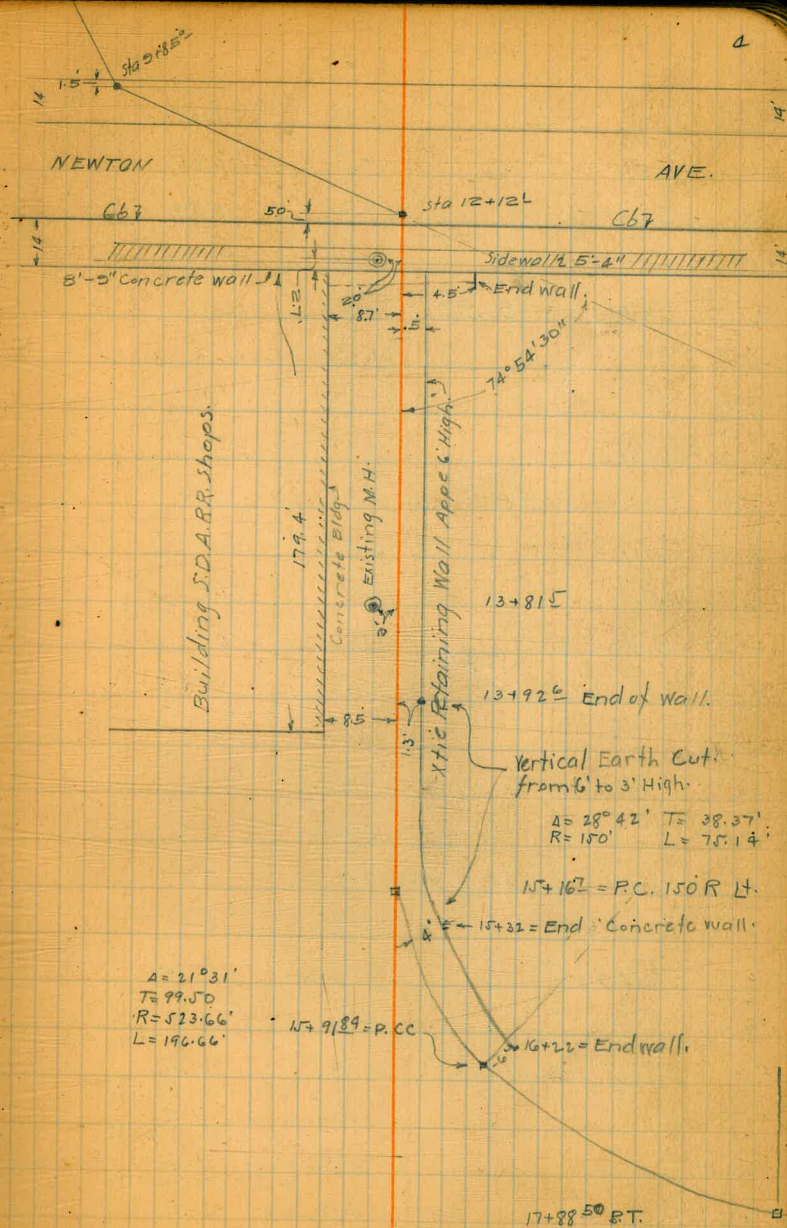




57042	Edge of Pavement:	8.72	4.06
5750		7.6	5.2
6+00		6.1	6.7
6+27 <sup>±</sup> ART		5.1	7.7
6+54 <sup>±</sup>	= Cb National Ave: Gut.	5.8	7.0
6+54 <sup>±</sup>	Cement Cb	4.97	walk also in: 7.81
7+00		5.3	7.5
7+50		3.7	9.1
8+00		3.5	9.3
#	3.27	11.91	4.14
			8.64 Rim M.H.
	Flow line Existing M.H.	7.13	4.78
8+50		1.0	10.9

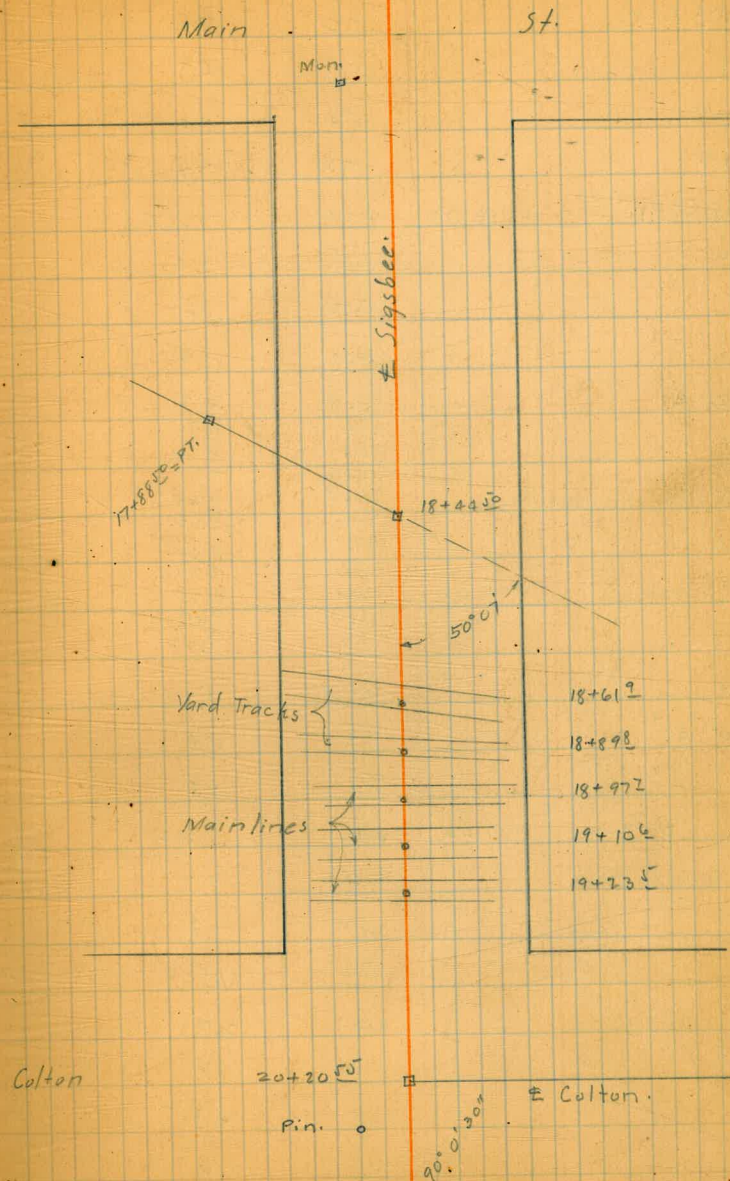


9+00		4.4	7.5
9+50		5.6	6.3
9+80 <sup>±</sup> A	on Rim		
	on sidewalk	4.52	7.38
	Flow line: Existing M.H.	7.59	4.32
10 <sup>00</sup>	On sidewalk:	4.21	7.70
10+30	On Cement Cb:	3.71	8.20
Earth gutter		4.5	7.4





	+	π 11.91	-		
10+50			3.6	8.3	
11+00			2.1	9.8	
11+48 <sup>5</sup>	Car track	N.R.	1.11	10.80	
11+59	"	"	S.R	0.80 <sup>5</sup>	11.06
#	8.41	19.92	0.40	11.51	
12+12 <sup>2</sup>	A.R. <sup>2</sup>		8.7	11.2	
Gutter			8.7	11.2	
12+17 <sup>2</sup>	Gement	Curb:	8.41	11.51	
12+28 <sup>2</sup>	Sidewalk	& M.H. Rim:	8.22	11.70	
	Flow line		15.92	4.0	
	Top of Wall.		0.1	19.8	
12+32	Bottom Wall.		11.6	8.3	
		2.78	12.46	note 6' higher 1' L.	
#	Nail In Bulkhead.		10.24	9.68	
12+50			4.2	8.3	
13			4.9	7.6	
13+50			5.0	7.5	
13+81 <sup>5</sup>	Poti	± Existing M.H.	4.7	7.8	
"	Top M.H.		4.05	8.41	
"	Flow line:		8.66	3.90	
14			4.6	7.9	
#	0.75	12.43	0.78	11.68	
	Top of fireplug.		3.5	8.9	
15+00			3.8	8.6	
15+16 <sup>2</sup>	P.C		3.9	8.5	
15+41 <sup>2</sup>			5.0	7.4	
15+66 <sup>2</sup>			5.3	7.1	





	+	$\pi$ 12.43	-	
15+518 <sup>9</sup>	R.C.E.		5.2	7.2
16+41			5.7	6.7
16+90 <sup>17</sup>			5.4	7.0
17+39 <sup>33</sup>			5.2	7.2
# 17+88 <sup>50</sup>	P.T. 5.73	13.58	4.58	7.85
18+0			5.5	8.1
+5			5.1	8.5
+9			3.7	9.9
18+44 <sup>5</sup>	A		3.9	9.7
18+61 <sup>9</sup>	On Rails.		{ 4.21	9.37
18+89 <sup>8</sup>			{ 4.11	9.47
18+97 <sup>7</sup>			{ 4.37	9.21
19+106			{ 4.36	9.22
19+23 <sup>5</sup>			{ 4.34	9.22
19+50			{ 4.29	9.24
20+20 <sup>50</sup>		AL <sup>4</sup>		{ 4.33
21			{ 4.41	9.25
# 9.51	17.13		{ 4.36	9.17
22			5.2	8.4
23			7.7	5.9
24			6.1	7.5
+70			5.96	7.62
25			8.4	8.7
+50			6.2	10.9
+70			5.6	11.5
26			4.9	12.2
			3.2	13.9
			2.8	14.3
			4.3	14.8
			4.5	14.6

Main.

13 Mon.

Beardsley &amp;

26+81<sup>3</sup>

Colton.

89<sup>53</sup>30+23<sup>3</sup> = Existing  
M.H



#	+	T 17.13 12.65	-	
	0.73		5.21	11.92 Rock
26+30			1.0	11.6
26+40			1.0	11.6
+50			0.2	12.4
26+81 <sup>3</sup> A			+0.2	12.8
27			0.2	12.4
28			2.4	10.4
29			5.4	7.2
+50			6.5	6.1
30			6.8	5.8
30+23 <sup>2</sup> = Existing M.H.			6.87	5.83
30+23 <sup>2</sup> = Flow line			13.00	-0.35

7

Check on B.P.N.W. Beardsley & Newton 28.00 = B.P.27.89

11.92  
16.08  
28.00



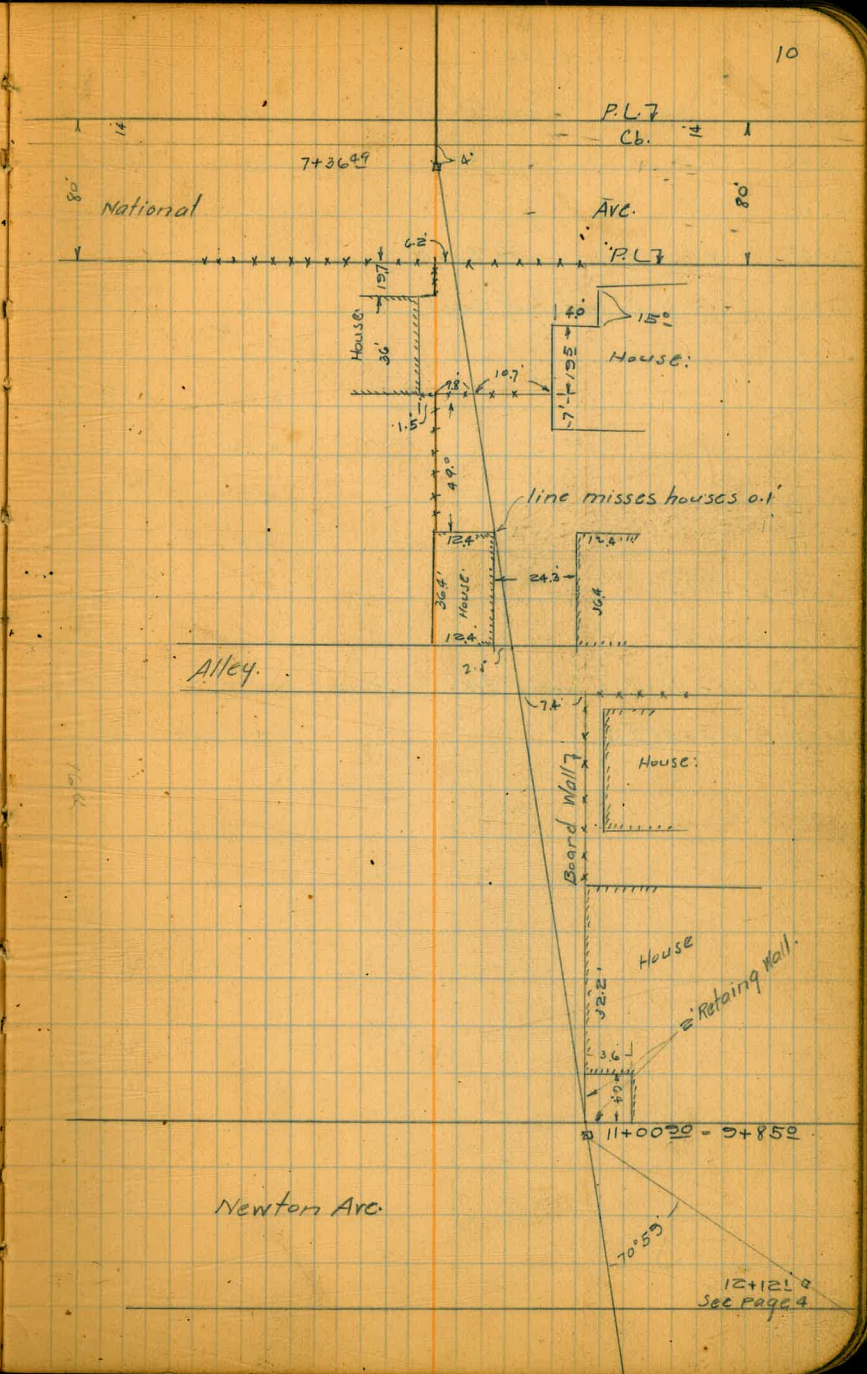








#	+	π 13.86	-	
#	3.68	16.09	1.45	12.41
5+56			5.3	10.8
5+56			3.8	12.3
5+59 <sup>o</sup> P.O.T. Hub			3.96	12.13
#	2.91	16.65	2.35	13.74
5+75 <sup>-</sup>			4.2	12.4
5+90			2.8	13.8
6+00			2.8	13.8
+50			3.8	12.9
7+00			4.6	12.0
7+25 On Cement Walk.			5.59	10.06
7+31 = Gutter: Dirt			6.2	10.4
7+36.49 = All Hub: 7+85			6.13	10.52
Gutter dirt			7.2	9.4
Curb			6.57	10.08
7+92 On Sidewalk.			6.36	10.29
8+00			6.6	10.0
9+00			5.9	10.7
#	4.57	15.99	5.23	11.42
+50			5.3	10.7
+60			5.1	10.9
+75 <sup>-</sup>			4.5	11.5
10+00			5.6	10.4
+25 <sup>-</sup>			7.3	8.7
+50			9.0	7.0
11+00 <sup>o</sup> = 9+85 Hub On Rim of Existing M.H.			8.68 8.65	7.31 7.34 = 7.38 = Previous Elev.





	+	$\pi$ B. Line	-	
	4.98	16.17	11.14	
0+9 <sup>E</sup>	N.R. of S.D.B.A.R.R.		4.43	11.69
0+19 <sup>L</sup>	S.R. " " " "		4.23	11.89
0+38 <sup>2</sup>	N.R. of Abandoned track.		3.93	12.19
0+47 <sup>2</sup>	S.R. of Abandoned track.		3.94	12.38
1+00			2.3	13.8
2+00			0.2	15.9
3+00			2.0	14.1
3 0+10			2.2	13.9
3 0+18			4.2	11.9
3+37 <sup>2</sup> A R+			4.9	11.3
3+46 = Fence:			3.0	13.1
4+16 <sup>2</sup> = Appx line of Logan Ave. On Floor.			3.01	13.11
4+27 <sup>3</sup> B = 3+48 <sup>60</sup> A			3.12 Hub	13.00







Sewer  $\pm$  1bis St.

Dennan  
Steck  
Kelly

	+	$\pi$	-		
	2.91	273.99		269.08 S.W. highdow - Hunter	
00 = S.L. + 1bis St on Pavement.			3.65	270.33	3+25.5
+50	7		4.2	269.8	2+75.5
1+00			5.7	268.3	2+25.5
1+50			7.9	266.1	1+75.5
#	0.55	261.88	12.66	261.33	
1+70			5.2	256.7	1+55.5
#	0.30	249.32	12.86	249.02	
1+95			2.4	246.9	1+30.5
2+10			4.8	244.5	1+15.5
+40			3.6	245.7	0+85.5
2+55			7.6	241.7	0+70.5
#	0.20	237.64	11.88	237.44	
2+70			2.5	235.1	0+55.5
2+90			11.0	226.2	0+35.5
#	1.53	226.40	12.77	224.87	
3+00			4.6	221.8	0+25.5
#				Hub	
3+25.5 $\pm$ Arbor Drive - 1bis.		10.50		215.90	0+00

Plotted  
10-31-24  
CAT.



