

1125

PASTS

FIELD BOOK

No. 385 F.

MICROFILMED

DEC 21 1964

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.
92 FIFTH ST. 79 NEW MONTGOMERY ST.
PORTLAND, ORE. SAN FRANCISCO, CAL.

AGENTS FOR
"BERGER" TRANSITS and LEVELS
"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS
"CHICAGO" STEEL TAPES, etc.

Cross Section of Albatross
Palm to Olive

20' wide
14' s/w

2.04 216.80 ✓

8.4 Palm

		7.6	209.2 ✓
W		4.5	212.3 ✓
+5		3.3	213.5 ✓
cb		2.6	214.2 ✓
1/2		2.1	214.7 ✓
✓ e		2.3	214.5 ✓
1/4		1.9	214.9 ✓
cb		1.6	215.2 ✓
E			
	7' S		
E		1.7	215.1 ✓
cb		1.9	214.9 ✓
1/2		2.3	214.5 ✓
✓ e		2.4	214.4 ✓
1/2		2.7	214.7 ✓
cb		3.4	213.4 ✓
W		5.1	211.7 ✓
	25' S		
W		4.8	212.0 ✓
cb		3.8	213.0 ✓
1/2		3.0	213.8 ✓
✓ e		2.7	214.1 ✓
1/2		2.8	214.0 ✓
cb		2.2	214.6 ✓

216.80

E

1.9

214.9 ✓

50' S

E		2.5	214.3 ✓
cb		3.0	213.8 ✓
✓ 1/2		3.5	213.3 ✓
e		3.4	213.4 ✓
1/2		3.7	213.1 ✓
cb		4.5	212.3 ✓
W		5.3	211.5 ✓

75' S

W		6.2	210.6 ✓
cb		5.2	211.2 ✓
✓ 1/2		4.5	212.3 ✓
e		4.2	212.6 ✓
1/2		4.1	212.7 ✓
cb		4.0	212.8 ✓
E		3.3	213.5 ✓

100' S

E		4.4	212.4 ✓
cb		4.6	212.2 ✓
1/2		5.4	211.4 ✓
✓ e		5.5	211.3 ✓
1/2		5.6	211.2 ✓
cb		6.2	210.6 ✓
W		7.5	209.3 ✓

110' S on EL & Garage

4.6

212.18 Con. floor

2-16-80

125' S				
W		8.9	207.9	✓
cb		7.8	209.0	✓
1/4		7.1	209.7	✓
✓ c		7.0	209.8	✓
1/4		6.8	210.0	✓
cb		6.0	210.8	✓
E		4.9	211.9	✓
150' S				
E		6.3	210.5	✓
cb		7.2	209.6	✓
1/4		8.1	208.7	✓
✓ c		8.4	208.4	✓
1/4		8.8	208.0	✓
cb		9.7	207.1	✓
W		9.7	207.1	✓
175' S				
W		10.0	206.8	✓
cb		10.4	206.4	✓
1/4		9.5	207.3	✓
✓ c		9.0	207.8	✓
1/4		8.8	208.0	✓
cb	on slope of 3' corr. walk	8.0	208.8	✓
E		7.5	209.3	✓
200' S				
E		7.9	208.9	✓

2-16-80

Albatross

cb		8.6	208.2	✓
1/4		9.1	207.7	✓
c		9.2	207.6	✓
1/4		9.6	207.2	✓
cb		9.8	207.0	✓
W		10.6	206.2	✓
225' S				
W		9.7	207.1	✓
cb		9.4	207.4	✓
1/4		9.2	207.6	✓
✓ c		9.6	207.2	✓
1/4		9.5	207.3	✓
cb		9.5	207.3	✓
E		9.3	207.5	✓
250' S				
E		12.1	204.7	✓
cb		10.3	206.5	✓
1/4		10.1	206.7	✓
✓ c		9.7	207.1	✓
1/4		9.6	207.2	✓
cb		8.9	207.9	✓
W		9.2	207.6	✓
275' S				
W		10.0	206.8	✓
cb		9.9	206.9	✓
1/4		10.4	206.9	✓

216.80

✓c		10.6	206.2	✓
1/4		10.8	206.0	✓
cb		11.6	205.2	✓
E		12.5	204.3	✓
T.P.	0.19	206.46	10.53	206.27 ✓
	300° S = NL + Olive			
E		12.0	194.5	✓
+d		7.8	198.7	✓
+8		4.9	201.6	✓
✓cb		3.0	203.5	✓
1/4		1.7	204.8	✓
c		1.5	205.0	✓
1/4		0.9	205.6	✓
cb		0.9	205.6	✓
w		0.7	205.8	✓
Olive = 14 dts 13 1/4's	Ncb.			
w		1.1	205.4	✓
cb		1.1	205.4	✓
1/4		1.7	204.8	✓
✓c		2.3	204.2	✓
1/4		3.8	202.7	✓
+6		4.4	202.1	✓
cb		7.8	198.7	✓
E		13.8	192.7	✓
	N 1/4			
E		21.1	185.4	✓

206.46

Albatross

3

cb		14.4	192.1	✓
+v		12.5	194.0	✓
1/4		6.5	200.0	✓
+4		4.5	202.0	✓
✓c		3.3	203.2	✓
1/4		2.0	204.5	✓
cb		1.5	205.0	✓
w		1.6	204.9	✓
	center olive			
w		1.9	204.6	✓
cb		1.8	204.7	✓
1/4		2.5	204.0	✓
✓c on Max.		4.80	201.66	✓
+5		5.8	200.7	✓
1/4		10.4	196.1	✓
cb		20.1	186.4	✓
E		25.3	181.2	✓
	S 1/4			
E		32.2	174.3	✓
cb		27.0	179.5	✓
1/4		20.1	186.4	✓
✓c		7.2	199.3	✓
1/4		3.9	202.6	✓
cb		2.5	204.0	✓
w		2.1	204.4	✓

20646

S db

w	2.5	204.0 ✓
cb	3.0	203.5 ✓
1/2	5.2	201.3 ✓
+7	7.3	199.2 ✓
✓c	10.6	195.9 ✓
1/4	25.1	181.4 ✓
cb	31.8	174.7 ✓
E	37.5	169.0 ✓

SL Olive

E	44.5	162.0 ✓
cb	36.0	170.5 ✓
1/2	27.1	179.4 ✓
c	17.6	188.9 ✓
1/4	7.9	198.6 ✓
cb	4.0	202.5 ✓
w	3.1	203.4 ✓

Cross Section of Olive 80' wide
Albatross to BRANT. 14' s/w #

206.46

WL Albatross = 0100

g	3.1	203.4 ✓
cb	2.5	204.0 ✓
1/4	2.1	204.4 ✓
e	1.9	204.6 ✓
1/4	1.6	204.9 ✓
cb	1.1	205.4 ✓
w	0.7	205.8 ✓

25' w

w	1.7	204.8 ✓
cb	2.1	204.4 ✓
1/4	2.1	204.4 ✓
c	2.4	204.1 ✓
1/4	2.5	204.0 ✓
cb	2.9	203.6 ✓
S	3.5	203.0 ✓

50' w

S	4.3	202.2 ✓
cb	4.0	202.5 ✓
1/2	3.7	202.8 ✓
c	3.4	203.1 ✓
1/4	3.3	203.2 ✓
cb	2.8	203.7 ✓
w	2.1	203.8 ✓

20646

75' W

N	4.4	202.1 ✓
cb	4.2	202.3 ✓
1/4	5.5	201.0 ✓
+3	4.5	202.0 ✓
C	4.8	201.7 ✓
1/4	5.1	201.4 ✓
cb	5.4	201.1 ✓
S	5.7	200.8 ✓

100' W

S	7.6	198.9 ✓
cb	7.4	199.1 ✓
1/4	7.0	199.5 ✓
C	6.9	199.6 ✓
+6	7.9	198.6 ✓
1/4	7.4	199.1 ✓
cb	7.0	199.5 ✓
N	6.7	199.8 ✓

115' W

N	8.1	198.4 ✓
cb	8.2	198.3 ✓
1/4	8.5	198.0 ✓
C	9.1	197.4 ✓
+3	8.5	198.0 ✓
1/4	8.3	198.2 ✓
d	8.4	198.1 ✓
S	8.5	198.0 ✓

20646

Olive

125' W

S	9.0	197.5 ✓
cb	9.3	197.2 ✓
1/4	9.1	197.4 ✓
+5	9.2	197.3 ✓
+6	9.8	196.7 ✓
C	10.2	196.3 ✓
1/4	9.3	197.2 ✓
cb	9.3	197.2 ✓
N	11.5	195.0 ✓

150' W

N	21.7	184.8 ✓
cb	19.0	187.5 ✓
1/4	16.4	190.1 ✓
+7	14.3	192.2 ✓
C	12.0	194.5 ✓
+10	12.5	194.0 ✓
1/4	12.0	194.5 ✓
+5	11.2	195.3 ✓
cb	10.9	195.6 ✓
S	10.6	195.9 ✓

175' W

S	12.3	194.2 ✓	
cb	13.2	193.3 ✓	
T.P. 0.18	193.54 ✓	13.10	193.36 ✓
+6	0.8	192.7 ✓	

19354

1/4	2.0	191.5 ✓	
+4	2.0	191.5 ✓	
+7	1.4	192.1 ✓	
C	5.0	188.5 ✓	
1/4	9.6	183.9 ✓	
cb	12.2	181.3 ✓	
N	16.0	177.5 ✓	
200' W = EL of Brant			
N	23.2	170.3 ✓ 10' SW	
cb	19.5	174.0 ✓ 15' 1/2 S	
1/4	14.0	179.5 ✓	
C	9.2	184.1 ✓	
1/4	3.7	189.8 ✓	
+6	4.5	189.0 ✓	
cb	4.9	188.6 ✓	
+3	2.5	191.0 ✓	
S	1.5	192.0 ✓	
Ect			
S	3.3	190.2 ✓	
+5	3.8	189.7 ✓	
+7	5.9	187.6 ✓	
cb	5.6	187.9 ✓	
+9	4.9	188.6 ✓	
1/4	6.5	187.0 ✓	
+3	8.6	184.9 ✓	
C	11.8	181.7 ✓	

193.54

Olive

6

1/4	17.0	176.5 ✓	
cb	21.7	171.8 ✓	
+7	23.8	169.7 ✓	
N	26.9	166.6 ✓	
+4			
N	28.9	164.6 ✓	
+7	24.4	169.1 ✓	
cb	22.6	170.9 ✓	
1/4	18.0	175.5 ✓	
C	12.6	180.9 ✓	
+10	9.6	183.9 ✓	
1/4	7.9	185.6 ✓	
+5	5.3	188.2 ✓	
cb	5.5	188.0 ✓	
+11	6.2	187.3 ✓	
S	4.0	189.5 ✓	
+7			
S	6.4	187.1 ✓	
+10	5.9	187.6 ✓	
cb	5.5	188.0 ✓	
+5	5.7	187.8 ✓	
1/4	9.6	183.9 ✓	
C	13.1	180.4 ✓	
1/4	18.5	175.0 ✓	
cb	23.0	170.5 ✓	
N	29.6	163.9 ✓	

19354

E 1/4

N	30.8	162.7	✓
cb	25.6	167.9	✓
1/4	20.0	173.5	✓
c	13.8	179.7	✓
1/4	10.8	182.7	✓
+9	6.9	186.6	✓
cb	5.9	187.6	✓
+9	6.0	187.5	✓
S	6.5	187.0	✓

Center

S	6.8	186.7	✓
+7	7.5	186.0	✓
cb	10.3	183.2	✓
1/4	12.9	180.6	✓
c	17.6	175.9	✓
+3	18.2	175.3	✓
+5	22.4	171.1	✓
1/4	23.4	170.1	✓
+7	24.8	168.7	✓
cb	28.2	165.3	✓
N	33.0	160.5	✓

+8

N	34.8	158.7	✓
cb	29.6	163.9	✓
+8	26.1	167.4	✓

19354

Olive

1/4	23.1	170.4	✓
+3	21.5	172.0	✓
c	21.7	171.8	✓
1/4	20.8	172.7	✓
cb	19.7	173.8	✓
+5	19.2	174.3	✓
S	10.4	183.1	✓
	+10		
S	17.1	176.4	✓
cb	19.2	174.3	✓
1/4	21.0	172.5	✓
c	21.7	171.8	✓
+10	21.6	171.9	✓
1/4	23.0	170.5	✓
+4	27.0	166.5	✓
cb	30.2	163.1	✓
N	36.0	157.5	✓
	W 1/2		
N	36.4	157.9	✓
cb	31.1	162.4	✓
+7	27.9	165.6	✓
1/4	27.9	170.6	✓
+3	21.6	171.9	✓
c	21.8	171.7	✓
1/4	21.0	172.5	✓
cb	19.1	174.4	✓
S	16.7	176.8	✓

19354

wcb

N	S	15.6	177.9	✓
cb	cb	18.9	174.6	✓
+9	+9	25.5	168.0	✓
1/4	1/4	23.5	170.0	✓
+3	+3	22.1	171.4	✓
C	C	23.3	170.2	✓
+6	+6	23.0	170.5	✓
1/4	1/4	25.5	168.0	✓
+6	+6	30.8	162.7	✓
cb	cb	34.0	159.5	✓
N	N	38.8	154.7	✓
+7				
N	N	41.0	152.5	✓
cb	cb	35.8	157.7	✓
1/4	1/4	30.4	163.1	✓
+9	+9	24.7	169.4	✓
e	e	24.5	169.0	✓
1/4	1/4	25.0	168.5	✓
+4	+4	27.1	166.4	✓
cb	cb	27.4	166.1	✓
+6	+6	27.2	166.3	✓
S	S	20.3	173.2	✓
+10				
S	S	27.5	166.0	✓
cb	cb	27.4	166.1	✓

Olive

8

+9	27.1	166.4	✓
1/4	25.2	168.3	✓
C	24.8	168.7	✓
+3	24.5	169.0	✓
1/4	30.3	163.2	✓
cb	35.6	157.9	✓
N	40.7	152.8	✓

wL of BRANT

N	41.3	152.2	✓
cb	37.0	156.5	✓
1/4	32.5	161.0	✓
C	25.3	168.2	✓
1/4	26.2	167.3	✓
cb	27.4	166.1	✓
S	27.5	166.0	✓

2/19/25

Gregory X

Section of BRANT ST
from S.L. of Olive to Nutmeg

193.54 H.D. from last page.

S.L. Olive

E	1.5	192.0 ✓
cb	3.3	190.2 ✓
+4	4.0	189.5 ✓
+7	6.4	187.1 ✓
1/4	6.5	187.0 ✓
C	6.8	186.7 ✓
+8	10.4	183.1 ✓
+10	17.1	176.4 ✓
1/4	16.7	176.8 ✓
cb	15.6	177.9 ✓
+7	20.3	173.2 ✓
+10	27.5	166.0 ✓
W	27.5	166.0 ✓
25' 5"		
W	28.0	165.5 ✓
+1	28.0	165.5 ✓
+3	17.8	175.7 ✓
F5	16.6	176.9 ✓
+8	16.0	177.5 ✓
+10	14.5	179.0 ✓
cb	12.6	180.9 ✓
+3	13.3	180.2 ✓
1/4	9.7	183.8 ✓

280
23.0

+5	7.4	186.1 ✓
C	7.0	186.5 ✓
+9	6.9	186.6 ✓
+11	4.9	188.6 ✓
1/4	4.4	189.1 ✓
+2	3.3	190.2 ✓
cb	3.7	190.8 ✓
E	1.4	192.1 ✓
53' 5"		
E	1.4	192.1 ✓
cb	2.7	190.8 ✓
+11	3.2	190.3 ✓
1/4	4.3	189.2 ✓
+8	6.6	186.9 ✓
C	7.2	186.3 ✓
1/4	7.8	185.7 ✓
+4	11.5	182.0 ✓
cb	11.3	182.2 ✓
+6	13.8	179.7 ✓
+10	14.6	178.9 ✓
+13	17.5	176.0 ✓
W	27.6	165.9 ✓
54' 5"		
W	17.5	176.0 ✓
+2	17.4	176.1 ✓
+4	14.6	178.9 ✓

193.54

+8	13.8	179.7 ✓
cb	11.3	182.2 ✓
+9	11.5	182.0 ✓
1/4	7.8	185.7 ✓
c	7.2	186.3 ✓
+5	6.6	186.9 ✓
1/4	4.3	189.2 ✓
+2	3.2	190.3 ✓
cb	2.7	190.8 ✓
E	1.4	192.1 ✓
75' S		
E	1.8	191.7 ✓
cb	3.0	190.5 ✓
+12	3.8	189.7 ✓
1/4	4.3	189.2 ✓
+7	6.9	186.6 ✓
c	7.1	186.4 ✓
1/4	7.4	186.1 ✓
+2	10.6	182.9 ✓
cb	10.1	183.4 ✓
+4	12.1	181.4 ✓
+10	13.5	180.0 ✓
+12	16.2	177.3 ✓
W	16.0	177.5 ✓

