

1128

MARK

BOOK

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IRVING PARK STATION

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92 FIFTH ST.
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SAN FRANCISCO, CAL.

AGENTS FOR

"BERGER" TRANSITS and LEVELS

"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS

"CHICAGO" STEEL TAPES, etc.

40' wide
14' cbs
13' 1/2

Diamond Ave X Sec.
from W. Line Allison To W. Line Parino
at Cass St
See page 27 for X sec West

5 1/2 x 25
mills

N.E. Cass
& Gannett

BM.	508	33.62	28.54
T.P.	9.52	38.82	43.2

W Line Allison 10' cbs 15' 1/4

N	5.7	33.1
cb	6.0	32.0
1/4	6.5	32.3
C	6.5	32.3
1/4	6.7	32.1
cb	7.8	31.0
S	7.7	31.1

10' E = W cb Allison

S	7.3	31.5
cb	6.9	31.9
1/4	6.6	32.2
C	6.3	32.5
1/4	6.2	32.6
cb	5.7	33.1
N	5.4	33.4

21' E of W Line

N	5.3	33.3
cb	5.4	33.4
1/4	6.7	32.1
C	6.9	31.9
1/4	7.0	31.8
cb	7.3	31.5
S	7.8	31.1

38.82

25' E of W Line = W 1/4

S	7.9	30.9
cb	7.7	31.1
1/4	7.5	31.3
C	7.2	31.6
1/4	7.0	31.8
cb	8.1	30.7
N	7.5	31.3

6' E = Track

N	6.41	32.41	on rail
cb	6.7	32.1	
1/4	7.0	31.8	
C	7.2	31.6	
1/4	7.8	31.0	
cb	8.1	30.7	
S	7.93	30.89	on rail

12' E of W 1/4

S	7.9	30.9
cb	7.7	31.1
1/4	7.4	31.4
C	7.1	31.7
1/4	6.8	32.0
cb	8.0	30.8
N	7.6	31.2

@ Allison

N	5.1	33.7
cb	5.9	32.9

3882

1/4	6.7	32.1
c	7.1	31.7
1/4	7.2	31.6
ch	7.2	31.6
S	7.1	31.7
E 1/4		
S	7.0	31.8
ch	6.5	32.3
1/4	6.4	32.4
c	6.3	32.5
1/4	6.2	32.6
ch	5.7	33.1
N	5.7	33.1
E. Ch.		
N	5.9	32.9
ch	6.2	32.6
1/4	6.3	32.5
c	6.5	32.3
1/4	6.4	32.2
ch	7.1	31.7
S	7.4	31.4
00 = E. Line Allison		
S	7.5	31.3
ch	7.2	31.5
1/4	6.7	32.7
c	6.5	32.3

3882

Diamond

1/4	6.5	32.3
ch	5.8	33.0
N	5.3	33.5
50' E		
N	4.9	33.9
ch	5.3	33.5
1/4	5.9	32.9
c	6.0	32.8
1/4	6.3	32.5
ch	6.4	32.4
S	6.8	32.0
+5	7.0	31.8
100' E		
-5	6.6	32.2
S	6.4	32.4
ch	5.8	33.0
1/4	5.7	33.1
c	5.7	33.1
1/4	5.5	33.3
ch	5.0	33.8
N	4.5	34.3
150' E		
N	4.1	34.7
ch	4.5	34.3
1/4	5.0	33.8
c	5.2	33.6

38.82

1/4	5.3	32.5
cl	5.6	33.2
S	5.9	32.9
+5	5.9	32.9

200' E.

-5	5.9	32.9
S	5.8	33.0
cl	5.4	33.8
1/4	4.9	33.9
E	4.8	34.0
1/4	4.6	34.2
cl	4.3	34.5
N	3.8	35.0

250' E.

N	3.5	35.3
cl	3.9	34.9
1/4	4.1	34.7
E	4.5	34.3
1/4	4.6	34.2
cl	4.9	33.9
S	5.3	33.5
+5	5.5	33.3

300 E.

-5	5.0	33.8
S	4.7	34.1
cl	4.3	34.5

38.82

Diamond

3

1/4	4.0	34.8
E	4.0	34.8
1/4	3.7	35.1
cl	3.2	35.6
N	2.8	36.0

350' E.

N	2.4	36.4
cl	2.9	35.9
1/4	3.2	35.6
E	3.7	35.1
1/4	3.6	35.2
cl	3.8	35.0
S	4.3	34.5
+5	4.6	34.2

400' E.

-5	4.0	34.8
S	3.9	34.9
cl	3.5	35.3
1/4	3.2	35.6
E	3.3	35.5
1/4	2.8	36.0
cl	2.6	36.2
N	2.2	36.6

450' E.

N	1.7	37.1
cl	2.0	36.8

38.82

1/4	2.5	36.3
c	2.8	36.0
1/4	2.8	36.0
cl	3.1	35.7
S	3.6	35.2
+5	3.6	35.2

500' E = W. Line Bayard 80' wide

-5	3.1	35.7
S	3.0	35.8
cl	2.6	36.2
1/4	2.0	36.8
c	2.1	36.7
1/4	2.2	36.6
cl	1.4	37.4
N	1.2	37.6

40' E = ~~4~~

N	0.7	38.1
cl	0.9	37.9
1/4	1.2	37.6
c	1.6	37.2
1/4	1.5	37.3
cl	1.8	37.0
S	2.4	36.4
+5	2.5	36.3

T.P. 9.27 46.59 1.50 37.32

46.59

Diamond

00 = E Line Bayard

-5	9.4	37.2
S	9.3	37.3
cl	8.9	37.7
1/4	8.9	37.7
c	8.5	38.1
1/4	8.1	38.5
cl	8.2	38.4
N	7.7	38.9

50' E

N	7.1	39.5
cl	7.4	39.2
1/4	7.7	38.9
c	7.9	38.7
1/4	8.5	38.1
cl	8.5	38.1
S	9.0	37.6
+5	9.1	37.5

100' E

-5	8.4	38.2
S	8.4	38.2
cl	8.0	38.6
1/4	7.9	38.7
c	7.4	39.2
1/4	6.8	39.8
cl	6.9	39.7
N	6.5	40.1

46.59

150' N

N	6.7	40.4
cl	4.6	40.0
1/4	4.4	40.2
C	4.6	40.0
1/4	7.2	39.4
cl	7.5	39.1
S	7.9	38.7
+5	8.0	38.5

200' E

-5	7.7	38.9
S	7.6	39.0
cl	7.0	39.6
1/4	6.9	39.7
C	6.4	40.2
1/4	6.0	40.5
cl	5.8	40.8
N	5.4	41.2

250' E

N	5.1	41.5
cl	5.5	41.1
1/4	5.6	41.0
C	6.0	40.6
1/4	6.3	40.3
cl	6.4	40.2
S	7.0	39.6
+5	7.1	39.5

46.59

Diameter 5

-5	6.6	40.0
S	6.4	40.2
cl	5.9	40.7
1/4	5.9	40.7
C	5.4	41.2
1/4	5.1	41.5
cl	5.1	41.5
N	4.4	42.2

350' N

N	3.9	42.7
cl	4.2	42.4
1/4	4.1	42.5
C	4.5	42.1
1/4	5.0	41.6
cl	5.2	41.4
S	5.6	41.0
+5	5.7	40.9

400' E

-5	5.0	41.6
S	4.9	41.7
cl	4.4	42.2
1/4	4.4	42.2
C	4.0	42.6
1/4	3.5	43.1
cl	3.4	43.2
N	3.1	43.5

46.59

450' E

N	2.6	44.0
cb	2.9	43.7
1/4	2.9	43.7
C	3.3	43.3
1/4	3.7	42.9
cb	3.9	42.7
S	4.0	42.6
+5	4.4	42.2

500' E = W Line Cass 14' chs 13' 1/2"

-5	3.7	42.9
S	3.6	43.0
cb	2.9	43.7
1/4	2.8	43.8
C	2.4	44.2
1/4	2.0	44.6
cb	1.8	44.8
N	1.9	44.7

W. chs.

N	1.7	44.9
cb	1.9	44.7
1/4	2.0	44.6
C	2.2	44.4
1/4	3.0	43.6
cb	3.0	43.6
S	3.3	43.3

46.59

Diamond U

W 1/4

S	2.8	43.8
cb	3.3	43.3
1/4	3.0	43.6
C	2.8	43.8
1/4	2.8	43.8
cb	2.4	44.2
N	2.2	44.4

3' E = W Line Paving

N	1.65	44.94
S	3.25	43.34

10' E of E. Cass = E. Line Paving

S	3.15	43.44
N	1.68	44.91

Spk Elec Pole S.W.

T.P. 9.64 53.42 2.81 43.78 Diamond - Cass

X Sec of Ctr. 30' of Diamond Ave
from Cass to Repdleton

5' E of E. edge Paving

N	9.0	44.4
+5	9.2	44.2
C	9.3	44.1
+10	9.5	43.9
S	9.7	43.7

005 E Line of Cass

S	9.0	44.4
+5	8.5	44.5
C	8.3	45.1
+10	8.4	45.0
+12	8.1	45.3
N	8.0	45.4

53.42

	50' E	
N	7.1	46.3
+3	7.2	46.2
+5	8.0	45.4
C	7.4	46.0
+10	8.0	45.4
S+15	8.1	45.3

100' E

S	7.4	46.0
+5	7.3	46.1
C	6.7	46.7
+10	7.7	45.7
+12	6.6	46.8
N	6.6	46.8

150' E

N	6.2	47.2
+3	6.2	47.2
+5	6.9	46.5
C	6.1	47.3
+10	6.7	46.7
S	6.9	46.5

200' E

S	6.6	46.8
+5	6.5	46.9
C	5.8	47.6
+10	6.4	47.0
+12	5.6	47.8
N	5.7	47.7

53.42

Diamond

7

250' E

N	4.9	48.5
+3	5.0	48.4
+5	5.8	47.6
C	5.3	48.1
+10	5.8	47.6
S	6.1	47.3

300' E

S	5.1	48.3
+5	5.1	48.5
C	4.4	49.0
+10	5.1	48.3
+12	4.1	49.3
N	4.1	49.3

350' E

N	3.2	50.2
+3	3.2	50.2
+5	4.0	49.4
C	3.5	49.9
+10	4.3	49.1
S	4.2	49.2

400' E

S	3.5	49.9
+5	3.4	50.0
C	2.6	50.8
+10	3.3	50.1
+12	2.4	51.0
N	2.3	51.1

53.42

450' E

N	1.7	51.7
+3	1.6	51.8
+5	2.5	50.7
C	2.0	51.4
+10	2.6	50.8
S	2.7	50.7

500' E = W. Line Dawes

S	1.9	51.5
+5	1.6	51.8
C	1.0	52.4
+10	1.6	51.8
+12	0.8	52.6
N	0.8	52.6

20' E of W. Line

N	0.8	52.6
+5	0.9	52.5
C	0.7	52.7
+10	1.2	52.2
S	1.6	51.8

40' E of W. Line = ϕ

S	1.0	52.4
+5	0.8	52.6
C	0.5	52.9
+10	0.3	53.1
N	0.2	53.2

T.P.

10.30

63.17

0.55

52.87

Nail Top Pole
S.E. Diamond
+ D

63.17

Diamond

8

60' E of W. Line

N	10.0	53.2
+5	10.0	53.2
C	10.1	53.1
+10	10.6	52.5
S	10.7	52.5

80' E of W. Line = E. Line Dawes = 00

S	10.3	52.9
+5	10.0	53.2
C	9.7	53.5
+10	9.9	53.3
N	9.5	53.7

50' E

N	8.7	54.5
+3	8.7	54.5
+5	9.4	53.8
C	9.0	54.2
+10	9.1	54.1
S	9.7	53.5

100' E.

S	8.6	54.5
+5	8.5	54.7
C	8.3	54.9
+10	8.8	54.4
+12	8.1	55.1
N	9.1	55.1

63.17

	150' E	
N	7.4	55.8
+3		
+5	7.9	55.3
C	7.8	55.4
+10	8.2	55.0
S	8.6	54.6
	200' E	
S	7.9	55.3
+5	7.5	55.7
C	7.1	56.1
+10	7.3	55.9
N	7.0	56.2
	250' E	
N	5.5	57.7
+3	5.5	57.7
+5	5.9	57.3
C	5.6	57.6
+10	6.2	57.0
S	6.2	57.0
	300' E	
S	5.2	58.0
+5	5.1	58.1
C	4.7	58.5
+10	5.4	57.8
+12	4.3	58.9
N	4.3	58.9

Diamond

63.17

	350' E	
N	3.4	59.8
+3	3.4	59.8
+5	4.4	58.8
C	4.0	59.2
+10	4.5	58.7
S	4.7	58.5
	400' E	
S	3.8	59.4
+5	3.6	59.6
C	3.2	60.0
+10	3.4	59.8
+12	2.5	60.7
N	2.8	60.7
	450' E	
N	2.5	60.7
+3	2.4	60.8
+5	3.0	60.2
C	2.8	60.4
+10	3.1	60.1
S	3.3	59.9
	500' E = W Line Events	
S	2.7	60.5
+5	2.6	60.6
C	2.7	61.0
+10	2.6	60.6
+12	2.1	61.1
N	1.9	61.3

63.17
40' E = 4

N	1.7	61.5
+5	2.1	61.1
C	2.0	61.2
+10	2.4	60.8
S	2.7	60.5

80' E = E Line Exerts = 00

S	2.0	61.2
+5	1.8	61.4
C	1.6	61.5
+10	1.7	61.5
+12	1.4	61.8
N	1.3	61.9

50' E

N	1.2	62.0		
+3	1.7	62.1		
+5	1.4	61.8		
C	1.3	61.9		
+10	1.4	61.8		
S	1.9	61.3		
T.R	9.16	71.28	1.05	62.12

100' E

S	9.7	61.6
+5	9.2	62.4
C	9.0	62.3
+10	9.6	61.7
+12	8.9	62.4
N	8.9	62.4

71.28

Diamond 70

150' E

N	8.5	62.8
+3	8.4	62.9
+5	9.2	62.1
C	8.6	62.7
+10	8.8	62.5
S	9.2	62.1

200' E

S	8.9	62.4
+5	8.3	63.0
C	8.3	63.0
+10	8.6	62.7
+12	7.9	63.4
N	7.8	63.5

250' E

N	7.4	63.9
+3	7.4	63.9
+5	8.3	63.0
C	7.8	63.5
+10	8.0	63.3
S	8.4	62.9

300' E

S	7.8	63.5
+5	7.3	64.0
C	7.2	64.1
+10	7.7	63.6
+12	6.9	64.4
N	6.8	64.5

71.28
350' E

N	6.4	64.9
+5	6.4	64.9
+7	7.1	64.2
E	6.6	64.7
+10	6.8	64.5
S	7.3	64.0

400' E

S	6.8	64.5
+5	6.3	65.0
E	6.2	65.1
+7	6.7	64.6
+10	5.9	65.4
N	5.7	65.6

450' E

N	5.2	66.1
+5	5.3	66.0
+7	6.0	65.0
E	5.5	65.7
+10	5.8	65.5
S	6.1	65.2

500' E = W. line Fanuel

S	5.6	65.7
+5	5.2	66.1
E	4.8	66.5
+10	7.7	66.6
N	4.6	66.7

Diamond

11

71.28
40' E = C Fanuel

N	4.1	67.2
+5	4.6	66.7
E	4.5	66.8
+10	4.8	66.5
S	5.1	66.2

80' E = E line Fanuel = 00

S	4.9	66.4
+5	4.3	67.0
E	4.0	67.3
+8	4.2	67.1
+10	3.6	67.7
N	3.5	67.8

50' E

N	3.4	67.9
+3	3.4	67.9
+5	4.1	67.2
E	3.6	67.7
+10	4.2	67.1
S	4.8	66.5

100' E

S	4.3	67.0
+5	3.9	67.4
E	3.5	67.8
+10	3.9	67.4
+11	3.7	67.6
N	3.5	67.8

71.28

N	150'E	3.0	68.3
+4		3.0	68.3
+5		3.5	67.8
C		3.1	68.2
+10		3.6	67.7
S		3.9	67.4

200'E

S		4.1	67.2
+5		3.6	67.7
C		3.2	68.1
+10		3.6	67.7
+12		3.1	68.2
N		3.3	68.0

250'E

N		2.4	68.9
+2		2.4	68.9
+5		3.0	68.3
C		2.6	68.7
+10		3.2	68.1
S		3.4	67.9

300'E

S		3.0	68.3
+5		2.8	68.5
C		1.8	69.5
+10		2.6	68.7
+12		1.8	69.5
N		1.8	69.5

71.28

Diamond

12

350'E

N		1.7	69.6
+3		1.8	69.5
+5		2.3	69.0
C		1.6	69.7
+10		2.3	69.0
S		2.9	68.4

T.P. 6.30 76.34 1.24 70.04

400'E

S		7.7	68.6
+5		7.0	69.3
C		6.4	69.9
+8		7.2	69.1
+10		6.6	69.7
N		6.4	69.9

450'E

N		6.1	70.2
+3		6.3	70.0
+5		6.7	69.6
C		6.2	70.1
+10		6.6	69.7
S		7.0	69.3

500'E = W Line Gresham

S		6.8	69.5
+5		6.3	70.0
C		5.8	70.5
+9		6.3	70.0

76.34

+10	5.9	70.4
N	5.8	70.5
	40'E = E	
N	5.7	70.6
+5	5.9	70.4
E	5.5	70.8
+10	4.1	70.2
S	6.4	69.9
	80'E = E. line Bresham	
S	6.2	70.1
+5	5.9	70.4
E	5.4	70.9
+9	5.9	70.4
+10	5.5	70.8
N	5.4	70.9
	50'E	
N	5.0	71.3
+5	5.1	71.2
+7	5.6	70.7
E	5.0	71.3
+10	5.7	70.6
S	6.0	70.3
	100'E	
S	5.5	70.8
+5	5.1	71.2
E	4.6	71.7