	+	+	-	-
	SEWER ±	HAWK ±		
Dannan. Steck. Kelly:			see page 46 for Extension N.	
	6.18	275.26		269.08
#	2.22	271.21	6.27	268.99
00 = S.L. Hunter St: On Paving			3.16	268.05
+50			8.6	262.6
+70			10.3	260.9
+100			12.2	259.0
+20			14.0	257.2
#	2.52	260.74	12.99	258.22
+45			15.2	245.5
#	1.18	248.92	13.00	247.74
#	0.06	236.42	12.56	236.36
+76			2.5	233.9
+94			11.5	224.9
#	1.35	224.90	12.87	223.55
+200			2.6	220.3
+05			5.1	219.8
+07			8.2	216.7
+16			7.1	215.8
#	0.35	212.60	12.65	212.25
+20			2.0	210.6
+30			2.9	209.7
+34			9.0	203.6
+47			9.5	203.1
#	0.23	199.93	12.90	199.70
+55			2.6	197.3
+67			4.8	195.1
+77			10.1	189.8

Plotted  
10-31-20  
CAT

	+	+	-
		199.93	
#	0.14	189.61	12.46
2+87			187.47
3+12			+04
3+262 = ± Hawk & Arbor Drive!			188.0
			8.0
			177.6
			11.99
			175.62



Dennan  
Steak

#114 Sewer & Arbor Drive from Ibis to Hawk thence angling

	0.74	216.64		215.90 Hub. See Page 13
00=Ibis & Arbor drive:			Hub	215.90
0+50			0.74	205.6
#	0.26	203.90	11.0	203.64
+90			13.00	199.6
1+00			9.3	195.3
1+50			8.6	191.1
#	0.75	191.89	12.8	191.14
2+00			12.76	185.6
#	3.55	184.77	6.3	181.24
2+50			10.67	178.5
# 2+65 ALT	3.53	179.21	6.3	175.68
3+00			7.09	174.6
+50			4.6	177.4
4+00			1.8	175.1
4+05 ALT			4.1	174.56
+20			Hub	4.65
+50			2.2	177.0
4+66 ALT RT			9.0	170.2
5+00			9.01	174.3
5+24 ALT	3.87	179.31	4.9	175.44
5+50			Hub	3.77
+65			8.4	170.9
+80			10.2	169.1
6+00			6.2	173.1
			7.8	171.5

Plotted  
10-31-22  
CAT

+25			3.4	175.9
6+37 ALT			4.81	174.5
+50			6.4	172.9
+75			11.8	167.5
6+97 ALT RT			8.95	170.3
+700			9.0	170.3
+25			5.3	174.0
# 7+53 ALT	2.90	175.90	6.31	173.00
+85			1.7	172.2
8+00			6.3	169.6
+100			8.0	167.9
+26			1.2	174.7
+48			8.6	167.3
8+64 ALT RT			Hub	0.87
# 3+50		177.22	2.18	173.72
+80			12.1	165.1
9+00			2.8	174.4
+15			+0.2	177.4
+22			1.4	175.8
+37			7.4	169.8
+50			2.2	175.0
+60			1.7	175.5
+80			3.1	174.1
10+00			14.0	163.2
+23			2.0	175.2
10+40 ALT			1.91	175.31



	+	$\pi$	-	
		177.22		
+50			2.4	174.8
+60			7.7	169.5
+80			2.2	175.0
11+00			3.1	174.1
+10			1.0	176.1
+50			2.6	174.6
+70			3.6	173.6
12+00			3.1	174.1
# 12+182A	2.60	176.35	3.47	173.75
12+53			19.6	156.8
12+58			18.7	157.7
+85			7.3	169.1
13			7.6	168.8
+50			8.8	167.6
13+82A	4.84	169.05	12.14	164.21
14+00			2.7	166.4
+25			2.2	166.9
+50			5.0	164.1
14+54A			5.81	163.24
#	-0.02	156.10	12.93	156.12
15+00			2.3	153.8
+20			7.8	148.3
#	0.15	143.69	12.56	143.54
+36			2.1	141.6
+57			9.7	134.0
#	0.04	131.39	12.34	131.35

	+	$\pi$	-	
		131.39		16
15780			28	128.6
16+00			5.0	126.4
+25			11.1	120.3
# 0.69		119.45	12.63	118.76
+45			3.7	115.8
+48			7.4	112.1
+53			5.6	113.9
+55			6.5	113.0
+80			11.2	108.3
17			12.8	106.7
# 0.43		107.38	Top of H 12.50	106.95
+25			3.6	103.8
+50			9.7	97.7
# 0.06		94.83	12.61	94.77
+25			2.6	92.2
18+00			8.7	86.1
# 0.11		82.19	12.75	82.08
+20			3.0	79.2
+55			10.2	72.0
# 3.87		73.41	12.65	69.54
19+00			7.0	66.4
19+43				Hub.
				66.69 - 66.52 Mission Valley Line



19+435

14+54° Δ Lt 6° 24'

13+82° Δ Lt 37° 30'

12+18° Δ Rt 12° 55'

10+40 Δ Lt 6° 32'

8+64° Δ Rt 5° 12'

7+53° Δ Lt 28° 54'

6+97° Δ Rt 54° 16'

6+37° Δ Lt 22° 15'

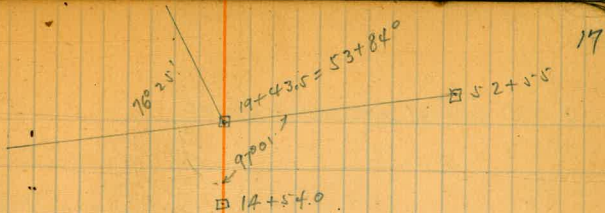
5+24° Δ Lt 16° 28'

4+66° Δ Rt 26° 0'

4+05° Δ Lt 52° 14'

2+65° Δ 19° 26' Lt ⊥ Arbor drive & Hawk

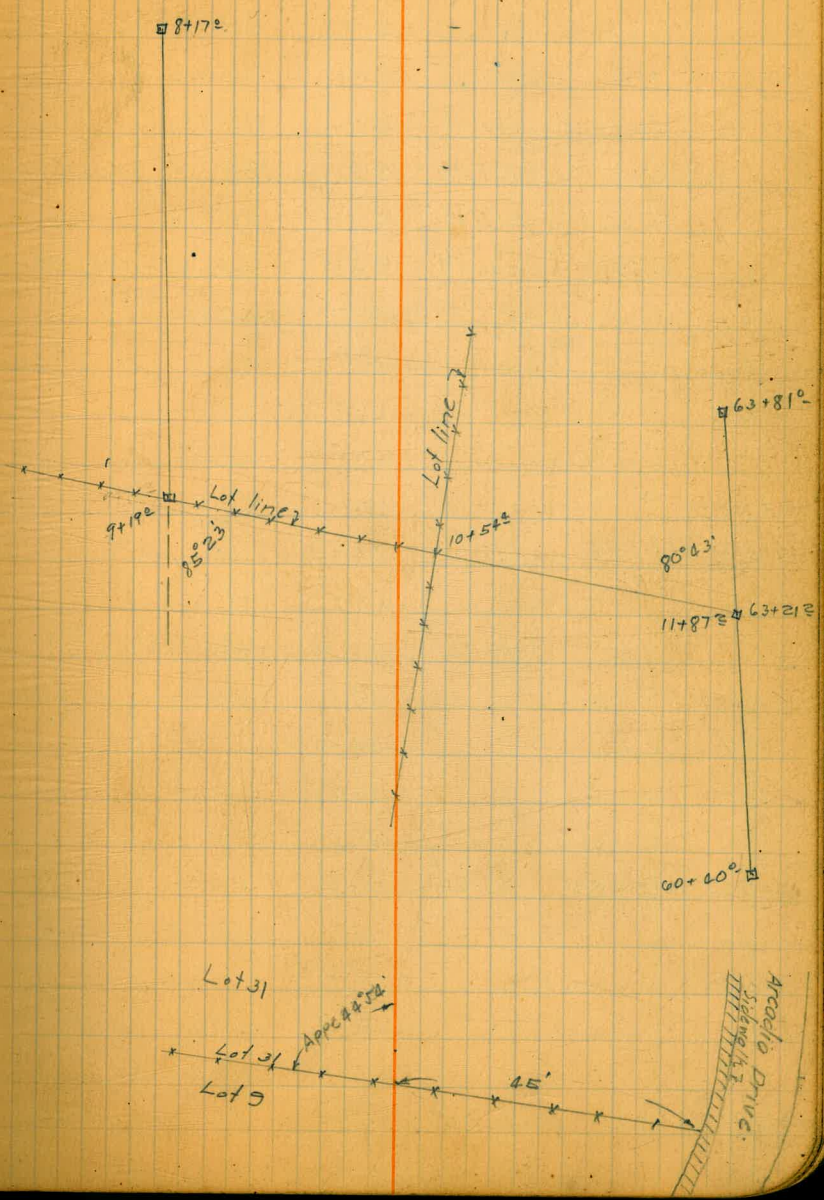
00 = ⊥ Arbor Drive & Ibis.





Line below Arcadia Drive

- 9+192 AL 85°23'
- 8+170 AR 4°13'
- 6+830 AR 3°22'
- 5+680 AL 10°25'
- 4+890 AR 11°36'
- 3+620 AR 100°57'
- 2+140 AR 20°39' R
- 0+00





Line Below Arcadia Drive

	0.85	269.93		269.08 B.P. Jackson & Hunt	
#	0.24	257.17	13.00	256.93	
#	1.75	247.38	11.54	245.63	
#	5.06	240.10	12.74	234.69	
#	0.63	227.90	12.83	227.27 On Curb	
#	0.35	215.49	12.76	215.14	
	0.52	206.59	9.42	206.07 = Hub Sta 0+00 of line below Arcadia	
0+00			0.52	206.1	
0+50			5.7	200.9	
1+00			7.3	199.3	
1+50			7.5	199.1	
2+00			9.7	196.9 Hub.	
2+14° Δ RT	3.53	198.69	11.43	195.16	
+50			5.9	192.8	
#	1.20	187.53	12.36	186.33	
3+00			3.3	184.2	
+10			4.2	183.3	
+30			3.2	184.5	
+50			7.0	180.5	
#	3+62° Δ RT	48.2	181.61	10.74	176.79
+82			3.7	177.9	
4+00			3.3	178.3	
+10			4.5	177.1	
+50			5.6	176.0	
#	4+89° Δ	5.71	182.36	4.96	176.65

Plotted  
10-31-22  
CAT

10%

				182.36			19
5+00					4.2		178.2
+48					5.3		177.1
+50					7.5		174.9
+52					8.6		173.8
+60					6.0		176.0
#	5+68° Δ RT	5.38	182.73	5.01	177.35	172.94	
6+00					2.9		179.8
6+50					3.8		178.9
6+69					9.59		170.14
#	6+83	3.22	181.63	4.32	178.41	171.79	46.6
6+98					4.0		177.6
7+00					5.3		176.3
+03					3.9		177.7
+50					4.2		177.4
8+00					3.4		178.2
#	8+17° Δ RT	8.38	183.03	6.98	174.65		
+50					10.9		172.1
+70					6.8		176.2
9+00					6.9		176.1
9+19					6.15		176.8
+24					7.6		175.4
#				0.51	170.99	12.55	170.48
+50					11.7		159.3
#				0.26	158.45	12.80	158.19
#				0.05	145.74	12.76	145.69
10+00					10.1		135.6

Covered 2.2  
Cor Culvert 24" diameter.  
Note: Sewer must go under.

Small Wash.

Bottom of culvert.

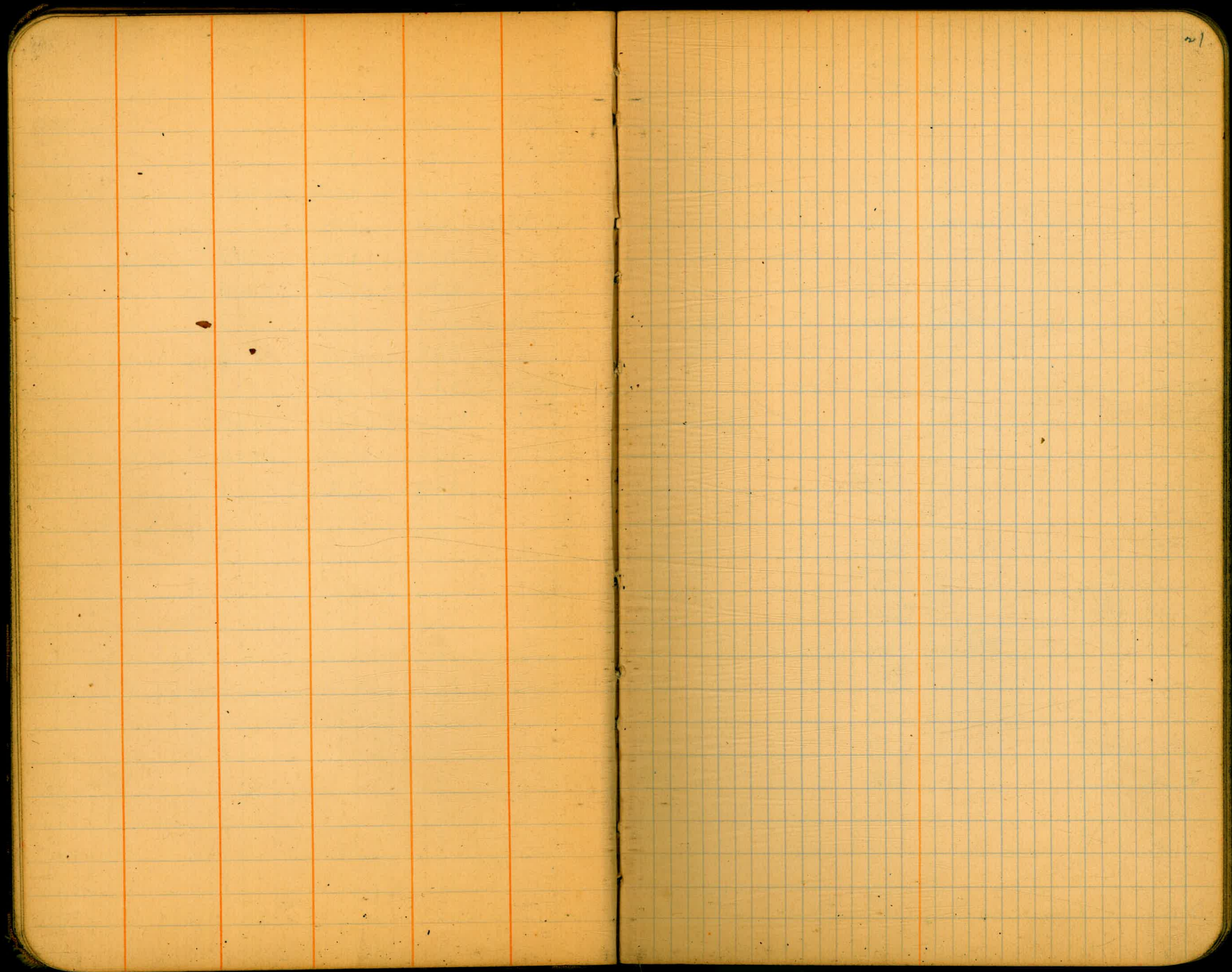
Cont. from Page 49.

9+76.92



	+	+	-		
		145.74			
#	0.89	134.13	12.50	133.24	
10+15			6.0	128.1	9+91.9 ✓
10+35			10.1	124.0	10+11.9 ✓
#	1.03	122.23	12.93	121.20	
10+50			9.0	113. ✓	10+26.9 ✓
#	0.28	109.67	12.84	109.39	
#	0.55	97.69	12.53	97.14	
11+00			6.4	91.3	10+76.9 ✓
#	0.40	85.39	12.70	84.99	
+50			11.6	73.8	11+26.9 ✓
#	1.42	74.10	12.71	72.68	
11+87 = 63+21 =	2.74	64.10	12.74	61.36	11+64.1 ✓
			4.56	59.54 = 59.69 on	63+81 =
				Check	





21

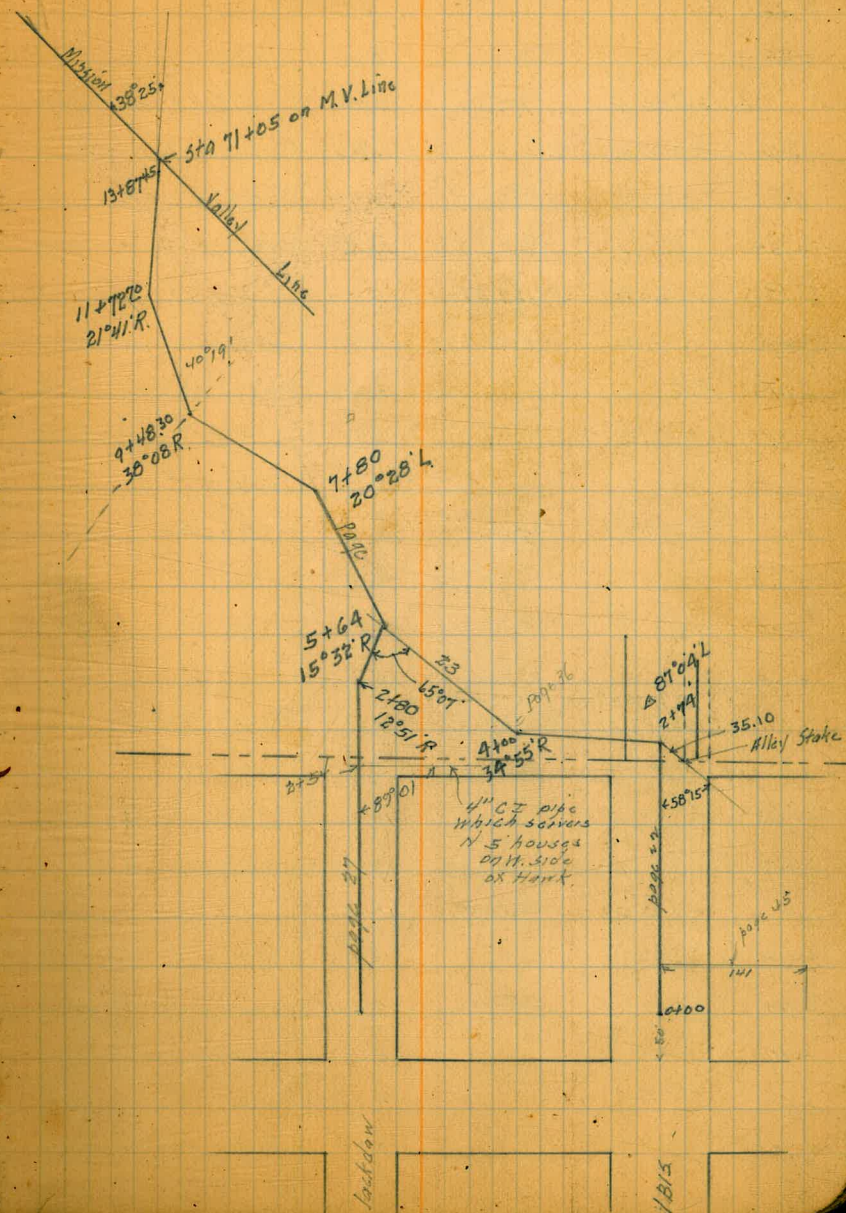


8/11/24 Gregg

Preliminary Sewer  
 4 1/2' dia from 50' N of Hunter  
 To 274' N thence down Canon  
 To Mission Valley Trunk

50' N. of Hunter on 6 1/2' dia = 0+00	358	272.60	269.00	BPSW Sackdown
		47	267.9	
+16		64	266.7	
+50		111	261.5	
T.P.	0.02	259.72	1290	259.70
1		5.1	254.6	
+50		11.5	248.2	
T.P.	0.30	247.29	12.73	246.99
+80		34	243.9	
+94		6.1	241.2	
2		7.7	239.6	
+03.0		90	238.3	
+050		11.7	235.6	
+080		140	233.3	
T.P.	0.00	234.43	12.86	234.43
+20		5.4	229.0	
+46		14.1	220.3	
T.P.	0.33	223.06	11.73	222.93
+59 = Top of 4" C.I. Sewer pipe		7.40	215.7	
+67		9.6	213.5	
+74 Δ Spot	0.07	210.22	12.91	210.15 on kid
3		40	206.2	
+20		5.9	204.3	
+35		9.2	201.0	
+42		12.6	197.6	
T.P.	0.14	197.63	12.73	197.49