BRANT

10

105' S

W	15.3	178.2 ✓
+4	12.7	180.8 ✓
+10	11.7	181.8 ✓
cb	10.2	183.3 ✓
+1	9.2	184.3 ✓
+9	9.5	184.0 ✓
1/4	7.1	186.4 ✓
c	6.9	186.6 ✓
+7	6.6	186.9 ✓
1/4	4.2	189.3 ✓
+6	4.3	189.2 ✓
cb	3.0	190.5 ✓
E	1.8	191.7 ✓
125' S		
E	1.7	191.8 ✓
cb	3.0	190.5 ✓
+6	3.6	189.9 ✓
+7	4.1	189.4 ✓
1/4	4.3	189.2 ✓
+3	4.3	189.2 ✓
+6	6.2	187.1 ✓
c	6.6	186.9 ✓
+12	6.6	186.9 ✓
1/4	7.8	185.7 ✓
+1	8.6	184.9 ✓

19354

65	8.7	184.8 ✓
+9	12.5	181.0 ✓
+12	14.8	178.7 ✓
W	15.1	178.4 ✓

150'S

W	14.5	179.0 ✓
+1	14.3	179.2 ✓
+4	11.8	181.7 ✓
cb	9.5	184.0 ✓
+4	8.5	185.0 ✓
1/4	8.2	185.3 ✓
+2	6.3	187.2 ✓
C	6.3	187.2 ✓
+6	6.0	187.5 ✓
+8	4.4	189.1 ✓
1/4	4.5	189.0 ✓
+4	3.6	189.9 ✓
cb	2.8	190.7 ✓
E	2.0	191.5 ✓
T.P. ^{4.3} 1911 in pole 19140	6.27	187.27 ✓

175'S

E	0.0	171.4 ✓
cb	0.8	170.6 ✓
+11	1.6	189.8 ✓
1/4	2.6	188.8 ✓
+8	3.3	188.1 ✓

19140

BRANT

11

+10	3.9	187.5 ✓
+2	4.0	187.4 ✓
1/4	4.6	186.8 ✓
cb	5.7	185.7 ✓
+12	7.8	183.6 ✓
W	10.0	181.4 ✓

200'S

W	7.5	183.9 ✓
+3	5.7	185.7 ✓
cb	5.1	186.3 ✓
1/4	4.5	186.9 ✓
C	4.1	187.3 ✓
+4	4.2	187.2 ✓
1/4	2.3	189.1 ✓
cb	1.6	190.0 ✓
E	1.0	190.4 ✓

205'S

E	1.4	190.0 ✓
cb	1.6	189.8 ✓
1/4	2.5	188.9 ✓
+10	4.3	187.1 ✓
C	4.2	187.2 ✓
1/4	4.6	186.8 ✓
cb	5.2	186.2 ✓
W	5.8	185.6 ✓

191.40

225'S

W	5.6	185.8	✓
cb	5.4	186.0	✓
1/4	5.1	186.3	✓
c	4.8	186.6	✓
+7	4.8	186.6	✓
+9	3.8	187.6	✓
1/4	3.5	187.9	✓
ct	2.5	188.9	✓
E	2.4	189.0	✓

250'S

E	4.5	186.9	✓
cb	4.0	187.4	✓
+7	4.7	186.7	✓
+9	5.7	185.7	✓
1/4	5.7	185.7	✓
c	5.2	186.2	✓
1/4	5.5	185.9	✓
ct	5.9	185.5	✓
W	6.1	185.3	✓

275'S

W	6.2	185.2	✓
cb	6.5	184.9	✓
1/4	6.5	184.9	✓
C	6.4	185.0	✓
1/4	6.6	184.8	✓
cb	7.2	184.2	✓
E	7.7	183.7	✓

191.40

Branit

12

300'S = NL Nutmeg

E	11.6	179.8	✓
cb	10.5	180.9	✓
1/4	9.4	182.0	✓
c	8.2	183.2	✓
+2	7.4	184.0	✓
1/4	8.4	183.0	✓
ct	7.9	183.5	✓
W	7.9	183.5	✓

N ct

W	8.7	182.7	✓
cb	8.8	182.6	✓
+4	9.7	181.7	✓
1/4	8.7	182.7	✓
+6	8.8	182.6	✓
+10	10.3	181.1	✓
C	11.0	180.4	✓
1/4	12.1	179.3	✓
cb	13.5	177.9	✓
E	15.3	176.1	✓

N 1/4

E	18.2	173.2	✓
cb	16.8	174.6	✓
1/4	13.9	177.5	✓
c	13.3	178.1	✓
1/4	10.7	180.7	✓

191.40

+4		9.6	181.8	✓
cb		10.1	181.3	✓
+9		10.8	180.6	✓
w		9.8	181.6	✓
	+3			
w		11.2	180.2	✓
cb		10.0	181.4	✓
+6		10.2	181.2	✓
1/2		11.7	179.7	✓
c		14.3	177.1	✓
T.P.	236	181.26	12.50	178.90 ✓
1/2		5.1	176.2	✓
cb		7.0	174.3	✓
E		8.4	172.9	✓
	CENTER			
E		10.8	170.5	✓
cb		9.4	171.9	✓
1/2		7.8	173.5	✓
c		6.4	174.9	✓
1/2		3.9	177.4	✓
cb		1.7	179.6	✓
+6		0.4	179.9	✓
w		1.1	180.2	✓
	+5			
w		1.0	180.3	✓
+5		2.5	178.8	✓

181.26

BRANT

13

cb		3.6	177.7	✓
1/2		5.9	175.4	✓
c		7.8	173.5	✓
1/2		9.1	172.2	✓
cb		10.7	170.6	✓
E		12.8	168.5	✓
	S 1/2			
E		15.0	166.3	✓
cb		13.0	168.3	✓
1/2		11.7	169.6	✓
c		10.3	171.0	✓
1/2		8.2	173.1	✓
cb		6.5	174.8	✓
w		4.4	176.9	✓
	+5			
w		4.5	176.8	✓
cb		6.7	174.6	✓
1/2		8.8	172.5	✓
c		10.7	170.6	✓
1/2		12.1	169.2	✓
cb		13.5	167.8	✓
E		16.3	165.0	✓
	S 1/2			
E		20.5	160.8	✓
cb		16.8	164.5	✓
1/2		15.6	165.7	✓

18126

14

C			14.6	166.9	✓
2-1/4			12.5	168.8	✓
1/2			10.6	170.7	✓
W			7.9	173.4	✓

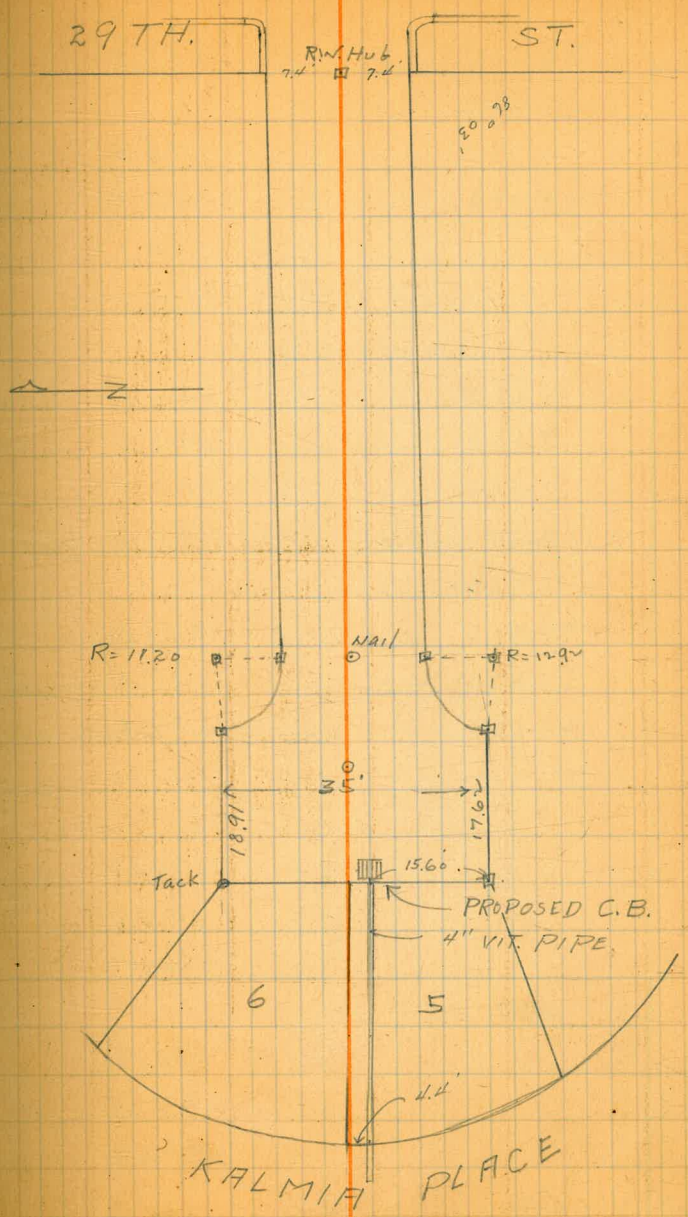
SL

W			13.4	167.9	✓
cb	+5		14.3	167.0	✓
1/4	cb		17.4	163.9	✓
A	1/4		20.6	160.7	✓
1/4	C		21.2	160.1	✓
	1/4		21.9	159.4	✓
	cb		23.0	158.3	✓
	E		27.2	154.1	✓

T.P.	020	168.18	13.28	167.98	Ward + Brant
			11.70	156.48	156.51 top of 1950.

3/7/5 CROSS SECTION OF ALLEY
 Moore L.P. DELANO TRACT. 15' wide

ON P&E:	5.85	291.93	286.08	Kalmia + 29th
		W.L. 29th		
- S on curb		5.15	286.78	
C		5.1	286.8	
N ✓ ✓		5.15	286.78	
		8' w		
- 0.4 EL Conc. Drive to Garage		4.53	287.40	East Entrance
C		4.7	287.2	
S		4.7	287.2	
		14.9 w		
S EL Conc. Drive to Garage		4.88	287.05	✓ ✓
C		4.9	287.0	
N		4.7	287.2	
		23.5 w		
N		4.8	287.1	
C		5.2	286.7	
S W ✓ ✓		5.2	286.7	
+ 0.5		5.4	286.69	
		27.9 w		
S		5.4	286.5	
C		5.5	286.4	
N		5.0	286.9	
+ w W/L of Conc. Drive		4.71	287.22	East Entrance El Garage
		50.6 w		
- 1.3 EL Conc. Apron to Garage		7.46	284.47	S Entrance
C		7.3	284.6	



291.93

279.12

16

S			7.2	284.5
	65.1 W			
N			8.3	283.6
C			8.6	283.3
N			7.8	284.1
+ 1.8	W of Conv. Apron		7.54	284.39
	80.2 W			
N			9.4	282.5
C			9.7	282.2
S			9.4	282.5
+ 7	☐ of Garage Conv. floor		9.32	282.61
	105 W			
S			12.8	279.1
C			12.4	279.5
N			12.1	279.8
T.P.	0.19	279.12	13.00	278.93
		(as)		
		130.85 N = P.C.		
N	on Hub		2.08	277.04
C			2.2	276.9
S	✓ ✓		2.70	276.42
	138.65	119.97		EC
S	✓ ✓		4.67	274.45
+ 17.5 = ☐			3.9	275.2
N	✓ ✓		3.46	275.66
	159.94	161.35		W.L. of Square
N			5.1	274.0

+ 10.8	☐ of Garage Conv. floor	4.67	274.48	E. Entrance
C		5.0	274.1	
+ 1.8	☐ of proposed Drain	5.2	273.9	
S	on Hub	6.37	272.75	

Levels for Vit. Pipe Drain.

W.L. of Square = 0100

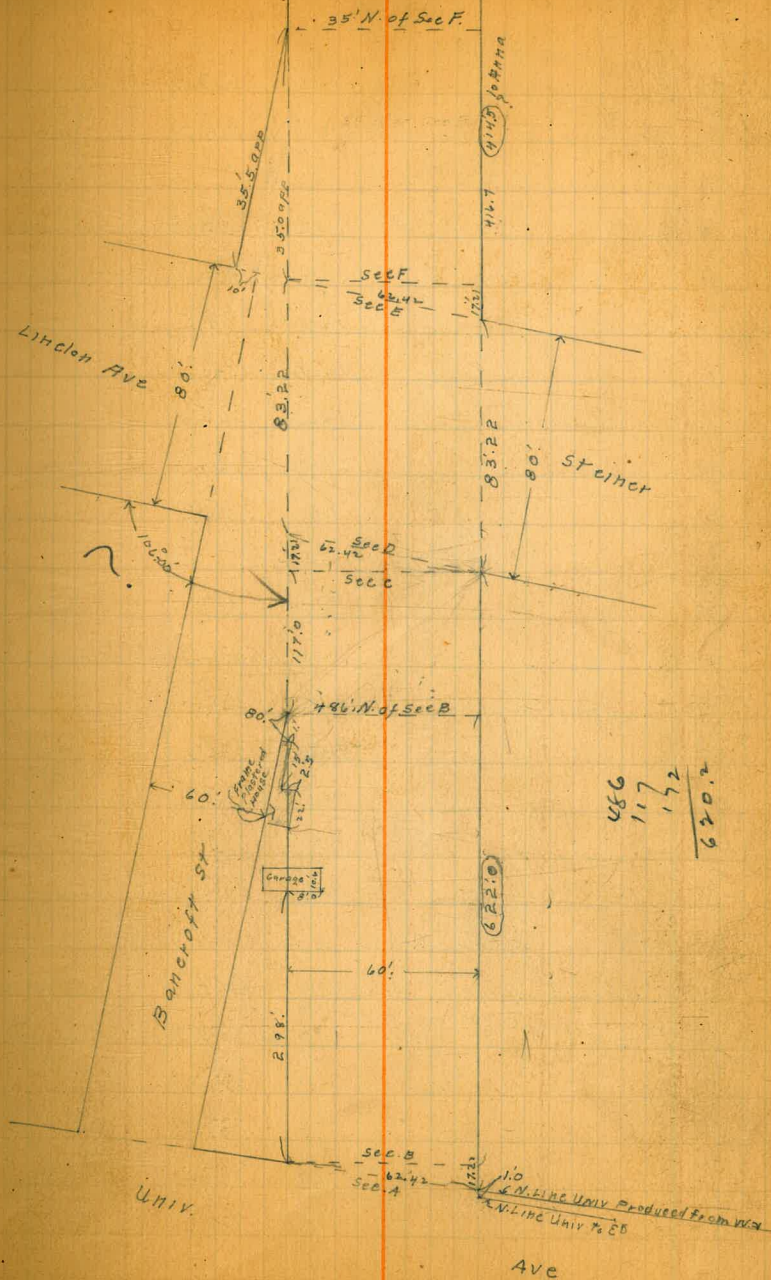
0100		5.2	273.9	
+ 8		7.3	271.8	
+ 50		12.0	267.1	
T.P.	3.41	269.62	12.91	266.21
+ 85		6.7	262.9	
+ 91	E Edge of S/W	10.18	259.44	
+ 96	top curb	10.34	259.28	
+ 96	Butter on Paving	10.92	258.70	

60' wide
10' cbs.
10' 1/4

Boundary St
X Sec from N. Line University to S. Line El Cajon

3/14/25
7.871

B.M.	11.90	345.34	333.44	N. Univ and Boundary
	See A = N. Line Univ			
E		11.9	333.4	
78		12.2	333.1	
cb		12.7	332.6	
1/4		12.7	332.6	
C		12.4	332.9	
1/4		12.4	332.9	
cb		12.1	333.2	no yardage
cbkint cb		11.97	333.37	333.4
W		11.7	333.6	
	See B = 00			
W		11.7	333.6	
cb		11.6	333.7	
1/4		12.4	333.0	
C		12.4	333.0	
1/4		12.1	333.2	
cb		11.5	333.8	
1/4		11.0	334.3	
E		10.9	334.4	
	7' N of Sec B.			
E		10.6	334.7	
cb		11.3	334.0	
1/4		12.0	333.3	
C		12.2	333.1	
1/4		12.3	333.0	



34534

7' N. con

cb	12.1	333.2
w	12.1	333.2

50' N.