76.34

Diamond

13

+10	5.2	71.1
+12	4.6	71.7
N	4.6	71.7
	150'E	
N	3.8	72.5
+4	3.6	72.7
+5	4.5	71.8
E	3.9	72.4
+10	4.4	71.9
S	4.8	71.5
	200'E	
S	4.0	72.3
+5	3.7	72.6
E	3.2	73.1
+10	3.7	72.6
+11	3.2	73.1
N	3.3	73.0
	250'E	
N	2.5	73.8
+4	2.5	73.8
+5	2.9	73.4
E	2.2	74.1
+10	2.5	73.9
S	2.9	73.4

74.34

300' E

S	2.2	74.1
+5	2.0	74.3
C	1.8	74.5
+10	2.2	74.1
N	1.8	74.5

350' E

N	0.6	75.7
+5	1.1	75.2
C	1.0	75.3
+10	1.4	74.9
S	1.6	74.7

400' E

S	0.8	75.7
+5	0.4	75.9
C	0.0	76.3
+10	0.4	75.9
T.P.	6.90	83.10
N	6.6	76.5

450' E

N	5.8	77.3
+3	6.4	76.7
+5	6.7	76.4
C	6.3	76.8
+10	6.6	76.5
S	7.0	76.1

83.10

500' E = W. Line Haines

S	6.5	76.6
+5	6.2	76.9
C	5.9	77.2
+10	6.1	77.0
+12	6.2	76.9
N	5.4	77.7

40' E = ϕ

N	5.6	77.5
+5	5.9	77.2
C	6.2	76.9
+10	6.3	76.8
S	6.5	76.6

80' E = E. Line Haines = 00

S	6.0	77.1
+5	6.1	77.0
C	6.0	77.1
+10	5.8	77.3
N	5.6	77.5

50' E

N	4.9	78.2
+5	5.3	77.8
+6	5.9	77.2
C	5.5	77.6
+10	5.7	77.4
S	6.0	77.1

Diamond 14

83.10

100' E.

S	5.7	77.4
+5	5.4	77.7
C	5.3	77.8
+10	5.3	77.8
N	4.9	78.2

150' E.

N	4.6	78.5
+5	5.2	77.9
C	5.1	78.0
+10	5.4	77.7
S	5.7	77.4

200' E.

S	5.4	77.7
+5	5.2	77.9
C	4.8	78.3
+10	4.7	78.4
N	4.6	78.5

250' E.

N	4.4	78.7
+5	4.6	78.5
C	4.9	78.7
+10	4.8	78.3
S	5.0	78.1

300' E.

S	4.7	78.4
+5	4.3	78.8

83.10

Diamond 15

C	4.5	78.6
+10	4.5	78.6
N	4.3	78.8

350' E.

N	4.0	79.1
+5	4.1	79.0
C	4.0	79.1
+10	3.9	79.2
S	4.1	79.0

400' E.

S	3.1	80.0
+5	3.4	79.7
C	3.2	79.9
+10	3.2	79.9
N	3.0	80.1

450' N.

N	1.9	81.2
+5	1.9	81.2
C	2.1	81.0
+10	2.3	80.8
S	2.0	81.1

500' N = W. line In graph 100' wide

S	0.8	82.3
+5	0.8	82.3
C	0.7	82.4
+10	0.7	82.4
N	0.4	82.7

T.P.	12.28	83.10	95.12	0.26	82.84
			50' E = ϕ		
N			11.3		83.8
+5			11.3		83.8
C			11.3		83.8
+10			11.7		83.4
S			11.8		83.3
		100' E of W line = E. line Ingraham = 00			
S			10.8		84.3
+5			10.6		84.5
C			10.1		85.0
+10			10.3		84.8
N			10.3		84.8
		50' E.			
N			9.3		85.8
+5			9.0		86.1
C			8.7		86.4
+10			9.3		85.8
S			9.7		85.4
		100' E			
S			8.8		86.3
+5			8.2		86.9
C			7.7		87.4
+10			8.2		86.9
N			8.2		86.9

	95.12	Diamond 14
	150' E	
N	7.1	88.0
+5	7.1	88.0
C	6.8	88.3
+10	7.7	87.4
S	7.9	87.2
	200' E	
S	7.2	87.9
+5	6.9	88.2
C	6.2	88.9
+10	6.5	88.4
N	6.5	88.6
	250' E	
N	6.1	89.0
+5	6.1	89.0
C	5.6	89.5
+10	6.4	88.7
S	6.5	88.6
	300' E	
S	5.7	89.4
+5	5.6	89.5
C	4.9	90.2
+10	5.2	89.9
N	5.2	89.9
	350' E	
N	4.7	90.4
+5	4.3	90.8

9512
350' E (con)

C	4.0	911
+10	4.7	904
S	4.9	902

400' E

S	4.2	909
+5	4.0	911
C	3.2	919
+10	3.8	913
N	3.8	913

450' E

N	3.2	919
+5	3.0	921
C	2.2	929
+10	3.2	919
S	3.2	919

500' E = W. Line Jewell.

S	2.6	925
+5	2.3	928
C	1.8	933
+10	2.3	928
N	2.2	929

40' E = E

N	1.2	939
+5	1.5	936
C	1.3	938
+10	1.6	935
S	1.7	934

95.12

Diamond

17

80' E of White = E Line Jewell = 00

S	1.1	940		
+5	1.0	941		
C	1.0	941		
+10	0.6	945		
N	0.5	946		
T.P.	13.02	107.34	0.80	94.32

50' E

N	12.5	948
+5	12.8	945
C	12.9	944
+10	13.1	942
S	13.3	940

100' E

S	13.7	939
+5	13.1	942
C	13.5	946
+10	13.3	950
N	13.1	952

150' E

N	11.7	950
+5	11.7	956
C	12.0	953
+10	12.6	947
S	12.9	944

200' E

S	11.2	96.1
+5	10.8	96.5

107.34
800E Cont

C	10.2	97.1
+10	10.6	96.7
N	10.4	96.9
250E		
N	8.3	99.0
+5	8.3	99.0
C	8.2	99.1
+10	8.8	98.5
S	8.8	98.5
300E		
S	6.2	101.1
+5	6.1	101.2
C	5.8	101.5
+10	6.0	101.3
N	5.7	101.6
350E		
N	3.2	104.1
+5	3.2	104.1
C	2.9	104.4
+10	3.2	104.1
S	3.1	104.2
400E		
S	0.6	106.7
+5	0.7	106.6
C	0.4	106.9
+10	0.7	106.6
N	0.9	106.4

Diamond 18

107.34

T.P.	5.15	112.31	0.18	107.16
		450E		
N			3.5	108.8
+5			3.8	108.5
C			3.4	108.9
+10			4.0	108.3
S			4.0	108.3
500E				
S			3.3	109.0
+5			2.9	109.4
C			2.5	109.8
+10			2.8	109.5
N			2.7	109.6
540E				
N			2.5	109.8
+5			2.9	109.4
C			2.6	109.7
+10			3.1	109.2
S			3.7	108.6
580E				
S			3.9	108.4
+5			4.0	108.3
C			3.8	108.5
+10			4.0	108.3
N			3.9	108.4

112.31

640' E

N	4.9	107.4
+5	5.0	107.3
+5	5.5	106.8
+5	5.5	106.8
- C	5.3	107.0
+10	5.7	106.6
S	5.9	106.4

700' E

S	7.4	104.9
+5	7.4	104.9
C	6.8	105.5
+10	6.8	105.5
N	6.2	106.1

750' E

N	7.0	105.3
+5	7.0	105.3
C	7.5	104.8
+10	8.1	104.2
S	8.3	104.0

800' E

S	8.4	103.9
+5	8.1	104.2
C	7.7	104.6
+10	7.4	104.9
N	7.5	104.8

Diamond

19

112.31

850' E

N	7.6	104.7
+5	7.4	104.9
C	7.8	104.5
+10	8.3	104.0
S	8.4	103.9

900' E

S	8.1	104.2
+5	7.8	104.5
C	7.2	105.1
+10	7.1	105.2
N	7.3	105.0

950' E

N	5.8	106.5
+5	6.4	105.9
C	6.4	105.9
+10	6.8	105.5
S	7.5	104.8

1000' E

S	6.5	105.8
+5	6.1	106.2
C	5.4	106.9
+10	5.7	106.6
N	5.2	107.1

T.P. 3.71 110.90 5.12 107.19

110.90

1040 E

N	3.4	107.5
+5	4.0	106.9
E	3.9	107.0
+10	4.2	106.7
S	4.4	106.5

1080' E = w. line Lamont

S	5.0	105.9
+5	5.0	105.9
E	4.5	106.4
+10	4.5	106.4
N	4.5	106.4

Chkoncarb

3.88

107.02

N.W. Cor Lamont
& Diamond

00 = E. line Lamont

N	5.0	105.9
+5	5.1	105.8
E	5.3	105.6
+10	5.2	105.7
S	5.1	105.8

15' E

S	4.6	106.3
+5	4.5	106.4
E	4.2	106.7
+10	4.2	106.7
N	4.1	106.8

110.90

50' E

N	3.8	107.1
+5	4.4	106.5
E	4.2	106.7
+10	5.0	105.9
S	5.3	105.6

100' E

S	5.4	105.5
+5	4.7	106.2
E	4.4	106.5
+10	4.6	106.3
N	4.2	106.7

150' E

N	4.1	106.8
+5	4.3	106.6
E	4.1	106.8
+10	4.9	106.0
S	5.6	105.3

200' E

S	4.3	104.5
+5	5.4	105.4
E	4.9	106.0
+10	4.7	106.2
N	4.5	106.4

250' E

N	5.3	105.2
+5	5.4	105.3

Diamond 20

110.90

250' E (cont)

C	6.0	104.9
+10	6.6	104.3
S	7.0	103.9

300' E

S	8.0	102.9
+5	7.8	103.1
E	7.0	103.9
+10	7.2	103.7
N	6.7	104.2

350' E

N	8.3	102.5
+5	8.9	102.0
E	8.7	102.2
+10	9.3	101.5
S	9.7	101.2

400' E

S	11.1	99.8
+5	10.9	100.0
E	10.6	100.3
+10	10.0	100.9
N	9.4	101.5

450' E

N	10.9	100.0
+5	11.1	99.8
E	12.0	98.9
+10	12.7	99.2
S	11.7	99.2

110.90

Diamond

21

J.P. 0.95 100.49 11.36 99.54

485' E

S	1.8	98.7
+5	2.0	98.5
E	2.7	97.8
+10	3.0	97.5
N	3.1	97.4

500' E = White Marvell

N	3.3	97.2
+5	3.1	97.4
E	3.4	97.1
+10	2.9	97.6
S	2.7	97.8

10' E

S	3.9	96.6
+5	3.9	96.6
E	3.9	96.5
+10	3.7	96.8
N	3.7	96.8

40' E = E

N	4.3	96.2
+5	4.3	96.2
E	4.6	95.7
+10	4.7	95.6
S	4.9	95.6

100.49

80'E = E. Line Motrell

S	5.0	95.5
+5	4.8	95.7
C	4.9	95.6
+10	4.5	96.0
N	4.2	96.3

25'E

N	4.7	95.8
+5	4.9	95.6
C	4.9	95.6
+10	5.1	95.4
S	5.5	95.0

65'E

-5	7.9	92.6
S	8.2	92.3
+5	8.3	92.2
C	8.3	92.2
+10	8.0	92.5
N	7.9	92.5
+5	7.7	92.8

100'E

-5	8.6	91.9
N	8.7	91.8
+5	9.0	91.5
C	8.8	91.7
+10	8.9	91.6
S	9.3	91.2
+5	8.9	91.6

Diamond

100.49

150'E

-5	9.6	90.9
S	10.3	90.2
+5	10.3	90.2
C	9.4	91.1
+10	9.4	91.1
N	9.2	91.3
+5	9.0	91.5

200'E

-5	10.0	90.5
N	10.0	90.5
+5	10.2	90.3
C	10.3	90.2
+3	9.2	91.3
+10	10.2	90.3
S	11.1	89.4
+5	10.3	90.2

250'E

-5	10.7	89.8
S	11.4	89.1
+5	11.2	89.3
+8	10.7	89.8
C	10.2	90.3
+10	10.4	90.1
N	10.4	90.1
+5	10.4	90.1

100.49
300' E

-5	10.4	90.1
N	10.7	89.8
+5	10.3	90.2
C	10.9	89.6
+10	12.2	88.3
S	12.6	87.9
+5	11.3	89.2

350' E

-5	11.9	88.6
S	12.6	87.9
+5	12.0	88.5
+8	11.0	89.5
C	10.8	89.7
+10	10.6	89.9
N	10.8	89.7
+5	10.7	89.8

400' E

-5	11.1	89.4
N	11.3	89.2
+5	10.9	89.6
C	11.2	89.3
+8	11.5	89.0
+10	12.7	87.8
S	13.0	87.5
+5	12.9	87.6

100.49
450' E
Diamond 23

-5	13.6	86.9
S	13.4	87.1
+5	11.7	88.8
C	11.7	88.8
+10	11.4	89.1
N	11.2	89.3
+5	11.2	89.3

500' E = W Line Noyes

N	7.6	92.9
+5	9.1	91.4
C	9.7	90.8
+10	10.5	90.0
S	11.4	89.1
+5	11.9	88.6

T.P. 788 103.09 5.28 95.21
40' E = E

S	10.9	92.2
+5	10.2	92.9
C	9.4	93.7
+10	8.6	94.5
N	8.1	95.0

90' E = E Line Noyes

N	6.4	96.7
+5	6.8	96.3
C	6.7	96.4
+10	7.2	95.9
S	7.6	95.5

10309

25' E

S	7.4	95.7
+5	7.0	96.1
C	5.8	97.3
+10	5.8	97.3
N	6.1	97.0

50' E

N	6.5	96.6
+5	6.4	96.7
C	6.7	96.4
+10	8.8	94.3
S	9.3	93.8
+5	9.6	93.5

T.P.