Plotted  
 11-3-24  
 CAT





+50			0.6	197.0	
+64			4.9	192.7	
+85			8.0	189.6	
4	$\Delta$ 34°55' R	7.61 194.50	10.74	186.89	on hub
+40			14.2	180.3	
+45			16.2	178.3	
+54			16.9	177.6	
T.P.	0.81	182.31	13.00	181.50	
+60			1.7	180.6	
+74.32	POT		3.99	178.3	on hub
+85			4.8	177.5	7.2 Lower
5			8.1	174.2	4'11"-6.4 Lower
T.P.	0.61	180.26	12.66	169.65	
+35			6.5	163.8	
+37			8.0	162.3	
+55			10.0	160.3	
+64	$\Delta$ 1532' R	see page 47 for line on Jackson 007 159.02	11.31	158.95	
6			6.6	152.4	
+25			10.9	148.1	
+27			13.7	145.3	
T.P.	0.25	146.57	12.70	146.32	
+37			3.3	143.3	
+40			2.6	144.0	
+47			4.4	142.2	
+67			7.0	139.6	
+72			10.8	135.8	3'E 5.2 Lower

+80			11.2	135.4	
T.P.	0.11	133.80	12.88	133.69	
7			0.78	133.0	on hub
+25			6.5	127.3	
T.P.	0.00	121.09	12.71	121.09	
+50			2.5	118.6	
+70			8.6	112.5	
+80			9.74	111.4	on hub
8+05.0			13.8	107.3	
T.P.	0.38	108.43	13.04	108.05	
+25			3.5	104.7	
+45			7.0	101.4	
+70			12.9	95.5	
+80			13.1	95.3	
+90			13.9	94.5	
9			13.2	95.2	
T.P.	0.61	96.45	12.59	95.84	
+30			6.5	90.0	
+48.30	$\Delta$ 38°08' R		9.31	87.14	on hub
+88			12.1	84.4	
+89			14.4	82.1	
10			15.0	81.5	
+06.0			15.6	80.9	
+08.0			15.2	83.3	
T.P.	1.32	85.33	12.44	84.01	
+45			5.3	80.0	



85.33

+50			6.8	78.5	
+58			6.3	79.0	
+80			8.7	78.6	
11			8.7	78.6	
+15			10.6	74.7	
+50			13.2	74.1	
TP	0.21	73.75	12.29	73.04	
+72.70	Δ 21°41'R		2.74	70.6	on hub
+92			5.3	68.0	3' E = 4' lower
12			5.9	67.4	
+25			8.4	64.9	
+46			11.4	61.9	
+70			10.7	62.6	
13			13.5	59.8	
TP	2.31	63.46	12.10	61.15	
+15			5.5	58.0	
+50			7.1	56.4	
+87.45	= 71+05 on MV Line		7.23	54.23	



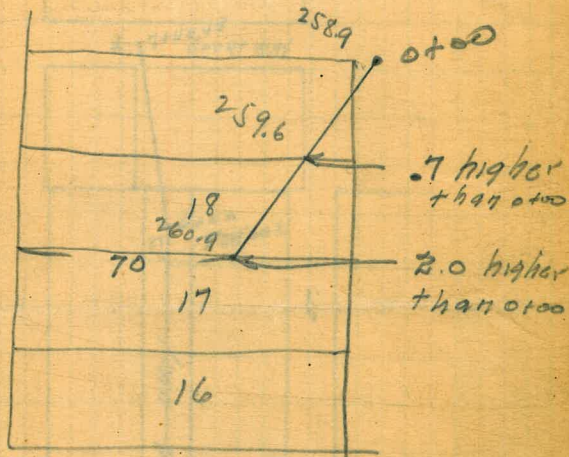
8/11/24 Gregory Sewer Levels dot Blk bat  
 GOLDFINCH & HAWK  
 from 200 Fox Barr to COURTWAY  
 6.84 275.86 269.02 BPSM broken

T.P.	0.21	268.29	7.78	268.08	
100' N. of N.L. Hunter = 0+00			9.4	258.9	0+25
+50			7.1	261.2	0+75
+75			7.2	261.1	1+00
			8.6	259.7	1+25
+40			10.0	258.3	1+45
+50			12.9	255.4	1+75
T.P.	0.27	256.31	12.25	256.04	
+74			4.4	251.9	1+99
+99.97 POT.			7.13	249.18	on hub
+15			8.2	248.1	2+40
+20			10.0	246.3	2+45
+35			10.4	245.9	2+60
+50			12.2	244.1	2+75
T.P.	0.89	245.03	12.17	244.14	
+65			4.8	242.2	2+90
+90			4.9	240.1	3+15
3			7.1	237.9	edge of pipe (3+23) 3+25
+25			10.9	234.1	3+50
+35			11.5	233.5	3+60
T.P.	4.01	238.01	11.03	236.00	
+50			6.5	231.5	3+75
+75			6.8	231.2	4+01
4			8.4	229.6	4+25
+30 POT.			9.14	229.9	4+55 on hub

Stations used in plotting.



HAWK



HUNTER

Change for Loring  
7-21-25



8/11/24 Gregory

5  
6  
7

6.84

T.P.

0.21

100' N. of NL.  
Hunter = 0100

+50

+75

+20

+50

T.P.

0.27

+74

+99.97 POT.

+15

+20

+35

+50

T.P.

0.59

+65

+90

3

+25

+35

T.P.

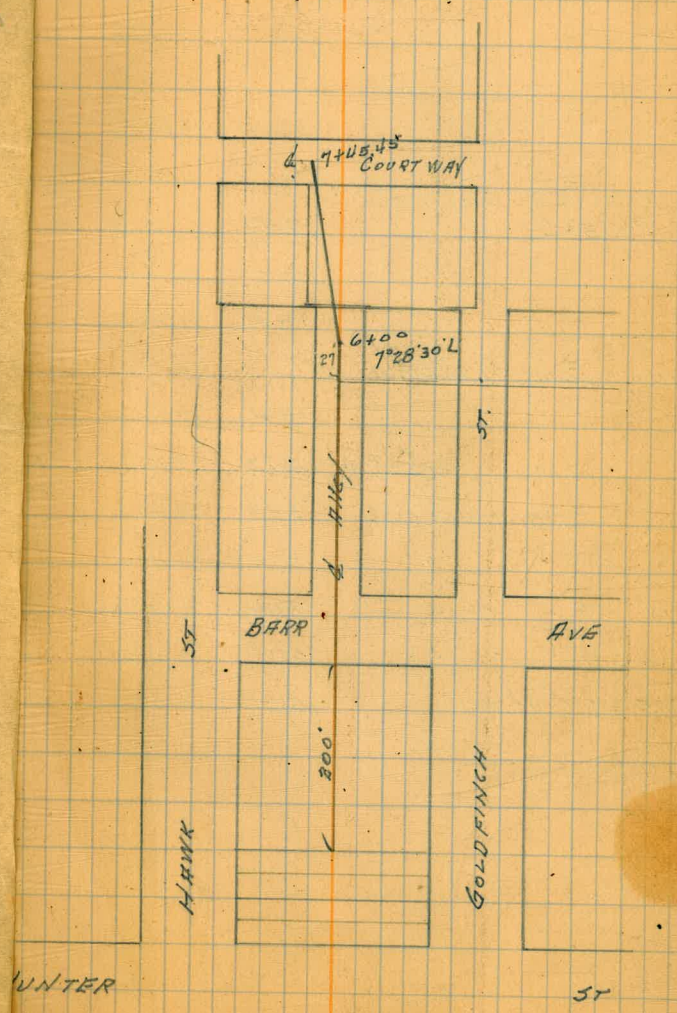
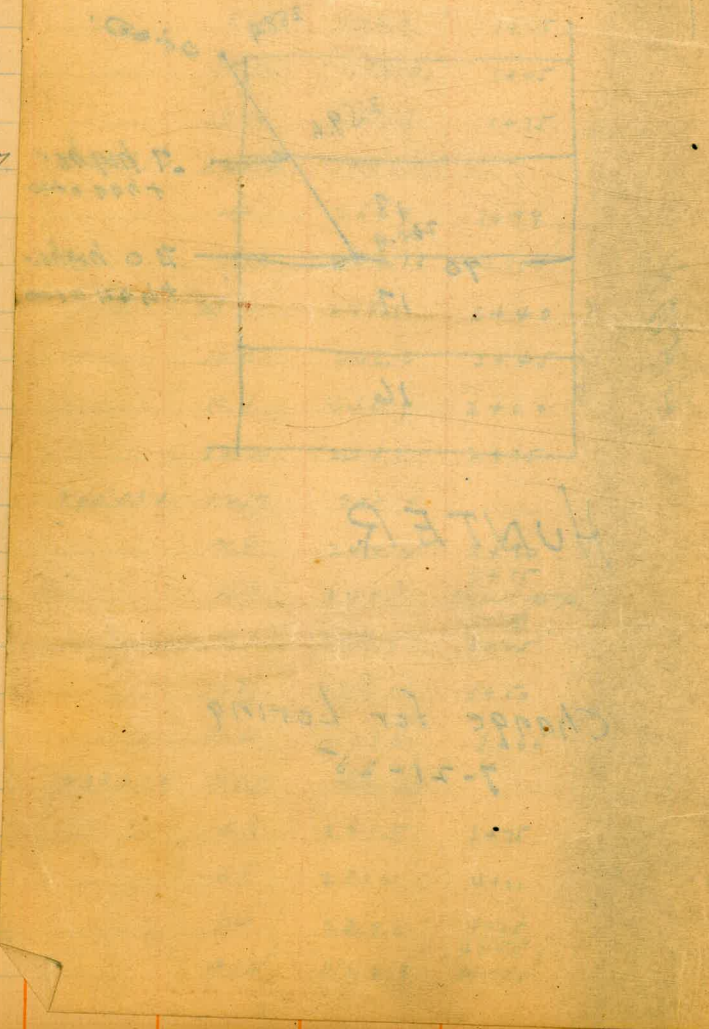
1.01

+50

+75

4

+30 POT.





+50			11.0	227.0	4+75
+75			12.9	225.1	5+00
TP	0.48	22578 ✓	12.71	22530	
5			0.8	225.0	5+W
+35			2.8	223.0	5+50
+55			6.0	219.8	5+80
+56			7.9	217.9	5+81
+73 Δ	66°46'R	see page 25	8.5	217.9	5+98
6	Δ 7°28'30"L		10.97	214.81	07 100
+29			12.4	213.4	
+30			13.2	212.6	
+32.20	= Fence S. of lot.				
+50			13.4	212.4	
TP	1.10	21505 ✓	11.83	21395	
+91.10	= E. Edge concrete drive		3.43	211.62	
7+05.30	= W ✓		4.02	211.03	
+24.80	= E ✓		4.74	210.31	
+33	= W ✓		5.74	209.31	
+45.45	= d Court Way		5.69	209.36	

Abandoned  
See page 54 for  
continuance to E  
of Goldfinch St



8/1/21 Gregory. Sewer Levels & Lockdown  
 from 50' N. of Hunter to bottom  
 of Canon in Avalon Heights  
 see sketch page 22  
 26908 26902 SP 5W  
 Lockdown

50' N. of Hunter = 0+00	0.06	26908	26902	SP 5W Lockdown
	on paring	6.26	262.84	
+50	✓	10.70	258.38	Not according to est. gr. CAT
T.P.	0.15	256.46	256.25	
1	on paring	2.90	253.5	
+50 = End of ✓		7.75	248.65	
+72.72	P.O.T	9.24	247.16	on hub
+75		10.0	246.40	
T.P.	139	245.11	243.72	
+95		12.4	232.7	
T.P.	019	232.41	232.22	
2		5.4	227.0	
+18		10.6	221.8	
+19		8.3	224.1	
+25		13.7	218.7	
+30		12.2	220.2	
T.P.	00	219.15	219.15	
+40		2.2	217.0	
+41		5.1	214.1	
+44		8.9	210.3	
+45		3.8	215.4	
+60		8.8	210.4	
T.P.	093	207.24	206.21	
+80	Δ 72° 51' R	5.29	201.8	on hub
3		11.7	195.4	
T.P.	0.08	194.51	194.43	

Flashed  
 11-5-22  
 CAT

T.P.	0.81	182.32	1300	181.51
+40			3.2	179.0
T.P.	0.61	170.27	1266	169.66
+80			11.0	159.3
+83 = 5+64 pages			1131	158.96



8/13/24 Gregory

Canon Line bet Ingalls & Lark  
North of Montecito

$\Delta 11450^{\circ} R \pm 28^{\circ} 59'$

Continued Page 39

$10404^{\circ} R \pm 16^{\circ} 15'$

$8743^{\circ} R \pm 12^{\circ} 11'$

$7460^{\circ} P.O.T.$

$5970^{\circ} \Delta \pm 10^{\circ} 55'$

$4180^{\circ} P.O.T.$

$4120^{\circ} \Delta \pm 13^{\circ} 19'$

$4106^{\circ} \textcircled{O} P.O.T.$

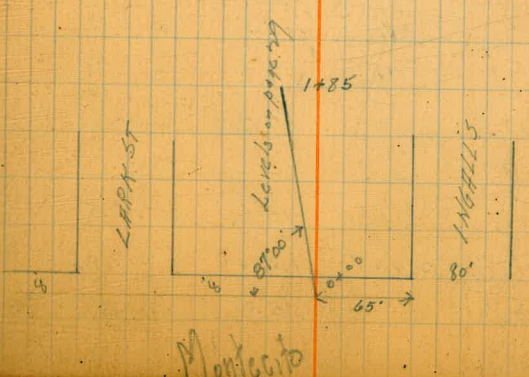
2

$2159^{\circ} \Delta 38^{\circ} 06' R$

MND 9-16-24

$1185^{\circ} \Delta 17^{\circ} 20' L$

0+00





8/13/24	Gregory	Levels on Line Shown on page 28		BPSW load down + Moisture
	1.63	277.13	275.50	2+10
0+00		11.23	265.90	on hub
+03		11.7	265.4	
TP	0.91	265.43	264.52	
+20		11.6	253.8	
TP	0.08	252.82	252.74	
TP	00	239.88	232.88	
+50		6.1	233.8	
+65		13.2	226.7	
+69		14.2	225.7	
+71		16.4	223.5	
+84		18.2	221.7	
TP	0.05	227.06	227.01	
+88		5.0	222.1	
+94		6.1	221.0	
+96		9.8	217.3	
1+06.0		10.4	216.7	
+07.0		7.7	219.4	2'W = 3.2 lower
+28		11.0	216.1	
+31		13.5	213.6	
+40		14.0	213.1	
+42		12.7	214.4	
+50		15.0	212.1	
+71		15.6	211.5	
TP	0.21	214.27	214.06	
+85 Δ	17.20'L	5.38	208.9	on hub

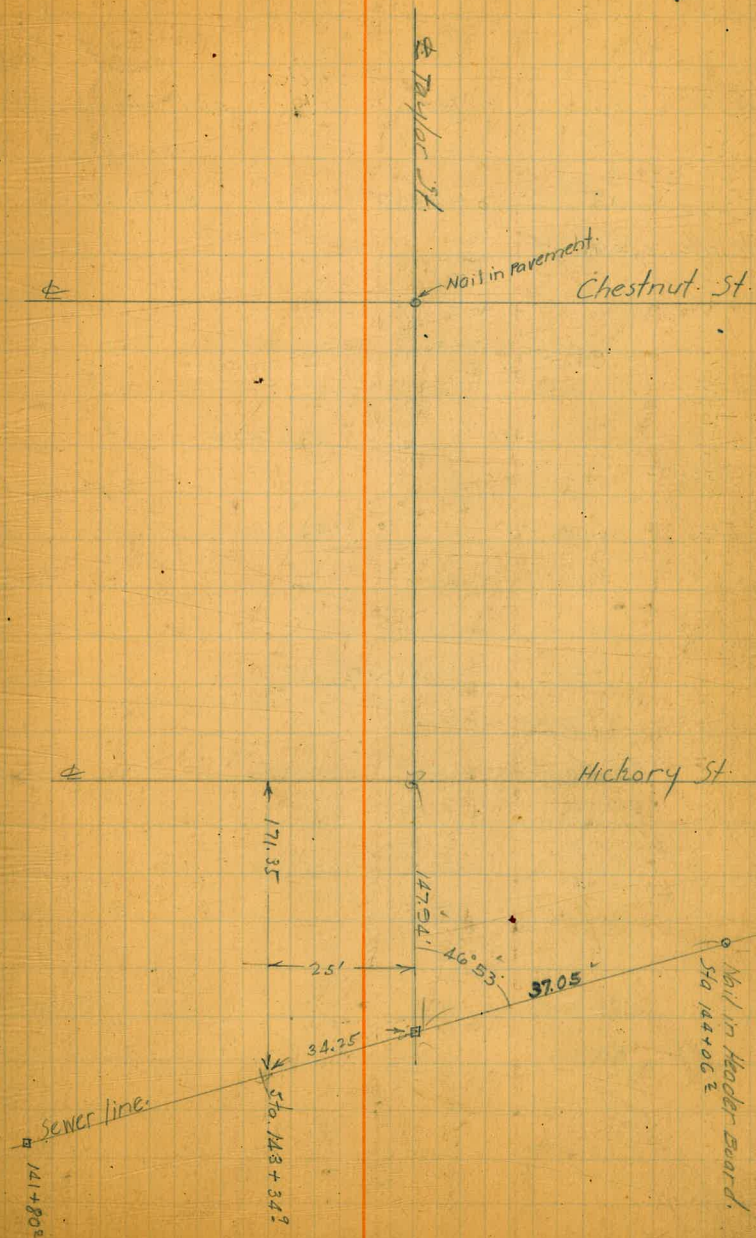
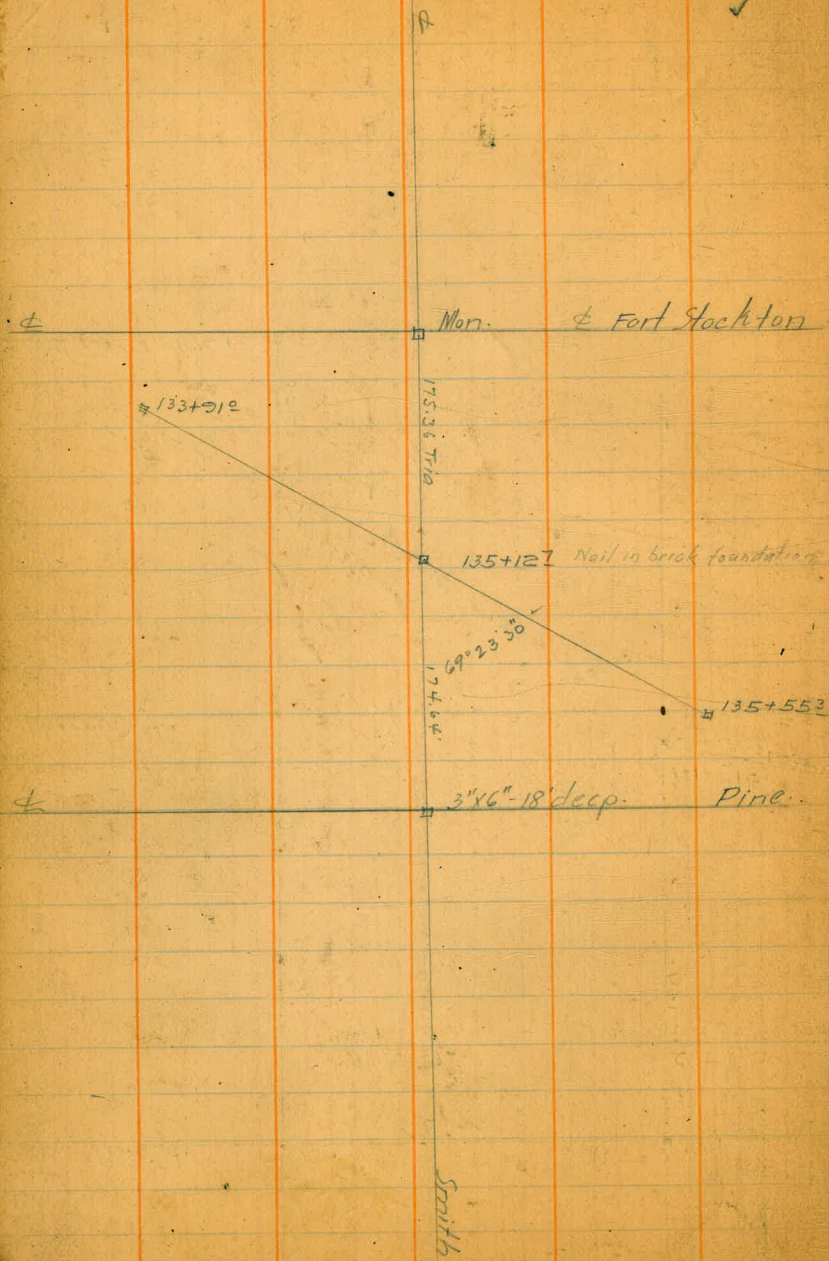
				9.0	205.3		
				10.5	203.8		
				14.1	200.2		
				15.2	199.1		
				12.2	202.1		
				12.6	201.7		
				15.7	198.4		
				18.2	196.1		
				22.0	192.3		
			TP 1.20	202.48	12.99	201.28	
				9.3	193.2		
				4.0	198.5		
			+59.10	38.06'R	5.61	196.9 on hub	
				4.9	197.6		
				3.4	199.1		
			3+13		7.25	195.2 on hub	
				12.3	190.2		
			TP -0.02	190.74	11.69	190.79	
				4.9	185.9		
				5.5	185.3		
				8.9	181.9		
			+06	0.44	188.18	9.03	181.74
				6.5	181.7		
				10.9	177.3		
				12.1	176.1		
				7.0	181.2		