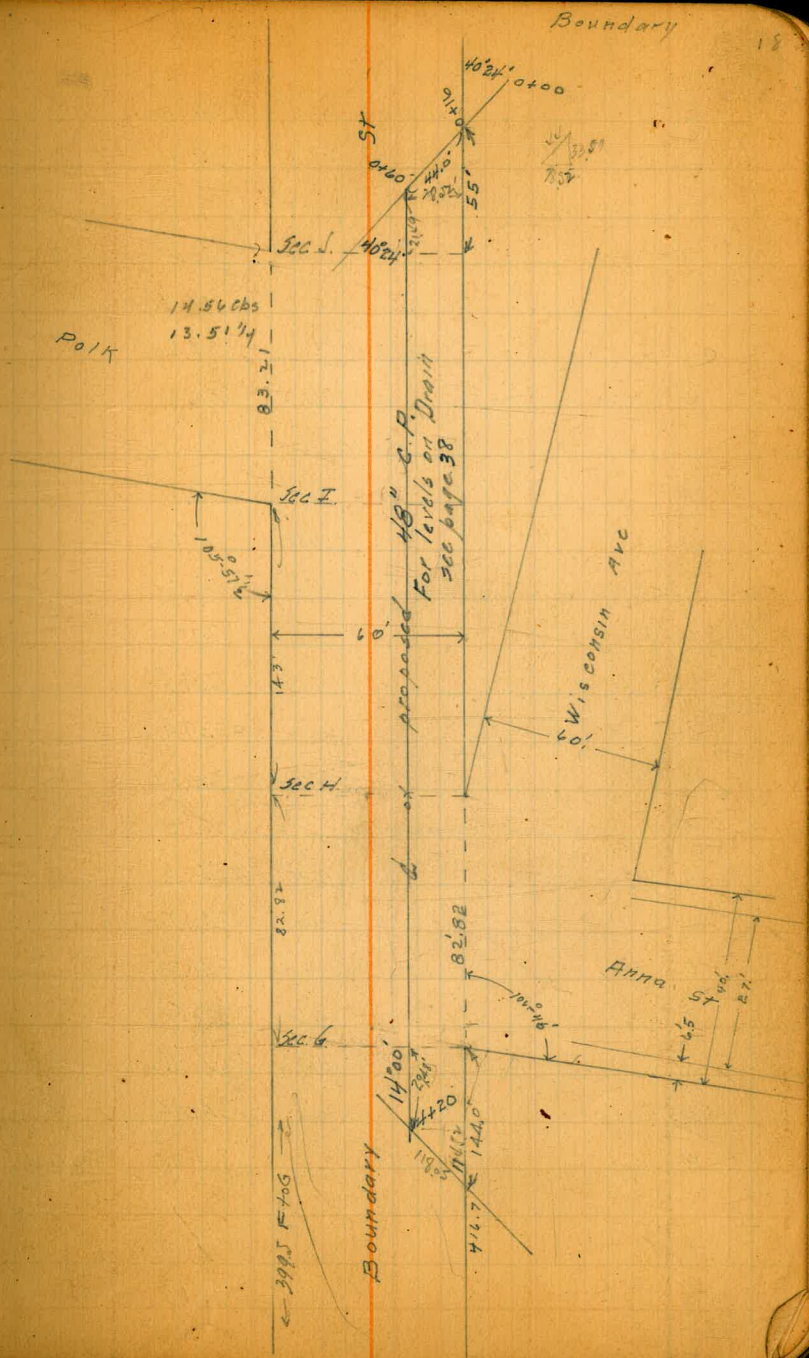
w	11.0	334.3
cb	10.7	334.6
1/4	10.8	334.5
c	10.9	334.3
1/4	10.3	335.0
cb	9.8	335.5
e	9.4	335.9

150' N

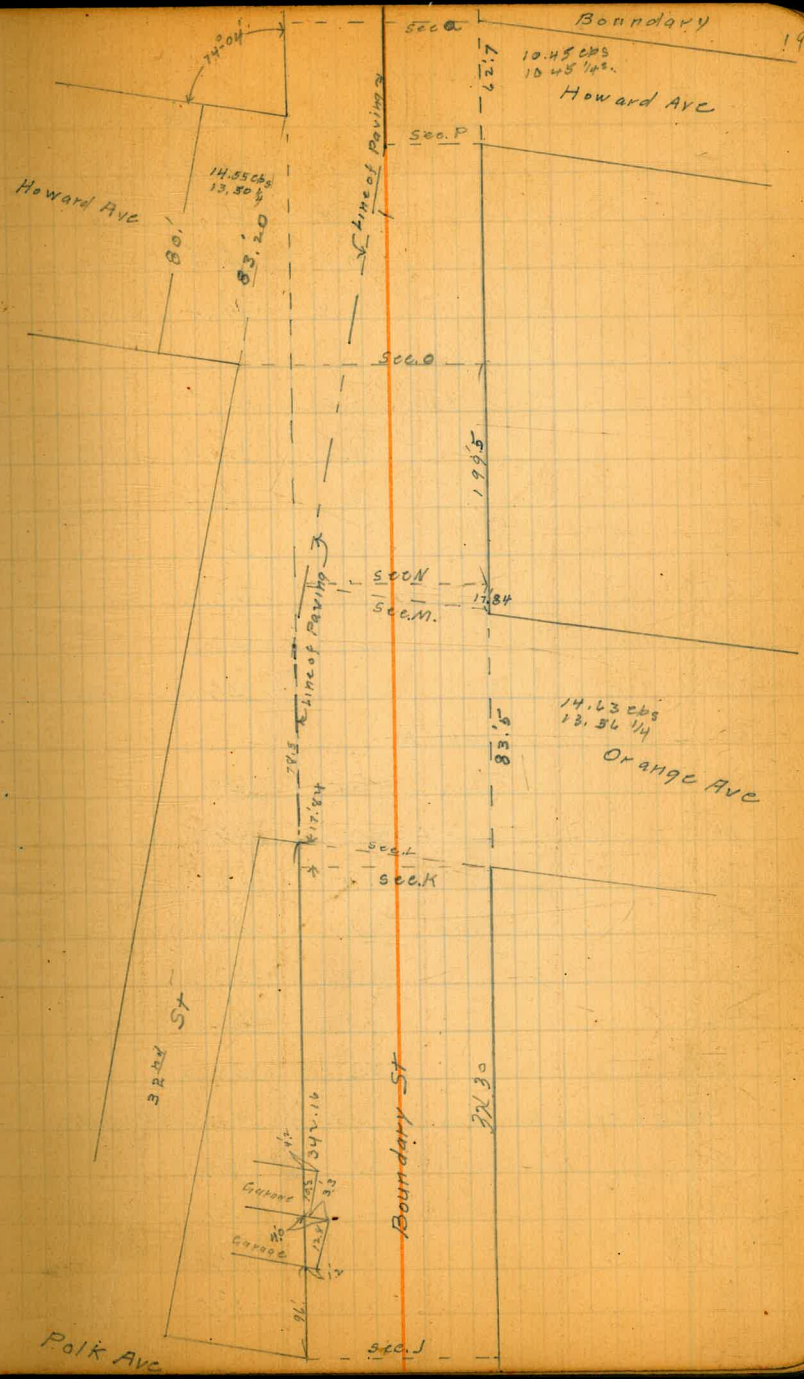
e	8.2	337.1
cb	9.0	336.3
1/4	9.3	336.0
c	9.3	336.0
1/4	9.4	335.9
cb	9.4	335.9
w	9.5	335.8

150' N

w	8.9	336.7
cb	8.2	337.1
1/4	8.0	337.3
c	8.2	337.1
1/4	7.9	337.4
cb	7.7	337.6
e	7.0	338.3



	200' N		
E	6.0	339.3	
cb	6.3	339.0	
1/4	6.7	338.6	
E	7.0	338.3	
1/4	6.9	338.4	
cb	7.2	338.1	
W	7.5	337.8	
	250' N		
W	6.2	339.1	
cb	6.0	339.3	
1/4	5.9	339.5	
E	5.6	339.7	
1/4	5.5	339.8	
cb	5.4	339.9	
E	5.2	340.1	
	300' N		
E	4.5	340.8	
cb	4.6	340.7	
1/4	4.6	340.7	
E	4.8	340.5	
1/4	4.7	340.6	
cb	4.9	340.4	
W	5.1	340.2	Under Garage
	350' N		
W	4.0	341.3	
cb	4.0	341.3	



34534

350' N (cont)

1/4	4.0	341.3
e	3.9	341.4
1/4	3.8	341.5
cb	3.8	341.5
e	3.9	341.4

400' N

e	3.5	341.8
cb	3.4	341.9
1/4	3.1	342.2
e	3.1	342.2
1/4	3.0	342.3
cb	3.1	342.2
w	3.3	342.0

Under House

450' N.

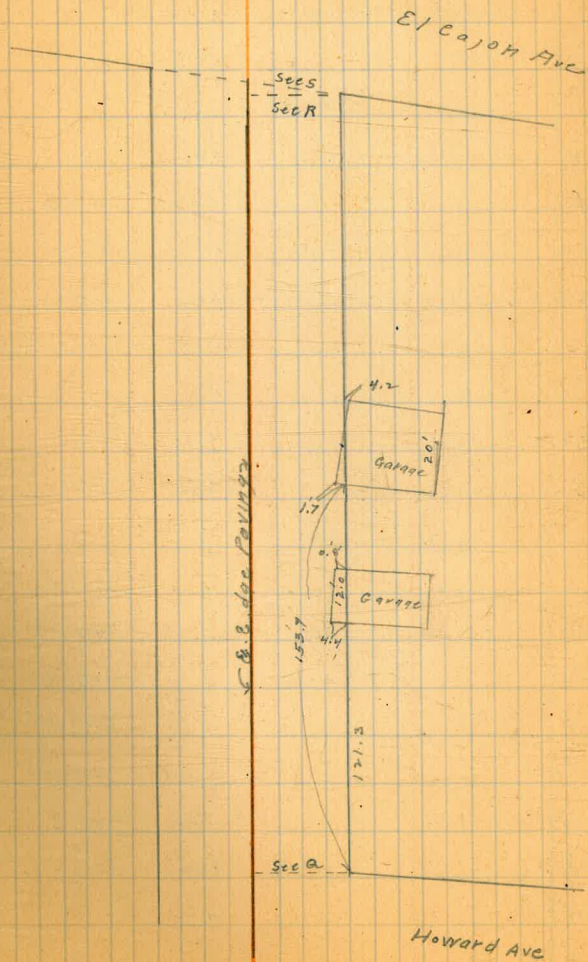
w	2.4	342.9
cb	2.4	342.9
1/4	2.4	342.9
e	2.6	342.7
1/4	2.8	342.5
cb	3.1	342.2
e	3.3	342.0

486' N = Pt. W. Line Boundary & E. Line Bancroft Page 17

e	3.1	342.2
cb	2.8	342.5
1/4	2.5	342.8
e	2.3	343.0

Boundary

20



345.34

486' N (coh)

14	2.0	343.3
cb	1.9	343.4
+ 8	1.9	343.4
w	4.7	340.6

= End return on E. line Bancroft + w line Boundary

w	5.11	340.73	on emt. cb.
---	------	--------	-------------

500' N

w	5.0	340.3
+ 5	1.8	343.5
cb	1.8	343.5
14	2.0	343.3
c	2.5	342.8
14	2.6	342.7
cb	2.8	342.5
c	3.0	342.3

535' N

E	2.7	342.6
cb	2.6	342.7
14	2.6	342.7
c	2.3	343.0
14	2.0	343.3
cb	1.7	343.6
+ 5	1.8	343.5
w	4.2	341.1

345.34

Boundary

550' N

w	4.0	341.3
+ 5	1.7	343.6
cb	1.7	343.6
14	1.9	343.4
c	2.2	343.1
14	2.5	342.8
cb	2.2	343.1
+ 5	2.1	342.2
c	3.2	342.1

557' N

E	2.1	343.2		
cb	2.2	343.1		
14	2.6	342.7		
c	2.3	343.0		
14	2.1	343.2		
cb	1.8	343.5		
+ 5	1.8	343.5		
w	3.9	341.4		
T.P.	2.95	346.51	1.78	343.56

603' N of Sec B. = Sec C. Page 17

w	4.0	342.5
+ 5	2.9	343.6
cb	2.9	343.6
14	3.3	343.2
c	3.7	342.8
14	4.0	342.5
cb	3.6	342.9
E	4.1	342.4

0.25
4.0
4.25
4.86

Boundary { 62.42 wide
10.4 cbs
on Diagonal } 10.4 1/43

346.51

See D = S. Line Linclon

E	4.1	342.4
cb	3.2	343.3
1/4	2.7	343.8
e	3.3	343.2
1/4	3.3	343.2
cb	3.3	343.2
w	3.4	343.1
	S. cb	
w	4.1	342.4
cb	4.0	342.5
1/4	4.0	342.5
e	4.1	342.4
1/4	3.9	342.6
cb	3.9	342.6
E	3.8	342.7
	S. 1/4	
E	3.7	342.8
cb	3.2	343.3
1/4	3.3	343.2
C	3.0	343.5
1/4	3.3	343.2
cb	3.0	343.5
w	3.4	343.1
	⊕ Linclon	
w	3.1	343.4
cb	3.0	343.5

Linclon 593.22 wide
14.57 cbs
on Diagonal } 13.52 1/43

346.51

Boundary

1/4	2.4	344.1
C	2.4	344.1
1/4	2.2	344.3
cb	2.5	344.0
E	3.0	343.5
	N. 1/4	
E	3.1	343.4
cb	3.2	343.3
1/4	3.4	343.1
E	3.0	343.5
1/4	3.4	343.1
cb	3.4	343.1
w	3.2	343.3
	N. cb,	
w	3.4	343.1
cb	3.3	343.2
1/4	3.7	342.8
C	3.7	342.8
1/4	3.8	342.7
cb	4.0	342.5
e	4.5	342.0
	See E = N. Line Linclon	
E	4.6	341.9
cb	3.8	342.7
1/4	3.8	342.7
C	3.9	342.6

346.51

Sec E Coy

1/4	3.7	342.8
cb	3.5	343.0
w	3.3	343.2
+10 W. Line Bancroft	3.2	343.3

00 = Sec F

w	3.3	343.2
cb	3.8	342.7
1/4	4.2	341.7
c	4.7	341.8
1/4	4.4	342.2
cb	5.3	341.2
E	8.2	338.3
+10	10.2	336.3

5' N of Sec F

-10	9.7	336.8
E	8.8	337.7
cb	7.5	339.0
1/4	6.3	340.2
c	5.4	341.1
1/4	4.6	341.9
cb	4.0	342.5
w	3.3	343.2
+10	3.0	343.5

35' N. of Sec F = P.I. W. Line Boundary + w line Bancroft

w	3.5	343.0
cb	4.1	342.4

346.51

Boundary

1/4	4.8	341.7
c	5.5	341.0
1/4	4.6	339.9
cb	7.6	338.9
E	8.9	337.6
+10	10.6	335.9

65' N.

-10	11.5	335.0
E	9.8	336.7
cb	7.6	338.9
+5	6.5	340.0
1/4	6.2	340.3
c	5.1	341.4
1/4	5.3	341.2
cb	4.6	341.9
w	3.5	343.0

100' wide N

w	4.0	342.5
cb	5.0	341.5
1/4	5.5	341.0
c	6.0	340.5
1/4	6.7	339.8
cb	8.5	338.0
E	10.7	335.8
+10	12.3	334.2

346.51

150' N

-15	13.7	332.8
E	10.0	336.5
cb	8.5	338.0
1/4	7.8	338.7
C	7.0	339.5
1/4	6.3	340.2
cb	5.5	341.0
W	4.5	342.0

170' N

W	4.1	347.4
cb	5.6	340.9
1/4	6.6	339.9
C	6.9	339.6
1/4	7.7	338.8
cb	8.8	337.7
E	9.8	326.7
+16	14.2	337.3
+20	16.4	330.1
+22	16.2	330.3

200' N

-20	13.1	333.4
-10	15.0	331.5
E	12.7	333.8
cb	8.7	337.8
1/4	7.3	339.2
C	6.5	340.0

346.51

Boundary

24

1/4	6.0	340.5
cb	5.4	341.1
W	4.2	342.3

225' N

W	4.0	342.5
cb	5.4	341.1
1/4	5.8	340.7
C	6.5	340.0
1/4	7.9	338.6
cb	10.4	336.1
E	12.9	333.6
+5	14.8	331.7
+12	13.8	332.7

250' N

-12	11.5	335.0
-6	13.7	332.8
E	12.5	334.0
cb	11.1	335.4
1/4	9.0	337.5
C	7.4	339.1
1/4	6.0	340.5
cb	5.6	340.9
W	4.5	342.0

346.51

270' N

W	4.5	342.0
cb	5.8	340.7
1/4	4.0	340.5
C	8.0	338.5
1/4	9.3	337.2
cb	11.2	335.3
E	13.4	333.1
+5	11.7	334.8
+10	11.9	334.6

300' N

-10	9.1	337.4	-
-1	11.6	334.9	-
E	12.4	334.1	creek
+6	12.0	334.5	-
+7	11.1	335.4	-
cb	11.6	334.9	-
1/4	9.6	336.9	-
+5	8.2	338.3	-
E	8.0	338.5	-
1/4	7.0	339.5	-
cb	5.8	340.7	-
W	5.0	341.5	-