364

101.63

5.10

97.99

Nails in Pole. See
Diamond
150' E of Naves

85' E

S	6.2	95.4
+5	5.8	95.8
C	5.3	96.3
+10	4.6	97.0
N	4.4	97.2

110' E

N	2.4	99.2
+5	2.0	99.6
C	2.4	99.2
+10	2.9	98.7
S	3.5	98.1

101.63

Diamond 24

135' E

S	3.0	98.6
+5	2.6	99.0
C	1.6	100.0
+10	0.9	100.7
N	1.2	100.4

165' E

N	1.3	100.3
+5	1.3	100.3
C	1.7	99.9
+10	2.4	99.0
S	3.3	98.3

200' E

S	3.8	97.8
+5	3.3	98.3
C	2.4	99.2
+10	2.4	99.2
N	2.2	99.4

240' E

N	3.7	97.9
+5	3.7	97.9
C	3.3	98.3
+10	3.8	97.8
S	4.4	97.2

260' E

S	6.6	95.0
+5	6.1	95.5

101.63

C		5.4	96.2
+10		5.2	96.4
N		5.7	96.5
	300' E		
N		7.2	94.4
+5		7.2	94.4
C		7.6	94.0
+10		8.4	93.2
S		8.7	92.9
	350' E		
S		9.6	92.0
+5		9.2	92.4
C		8.8	92.8
+10		8.5	93.1
N		8.4	93.2
	400' E		
N		7.4	93.8
+5		8.2	93.4
C		8.7	92.9
+10		9.2	92.4
S		9.8	91.8
	435' E		
S		9.4	92.2
+5		8.8	92.8
T.P.	2.49	95.06	92.57
C		1.9	93.3

95.00

Diamond

25

+10		0.9	94.2
N		0.1	95.0
	455' E		
N		70.2	95.3
+5		0.3	94.8
C		1.9	93.2
+10		2.4	92.7
S		3.2	91.9
	500' E = W. LINE Olney		
S		5.6	89.5
+5		5.0	90.1
C		4.0	91.1
+3		3.6	91.5
+10		1.7	93.4
N		0.7	94.4
	13' E		
N		2.4	92.7
+5		3.2	91.9
+9		4.5	90.6
C		5.1	90.0
+10		6.1	89.0
S		6.8	88.3
	23' E		
S		7.9	87.3
+5		6.7	88.4
C		5.8	89.3

95.06

+10	5.1	90.0
N	4.7	90.4

40' E = ϕ

N	5.8	89.3	1' cut of Lees
+5	6.0	89.1	
C	7.3	87.8	
+10	8.1	87.0	
S	8.6	86.5	

55' E

S	9.8	85.3
+5	9.3	85.8
C	8.6	86.5
+10	7.9	87.2
N	7.9	87.2

80' E = E line of Hwy

N	8.6	86.5
+5	8.9	86.2
C	9.1	86.0
+10	10.1	85.0
S	10.7	84.4

35' E

S	11.3	83.8
+5	11.0	84.1
C	9.9	85.2
+10	9.6	85.5
N	9.3	85.8

95.06

Diamond

26

65' E

N	9.1	86.0
+5	9.2	85.9
C	9.4	85.7
+10	10.3	84.8
S	10.5	84.3

100' E

S	10.8	84.8
+5	10.6	84.5
C	9.8	85.3
+10	9.1	86.0
N	8.8	86.3

150' E

N	8.9	86.2
+5	9.1	86.0
C	9.8	85.3
+10	10.5	84.6
S	10.5	84.6

200' E

S	9.6	85.5
+5	9.6	85.5
C	9.1	86.0
+10	9.0	86.1
N	8.9	86.2

Continued on Page 29

Diamond St 2 Sec from W. line
of Allison to W. end street

	5.95	36.84	30.89	Key Rail Page 1
		10' W. of W. line of Allison		
Seb. rail - gutter cont. into grade		7.0	29.8	
" " " "		6.0	30.8	
" "		5.5	31.3	
" "		4.9	31.9	
" "		4.6	32.2	
" "		4.5	32.3	
" "		4.4	32.4	
		30' W. of W. line Allison		
" "		4.2	32.6	
" "		4.6	32.2	
" "		5.0	31.8	
" "		5.4	31.4	
" "		5.4	31.4	
" "		6.0	30.8	
+ 12.9 = gutter cont. curb into grade		7.2	29.6	
		100' W.		
Seb. rail - gutter		7.4	29.4	
" " " "		5.4	31.4	
" "		5.2	31.6	
" "		5.4	31.4	
" "		5.0	31.8	
" "		4.6	32.2	
" "		4.3	32.5	

	36.84 150' W	Diamond 27
N	4.4	32.4
U	4.7	32.1
" "	5.1	31.7
" "	5.3	31.5
" "	5.3	31.5
" "	5.7	31.1
+ 12.9 = gutter	7.5	29.3
	200' W = E line Alley Not graded Alley returns in	
S. ring	6.66	30.14 on curb No yardage
" " in gutter	7.6	29.2
S. C. P.	6.83	30.01 on curb No yardage
" " 20.1 in gutter	8.0	28.8
+ 2.1	5.3	31.5
" "	4.9	31.9
" "	5.0	31.8
" "	5.0	31.8
" "	4.8	32.0
" "	4.5	32.3
	204' W.	
" "	4.4	32.4
" "	4.7	32.1
" "	5.1	31.7
" "	5.1	31.7
" "	5.1	31.7
" "	5.4	31.4
" "	5.8	31.0

36.84

217' W

S	5.8	31.0
cb	5.6	31.2
1/4	5.1	31.7
C	5.0	31.8
1/4	5.0	31.8
cb	4.7	32.1
N	4.5	32.3

220' W = white Alley

N	4.3	32.5
cb	4.7	32.1
1/4	5.0	31.8
e	5.1	31.7
1/4	5.0	31.8
+11	5.4	31.4
cb, 1/4 gutter	8.1	28.7
smcb	6.98	29.96
S, in gutter	7.9	28.9

250' W

5cb 10.1 = gutter	7.9	28.9
+2	5.3	31.5
1/4	5.0	31.8
C	5.1	31.7
1/4	5.0	31.8
cb	4.6	32.2
N	4.4	32.4

Diamond

28

36.84

300' W

N	4.4	32.2
cb	4.6	32.2
1/4	5.0	31.8
e	5.1	31.7
1/4	5.0	31.8
+11	5.4	31.4
+12.9 = gutter dmt cb in to grade	7.3	29.5

350' W

5cb 10.1 = gutter	6.9	29.9
+2	5.4	31.2
1/4	5.0	31.8
C	5.0	31.8
1/4	4.9	31.9
cb	4.7	32.1
N	4.4	32.4

Use this
378 W on S, and 382 W on N = W. End B/Ks

N	4.3	32.5
cb	4.6	32.2
1/4	4.9	31.9
e	5.0	31.8
1/4	4.9	31.9
+11	5.3	31.3
+12.9 = gutter dmt cb in cb	6.6	30.2
	5.46	31.31

95.06
Continued from Page 26
250' E

N	8.8	86.3
+5	8.8	86.3
C	9.5	85.6
+10	9.9	85.2
S	10.0	85.1

300' E

S	10.4	84.7
+5	10.3	84.8
C	9.7	85.4
+10	9.2	85.9
N	9.2	85.9

350' E

N	9.9	85.2
+5	9.8	85.5
C	10.4	84.7
+10	10.9	84.2
S	10.0	85.1
T.P.	1.95	86.22
		10.79
		84.27

400' E

S	2.4	83.8
+5	2.4	83.8
C	1.9	84.3
+10	1.2	85.0
N	1.2	85.0

86.22

Diamond

29

450' E

N	1.4	84.8
+5	1.3	84.9
C	2.0	84.2
+10	2.3	83.9
S	2.5	83.7
+10	2.9	83.3

500' E = W Line Pendleton

-10	3.7	82.5
S	3.1	83.1
+5	3.0	83.2
C	2.5	83.7
+10	2.0	84.2
N	1.8	84.4

40' E = ~~C~~

N	2.7	84.0
+5	2.3	83.9
C	3.1	83.1
+10	3.5	82.7
S	3.9	82.3
+10	4.4	81.9

80' E = E Line Pendleton

-10	5.0	81.2
S	4.1	82.1
+5	3.8	82.4
C	4.0	82.2
+10	3.0	83.2
N	3.0	83.2

Pendleton St X Sec
 from S. Line Diamond to N. Line Garnett

86.22
 000' S Line Diamond

E	5.4
+5	5.3
C	5.3
+10	4.9
W	4.9
+10	4.7

50' S

+10	6.8
W	7.1
+5	7.3
C	7.6
+10	7.8
E	8.1

100' S

E	10.0
+5	9.4
C	9.7
+10	9.2
W	9.1

150' S

W	11.0
+5	11.2
C	11.5
+10	11.7
E	11.9

86.22

30

TR 0.31 73.90 17.63 73.59

200' S

E	2.0
+5	1.7
C	1.4
+10	1.1
W	1.1

235' S

W	2.4
+5	2.8
C	3.1
+10	3.3
E	3.6

270' S = N. Line Emerald

E	4.9
+5	4.6
C	4.1
+10	3.9
W	3.8

10' S

W	4.8
+5	4.8
C	5.0
+10	5.2
E	5.5

73.90
20' S

E	5.2
+5	4.9
C	4.7
+10	4.7
W	4.6

40' S = ϕ

W	5.2
+5	5.1
C	5.1
+10	5.2
E	5.3

80' S = W. line Emerald

E	6.0
+5	5.9
C	5.9
+10	6.0
W	6.1

50' S

W	7.3
+5	7.3
C	7.1
+10	7.0
E	7.1

100' S

E	7.4
+5	7.4

73.90

Pendleton 31

E	7.8
+10	8.1
W	8.1

135' S

W	8.7
+5	8.6
C	8.6
+10	8.6
E	8.6

165' S

E	9.7
+5	9.5
C	9.6
+10	9.7
W	9.8

200' S

W	11.2
+5	11.3
C	11.3
+10	11.5
E	11.6

T.P. 0.22 61.58 12.54 61.36

235' S

E	1.5
+5	1.3
C	1.4

61.58

T10. 1.3

W 1.4

270'S = N. line Field SPRAY

W 3.8

+5 3.9

C 4.0

+10 4.0

E 4.0

40'S = ~~E~~

E 7.2

+5 7.3

C 7.3

+10 7.2

W 7.2

80'S = S. line Field SPRAY

W 10.2

+5 10.2

C 10.3

+10 10.1

E 10.2

45'S

E 13.0

+5 13.0

C 13.0

+10 12.7

W 12.8

Pendleton. 32

61.58

T.P. 0.89 49.85 12.62 78.96

85'S

W 3.0

+5 3.1

C 3.2

+10 3.1

E 3.0

130'S

E 5.9

+5 6.1

C 6.1

+10 6.5

W 6.5

165'S

W 8.8

+5 8.7

C 8.4

+10 7.8

E 7.3

200'S

E 9.4

+5 9.6

C 10.0

+10 10.5

W 10.7

49.85

235'.5

W			12.7	
+5			11.8	
C			11.5	
+10			11.2	
E			11.0	
T.P.	3.32	40.99	12.18	37.67

270'. S=N. Line Garnett

E			4.0	
+5			4.2	
C			4.3	
+10			4.3	
W			4.4	

30'. S=N. Line Faving

10' W of Φ			5.31	On paving
Φ Pundleton			5.32	✓
10' E of Φ			5.59	✓

23

Moore
5/20/55

CROSS SECTION of AUBURN DRIVE
E.L. EUCLID to So. ✓ 50' wide
10' cbr

N.W. CP	590	346.53	340.63	UNIV. AVE EUCLID
T.P.	702	347.01 ✓	6.5 ✓	339.99

Sec A

N	6.0	41.0
+10	5.6	41.4
+15	6.8	40.2
+23	7.3	39.7
+50	7.5	39.5
+80	6.7	40.3
+83	4.2	42.8
+01.9 = SL	3.6	43.4

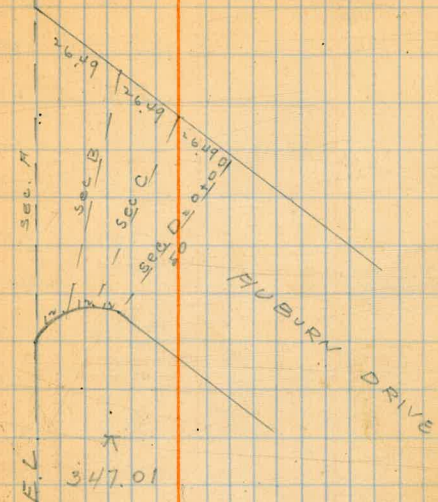
Sec B

N	6.3	40.7
+14	6.1	40.9
+15	6.7	40.3
+40	6.3	40.7
+90	6.0	41.0
+65	4.3	42.7
+76 = SL	3.9	43.1

Sec C

N	6.5	40.5
+13	6.2	40.8
+14	6.6	40.4
+30	5.9	41.1
+40	6.1	40.9
+45	5.5	41.5
+39 = SL	4.8	42.2 ✓

EUCLID AVE



Sec D = 0+00

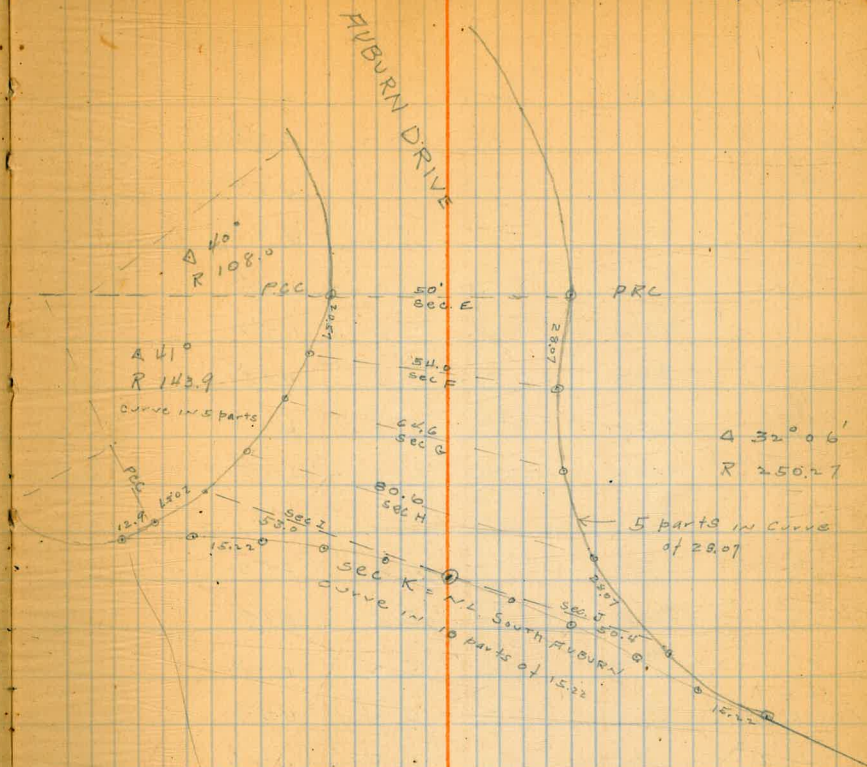
SL = STATIONING

S	4.5	42.5
+8	5.3	41.7
2	5.7	41.3
14	5.5	41.5
8	5.8	41.2
14	6.3	40.7
+5	6.5	40.5
25	6.1	40.9
N	6.6	40.4
0+25		
N	6.5	40.5 ✓

347.01

dt		5.9	41.1
+v		6.3	40.7
1/4		6.1	40.9
v		5.1	41.6
1/2		5.3	41.7
+d		5.3	41.7
+7		5.8	41.2
dt		4.9	42.1
S		4.6	42.4
	0+50		
S:		4.4	42.6
dt		4.7	42.3
+1		5.3	41.7
1/4		4.9	42.1
o		5.1	41.9
1/2		5.8	41.2
dt		6.0	41.0
1/4		6.3	40.7
	0+75		
1/4		6.0	41.0
dt		5.5	41.5
1/4		5.7	41.3
e		5.0	42.0
1/2		4.6	42.4
dt		4.9	42.1
S		4.5	42.5

35



347.01

	1700		
S		4.2	42.8
cb		4.6	42.4
+3		5.0	42.0
1/4		4.5	42.5
e		4.8	42.2
1/4		5.5	41.5
cb		5.8	41.2
N		6.2	40.8

	125		
N		6.0	41.0
cb		5.5	41.5
1/4		5.2	41.8
e		4.4	42.6
1/4		4.4	42.6
cb		4.5	42.5
S		3.9	43.1

	150		
S		4.2	42.8
cb		4.7	42.3
+3		5.0	42.0
1/4		4.7	42.3
e		4.8	42.2
1/4		5.2	41.8
+5		5.5	41.5
cb		5.2	41.8

347.01

AUBURN₃₆

		5.5	41.5
N	175		
N		5.1	41.9
cb		5.2	41.8
1/4		5.3	41.7
e		5.0	42.0
1/4		5.0	42.0
+5		5.3	41.7
cb		4.8	42.2
S		4.5	42.5

	200		
S		4.6	42.4
cb		5.1	41.9
1/4		5.2	41.8
e		5.1	41.9
1/4		5.4	41.6
cb		5.5	41.5
N		5.6	41.6

	225		
N		5.5	41.5
cb		5.6	41.4
1/4		5.4	41.6
e		5.0	42.0
1/4		5.2	41.8
+5		5.1	41.6
		5.0	42.0

34701

S		4.7	42.3
	2.50'		
S		4.8	42.2
cb		5.0	42.0
+N		5.6	41.4
1/4		5.2	41.8
c		5.2	41.8
1/4		5.5	41.5
cb		5.6	41.4
N		5.6	41.4

2.75'

N		5.8	41.2
cb		5.6	41.4
1/4		5.4	41.6
c		5.2	41.8
1/2		5.3	41.7
+S		5.6	41.4
cb		5.2	41.8
S		4.9	42.1

305.5 = PC.