Continued Page 38









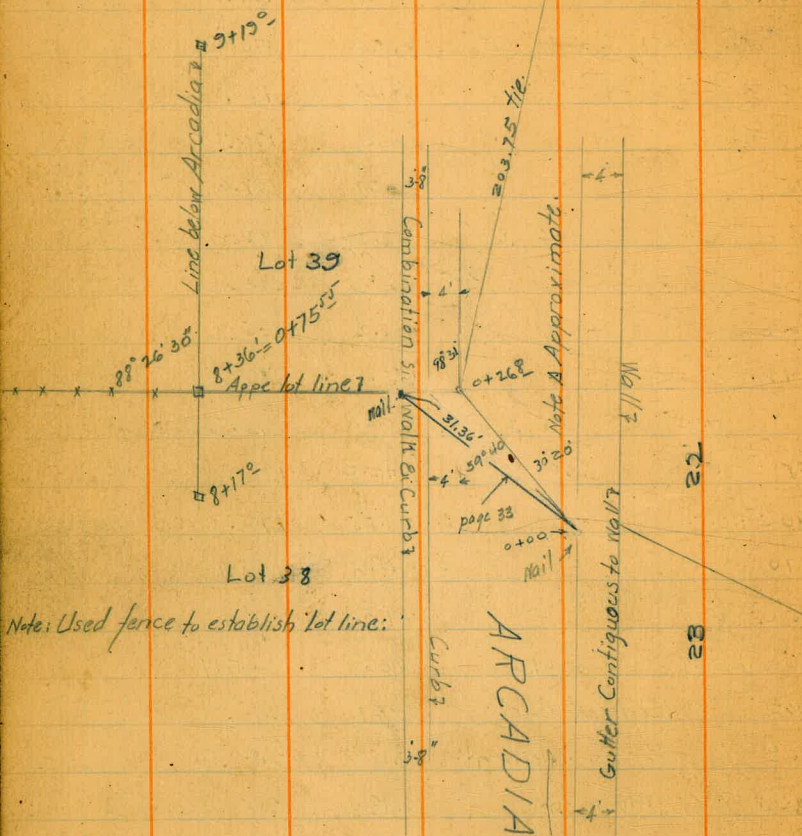






Line between Lots 39 & 40 to an intersection with the line below Arcadia:

Donnan  
Steck  
Kelly Sep 1st 1924



Note: Used fence to establish lot line:

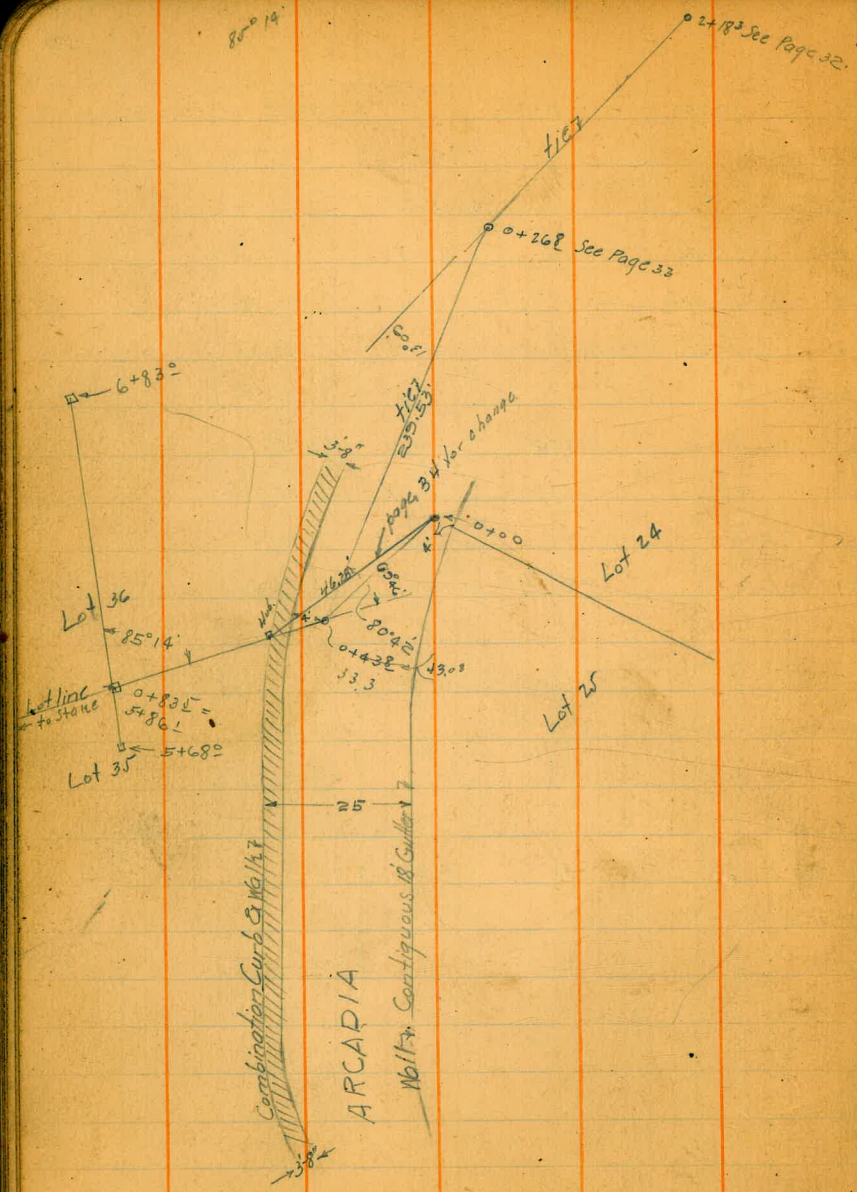
Sta	+	π	-	File
	0.72	205.91		205.19 Sec Page 32
0+0-0			6.17	199.74
0+26.8 Δ			5.20	200.71
0+30.8	On gutter Payment		5.19	200.72
0+30.8	On Curb		4.71	201.20
0+34.5	On inner edge walk		4.67	201.24
0+40			5.4	200.5
#	0.30	193.84	12.37	193.54
#	0.95	183.24	11.55	182.29
0+75.5 = 8+36			11.08	172.16
8+17	Check		8.67	174.57 = 174.65

Relocation of above from 0+00 to 0+34.5

same as above	0+00	7.28	207.02	199.74
+11.0	on pavement		6.68	
+25.25			6.45	
+27.0	on curb + walk		5.90	
+31.36 Δ = 0+34.5	above		5.79	

Plotted  
11-3-24  
CAT





	+	Δ	-	EIC	34
	0.24	205.43		205.19 See Page 32.	
0+00	On Pavement	↑	7.15	198.28	
43.08	"				
0+438 Δ	"		6.15	199.28	
0+478	In Gutter	"	6.25	199.18	
0+479	On Curb		5.70	199.73	
0+500	On Walk		5.69	199.74	
0+518	Edge Walk		5.66	199.77	177.35
0+58	Edge of fill Ground.		6.1	199.3	
#	1.22	193.85	12.76	194.67	
#	1.56	183.88	11.57	182.32	
0+835 = 5+861			4.73	179.15	
5+680	Check on Old line		6.57	177.34 = 177.35	

see notes below for change

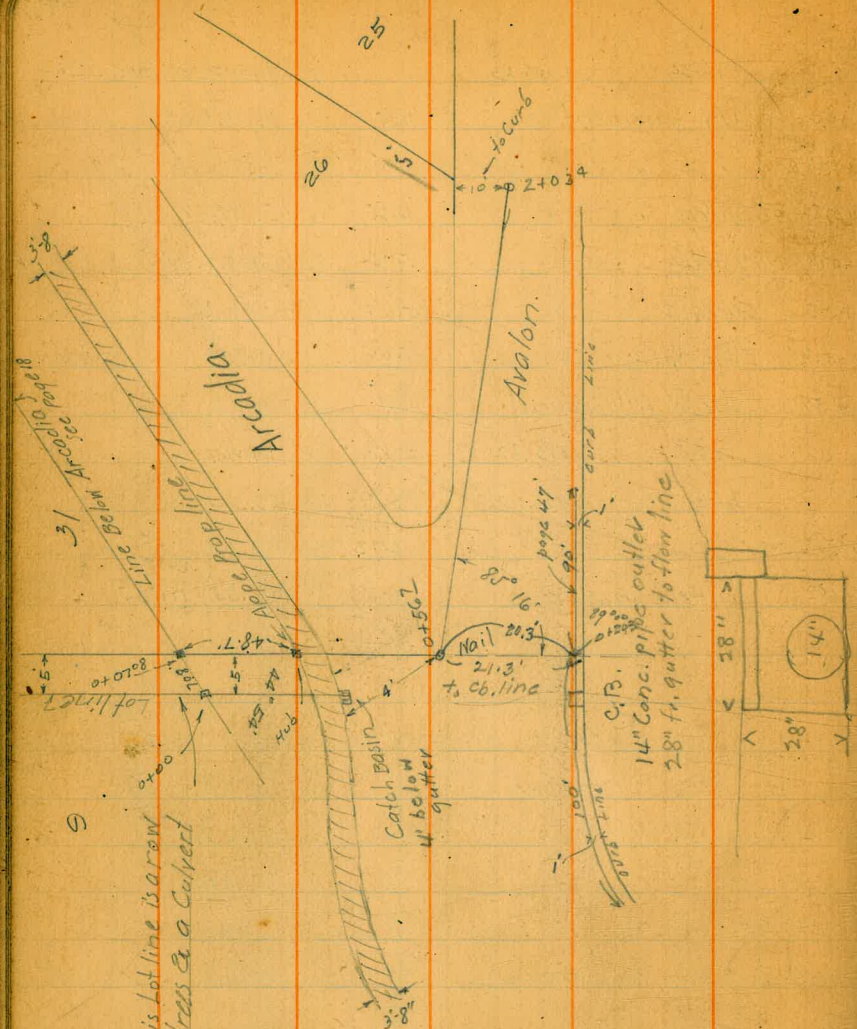
Plotted 11-2-24 CAT

30 meas above

Relocation of above from 0+00 to 0+51.6

0+00	7.00	205.28		198.28	
+20	on pavement		6.35	198.93	
+35	"		6.18	199.10	
+38.015	on curb		5.69	199.59	
+46.38 = N.L. Arcadia = 0+51.6 above			5.59	199.69	on hub





Note: Along this lot line is a row of Eucalyptus trees & a Conduit

	+	x	-	E/c
	10.69	216.76		206.07 Hub Sec Page 17
00			Hub:	
+25			12.54	204.22
#	12.32	228.33	4.8	211.0
0+41			0.75	216.01
0+48 <sup>Inner</sup>			3.1	225.2
0+52 <sup>On Edge Walk</sup>			2.77	220.56
0+56 <sup>Curb</sup>			2.77	225.56
0+52 <sup>Pavement Gutter</sup>			3.21	225.12
0+56 <sup>Δ Pavement</sup>			3.15	225.18
1+00			3.55	224.78
#	10.14	237.71	0.70	227.63
1+50			8.78	228.99
2+03			1.87	235.95

Abandoned

S

House on lot 26

1.69	227.25	225.56	See Above:
Soil pipe Comes from house about this	E/c	5.3	224.0
Pipe would have to be about this at Car house:	7.0	220.35	







	+	π	-	
	10.57	237.84		227.27 See Page 19 On Curb
	12.51	249.97	0.38	237.46 On Septic tanks
	12.94	260.88	2.11	247.88 <sup>6</sup>
3+91Z			Hub. 2.70	258.1
3+50			5.3	255.5
3+00			7.7	253.1
# 2+68A	2.51	254.18 <sup>6</sup>	9.15	Hub 7.5 251.64
2+50			3.2	251.0
2+00			4.6	249.6
1+70A			5.52	Hub 7.4 248.68
1+66			6.2	248.0
1+61 <sup>2</sup>	Curb		10.24	243.92
1+61 <sup>2</sup>	Gutter Pavement		10.87	243.29
1+40	"	"	9.99	244.17
1+36 <sup>2</sup>	Edge Pavement		9.52	244.64
1+36 <sup>2</sup>	Ground		Hub 10.00	244.16
1+01/2 P.O.T.	0.60	242.08 <sup>2</sup>	11.86	242.38 <sup>2</sup>
#	1.08	231.98 <sup>3</sup>	12.05	230.88 <sup>5</sup>
0+85			2.2	229.7
0+50			9.2	222.7
# 0+35A	0.19	219.14 <sup>5</sup>	12.97	Hub. 218.88 <sup>6</sup>
0+00 = 2+74 <sup>2</sup>			8.98	210.14 <sup>7</sup> = 210.15 Bob

Plotted  
11-5-24  
CAT

	+	π	-	E/c
	12.65	222.43		209.78 On Pavement See Page 32
	7.15	226.78	2.80	219.63 ✓
On Curb				10.99
P.L. = 00 = 5' from Curb Line				10.77
+10				9.10
+60				0.6
#	12.90	238.69		0.99
74.33 = End lot				10.0
				225.79
				216.8

Above is Along lot line between 18 & 19



	+	π	- Continued from Page 29.	
		188.18		
4+20° Δ L	19° 19'		6.37	181.8
4+50			4.1	184.1
4+80°			6.45	181.7
4+95			9.5	178.7
5+0			8.9	179.3
+15			7.0	181.2
+50			7.0	181.2
# 10° 55'				
5+70° Δ L	0.81	178.07	10.92	177.26
5+83			7.6	170.5
6+0			7.9	170.2
6+30			7.0	171.1
6+50			8.8	169.3
#	1.72	167.78	12.01	166.06
6+89			10.0	157.8
7+0			9.5	158.3
7+35			7.6	160.2
7+50			9.9	157.9
#	0.20	155.60	12.38	155.40 Top of Guard Stake
7+60° ROT			Hub 1.09	154.5
7+80			10.3	145.3
8+0			8.5	147.1
+15			8.8	146.8
#	0.19	143.36	12.43	143.17
8+30			2.7	140.7
+50			3.4	140.0
8+64			3.1	140.3

	+	π	-	
	143.36			
8+74° Δ RT	12° 11'		Hub 4.78	138.6
9+0			7.3	136.1
9+15			8.5	134.9
9+50			8.2	135.2
9+70			7.7	135.7
10+0			11.7	131.7
# 0.37 16° 15'			Hub 12.81	130.55
10+04° Δ RT	130.95		9.9	121.0
10+50			9.3	121.6
10+80			13.2	117.7
# 0.24 118.34			12.80	118.18 Top Sta Stk.
11+50° Δ RT	28° 59' R		4.87	113.5
11+70			5.2	113.2
11+90			11.0	107.4
12+0			Bottom Canyon	102.8
12+05			11.8	106.6
12+10			10.0	108.4
12+30			5.2	113.2
12+50			6.4	112.0
12+60° Δ L	0.57 33° 28' L 9		Hub 8.84	109.55
12+88			11.0	98.8
13			10.1	99.7
13+30			9.0	100.8
+50			12.4	97.4
# 0.46 98.45			Hub 11.83	97.98 Top of Sta Stk.
13+75			5.5	92.9



From Page 28

11+72<sup>2</sup>A Sec Page 23

14+76<sup>2</sup> = 9+48<sup>2</sup> Sec Page 23 Alt 40°19'

12+63<sup>2</sup> Alt 23°28'

+

14+20  
+20  
+10  
14+76<sup>2</sup> = 9+48<sup>2</sup>

87.16

π  
98.05

39

-

5.0	93.4
5.7	92.7
10.4	88.0
11.34	87.05 <sup>8</sup> = 87.16 - Sec Page 23



56+62<sup>o</sup> Mission Valley

55+36<sup>o</sup> Mission Valley  
9153<sup>o</sup> =  $\Delta$  (78° 05')

7+00<sup>o</sup> Δ Rt. 26° 07'

6+26<sup>o</sup> Δ Rt. 23° 13'

5+41<sup>o</sup> Δ Rt. 10° 48' 9° 24'  
5+41.50

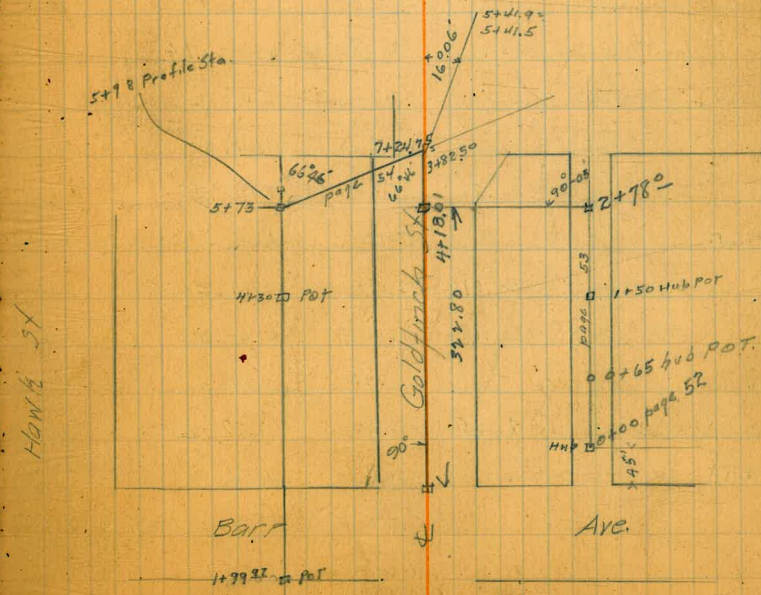
5+45<sup>o</sup> Δ Rt. 17° 30' moved angle pt 3. see page 54  
3+82.50 = New  $\Delta$  16° 06' R.