320' N

W	5.2	341.3
cb	5.7	340.8
1/4	6.4	340.1

346.51

Boundary

25

C	8.4	338.1	-
1/4	10.1	336.4	-
cb	10.8	335.7	creek
E	9.6	336.9	-
+8	8.4	338.1	-

350' N

-5	5.2	341.3	-
E	6.2	340.3	-
cb	8.2	338.3	-
1/4	9.6	336.9	creek
C	9.4	337.1	-
1/4	7.0	339.5	-
cb	5.2	341.3	-
W	4.7	341.8	-

375' N

W	4.2	342.3	-
cb	4.8	341.7	-
1/4	7.4	339.1	-
+7	9.4	337.1	creek
E	8.8	337.7	-
1/4	7.8	338.7	-
+5	6.0	340.5	-
cb	5.5	341.0	-
E	3.7	342.8	-
+5	3.2	343.3	-
T.P.	6.32	350.05	2.78 343.73

399.5' N = Sec G Page 18 = S Line Anno

E	6.4	343.6
cb	6.8	343.2
1/4	8.1	341.9
C	9.4	340.6
1/4	11.2	338.8
+2	12.0	338.0
+4	9.6	340.4
cb	7.0	343.0
W	7.1	342.9

66' N of Sec G = S' ch Anno Page 18

W	7.0	343.0
cb	7.3	342.7
+7	10.3	339.7
+8	11.4	338.7
1/4	10.5	339.5
+3	8.4	341.7
C	8.8	341.2
1/4	7.8	342.2
cb	6.9	343.1
E	6.4	343.6

15' N of Sec G

C	6.4	343.6
cb	6.8	343.2
1/4	7.6	342.4
C	8.8	341.2
+7	9.0	341.0

+8	11.7	338.3
1/4	9.5	340.5
cb	8.0	342.0
+3	6.8	343.2
W	6.7	343.3

30' N of Sec G

W	6.6	343.4
cb	6.9	343.1
1/4	9.4	340.6
C	10.2	339.8
+2	11.6	338.4
+8	9.4	340.2
1/4	9.2	340.8
cb	6.6	343.4
E	6.1	343.9

35' N

E	6.3	343.7
cb	6.6	343.4
1/4	7.6	342.4
+1	9.4	340.6
+5	11.8	338.2
C	10.4	339.6
+4	6.9	343.1
1/4	7.1	342.9
+5	6.6	343.2
cb	6.8	343.2
W	6.4	343.6
W	6.1	343.9
cb	6.4	343.6
1/4	6.6	343.4
C	7.3	342.7
1/4	7.3	342.7
cb	6.6	343.4
E	5.9	344.1

39' N

56'N

E	6.0	344.0
cb	6.4	343.6
1/4	7.0	343.0
c	7.0	343.0
1/4	6.2	343.8
cb	5.5	344.5
w	5.3	344.7

58'N

w	5.2	344.8
cb	5.6	344.4
1/4	6.0	344.0
1/4	6.7	343.3
c	9.9	340.1
+3	11.5	338.5
1/4	8.8	341.7
+0.5	7.0	343.0
cb	6.2	343.8
E o.k	6.0	344.0

↑
change

W o.k

cb

65'N

w	5.3	344.7
cb	5.7	344.3

Boundary 27

1/4	5.9	344.1
+4	6.2	343.8
c	10.8	339.2
+6	11.4	338.6
1/4	9.3	339.7
+3	7.5	342.5
cb	7.1	342.9
E	6.2	343.8

82.82 N of Sec G = Sec H = P.I. W line Wisconsin St & E. Line Boundary

E	6.3	343.7
cb	7.6	342.4
+5	8.0	342.0
1/4	9.6	340.4
+5	10.0	340.0 creek
c	9.5	340.5
1/4	7.5	342.8
cb	6.1	343.9
w	5.5	344.5

42' N of Sec H

w	6.2	343.8
cb	7.0	343.0
1/4	7.5	342.5
c	8.0	342.0

42' N (con)

1/4	8.5	341.5
cb	7.8	342.2
E	6.4	343.6

45' N

E	5.7	344.3
+6	5.8	344.2
cb	8.5	341.5
1/4	8.3	341.7
C	8.0	342.0
1/4	7.5	342.5
cb	6.8	343.2
W	6.1	343.9

65' N

W	6.1	343.9
cb	7.1	342.9
1/4	7.7	342.2
C	7.8	343.4
1/4	7.9	342.1
cb	6.9	343.1
E	5.8	344.7

75' N = s. cor House, ^{on E.} 2.2' N street

E	6.5	343.5
cb	7.4	342.6
1/4	7.8	342.2
C	7.7	342.2
1/4	8.0	342.0

cb	7.3	342.7
W	6.8	343.2

100' N

W	5.0	345.0
+6	7.2	342.8
cb	7.4	342.6
1/4	7.4	342.6
C	8.2	341.8
+6	7.1	342.9
1/4	7.0	343.0
cb	7.0	343.0
E	5.2	344.8

110' N

E	4.3	345.7
cb	6.1	343.9
1/4	7.0	343.0
C	8.1	341.9
+5	6.9	343.1
1/4	6.9	343.1
cb	7.1	342.9
W	6.8	343.2
+5	6.0	344.0
-5	5.6	344.2
W	5.8	344.2
cb	5.2	344.8
1/4	5.6	344.2
+5	5.2	344.8

143' N of sec. H = sec. I = s. line Polk Ave. ^(83.21 wide)
_(3.51 1/2)

sect (con)

c	7.4	347.6
1/4	7.6	347.4
+5	6.0	344.0
cb	5.2	344.8
+4	5.0	345.0
E	3.6	346.4

S. cb.

E	2.8	347.2
+3	2.4	347.2
+6	4.5	345.5
cb	4.5	345.5
+5	11.3	345.7
+8	6.8	343.2
1/4	6.8	343.2
+5	8.5	341.5
c	8.0	342.0
+3	4.5	345.5
1/4	3.2	346.8
cb	2.4	347.6
w	1.4	348.6

S. 1/4

w	1.2	348.4
cb	1.7	348.3
1/4	1.9	348.1
+5	2.0	348.0
c	4.5	343.5

+5	4.2	343.7
1/4	5.4	344.6
cb	4.2	345.8
+5	3.9	346.1
+7	3.0	347.0
E	3.0	347.0

E. Polk

E	2.5	347.5
cb	3.9	346.1
+5	3.5	346.5
1/4	4.7	345.3
+5	6.0	344.6
E	6.1	343.9
1/4	6.1	345.9
cb	0.7	349.3
w	0.6	349.4

N 1/4

w	0.0	350.0
cb	0.4	349.6
+5	4.1	345.9
1/4	4.5	345.5
c	5.5	344.5
+7	4.4	345.6
1/4	3.2	346.8
cb	2.9	347.1
E	3.1	346.9

T.P.	9.94	357.62	2.37	347.68
		N. Ch.		
E			10.4	347.2
cb			10.7	346.9
+5			10.3	347.3
1/4			11.3	346.3
+4			12.5	345.1
E			12.8	347.8
+7			12.5	345.1
1/4			10.8	346.8
cb			10.7	346.9
W			9.0	348.6
+5			9.1	348.5

00 = N. Line Paik = Sec J

-5			9.5	348.1
W		35	10.1	347.5
cb			10.2	347.4
1/4			11.1	346.5
+5			12.5	345.1
E			12.7	344.9
+7			11.3	346.3
1/4			11.3	346.3
cb			10.4	347.2
E			10.3	347.0

		30' N	
-5		9.4	348.2
E		9.6	348.0
cb		10.2	347.4
+2		11.8	345.8
1/4		12.2	345.4
+6		12.3	345.3
C		11.0	346.6
1/4		10.3	347.3
cb		9.4	348.2
W		8.1	349.5

45' N

W		7.2	350.4
cb		8.1	349.5
1/4		9.3	348.3
E		10.0	347.6
1/4		11.1	346.5
+3		12.1	345.5
cb		11.9	345.7
+7		11.6	346.0
E		10.1	347.5
+5		10.8	346.8

55' N

-5		10.5	347.1
E		11.4	346.2
cb		11.8	345.8
1/4		10.6	347.0

e	9.3	348.3
1/4	8.2	349.4
+5	7.5	350.1
cb	7.4	350.2
w	7.0	350.6

70' N

w	6.3	351.3
cb	6.9	350.7
1/4	7.1	350.5
e	8.1	349.5
1/4	8.5	349.1
cb	10.2	347.4
e	11.1	346.5
+10	11.2	346.4

100' N

-5	8.3	349.3
e	8.3	349.3
cb	7.4	350.2
1/4	6.8	350.8
e	7.0	350.6
1/4	6.9	350.7
cb	6.6	351.0
w	6.1	351.5

135' N

w	5.6	357.0
cb	5.8	351.8

4 Hds per page

1/4	5.8	351.8
e	6.0	351.6
1/4	6.1	351.5
cb	6.1	351.5
e	6.2	351.4
+5	6.4	351.2

165' N

-5	5.5	352.1
e	5.6	357.0
cb	5.7	351.9
1/4	5.5	352.1
e	5.3	352.3
1/4	5.1	352.5
cb	5.0	352.6
w	4.8	357.8
+3	4.6	353.0

200' N

-3	3.6	354.1
w	3.9	353.7
cb	4.1	353.5
1/4	4.3	353.3
e	4.4	353.2
1/4	4.4	353.2
cb	4.2	353.4
e	4.2	353.4
+5	4.1	353.5

255' N

-5		1.2	356.4
E		1.0	356.6
cb		1.6	356.0
1/4		1.8	355.8
c		2.0	355.6
1/4		2.2	355.4
cb		2.2	355.4
w		1.6	356.0
+5		1.4	356.2

T.P. 12.74 36869 1.67 355.95

270' N

-3		12.7	356.0
w		12.7	356.0
cb		12.5	356.2
1/4		12.4	356.1
c		12.2	356.5
1/1		12.1	356.6
cb		11.7	357.0
E		10.9	357.8

300' N

E		9.6	359.1
cb		10.2	358.5
1/4		10.4	358.3
c		11.0	357.7
1/4		11.3	357.4
cb		11.3	357.4
w		11.1	357.6

324.20 N = Sec K Page 18

w		10.5	358.2
cb		10.2	358.5
1/4		10.0	358.7
c		9.6	359.1
1/4		9.2	359.5
cb		8.9	359.8
E		8.4	360.3

Sec L = S Line Orange

E		8.4	360.3
cb		8.8	359.9
1/4		9.0	359.7
c		9.2	359.5
1/4		9.4	359.3
cb		9.6	359.1
w		9.9	358.8

S cb.

w		10.27	358.42	ohmt cb
cb		9.1	359.6	
1/4		8.6	360.1	
c		8.5	360.2	
1/4		8.2	360.5	
cb		8.1	360.6	
E		8.1	360.6	

368.69

Orange

E	4.6	362.1	
cb	4.6	362.1	
1/4	4.7	362.0	
C	7.1	361.6	
1/4	7.6	361.1	
cb	7.9	360.8	
W	9.30	359.4	on paving

N. cb

W	8.37	360.32	" "
+2	6.8	361.9	
cb	4.7	362.0	
1/4	6.5	362.2	
C	4.3	362.4	
1/4	5.8	362.9	
cb	5.7	363.0	
E	5.9	362.8	

Sec M = N Line Orange

E	5.1	363.6	
cb	5.3	363.4	
1/4	5.5	363.2	
C	5.6	363.1	
1/4	6.0	362.7	
cb	6.0	362.7	
+7	6.4	362.3	
W	7.87	360.82	on paving

368.69

Boundary

33

sec N.

W	7.87	360.82	on paving
+2	6.3	362.4	
cb	5.9	362.8	
1/4	5.7	363.0	
C	5.3	363.4	
1/4	5.1	363.6	
cb	5.0	363.7	
E	4.8	363.9	

50' N of sec N

E	3.4	365.3	
cb	3.3	365.4	
1/4	3.0	365.7	
C	3.2	365.5	
1/4	3.5	365.7	
cb	3.9	364.8	
+2	4.3	364.4	
+32	5.97	362.72	E. edge of paving on paving

85' N.

Wcb. 0.8	4.72	363.97	Boundary 49.2 from E. Line, E edge paving
" " +5	3.1	365.6	
1/4	2.8	365.9	
C	2.5	366.2	
1/4	2.3	366.4	
cb	2.5	366.2	
E	2.8	365.9	

378.69

135' N

E	1.8	366.9
cb	1.9	366.8
1/4	1.8	366.9
C	1.9	366.8
1/4	2.2	366.5
+3.2	2.96	365.73

on E edge
Paving

199.5 N. of Sec N. = Sec O. P. 18

N 1/4 + 4.75

E	0.76	367.93
C	0.9	367.8
1/4	0.9	367.8
cb	1.3	367.4
E	1.1	367.6

on E. edge paving

T.P. 10.26 378.39 0.56 368.13

46' N. of Sec. O = P.I. E 32nd a E Boundary = on E edge paving

E	10.3	368.1
cb	10.0	368.4
1/4	9.8	368.6
E	9.66	368.73

on E edge paving

68.4 N. of Sec O = S line Howard on E = Sec P

E	9.30	369.1
1/4	9.4	369.0
cb	10.0	369.4
E	10.1	368.3

S. cb

E	9.9	369.5
cb	9.4	369.0

378.39

Boundary 34

1/4	9.1	369.3
C	9.10	369.79
ϕ		
C	8.67	369.72
1/4	8.7	369.7
cb	8.7	369.7
E	9.2	369.2

on E. edge paving

" " " "

N. cb,

E	8.4	370.0
cb	8.3	370.1
1/4	8.1	370.3
C	8.16	370.22

on E. edge paving

Sec Q = N line Howard on E

C	7.91	370.48
1/4	7.9	370.5
cb	8.1	370.3
E	8.1	370.3

50' N. of Sec Q

E	6.5	371.9
cb	6.5	371.9
1/4	6.4	372.0
C	6.76	371.63

on E. edge paving

100' N

C	5.55	372.84
1/4	5.6	372.8
cb	5.6	372.8
E	5.4	373.0

" " " "

150' N.

E	3.8	374.6	
cb	4.3	374.1	
1/4	4.6	373.8	
B	4.45	373.94	on E. edge Paving

200' N

C	3.34	375.05	" " " "
1/4	2.7	375.7	
cb	2.8	375.6	
C	2.8	375.6	

250' N

E	2.3	376.1	
cb	2.6	375.8	
1/4	2.7	375.7	
C	2.23	376.16	on R. edge Paving

386' N = Sec R = RT L From S Line El Cajon Ave.

C	1.51	376.88	" " " "
1/4	1.7	376.7	
cb	1.6	376.8	
E	1.7	376.7	

Sec S = S Line El Cajon produced from E.

E	1.7	376.7	
cb	1.45	376.94	on catch
1/4	1.7	377.0	
C	1.26	377.13	on E. edge Paving
chken BM.	0.84	377.55 = 377.49	SPK S.W. Boundary & El Cajon

Polk Ave
 2. Sec from E. Line 32nd to W. Line Boundary
 3/17/25⁸
 F.P.M.