S		5.1	41.9
cb		5.2	41.6
1/4	29.05	5.1	41.9
c		5.1	41.9
1/4		5.4	41.6
cb		5.7	41.3

34701

AUBURN 37

N		5.9	41.1
	334.55		
N		5.8	41.2
cb		5.6	41.4
1/4		5.4	41.6
c	29.05	5.0	42.0
1/4		5.1	41.9
+S		5.6	41.4
cb		5.3	41.7
S		5.3	41.7

363.60

S		5.3	41.7
cb		5.4	41.6
+S		5.8	41.2
1/4		5.4	41.6
c	29.05	5.2	41.8
1/4		5.5	41.5
cb		5.7	41.3
N		5.8	41.2

392.65

N		5.7	41.3
cb		5.5	41.5
1/4		5.5	41.5
c	29.05	5.3	41.7
1/4		5.4	41.6
+S		5.7	41.3

34701

S db.		5.2	41.8
S		5.1	41.9
	421.70		
S		5.1	41.9
db		5.3	41.7
1/4	(29.05)	5.4	41.6
c		5.1	41.9
1/4		5.2	41.6
u		5.6	41.4
N		5.7	41.3
	450.75 = EC		
N		5.9	41.1
db		5.3	41.7
1/4		5.2	41.7
c		4.8	42.2
1/4		5.1	41.9
db		5.0	42.0
S		4.9	42.1
T.P	427	4.63	342.38
	475 e		
S		4.0	42.7
db		4.1	42.6
+2		4.6	42.1
1/4		4.4	42.3
c		4.5	42.2
1/4		5.0	41.7

346.65

RUBURN 38

db		5.2	41.5
N		5.8	40.9
	500 e		
N		6.2	40.5
db		5.4	41.3
1/4		5.2	41.5
c		4.7	42.0
1/4		4.6	42.1
+6		4.9	41.8
db		4.4	42.3
S		4.2	42.5
	525 e		
S		4.1	42.6
db		4.7	42.0
+3		5.0	41.7
1/4		4.8	41.9
c		4.9	41.8
1/4		5.5	41.2
db		5.7	41.0
1/4		6.3	40.4
	550		
N		6.4	40.3
db		5.7	41.0
1/4		5.6	41.1
c		5.2	41.5
1/4		5.0	41.7

346.65

1/2 + 6		5.0	41.7
cb		4.4	42.3
S		3.8	42.9
	575' E		
S		4.3	42.4
cb		4.7	42.0
tr		5.1	41.6
1/4		4.9	41.8
e		4.9	41.8
1/4		5.5	41.2
cb		5.5	41.2
N		6.3	40.4
	600' E		
N		6.2	40.5
cb		5.6	41.1
1/4		5.4	41.3
e		4.8	41.9
1/4		4.8	41.9
+ 6		5.0	41.7
cb		4.7	42.0
S		4.3	42.4
	625' E		
S		4.2	42.5
cb		4.6	42.1
tr		4.9	41.8
1/4		4.7	42.0

346.65

FVUBURN 39

e		4.6	42.1
1/4		5.1	41.6
cb		5.2	41.5
N		5.6	41.1
	650' E		
1/4		5.0	41.7
cb		4.7	42.0
1/4		4.6	42.1
e		4.2	42.5
1/4		4.2	42.4
cb		4.2	42.5
S		4.0	42.7
	675' E		
S		3.6	43.1
cb		3.9	42.8
1/4		4.0	42.7
e		3.8	42.9
1/4		4.1	42.6
cb		4.2	42.5
N		4.7	42.0
	700' E		
N		4.4	42.3
cb		4.1	42.6
1/4		3.7	43.0
e		3.6	43.1
1/4		3.6	43.1

346.65

cb		3.6	43.1
S		3.2	43.5
	731.25 = FC.		
S		3.3	43.4
cb	(3042)	3.5	43.2
1/4		3.4	43.3
e		3.3	43.4
1/4		3.7	43.0
cb		3.9	42.8
N		4.2	42.5
	761.77		
N		4.6	42.1
u		4.1	42.6
1/4		3.8	42.9
e	(3042)	3.6	43.1
1/4		3.5	43.2
cb		3.6	43.1
S		3.2	43.5
	792.19 e		
S		2.2	43.5
d		3.8	42.9
1/4	(3042)	4.2	42.5
e		4.2	42.5
1/4		4.2	42.5
cb		4.9	41.8
N		5.6	41.1

346.65

AUBURN

40

	822.6		
N		6.9	39.8
cb		5.9	40.8
1/4		5.1	41.6
c	(3042)	5.2	41.5
1/4		5.1	41.6
+5		5.1	41.6
cb		4.4	42.3
S		4.2	42.5
	853.03 = EC.		
S		5.2	41.5
d		5.6	41.1
+3		6.4	40.3
1/4		6.5	40.2
e		6.5	40.2
1/4		6.5	40.2
+4		7.0	39.7
cb		7.4	39.3
N		8.7	38.0
+5		9.3	37.4
	875.4		
-5		11.7	35.0
N		10.7	36.0
cb		9.4	37.3
1/4		7.9	38.8
c		7.7	39.0
1/4		7.5	39.2

346.65

+5		7.4	39.3
cb		6.7	40.0
S		6.3	40.4
	910 E		
S		8.6	38.1
cb		9.8	36.9
1/4		10.5	36.2
C		10.5	36.2
1/4		10.9	35.8
cb		12.1	34.6
N		13.0	33.7
+5		13.4	33.3
T.P.	2.83	12.55	334.10
	936.15 = P.C.		
-10		7.2	29.5
N		6.1	30.8
cb		4.7	32.2
1/4		3.2	33.7
C	(15.15)	3.4	33.5
1/4		3.5	33.4
cb		3.1	33.8
+2		1.4	35.5
S	951.30	1.2	35.7
	451.26		
S		2.7	34.2
+7		3.1	33.8

336.93

AUBURN 41

+8		4.3	32.6
cb		4.7	32.2
1/4		4.8	32.1
C	(15.15)	5.0	31.9
1/4		5.4	31.5
cb		6.9	30.0
N		8.1	28.8
+10	966.45	9.1	27.8
	966.37 E		
-10		11.3	25.6
N		9.8	27.1
cb		8.3	28.6
1/4		7.0	29.9
C		6.5	30.4
1/4	(15.15)	6.6	30.3
cb		6.2	30.7
+2		6.0	30.9
+4		4.5	32.4
S	981.60	4.2	32.7
	981.48 E		
S		5.2	31.7
+8		6.1	30.8
cb	(15.15)	7.5	29.4
1/4		8.0	28.9
C		7.6	29.3
1/4		7.8	29.1

336.93

dt		8.8	28.1
N		10.0	26.9
+10	99675 99659 E	11.6	25.3
-10		12.2	24.7
N		10.7	26.2
dt		9.6	27.3
1/4	(1515)	8.8	28.1
C		8.5	28.4
1/2		9.0	27.9
dt		8.6	28.3
+2		7.4	29.5
S	101190 101170 E	6.4	30.5
S		7.0	29.9
+8		8.1	28.8
dt		9.6	27.3
1/4		9.7	27.2
C	(1515)	9.5	27.4
1/4		9.6	27.3
dt		10.2	26.7
N		12.0	24.9
+10	1027.05 1026.81 E	13.6	23.3
-10		12.7	22.2
N		13.2	23.7

336.93

AUBURN

42

+5		12.5	24.4	
dt		11.3	25.6	
1/4		10.3	26.6	
C	(1515)	10.3	26.6	
1/4		10.2	26.6	
dt		10.4	26.5	
+3		10.2	26.7	
+5		8.8	28.1	
S	104220 104192 E = PRC	8.1	28.8	
S		8.6	28.3	
+6		10.1	26.8	
+8		10.9	26.0	
dt	(27.28)	11.0	25.9	
1/4		11.0	25.9	
C		11.1	25.8	
1/4		11.2	25.7	
+6		11.2	25.7	
dt		11.8	25.1	
+5		13.2	23.7	
T.P.	305	328.58	11.40	325.53
N on Hub			5.48	323.10
+10	106948 106919 E		6.8	21.8
-10			6.7	21.9
N			5.6	23.0

328.58

+5		1.1	24.5
cb		3.9	24.7
1/4		3.8	24.8
c		3.7	24.9
1/4		3.6	25.0
cb		3.6	25.2
+4		1.7	26.9
S	1096.76	1.1	27.5
	1096.46 e		
	27.77		
S		2.0	26.6
+6		2.5	26.1
cb		4.7	23.9
+4		5.6	23.0
1/4	(27.28)	5.0	23.6
c		4.7	23.9
1/4		5.0	23.6
cb		5.2	23.4
N		6.0	22.6
+2		7.0	21.6
+10	1124.04	7.5	21.1
	(1113.73 e) ?		
-10		8.5	20.1
N		7.5	21.1
+5	(27.28)	6.8	21.8
cb		6.7	22.0
1/4		6.8	21.8

328.58

AUBURN

4.3

c		6.5	22.1
1/4		6.8	21.8
cb		5.6	23.0
+5		4.5	24.1
	1151.32	3.7	24.9
	1141.0 e		
S		5.3	23.3
+7		6.0	22.6
cb		7.6	21.0
1/4		8.3	20.3
c	(27.28)	8.2	20.4
1/4		8.3	20.3
cb		8.4	20.2
N		8.2	20.4
+10		8.2	20.4
	1178.60		
	(1168.27 e = PRC.)	(1178.71)	
-0		10.7	17.9
N		10.6	18.0
cb		10.7	17.9
1/4	(4')	10.9	17.7
c		10.6	18.0
1/4		10.6	18.0
cb		10.5	18.1
+5		8.6	20.0
S		7.8	20.8
	1182.60		
	(1172.27 e)	(1182.71)	
S		8.5	20.1

328.58

+5		9.2	19.4
cb		11.0	17.6
1/4		11.1	17.5
c		11.1	17.5
1/4	(2)	11.2	17.4
cb		11.6	17.0
+7		10.2	18.2
N		10.5	18.1
+10	1184.60 (1174.27 E)	10.5	18.1
		(1184.71)	
-10		13.6	15.0
N		12.2	16.2
cb	(9.08)	12.1	16.5
1/4		11.3	17.3
c	1193.68 (1190.31 E)	11.3	17.3
		(1193.79)	
-10		16.8	11.8
N		14.3	14.3
cb		12.8	15.8
1/4		12.6	16.0
c	(15.08)	12.7	15.9
1/4		12.6	16.0
cb		13.1	15.6
+2		12.7	15.9
S		9.8	18.8

✓

328.58

FURN 4.4

1208.76
(1212.35 E)

S		12.2	16.4	
T.P.	0.58	316.21	12.95	315.63
+6		2.1	14.1	
cb		2.1	14.1	
1/4		2.0	14.2	
e		2.4	13.8	
1/4	(15.08)	2.7	13.5	
cb		2.6	13.6	
+5		3.2	13.0	
N		4.9	11.3	
+10	1223.84 (1234.39 E)	5.7	10.5	
-10		9.5	06.7	
N		7.5	08.7	
+7		4.8	11.4	
cb		4.8	11.4	
1/4		4.7	11.5	
c	(15.08)	4.5	11.7	
1/4		3.5	12.7	
cb		3.6	12.6	
+4		4.2	12.0	
S	1238.92 (1250.43)	1.0	15.2	
S		2.1	14.1	
+5		5.1	11.1	

✓

316.21

Dr		5.1	11.1
1/2		5.2	11.0
e		6.1	10.1
1/4		7.8	8.4
cb	(1508)	7.5	8.7
+7		8.0	8.2
N		9.0	7.2
+10	1754.00	11.3	4.9
	PRC own (1278.47 E = PCC. own S = Sec E)		see page 35
-10		14.3	1.9
N		12.0	4.2
+3		10.5	5.7
cb		10.3	5.9
1/4		9.6	6.6
e		7.2	9.0
1/4		6.5	9.7
cb		6.8	9.4
+6		6.1	10.1
S		3.7	12.5
	Sec F		
S		5.3	10.9
+3		7.2	9.0
+28		8.1	8.1
+34		11.5	4.7
+45		14.1	2.1
+51 = NL		14.3	1.9
			✓

316.21

AUBURN

45.

NL +5		15.6	0.6
✓ +15		18.8	297.4
	Sec G		
S		6.0	10.2
+2		7.5	8.4
+31		8.4	7.8
+45		15.7	0.5
+53		18.0	298.2
+64.6 = NL		19.1	297.1
NL +15		25.6	290.6
T.P. 107	31398	3.30	31291
	Sec H		
S = NL		3.1	10.9
+3		5.0	9.0
+32		5.5	8.5
+40		8.5	5.5
+50		14.6	299.4
+57		17.2	296.8
+60		19.4	294.6
+63		19.0	295.0
+77		20.7	293.3
+80.6 = NL + EL		22.8	291.2
EL +15		27.4	286.6
✓ +2.5		29.5	284.5
	Sec I		
S		1.1	312.9
			✓

Nail in pole
S side

313.98

+6	4.3	9.7
+38	5.3	8.7
+42	7.1	6.9
+53 = Cr. Curve on N.E. of S. Auburn	13.5	300.5

Sec J

0+00 = Cr. Curve N.E. of S. Auburn	13.5	300.5
+15	17.7	296.3
+25	22.7	291.3
+45	25.3	289.7
+50.4 = N. E. L.	26.8	287.2
N +15	30.5	283.5
✓ +25	32.2	281.8

Sec K = N.E. of S. Auburn

-23	35.2	278.6
-1	32.9	281.1
N.L.	31.2	282.6
+15.2	28.7	285.3
+30.4	26.0	288.0
+45.6	24.0	290.0
+55.0	22.7	291.3
+60.8	17.8	296.2
+76.10 = Cr. Curve	13.5	300.5
+91.3	5.1	8.9
106.54	4.3	9.7
121.76	3.6	10.4
136.98	2.6	11.4

313.98

AUBURN

44

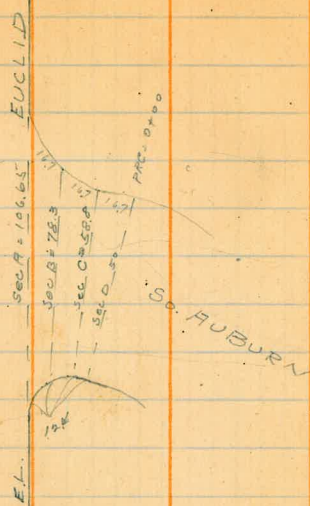
152.20 = P.R.C. N.E. of S. Auburn +0.5 314.5

CROSS SECTION of
So. HUBURN EUCLID South

50' W 140
10' Ck

34607

S. HUBURN 47



BM	346	344.09		342.63
TP	625	346.07	427	339.82

Sec A = EL EUCLID

N		4.1	42.0
+30		4.5	41.6
+38		6.2	39.9
+60		6.1	40.0
+80		7.2	38.9
+86		6.8	39.3
106.65 = SL		6.8	39.3
Sec B			
S		6.9	39.2
+13		7.1	39.0

+38	5.9	40.2
+48	6.0	40.1
+60	5.4	40.7
+61	4.8	41.3
+78.3 = N.L.	4.3	41.8

Sec C

N	4.3	41.8
+13	5.4	40.7
+30	5.7	40.4
+41	6.6	39.5
+58.8 = SL	6.9	39.2

Sec D = 0+00

STATIONING on S.L.