3+45<sup>o</sup> P.O.T.

2+50 P.O.T.

0+00

395 13  
12 6  
582 .50  
573  
40





	+	π	-	
	3.88	252.54 ✓		Hub 249.66 Sec Page 37
	2.55	249.51 ✓	5.58	246.96 ✓
0+0			5.51	244.0
0+50			11.8	237.7
#	0.93	237.72 ✓	12.72	236.79 ✓
100			5.0	232.7
# 150			11.0	226.7
#	0.32	225.32 ✓	12.72	225.00 ✓
200			5.1	220.2
2+35			10.1	215.2
#	2.21	215.12 ✓	12.41	212.91 ✓
2+50° P.O.T.			3.58	211.5
2+65			6.8	208.3
2+86			12.2	202.9
#	1.45	204.19 ✓	12.38	202.74 ✓
300			3.6	200.6
3+30			9.2	194.8
#	2.09	193.86 ✓	12.42	191.77 ✓
3+45° P.O.T.			7.90	186.0
#	1.34	182.61 ✓	12.59	181.27 ✓
#	0.87	171.18	12.30	170.31 ✓
3+78°			10.2	161.0
#	0.34	158.60 ✓	12.92	158.26 ✓
3+95° ART			4.61	154.0
400			5.7	152.9
4+15			10.0	148.1

see page 54

	+	π	-	
		158.60		53484° ART 66.92 MI 56+62° M.V. 63.28
4+33			7.7	150.9
#	1.70	147.59 ✓	12.71	145.89 ✓
4+50			3.0	144.0
4+68		see page 54	9.0	138.6
5+00			10.5	137.1
5+20			10.2	137.4
#	1.09	136.05 ✓	12.63	134.96 ✓
5+41.5			0.76	135.3
5+41.2 ART			3.5	132.6
5+50			5.9	130.2 ✓
5+60			12.35	123.70 Rec 1 ✓
#	0.58	124.28 ✓	12.35	123.70 Rec 1 ✓
6+00			4.2	120.1
#	0.70	115.27 ✓	9.71	114.57 ✓
6+26° ART			7.4	107.9
+00			10.71	104.56 ✓
# 150		106.08 ✓	6.95	99.13
7+00 ART			10.69	95.39 ✓
#	0.95	96.34 ✓	11.7	94.6
7+50			11.05	85.29 ✓
#	0.58	85.67 ✓	1.3	84.4
8+00			6.6	79.1
8+50			11.63	74.04 ✓
#	0.08	74.12 ✓	3.6	70.5
9+00			6.4	67.7
9+32 = 55+36° Mission Valley			11.09	63.03
56+62°			11.13	62.99 = 63.28

56+62° M.V.



11/13/24 Gregory

Sewer Levels on  $\Delta$  of BIK.  
bet Pine & Cherry from 2' E of  
 $\Delta$  of Ampudia To 75' E of E.L. of  
Ampudia

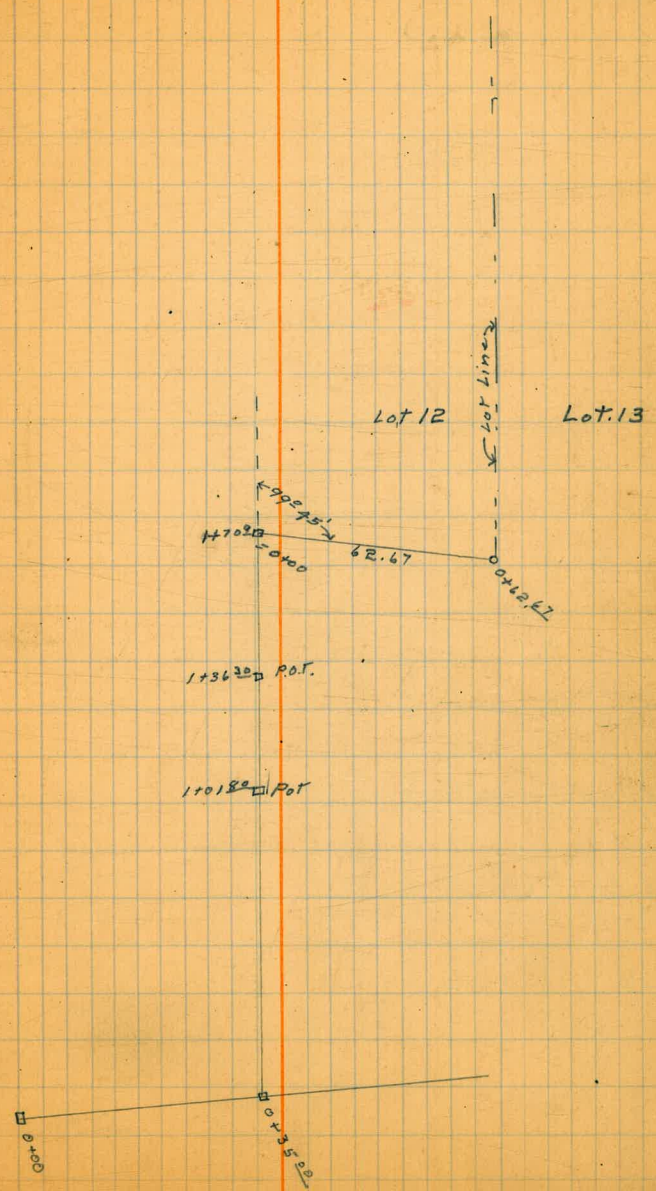
	6.76	273.82		267.06	NETRIA's 2 Ft Stockton
150' N of Pine 8.75' E of E.L. Ampudia = 0+00	5.74	275.53	4.03	269.79	
			8.9	266.63	
+25			10.8	264.7	
T.P.	3.85	267.19	12.19	263.34	
+50			4.8	262.2	
+60			5.9	261.3	
+75			8.3	259.9	
+96			10.2	257.0	
+98			11.5	255.7	
1+00			11.5	255.7	
+03 = Edge of paving			11.98	255.31	
✓ ✓ ✓		13.3'	West of $\Delta$ Ampudia		

Plotted  
11-14-24  
CAT

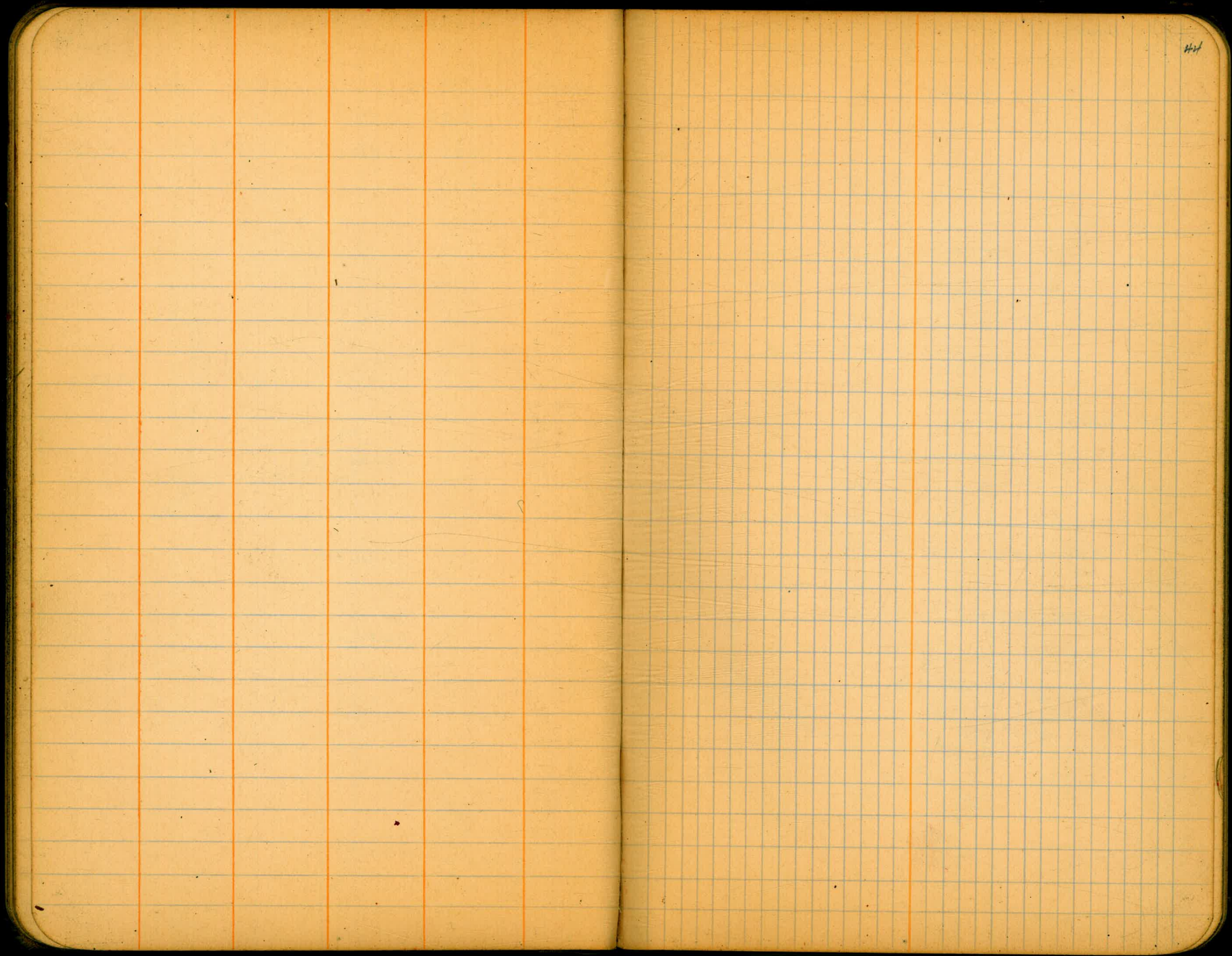


Sewer Extension in Area d14 Drive sec P. 36

00=1+70 <sup>00</sup> A36	5.13	253.77	248.64	on Hub
0+30	(2+00.9)	5.1	248.7	
0+62.67	(2+33.57)	5.3	248.5	









1/2/25 Gregory

Sewer Levels from d of  
1b13 St 101' N-X Hunter  
thru 61K E of 1b13

45

	5.11	274.13		269.02	BP SW Jackson + Hunter
101' N. of N.E. Hunter on d of 1b13 = 0+00			12.8		
0+26			12.4		
+27			11.8		
+33			11.3		
+40			10.8		
T.P.	1.84	266.55	9.42	264.71	
+55			2.9		
1+00			3.2		
1+39			3.5		
+41 Δ 90° 00' R.			2.2		
+42 = concrete foundation wall (poor)			2.0		
+50 = s. edge			0.0		
T.P.	9.10	272.35	3.30	263.25	
+80 = N. side of garage wood.			3.9		
T.P.			2.30	270.05	
2+02 = under garage.			1.8		

Abandoned  
CAT

This line is the bunk  
see page 46  
for the connection to the two  
houses under consideration



1/2/25

Gregory

Sawyer Levels Hawk St 24'E. of W.L. Hawk  
on a line which is produced  
N. from stoo on page 14400  
27 696

46

	5.99	275.01	267.02	SW. Jackdaw + Hunter
St. Hunter = 24'E. of W.L. Hawk = 0+00	3.07	<del>271.05</del> 275.01	6.98 268.03	
+10 on parv			3.26 267.79	
+25 ✓ ✓			2.73 268.32	
+40 ✓ ✓			3.15 267.90	
+45 ✓ ✓			3.07 267.98	
+45.1 on curb			2.46 269.59	
+50			2.6 268.5	
+98			4.0 267.1	
1+00 = Δ 90° L.			4.4 266.7	
<del>+20</del>			3.7 267.4	
<del>+24 = W.L. Hawk</del>			3.1 268.0	

Plotted  
1-2-26  
CAT



1/25 Gregory

Sewer Levels  
Avalon Drive at Arcadia Dr.  
see sketch page 35

stn 0+56.7 page 35	4.30	229.86	225.56
= 0+00	on paving	4.67	225.19
+10	✓ ✓	4.75	225.11
+19.0	✓ ✓	5.41	224.45
+20.3	89'00" L in cement gutter	5.74	224.12
+60	✓ ✓ ✓	5.45	224.41
+88	✓ ✓ -	4.10	225.76
1 +10.3		1.73	228.13

Levels S. of 0+20.3

0+20.3 above			
= 0+00	91'00" R. from Line to West	5.74	224.12
+04.3	N. edge cement C.B. Top	5.74	224.12
+04.4	✓ ✓ ✓ Flow Line	8.00	221.86
+06.7	5 ✓ ✓ ✓ ✓	8.00	221.86
+06.75	✓ ✓ ✓ ✓ Top	5.71	224.15
+30	on paving	4.72	225.14
+65	✓ ✓	2.94	226.92
1 +00		0.94	228.92

Plotted 1-5-22  
CAT  
25







1) 2) 3)

Levels from 8+36 page 33  
straight to 9+50 page 32

	12.32	171.22	158.90	hub 4+35.65
0+00 = hub & 9+50	12.32	158.9	9+26.9	
+01.0	11.6	159.6	9+25.9	
+22	8.2	163.0	9+04.9	
+31	5.2	166.0	8+95.9	
+43	1.8	169.4	8+83.9	
+59.5	2.7	168.5	8+67.4	
+62	1.4	169.8	8+64.9	
+78	1.8	169.4	8+42.9	
+88	0.5	170.7	8+38.9	
T.P.	1.95	172.96	0.21	171.01
+90.82 = 8+36	0.71	172.25	8+36.1	

Contd. Page 17

This stationing used  
in plotting



1/2/25 Gregory Sewer Levels 2' N. of  
 S Line Lot 18 Avalon from  
 1' E of WL of Hawk St to  
 W. Line Lot 18  
 237.92 from page 48

1+17 page 48  
 20+00

on walk	10.57	227.35
+06.0	9.4	228.5
+035	6.0	231.9
+65	1.1	236.8
+75.33	+ 1.0	238.9

Plotted  
 1-12-25  
 CAT

50

1/2/25 Gregory Sewer Levels on Lot Line  
 between Lots 19 & 21 Avalon  
 from 1' E of WL Hawk to WL of  
 Lot 21

225.29 from page 48

1' E of WL Hawk St to 05 page 48 20+00 on walk	13.53	211.76
+01.0 = inside edge of Walk.	13.50	211.79
+01.1 Top of Wall	11.21	214.08
+025.	7.0	218.3
+50	2.7	222.6
T.P. 6.00 231.29	0.00	225.29
1+04.91 = WL Lot 21	0.00	231.29



Sewer Levels from EL Hawk & d  
Court Way to

6 Court Way  
= EL Hawk  
= 0+00

213.01 from page 48

Contd from  
Page 32

+ 30	on paving	0.80	212.21	1400
+ 30	✓ ✓	1.19	211.82	1430
+ 42	in gutter	1.90	211.11	144✓
+ 42	on curb	1.22	211.79	144✓
+ 44.97	on walk	1.25	211.76	144.97

Plotted 1-12-25



1/2/25 Gregory  
 sketch on page 40  
 Sewer Levels  
 of Alley bet. Falcon + Gold Finch  
 from 45' Max Barr to 32.3' W  
 from 0 W. to 6 Alley W. of Gold Finch 5473 P. 25

BM.	0.60	249.78		249.18	on Hub 1177 25 P. 25
T.P.	0.24	238.32	11.70	238.08	
00			10.95	227.3	on Hub sec P. 40
T05			10.2	28.1	
T25			8.5	29.8	
T45			7.4	30.9	
T65			4.90	33.4	on Hub
T78			1.4	36.9	
1+00			1.4	36.9	
T65			3.5	34.8	
T80			5.6	32.7	
2+00			9.1	29.2	
T25			12.8	25.5	
T.P.	0.42	226.69	12.05	226.27	
T50			3.6	23.1	
T65			4.7	22.0	
2+78	Δ ??		7.90	18.8	on Hub
3+00	Δ 90° 05' L		9.8	16.9	
T35			13.7	13.0	
T.P.	0.60	214.79	12.50	214.19	
T55			5.3	09.5	
T69			7.9	06.9	
T70			10.2	04.6	
T85			10.0	04.8	
4+00			14.2	200.6	



