

1145

TRANSIT-BOOK
1309

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

1947

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----|
| 0 | 0.00 | 0.15 | 0.30 | 0.45 | 0.60 | 0.75 | 0.90 | 1.05 | 1.20 | 1.35 | 0 |
| 1 | 1.50 | 1.65 | 1.80 | 1.95 | 2.10 | 2.25 | 2.40 | 2.55 | 2.70 | 2.85 | 1 |
| 2 | 3.00 | 3.15 | 3.30 | 3.45 | 3.60 | 3.75 | 3.90 | 4.05 | 4.20 | 4.35 | 2 |
| 3 | 4.50 | 4.65 | 4.80 | 4.95 | 5.10 | 5.25 | 5.40 | 5.55 | 5.70 | 5.85 | 3 |
| 4 | 6.00 | 6.15 | 6.30 | 6.45 | 6.60 | 6.75 | 6.90 | 7.05 | 7.20 | 7.35 | 4 |
| 5 | 7.50 | 7.65 | 7.80 | 7.95 | 8.10 | 8.25 | 8.40 | 8.55 | 8.70 | 8.85 | 5 |
| 6 | 9.00 | 9.15 | 9.30 | 9.45 | 9.60 | 9.75 | 9.90 | 10.05 | 10.20 | 10.35 | 6 |
| 7 | 10.50 | 10.65 | 10.80 | 10.95 | 11.10 | 11.25 | 11.40 | 11.55 | 11.70 | 11.85 | 7 |
| 8 | 12.00 | 12.15 | 12.30 | 12.45 | 12.60 | 12.75 | 12.90 | 13.05 | 13.20 | 13.35 | 8 |
| 9 | 13.50 | 13.65 | 13.80 | 13.95 | 14.10 | 14.25 | 14.40 | 14.55 | 14.70 | 14.85 | 9 |
| 10 | 15.00 | 15.15 | 15.30 | 15.45 | 15.60 | 15.75 | 15.90 | 16.05 | 16.20 | 16.35 | 10 |
| 11 | 16.50 | 16.65 | 16.80 | 16.95 | 17.10 | 17.25 | 17.40 | 17.55 | 17.70 | 17.85 | 11 |
| 12 | 18.00 | 18.15 | 18.30 | 18.45 | 18.60 | 18.75 | 18.90 | 19.05 | 19.20 | 19.35 | 12 |
| 13 | 19.50 | 19.65 | 19.80 | 19.95 | 20.10 | 20.25 | 20.40 | 20.55 | 20.70 | 20.85 | 13 |
| 14 | 21.00 | 21.15 | 21.30 | 21.45 | 21.60 | 21.75 | 21.90 | 22.05 | 22.20 | 22.35 | 14 |
| 15 | 22.50 | 22.65 | 22.80 | 22.95 | 23.10 | 23.25 | 23.40 | 23.55 | 23.70 | 23.85 | 15 |
| 16 | 24.00 | 24.15 | 24.30 | 24.45 | 24.60 | 24.75 | 24.90 | 25.05 | 25.20 | 25.35 | 16 |
| 17 | 25.50 | 25.65 | 25.80 | 25.95 | 26.10 | 26.25 | 26.40 | 26.55 | 26.70 | 26.85 | 17 |
| 18 | 27.00 | 27.15 | 27.30 | 27.45 | 27.60 | 27.75 | 27.90 | 28.05 | 28.20 | 28.35 | 18 |
| 19 | 28.50 | 28.65 | 28.80 | 28.95 | 29.10 | 29.25 | 29.40 | 29.55 | 29.70 | 29.85 | 19 |
| 20 | 30.00 | 30.15 | 30.30 | 30.45 | 30.60 | 30.75 | 30.90 | 31.05 | 31.20 | 31.35 | 20 |
| 21 | 31.50 | 31.65 | 31.80 | 31.95 | 32.10 | 32.25 | 32.40 | 32.55 | 32.70 | 32.85 | 21 |
| 22 | 33.00 | 33.15 | 33.30 | 33.45 | 33.60 | 33.75 | 33.90 | 34.05 | 34.20 | 34.35 | 22 |
| 23 | 34.50 | 34.65 | 34.80 | 34.95 | 35.10 | 35.25 | 35.40 | 35.55 | 35.70 | 35.85 | 23 |
| 24 | 36.00 | 36.15 | 36.30 | 36.45 | 36.60 | 36.75 | 36.90 | 37.05 | 37.20 | 37.35 | 24 |
| 25 | 37.50 | 37.65 | 37.80 | 37.95 | 38.10 | 38.25 | 38.40 | 38.55 | 38.70 | 38.85 | 25 |
| 26 | 39.00 | 39.15 | 39.30 | 39.45 | 39.60 | 39.75 | 39.90 | 40.05 | 40.20 | 40.35 | 26 |
| 27 | 40.50 | 40.65 | 40.80 | 40.95 | 41.10 | 41.25 | 41.40 | 41.55 | 41.70 | 41.85 | 27 |
| 28 | 42.00 | 42.15 | 42.30 | 42.45 | 42.60 | 42.75 | 42.90 | 43.05 | 43.20 | 43.35 | 28 |
| 29 | 43.50 | 43.65 | 43.80 | 43.95 | 44.10 | 44.25 | 44.40 | 44.55 | 44.70 | 44.85 | 29 |
| 30 | 45.00 | 45.15 | 45.30 | 45.45 | 45.60 | 45.75 | 45.90 | 46.05 | 46.20 | 46.35 | 30 |
| 31 | 46.50 | 46.65 | 46.80 | 46.95 | 47.10 | 47.25 | 47.40 | 47.55 | 47.70 | 47.85 | 31 |
| 32 | 48.00 | 48.15 | 48.30 | 48.45 | 48.60 | 48.75 | 48.90 | 49.05 | 49.20 | 49.35 | 32 |
| 33 | 49.50 | 49.65 | 49.80 | 49.95 | 50.10 | 50.25 | 50.40 | 50.55 | 50.70 | 50.85 | 33 |
| 34 | 51.00 | 51.15 | 51.30 | 51.45 | 51.60 | 51.75 | 51.90 | 52.05 | 52.20 | 52.35 | 34 |
| 35 | 52.50 | 52.65 | 52.80 | 52.95 | 53.10 | 53.25 | 53.40 | 53.55 | 53.70 | 53.85 | 35 |
| 36 | 54.00 | 54.15 | 54.30 | 54.45 | 54.60 | 54.75 | 54.90 | 55.05 | 55.20 | 55.35 | 36 |
| 37 | 55.50 | 55.65 | 55.80 | 55.95 | 56.10 | 56.25 | 56.40 | 56.55 | 56.70 | 56.85 | 37 |
| 38 | 57.00 | 57.15 | 57.30 | 57.45 | 57.60 | 57.75 | 57.90 | 58.05 | 58.20 | 58.35 | 38 |
| 39 | 58.50 | 58.65 | 58.80 | 58.95 | 59.10 | 59.25 | 59.40 | 59.55 | 59.70 | 59.85 | 39 |
| 40 | 60.00 | 60.15 | 60.30 | 60.45 | 60.60 | 60.75 | 60.90 | 61.05 | 61.20 | 61.35 | 40 |
| 41 | 61.50 | 61.65 | 61.80 | 61.95 | 62.10 | 62.25 | 62.40 | 62.55 | 62.70 | 62.85 | 41 |
| 42 | 63.00 | 63.15 | 63.30 | 63.45 | 63.60 | 63.75 | 63.90 | 64.05 | 64.20 | 64.35 | 42 |
| 43 | 64.50 | 64.65 | 64.80 | 64.95 | 65.10 | 65.25 | 65.40 | 65.55 | 65.70 | 65.85 | 43 |
| 44 | 66.00 | 66.15 | 66.30 | 66.45 | 66.60 | 66.75 | 66.90 | 67.05 | 67.20 | 67.35 | 44 |
| 45 | 67.50 | 67.65 | 67.80 | 67.95 | 68.10 | 68.25 | 68.40 | 68.55 | 68.70 | 68.85 | 45 |
| 46 | 69.00 | 69.15 | 69.30 | 69.45 | 69.60 | 69.75 | 69.90 | 70.05 | 70.20 | 70.35 | 46 |
| 47 | 70.50 | 70.65 | 70.80 | 70.95 | 71.10 | 71.25 | 71.40 | 71.55 | 71.70 | 71.85 | 47 |
| 48 | 72.00 | 72.15 | 72.30 | 72.45 | 72.60 | 72.75 | 72.90 | 73.05 | 73.20 | 73.35 | 48 |
| 49 | 73.50 | 73.65 | 73.80 | 73.95 | 74.10 | 74.25 | 74.40 | 74.55 | 74.70 | 74.85 | 49 |
| 50 | 75.00 | 75.15 | 75.30 | 75.45 | 75.60 | 75.75 | 75.90 | 76.05 | 76.20 | 76.35 | 50 |