3	6.8	39.3
6	6.7	39.4
10	6.3	39.8
2	5.7	40.4
1/4	5.4	40.7
1/2	5.3	40.8
3/4	4.5	41.6

44.08 E = 45.8 on N.L.

N	3.5	42.5
6	4.1	42.0
12	4.4	41.4
18	4.9	41.2
24	4.9	41.2
30	5.5	40.6

34607

cb		6.1	40.0
S		6.6	39.7
	88.16' E		
S		5.3	40.8
cb		5.5	40.6
1/4		5.0	41.1
c		4.4	41.7
1/4		4.1	42.0
cb		4.0	42.1
N		3.0	43.1

132.2' E = EC

N		3.3	42.8
cb		3.8	42.3
1/4		4.0	42.1
c		3.9	42.2
1/4		4.3	41.8
cb		5.2	40.8
S - 4 Conv. Drive		5.4	40.7

135.2'

S		5.3	40.8
cb		5.7	40.4

136.2'

cb		5.8	40.3
S		7.0	39.1
+5		7.4	38.7

34607

S. HUBURN 48

175' E

-5		6.7	39.4
cb		5.8	40.3
1/4		5.1	41.0
c		4.8	41.3
1/4		4.8	41.3
cb		5.1	41.0
N		4.6	41.5

200' E

N		5.4	40.7
cb		5.9	40.2
1/4		5.9	40.2
c		5.5	40.6
1/4		5.5	40.6
cb		5.8	40.3
S		6.3	39.8
+5		6.6	39.5

225' E

-5		7.0	39.1
S		6.8	39.3
cb		6.4	39.7
1/4		6.5	39.6
c		6.5	39.6
1/4		6.7	39.4
cb		6.9	39.2
N		6.3	39.8

3460.7

250' E

N	6.8	39.3
cb	7.3	38.8
1/4	7.8	38.3
e	7.6	38.5
1/4	7.5	38.6
cb	7.9	38.2
S	7.9	38.2
+5	8.0	38.1

275' E

-5	9.0	37.1
S	8.9	37.2
cb	8.8	37.3
1/4	8.5	37.6
e	8.2	37.9
1/4	8.2	37.9
cb	8.0	38.1
N	7.4	38.7

300' E

N	7.8	38.3
cb	8.2	37.9
1/4	8.2	37.7
e	8.5	37.6
1/4	8.8	37.3
cb	9.6	36.5
S	10.5	35.6
+5	11.4	34.7 ✓

346.07

S. AUBURN

49

325'

-5	11.2	34.9
S	10.4	35.7
cb	9.5	36.6
1/4	9.0	37.1
e	8.6	37.5
1/4	8.5	37.6
cb	8.1	38.0
N	7.5	38.6

350'

N	7.4	38.7
cb	8.0	38.1
1/4	8.2	37.8
e	8.2	37.8
1/4	8.7	37.4
cb	9.2	36.9
S	10.0	36.1
+5	10.2	35.8

375' E

-5	9.9	36.2
S	9.5	36.6
cb	9.6	36.5
1/4	8.2	37.9
e	7.7	38.4
1/4	7.8	38.3
+5	7.9	38.2 ✓

34607

cb		7.3	388	
N		6.7	394	
TP	5.55	34402	7.60	33847

412.74 = PC.

N		4.4	39.6
cb		5.2	38.8
1/4		5.5	38.5
C		5.4	38.6
1/4		5.8	38.2
cb		6.6	37.4
S		7.4	36.6
+5		7.7	36.3

437.75 E

-5		7.8	36.2
S		7.4	36.6
cb		6.4	37.6
1/4		5.7	38.3
C		5.1	38.9
1/4		5.0	39.0
cb		4.7	39.3
N		3.9	40.1

462.76

N		3.9	40.1
cb		4.5	39.5
1/4		4.9	39.1
C		4.8	39.2

34402

S. AUBURN 50

1/4		5.5	38.5
cb		6.2	37.8
S		7.1	36.9
+5		7.5	36.5

487.77 E

S		6.8	37.2
cb		6.0	38.0
1/4		5.6	38.4
S		5.2	38.8
1/4		4.9	39.1
cb		4.8	39.2
N		3.8	40.2

512.78 E

N		3.9	40.1
cb		4.5	39.2
1/4		5.1	38.9
C		5.1	38.9
1/4		5.2	38.8
cb		6.2	37.8
S		7.0	37.0

537.79 E = E.C.

S		7.2	36.8
cb		6.5	37.5
1/4		5.8	38.2
S		5.3	38.7
1/4		5.3	38.7

34402

cb	5.0	390
N	4.0	400
525' E		
N	4.5	395
cb	5.2	387
1/4	5.6	384
e	5.6	384
1/4	6.0	380
cb	6.4	37.2
S	7.6	364

600' E

S	7.7	363
cb	7.0	370
1/4	6.3	377
e	5.7	383
1/4	5.5	385
cb	5.6	384
N	4.7	393

650' E

N	4.6	394
cb	5.4	386
1/4	5.6	384
e	5.6	384
1/4	6.1	37.9
cb	6.7	37.3
S	7.2	36.8

34402 S. AUBURN 151

700' E

S	6.9	37.1
cb	6.5	37.5
1/4	6.4	37.6
e	6.0	38.0
1/4	6.2	37.8
+5	6.3	37.7
cb	5.9	38.1
N	5.6	38.4

725' E

N	6.0	38.0
cb	6.2	37.8
+3	6.7	37.3
1/4	6.6	37.4
e	6.2	37.7
1/4	6.5	37.5
cb	6.7	37.3
S	7.0	37.0

747.51' E = P.C.

S	7.1	36.9
cb	6.9	37.1
+2	7.5	36.5
1/4	7.2	36.8
e	6.6	37.4
1/4	6.9	37.1
cb	7.1	36.9

34402

N		6.9	37.1
	774.27 E		
N		8.2	35.8
cb		7.9	36.1
+3		8.4	35.6
1/4		7.9	36.1
c		7.5	36.5
1/4		8.1	35.9
+U		8.5	35.5
cb		7.4	36.6
S		7.4	36.6
	801.03		
S		8.2	35.7
cb		8.2	35.7
+5		8.4	35.6
1/4		10.1	33.9
e		9.6	34.4
1/4		9.9	34.1
+3		10.1	33.9
cb		9.7	34.3
N		10.6	33.4
T.P.	1.60	335.38	10.24
	827.79 E		
N		4.6	30.8
+6		3.8	31.6
cb		4.0	31.4

33538

S. HUBURN 52

1/4		4.1	31.3
c		4.0	31.4
1/4		4.3	31.1
+5		1.6	33.8
cb		1.4	34.0
S		1.1	34.3
	854.55 E		
c		4.1	31.3
cb		4.9	30.5
+2		5.5	29.9
+4		7.1	28.3
1/4		8.1	27.3
c		8.3	27.1
1/4		8.3	27.1
cb		8.2	27.2
+2		7.2	28.2
N		7.9	27.5
	881.31 E = P & C		
N		11.4	24.0
+1		10.9	24.5
+8		11.7	23.7
cb		11.8	23.6
1/4		11.6	23.8
c		11.8	23.6
1/4		11.9	23.5
+3		9.9	25.5

33538

cb		97	257
S		9.6	258
T.P.	0.851	323.70	12.53
	700.76'E		322.85
S		0.6	23.1
cb		0.3	23.4
1/4		1.3	22.4
+3		2.0	21.7
C	1945	1.4	22.3
1/4		1.5	22.2
cb		1.8	21.9
N		0.7	23.0
	920.21'E		
N		1.5	22.2
+3		1.8	21.9
+2		3.2	20.5
cb		3.1	20.6
1/4	1945	3.3	20.4
e		3.4	20.3
1/4		3.5	20.2
cb		2.1	21.6
S		2.1	21.6
	939.66'E		
S		4.6	19.1
cb		4.1	19.6
1/4		4.8	18.9

323.70

S AUBURN / 53

C		4.7	19.0
1/4		4.5	19.2
cb		4.6	19.1
+4	1945	4.7	19.0
N		2.8	20.9
	959.11'E		
N		4.3	19.4
+2		4.8	18.9
+4		5.8	17.9
+7		6.7	17.0
cb		6.6	17.1
1/4		6.5	17.2
C		6.2	17.5
1/4		6.2	17.5
+3		5.9	17.8
cb		6.5	17.2
S		7.4	16.3
	978.56'E		
S		10.1	13.6
cb		9.4	14.5
1/4		8.1	15.6
+4		8.6	15.1
C		8.4	15.3
1/4		8.4	15.3
cb		8.5	15.2
+5		8.3	15.4

32370

N	6.1	17.6	
	996.0' E = P.R. on SL + intersection of NE of SAUBURN ^{drive} and SL of Hubon		
N	9.2	314.5	
+J	10.2	13.5	
cb	12.0	13.7	
1/4	10.1	13.6	
c	10.2	13.5	
1/4	10.0	13.7	
cb	11.9	11.8	
S	14.0	09.7	
check to north pole	10.78	312.92	312.91
1.57	312.48	312.91	

1005.4' E STA. on S.L.

S	5.5	309.0
cb	4.3	10.2
1/4	1.9	12.6
c	1.9	12.6
1/4	2.1	12.4
cb	2.3	12.2
+S	2.3	12.2
N	3.1	11.4

1012.81 E

N	4.1	10.4
cb	3.4	11.1
1/4	3.3	11.2

312.48

S. HUBURN 54

C	3.1	11.4
1/4	3.9	10.6
cb	6.3	08.2
S	7.1	07.4
	1020.21 E	
S	9.3	05.2
cb	8.7	05.8
1/4	7.7	06.8
c	4.8	09.7
1/4	4.2	10.3
cb	4.6	09.9
N	4.8	09.7

1027.61 E

N	5.9	08.6
cb	8.3	06.2
1/4	10.1	04.4
c	11.4	03.1
1/4	11.5	03.0
cb	11.2	03.2
S	11.2	03.1
T.P.	105 1035.01	302.92
	12.61	301.87
S	2.1	300.8
cb	2.5	300.4
1/4	2.6	300.3
c	2.6	300.3
1/4	2.8	300.1

302.9v

d		2.8	300.1
w		2.5	300.4
	104.41' E		
N		6.3	296.6
d		5.9	297.0
1/4		6.2	296.7
c		5.4	297.5
1/4		5.3	297.6
C		5.1	297.8
S		4.0	298.9
	1049.81' E		
S		6.1	296.8
cb		7.2	295.7
1/4		7.5	295.4
e		8.6	294.3
1/4		9.1	293.8
cb		9.3	293.6
+5		12.3	290.6
N		11.5	291.4
	1057.21' E		
N		14.4	288.5
cb		14.8	288.1
+3		15.6	287.3
+4		14.4	288.5
1/4		13.4	289.5
+3		12.4	290.5

302.9v

S HUBURN 55

C		11.8	291.1	
1/4		10.9	292.0	
cb		9.8	293.1	
S		8.1	294.8	
	1064.41' E			
S		10.1	292.8	
cb		12.1	290.8	
T.P.	0.73	290.78	12.87	290.05
1/4		1.2	89.6	
c		2.4	88.4	
1/4		6.1	84.7	
+3		4.7	86.1	
cb		4.8	86.0	
N		5.0	85.8	
	1072.01' E = EC			
N		7.3	83.5	
cb		7.0	83.8	
1/4		6.9	83.9	
+2		7.6	83.2	
c		4.8	86.0	
1/4		-3.0	87.8	
cb		-1.6	89.2	
S		+0.2	91.0	
	11.00' E			
S		-4.0	86.5	
cb		5.3	85.5	

29078

1/4		6.5	843
0		8.6	822
1/4		11.4	79.4
cb		11.1	79.7
N		10.7	80.1
+15		13.2	77.6
	1125' E		
-15		16.7	74.1
N		14.0	76.8
cb		14.3	76.5
+4		14.7	76.1
1/4		13.9	76.9
0		12.3	78.5
1/4		9.7	81.1
cb		8.5	82.3
S		7.6	83.2
	1150' E		
S		10.0	80.8
cb		11.4	79.4
1/4		12.5	78.3
T.P.	001	12.52	78.26
+4		0.5	77.8
0		2.2	76.1
1/4		5.0	73.3
cb		5.3	73.0
N		5.3	73.0

278.27

S. HUBURN

56

+7		8.2	70.1
+15		9.6	68.7
	1175' E		
-15		12.7	65.6
-5		11.0	67.3
N		9.1	69.2
cb		8.7	69.6
1/4		8.9	69.4
+6		8.9	69.4
0		7.9	70.4
1/4		5.8	72.5
cb		3.7	74.6
S		0.7	77.6
	1200' E		
S		7.6	70.7
cb		9.5	68.8
+5		10.1	68.2
1/4		11.3	67.0
0		12.4	65.9
T.P.	020	12.80	65.47
1/4		0.0	65.7
+5		0.0	65.7
cb		0.6	65.1
N		3.1	62.6
+15		4.1	61.6

26567

1225' E

-15	6.1	59.6
N	5.4	60.3
cb	4.5	61.2
1/4	3.2	62.5
c	3.1	62.6
1/4	3.2	62.5
cb	2.0	63.7
S	1.1	64.6

1275' E

S	6.5	59.2
cb	7.3	58.4
1/4	7.6	58.1
c	7.6	58.1
1/4	8.1	57.6
cb	8.5	57.2
N	9.0	56.7
+10	9.1	56.6

1325' E

-10	10.6	55.1
N	10.6	55.1
cb	10.5	55.2
1/4	9.8	55.9
c	9.9	55.8
1/4	9.6	56.1
cb	9.7	56.0

26567

S HUBURN

57

S 9.3 56.4

1375' E

S	12.7	53.0
cb	12.6	53.1
1/4	12.7	53.0
c	13.2	52.5
T.P	2.50	55.26
1/4	12.9	52.76
cb	2.2	52.9
N	2.3	53.0
+10	2.5	52.8

1400' E

-10	3.6	51.7
N	3.5	51.8
cb	3.6	51.7
1/4	4.1	51.2
c	4.5	50.8
1/4	4.5	50.8
cb	3.5	51.8
S	2.8	52.5

FINIS

Continued from Book 1130 Page 23

Dorrison
Bliss
Northern July 10th 25

Xsection of Muir Ave Thru Ocean View Add.

50 ft 10' Gls 7 1/2' Quarters.

2.79 108.98 ✓

106.19 Cor Pipe on Dix
Line Between Ocean
View & Sunset Grove.
N Side of Muir Ave.
Beds Page

4+972 = Division line between Ocean View & Sunset Grove

4+978

N.L.-10	3.5	105.5 ✓
N.L.	2.8	106.2 ✓
Cb	1.8	107.2 ✓
1/4	1.2	107.8 ✓
E	0.6	108.4 ✓
1/4	0.0	109.0 ✓
Cb	+ 0.7	109.7 ✓
S.L.	+ 1.4	110.2 ✓
	5+25	
S.L.	2.3	106.7 ✓
Cb	3.0	106.0 ✓
1/4	3.7	105.3 ✓
E	4.1	104.9 ✓
1/4	4.5	104.5 ✓
Cb	5.2	103.8 ✓
N.L.	6.1	102.9 ✓
+10	6.9	102.1 ✓
	5+50	
N.L.-10	9.6	99.4 ✓

108.98

58

N.L.	8.9	100.1 ✓
Cb	8.4	100.6 ✓
1/4	7.4	101.6 ✓
E	7.3	101.7 ✓
1/4	6.9	102.1 ✓
Cb	6.4	102.6 ✓
S.L.	5.6	103.4 ✓
	5+75	
S.L.	8.7	100.3 ✓
Cb	9.5	99.5 ✓
1/4	9.9	99.1 ✓
E	10.1	98.9 ✓
1/4	10.4	98.6 ✓
Cb	11.2	97.8 ✓
N.L.	11.8	97.2 ✓
N.L.+10	12.3	96.7 ✓
H	0.24	96.21 ✓
	6+00	
N.L.-10	2.1	94.1 ✓
N.L.	1.7	94.5 ✓
Cb	1.1	95.1 ✓
1/4	0.3	95.9 ✓
E	+0.2	96.4 ✓
1/4	0.3	95.9 ✓
Cb	+0.4	96.6 ✓
S.L.	+1.1	97.3 ✓

	+	π	-	
		96.21		
		6+25		
S.u.			1.5	94.7 ✓
cb			2.0	94.2 ✓
1/4			2.8	93.4 ✓
+			2.4	93.8 ✓
1/2			3.5	92.7 ✓
cb			3.4	92.8 ✓
M.u.			3.6	92.6 ✓
		6+50		
M.u.			6.3	89.9 ✓
cb			5.7	90.5 ✓
+3			6.1	90.1 ✓
1/2			5.5	90.7 ✓
+			4.8	91.4 ✓
1/4			5.1	91.1 ✓
cb			4.9	91.3 ✓
S.u.			4.3	91.9 ✓
		6+75		
S.u.			6.9	89.3 ✓
cb			7.1	89.1 ✓
1/4			8.3	87.9 ✓
+			7.7	88.5 ✓
++			7.7	88.5 ✓
1/4			9.1	87.1 ✓
++			8.8	87.4 ✓
cb			8.2	88.0 ✓
M.u.			8.7	87.5 ✓