TP	0.52	214.79	12.73	202.06	
4+06		202.54	2.4	200.14	(See Sketch Page 40)
4+18			7.63	194.95	on Hub @ Gold Finch
<del>427</del>			12.5	190.1	
<del>438</del>			20.9	181.7	
442			27.9	174.7	
445			28.4	174.2	
448			28.0	174.6	
<del>460</del>			15.9	186.7	
470			7.8	194.8	
485			0.4	202.4	
T.P.	8.79	211.33	0.04	202.54	
495			2.6	208.7	
T.P.	7.08	218.11	0.30	211.03	
<del>5+00</del>			6.6	211.5	
440			3.9	214.4	
5+5745			1.40	216.7	on Hub
Chkonhub 6+00 Δ See P. 26			3.32	214.79 = 214.81	= 5+73 P 26440

see page 54  
for proper location  
of this portion

Contd Page 41



4/8/24 Gregory Sewer Levels from 6 of Alley bet Goldfinch & Hawk to 2 Goldfinch

page 26	v.v.7	v.17.08	214.81	hub at 6 <sup>page 26</sup>	+45
5+73 A	66°46' R.	0.33	216.75	5+98	+50
+98		3.5	213.6	6+23	+55
6+30		6.1	211.0	6+55	+75
+35		7.5	209.58	6+60	+85
T.P.	0.35	204.67	12.76	204.32	5
+50		3.8	200.9	6+75	T.P. 178 145.66
+58		5.7	199.0	6+83	+26
T.P.	0.09	191.88	12.88	191.79	+34
+71		5.5	186.38	6+96	+41.5 = 5+41.9 page 41
+75		8.2	183.7	7+00	10.26
T.P.	0.87	179.51	12.74	179.14	135.40 on hub
+79		2.1	177.4	7+04	
+92		10.2	169.3	7+17	
T.P.	0.25	166.90	12.86	166.65	
+99		0.60	166.3	7+24	
7+04		5.7	161.2	7+29	
+14		7.2	159.7	7+39	
+24.75	Equation Δ = 3+82.50 page 41	7.4	159.5	7+49.75	
4+00		11.5	155.4		
+06.0		11.5	155.4		
T.P.	0.39	154.50	12.79	154.11	
+14		3.0	151.5		
+18		6.9	147.6		
+25		8.2	146.3		
+35		5.8	148.7		

stationary used in plotting CAT

154.12  
5+73  
1 51.8  
724.8  
54

9.2	145.3
10.0	144.5
11.7	142.8
14.7	139.8
15.0	139.5
16.7	137.8
10.62	143.88
7.7	138.0
8.5	137.2

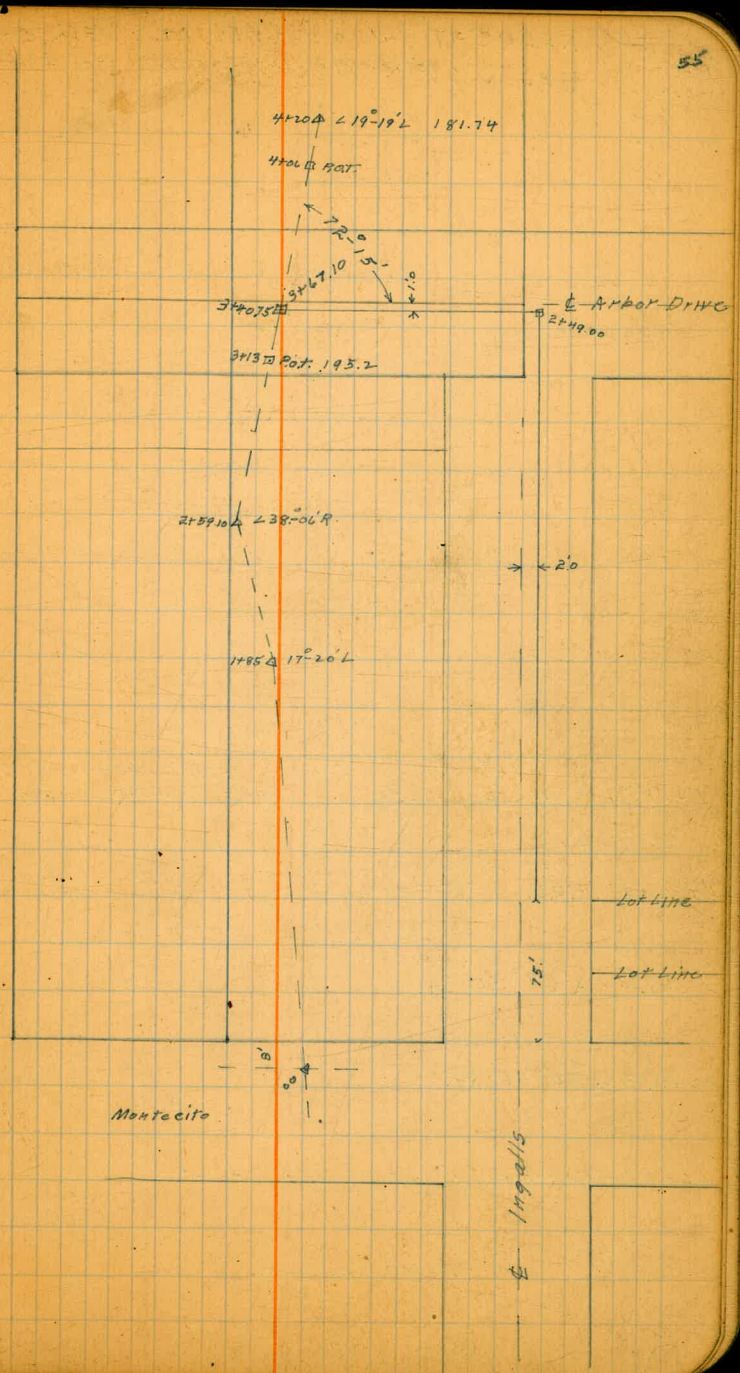


Sewer Levels on Line 2.0 of E Ingalls  
 from Pt. 75' N. of N. Line Montecito to a Line 1.5 of  
 S. Line Arbor Drive thence West to Pt. Line, Page 28

B.M.	3.77	279.27		275.5	S.W. Montecito + Jackdaw
T.P.	0.17	270.28	9.18	270.29	
00=75' N of Montecito			1.7	268.4	
150			3.0	267.3	
1+00			4.3	266.0	
1+50			5.5	264.8	
2+00			7.7	262.6	
2+25			8.6	261.7	
T.P.	0.26	257.27	13.27	257.01	
2+49.00 ± 90° L			11.85	245.4 ✓	on stub
T.P.	0.19	244.72	12.74	244.53	
2+70			6.5	238.2 ✓	
T.P.	0.0	232.08	12.64	232.08	
3+05			9.4	222.7	
T.P.	0.01	219.16	12.93	219.15	
2+23			2.6	216.6	
T.P.	0.19	207.42	11.93	207.23	
3+49			5.0	202.4	
3+60			11.4	196.0	
T.P.	2.47	197.27	12.62	194.80	
2+67.10 ± 72			5.85	191.4 ✓	on stub
3+3 P. of P. 29			2.04	195.23 = 195.27	

Plotted 2-1-1947  
 C.A.T.

Lark St





Moore  
Preston  
Walker  
#4/25

RELOCATION of PRELIM. SEWER LINE  
BELOW ARCADIA DRIVE See P. 18 THIS BOOK

56

5+44.77 =  $\Delta$  STA. 11+72.70  $91^{\circ}48'$  RT. to JUNCTION of M.V. LINE STA 13+87.45  
JUNCTION WITH KING'S CANYON

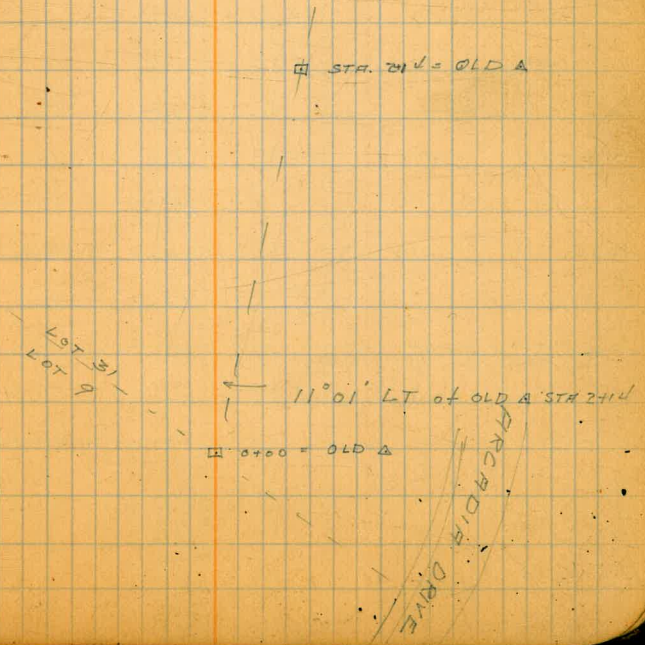
4+32.50 P.O.T.

3+49.38 =  $\Delta$   $68^{\circ}30'$  Lt.

2+11.93 =  $\Delta$   $34^{\circ}46'$  RT.

0+00 = Set New Hub  $11^{\circ}01'$  Lt. of old A STA. 2+14

Page 57 for levels





Moore  
5/1/25

LEVELS ON PRELIM. SEWER RELOCATION  
BELOW ARCADIA DRIVE  
sec P 50

ON OLD A Hub 11.29	206.45	195.16	STA. 2+10
0+00 on New Hub		0.63	205.9
+07		2.5	204.0
+25		5.0	201.5
+50		7.3	199.2
+75		8.7	197.8
1+00		10.6	195.9
+25		13.0	193.5
T.P. 0.93	194.43	12.95	193.50
+50		4.5	189.9
+60		7.1	187.3
+75		8.7	185.7
2+00		12.4	182.0
T.P. 0.38	182.51	12.30	182.13
+11.93 Δ on Hub		2.85	179.6
+25		3.2	179.3
+50		7.0	175.5
+75		9.1	173.4
3+00		12.6	169.9
+16		13.9	168.6
+49.38 Δ on Hub		12.80	169.7
T.P. 0.28	169.99	12.80	169.71
+75		10.8	159.2
T.P. 0.26	157.75	12.50	157.49
4+00		11.0	146.8
T.P. 0.68	145.93	12.50	145.25

Plotted on Sewer Profile Sheet  
5-8-25. CAT

145.93

4+32.50 P.O.T. on Hub		11.66	134.2
T.P. 0.44	134.71	11.46	134.27
+50		12.9	121.8
T.P. 0.45	122.71	12.45	122.26
T.P. 1.34	111.27	12.78	109.93
4+75		9.6	101.7
T.P. 0.36	99.42	12.21	99.06
T.P. 0.39	87.01	12.80	86.62
5+00		4.4	82.6
+10		11.6	75.4
T.P. 1.87	76.20	12.68	74.33
+22		6.5	69.7
+26		8.0	68.2
+27		10.1	66.1
+31		10.2	66.0
+33		6.7	69.5
+44.77 on old Hub		5.79	70.41
4+72.70 on new line			

check this  
E.I.V. please  
70.17



Sewer Construction  
 & Chestnut St  
 from & Arista to 225' E of & Arista

1308  
 23420  
 871  
 23507

M.H. @ Arista = 0+00		235.07			225.0	+6.96
			3.11	231.96	226.5 } 0mg	+5.46
+50			1.83	233.24	228.79	+4.45
1	003	247.29		227.26	BM Arista	+4.44
			1176	235.53	231.09	+4.44
+50			944	237.85	233.39	+4.46
2			706	240.23	235.68	+4.55
+25 DE			5.94	241.35	236.83	+4.52



Sewer Construction  
 & Arista from & Chestnut  
 To 175 S. X Whitman  
 v3507 ramp 58

22498

59

M.H. & Chestnut 20100		311	23196	225.0	+696
+50		480	230.27	223.21	+7.06
1		680	228.27	221.42	+6.85
+50		873	226.34	219.63	+6.71
2		1064	224.43	217.84	+6.59
+50	0.81 223.42	1246	222.61	216.05	+6.56
3		260	220.82	214.27	+6.55
+50 M.H. & Whitman		440	219.02	212.50	+6.52
4		574	217.63	211.10	+6.53
+50		726	216.16	209.69	+6.47
5		891	214.51	208.29	+6.22
+25		1139	212.03	207.59	+4.44

v1820



Cypress Richmond to Vermont: 50' Wide 10 Cds 7 1/2 Qts.

Dunnary  
Bliss  
Northern

June 27th 1925

For new sections on this intersection see Book 1208 Page 11.

3.13 288.09 280.96 N.E. Ver & Perrin

3.04 283.92 7.71 280.38 Hub 13 Ver & N.E. Cypress

W.L. of Vermont St Int 80' St 14 Cds.

N.L. 2.1 281.8

2.3 281.6

2.7 281.2

E 2.5 281.4

2.5 281.4

2.3 281.6

S.L. 2.1 281.8

W. Cb of Vermont

S.L. 4.0 279.9

2.7 281.2

2.7 281.2

E 3.0 280.9

3.1 280.8

3.3 280.6

N.L. 3.2 280.7

W. 1/4 of Vermont.

N.L. 3.0 280.4

3.8 280.1

3.0 280.4

28392

60

E 3.5 280.4

6.9 277.0

9.7 274.2

S.L. E of Vermont. 12.4 271.5

S.L. + 20 11.7 272.2

S.L. - 25 16.4 267.5

S.L. 15.8 268.1

Cb 11.2 272.5

1/2 10.5 272.4

+5.5 Top of Concrete Manhole (Sew) 7.0 276.4

E 7.2 276.7

+5 4.3 279.6

1/2 4.3 279.6

Cb 4.5 279.4

N.L. 4.3 279.6

E 1/4 of Vermont.

N.L. 4.8 279.1

Cb 5.0 278.9

5.3 278.6

E 9.6 274.3

1/2 14.1 269.8

Cb 18.7 265.2

S.L. 22.8 261.1

+20 23.5 260.4

+10 23.1 260.8



+  
π  
283.92

1/4 Carb of Vermont.

S.L. - 50	30.1	253.4
S.L. - 25	31.7	252.2
S.L. - 15	31.1	252.8
S.L.	11.8	272.1
Cb.	18.0	265.9
1/2	14.2	269.7
ε.	9.2	274.7
1/4	5.1	278.8
cb.	5.0	278.9
N.L.	4.7	279.2

00+00 E.L. Vermont S4

N.L.	4.4	279.5
	8.5	279.4
	4.7	279.2
ε	5.5	278.4
1/2	9.2	274.7
Cb	15.1	268.8
S.L.	19.9	264.0
+26	33.1	250.8
+50	35.8	248.1
+55	38.0	245.9
0+25		
-44	28.0	255.9
-29	23.0	260.9
-14	19.1	264.8

+  
π  
283.92

61.

S.L.	11.5	272.4
cb	6.8	277.1
+4	5.1	278.8
1/4	4.5	279.4
ε	4.0	279.9
1/2	3.8	280.1
cb	3.5	280.4
N.L.	2.5	281.4
	0+50	
N.L.	1.2	282.7
	1.9	282.0
	2.4	281.5
	2.4	281.5
	2.6	281.3
	2.6	281.3
S.L.	4.0	279.9
+10	5.2	278.7
	0+70	
S.L.	1.3	282.6
cb	1.2	282.7
1/2	1.4	282.5
ε	1.3	282.6
1/4	1.1	282.8
+5.5	1.3	282.6
cb	0.8	283.1
+6	0.5	283.4



	+	Σ	-	
		283.92		
N.C.			0.3	283.6
		1+00		
N.C.			+0.5	284.4
+3			+0.4	284.3
+4			+0.1	284.0
cb			0.0	283.9
+2			0.6	283.3
1/4			0.6	283.3
±			0.6	283.3
			0.8	283.1
			0.5	283.4
S.C.			0.3	283.6
#	7.13	290.45	0.60	283.22
		1+25		
S.C.			6.2	284.0
			6.5	283.9
			6.4	284.0
			6.2	284.2
1/4			6.2	284.2
+5.5			6.4	284.0
cb			5.7	284.7
+6			5.7	284.7
N.C.			5.2	285.2
		1+50		
N.C.			4.7	285.7
+3			4.7	285.7
+4			5.2	285.2

	+	Σ	-	
		290.45		
cb			5.6	284.8
+1			5.8	284.6
			5.7	284.7
			5.9	284.5
1/4			6.1	284.3
			6.0	284.4
S.C.			5.9	284.5
		1+75		
S.C.			5.5	284.9
cb			5.6	284.8
1/4			5.8	284.6
±			5.6	284.8
1/4			5.6	284.8
+6.5			5.5	284.9
cb			5.3	285.1
+6			5.0	285.4
+7			4.5	285.9
N.C.			4.4	286.0
		2+00		
N.C.			4.2	286.2
+2			4.2	286.2
+3			4.7	285.7
+9			4.6	285.9
cb			5.1	285.3
+1			5.3	285.4
1/4			5.2	285.2

0.17  
6.4  
2.8



	+	$\pi$ 290.45	-	
$\epsilon$			5.2	285.2
			5.5	284.9
cb			5.4	285.0
S.L			5.1	285.3
		2+25		
S.L			5.0	285.4
cb			5.3	285.1
			5.3	285.1
			5.0	285.4
			5.0	285.4
cb			5.1	285.3
+1			4.6	285.8
+6			4.5	285.9
+7			4.1	286.3
N.L			3.8	286.6
		2+50		
N.L			4.0	286.4
+2			4.1	286.3
cb			4.8	285.6
			0.9	285.5
			4.9	285.5
			5.2	285.2
			5.3	285.1
S.L			5.2	285.2
		2+75		
S.L			5.3	285.1

	+	$\pi$ 290.45	-	
			4.9	285.5
			5.0	285.4
$\epsilon$			5.0	285.4
1/2			4.9	285.5
cb			4.9	285.5
N.L			3.8	286.6
		3+00		
N.L			4.1	286.3
			4.9	285.5
			5.0	285.4
			5.0	285.4
			5.2	285.2
cb			5.3	285.1
+8			5.8	284.6
S.L			6.9	283.5
+10			13.0	277.4
		3+25		
S.L -40			30.3	260.1
-25			26.0	264.4
-11			22.5	267.9
-1			17.6	272.8
S.L			12.2	278.2
cb			5.7	284.7
1/2			5.3	285.1
$\epsilon$			5.2	285.2
1/2			5.1	285.3



	+	$\pi$ 290.45	-	
cb			5.1	285.3
N.L.			4.3	286.1
		3+00		
N.L.			3.9	286.5
cb			4.9	285.5
1/4			5.2	285.2
E			5.3	285.1
+5			5.5	284.9
1/4			6.0	284.4
cb			8.8	281.6
+4			9.2	281.2
+5			13.3	277.1
S.L.			15.9	274.5
+15			20.3	270.1
+30			29.1	261.3
400			37.4	253.0
+60			40.3	250.1
		3+75		
S.L. -65			46.1	244.3
-50			41.6	248.8
-30			30.5	256.9
-15			26.9	263.5
S.L.			20.8	269.6
cb			15.1	275.3
1/4			12.7	277.7
E			8.4	282.0

	+	$\pi$ 290.45	-	
+5			6.0	284.4
1/4			5.5	284.9
cb			4.9	285.5
N.L.			3.9	286.5
		4+00		
N.L. On Cement wall 0.5 in st.			4.0	286.4
+0.5			4.6	285.8
cb			5.0	285.4
+3			5.1	285.3
1/4			8.3	282.1
E			14.7	275.7
1/4			16.7	273.7
cb			20.1	270.3
S.L.			25.0	265.4
+15			32.1	258.3
+35			40.0	250.0
+60			47.1	243.3
470			49.8	240.6
		4+25		
N.L. On Cement Wall 0.5 in st.			4.2	286.2
+0.5			4.9	285.5
cb			5.5	284.9
+1.5			5.9	284.5
+4			9.3	281.1
1/4			11.7	278.7
E			14.1	276.3



	+	290.45	-	
1/4			16.7	273.7
cb			21.0	269.4
S.L.			26.0	265.4
+15			32.9	257.5
+30			39.0	250.9
+50			46.8	243.6
+70			51.6	238.8

4+00

N.L.			6.3	284.1
+7			7.0	282.9
cb			11.0	278.9
1/4			16.0	273.9
1/4			18.7	271.7
1/4			21.9	268.6
cb			24.8	265.6
S.L.			30.1	260.3
+15			36.5	253.9
+30			42.8	247.6
+70			52.9	237.5

4+75

N.L.			8.3	282.1
cb			13.0	277.4
1/4			16.7	273.7
E			20.2	270.2
1/4			23.4	267.0
cb			27.0	263.4

	+	290.45	-	
S.L.			32.1	258.3
+15			38.1	252.3
+30			43.9	246.5
+70			54.3	236.1

4+76

N.L.			11.7	278.7
------	--	--	------	-------

5+00

-15			22.3	268.1
N.L.			21.5	268.9
cb			20.8	269.6
1/4			19.3	271.1
E			20.6	269.8
1/4			22.2	268.2
cb			25.2	265.2
S.L.			31.3	259.1
+15			37.5	252.9
+30			44.2	246.2
+70			56.2	234.2

# 7.69 288.07

10.07 280.38 Hub 13' Ver  
21 N.L. Cypress  
- 284.96 = Initial 5M

3.11



Sewer in alley Bk 83 E.W. Morse Sub

June 27th 20  
Dannan  
9133  
Northern.