Computed by L. Leland Locke.

See index

CROSS-SECTIONING
TABLE

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Mechanical Analysis Tests

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Dec 1904

4 Tests of Linda Vista Sand taken from
near S.E. Cor of Cantonment

7-14-17

Briquettes made with Linda Vista Sand screened
with 1/4" screen and

| Sample # | Ratio | 24 hrs. # days |
|-----------|-------|-------------------|
| Sample #1 | 1:1 | 305 301 |
| " #2 | 1:2 | 155 163 |
| " #3 | Neat | 443 452 |

Mechanical Analysis 7-16-17

Sample #1 - 800 grams passing 1/4" mesh.

| Size of Sieve | Retained in Sieve-Grams | Passing Sieve Grams | Percentage finer than sieve |
|---------------|-------------------------|---------------------|-----------------------------|
| 100 | 20.7 | 15.8 | 1.97 |
| 80 | 91.0 | 36.5 | 4.56 |
| 50 | 125.7 | 127.5 | 15.94 |
| 40 | 187.5 | 253.2 | 31.65 |
| 30 | 172.5 | 440.7 | 55.08 |
| 20 | 183.5 | 613.2 | 76.65 |

Uniformity Coefficient = $\frac{.0228}{.0088} = 2.59$

San Clemente Canyon

5

Gramwell, Hayler + Crane

Mechanical Analysis

7-16-17

Sample #2 - 500 grams passing 1/4" mesh.

| Size of Sieve | Retained in Sieve-Grams | Passing Sieve Grams | Percentage finer than sieve |
|---------------|-------------------------|---------------------|-----------------------------|
| 100 | 7.50 | 3.3 | .66 |
| 80 | 47.25 | 10.8 | 2.16 |
| 50 | 74.25 | 58.05 | 11.61 |
| 40 | 116.00 | 132.30 | 26.46 |
| 30 | 111.00 | 248.30 | 49.66 |
| 20 | 141.60 | 359.30 | 71.86 |

Uniformity coefficient $\frac{.0263}{.0103} = 2.55$

See Lab 2

6. Tests of Mission Valley Sand used on Kansas St Paving from University to the Park

7

Mechanical Analysis Cronwell-Haylex - 7-17-17

Sample #3 - 100 grams

| Size of Sieve | Retained in Sieve - Grams | Passing Sieve Grams | Percentage finer than sieve |
|---------------|---------------------------|---------------------|-----------------------------|
| 100 | 6.0 | 3.7 | 3.7 |
| 80 | 16.8 | 9.7 | 9.7 |
| 50 | 14.95 | 26.5 | 26.5 |
| 40 | 18.15 | 41.45 | 41.45 |
| 30 | 21.85 | 59.60 | 59.60 |
| 20 | 18.55 | 81.45 | 81.45 |