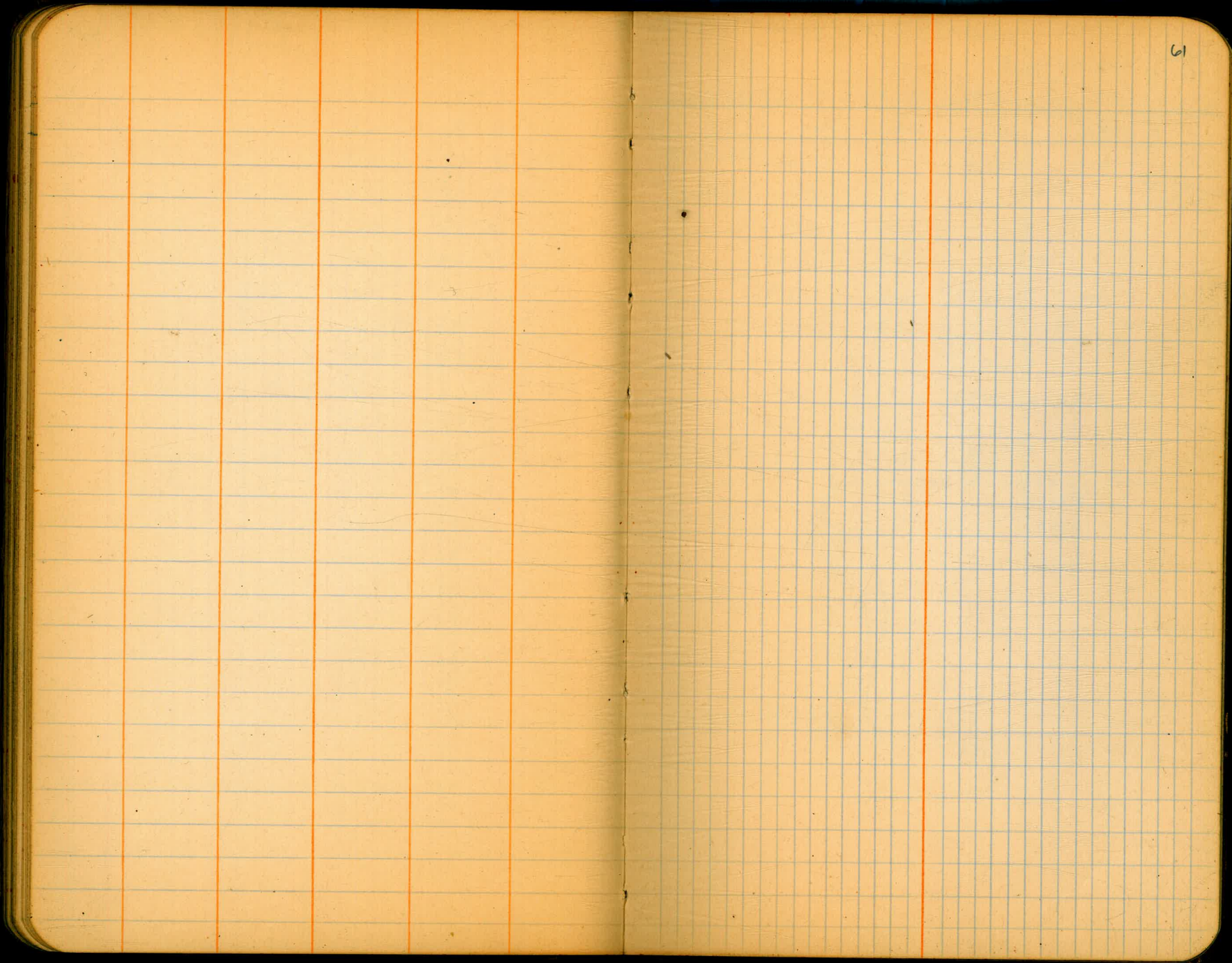
	+	π	-	
		96.21		59
		7+00		
M.u.			11.0	85.0 ✓
cb			10.5	85.7 ✓
+3			11.4	84.8 ✓
1/2			11.2	85.0 ✓
++			10.9	85.3 ✓
+			10.7	85.5 ✓
1/4			10.7	85.5 ✓
+6			10.2	86.0 ✓
cb			9.6	86.6 ✓
S.u.			9.1	87.1 ✓
		7+25		
S.u.			11.5	84.7 ✓
+9			11.7	84.5 ✓
cb			12.1	84.1 ✓
+5			13.1	83.1 ✓
H	2.90	86.96 ✓	12.15	84.06
1/2			4.0	83.0 ✓
+4			3.9	83.1 ✓
+			4.8	82.2 ✓
1/2			4.6	82.4 ✓
+2			4.4	82.6 ✓
cb			3.7	83.3 ✓
M.u.			4.1	82.9 ✓
		7+35		
M.u.			5.2	81.8 ✓

	+	π 86.96	-	
cb			4.7	82.3 ✓
+4			5.6	81.4 ✓
1/4			6.0	81.0 ✓
±			6.5	80.5 ✓
+2			6.6	80.4 ✓
1/2			6.3	80.7 ✓
+3			6.0	81.0 ✓
cb			2.0	83.5 ✓
S.L.			2.3	83.7 ✓

7+38⁶ = E.L. Guizot St.

S.L.			7.4	79.6 ✓
cb On cement Curb			7.88	79.08 ✓
Gutter level with curb			7.9	79.1 ✓
1/4			7.4	79.6 ✓
±			7.2	79.8 ✓
1/4			7.6	79.4 ✓
Gutter level with curb			8.9	78.1 ✓
On cement cb			8.88	78.08 ✓
N.L.			8.7	78.3 ✓
#			7.72	79.24 = 79.13 See Page Book

N.B. There is a 4' concrete retaining wall on the East side of Guizot St built across the west sidewalk of Muir St, but the owner says he is going to remove the portion in the St. immediately.

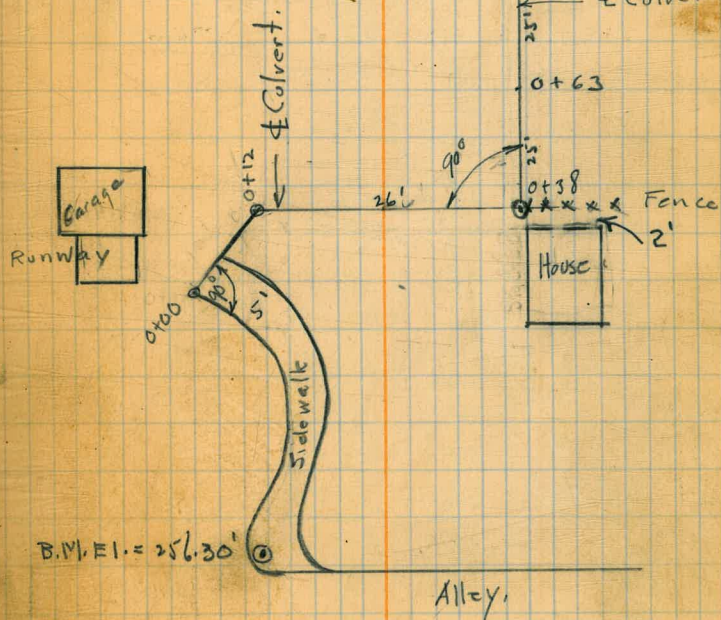


61

Henny
Stark } Aug. 17-1925

Level lines for Culvert from N.L. Eagle St. to Bottom of Canyon

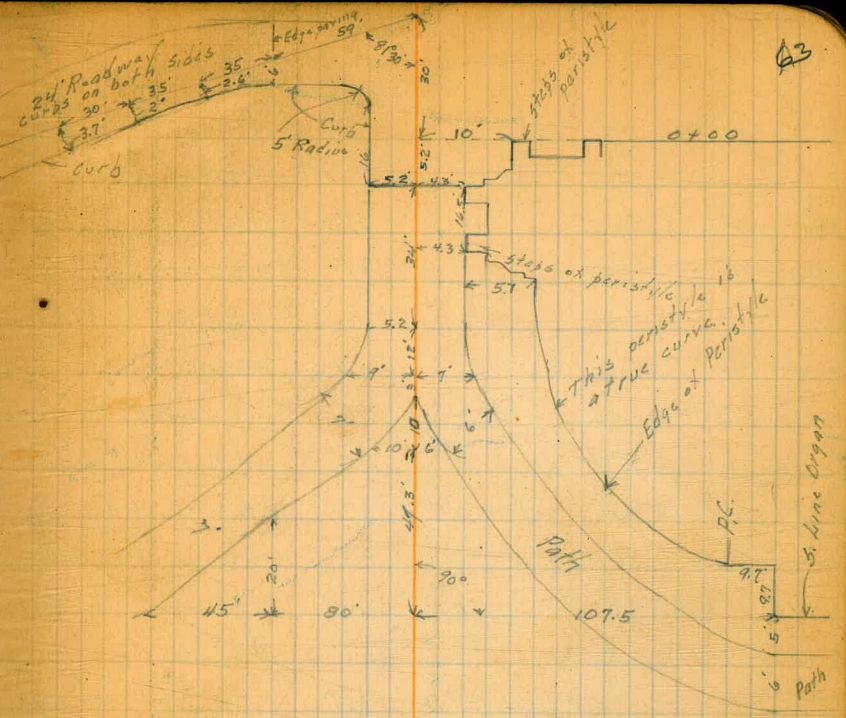
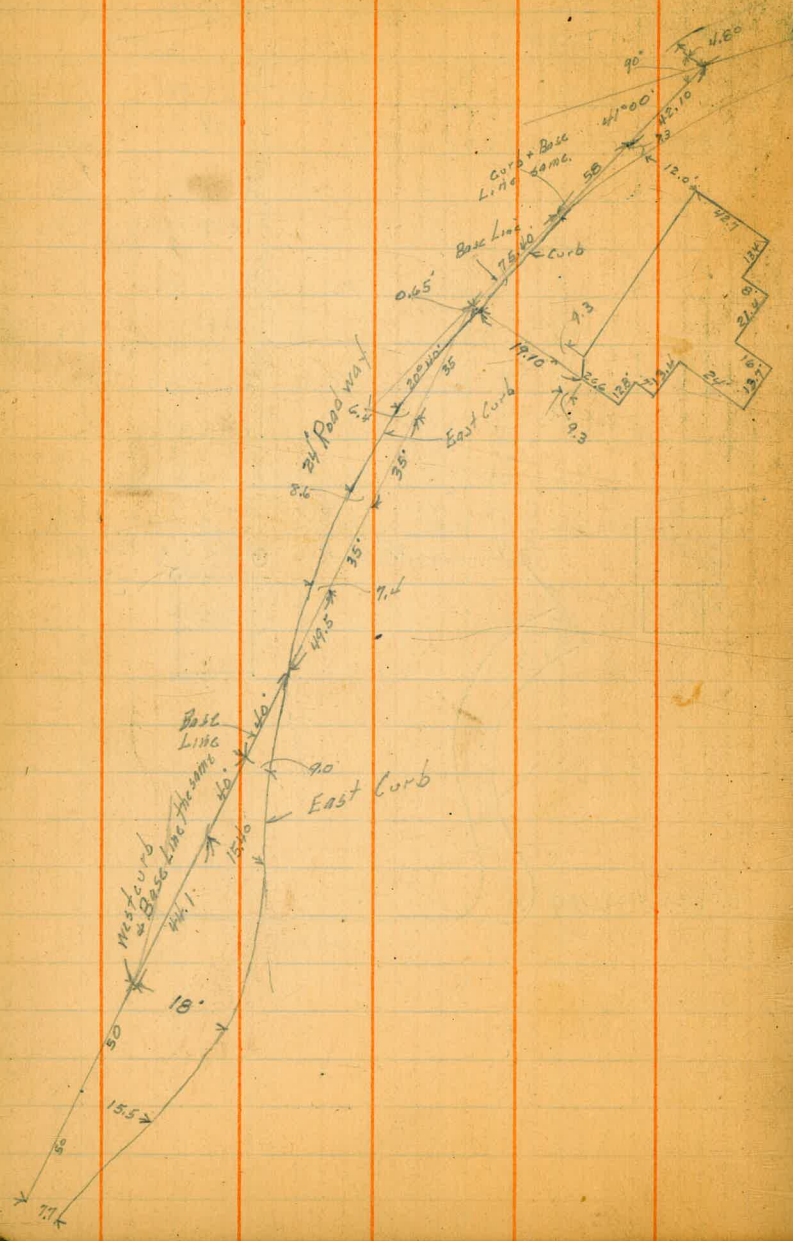
	B.S.	H.I.	F.S.	Elev.	
B.M.	1.69	257.99		256.30	✓ NE Cor Alley.
Location of Catch Basin			1.9	256.10	✓ Top of Corb.
0+1 ✓			3.3	254.7	✓
0+38			5.3	252.7	✓
T.P.	0.99	252.24 ✓	6.95	251.24 ✓	
0+63 TP			7.72	249.52 ✓	
0+88 TP	0.05 ✓	204.77 ✓	11.21	233.56 ✓	
1+13 TP	0.17	233.73 ✓	10.7	223.0 ✓	
1+38 TP	0.16	223.16 ✓	9.06	214.10 ✓	
1+73	0.01	214.11 ✓	10.65	203.46	✓ Bottom of Canyon



62

8/24/11
Gregory

Contour Survey of Rose Garden
South of Oregon Balboa Park.



Q3

20' = 1''

8/24/25

Gregory

Levels on Rose Garden
S. of Dragon Pavilion
Bellevue Park

64

	0.27	780.37	200.00	Top of Level of 5965 Assumed level				
0+00 on A Line ✓			196.77 ✓		2+00 & 50' W of A Line	8.0	192.4 ✓	
0+39 ✓ A ✓			196.6 ✓		2+00 & on ✓	8.8	191.6 ✓	
0+50 ✓ ✓ ✓			196.4 ✓		2+00 & 50' E of ✓	9.7	190.7 ✓	
0+50-9' W of A Line ✓			196.1 ✓		2+00 & 100' ✓	11.5	188.9 ✓	
0+50 & 7' E ✓ ✓			196.4 ✓		2+00 & 130' ✓	14.7	185.7 ✓	
1+11.5 on A Line ✓			194.7 ✓		2+00 & 140' ✓	19.4	181.0 ✓	
1+11.5 & 50' W of A Line ✓			194.1 ✓		2+50 & 125' E ✓	14.9	185.5 ✓	
1+11.5 & 100' ✓ ✓ ✓			194.3 ✓		2+50 & 100' ✓	12.6	187.8 ✓	
1+11.5 & 105' ✓ ✓ ✓ = Edge path			193.4 ✓		2+50 & 50' ✓	10.0	190.4 ✓	
1+11.5 & 50' E ✓ ✓ ✓			195.3 ✓		2+50 & on ✓	9.5	190.9 ✓	
1+11.5 & 77' ✓ ✓ ✓ = Edge path			194.3 ✓		2+50 & 50' W of ✓	8.2	192.2 ✓	
1+11.5 & 107' ✓ ✓ ✓ = Dragon			194.1 ✓		2+50 & 100' ✓	7.4	193.0 ✓	
1+50' & 50' ✓ ✓ ✓			192.0 ✓		2+50 & 150' ✓	9.1	191.3 ✓	
1+50 & 100' ✓ ✓ ✓			190.1 ✓		2+50 & 200' ✓	10.0	190.2 ✓	
1+50 & 135' ✓ ✓ ✓			188.2 ✓		2+50 & 217' ✓ ✓ ✓ = Edge path	10.9	189.5 ✓	
1+50 & 130' ✓ ✓ ✓			185.4 ✓		T.P. 6.18 195.88	10.67	189.70	
1+50 & 50' W ✓ ✓ ✓			193.5 ✓		3+00 & 215' W of A Line	10.1	185.8 ✓	
1+50 & 100' ✓ ✓ ✓			193.9 ✓		3+00 & 225' ✓	7.1	188.8 ✓	
1+50 & 150' ✓ ✓ ✓			193.4 ✓		3+00 & 200' ✓	7.0	188.9 ✓	
1+50 & 170' ✓ ✓ ✓ = E. Edge path			192.0 ✓		3+00 & 165' ✓	7.3	188.6 ✓	
2+00 & 206' ✓ ✓ ✓ ✓			190.1 ✓		3+00 & 145' ✓	5.8	190.1 ✓	
2+00 & 200' ✓ ✓ ✓			191.1 ✓		3+00 & 125' ✓	6.5	189.4 ✓	
2+00 & 150' ✓ ✓ ✓			193.0 ✓		3+00 & 100' ✓	5.0	190.9 ✓	
2+00 & 100' ✓ ✓ ✓			194.0 ✓		3+00 & 65' ✓	3.7	194.2 ✓	
					3+00 & on A Line	5.8	190.1 ✓	
					3+00 & 50' E of ✓	6.6	189.3 ✓	

3+00	&	100	Fox A Line	9.0	186.9	✓
3+00	&	107	✓ ✓ ✓	10.0	185.9	✓
3+50	&	124	✓ ✓ ✓	12.0	183.9	✓
3+50	&	118	✓ ✓ ✓	10.5	185.4	✓
3+50	&	100	✓ ✓ ✓	9.2	186.7	✓
3+50	&	50	✓ ✓ ✓	8.9	187.0	✓
3+50	&		on ✓	7.1	188.8	✓
3+50	&	35	W ox ✓	5.6	190.3	✓
3+50	&	70	✓ ✓ ✓	5.0	190.9	✓
3+50	&	100	✓ ✓ ✓	6.2	189.7	✓
3+50	&	130	✓ ✓ ✓	8.6	187.3	✓
3+50	&	150	✓ ✓ ✓	8.3	187.6	✓
3+50	&	170	✓ ✓ ✓	9.6	186.3	✓
3+50	&	200	✓ ✓ ✓	9.0	186.9	✓
3+50	&	250	✓ ✓ ✓	9.8	186.1	✓
3+90	&	399	✓ ✓ ✓ ✓ = Pond	15.7	180.2	✓
3+90	&	350	✓ ✓ ✓	15.2	180.7	✓
3+90	&	300	✓ ✓ ✓	13.4	182.5	✓
3+90	&	250	✓ ✓ ✓	12.0	183.9	✓
4+00	&	200	✓ ✓ ✓	11.4	184.5	✓
4+00	&	185	✓ ✓ ✓	11.8	184.1	✓
4+00	&	150	✓ ✓ ✓	10.1	185.8	✓
4+00	&	100	✓ ✓ ✓	7.6	188.3	✓
4+00	&	65	✓ ✓ ✓	5.8	190.1	✓
4+00	&	35	✓ ✓ ✓	6.4	189.5	✓
4+00	&		on A ✓	8.2	187.7	✓