	172	159.33		157.61 Mon N.W. Cor 30 <sup>th</sup> & G
	3.37	153.59	9.11	150.22 Hub SW 3 <sup>th</sup> G
Hub E of alley & W. 7 line 30 <sup>th</sup>			5.58	148.61
0+00 = E Alley & W.C. 20 <sup>th</sup> St.			7.9	145.7
+10			12.0	141.6
#	0.38	141.07	12.90	140.69
+25			2.2	138.9
+38			6.4	134.7
+50			7.7	133.4
#	0.11	128.16	13.02	128.00
1+00			0.9	127.3
1+50			5.6	122.6
1+53			6.1	122.1
2+00			6.9	121.3
2+50			9.3	118.9
#	1.77	120.08	9.85	118.31
2+58			2.2	117.9
3+00			2.7	117.4
3+50			2.6	117.5
#	12.81	131.22	1.67	118.41
4+00			10.5	120.7
4+23 = Flow line Sewer E 29 <sup>th</sup> St			10.92	114.30
#	11.45	142.67	0.00	131.22 Nail.
#	11.76	154.28	0.10	142.52
#	5.44	157.65	0.07	154.21
#			2.07	159.58 = Initial BM

Note: Ele Ground at manhole 126.0

Top M.H. 121.7

Dig down to M.H. under to of dump:

Extension of Sewer Leads E Alley Bk 83 E.W. Morse Sub

30<sup>th</sup> & Broadway 74.84 S.W. B.P.

From E Alley + W.C. 30<sup>th</sup> St to 1.70' East.

BM	1.00	158.61		157.61 N.W. Mon. 30 <sup>th</sup> St
TP	9.55	157.66	10.50	148.11
0+0 = W.C. 30 <sup>th</sup> St & Alley			11.7	146.0
+5			9.6	148.1
+14			9.7	148.0
+17 Gutter			10.7	147.0
+35 E 30 <sup>th</sup> St			10.4	147.3
+66 Gutter			10.3	147.4
+80			9.3	148.4
+90			7.8	150.5
1+00			6.6	151.1
+80			5.5	152.2
+35			3.8	153.9
+70			2.8	154.9
B.M.			0.04	157.68



June 29th 1920  
Donnan  
Bliss  
Northern.

Sewer Cuts 20th & B St.

	+	π	-	
	3.25	98.09		94.84 B.P. SW. 20th & D <sup>st</sup>
	1.45	88.52	11.02	87.07
1400 =				+3.29
	0.48	76.02	12.98	75.54
1400				+3.27
0+0-0				70.00
				-3.70
0+00 = M.H. = ± of 20th St & ± of B St.				66.00
				+5.77
0+00				62.00
				+4.19
1400				60.96
				+3.95
#	9.36	72.37	12.91	63.11
				+2.97
1400				58.88
				+3.38
2+00				57.84
				+4.17
2+40 = M.H. to be constructed on B St. = M.H.				57.00
				+7.25
E.C. 20th & ± of B St. D.E				63.50
#	12.92	85.11	0.20	72.17
#	13.02	97.96	0.17	84.94
			3.15	94.81 = Initial B.M.

88.52  
74.00  
14.52  
11.23  
+3.29

76.02  
70.00  
6.02  
2.70  
+3.27

76.02  
66.00  
10.02  
6.32  
+3.70

76.02  
62.00  
14.02  
8.24  
+5.77

76.02  
60.96  
15.06  
10.87  
+4.19

76.02  
59.92  
16.10  
12.91  
+3.19

72.37  
58.88  
13.46  
10.49  
+2.97

72.37  
63.50  
8.87  
1.62  
+7.25

72.37  
57.84  
14.53  
11.10  
+3.38

72.37  
57.00  
15.37  
11.20  
+4.17



Note:  $\frac{+}{-}$  breaks measured from Cbs or  $\frac{+}{-}$  or P.C.

Xsection of Aloha Place & Chestnut St 30' wide 5' walks

6.90 207.93 2510.3 NW. Hickory St  
Witherby, B.P.  
1.28 248.14 10.17 246.76

31' Southwesterly from  $\pm 00 =$  End of 4' Combination Curb & walk on the Northwesterly side of Aloha Place.

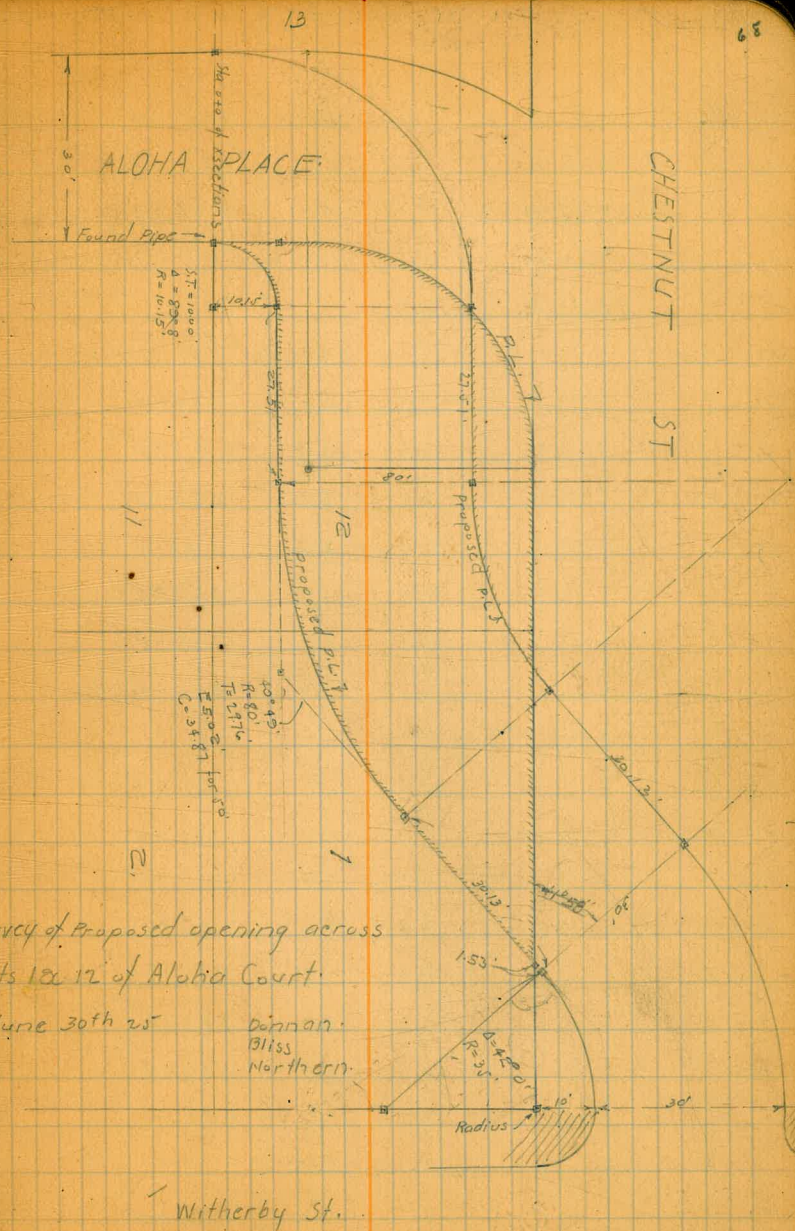
S.E.L.	8.6	239.54
$\pm 00$ Cement Cb	8.60	239.54
Gutter	9.4	238.74
$\frac{+}{-}$	9.2	238.94
Gutter	10.2	237.94
Cement Curb	9.60	238.54
N.W.L.	9.8	238.34

14' Southwesterly from  $\pm 00 =$  End of 4' Combination Curb & walk on the Southeasterly side of Aloha Place.

N.W.L.	9.2	238.94
+3	8.0	240.14
Cb	8.7	239.44
$\frac{+}{-}$	8.8	239.34
Gutter	9.0	239.14
Cement Cb	8.13	240.01
S.E.L.	8.1	240.04

See sketch  $\pm 00 =$  P.C. Curve:  $R = 10.15' \text{ \& } 40.15'$

S.E.L.	7.9	240.24
+3	8.6	239.54
Cb	8.6	239.54
$\frac{+}{-}$	8.9	239.24





	+	π 248.14	-
+7		8.8	239.34
Cb		8.1	240.04
N.W.C. = Break of slope.		9.9	238.24
N.W.C. + 17		21.6	226.54
		Note: Slope continues out very steep	
		Centre of Curve:	
N.L. - 30		23.0	225.14
		Note: Slope continues out very steep	
" - 7		9.5	238.64
N.L.		7.3	240.84
N.L. + 3		8.2	239.94
Cb		8.4	239.74
⊕		8.2	239.94
Cb		8.2	239.94
S.C.		7.7	240.44
		End of Curve:	
S.C.		6.7	241.44
Cb		7.1	241.04
⊕		7.4	240.74
Cb		7.2	240.94
N.L.		7.2	240.94
+3		6.2	241.94
+5		6.7	241.44
+30		29.1	219.04
		See sketch PC Curve: R = 50' @ 80'	
N.L. - 29		25.3	222.84
N.C. = Break of slope.		5.8	242.34
N.L. + 15		5.0	243.14

	+	π 248.14	-
Cb		6.2	241.94
⊕		6.1	242.04
⊕ + 5		5.7	242.44
Cb		4.9	243.24
S.C.		4.5	243.64
		Centre of Curve	
S.C.		3.3	244.84
Cb		4.0	244.14
⊕		4.4	243.74
Cb		4.3	.84
N.L. Break of slope.		3.3	
N.L. + 30		23.4	
		E.C.	
N.L. - 24		17.0	
N.L. = Break of slope.		2.7	
+3		1.4	
Cb		1.6	
+3		2.7	
⊕		2.5	
Cb		1.9	
S.C.		1.4	
#	906	254.84	1.38 246.76
		PC. Radius = 35' @ 65'	
S.C.		6.1	
Cb		6.2	
⊕		6.6	



cb	6.5
H.L. = Break of slope.	5.9
+9	10.4
+12	7.3
Centre of Curve	
N.L. - 4	5.2
N.L.	6.0
cb	5.3
cb + 3	4.4
⊕	4.9
cb	4.5
S.L.	4.3

W.L. Witherby St. paved.

S.L. on Curb Return.	2.82
Gutter <sup>of 50' st.</sup> Pavement	3.59
cb	3.34
⊕	3.13
cb	3.35
Gutter of 50' st	3.54
N.L. = cb for 50' st.	2.89
#	4.79

251.05 = Initial B.M.



Cross Section Treat St

From East Line 27th St 100'E

Width 54

CBs 10

9/5 8.5

192.37

12.34

192.37

180.01

S.W.C.P.

E+27th St

E.L. 27th St

S	103	176.1 ✓
CB	159	176.5 ✓
2	155	176.9 ✓
2	156	176.8 ✓
1/4	154	77.0 ✓
CB	146	77.8 ✓
N	143	78.1 ✓
	C'E	
-6	57	86.7 ✓
N	135	78.9 ✓
CB	144	78.0 ✓
1/4	147	77.7 ✓
2	152	77.2 ✓
1/4	155	76.9 ✓
CB	159	76.5 ✓
S	161	76.3 ✓
7.6	75	84.9 ✓
	25'E	
-6	61	86.3 ✓
-5	148	77.6 ✓
S	148	77.6 ✓
CB	151	77.3 ✓
1/4	148	77.6 ✓

2	146	77.8 ✓
1/4	141	78.3 ✓
CB	145	77.9 ✓
+5	142	78.2 ✓
N	116	80.8 ✓
+6	4.5	87.9 ✓
	44'E	
-6	41	88.3 ✓
N	10.0	82.4 ✓
+5	13.3	79.1 ✓
CB	137	78.7 ✓
1/4	138	78.6 ✓
2	139	78.5 ✓
1/4	145	77.9 ✓
CB	145	77.9 ✓
S	145	77.9 ✓
+5	47	87.7 ✓
	50'E	
-1	4.5	87.9 ✓
S	5.4	87.0 ✓
+5	147	77.7 ✓
CB	147	77.7 ✓
1/4	143	78.1 ✓
2	13.9	78.5 ✓
1/4	13.7	79.0 ✓
CB	13.7	78.7 ✓



Treat St

192.37

44		18.7	78.7 ✓
N		19.9	81.5 ✓
+2		38	88.6 ✓
	55°E		
-3		3.9	88.5 ✓
N		11.6	80.8 ✓
+6		13.8	78.6 ✓
CB		13.2	79.2 ✓
1/4		12.9	79.5 ✓
2.0		13.0	79.4 ✓
+2		13.0	79.4 ✓
+4		14.2	78.2 ✓
1/4		14.4	78.0 ✓
CB		14.7	77.7 ✓
+5		14.5	77.9 ✓
S		4.4	88.0 ✓
	62°E		
-3		4.4	88.0 ✓
S		9.3	83.1 ✓
CB		11.9	80.5 ✓
1/4		13.4	79.0 ✓
2		12.0	80.4 ✓
1/4		12.1	80.3 ✓
CB		12.4	80.0 ✓
+4		13.4	79.0 ✓

192.37

72

N		10.3	82.1 ✓
+3		4.1	88.3 ✓
	70°E		
-3		4.1	88.3 ✓
N		11.3	81.1 ✓
+6		12.6	79.8 ✓
CB		11.2	81.2 ✓
1/4		10.6	81.8 ✓
2		10.7	81.7 ✓
+4		11.2	81.2 ✓
1/4		9.7	82.7 ✓
CB		10.1	82.3 ✓
+7		8.0	84.4 ✓
3		4.2	88.2 ✓
	75°E		
S		4.2	88.1 ✓
CB		4.2	88.2 ✓
1/4		4.1	88.3 ✓
+4		10.0	82.4 ✓
2		9.8	82.6 ✓
1/4		10.1	82.3 ✓
CB		10.4	82.0 ✓
+5		10.4	82.0 ✓
N		4.2	88.2 ✓
	90°E		
N		4.9	87.5 ✓



Treat St.