T.P. see Page 30	8.37	356.05	347.68	
		00 = E. Line 32 nd ST		
S		2.6	353.5	
cb		2.90	353.15	onemt cb
+1		3.6	352.5	
1/4		3.4	352.7	
C		3.1	353.0	
1/4		3.7	352.9	
+12		3.7	352.4	
cb		3.01	353.04	onemt cb
N		2.6	353.5	
	5' E.			
N		2.2	353.9	
+13		2.7	353.4	
cb		3.7	353.4	
1/4		3.1	353.0	
C		3.2	352.9	
1/4		3.5	352.6	
+11		3.2	352.9	
cb		2.4	353.7	
S		1.8	354.3	
	30' E			
S		3.1	353.0	
cb		3.2	352.9	
+15		2.1	354.0	
1/4		2.7	353.4	

356.05

Folk 36

+3	4.1	352.0
+6	2.6	353.5
C	2.9	353.2
1/4	2.4	353.7
+10	2.8	352.3
cb	4.2	351.9
1/4	2.2	353.9
+8	2.8	352.3
+10	3.6	352.5
N	3.6	352.5
	50' E	
N	4.4	351.7
cb	4.5	351.6
+7	2.1	352.0
1/4	2.8	353.3
C	2.8	353.3
+7	2.9	353.2
+9	4.3	351.7
10	3.3	352.8
1/4	3.3	352.8
+11	3.2	352.9
cb	4.0	352.1
S	4.0	352.1

75' E

S	5.4	350.7
cb	5.2	350.9
+5	4.1	357.0
+11	3.9	357.2
1/4	4.7	351.4
+2	3.8	352.3
C	4.4	351.7
1/4	4.5	351.6
cb	5.4	350.7
+4	6.0	350.1
+5	4.8	351.3
N	5.3	350.8
	100' E	
-5	6.8	349.3
N	7.0	349.1
+2	7.1	349.0
+8	5.4	350.7
cb	6.3	349.8
1/4	5.0	351.1
C	5.6	350.5
1/4	5.3	350.8
+3	5.0	351.1
+4	5.8	350.3
+6	5.1	351.0
cb	5.6	350.5
+4	6.8	349.3

PALK 37

+6	8.1	348.0
S	8.1	348.0
+5	7.9	348.2
	115' E	
-5	11.1	345.0
S	11.2	344.9
+5	10.9	345.2
+11	7.6	348.5
cb	6.5	349.3
+4	6.2	349.9
+5	7.1	349.0
+6	4.3	349.8
1/4	5.9	350.2
C	6.3	349.8
1/4	5.7	350.4
+2	5.7	350.4
cb	7.2	348.9
+4	7.0	349.1
N	8.5	347.5
	N	
	115.8 E on S to 138.7 E on S = W. Line Boundary	
N	8.5	347.5
cb	7.4	348.6
1/4	6.0	350.0
C	6.6	349.4
1/4	7.2	348.8
cb	7.4	348.6
S	11.8	344.2

3/17/26

Levels on Drain
on Boundary St.
at Polk

34680

for Location
see page 18

356.05

142 ft from page 36

0+00

9.38 346.67 on stub

+50

9.0 337.8

+16

10.2 345.9

+70

9.6 337.2

+60 Δ 40°24' L

10.79 345.26 on stub

+85

10.3 336.5

1

11.2 344.9

5

10.7 336.1

+42.30 = center 30" Water pipe

12.70 343.35 = Top of pipe

+25

11.3 335.5

+45

14.4 341.7

+35

12.1 334.7

+55

13.2 342.9

+55

12.4 334.4

TP

171

34680

11.96 344.09

+65

14.3 332.5

+75

13.0 333.8

2

3.9 347.9

6

13.7 332.1

+20

3.4 343.4

+15

14.0 331.8

+50

3.7 343.1

+25

15.8 331.0

+60

4.0 347.8

+35

16.2 330.6

+70

3.3 343.5

3

3.9 342.9

+10

6.0 340.8

+20

7.1 339.7

+35

6.6 340.2

+36

2.7 344.1

+53

2.9 343.9

+54

7.0 339.8

+64

7.4 339.4

+70

3.8 343.0

+92

4.8 342.0

4

5.7 341.1

+20 Δ 14°00' L

8.15 337.65 on stub

Plumosa Terrace
Levels for establishment of grade

4/28/25
miles

39

B.M.	358	272.89	269.31	SW Plumosa 4 Palmetto
S. Line Hunter N. End of Paving				
E		8.20	64.69	on cb
E		8.75	64.14	" Paving
☉		9.20	63.69	" "
W		9.22	63.67	" "
W		8.85	64.04	" cb
33' N of S. Line				
W		10.47	62.42	on N. end cb
35' N of S. Line				
E		11.2	61.7	
E		10.13	62.76	on N. end cb
50' N = N Line Hunter				
☉		12.3	60.6	
T.P.	0.61	260.73	12.77	260.12
00 = 75.08 N. of N. Line Hunter = P.C.				
☉		5.7	255.0	
+45.33 = P.C.C.		8.7	52.5	
+18.84 = E.C.		9.6	51.1	
+88.51 = P.C.		10.7	50.0	
T.P.	0.82	248.58 [✓]	12.97	247.76
+449.26 = E.C.		1.5	47.1	
+9498 = P.C.		4.8	43.8	
2+23.15 = P.C.C.	Brk	'	7.7	40.9
2+65.6 = E.C.		12.1	36.5	
T.P.	0.25	235.95	12.88	235.70

235.95

2+96.34 = P.C.

2.4 33.5

3+29.14 = P.C.C.

7.3 28.7

T.P.

0.28

224.06^c

12.17 223.78

3+71.12 = P.C.C.

1.8 22.3

4+20.83 = E.C.

8.0 16.1

4+77.73 = P.C. 10' R.O.M.W.

W
Q
E

12.8 211.3

13.2 10.9

13.2 10.9

T.P.

1.39

212.65

12.80 211.26

48' No of 4+77.73

ONE = A

5.6 207.1

B

6.6 206.1

C

9.0 203.2

D

9.8 202.9

E

9.0 203.2

F

4.0 208.7

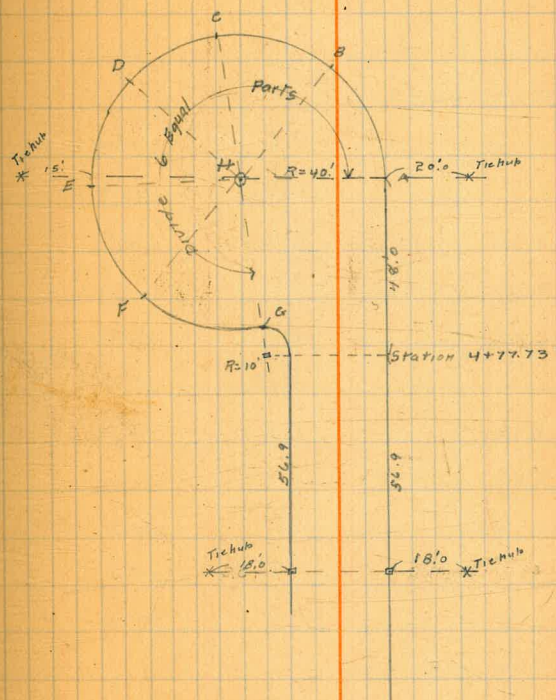
G

2.1 210.6

H = ET Banjo

6.0 206.7

40



Moore
sittlesLEVELS on 30' strip West of
ALLISON bet. Garnet & Diamond

41

one NW Return	7.55	27.05	19.50	Feldspar & ALLISON
		NL Garnet = 0+00		
W		10.1	19.0	
C		10.3	16.8	
E		10.6	16.5	
		50' N		
E		9.6	17.5	
C		9.4	17.7	
W		9.4	17.7	
		100' N		
W		8.1	19.0	
C		8.6	18.5	
E		8.8	18.3	
		150' N		
E		8.1	19.0	
C		7.9	19.2	
W		7.9	19.2	
		200' N		
W		7.2	19.9	
C		6.9	20.2	
E		6.7	20.4	
		225' N		
E		5.8	21.3	
C		6.0	21.1	
W		6.1	21.0	

270' W = SL FELDSTAR	=	50' wide
6.3	20.8	14' s/w
6.4	20.7	13' 1/4 s
6.5	20.6	
	Scb	
6.2	20.9	
6.2	20.9	
6.0	21.1	
	+3	
6.3	20.8	
6.6	20.5	
6.6	20.5	
	5 1/4	
5.9	21.2	
5.9	21.2	
5.9	21.2	
	4	
5.4	21.7	
5.3	21.8	
5.3	21.8	
	N 1/4	
6.1	21.0	
6.0	21.1	
5.7	21.4	
	+6	
6.2	20.9	

2705

C		6.2	209
E		6.4	207
	19		
E		5.8	213
C		5.5	216
W		5.6	215
	N dr		
W		5.5	216
C		5.5	216
E		5.4	215
	NL FELDSPAR = 0+00		
E		5.7	214
C		5.4	217
W		5.2	219
	50' N		
W		4.7	224
C		4.9	222
E		5.0	221
	100' N		
E		4.1	230
C		4.0	231
W		3.6	235
	150' N		
W		3.1	240
C		3.3	238
E		3.3	238

P. B. ESPLANADE 42

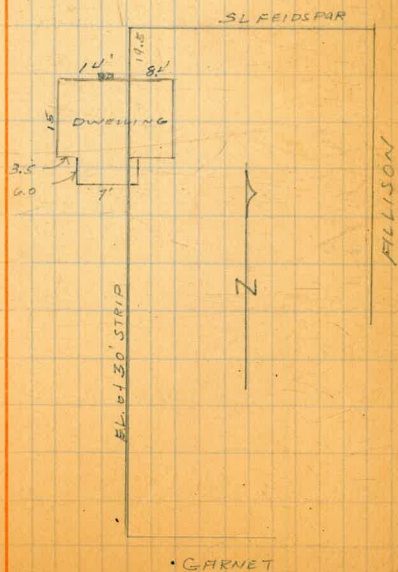
		200' N					
E			2.4				24.7
C			2.6				24.5
W			2.4				24.7
		215' N					
W			2.2				24.9
C			2.2				24.9
E			1.4				25.7
		240' N					
E			1.8				25.3
C			2.1				25.0
W			1.9				25.2
		270' N = SL EIMERHID				20' wide	
W			1.3				25.8
C			1.5				25.6
E			1.5				25.6
T.P.	8.31	33.79	1.57				25.48
		50'					
E			8.0				25.8
C			8.1				25.7
W			8.0				25.8
		5' 1/4					
W			7.7				26.1
C			7.9				25.9
E			7.9				25.9

3379

Pac. B. Esplanade. 43

E		7.6	26.2
C		7.6	26.2
W		7.5	26.3
	N/W		
W		7.0	26.8
C		7.3	26.5
E		7.2	26.6
	N/CB		
E		7.1	26.7
C		7.0	26.8
W		7.0	26.8
	NL EMERALD	0.00	
W		6.6	27.2
C		6.8	27.0
E		6.8	27.0
	50' N		
E		5.8	28.0
C		5.7	28.1
W		5.7	28.1
	100' N		
W		4.6	29.2
C		4.9	28.9
E		5.0	28.8
	150' N		
E		4.1	29.7
C		4.0	29.8

W		4.1	29.7
	200' N		
W		3.4	30.4
C		3.5	30.3
E		3.4	30.4
	250' N		
E		2.8	31.0
C		2.7	31.1
W		2.5	31.3
	SL DIAMOND		
W		2.3	31.5
C		2.5	31.3
E		2.4	31.4



BOUNDARY ST
 (Sec. 0 + 15' strip E of EL UNIV. to RR and St)

Moore
 Preston
 Walker

343.00

44

BM	956	343.00	333.14	UNIV. RR Boundary
				Sec A = NL UNIV.
EL +15		10.4	332.6	
				Sec B = 6100
EL +10		8.6	334.4	
+15		9.6	333.4	
				7' N
EL +12		7.9	335.1	
+15		9.0	334.0	
				13' N
EL		8.2	334.8	
+15		8.3	334.7	
				14' N
EL		8.1	334.9	
+8		7.8	335.2	
+15		10.5	332.5	
+20		11.3	331.7	
				26' N
EV		7.7	335.3	
+8		7.5	335.5	
+15		9.5	333.5	
+20		10.9	332.1	
				30' N
EL		7.6	335.4	
+15		7.1	335.9	

EL +15	50' N	6.8	336.2
	100' N		
EL +15		5.3	337.7
	150' N		
EL +15		4.2	338.8
	200' N		
EL +15		3.3	339.7
	250' N		
EL +15		2.2	340.6
	300' N		
EL +15		2.0	341.0
	350' N		
EL +15		1.7	341.3
	400' N		
EL +15		1.4	341.6
	450' N		
EL +15		1.5	341.5
	486' N		
EL +15		0.8	342.2
T.P. 1/2'	347.01	0.80	342.20
	500' N		
E +15		4.5	342.5
	535' N		
E +15		4.9	342.1

34701

	550 N		
E + 15		4.8	347.2
	557 N		
F + 15		3.4	348.6
	603 N = SU STATION		ST
E + 15		4.0	343.0
	5 CB		
E + 15		4.4	347.6
	5 1/4		
✓		4.8	342.2
	4		
✓		5.4	341.1
	N 1/4		
✓		5.6	341.4
	N CB		
✓		5.7	341.3
	N 1/2 = Sec E		
✓		6.7	340.1
	+5		
EL		6.4	340.6
+ 15		11.0	336.0
+ 20		12.2	334.8
	Sec F = 0 + 00		
E + 15		11.2	335.8
✓ + 20		12.0	335.0

34701

Boundary ST #5

	5' N		
EL + 15		11.2	335.0
✓ + 20		11.6	335.4
	35' N		
EL + 15		11.7	335.3
✓ + 20		12.3	334.7
	65' N		
EL + 15		12.5	334.5
✓ + 25		14.1	332.9
	100' N		
EL + 15		13.6	333.4
✓ + 25		15.6	331.4
	150' N		
EL + 15		11.4	335.6
✓ + 15		15.1	331.9
✓ + 25		18.4	328.6
	170' N		
EL + 15		14.0	333.0
✓ + 15		17.4	329.6
✓ + 20		17.5	329.5
✓ + 25		14.5	332.5
	200' N		
EL + 15		15.7	331.3
✓ + 15		14.0	333.0
✓ + 25		12.1	334.9

34701

225' N

EL + 5	15.8	331.2
✓ + 10	13.5	333.5
✓ + 15	12.8	334.2
✓ + 25	11.1	335.9

250' N

EL + 4	14.1	337.9
✓ + 8	14.0	333.0
✓ + 15	12.0	335.0
✓ + 25	9.8	337.2

270' N

EV + 4	12.6	333.4
✓ + 7	12.3	334.7
✓ + 15	11.7	335.3
✓ + 25	9.2	337.4

300' N

EV + 15	9.2	337.6
✓ + 25	6.7	340.3

320' N

EV + 15	6.6	340.4
✓ + 20	5.6	341.4

350' N

EL + 15	4.8	342.2
---------	-----	-------

375' N

EV + 15	3.7	343.3
---------	-----	-------

34701

Boundary 46

399.5' N = SL ANNA ST

EL + 15	3.7	343.3
---------	-----	-------

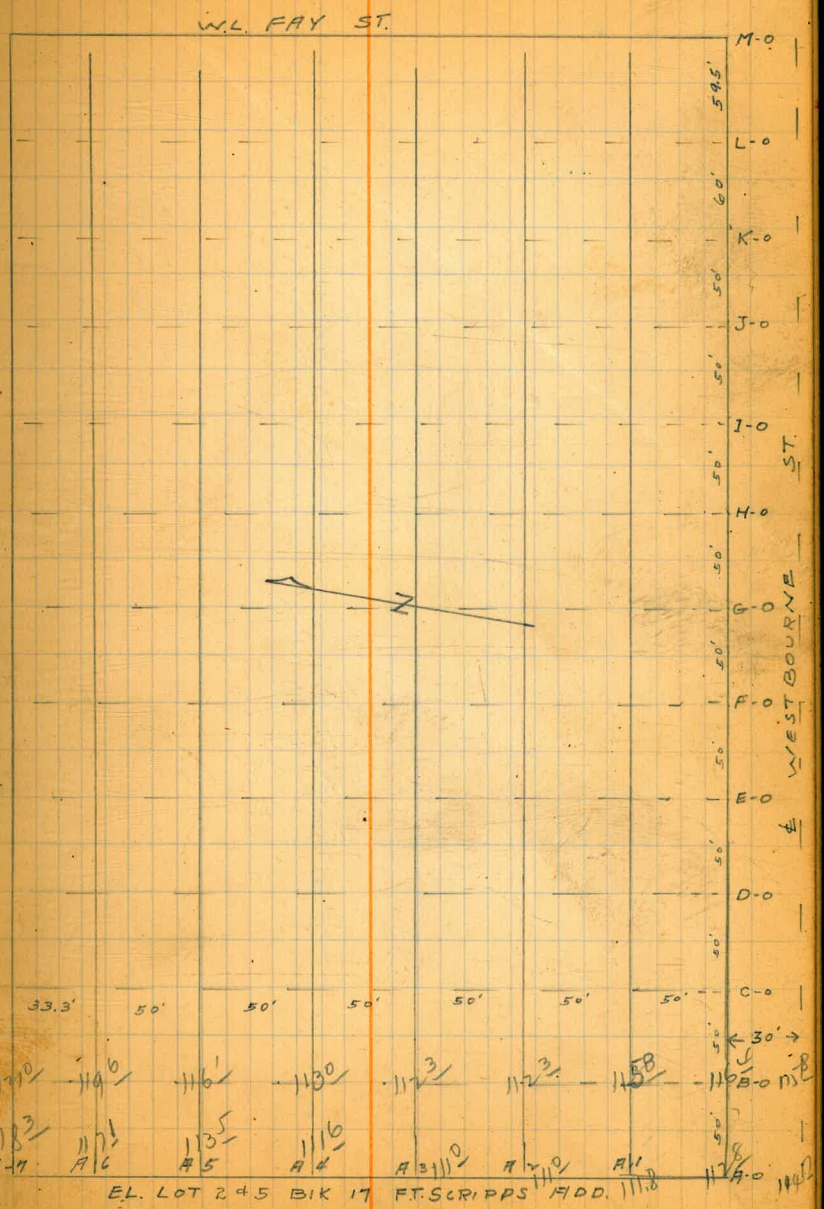
5/8/25

CROSS SECTION OF LA JOLLA JR. HIGH SCHOOL PROPERTY. Lot 2 J.G. BURNES ADD.