ROSE GARDEN 65

4+00	+ 15'	Fox A Line	9.6	186.3	✓	
4+00	&	25	✓ ✓ ✓	13.3	182.6	✓
4+00	+ 45'	✓ ✓ ✓	22.3	173.6	✓	
4+00	+ 65	✓ ✓ ✓	9.7	186.2	✓	
4+00	+ 125	✓ ✓ ✓	9.9	186.0	✓	
4+00	+ 135	✓ ✓ ✓	12.9	183.0	✓	
4+15	&	100	✓ ✓ ✓	9.5	186.4	✓
4+50	+ 15'	✓ ✓ ✓	11.2	184.7	✓	
4+50	&	on ✓	9.4	186.5	✓	
4+50	+ 40'	W, ox ✓	7.1	188.8	✓	
4+50	+ 75	✓ ✓ ✓	7.3	188.6	✓	
4+50	+ 100	✓ ✓ ✓	7.9	188.0	✓	
4+50	+ 150	✓ ✓ ✓	9.7	186.2	✓	
4+50	+ 200	✓ ✓ ✓	12.4	183.5	✓	
4+50	&	235	✓ ✓ ✓	15.2	180.7	✓
4+50	+ 300	✓ ✓ ✓	17.3	178.6	✓	
4+80	+ 300	✓ ✓ ✓	19.2	176.7	✓ edge canopy	
4+50	+ 350	✓ ✓ ✓	17.7	178.2	✓	
4+50	+ 428	✓ ✓ ✓ = Pond	17.4	177.5	✓	
4+70	+ 350	✓ ✓ ✓	17.8	178.1	✓ edge canopy	
T.P.	7.11	190.24	12.75	183.13	✓	
5+00	+ 290	W ox A Line	14.9	175.3	✓ edge canopy	
5+20	+ 250	✓ ✓ ✓	12.0	178.2	✓	
5+00	+ 225	✓ ✓ ✓	11.2	179.0	✓	
5+00	+ 220	✓ ✓ ✓	9.9	180.3	✓	
5+00	+ 200	✓ ✓ ✓	7.1	183.1	✓	
5+00	+ 165	✓ ✓ ✓	4.7	185.5	✓	

5+00 + 100' W of A Line	3.1	187.1	✓
5+00 + 50 ✓ ✓ ✓ ✓	2.8	187.4	✓
5+00 + 07 ✓ ✓ ✓ ✓	5.0	185.2	✓
5+00 + 24 E ox ✓ ✓	7.9	182.3	✓
5+50 + 25 ✓ ✓ ✓ ✓	10.8	179.4	✓
5+50 + 3 ✓ ✓ ✓ ✓	6.3	183.9	✓
5+50 + 10' W ✓ ✓ ✓ ✓	6.3	183.9	✓
5+50 + 35 ✓ ✓ ✓ ✓	4.6	185.6	✓
5+50 + 100 ✓ ✓ ✓ ✓	4.1	186.1	✓
5+50 + 165' ✓ ✓ ✓ ✓	6.3	183.9	✓
5+50 + 190' ✓ ✓ ✓ ✓	8.7	181.5	✓
5+50 + 193 ✓ ✓ ✓ ✓	10.1	180.1	✓
5+50 + 235 ✓ ✓ ✓ ✓	13.7	176.5	edge corner
6+00 + 200 ✓ ✓ ✓ ✓	13.3	176.9	✓
6+00 + 182 ✓ ✓ ✓ ✓	9.5	180.7	✓
6+00 + 162 ✓ ✓ ✓ ✓	8.8	181.4	✓
6+00 + 158 ✓ ✓ ✓ ✓	7.7	182.5	✓
6+00 + 100 ✓ ✓ ✓ ✓	6.0	184.2	✓
6+00 + 50' ✓ ✓ ✓ ✓	5.7	184.5	✓
6+00 + 07 ✓ ✓ ✓ ✓	7.8	182.4	✓
6+00 + 20 E ox ✓ ✓ ✓ ✓	12.0	178.2	✓
6+50 + 40 ✓ ✓ ✓ ✓	13.5	176.7	✓
6+50 + 07 ✓ ✓ ✓ ✓	10.1	180.1	✓
6+50 + 30' W ox ✓ ✓	7.3	182.9	✓
6+50 + 100 ✓ ✓ ✓ ✓	7.5	182.7	✓
6+50 + 120 ✓ ✓ ✓ ✓	8.0	182.2	✓

6+50 + 150' W of A Line	10.3	179.9	✓
6+50 + 165 ✓ ✓ ✓ ✓	12.9	177.3	✓
7+00 + 125' ✓ ✓ ✓ ✓	13.0	177.2	✓
7+00 + 100' ✓ ✓ ✓ ✓	10.7	179.5	✓
7+00 + 60' ✓ ✓ ✓ ✓	8.5	181.7	✓
7+00 + 25' ✓ ✓ ✓ ✓	8.7	181.5	✓
7+00 + 10' on A ✓ ✓	11.6	178.6	✓
7+00 + 10' E ox ✓ ✓	13.2	177.0	✓
7+25 + 07 on A Line	12.2	178.0	✓
7+50 + 10' E ox ✓ ✓	15.7	174.5	✓
7+50 + 07 on A ✓ ✓	13.9	176.3	✓
7+50 + 45' W ox ✓ ✓	11.0	179.2	✓
7+90 + 45 ✓ ✓ ✓ ✓	16.2	174.0	✓
8+00 + 80' ✓ ✓ ✓ ✓	18.0	172.2	✓
7+50 + 80' ✓ ✓ ✓ ✓	12.3	177.9	✓
7+50 + 100 ✓ ✓ ✓ ✓	15.4	174.8	✓
7+80 + 100 ✓ ✓ ✓ ✓	18.4	171.8	✓
7+50 + 110 ✓ ✓ ✓ ✓	17.0	173.2	✓

Cross Section Crane Place
From S Line Satter to 110'S PC.

40 wide
5' obs.
7/8 GTS

BM	3.56	260.55	256.90
TR	5.77	260.80	255.03
		0+0 = S.L. Satter St.	
E		5.7	255.10
CB Top		5.77	255.03
Gutter Top Fining		6.38	254.42
" "		6.44	254.56
B		6.44	254.56
" "		6.41	254.39
Gutter "		6.81	253.99
CB Top		6.30	254.50
" "		6.22	254.58
	7.15		
" "		5.6	255.2
CB		6.2	254.6
7.1		6.5	254.3
7.4		6.4	254.4
B		6.2	254.6
7.4		6.2	254.6
7.2		6.1	254.7
CB		4.2	256.6
E		2.9	258.4
7.2		1.6	259.2
1.5		1.3	259.5

25.9

SPINE ON
Satter
Guldfach

See 931-B
CAT 9-8-21

No Carbin on Crane Place

260.80

-5	0.9	259.9
E	1.8	259.0
CB	3.7	257.1
7.5	5.5	255.3
7.4	5.7	255.1
E	5.8	255.0
7.4	5.5	255.3
CB	5.2	255.5
7.2	5.0	255.8
	50.9	
" "	4.8	256.0
CB	5.0	255.8
7.2	5.2	255.6
7.4	4.9	255.9
E	4.8	256.0
7.4	4.8	256.0
7.4	4.6	256.2
CB	4.0	256.8
E	2.5	258.3
7.5	1.1	259.7
	75.9	
-5	1.7	259.1
E	3.1	257.7
CB	4.4	256.4
7.4	4.7	256.1

67

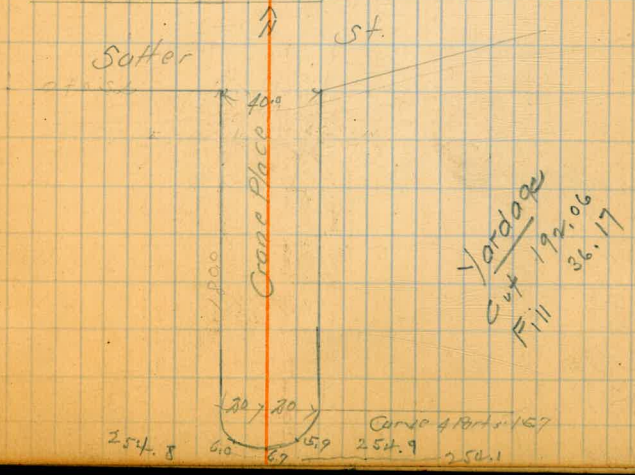
3.5-4.5
Satter
7.15
Highway

Gross Section Crane Place

	26080	26080	26080
2	48	256.0	
1/4	49	255.9	
CB	50	255.8	
1/4	48	256.0	
100'S			
1/4	51	255.7	
CB	50	255.8	
1/4	50	255.8	
2	48	256.0	
1/4	50	255.8	
CB	48	256.0	
E	49	257.9	
1/2	115	259.3	
125'S			
-2	30	258.8	
E	30	257.8	
+1	40	256.8	
CB	47	256.1	
1/4	49	255.9	
2	50	255.8	
1/4	51	255.7	
CB	52	255.6	
1/2	52	255	
150'S			
1/4	50	255.8	

See 931-B

	26080	26080
CA	53	255.5
1/4	54	255.4
E	53	255.5
1/4	52	255.6
CB	52	255.6
1/4	49	256.0
E	48	256.6
1/2	38	257.6
180'S		
E	53	255.5
CB	58	254.9
1/4	59	254.9
2	60	254.8
1/4	61	254.7
CB	62	254.6
1/4	66	254.2

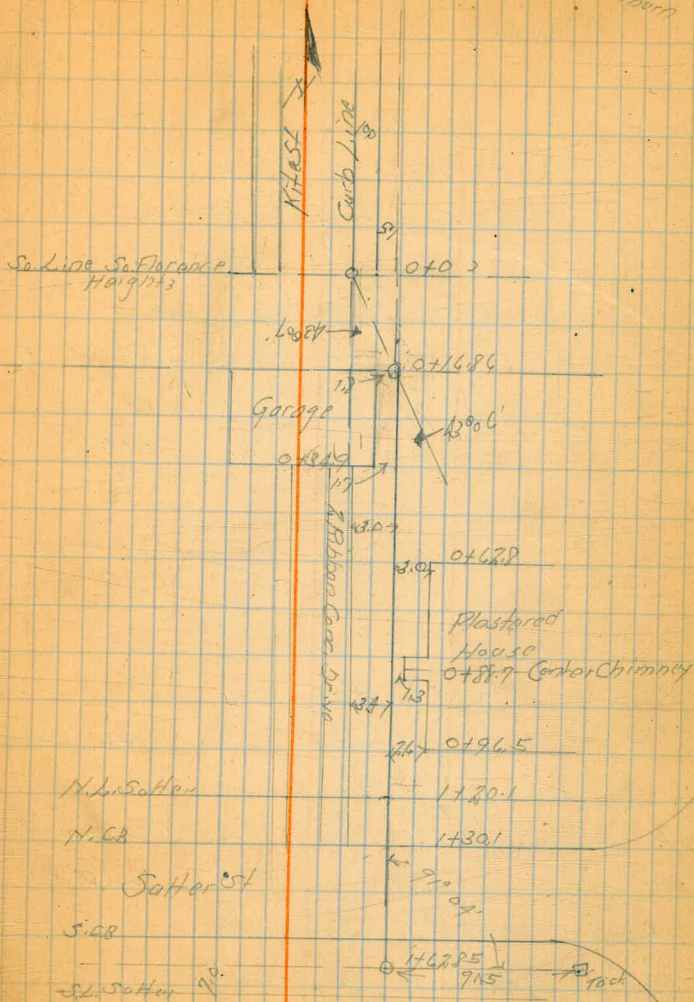


Proposed Culvert

Through portion of 1/4 of 1/4 of 1/4 of P.L. 1122.
And S.W. 1/4 of 1/4 of 1/4 of P.L. 1122

B.M.	1181	273.81	262.00	32N.M. Sackman Sutter	
1+60.1	S.C.B. Sutter St.	8.09	265.72	See 730-B & 732-B	
1+45.1	do Sutter St.	9.01	265.80		
1+30.1	Top curb north Sutter	7.67	266.14		
	Gutter Top Paving	8.28	265.53		
1+23	" " " "	7.45	266.36		
115		5.3	268.5		
1+00		4.8	269.0		
0+88		4.7	269.1		
0+63		4.3	269.5		
0+45		4.2	269.6		
0+35		3.5	270.3		
TP					
0+16.8	to 569	276.11	3.39		270.42
0+8			4.9	271.2	
0+0	Top Curb End of Right of Way		5.30	270.81	
TP	3.13	2735.5	5.69	270.42	
B.M.			11.56	261.99	32N.M. Sackman Sutter

9-5-25
Sackman
Sutter
Northern



Sackman

7th + 8th

Penn + Robinson CROSS SECTION
OF ALLEY 20' wide

BIK 7 CRITTENDEN ADD.

NWDP 120 ✓88.06 286.86 Penn + 6th

T.P. 129 ✓77.65 1170 ✓76.36

35' S of NL ON BL ALLEY

E 7.3 270.3

0+00 = NL OF PENN. AVE

E 6.5 271.1 Fence in Alley

C 6.7 271.0

+8 6.8 270.9

W 6.5 271.2

25' N

W 6.0 271.7

+5 6.5 271.2

C 6.4 271.3

E 6.2 271.5 Fence 5' in alley

T.P. 5+1 ✓76.89 6.7 271.48

4' N

E & Garage dirt floor 5.0 271.9

C 5.4 271.5

W 5.2 271.7

+6 ✓ ✓ ✓ ✓ 4.4 272.5

57' N

W 4.1 272.8

+3 5.3 271.6

C 5.2 271.7

E 4.6 272.3

Moore
10/6/85

276.89

70

+1.5 & Conc. Apron 4.5 272.4

+3.5 & Garage concrete floor 4.35 272.54

93' N

E 4.4 272.5

C 4.8 272.1

W 4.2 272.7

+4.4 & Garage 4.1 272.8

125' N

W 3.8 273.1

C 4.2 272.7

E 3.2 273.7

142' N

E 3.0 273.9

C 3.7 273.2

W 3.2 273.7

+3 & Garage dirt floor 3.0 273.9

155' N

E & Garage dirt floor 2.6 274.3 6' out

160' N

W & of Double garage dirt floor 2.5 274.4

C 2.9 274.0

E 2.4 274.5

195' N

E & garage dirt floor 1.9 275.0 1' out

C 2.5 274.4

W 2.2 274.7

276.89

TP.	5.70	280.95	16.4	275.25
	225' N			
W			5.9	275.0
C			5.8	275.1
+7			5.1	275.8
E			4.3	276.6
	240.5' N			
-3.4	⊕ Garage Conc floor		4.6	275.3
-1.4	✓	✓ Floor	4.77	276.18
E			5.0	275.9
C			5.4	275.5
W			5.7	275.2
+5.3	⊕ garage ^{conc.} floor		5.7	275.48
	263' N			
-5.5	⊕ double garage floor?		4.9	276.0
W			4.9	276.0
C			4.8	276.1
E			4.0	276.9
	292' N			
-5.2	⊕ garage wood floor		3.60	277.35
E			4.2	276.7
C			4.8	276.1
W			4.7	276.2
	343' N			
W			4.6	276.3
C			4.5	276.4

280.95

71

E			4.5	276.2
+3.2	Conc Floor		4.25	276.7
+4.9	⊕ Garage Conc floor		4.15	276.8
	357' N			
E	⊕ Garage Conc floor		4.6	276.3
	370' N			LAST Garage on ALLEY
E			4.7	276.2
C			4.7	276.2
W			4.9	276.0
	400' N	S edge of Canyon		
W			5.8	275.1
C			5.5	275.4
E			6.1	274.8