Uniformity Coefficient $\frac{.0201}{.0068} = 2.96$

Like Lumber

TEST #4 - OTAY RIVER SAND - FOR TANK AT
LINDA VISTA
- MECHANICAL ANALYSIS -

SAMPLE - 1000 GRAMS - NOT SCREENED THROUGH
1/4" MESH

| SIZE OF SIEVE | RETAINED IN SIEVE - GRAMS | PASSING SIEVE - GRAMS | PERCENTAGE FINER THAN SIEVE |
|---------------|---------------------------|-----------------------|-----------------------------|
| 100 | 32.0 | 9.4 | 64.26 - 0.94 |
| 80 | 138.9 | 41.4 | 44.22 - 4.4 |
| 50 | 123.8 | 180.3 | 30.41 - 18.03 |
| 40 | 138.1 | 304.1 | 18.03 - 30.4 |
| 30 | 200.4 | 442.2 | 4.74 - 44.2 |
| 20 | 357.0 | 642.6 | 0.94 - 64.2 |
| | 987 | 1820 | |

UNIFORMITY COEFFICIENT = $\frac{.0308}{.0087} = 3.54$

TEST #5 - BY CRANE SEPT 24/17
- MECHANICAL ANALYSIS -

SAMPLE 1000 GRAMS - PASSED 1/4" MESH

| SIZE OF SIEVE | RETAINED IN SIEVE - GRAMS | PASSING SIEVE - GRAMS | PERCENTAGE FINER THAN SIEVE | REMARKS |
|---------------|---------------------------|-----------------------|-----------------------------|---------------------------------------|
| 20 | 110.5 | 892.3 | 89.23 | |
| 30 | 223.9 | 668.4 | 66.84 | |
| 40 | 187.4 | 481.0 | 48.10 | |
| 50 | 171.8 | 309.2 | 30.92 | SPEC. ALLOW ONLY 25% SHOULD BE REJECT |
| 80 | 192.7 | 116.5 | 11.65 | |
| 100 | 66.5 | 50.0 | 5.00 | 50% IS LIMIT |
| | 1002.8 | | | |

TEST SPECIMENS - 150 GRMS - CEMENT
450 " - SAND - SEPT-25/17
54 " - WATER

LEFT IN MOULDS IN MOIST AIR 24 HRS -
AT 7 DAYS - BREAKING TEST -

| | |
|---------------------------------------|-------------|
| | LB'S. |
| SPEC #1 - TESTING SAND | 265 |
| " #2 | 236 |
| | 501 |
| | Ave = 250.5 |
| SPEC #3 - CONTRACTORS SAND | 190 |
| " #4 | 168 |
| | Ave = 179# |
| STANDARD SPEC. 700/0 @ 250 = 175 LBS. | 358 |

CONDEM.

16200 16120

TEST # 6 - OCT. 23 - 1917 - BY W.F. CRANE

SAMPLE - VICTOR CEMENT FROM CAR.
 # 27342 - FROM FAIRCHILD - GILMORE WILTON CO.
 FOR WALNUT ST. PAVING. - [REITTY - INSPECTOR]

TEST SPECIMENS MADE OCT 22 - 20% H₂O MARKED N.C.

TEST OCT 23 - SPECIMENS HAVING BEEN IN MOIST AIR 24 HRS.

| | BREAKING LOAD. | REMARKS |
|---------------------------|----------------|-------------------|
| SPECIMEN #1 | 218 LBS. | MINIMUM ALLOWABLE |
| " #2 | 218 LBS. | 175 LBS. |
| OCT-30 | | |
| NOTE - TEST 12 HRS LATE - | | |
| | BREAKING LOAD | |
| SPECIMEN #1 | 705 | MIN ALLOWABLE AT |
| " #2 | 655 | 7 DAYS - 500 LBS. |

| SPEC. # | BREAKING LOAD |
|---------|---------------|
| #1 | 759 |
| #2 | 822 |

O.K.
W.F.C.

TEST # 7 - NOV. 1, 1917 - BY W.F. CRANE

SAMPLE - RIVERSIDE CEMENT FROM WALNUT
 ST. PAVING - FAIRCHILD - GILMORE WILTON CO.
 REITTY - INSPECTOR

TEST SPECIMENS MADE NOV. 1 1907 - 10 A.M.

20% H₂O - MARKED R. 11

TEST NOV. 2 - SPECIMENS HAVING BEEN IN MOIST AIR FOR 24 HRS.

| | BREAKING LOAD | REMARKS |
|-------------|---------------|--|
| SPECIMEN #1 | 350 LBS. | MINIMUM ALLOWABLE |
| " #2 | 436 LBS. | 175 LBS. FOR 1 DAY TEST. VERY MUCH IN EXCESS OF MINIMUM ALLOWABLE. |

TEST NOV 8 - 7 DAYS

| | BREAKING LOAD |
|-------------|---------------|
| SPECIMEN #1 | 867 LBS. |
| " #2 | 915 LBS. |

| | BREAKING LOAD |
|-------------|---------------|
| SPECIMEN #1 | 884 |
| " #2 | 905 |

O.K.
W.F.C.

TEST #8 - NOV 19 1917 - BY - W.F. CRANE

SAMPLE - VICTOR CEMENT - TO BE USED
ON HERMOSA WAY ETC. - FAIRCHILD - GILMORE
WILTON CO. - CONTRACTORS.