13

OB		47	87.7 ✓
+4		67	85.7 ✓
1/4		71	85.3 ✓
2		69	85.5 ✓
+3		64	86.0 ✓
+5		47	87.7 ✓
1/4		48	87.6 ✓
OB		45	87.9 ✓
S		44	87.8 ✓
	100° E		
S		48	87.6 ✓
OB		47	87.5 ✓
1/4		51	87.3 ✓
2		59	86.5 ✓
1/4		59	86.5 ✓
OB		55	86.9 ✓
N		51	87.3 ✓



12/5/25  
Moore

FIR ST. XSEX:  
FERN TO GROVE

40' wide  
6' dia  
7 1/4's

264.03

74

SEBP	0.77	270.24	269.47
T. P. ON RAIN	4.03	264.03	10.24
EL FERN = 0+00			<u>264.0</u>
N on cen. NE edge of s/w		3.81	260.23
cb v v cb		4.03	260.00
gut on paving		4.49	259.55
1/4 v v		4.47	259.57
e v v		4.58	259.46
1/4 v v		4.88	259.16
gut v v		5.38	258.86
cb on cement		5.07	258.97
S v v		4.82	259.22
	25' E		
S		5.8	258.2
cb		5.8	258.2
1/4		5.7	258.3
c		5.2	258.8
1/4		5.1	258.9
gut		5.0	259.0
cb on cement		4.29	259.7
N v v		4.10	259.9
	50' E		
N on cen		4.42	259.6
cb on cement in driveway		4.88	259.1
gut		5.0	259.0
1/4		5.4	258.6

Grape + Fern	C	5.5	<del>264.0</del> 258.5
	1/4	5.5	258.5
	cb	5.8	258.2
+3 = Wedge of Evergreen hedge		5.9	258.1
	S	6.0	258.0
			75' E = E cen walk 4.17 wide
	S	5.7	258.3
+3.5 edge of		5.72	258.3
	cb	5.7	258.3
	1/4	5.5	258.5
	c	5.7	258.3
	1/4	5.6	258.4
	gut	5.5	258.5
	cb on cement	4.81	259.2
	N v v	4.66	259.3
			97' E = E edge of Evergreen hedge
	N on cen	4.92	259.1
	cb v v cb	5.06	258.9
	gut	5.5	258.5
	1/4	5.9	258.1
	c	5.9	258.1
	1/4	5.6	258.4
	cb	6.0	258.0
	+3 hedge	6.3	257.7
	S hedge angles S to SL	6.3	257.7



264.03

111'E = E end of contiguous <sup>264.0</sup> s/c

s	6.4	257.6
ct	6.5	257.5
1/4	6.5	257.5
c	6.2	257.8
1/4	6.2	257.8
got	5.7	258.3
ct on cement	5.2	258.8
N. v. w edge of walk	4.88	259.1

123'E

N	6.2	257.8
ct	6.7	257.8
1/4	7.1	256.9
c	7.2	256.6
1/4	7.8	256.2
ct	7.9	256.1
J	8.0	256.0

146'E

s	10.1	253.9
ct	10.7	253.3
1/4	10.0	254.0
c	9.8	254.2
1/4	9.4	254.6
ct	8.7	255.3
N = 4 Pepper tree	6.8	257.2 24" diam.
T.P. 062 ~ 254.04	10.61	253.42

254.04

FIR ST 75

146'E

N	0.5	254.0	253.5
ct	0.7	253.3	
1/4	0.8	253.2	
c	0.5	253.5	
+3	1.2	252.8	
1/4	0.9	253.1	
ct	2.1	251.9	
S	1.6	252.4	

156'E

-10	4.5	249.5
S	5.3	248.7
ct	5.3	248.7
1/4	3.9	250.1
+5	3.2	250.8
c	3.3	250.7
+3	3.4	250.6
1/4	2.3	251.7
ct	1.5	252.5
N	1.6	252.4

171'E

-1	4.2	249.6
N	4.4	249.6
+0.5	7.1	246.9
ct	7.9	246.1
+4	7.1	246.9
1/4	7.5	246.5



25404

			254.0
+5		8.0	246.0
c		8.8	245.2
1/4		9.1	244.9
cb		9.0	245.0
S		9.3	244.7
+10		9.7	244.3
	181'E		
-10		12.0	242.0
S		11.8	242.2
+4		11.6	242.4
+5		10.6	243.4
cb		10.6	243.4
1/4		10.6	243.4
c		9.9	244.1
1/4		9.7	244.3
cb		8.9	245.1
+5	Eucalyptus 30" diam	8.6	245.4
✓		8.7	245.3
+10		9.0	245.0
T.P.	0.43	241.80	1267
	195'E		241.8
→ -1.4 = 4'E of center of dwelling		2.0	239.8
✓		2.0	239.8
+0.8 Eucalyptus 30" diam		2.0	239.8
cb		1.9	239.9
1/4		2.7	239.1

24180

			FIR	ST	76
			241.8		
c		3.2	238.6		
1/4		3.7	238.1		
cb		3.9	237.9		
S = edge of porch to dwelling		4.0	237.8		1.5 above = Floor EIV center of main portion of dwelling
	223.40 = W.L. Grove	ST			
-10		16.7	225.1		
S		16.8	225.0		
cb		16.0	225.8		
1/4		15.7	226.1		
c		15.1	226.7		
1/4		14.3	227.5		
cb		13.8	228.0		
N		12.3	229.5		
1/4 +0.1 = center of dwelling = edge of porch to dwelling		12.4	229.6		5' above = Floor EIV
T.P.	12.65	254.02	0.53	241.37	
T.P.	9.59	263.02	0.59	253.43	
T.P.	11.71	271.89	2.34	260.68	
T.P.	3.06	272.64	2.31	269.58	
about to BM. Grape + Fern			31.6	269.48	269.47



Relocation Mission Valley Line  
from sta 52+55 to 53+84 Book 1109 P. 53

10/11/26  
Miller

10.26 55 2000 R 92-14 7  
4.00  
14.26 10.26

73.90

77

Station	Grade	Grade	Grade
52+55 BM. Hub A 3°22' R 0° 73.90		72.98	67.06
+60	1.7	72.2	
+88	1.4	72.5	
53+00	2.0	71.9	
+06	1.4	72.5	
+22	3.0	70.9	
53+32 A 13°38' L	5.92	67.98	60.83
+40	5.6	68.3	
+62	8.0	65.9	
+87	6.4	67.5	
54+00	7.8	66.1	60.63
+45	9.0	64.9	
+65	8.3	65.6	
+91 Wash	10.9	63.0	
+95	10.0	63.9	
55+00	10.8	63.1	60.33
+15	10.0	63.3	
55+25 A 87°45' R	10.12	63.78	62.78
+35	12.4	61.5	
+43	12.4	61.5	
+45	13.8	60.1	
+53	13.9	60.0	60.17
+54	12.8	61.1	
+75	9.6	64.3	
55+85 A 77°23' R	7.98	65.92	60.07

Station	Grade	Grade	Grade
56+00	7.4	66.5	60.03
+10	7.5	66.4	
+40	9.7	64.2	
+65	10.1	63.8	
57+00	8.5	65.4	59.73
+15	7.1	66.8	
+40	9.4	64.1	
+65	9.2	64.7	
+90	10.8	63.1	
58+00	10.6	63.3	59.43
58+04.20 A 20°00' R	10.31	63.59	
+27	10.0	63.9	
+45	8.8	65.1	
+65	6.9	67.0	
58+79.40 A 72°14' R to A 52+55 = 53+84.0 A Book 1109 P. 53	7.28	66.6	59.19

This hub replaced

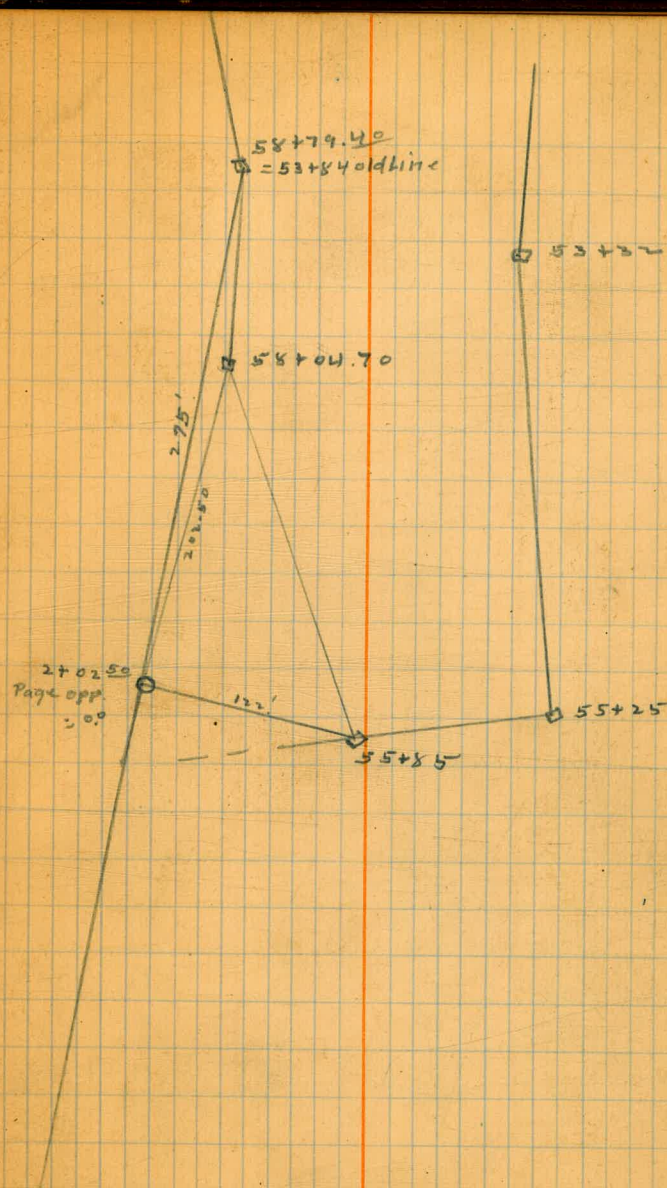


Relocation from Sta 58+04.25 Page 77

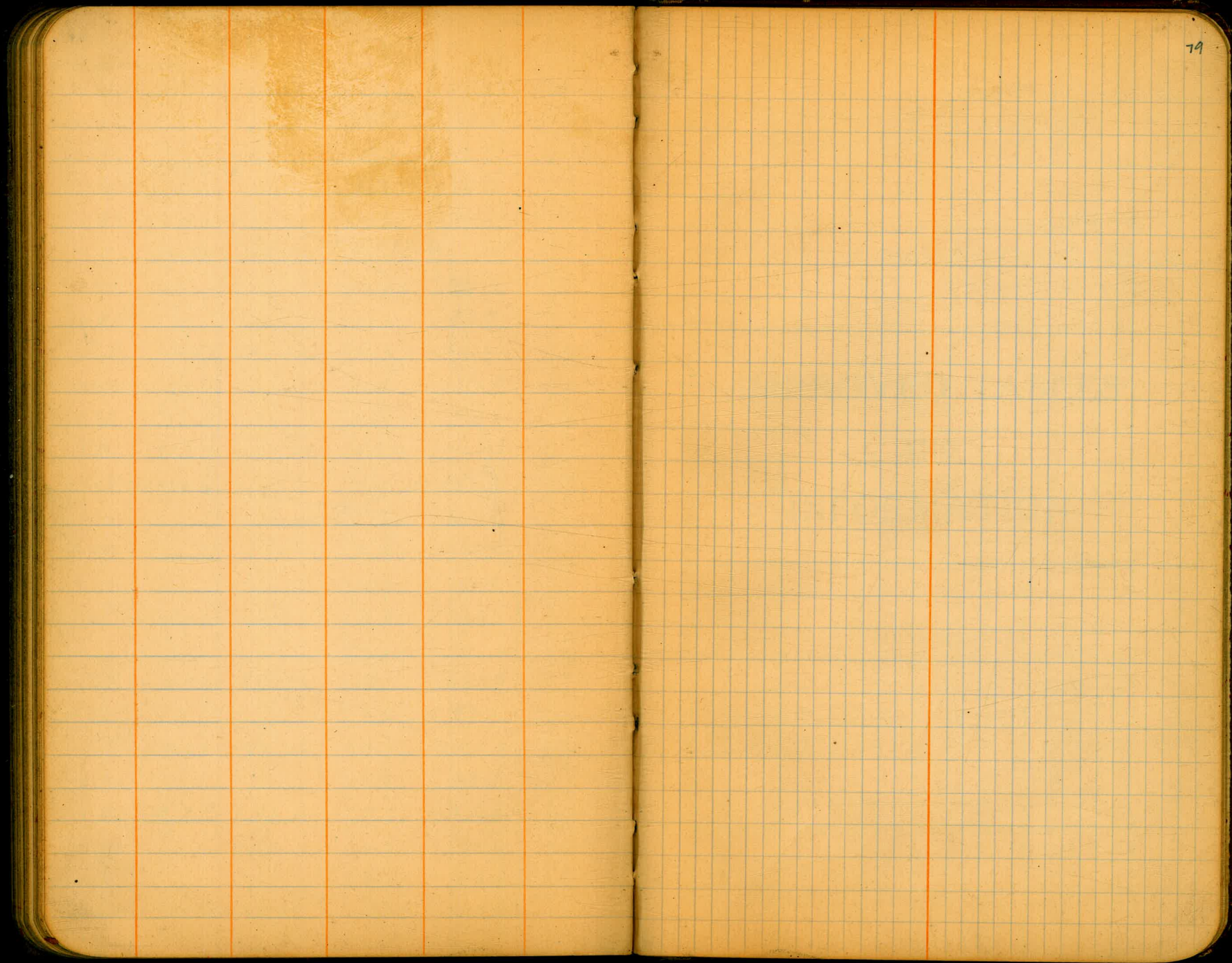
South R

58+04.25A Page 77

00:1 B.M.	13.25	76.84	63.59	Hub
0+05		12.6	64.2	
0+30		5.7	71.1	
+40		3.6	73.2	
+50		2.0	74.8	
T.P.	12.30	88.92	0.22	76.62
+60		10.7	78.2	
+85		1.0	87.9	
T.P.	12.50	101.12	0.30	88.62
+100		11.1	90.0	
+30		3.1	98.0	
T.P.	10.60	111.42	0.30	100.82
+50		8.6	102.8	
+60		7.6	103.8	
+80		3.5	107.9	
+90		3.6	107.8	
(2+2 <sup>50</sup> + 0 - 500)		1.8	109.6	P.O.T.
T.P.	0.40	98.72	13.1	98.32
+30		2.6	96.1	
T.P.	0.40	86.02	13.1	85.62
+70		6.3	79.7	
+90 T.R.	1.0	74.32	12.7	73.32
+95		1.7	72.6	
+105		5.1	69.2	
1 in 2 Hub 55+85A Page 77		8.40	65.92	







79



Geo. Northern  
Voltaire St.  
Ocean Beach-

W. F. Bliss  
4836 Del Monte Ave  
Ocean Beach

DIRECTIONS FOR USE OF TABLES

228.33  
06  
227.27

TABLE No. 1.

Distance of slope stake from side or shoulder  
stake for any width roadway, slope 1% to 10%  
If ground is nearly level, the cut or fill at side  
stake is located by the double entry method in

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Tangent and External for curve of  
any other degree, divide by degree of curve and  
add correction found in column of corrections.  
Degree of curve with a given  $L$  may be found  
by dividing tangent (or external), opposite  $L$  by  
given tangent (or external).

The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the radius.



TABLE VI (continued)  
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	sec
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	2.349	790	2.423	808	2.497	826	2.572	844	2.647	862	2.723	38
52	880	2.799	898	2.876	916	2.954	934	3.032	951	3.111	969	3.190	37
53	986	3.270	8004	3.351	8021	3.432	8039	3.514	8056	3.597	8073	3.680	36
54	8090	3.764	107	3.848	124	3.934	141	4.019	158	4.106	175	4.193	35
55	192	4.281	208	4.370	225	4.460	241	4.550	258	4.641	274	4.733	34
56	290	4.826	307	4.919	323	5.013	339	5.108	355	5.204	371	5.301	33
57	387	5.399	403	5.497	418	5.597	434	5.697	450	5.798	465	5.900	32
58	480	6.003	496	6.107	511	6.212	526	6.319	542	6.426	557	6.534	31
59	572	6.643	587	6.753	601	6.864	615	6.977	631	7.090	646	7.205	30
60	660	1.7321	3675	1.7437	3689	1.7556	3704	1.7675	3718	1.7797	3732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	1.445	075	1.609	088	1.775	100	.1943	112	.2113	124	.2286	24
66	135	2.460	147	2.637	159	2.817	171	.2998	182	3.183	194	3.369	23
67	205	3.559	216	3.750	228	3.945	239	.4142	250	4.342	261	4.545	22
68	272	4.751	283	4.960	293	5.172	304	.5386	315	5.605	325	5.826	21
69	336	6.051	346	6.279	356	6.511	367	.6746	377	6.985	387	7.228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	3.2041	555	3.2371	17
73	563	3.2709	572	3.3052	580	3.3402	588	3.3759	596	3.4124	605	3.4495	16
74	613	4.874	621	5.261	628	5.656	636	6.059	644	6.470	652	6.891	15
75	659	7.321	667	7.760	674	8.208	681	8.657	689	9.136	696	9.617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	3.315	750	3.397	757	3.484	763	3.570	769	3.658	775	3.748	12
78	781	7.046	787	7.729	793	8.430	799	9.152	805	9.894	811	10.658	11
79	816	1.446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	5.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	6.8269	899	6.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.031	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.53	1.000	171.88	1.000	343.77	0
deg.	cos 60'	cot 60'	cos 50'	cot 50'	cos 40'	cot 40'	cos 30'	cot 30'	cos 20'	cot 20'	cos 10'	cot 10'	deg.

TABLE VII  
RODS IN FEET AND INCHES

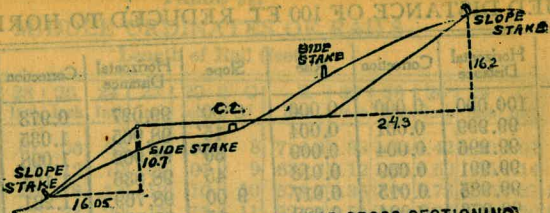
Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII  
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84



INCLINATION OF 100 FT. REDUCED TO HORIZONTAL



**DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.**

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

C  
0-1  
0-2  
0-4  
1-0  
1-20  
1-40  
2-0  
2-20  
2-40  
3-0  
3-20  
3-40  
4-0  
4-20  
4-40  
5  
6  
7

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

To find

68  
03  
204

Huter - 1bis 270.60  
" Hawk 268.50

61.06 77.  
23 .03  
60.83 76.31

61.88

188.24  
12

45  
32  
77

10.6  
63.3

13.3  
60.6

74.7  
4.7  
79.4

58.79  
52.55  
6.24  
3  
1472  
61.06  
187  
59.19

130  
609

60.33

85  
255

79.4  
2382



190 20

19.1  
9.5  
9.6

12.7  
11.6

2.9  
2.0  
4.9

88° 12  
176 28

362  
487  
79

548  
669  
1217

14 104  
119.2  
824

11.14  
0.90  
11.90  
8.08  
28.8

18+24  
1+76  
20+20  
20.55

35.5  
36

8.24  
7.7  
10.92

26.8  
48.7  
75.5

4.18  
1.40  
5.58

12.79

6.7  
5 W 30<sup>th</sup> Markat. Spt. 142.51  
NW 30<sup>th</sup> + G BP. 157.06

271.21  
12.97  
258.22

27.8  
140  
418

121+32

1121  
17  
12.311

5+68  
18.2  
8.67

8+17.1  
8.361

337.6  
89.7  
427.3

95.15  
28  
67

427.3  
113  
416.0

16.72  
5.58  
11.74

38  
14  
59

169

94  
17  
78

3+449  
276  
372 J-ER

140

5 57.45

214.81

218.37  
3.33  
215.04

11.44  
5.1

11.14  
5.58  
16.72  
110  
65  
45

169.00  
25.25  
197.25

218.10  
12.79  
205.31  
9.39  
205.70  
10.76  
195.28 of 7 line

255 = N.E. Co Logan

290 = C.L. Track

3068 = C.L. "

3+449 = 2' M of old M.H.

3+905 = Int 16th St line

318

62.67

600  
250  
350  
780  
700  
566  
236

124  
479

19.0  
12.1  
31.1

87.2  
38.6  
127.8

26+813  
204206  
6.607

N

278  
45  
323

359.60  
244.38  
115.22

218.10  
3.33  
214.77

214.81  
3.33  
218.14  
7.08  
211.06  
288.79  
202.27

202.58  
202.24  
.51

38

308  
37

5 57° 40  
11 5 20