11/21/25
Moore

CROSS SECTION OF
ALLEY BIK 97 UNIV. HGTS 20' wide

N.W. BP	2.68	350.68	348.00	MEASUREMENT CAMPUS
T.P.	7.9	348.56	9.31	341.37
		NL VAN BUREN 20x200		<u>348.6</u>
W	ON PAVING	6.67		341.89
C	✓	6.67		341.89
E	✓	6.41		342.15
	9' N			
E		5.4		343.2
C		5.9		342.7
W		5.5		343.1
	50' N			
W		4.9		343.7
C		5.2		343.4
E		4.3		344.3
	70' N			
- G	Garage dirt floor	4.3		344.3
E		4.8		343.8
C		5.0		343.6
W		4.9		343.7
	105' N			
- 1.5'	SE of Garage dirt floor	4.1		344.5
W		4.2		344.4
C		4.7		343.9
E		4.4		344.2
+ G	Garage dirt floor	4.2		344.4

So. ENTRANCE

348.56

72

	120' N			<u>348.6</u>
E		3.0		345.6
+ 4		3.8		344.8
C		4.2		344.4
+ 8.5		3.2		345.2
	125' N = NL of Garage	dirt floor	1.5' in alley	
	133' N = G	wood	1.5' in alley	12' wide
W		3.3		345.3
C		3.4		345.2
E		3.2		345.4
T.P.	528	350.48	336	345.20
	159' N			<u>350.5</u>
- G	Garage CONC. floor	4.83		345.65
E		5.2		345.3
C		5.4		345.1
+ 8	fence 2' in alley			
W		5.0		345.5
	187' N			
W		4.2		346.3
+ 1	Eucalyptus tree	14" diam		
C		4.7		345.8
E		4.6		345.9
	200' N			
E		4.3		346.2
C		4.3		346.2
+ 7.5	fence 2.5' in alley			
W		4.5		346.0

			350.5
	240' N		
W		4.0	346.5
+ 2.5 fence in alley 2.5		4.1	346.4
C		4.1	346.4
E		4.0	346.5
+ 4.8 double Garage dirt floor		3.7	346.8
	275' N		
- 5 double Garage Conc floor		3.47	347.01
E		3.5	347.0
C		3.6	346.9
W		3.5	347.0
	286' N		
W 3 door Garage Conc floor	3.29	2.29	346.21
C		3.6	346.9
E		3.7	346.8
	314' N = SL of 4 door Garage Conc floor		
- 4		3.40	347.10
E		3.5	347.0
C		3.2	347.3
W		3.1	347.4
	333' N		
- 1.8 Garage dirt floor		3.1	347.4
W		3.1	347.4
C		3.3	347.2
E		3.4	347.1

			350.5
	349' N = NL of 4 door Garage Conc floor		
- 4		3.22	347.26
E		3.6	346.9
C		3.6	346.9
W		3.0	347.5
	365' N =		
W		2.5	348.0
+ 3		3.2	347.1
C		3.7	346.8
E		3.9	346.6
+ 4 E 3 door Garage dirt floor		3.9	346.6
	394' N		
E		3.8	346.7
C		3.6	346.9
W		3.4	347.1
+ 0.4 E Conc. Apron		3.38	347.10 12' wide
	430' N		
W		3.7	346.8
C		4.2	346.3
E		4.3	346.2
T.P. 559	351.95	4.1	346.36
	460' N		352.0
- 11 Garage Conc floor		5.26	346.74
E		5.5	346.5
C		5.4	346.6
W		5.4	346.6

351.95

	490' W		342.0	
W		5.7	346.3	
C		5.4	346.6	
E		5.6	346.4	
	516' W			
- 1.1	Garage Conv. Floor	5.38	346.82	
E		5.5	346.5	
C		5.5	346.5	
W		5.4	346.6	
	500' W = S.E. of shed W. in alley 10' wide			
	512' W = S end of lath fence W. in alley			
	504' W = N. v. v. v. v. 21' v. v.			
	550' W			
W		5.1	346.9	
C		5.1	346.9	
E		5.0	347.0	
	575' W			
E		4.7	347.3	
C	M.H.	4.8	347.2	
W		4.9	347.1	
	600' W = S.E. Meade Ave.			
W	on paving	5.09	346.86	
C	✓ ✓	5.19	346.76	
E	✓ ✓	4.70	347.25	
check to B.M.		3.91	348.04	348.00

Cross Section G-54

From E.L. 32nd St. to E.L. 33rd St.

60' wide
10' Sbs
10' Gts

72
1.14.26
5.15.20
3.15.20
10' 9' 15"

Six Man
F. 12.20.20

B.M.	011	9427 ✓	9416
TP	346	8514 ✓ 10.59	8112 ✓
		0+0 = E.L. 32nd St.	
H			5.3 79.8
CB Top			5.68 79.5
Gutter			5.9 79.4
H			6.0 79.1
+5			5.7 79.4
2			6.2 78.9
H			5.9 79.4
H			6.1 79.0
Gutter			6.1 79.0
CB Top			5.65 79.4
S			5.4 79.7
		15' E	
S			4.3 80.8
+7			4.2 80.9
CB			4.5 80.6
+5			4.9 80.4
H			5.1 80.0
+6			4.9 80.4
2			6.5 78.6
+3			6.1 79.0
+6			4.8 80.3
H			4.8 80.3
25			4.1 80.3

G St.

8514

N			4.8	80.3
		50' E		
N			5.3	79.8
CB			5.1	80.0
+9			5.2	79.9
1/4			6.7	78.4
+4			7.1	78.0
+8			5.1	80.0
S			5.0	80.1
1/4			5.0	80.1
+6			4.4	80.7
CB			4.7	80.4
+5			4.4	80.7
S			4.1	81.0
TP	271	8339 ✓	4.4	80.68
		75' E		
S			3.2	80.4
+4			3.5	79.9
CB			3.8	79.6
+5			3.5	79.9
1/4			9.0	79.4
+8			4.0	79.4
S			3.8	79.6
+7			3.9	79.5
1/4			4.9	78.5
+2			6.1	77.3
+8			4.4	79.0

8339

CB			4.2	79.4
N			4.2	79.4
		100' E		
N			5.0	78.4
+6			6.6	76.8
CB			6.6	77.4
+9			6.6	76.8
1/4			5.1	78.0
+6			3.2	80.4
S			3.9	79.5
1/4			4.3	79.1
CB			4.6	78.8
S			4.6	78.8
		125' E		
S			4.3	79.1
CB			4.6	78.8
1/4			4.7	78.7
S			4.4	78.8
1/4			6.4	77.0
+5			7.3	76.1
CB			7.9	75.5
N			8.9	74.5
		150' E		
+10			8.1	75.3
N			7.0	76.4
CB			6.7	77.2
1/4			5.0	78.4

GSA

83.39

S	5.6	78.4
W	4.9	78.5
CB	4.6	78.8
S	4.4	79.0

17.5 E

S	4.2	79.7
CB	4.6	78.8
W	5.1	78.3
TS	5.4	78.0
S	6.0	77.4
W	7.6	75.8
CB	9.5	73.9
N	10.6	74.8
+10	10.9	74.5

19.5 E

-70	16.7	66.7
N	15.8	67.6
CB	15.4	68.0
W	14.9	68.5
S	12.3	71.1
W	9.9	73.5
+5	9.0	74.4
CB	7.8	76.4
S	6.6	77.4
TR	0.98	71.84 ✓
		12.53
		70.86

21.3 E

-10

S	6.8	68.0
---	-----	------

71.84

S	5.5	66.3
CB	6.7	65.1
W	6.9	64.9
S	7.1	64.7
W	6.8	65.0
TS	6.6	65.7
CB	7.0	64.8
N	8.3	63.5
+30	9.7	64.1

22.0 E

-30	10.0	61.8
N	11.1	60.7
+5	11.0	60.8
CB	10.5	61.3
W	10.2	61.6
S	10.3	61.5
W	10.1	61.4
CB	10.0	61.8
W	11.2	60.6
S	12.1	59.7
+10	11.6	60.7
+6	5.5	66.6

25.0 E

-30	9.3	64.5
-25	4.3	60.5
S	13.0	58.8
CB	13.0	58.8

G.S.H.

7189

1/4	13.0	58.8
1/2	12.7	59.1
3/4	12.9	59.4
CB	12.5	59.3
N	12.7	59.1
+30	11.0	60.8
275° E ✓		
-30	11.8	60.6
N	12.1	59.7
CB	12.7	59.1
1/4	12.9	58.9
1/2	13.0	58.8
3/4	13.2	58.5
CB	13.6	58.4
S	12.1	57.7
+30	13.6	58.4
300° E ✓		
-30	15.6	56.6
-10	15.7	56.1
S	14.3	57.5
CB	14.0	57.8
1/4	13.4	58.4
1/2	13.1	58.7
3/4	12.6	59.4
CB	12.1	59.7
N	11.6	60.7
+30	10.4	61.4

7184

312° E ✓

-30	9.0	64.8
N	11.0	60.8
CB	11.5	60.3
1/4	12.0	59.8
1/2	12.5	59.3
3/4	13.1	58.7
CB	13.7	58.1
S	14.2	57.6
+30	16.2	55.6
+30	15.5	56.3
325° E ✓		
-30	16.5	55.3
S	14.0	57.8
CB	13.5	58.3
1/4	12.4	59.4
1/2	12.6	59.7
3/4	11.7	60.1
CB	10.1	61.7
+15	9.3	62.5
N	8.3	63.5
+15	5.4	66.4
346° E ✓		
-15	0.6	71.4
N	2.9	68.9
CB	6.4	65.4
1/4	9.0	64.8
1/2	9.5	64.3

Gst.

71.89

15		10.5	61.3
14		10.9	66.9
CB		11.3	60.5
S		12.2	59.6
730		14.8	57.0

350°E ✓

720		10.7	61.1
S		9.5	64.3
CB		8.7	63.1
14		8.1	63.7
20		7.3	64.5
76		6.8	65.0

14		5.6	66.4
CB		3.3	68.5

TP	10/16	80.82	118	70.66
N			8.8	74.0

415		5.5	75.3
-----	--	-----	------

375°E ✓

N		4.2	76.6
15		5.1	75.7

CB		6.0	74.8
14		6.4	74.4

S		6.7	74.1
14		7.7	73.1

CB		8.5	74.3
S		8.7	74.1

70		10.8	70.0
----	--	------	------

80.88

320°E ✓

S		5.9	74.9
CB		5.9	74.9

14		5.8	75.0
----	--	-----	------

S		5.6	75.2
---	--	-----	------

14		5.5	75.3
----	--	-----	------

CB		4.9	75.9
----	--	-----	------

N		4.0	76.8
---	--	-----	------

415°E ✓

N		4.0	76.8
---	--	-----	------

CB		3.8	77.0
----	--	-----	------

14		4.1	76.7
----	--	-----	------

S		4.4	76.4
---	--	-----	------

14		4.4	76.4
----	--	-----	------

CB		4.6	76.2
----	--	-----	------

S		4.8	76.0
---	--	-----	------

475°E ✓

S		3.9	76.9
---	--	-----	------

CB		3.9	76.9
----	--	-----	------

14		3.9	76.9
----	--	-----	------

S		3.8	77.0
---	--	-----	------

14		3.9	76.9
----	--	-----	------

CB		4.2	76.6
----	--	-----	------

N		3.9	76.9
---	--	-----	------

525°E ✓

N		4.8	76.0
---	--	-----	------

CB		4.8	76.0
----	--	-----	------

Gst.

8082

14	46	76.4
B	45	76.3
14	42	76.6
CB	42	76.6
S	42	76.6

550' E ✓

S	50	75.8
CB	50	75.8
14	45	76.3
L	45	76.3
14	47	76.1
15	52	75.6
CB	56	75.4
N	57	75.6

568' E ✓

N	58	75.0
CB	57	75.1
14	56	75.7
L	56	75.7
14	59	74.9
CB	62	74.6
S	67	74.1
TP	346	7735 ✓
		693 7389

600' E = 11/23rd st ✓

-15	28	67.6
S	89	68.5
CB	78	69.5

7735

14	70	70.4
B	65	70.9
15	60	71.5
14	46	74.8
CB	57	73.7
15	29	74.5
N	30	74.4

Mag. 100
G. 130051
2.71 74.57

10' E = CB

10	61	71.3
11	64	71.0
CB	67	70.7
14	70	70.4
L	75	69.9
14	83	69.1
CB	90	68.4
S	97	67.7
15	109	66.7

20' E = 14

15	120	65.4
S	113	66.1
CB	109	66.7
14	102	67.4
L	96	67.8
14	91	68.3
CB	86	68.8
N	80	69.4

30' E = 23rd st

G 54

7735

N	9.5	67.9
CB	10.0	67.4
1/4	10.7	66.7
2	11.2	66.7
1/4	11.7	65.7
CB	12.1	65.3
S	12.6	64.8
40'E - 1/4		
S	13.2	64.7
CB	12.6	64.8
1/4	12.1	65.3
2	11.9	65.5
1/4	11.5	65.9
CB	10.9	66.5
N	10.6	66.8
50'E - CB		
N	10.1	67.3
CB	10.9	66.5
1/4	11.7	65.7
2	12.3	65.1
1/4	12.6	64.8
CB	13.0	64.4
S	13.2	64.7
60'E - 2 1/2 3/4 3/4		
S	13.3	64.1
CB	13.0	64.4
1/4	12.4	65.0

7735

2	12.1	65.3
1/4	11.6	65.8
CB	10.9	66.5
N	10.3	66.1

DIRECTIONS FOR USE OF TABLES

Proposed Drain

TABLE No. 7

Distance of slope stake from side or shoulder
 stake $\frac{1}{2}$ width roadway, $\frac{1}{2}$ width of
 If ground is nearly level, the cut or fill at side
 stake is $\frac{1}{2}$ width of double entry method in

left column and top row. The number in body
 of table in same row and column gives distance
 level estimate the difference in elevation between
 the side stake and slope stake by this
 amount if cut elevate if fill. Add this amount
 to cut or fill at rod at the stake and cut
 target. If it does not make the right adjustment

IMPROVED TABLES AND INFORMATION

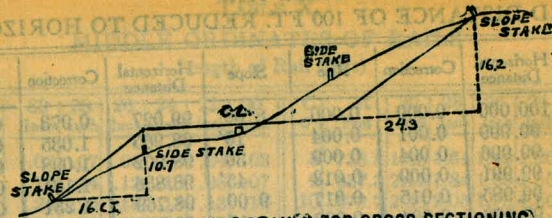
TABLE No. 8

To find tangent and external for curve of
 any other degree, divide by degree of curve and
 add correction found in column of corrections.
 Degree of curve with a given T may be found
 by dividing tangent (or external), opposite T by
 given tangent (or external).

The distance from a point on the tangent to
 the curve is very nearly the square of the tangent
 length divided by twice the radius.

33rd St

TABLE XII
INCLINATION OF 100 FT. REDUCED TO HORIZONTAL



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

79.47
26.49

$\frac{71.28}{60.24} = 1.183$
 $\frac{37.21}{12.42} = 3.00$
 $\frac{266}{243}$
 $\frac{2589}{167}$
 103.5
 101.9

1723
 10140
 2649
 20180
 3469

Sutter's Kite NE SP 219.95
 Gold Finch Sutter NE SP 156.99
 Jackdaws N.W. 262.00

STA SL
 305.5 = PC

W WDP Monroe + CAMPUS 349.01
 Tyler + CLOVSE 312.00

334.55 ✓	1306.54	4 28 03 11
363.60 ✓	1334.61	8 50
392.65 ✓	1362.68	13 24
421.70 ✓	1390.75	17 54 Storks
450.75 = EC ✓	1418.82 = EC	22 20 7.40
731.35 = PC ✓		26 48
761.77 ✓		31 16
792.19 ✓		35 44
	1306.54	40 12
	1278.07	44 40 30
	28.07	

So. FLYDERS

PC = 0400 SL STA

8.22.61 ✓	22.20	
8.53.03 = EC ✓	44.08	52
	66.12	59
9.36.15 = PC ✓	88.16	66
9.51.26 ✓	110.20	73
9.66.37 ✓	132.24 = EC	80
9.91.48 ✓	154.28	
9.96.59 ✓	390.7 = PC	473
10.11.70 ✓	415.71	1115
10.26.81 ✓	440.72	
10.41.92 = PRC ✓	465.73	
	490.74	
10.69.19 ✓	515.75 = EC	
10.96.46 ✓	725.47 = PC	125.07
11.2.73 ✓	752.23	513.75
11.41.00 ✓	778.44	29.70
11.68.27 = PRC ✓	805.75	
11.90.31 ✓	832.51	
12.12.38 ✓	859.27 = PRC	
12.30.39 ✓	887.12	
12.56.43 ✓	898.17	
12.78.47 = PRC ✓	917.22	
	937.07	
	956.52	
	975.97 = PRC	