NOV 19 - SPECIMENS 200/0 H₂O - MARKED 8

NOV 20 - BREAKING TEST

BREAKING LOAD

SPEC. #1 234

" #2 282

NOV 26 - 7 DAY TEST

SPEC. #1 640

" #2 758

DEC 26

SPEC. #1 705

" - #2 654

TEST #9 - NOV 19 1917 - BY - W.F. CRANE

SAMPLE - RIVERSIDE CEMENT - TO BE
USED ON HERMOSA WAY - FAIRCHILD - GILMORE
WILTON CO. - CONTRACTORS.

NOV 19 - SPECIMENS 200/0 H₂O - MARKED 9.

NOV 20 - BREAKING TEST.

BREAKING LOAD

SPEC. #1 381

" " 407

NOV 26 - 7 DAY TEST

SPEC. #1 672

" - #2 655

DEC 26

SPEC. #1 770

" - #2 755

TEST #10 - JAN 24, 1918 - BY W.F. CRANE.

SAMPLE - COLTON CEMENT - TO BE USED
ON LINDA VISTA ROAD - JOHN ENGBRETSEN

CONTRACTOR

JAN. 24: SPECIMENS 20% H₂O - MARKED #10

JAN 25. - BREAKING TEST - 1 DAY.

| | BREAKING LOAD | REMARKS |
|-------------|---------------|---------|
| SPECIMEN #1 | 341 LBS. | OK |
| " #2 | 338 LBS. | OK |

JAN 31 - BREAKING TEST - 7 DAY.

| | | |
|-------------|----------|----|
| SPECIMEN #1 | 832 LBS. | OK |
| " #2 | 733 LBS. | OK |

FEB 21 - BREAKING TEST - 28 DAY.

| | |
|---------|---------|
| SPEC #1 | 740 LBS |
| " #2 | 728 " |

TEST #11

TEST OF SAND FROM PACIFIC BEACH CAÑON.

PROPOSED FOR USE ON OCEAN BEACH SEWER.

[APPROX. HAUL - 2 MILES] TEST MADE JAN. 29, 1918

BY - H.V. DOLPH - INSPECTOR OF O.B. SEWER.

TEST MADE AT SAN DIEGO CEMENT PIPE WORKS.

- MECHANICAL ANALYSIS -

| PASSING SIEVE NO. | RETAINED ON SIEVE NO. | % RETAINED |
|----------------------|-----------------------------|---------------|
| 4 | 10 | 9.5 |
| 10 | 20 | 10.9 |
| 20 | 30 | 25.0 |
| 30 | 50 | 39.1 |
| 50 | 80 | 9.5 |
| 80 | 100 | 4.0 |
| 100 | 200 | 2.0 |

TEST #12 - FEB. 7, 1918 - BY W.F. CRANE

SAMPLE - COLTON CEMENT - TO BE USED ON
LINDA VISTA ROAD - ?FEB 7 - SPECIMENS - 20% H₂O -

FEB 8 - BREAKING TEST - 1 DAY.

| | BREAKING LOAD | REMARKS - |
|-------------|---------------|-----------|
| SPECIMEN #1 | 354 - LBS | OK |
| " #2 | 421 - " | OK |

FEB 14 - BREAKING TEST - 7 DAY.

| SPECIMEN #1 | 746 LBS |
|-------------|---------|
| " #2 | 755 LBS |

MARCH 7 - BREAKING TEST - 28 DAY.

TEST #13 - FEB. 13, 1918 - BY W.F. CRANE

SAMPLE - COLTON CEMENT - FOR LINDA VISTA ROAD

SETTING TEST

TEST STARTED 9-35 A.M. - INITIAL SET 12-25 P.M.

FINAL SET 12-40 P.M. - SAMPLE 500 G. CEM - 20% H₂O

DURATION OF TIME FOR INITIAL SET = 2 HR - 50 M.

" " " " FINAL " = 3 HR - 5 M.

O.K.

SPECIFIC GRAVITY - TEST -

| READING ON APPARATUS - | SPECIFIC GR |
|------------------------|--|
| 21.5 | $\frac{64}{21.5} = 2.97$ { CEM. HAD NOT BEEN DRIED } |
| 20.9 | $\frac{64}{20.9} = 3.06$ - CEMENT DRIED - |
| 20.9 | $\frac{64}{20.9} = 3.06$ |
| 20.85 | $\frac{64}{20.85} = 3.07$ |

BREAKING TEST - FEB. 14.

1-DAY

#1 - 360 LBS

#2 - 421 LBS

7-DAY - TEST FEB 20

#1 = 712 LBS

#2 = 698 LBS

TEST # 14 - FEB 20 1 P.M. to 4 P.M.

TO BE USED ON LINDA VISTA ROAD.

| FINENESS | | g/100 GRMS. | | g/100 PASSY | g/100 SPECIF |
|-----------------------|--|-------------|------|-------------|--------------|
| RETAINED ON 100 SIEVE | | 8.5 GR | 91.5 | 92 | |
| " " 200 " | | 22.0 GR | 63.5 | 75 | |
| PASSING - 200 " | | 67.7 GR | 98.2 | | |
| | | | | | (REJECT) |

STRENGTH FEB-20 - 3 P.M. - SPECIMEN - 20% H₂O.

FEB-21 - 1 DAY TEST

| SPECIMEN # | BREAKING LOAD |
|------------|---------------|
| 1 | 409 LBS. |
| " 2 | 357 " |

7 DAY TEST - FEB 27

| | |
|--------------|-----|
| SPECIMEN # 1 | 690 |
| " # 2 | 642 |

TEST # 15. ROCK - LINDA VISTA ROAD. FEB 20.