MOORE
PLANTATION
WALKER

SEPP	13.27	92.28		79.01	LA JOLLA DIV D Westbourne
T.P.	12.70	104.88	0.10	92.18	
T.P.	12.68	117.52	0.04	104.84	
T.P.	9.29	125.61	1.20	116.32	
A0 - 30 = Westbourne			10.9	114.7	
A0			12.8	112.8	
A1			13.8	111.8	
A2			14.6	111.0	
A3			14.6	111.0	
A4			14.0	111.6	
A5			12.1	113.5	
A6			8.5	117.1	
A7			7.3	118.3	
B7			4.6	121.0	
B6			6.0	119.6	
B5			9.5	116.1	
B4			12.6	113.0	
B3			13.3	112.3	
B2			13.3	112.3	
+30			12.6	113.0	
B1			9.8	115.8	
10' w. of Last			11.9	113.7	
B0			9.2	116.4	
10' w. of Last			11.2	114.4	
B0 +30 = Westbourne			9.8	115.8	

619.5
S.L. FERN GLEN



33.3' 50' 50' 50' 50' 50' 50' 50' 30' →

119.0 114.0 116.1 113.0 117.3 117.3 115.8 110.0

118.3 117.1 113.5 111.6 111.0 111.0 111.0 111.0

EL. LOT 245 BIK 17 FT. SCRIPPS ADD. 111.8

333.3'

125.61

C0-30 = 4	6.3	119.3
C0	5.9	119.7
C1	6.0	119.6
+15	6.8	118.8
+35	10.7	114.9
C2	11.1	114.5
C3	11.2	114.4
C4	10.9	114.7
C4+20	11.0	114.6
C5	9.7	115.9
C6	5.5	120.1
C7	2.4	123.2
D7	4.2	121.4
D4	7.4	118.2
D5	9.3	116.3
D4	9.4	116.2
D3	9.7	115.9
D2	9.8	115.8
+20	8.2	117.4
+40	3.6	122.0
D1	3.5	122.1
D0	3.4	122.2
+30 = 4	3.3	122.3
E0-30 = 4	0.7	124.9

125.61

E0	0.7	124.9	
E1	0.6	125.0	
+20	1.0	124.6	
E2	5.4	120.2	
E3	8.0	117.6	
E4	7.2	118.4	
E5	7.5	118.1	
E6	7.4	118.2	
E7	6.6	119.0	
F7	4.9	120.7	
F6	6.5	119.1	
F5	6.0	119.6	
F4	5.5	120.7	
F3	5.4	120.2	
+25	4.0	121.6	
+40	2.8	122.8	
F2	0.3	125.3	
TP 12.54	137.64	0.51	125.10
+15	10.7	127.0	
F1	10.3	127.3	
F0	10.0	127.6	
+30 = 4 Westborne	9.8	127.8	
G0-30 = 4	6.8	130.8	
G0	6.9	130.7	

13764

G1	9.2	128.4
G2	13.0	124.6
+15	14.3	123.3
10' E of Last	12.5	125.1
G3	14.9	122.7
10' E / /	12.6	125.0
G4	15.3	122.3
10' E / /	14.0	123.6
G5	16.3	121.3
10' E / /	14.0	123.6
G5+25	16.7	120.9
16' E of Last	15.8	121.8
25' E of G5+25	12.0	125.6
G6	17.0	120.6
8' E of Last	16.2	121.4
12' E of G6	14.5	123.1
G7	16.0	121.6
H7	12.3	125.3
H6	11.2	126.4
+20	9.4	128.2
H5	13.3	124.3
H4	12.8	124.8
H3	11.5	126.1
H2	10.4	127.2
H1	8.2	129.4

13764

49

H0	5.3	132.3	
H0+30 = Φ Westbourne	4.8	132.8	
I0 - 30 - ✓ ✓	2.2	135.2	
I0	2.7	134.9	
I1	6.1	131.5	
I2	8.2	129.4	
I3	9.7	127.9	
I4	10.9	126.7	
I5	11.2	126.4	
I6	7.2	130.4	
I7	7.5	130.1	
25' E of last	4.5	133.1	
I7	5.2	132.4	
J0	7.8	129.8	
J5	9.8	127.8	
J4	9.3	128.3	
J3	7.7	129.9	
J2	6.3	131.3	
J1	4.8	132.8	
J0	1.3	136.3	
+30 = Φ Westbourne	+0.3	137.9	
T.P. 973	147.22	0.15	137.49
K0 - 30 = Φ of Westbourne	7.9	137.3	

147.22

K ₀	10.4	136.8
K ₁	12.0	135.2
K ₂	15.1	132.1
K ₃	14.3	132.9
+25	13.6	133.6
K ₄	17.0	130.2
K ₅	17.1	130.1
K ₆	15.7	131.5
K ₇	14.0	133.2
L ₇	10.0	137.2
L ₆	11.1	136.1
L ₅	11.0	136.2
L ₄	12.2	135.0
L ₃	8.8	138.4
L ₂	10.5	136.7
L ₁	9.1	138.1
L ₀	7.2	139.9
+30 = E Westboro	5.6	141.6
M ₀₋₃₀ ✓ ✓ ✓	2.5	144.7
M ₀	3.5	143.7
M ₁	6.6	140.6
M ₂	4.7	142.5
M ₃	0.5	146.7
M ₄	4.2	143.0

147.22

58

+22	8.1	139.1
M ₅	7.8	139.4
M ₆	6.1	141.1
+23	5.1	142.1
M ₇	0.0	147.2
10' w of Last	5.0	142.2
T.P. 102'	157.09	0.3 ✓ 146.88
N ₇ on Westrail Jolla Elect. Co	3.7	153.38 E i' w of E FAX
N ₅ ✓ ✓ ✓ ✓	3.2	153.86 ✓ ✓ ✓ ✓
E Westboro ✓ ✓ ✓ ✓	3.8	153.25 ✓ ✓ ✓ ✓
on dirt ab w. Side FAX on E	4.7	152.9 of Fern Glen

Moore CURB LEVELS ON PARKVILLE COURT
 5/11/25 BIK 80 PARKVILLE ADD.

281.03

51

3EER 6.76 287.85 281.09 DWIGHT & ARIZONA 350'S

SL DWIGHT = 0+00

w cb 4.95 282.90 ✓

E cb 4.60 283.25 ✓

6'S

E cb 4.55 283.30 ✓

w cb 4.95 282.90 ✓

50'S

w cb 5.46 282.39 ✓

E cb 5.11 282.74 ✓

100'S

E cb 5.72 282.13 ✓

w cb 6.01 281.84 ✓

150'S

w cb 6.60 281.25 ✓

E cb 6.2 ✓ 281.61 ✓

200'S

E cb 6.88 280.97 ✓

w cb 7.19 280.66 ✓

250'S

w cb 7.82 280.03 ✓

E cb 7.4 ✓ 280.41 ✓

300'S

E cb 8.06 279.79 ✓

w 8.39 279.46 ✓

T.P. 1.95 281.03 8.77 279.08 ✓

w cb 2.17 278.86 ✓

E cb 1.78 279.25 ✓

400'S

E cb 2.42 278.61 ✓

w cb 2.82 278.21 ✓

450'S

w cb 3.44 277.59 ✓

E cb 3.03 278.00 ✓

500'S

E cb 3.63 277.40 ✓

w cb 4.13 276.90 ✓

550'S

w cb 4.61 276.42 ✓

E cb 4.27 276.76 ✓

600'S = H.L. MYRTLE

E cb 4.86 276.17 ✓

w 5.18 275.85 ✓

check to BIZ MYRTLE + ARIZONA 7.66 273.37 273.27

NOTE - Returns have 4' Radii

6/1/5
 Moore
 on BM 407 1818 1411
 CROSS SECTION of L ST
 EL 9th to W.L. 14th
 80' wide
 10' cbs
 NWBP
 L + 10th

	EL 9th		
N	6.5	112	✓
cb	6.5	112	✓
+ 10.7 = N Rail Santa Fe Spur	7.10	111	✓
N 1/4	7.0	114	✓
50' E			
N 1/4	6.2	116	✓
cb	5.8	114	✓
N	5.8	114	✓
100' E			
N	5.5	117	✓
cb	5.5	117	✓
N 1/4	6.2	110	✓
150' E			
N 1/4	5.2	112	✓
cb	5.1	131	✓
N	4.9	133	✓
185' E			
N	4.5	137	✓
cb	4.5	137	✓
N 1/4	5.1	132	✓
200' E = W.L. 10th			
N 1/4	4.9	133	✓
+ 2.2 = N Rail Santa Fe Spur	4.94	134	✓
cb	4.6	136	✓
N	4.4	138	✓

Note: - S side of L ST betw. 9th & 10th
 has Con'l Spur 10' wide

409 18.20 12.11 BM L + 10th

	EL 9th		
±	7.0	111	✓
1/4	7.5	102	✓
S cut	7.7	105	✓
50' E			
S cut	7.1	111	✓
1/4	6.6	116	✓
±	6.2	118	✓
100' E			
±	6.2	120	✓
1/4	6.3	119	✓
S cut	6.7	115	✓
150' E			
S cut	6.2	120	✓
1/4	5.7	125	✓
±	5.5	127	✓
185' E			
±	5.2	130	✓
1/4	5.2	130	✓
±	5.2	128	✓
S cut	6.6	116	✓
200' E = W.L. 10th			
S cut	6.1	121	✓
±	5.5	127	✓
1/4	5.2	130	✓
±	5.1	131	✓

18.20

EL 10th

18.2

N	3.9	143 ✓
cb	4.3	139 ✓
+12.3 = N Rail of Santa Fe Spur	4.80	134 ✓
1/2	4.8	134 ✓
C	5.0	137 ✓
1/2	5.0	138 ✓
cb	5.7	145 ✓
S	5.6	146 ✓
25' E		
S	5.0	13 ✓
cb	5.2	130 ✓
1/2	4.9	133 ✓
C	4.7	135 ✓
+ 10.4 = N Rail	4.9	133 ✓
1/2	4.3	132 ✓
+5	4.0	14 ✓
cb	4.0	142 ✓
N	4.0	142 ✓
50' E		
N	3.7	145 ✓
cb	4.0	142 ✓
1/2	4.1	141 ✓
+ 7.1 = N Rail	4.90	133 ✓
C	4.7	135 ✓
1/2	4.9	133 ✓

18.20

L ST

53

18.2

cb	5.1	131 ✓		
S	5.1	131 ✓		
TP	54'	18.93	4.68	135.2
	75' E			
<u>18.9</u>				
S	5.4	135 ✓		
cb	5.5	134 ✓		
1/2	5.2	137 ✓		
C	5.3	136 ✓		
+ 1.3 = N Rail	5.33	136 ✓		
+5	4.8	141 ✓		
1/2	4.8	141 ✓		
cb	4.6	143 ✓		
N	4.7	144 ✓		
100' E				
N	4.2	142 ✓		
cb	4.4	145 ✓		
1/2	4.4	145 ✓		
+8	4.5	144 ✓		
C	5.20	137 ✓		
+1 = N Rail	5.30	136 ✓		
1/2	5.0	139 ✓		
cb	5.4	135 ✓		
S	5.4	135 ✓		
110' E				
S	5.4	135 ✓		
cb	5.4	135 ✓		

18.93

	18.9	
1/4	4.9	140 ✓
+E	5.1	138 ✓
+11.8 = N Rail	5.25	138 ✓
C	5.1	138 ✓
+8	4.5	142 ✓
1/4	4.3	146 ✓
cb	4.3	146 ✓
N	4.0	149 ✓
	150' E	
N	3.8	152 ✓
cb	4.0	149 ✓
1/4	4.2	142 ✓
+7	4.3	146 ✓
C	4.8	141 ✓
+1.5 = N Rail	5.0	139 ✓
+10	4.8	141 ✓
1/4	4.8	141 ✓
cb	5.2	135 ✓
S	5.4	135 ✓
	190' E	
S	5.2	137 ✓
cb	4.7	142 ✓
1/4	4.2	145 ✓
+S	4.8	141 ✓
+11 = A/Rail	4.8	142 ✓
C	4.7	142 ✓

18.93

	18.9	L	ST
+E	4.2		145 ✓
1/4	4.5		144 ✓
cb	4.2		147 ✓
N	3.6		153 ✓
	200' E = W L 11+h		
N	3.7		15 ✓ ✓
cb	3.95		1498 ✓
+1	4.6		143 ✓
1/4	4.7		142 ✓
C	4.8		141 ✓
+1.7 = N Rail	4.73		1420 ✓
1/4	4.8		141 ✓
cb	5.0		139 ✓
S	5.2		137 ✓
	EL 11+h		
S	5.3		136 ✓
cb	5.47		1346 ✓
gut	5.9		130 ✓
1/4	5.0		139 ✓
+11 = N Rail	4.75		1418 ✓
C	4.7		142 ✓
1/4	4.8		141 ✓
gut	4.8		141 ✓
cb	3.95		1498 ✓
N	3.5		15.4 ✓

54

1893

50' E

~~189~~

N	3.8	15.1	✓
+U	3.9	15.0	✓
dt	5.3	13.6	✓
+1	5.8	13.1	✓
1/4	5.5	13.4	✓
+8	5.6	13.3	✓
C	5.9	13.0	✓
+2 = N Rail	6.2	12.9	✓
1/4	6.0	12.9	✓
dt	6.3	12.6	✓
S	6.3	12.6	✓
75' E			
S	6.8	12.1	✓
dt	6.8	12.1	✓
1/4	6.9	12.0	✓
+11.8 = N Rail	6.98	11.95	✓
C	6.8	12.1	✓
+4	6.2	12.7	✓
1/4	6.1	12.8	✓
+7	6.1	12.8	✓
dt	6.2	12.6	✓
+1	5.7	13.2	✓
+6	4.5	14.4	✓
N	4.3	14.6	✓

1893

L ST

55

100' E

~~1893~~

N	5.2	13.5	✓
+7	5.5	13.4	✓
+13	5.9	13.0	✓
dt	6.7	12.4	✓
1/4	6.5	12.4	✓
+8	6.7	12.4	✓
C	7.2	11.6	✓
+3.3 = N Rail	7.70	11.2	✓
1/4	7.5	11.4	✓
dt	7.3	11.6	✓
+5	7.4	11.5	✓
S	7.8	11.1	✓
125' E			
S	8.3	10.6	✓
dt	8.0	10.9	✓
1/4	8.2	10.5	✓
+6.7 = N Rail	8.48	10.45	✓
C	7.9	11.0	✓
+5	7.4	11.5	✓
1/4	7.1	11.8	✓
+8	6.9	12.0	✓
dt	7.1	11.8	✓
+1	6.6	12.3	✓
+10	5.8	13.1	✓
N	5.2	13.5	✓

18.93

	150' E	189	
N		5.8	131 ✓
+6		6.2	147 ✓
+13		7.3	11.6 ✓
cb		7.8	11.1 ✓
1/4		7.9	11.0 ✓
+8		8.1	10.8 ✓
C		8.5	10.4 ✓
+10.8 = N Rail		9.23	9.70 ✓
1/4		9.3	9.6 ✓
+8		9.4	9.5 ✓
cb		8.9	10.0 ✓
S		8.9	10.0 ✓

175' E

S		9.3	9.6 ✓
cb		9.5	9.4 ✓
+12 = N Rail		9.95	9.98 ✓
1/4		10.0	8.9 ✓
+6		9.1	9.5 ✓
C		9.3	9.5 ✓
1/4		9.2	9.2 ✓
cb		8.9	10.0 ✓
+1		8.0	10.9 ✓
N		6.9	12.0 ✓

195' E

N		7.3	11.6 ✓
---	--	-----	--------

18.93

L ST

54

cb		9.0	9.9 ✓
+1		10.0	8.9 ✓
	200' E = W L 14 + b		
N		9.0	9.9 ✓
cb	conn ct	9.50	9.4 ✓
got		10.3	8.6 ✓
1/4		10.2	8.7 ✓
C		10.2	8.7 ✓
1/4		10.6	8.3 ✓
+2.3 = N Rail		10.57	8.36 ✓
cb	conn ct	10.45	9.48 ✓
S		10.3	8.6 ✓
T.P. 441	11.97	11.37	7.56
	EL 12th	11.0	
N		3.3	8.7 ✓
cb	on conn ct	3.48	8.49 ✓
got		4.3	7.7 ✓
1/4		4.4	7.6 ✓
C		4.5	7.5 ✓
1/4		4.6	7.4 ✓
+2.4 = N Rail		4.8	7.4 ✓
	50' E		
cb + 10.6 = N Rail		5.4	6.6 ✓
1/4		4.9	7.1 ✓
C		4.5	7.5 ✓
1/4		4.4	7.6 ✓

11.97

			11.0	
d			2.8	72 ✓
#1			2.2	76 ✓
N			3.8	82 ✓
T.P.	6.40	13.36	5.01	6.96
	EL 12+h		13.4	
SL + 12 =	N edge of loading platform		5.7	72 ✓
S db			5.77	75.9 ✓
+6			6.2	70 ✓
	50' E			
SL + 12			5.5	79 ✓
db			5.6	78 ✓
+6			6.9	65 ✓
	100' E			
SV =	End of loading platform		5.7	72 ✓
+12	N edge of ✓		5.8	76 ✓
db			6.0	74 ✓
+6			7.3	61 ✓
+10.6 =	N Rail		7.25	61 ✓
1/2			6.2	70 ✓
c			6.1	73 ✓
1/2			6.1	73 ✓
db			6.7	62 ✓
+1			6.1	73 ✓
N			5.7	72 ✓
	150' E			
N			6.8	66 ✓

13.36

L S.T.