CU. CONTENTS OF CONTAINER = 14 QTS = 28 PLS

AMT. H₂O TO FILL VOIDS. = 11 1/4 PLS

11.25 ÷ 28 = 40.2 % VOIDS.

TEST #16 - FEB 25 - BY W.F. CRANE -

- FINENESS TEST -

SAMPLE - 100 GR. - HAVING BEEN HEATED -

PASSING #100 SIEVE 93.00 SPEC. 92% - O.K.

" #200 " 77.00 SPEC. 75% - O.K.

RET. ON #100 - 7.05
ERROR .005 GR

- DISINTEGRATION TEST -

PATS - 21.4 1/0 H₂O - 100 GRMS. CEMENT.

FEB 26 - BOILED 3 HRS - NO SIGN DISINTEGRATION

O.K.

TEST E May 20. By R.A. Schwartz.

Sample - Colton Cement to be used on

Linda Vista Road.

Breaking Test May 21 1918

1 Day.

No. E - 360 lbs. Specific Gravity

3.047.

7 Days.

TEST 17 RASchwartz
 Sand Utah St test for
 June 17, 1918 Strength.
 7 day 7 day
 17 HOWIA Sand 17 Missio V.S.
 187 127

Test 18 RASchwartz
 Sample Riverside Cement
 for Utah St. July 5, 1918.
 Geo. Daley Construction
 Test Started 8:30 A.M.
 No. 18 1 Day 409 lbs. 1

Test 19 RA Schwartz

Sample Riverside Cement

15th + E St. Aug. 5-1918 started

10 A.M. Broke 10 A.M. Aug. 6:

Broke at 445 lbs

Test Sorrento Sand used in Torrey Pines Road →
(from pit near Sorrento)

Sample No 1 200 Grams passing 1/4 mesh

| Sieve No | Retained on Gr. | Passing | % Finer than |
|----------|-----------------|---------|--------------|
| | 7.3 | | |
| 100 | 8.2 | 7.3 | 3.65 |
| 80 | 26.8 | 14.3 | 7.15 |
| 50 | 40.0 | 41.1 | 20.55 |
| 40 | 53.9 | 81.1 | 40.55 |
| 30 | 43.8 | 135.0 | 67.5 |
| 20 | 17.6 | 179.8 | 89.9 |
| 10 | 3.6 | 196.4 | 98.2 |
| | 201.2 | | |

Section Top of Biological Gr to top Torrey Pines Gr.

Oct 22-1918 Cromwell, Schmidt & Schwartz.

Sand Test. Started Oct. 22-1918

1 Part Cement 2 Parts Sand.

Standard Ottawa Sand

Sorrento Sand.

#1

#11

Broke Oct. 29, 1918

Broke Oct 29, 1918.

270#

150#

275#

180#

Sand Test # 2 Sorrento Sand

Silt Test

100 Grams Sand Washed lost 4 1/4%
in weight of silt.

275
19 25

Nov. 7, 1918.

Schwartz
Schmidt

Sand Test #4

Sand from El Carmel Valley Sorrento

200 Grams passing 1/4 Mesh

| Sieve No | Retained | Passing | % Finer than |
|----------|----------------------|---------|--------------|
| 100 | ²⁰⁰ 198.0 | 2.0 | 1% |
| 80 | ²⁰ 194.10 | 5.9 | 2.95 |
| 50 | 178.7 | 21.3 | 10.65 |
| 40 | 157.8 | 42.2 | 21.15 |
| 30 | 122.2 | 77.8 | 28.9 |
| 20 | 56.0 | 144.0 | 72.0 |
| 10 | 6.5 | 193.5 | 96.75 |

Test #5

March 5, 1919

San Diego River Sand Used by Daily

Park Blvd.

Sample No 1 200 Grams Passing 1/4" Mesh

| Sieve No | Grams Retained | Grams Passing | % Finer than |
|----------|------------------------|---------------|--------------|
| 100 | ^{199.2} 194.6 | 5.4 | 2.70 |
| 80 | 185.3 | 14.7 | 7.35 |
| 50 | 153.0 | 47.0 | 23.50 |
| 40 | 121.8 | 78.2 | 39.10 |
| 30 | 82.3 | 117.7 | 58.85 |
| 20 | 18.0 | 182.0 | 91.00 |
| 10 | 38 | 196.2 | 98.10 |

H A M

Sand Briquet Test 1 to 3 Mix
River Sand Victor Canal " Ottawa Sand

170

205

195

200

Test No 6 Sand used by
F. B. W. Co. on Garnet St. Otay Sand
200 Grams Passing $\frac{1}{4}$ " Mesh

| Sieve No | Retained | Passed | % finer than |
|----------|--------------|--------|--------------|
| 100 | 19.2 | 183.2 | 6.8 |
| 80 | 40.0 | 164.0 | 36.0 |
| 50 | 29.5 | 124.0 | 76.0 |
| 40 | 31.2 | 94.7 | 105.3 |
| 30 | 35.0 26.5 | 33.5 | 136.5 |
| 20 | 15.0 | 28.5 | 171.5 |
| 10 | 13.5 | 13.5 | 186.5 |

Washed 100 Grams lost $4\frac{1}{2}\%$ in
weight of silt

Tri Broken Stone Sept. 24. 1919

Portion Passing #4 Screen.

" Retained #8 Screen.

Test N° 7

Mission Valley

Sand

200 Gm Sample

| Sieve No | Retained | Passed | % Finer than |
|----------|----------|--------|--------------|
| 100 | 196.5 | 3.5 | 1.75% |
| 80 | 189.1 | 10.9 | 5.45 |
| 50 | 151.6 | 48.4 | 24.2 |
| 40 | 113.2 | 84.8 | 42.4 |
| 30 | 76.0 | 124.0 | 62.0 |
| 20 | 20.3 | 179.7 | 89.85 |
| 10 | 0.5 | 199.5 | 99.75 |

3 1/2% (Approx) Silt

Contains Much Mica

Oct 25-19

much too fine for use in
concrete.

J.W.

Test N^o 8

Mission Valley Sand.

Nov. 10 - 1919

200 Gm Sample,

| Sieve N ^o | Gm Retained | % Passed | % finer | % Coarser |
|----------------------|-------------|----------|---------|-----------|
| 100 | 197.2 | 2.1 | 1.05 | 98.95 |
| 80 | 194.2 | 5.8 | 2.90 | 97.1 |
| 50 | 179.1 | 20.9 | 10.45 | 89.55 |
| 30 | 106.3 | 41.7 | 45.85 | 54.15 |
| 20 | 41.2 | 158.3 | 79.15 | 20.85 |
| 10 | 7.2 | 192.7 | 96.35 | 3.65 |

 364.25

Fineness Modulus 3.64

Sand is clean.

Test No 9 Mission Valley

Near Lakeside Nov 13, 1919 J.W.

200 Gm. Sample

| Sieve | Gm Retained | Gm Passed | % Finer than | % Coarser than |
|-------|-------------|-----------|--------------|----------------|
| 100 | 195.1 | 4.9 | 2.45 | 97.55 |
| 80 | 190.3 | 9.7 | 4.85 | 95.15 |
| 50 | 171.8 | 28.2 | 14.1 | 85.90 |
| 30 | 107.4 | 92.6 | 46.3 | 53.70 |
| 20 | 50.2 | 149.8 | 74.9 | 25.1 |
| 10 | 18.3 | 181.7 | 90.85 | 9.15 |

366.55

Fineness Modulus = 3.67

Silt = 2.6%

for U.S. Navy.

Test No. 10

| Sieve No | Retained | Passed | % finer than |
|----------|----------|--------|--------------|
| 200 | 99.4 | .6 | .6 |
| 100 | 97.7 | 2.3 | 2.3 |
| 80 | 93.6 | 6.4 | 6.4 |
| 50 | 80.2 | 19.8 | 19.8 |
| 40 | 68.6 | 31.4 | 31.4 |
| 20 | 30.1 | 69.9 | 69.9 |
| 10 | 13.8 | 86.2 | 86.2 |

Test No. 10

$$\begin{array}{r} 100 \\ - 91.2 \\ \hline 8.8 \text{ pct} \end{array}$$

8 4
191.4
199.5

13

Feb. 16 1919

Riverview Sand

| Sieve No | Retained | Passed | % Finer than |
|----------|----------|--------|--------------|
| 200 | 199.5 | .5 | .2 |
| 100 | 191.4 | 8.6 | 4.3 |
| 80 | 174.9 | 25.1 | 12.5 |
| 50 | 158.1 | 41.9 | 20.9 |
| 30 | 135.3 | 64.7 | 32.3 |
| 20 | 90.7 | 109.3 | 54.6 |
| 10 | 26.6 | 178.4 | 81.7 |

Atay Sand

| | | | | |
|-----|-----|-------|-------|------|
| 100 | 109 | 198.4 | 2.6 | 1.3 |
| 80 | 192 | 187.5 | 12.5 | 6.2 |
| 50 | 585 | 168.3 | 31.7 | 15.8 |
| 30 | 460 | 110.8 | 89.2 | 45.6 |
| 20 | 320 | 65.8 | 134.2 | 62.1 |
| 10 | | 32.4 | 167.6 | 93.9 |

26
67.6
199.4

Azusa Sand

| Sieve No | Retained | Passed | % Finer |
|----------|----------|--------|---------|
| 100 | 15.2 | 199.9 | .1 |
| 80 | 30.0 | 184.7 | 15.3 |
| 50 | 51.7 | 154.7 | 22.6 |
| 30 | 30.0 | 103.0 | 48.5 |
| 20 | 31.3 | 73.3 | 126.0 |
| 10 | 42.0 | 42.0 | 158.0 |