57

			13.4	
+12			6.7	62 ✓
db			7.2	62 ✓
1/4			6.7	62 ✓
c			6.7	62 ✓
+8			6.7	62 ✓
1/4			7.0	64 ✓
+7			7.8	56 ✓
db			7.2	62 ✓
S			6.8	66 ✓
	200' E =	N L 13+h		
S			7.5	59 ✓
db			7.8	56 ✓
+10.6	N Rail		8.20	52 ✓ = End of Santa Fé Spur
1/2			8.1	53 ✓
c			7.9	55 ✓
1/4			7.9	55 ✓
+12			8.1	53 ✓
db	center		7.40	60 ✓
N			7.2	62 ✓
T.P.	7.56	13.50	7.22	59.4
	EL	13+h		
N			7.2	63 ✓
db			7.6	59 ✓
1/4			7.9	56 ✓
c			7.9	56 ✓
1/4			8.2	53 ✓

13.50

cb		8.1	54	/
S		8.1	54	/
	15' E			
S		7.9	56	/
cb		7.7	58	/
1/4		7.0	65	/
c		6.4	71	/
1/4		6.7	68	/
cb		6.6	69	/
N		6.9	66	/
	50' E			
N		6.0	75	/
cb		6.0	75	/
1/4		6.1	74	/
c		5.8	77	/
1/4		6.3	72	/
cb		7.0	65	/
S		7.3	62	/
	71' E			
S		6.9	66	/
cb		6.3	72	/
1/4		6.0	75	/
c		5.4	81	/
1/4		5.6	79	/
cb		5.6	79	/
+ 1/4 = pepper tree 14" DIAM				
N		5.3	82	/

13.50

ST.

58

	94' E			
			135	
N			4.8	87
	+ 9.5 = pepper tree 16" DIAM			
cb		4.9		86
1/4		5.1		84
c		4.7		88
1/4		5.7		78
cb		6.1		74
S		6.1		74
	141' E			
S		4.8		82
cb		4.8		82
1/4		4.8		87
c		4.3		92
1/4		4.3		92
cb		4.0		95
	+ 4.5 = pepper tree 16" DIAM			
N		3.8		97
	160' E			
N		3.2		103
	+ 9.5 = pepper 16" DIAM			
cb		4.0		95
1/4		4.7		88
c		4.6		89
1/4		4.6		89
cb		4.6		89

1350

L S T. 59

S			4.3	92	✓
	181' E				
S			4.6	89	✓
cb			4.6	89	✓
1/4			4.7	88	✓
c			4.5	90	✓
1/4			4.7	88	✓
cb			4.5	90	✓
+ 4.5' = pepper 20" DIAM					
N			3.6	99	✓
200' E = WL 14th					
N			3.9	96	✓
cb			4.1	94	✓
1/4			4.7	88	✓
1/4			4.7	88	✓
c			4.8	87	✓
1/4			4.8	87	✓
1/2			5.1	85	✓
cb			4.8	87	✓
S			4.5	90	✓
T.P.	4.63	13.56	4.57	8.93	✓
check to B.M. Imperial 4 1/4th					
			6.73	6.83	6.93

Moore
6/15/85
FILLEE XSEC ELCAJON
Below Sisson & Central
BLK 28 TERALTA

To ORANGE

15' wide

ELCAJON
CENTRAL

Map of the Re-sub of BLK 28 KVL Teralta ESD book P-390
Map 1037

SWBD 7th 371.88

364.66

250' S

SL ELCAJON = 0+00

F	6.6'	365.27	on paving
C	6.8'	365.04	✓ ✓
W	6.47	365.41	✓ ✓

F	5.2	366.7
---	-----	-------

C	5.0	366.9
---	-----	-------

W	5.3	366.6
---	-----	-------

25' S

300' S

W	6.0	365.9
---	-----	-------

W	5.2	366.5
---	-----	-------

C	5.5	366.4
---	-----	-------

C	5.2	366.5
---	-----	-------

E	5.2	366.7
---	-----	-------

E	5.3	366.6
---	-----	-------

350' S

50' S

F	5.6	366.3
---	-----	-------

E	4.6	367.3
---	-----	-------

C	5.9	366.0
---	-----	-------

C	5.1	366.8
---	-----	-------

W	6.3	365.6
---	-----	-------

W	5.0	366.9
---	-----	-------

400' S

100' S

W	6.3	365.6
---	-----	-------

W	5.1	366.8
---	-----	-------

C	6.1	365.8
---	-----	-------

C	5.2	366.5
---	-----	-------

E	6.0	365.9
---	-----	-------

E	5.3	366.6
---	-----	-------

450' S

150' S

E	5.7	366.2
---	-----	-------

F	5.2	366.5
---	-----	-------

C	5.9	366.0
---	-----	-------

C	4.8	367.1
---	-----	-------

W	6.3	365.6
---	-----	-------

W	4.7	367.2
---	-----	-------

T.P. 478 370.73 59.2 365.95

200' S

500' S

W	4.7	367.2
---	-----	-------

W	5.2	365.5
---	-----	-------

C	4.7	367.2
---	-----	-------

C	4.8	365.9
---	-----	-------

E	4.9	367.0
---	-----	-------

E	5.1	365.6
---	-----	-------

390.73

41

507'S

E - W = N end of 6 door Garage 5.0 ↓ 365.69 Conc. floor

543'S

W - 1 & Garage 5.3 365. ↓ dirt ✓

C 5.1 365.6

E 5. ↓ 365.3

563'S

E - W = S end of 6 door Garage 5.08 365.65 Conc. floor

E 5.2 365.5

C 5.2 365.5

W 5. ↓ 365.3

600'S

W 5.8 364.9

C 6.0 364.7

E 5.7 365.0

607'S = N L ORANGE AVE

E on Alley returned 6.29 364.44

C 6.2 364.5

W ✓ ✓ ✓ 6.46 364.27

Front 51 25cc
 from N. Line Spruce To S. Line Thorr

4/21/25
 miles

240.48

12

B.M. 239.48
 5.52 ~~246.48~~ ✓ 233.96
 spruce
 234.91 SPINE FRONT

150' N

0.62 N. Line Spruce
 E. Eb 5.52 234.0
 gutter 6.3 233.0
 1/4 6.3 233.7
 C 6.4 234.1
 1/4 6.5 234.0
 cl 7.1 233.4
 H 7.8 234.7
 W 7.4 233.1
 7.2 233.3

orient cl

W 5.7 234.6
 cl 6.5 234.0
 1/4 6.0 234.5
 C 5.0 235.5
 1/4 5.1 235.4
 E gutter 5.1 235.4

Errors in B.M.
 Elevs are 1' lower
 than shown.

200' N

50' N
 W 5.8 234.7
 cl 7.2 233.3
 1/4 6.8 233.7
 C 5.9 234.6
 1/4 5.7 234.8
 E gutter 5.9 234.6

C cl 4.17 236.3 orient cl
 gutter 4.8 235.7
 1/4 4.7 235.8
 C 5.0 235.5
 1/4 5.5 235.0
 cl 5.7 234.8
 W 5.3 235.7

223' N

100' N
 E cl 4.80 235.7 orient cl
 gutter 5.7 234.8
 1/4 5.5 235.0
 C 5.5 235.0
 1/4 6.3 234.4
 cl 6.8 233.7
 H 6.5 234.0
 W 6.4 234.1

W 4.3 236.7
 cl 4.0 236.5
 1/4 4.2 236.3
 C 4.5 236.0
 1/4 4.6 235.9
 E gutter 4.5 236.0

230' N

E gutter 4.6 235.9
 1/4 4.5 236.0
 C 4.3 236.7
 1/4 3.5 237.0

240.48

+7	3.9	436.6
cb	8.9	431.6
w	7.9	437.6
+5	5.3	435.4

R40' N ✓

-20	14.7	425.8
w	15.2	425.3
cb	13.4	427.1
1/4	3.3	437.2
c	3.9	436.6
1/4	4.3	436.4
E Guller	4.4	436.1

R50' N ✓

E Guller	4.4	436.1
1/4	4.2	426.3
c	3.9	436.7
+5	2.5	438.0
1/4	6.1	434.6
cb	16.1	424.4
+3	18.3	422.7
w	18.8	421.7
+30	21.5	419.0

R65' N ✓

-40	28.6	411.9
-20	28.0	412.5
w	25.1	415.4

Front

63

240.48

cb	24.6	415.9
1/4	9.0	431.5
+10	2.7	437.8
c	2.9	437.6
+3	3.8	436.7
1/4	4.2	436.3
Guller	4.4	436.1

R75' N ✓

Guller	4.8	436.2
1/4	4.0	436.5
c	3.3	437.2
+4	1.9	438.6
1/4	7.2	433.3
cb	22.0	418.5
w	29.0	411.5
+10	21.5	409.0
+30	33.0	407.5
+50	35.0	405.5

R85' N ✓

-40	39.7	400.8
-35	38.0	404.5
-10	34.3	406.7
w	29.6	410.9
cb	19.0	421.5
1/4	12.0	426.5
c	3.5	437.0

240.49

+4	2.5	438.0
+8	3.5	437.0
1/4	3.8	436.7
E gutter	4.4	436.1

300.5 N=S Line Thorn ✓

E cl	3.48	437.0	ancient cl
gutter	4.0	436.5	
1/4	3.6	436.7	
C	2.7	437.8	
+4	2.6	437.9	
1/4	11.0	449.5	
cl	19.2	441.3	
W	26.6	413.9	
+20	35.6	404.9	
+35	43.0	197.5	
+68	51.0	189.5	

314.5 N=S cl of Thorn

-60	43.0	197.5
-35	39.6	400.9
-30	37.2	403.3
-15	34.4	404.1
W	27.5	413.0
cl	19.5	441.0
1/4	10.0	430.5
C	3.1	437.4
+4	2.8	437.7

240.49

Front

64

+7	3.4	437.1
1/4	3.9	436.6
cl	3.5	437.0

60'S of THORN	cl OK
50'S " "	cl 0.09 Low
35'S " "	" 0.22 "
25'S " "	" 0.33 "
15'S " "	" 0.31 Low

165'S of Upas	cl OK
145'S " "	" 0.20 Low
100'S " "	cl 0.34 Low
90'S " "	" 0.63 Low
63'S " "	" 0.45 "
46'S " "	" 0.10 "
24'S " "	" 0.07 "

Front + Thorn N.E. + S.E. 14'x14' Returns "

" + Upas S.E. 14'x14' Return in

" + Walnut SE 14'x14' " "

" + " SW 14'x15' x 30' E+W Return in 36' Roadway

80' wide
20' dia
10' 1/4

Hornblend X See
from E. Line Ingraham 100' E

6/26/25

68.67

65

B.M. 5.45 68.67
00 = E. Line Ingraham 63.22

Bolt head SW
Garrett's Invention

S	5.1	63.6 ✓
cl	5.2	63.5 ✓
+4	5.6	63.1 ✓
1/4	5.6	63.1 ✓
E	5.5	63.2 ✓
1/4	5.6	63.1 ✓
+5	5.7	63.0 ✓
cl	4.9	63.8 ✓
N	4.3	64.4 ✓

50' E

N	2.8	65.9 ✓
+3	4.0	64.7 ✓
+19	4.1	64.6 ✓
cl	4.8	63.9 ✓
1/4	4.8	63.9 ✓
E	4.8	63.9 ✓
1/4	5.1	63.6 ✓
cl	5.1	63.6 ✓
+4	4.3	64.4 ✓
S	4.8	63.9 ✓

100' E

S	4.1	64.6 ✓
+15	3.9	64.8 ✓
cl	5.0	63.7 ✓
1/4	4.6	64.1 ✓

E	4.3	64.4 ✓
1/4	4.3	64.4 ✓
+6	4.8	64.2 ✓
cl	3.5	65.2 ✓
+19	3.2	65.5 ✓
N	2.2	66.5 ✓

130' E

N	1.9	66.8 ✓
+2	3.0	65.7 ✓
cl	3.3	65.4 ✓
+5	3.9	64.8 ✓
1/4	3.8	64.9 ✓
E	3.7	65.0 ✓
1/4	4.3	64.9 ✓
cl	4.7	64.0 ✓
+2	4.0	64.7 ✓
S	3.8	64.9 ✓

160' E

S	3.3	65.4 ✓
+5	3.9	64.8 ✓
+18	3.8	64.9 ✓
cl	4.3	64.4 ✓
1/4	4.2	64.5 ✓
E	3.6	65.1 ✓
1/4	3.5	65.2 ✓
+7	3.6	65.1 ✓

68.67

d	3.5	65.2 ✓
f1	2.6	66.1 ✓
718	2.6	66.1 ✓
N	1.2	67.5 ✓

Hornblend

66

20' wide X Sec E & W Alley
 BIK 155 Pacific Beech

6/24/25
 under

T.P.	0.75	31.74	30.99	on return SW. Alison & Diamond
				on apt cl
				on apt cl
N		2.75	28.99	
N		3.4	28.3	
E		3.4	28.3	
S		3.5	28.2	
S		3.15	28.59	
	7' W			
S		4.2	27.5	
E		4.1	27.6	
N		3.9	27.8	
	50' W			
N		3.8	27.9	
E		3.7	28.0	
S		4.2	27.5	
	80' W			
S		4.1	27.6	
E		3.6	28.1	
N		3.8	27.9	
	100' W			
N		3.4	28.3	
E		3.0	28.7	
S		3.2	28.5	
	715' W			
S		3.8	27.9	
E		3.2	28.5	
N		3.3	28.4	

31.74

67

	150' W		
N		3.3	28.4
E		3.3	28.4
S		3.8	27.9
	200' W = E. Line N & S. Alley		
S		3.4	28.3
E		3.0	28.7
N		3.1	28.6

X Sec N & S. Alley
 20' wide BIK 155 Pacific Beech

			00 = S. Line Diamond
E		1.60	30.14 on apt cl
E		0.7	31.0
E		0.6	31.1
W		0.6	31.1
W		1.59	30.15 on apt cl
	50' S		
W		1.5	30.2
E		1.5	30.2
E		1.6	30.1
	100' S		
E		2.5	29.2
E		2.5	29.2
W		2.5	29.2

31.74

	150' S		
W		3.3	28.4 ✓
E		3.3	28.4 ✓
E		3.5	28.2 ✓
	200' S		
E		4.2	27.5 ✓
E		4.3	27.4 ✓
W		4.3	27.4 ✓
	235' S		
W		5.0	26.7 ✓
E		5.0	26.7 ✓
E		5.1	26.6 ✓
	270' S = N. Line Emerald		
E		6.13	25.61 ✓ orient. d.
E		5.8	25.9 ✓
E		5.9	25.8 ✓
W		5.7	26.0 ✓
W		6.30	25.44 ✓ orient. d.
	<u>X-sec N-S. Alley 192, Pac. Beh.</u> 007 S. Line Emerald		
W		7.9	23.8 ✓
E		7.8	23.9 ✓
E		7.7	24.0 ✓
E		7.58	24.16 ✓ orient. d.
	50' S		
E		9.1	22.6 ✓
E		9.2	22.5 ✓
W		9.4	22.3 ✓

31.74

	100' S		
W		10.1	21.6 ✓
E		10.4	21.3 ✓
E		10.1	21.6 ✓
	115' S		
E		10.9	20.8 ✓
E		10.7	21.0 ✓
W		10.5	21.2 ✓
	150' S		
W		10.9	20.8 ✓
E		11.3	20.4 ✓
E		11.6	20.1 ✓
	200' S		
E		12.3	19.4 ✓
E		11.9	19.8 ✓
W		11.6	20.1 ✓
	235' S		
W		11.6	20.1 ✓
E		12.0	19.7 ✓
E		12.3	19.4 ✓
	270' S = N. Line Field spar		
E		10.85	20.89 orient. d.
E		12.1	19.6 ✓
E		12.0	19.7 ✓
W		11.9	19.8 ✓

B.M.	7.30	241.26	233.96	N.E. Front + Spruce
		S 1/4 of Thorn ^{14' elev} 13' 1/4s		
E		4.3	737.0	
cl		4.9	736.4	
1/4		5.3	736.0	
E		5.2	736.1	
1/4		12.6	728.7	
cl		19.8	721.5	
W		25.8	715.5	
+8		32.8	708.5	
+16		32.0	709.3	
+23		40.0	701.3	
+40		35.5	705.8	
		E Thorn		
-40		32.4	708.9	
-25		28.4	714.9	
-20		35.3	706.0	
-15		25.8	715.5	
W		22.0	719.3	
+9		22.6	718.7	
cl		19.3	727.0	
1/4		13.0	728.3	
E		5.3	736.0	
1/4		5.2	736.1	
cl		4.6	736.7	
E		3.8	737.5	