200
15.3
154.7
45.3
97.0
73.3
42.0
58

Sewer Prelim. in
Turnbull's Sub. +
Homestead Union

12/10/25
Moore

V

3677

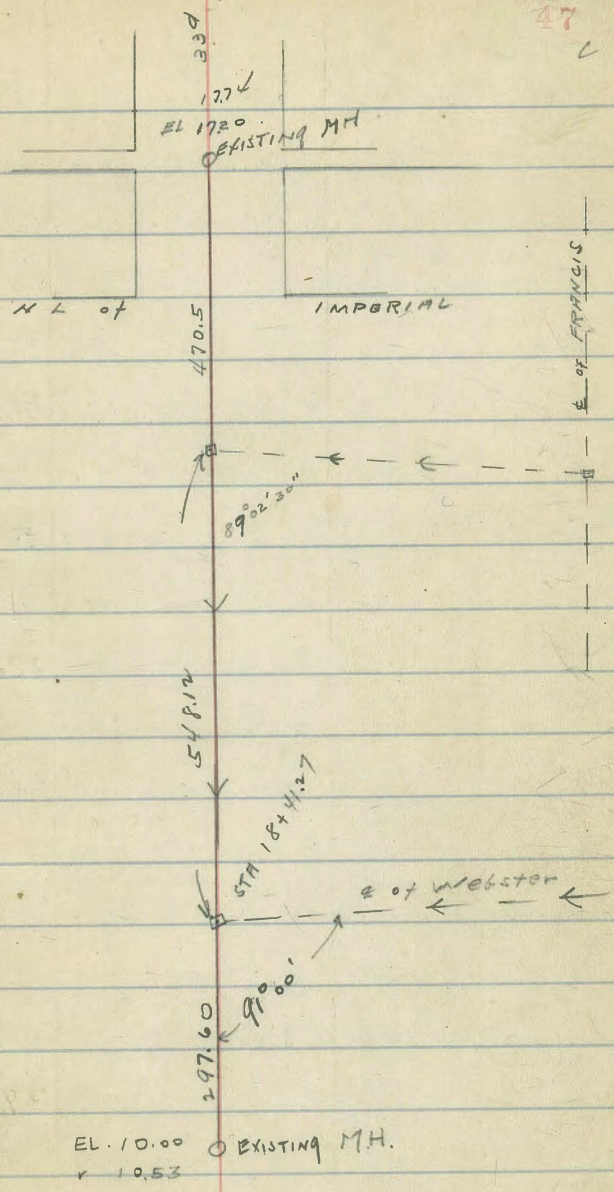
| | | | | | |
|---|---------------------------------|-------|-------------------|-------|----------------|
| EXISTING MH=0100 @ Alley (BKI Hunter's Add) + E of 34th St (20' wide) | 366 | 29 | 33.8 | | |
| North 170.2' to E Woolman, EAST 152.2' to E of Alley betw. 34th + graded | 400 | 0.7 | 36.0 | | |
| FRANCIS ST, thence North to W of Webster Ave ^{60' wide} thence | 60' west of 400 | 11.2 | 25.5 | | |
| EAST to W.L. of 30th ST. | T.P. | 12.78 | 49.42 | 0.13 | 36.64 |
| ON FIRE HGT. 768 | v 490 | 17.22 | 56.64 | 79 | 41.5 |
| EXISTING MH=0100 | Howling 2490 1396 1094 | 10.94 | 47.5 | 6.9 | 42.5 |
| ✓ ✓ RIM | 88 | 16.1 | 500 | 5.3 | 44.1 |
| 50' N | 8.3 | 16.6 | 550 | 0.4 | 49.0 |
| 100' ✓ | 7.3 | 17.6 | 60' west of 550 | 16.9 | 32.5 |
| 145' ✓ | 6.2 | 18.7 | T.P. | 9.39 | 58.29 |
| 150' ✓ | 5.2 | 19.7 | 600 | 5.8 | 52.4 |
| 170' ✓ = E Woolman 90' RT | 4.97 | 20.0 | 1993 ON HUB | 6.50 | 3.0 |
| 200 | 3.4 | 21.5 | 660 | 1.9 | 56.3 |
| T.P. | 12.05 | 36.77 | 2.18 | 4.7 | 667.6 = P.O.T. |
| 250 | 11.3 | 25.4 | 677 | 2.4 | 55.8 |
| 300 | 6.9 | 29.8 | 40' west of 667.6 | 20.0 | 38.29 |
| 322' = E Alley | 4.78 | 32.0 | 700 | 4.7 | 53.5 |
| 347 | 5.3 | 31.4 | 711 | 5.8 | 52.4 |
| 350 | 4.2 | 32.5 | 740 | 10.8 | 47.4 |
| 361 | 4.0 | 32.7 | T.P. | 4.37 | 50.07 |
| | | | | 12.59 | 45.70 |

| | | | |
|-------------------|------|-------|--------|
| 7+76.75 ♀ Minerva | 9.7 | 40.80 | IN HUB |
| 800 | 11.4 | 38.6 | |
| 829 | 14.6 | 35.4 | |
| 837 | 17.3 | 32.7 | |
| 850 | 16.0 | 34.0 | |
| 900 | 15.4 | 34.6 | |
| 55' W. of 900 | 22.4 | 27.6 | |
| 950 | 13.6 | 36.4 | |
| 1000 | 14.4 | 35.6 | |
| 1050 | 16.1 | 33.9 | |
| 1070 | 17.1 | 32.9 | |
| 1100 | 21.0 | 29.0 | |
| 1130 | 19.8 | 30.2 | |
| 1150 | 15.9 | 34.1 | |
| 1170 | 11.6 | 38.4 | |
| 1200 | 11.0 | 39.0 | |
| 60' W. of 1200 | 14.1 | 35.9 | |
| 1250 | 10.6 | 39.4 | |
| 1300 | 10.4 | 39.6 | |
| 1350 | 10.5 | 39.5 | |

| | | | |
|--------------|----------------------------|-------|-------------------------|
| 1400 | 11.5 | 38.5 | |
| T.P. 320 | 40.64 | 12.73 | 37.34 |
| 1450 | 4.4 | 36.2 | |
| 1470 | 5.5 | 34.8 | |
| 1475 | 9.0 | 31.6 | |
| 1479 | 6.0 | 34.6 | |
| 1491.6 v. 20 | bet. 3 & 4th Alley Francis | 580 | 34.84 |
| | | | 35.27 both + 1 material |