	N. 1/4	
E	4.0	737.3
cl	4.5	736.8
1/4	5.0	736.3
C	4.8	736.5
1/4	6.8	734.5
cl	11.2	730.1
W	19.0	724.3
+8	20.6	720.7
+15	25.0	716.3
+20	23.8	717.5
+35	27.8	713.5
	N. cl	
-30	22.3	718.0
-15	18.1	723.2
-14	22.4	718.9
W	15.0	726.3
cl	5.1	736.2
1/4	4.6	736.7
C	4.5	736.8
1/4	4.9	736.4
S cl	4.6	736.7
	80' wide 14' chon E 36' Roadway Thorn 30' " " W 9' 1/4s	
Ech	4.24	737.1 orient cl
Egalle	4.9	736.4
1/4	4.7	736.6
C	4.6	736.7

241.26

00 CCH

w 1/4	4.0	237.3
cl	3.6	237.7
+20	4.5	236.8
30' N		
w cl-20	3.6	237.7
cl-17	1.8	239.5
cl	2.8	238.5
1/4	3.5	237.8
c	4.3	237.0
1/4	4.4	236.9
gutter	4.4	236.9
65' N		
gutter	4.1	237.7
1/4	3.9	237.4
c	3.9	237.4
1/4	3.0	238.3
cl	2.8	238.5
+14	1.4	239.9
+20	3.9	237.4
100' N		
w cl-30	14.2	247.1
" " - 20	8.5	237.8
" " - 10	1.9	239.4
cl	1.8	239.5
1/4	2.7	238.6
c	3.3	238.0

241.26

Front ST

70

1/4		3.4	237.9
gutter		3.6	237.7
135' N			
gutter		3.3	238.0
1/4		3.0	238.3
c		2.5	238.8
1/4		2.0	239.3
+3		1.7	239.6
T.P.	5.96	244.93	2.29 238.97
w cl		9.5	235.4
+20		22.7	244.7
+60		33.7	241.7
155' N			
w cl-70		43.3	201.6
" " - 50		39.0	205.9
" " - 40		34.7	210.7
" " - 20		24.3	218.6
w cl		9.9	235.0
+5		5.9	239.0
1/4		6.4	238.5
c		6.3	238.6
1/4		6.5	238.4
gutter		6.8	238.1
200' N			
gutter		6.6	238.3
1/4		6.1	238.8

244.93

200' N COM

c	5.7	739.7
1/4	5.1	739.8
+3	5.0	739.9
cl	10.4	734.5
+20	24.0	720.9
+40	34.0	710.9
+60	37.0	707.9

225' N ✓

-60	31.4	713.5
-25	23.8	721.1
-20	20.8	724.1
cl	6.6	738.3
+3	4.5	740.4
1/4	4.3	740.6
c	5.3	739.6
1/4	5.7	739.7
gutter	6.0	738.9

249' N ✓

gutter	5.6	739.3
1/4	5.1	739.8
c	4.7	740.7
1/4	4.4	740.5
cl	4.7	740.7
+9	5.9	739.0
+20	13.3	731.6
+30	19.7	725.7
+40	19.8	725.1

244.93

250' N

Wcb-20	5.7	739.7 on lawn
cl	5.3	739.6 " "
+2	4.2	740.7
1/4	4.4	740.5
c	4.8	740.1
1/4	5.2	739.7
gutter	5.5	739.4

300' N = S. line

21 pas

80' wide

14' dia

13' 1/4

Est gutter	3.08	741.0 on lawn
gutter	4.3	740.6
1/4	4.3	740.6
c	4.3	740.6
1/4	3.9	741.0
+8	4.1	740.8
cl	4.6	740.3 on lawn
+20	4.5	740.4

S. cl ✓

-20	4.4	740.5
cl	4.4	740.5
1/4	3.7	741.7
c	4.0	740.9
1/4	3.9	741.0
cl	4.1	740.8
c	3.8	741.1
S. 1/4 ✓		
c	3.2	741.7
cl	3.6	741.3

24493

1/4	3.7	241.2	
E	3.6	241.3	
1/4	3.7	241.2	
cl	4.1	240.8	on lawn
+20	4.2	240.7	" "
	✓		
-20	4.4	240.5	on lawn
cl	4.0	240.9	" "
1/4	3.7	241.2	
E	3.4	241.5	
1/4	3.4	241.5	
cl	3.3	241.6	
E	2.9	242.0	
	R'N of 4		
w cl - 20	4.8	240.1	
w cl	3.9	241.0	
	N 1/4 ✓		
E	2.9	242.0	
cl	3.1	241.8	
1/4	2.9	242.0	
E	3.0	241.9	
1/4	3.5	241.4	
cl	3.5	241.4	
+5	4.2	240.7	on lawn
+20	4.7	240.2	" "

244.93

N. cl ✓

74

-20	4.4	240.3	on lawn
-5	4.5	240.4	" "
cl	3.2	241.7	
1/4	3.3	241.6	
E	2.9	242.0	
1/4	2.8	242.1	
cl	3.0	241.9	
E	2.5	242.4	
	00 = N. Line U pas		
E	2.1	242.8	
cl	2.7	242.2	
1/4	2.5	242.4	
E	2.6	242.3	
1/4	3.1	241.8	
cl	3.0	241.9	
+5	4.4	240.5	on lawn
+20	4.4	240.5	" "
T.P.	8.72	251.44	2.21 242.72
	56' N ✓		
-20	9.4	241.6	
cl	9.2	242.2	
1/4	8.4	242.8	
E	8.5	242.9	
1/4	8.1	243.3	
cl	8.5	242.9	
E	7.9	243.5	

251.44

	60' N ↓	
E	7.7	743.7
cl	8.3	743.1
1/4	8.0	743.4
C	8.5	742.9
1/4	9.3	741.1
cl	10.3	741.1
+20	10.4	741.0

115' N ↓

-20	9.7	741.7
cl	9.2	742.7
1/4	8.4	743.0
C	7.4	744.0
1/4	7.2	744.7
cl	6.8	744.6
+4	7.2	744.7
E	7.0	744.4

126' N ↓

E	6.7	744.7
+10	6.4	744.6
cl	6.2	745.7
1/4	6.4	745.0
C	7.0	744.4
1/4	7.8	743.6
cl	8.2	743.7
+26	8.2	743.7

251.44

73

135' N ↓

-20	8.2	743.7
cl	7.9	743.5
1/4	6.9	744.5
+6	5.7	745.7
C	5.6	745.8
1/4	5.3	746.1
cl	5.3	746.1
+4	5.7	745.7
E	6.1	745.3

151' N ↓

E	3.9	747.5
+9	3.8	747.6
cl	3.0	748.4
1/4	2.8	748.6
C	2.7	748.7
1/4	3.1	748.3
cl	4.5	746.9
+20	4.2	747.7

159' N ↓

-20	1.3	750.1
cl	1.5	749.9
1/4	1.9	749.5
C	1.9	749.5
1/4	2.3	749.7
cl	2.5	748.9
E	2.0	749.4

166. N = S. Line ✓

E	0.8	450.6	
cl	0.84	450.6	on emt cl No Yardage
cl	1.5	449.9	
1/4	1.3	450.1	
E	1.3	450.1	
1/4	1.4	450.0	
cl	1.30	450.1	on emt cl
W	1.3	450.1	

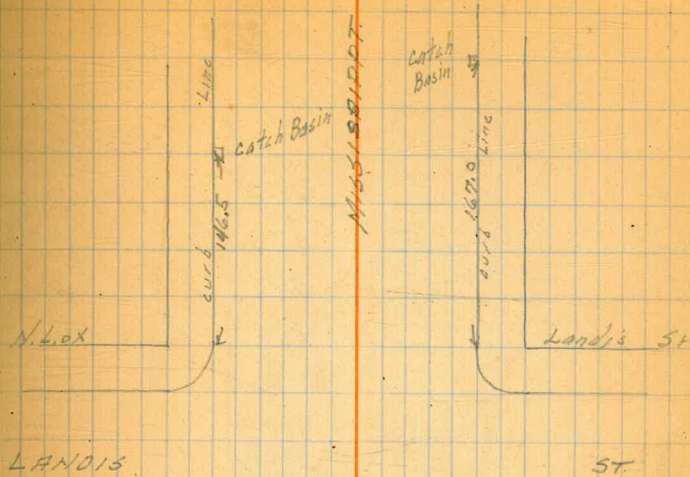
9/27/21

Gregory

Location & Elevations of
C. Basins on MISSISSIPPI
NORTH OF LANDIS

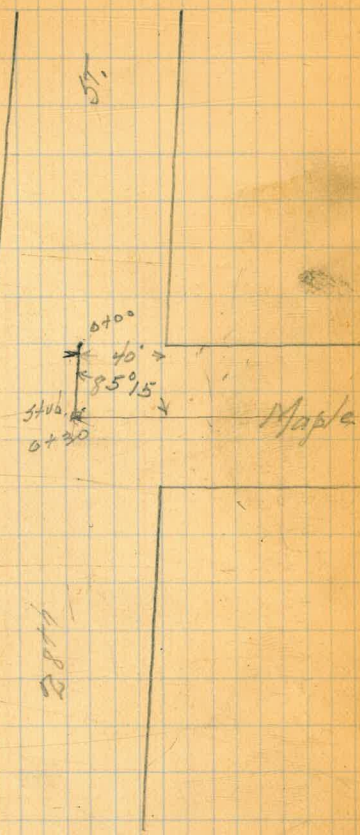
	110	272.61	8.28	271.51	SE Landis & Miss
Top of Frame East Curb Line @ 167' N. of Landis			6.17	263.63	
Top of Curb @ 167' N. of Landis				266.44	
Top of Catch Basin West CB Line			8.57	262.04	

75

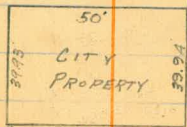
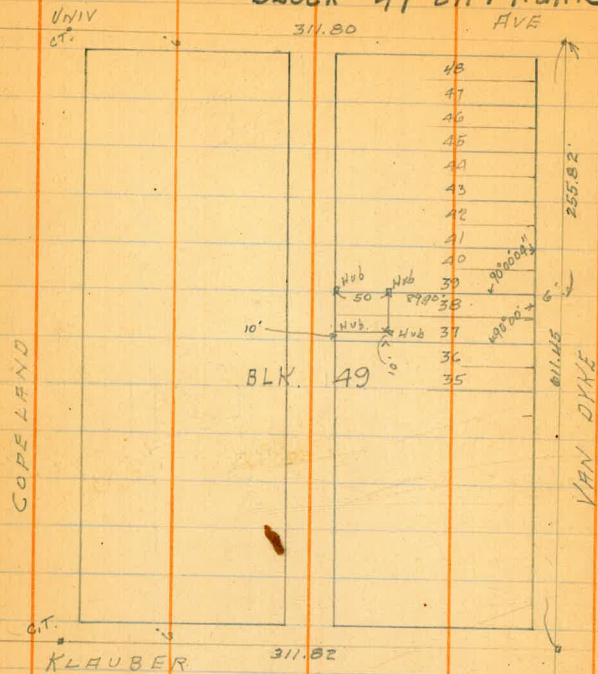


8/27/25 Sewer Levels on 4.2855+2
 from N.W. Maple to d Maple thence East
 on d Maple to M.H. in Canon

	5.35	300.30	224.95	32 NE 28- Palm
	0.31	290.15	10.46	289.84
	0.36	278.03	12.48	277.67
	1.56	266.56	13.03	265.00
0+00			<u>266.6</u> 4.5	261.1 ✓
0+30 Δ	94.45' L d Maple		9.34	257.44 on stub
+50			9.3	257.3 ✓
1			8.3	258.3 ✓
+50			10.9	255.7 ✓
T.P.	0.77	254.32	13.01	253.55
2			<u>254.3</u> 2.5	251.8 ✓
+25			5.1	249.2 ✓
+50			9.2	245.1 ✓
+60			10.7	243.6 ✓
T.P.	0.63	242.30	12.65	241.67
3			<u>242.3</u> 6.8	255.5 ✓
+15			10.9	231.2 ✓
TP	0.82	230.32	12.80	229.50
+30			<u>230.3</u> 6.6	223.7 ✓
+35			10.5	219.8 ✓
T.P.	1.45	219.52	12.25	218.07
+45			<u>219.5</u> 4.1	215.2 ✓
+50			6.6	212.9 ✓
+57			9.4	210.1 ✓
+60.8 = M.H.			9.85	209.67 Top M.H.
+60.8			14.51	205.01 Flow Line



10/23/71
Grap of Survey of the West 50' of
Lots 37 & 38 Except the W 50'
of 50. 10' of Lot 37 BLK 49 City Heights
BLOCK 49 CITY HEIGHTS



Tank Tower
sets off City
property this much.

Adams - Madison CROSS SECTION OF ALLEY 20' wide
30th - OHIO BIK II UNIV HTS.

Moore
11/21/55

394.35

78

SEBP	53'	394.35	389.04	Adams + 30th
		SL Adams = 0000		
W	on paving	46'	389.74	
C	✓	4.88	389.47	
E	✓ ✓	4.56	389.79	
	25'S			
E		3.7	390.6	
C		3.5	90.8	
W		3.8	90.5	
	50'S			
W		3.9	90.4	
E		3.7	90.6	
E		4.0	90.3	
	100'S			
E		4.1	90.2	
C		4.2	90.1	
W		4.1	90.2	
	106'S			
E	-6' E Double Garage	4.0	90.3	Cone floor
	150'S			
W		4.2	90.1	
C		4.5	89.8	
E		4.6	89.7	
	162'S			
W	-2' Double Garage	4.3	90.0	dirt floor

200'S		
E	4.7	389.6
C	4.7	89.6
W	4.6	89.7
	250'S	
W	4.7	89.6
C	4.8	89.5
E	4.5	89.8
	300'S	
E	5.1	89.2
C	5.2	89.0
W	5.3	89.0
	350'S	
W	5.6	88.7
C	5.7	88.6
E	5.5	88.8
	400'S	
E	5.8	88.5
C	5.7	88.6
W	5.7	88.6
	450'S	
W	6.0	88.3
C	5.9	88.4
E	5.7	88.6
	500'S	
E	5.8	88.5

394.35

79

V		5.7	388.6
W		5.9	88.4
	550'S		
W		6.1	88.2
C		5.9	88.4
E		5.8	88.5
	575'S		
E		5.9	88.4
C		6.3	88.0
W		6.2	88.1
	600'S = NW Madison		
W	ON ALLEY Return	6.91	387.44
C		7.2	387.15
E	✓ ✓ ✓	6.71	387.64

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in

left column and top row. The number in body of table in same row and column gives distance

level estimate the difference in elevation between the side stake and slope stake lower target by this amount if cut, elevation. Add this amount to cut or fill and find distance in table. Set up rod at target. If it does not make the right adjustment

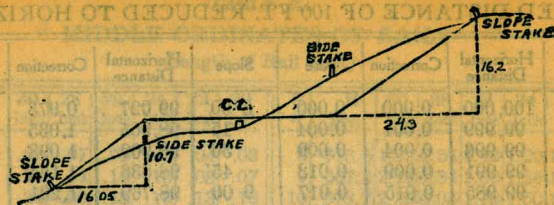
IMPROVED TABLES
AND
INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

11905
220
43805

S of = E 37.5 of 21.0 1/4 25.1

SL = E 44.5 of = 36.0 1/4 27.1

8d N. E ✓ ORANGE & EL CAJON

1.9 S.W. ✓ Alley back of Court

23.5 S. E ✓

27.9 N. W. L ✓

50.6 N. BL DRIVE

65.1 N. W. L ✓

80.2 S. W. ✓

105.

130.35

35.
15.7
19.3

17.5
15.7
1.8

297
180

643

1565

150
103.2
10
33.3

247
3.5
342.5

338

17.2
5.83
11.29
17.7
16.07
6.30
9.77
6.0
10.2
9.27
8.5

46.80	21.10	57.72	22.37
43.86	3.51	63.64	24.77
<u>290.66</u>	22.14	<u>121.40</u>	<u>157.84</u>
45.35	<u>247.08</u>	60.70	28.67
23.51	25.51		
68.84	20.83	30.87	
19.72	25.85	6.36	
88.56	46.68	37.23	
60.70	27.23	46.60	
149.26	38.39	<u>83.97</u>	
45.72	32.81	41.95	
194.98	49.22	40.35	
25.67	51.20	43.57	
225.65	<u>99.42</u>	<u>182.86</u>	
41.95	49.71	47.93	
<u>265.60</u>		84.05	
30.74		<u>76.5</u>	
296.38		58.70	
32.81			
329.19		100.26	
41.93		1.68	
371.12		<u>101.94</u>	
49.71		36.90	
420.83		45.04	
50.92		2.46	
<u>477.75</u>		<u>48.00</u>	
	14		
	<u>36</u>		
	.50		

27
27
27