46 SEWER PRELIM. & WEBSTER from
W/L of 36th west to EXISTING Sewer on 33rd

| Station | Dist | W/L | Elev | Notes |
|------------------------------|--------|-------|-------|------------------------------------|
| 56+ | 104.2 | 98.58 | 98.58 | Top Hyd 35th + Imperial |
| 69+ | 102.98 | 98.16 | 96.06 | |
| Webster & W/L 36th = 0+00 | -43 | 4.60 | 98.0 | |
| 50' W | | 3.9 | 98.8 | Less .23 for difference in benches |
| 100' W | | 4.3 | 98.3 | |
| 121.87 = & Alley Pardee | | 5.08 | 97.5 | on hub |
| 150 | | 6.3 | 96.3 | |
| 200 | | 8.4 | 94.2 | |
| 250 | | 10.9 | 91.8 | |
| 300 | | 13.6 | 89.0 | |
| TP | 0.47 | 90.62 | 12.83 | 90.15 |
| 350 | | 4.2 | 86.0 | |
| 400 | | 7.8 | 82.4 | |
| 460.5 = & Alley Pardee | | 8.93 | 81.3 | output |
| 450 | | 11.7 | 78.5 | |
| TP | 0.36 | 78.09 | 12.89 | 77.73 |
| 500 | | 3.1 | 74.5 | |
| 550 | | 6.3 | 71.3 | |
| 582.53 = & 35th to the North | | 7.78 | 69.8 | on hub |
| 600 | | 8.5 | 69.1 | |



| | | | | |
|---------------------|------------------------------------|-------|---------------|---------------|
| 650 | | 11.4 | 66.02 | |
| T.P. | 0.6' | 66.10 | 12.60 | 65.49 |
| 700 | | 2.7 | 63.1 | |
| 7359 ^d | at 35th & Alley Francis | 6.48 | 59.3 | |
| 740 | | 6.0 | 59.8 | |
| 800 | | 10.2 | 55.6 | |
| T.P. | 0.39 | 53.66 | 12.83 | 53.27 |
| 850 | | 1.70 | 51.5 | |
| 900 | | 6.1 | 47.1 | |
| 950 | | 10.2 | 43.0 | |
| T.P. | 0.23 | 41.67 | 12.62 | 41.04 |
| 10 | 2' west of BIR at ^{Union} | 1.6 | 39.0 | |
| 1004.4 ^d | | 18.6 | 38.8 | |
| 1060.40 | at FRANCIS & Alley 34th | 5.80 | 34.8 35.27 | |
| | 580 | 4.64 | 34.8 | Elv. from 33' |
| 1077 | w of w. 30th | 7.0 | 33.64 | |
| 1090 | | 12.9 | 27.74 | |
| T.P. | 0.16 | 27.87 | 12.93 | 27.71 |
| 1100 | | 2.90 | 24.9 | |
| 1160 | | 9.6 | 18.2 | |

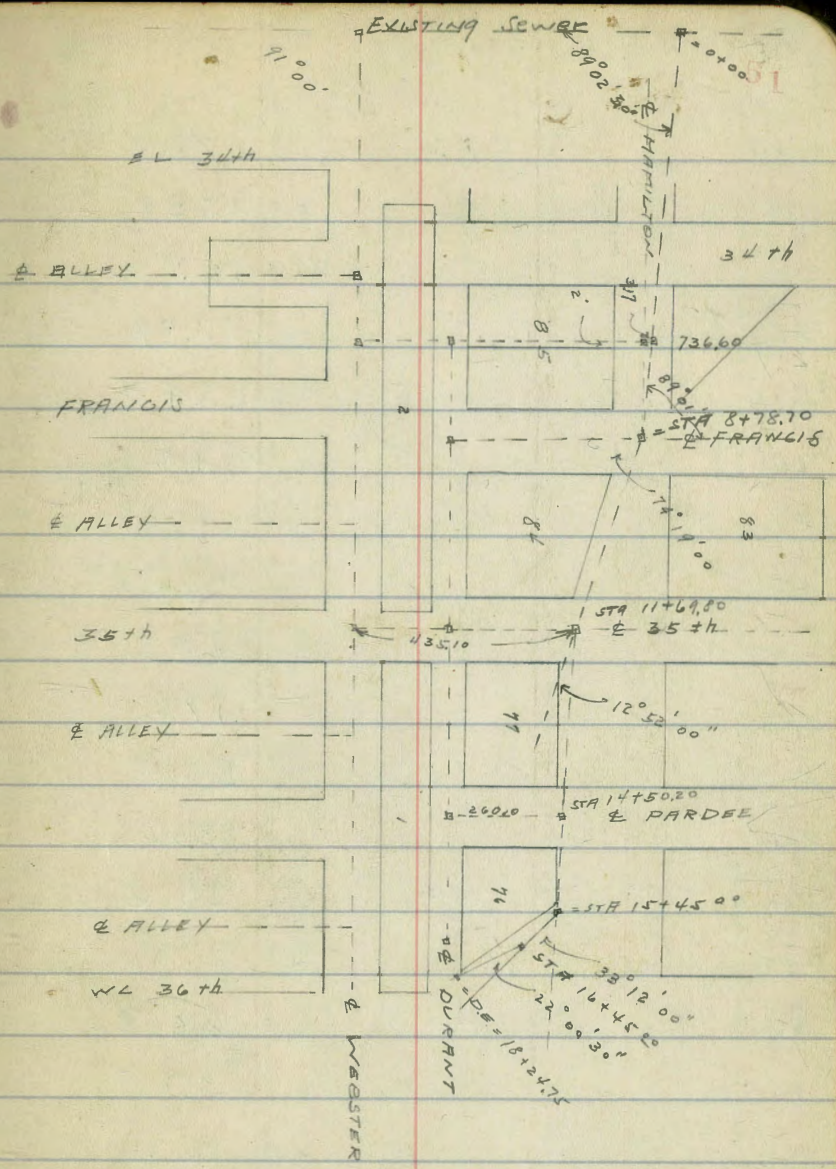
| | | | | |
|---------|----------------------------|-------|-------|--------|
| 1171 | | 13.4 | 14.4 | |
| T.P. | 6.3' | 22.26 | 11.95 | 15.94 |
| 1200 | = Cholla Creek | 9.4 | 13.0 | |
| 1250 | | 10.9 | 11.4 | |
| 1260 | | 8.4 | 13.2 | |
| 1266 | | 4.4 | 17.9 | |
| 1300 | | 4.6 | 17.7 | |
| 1400 | = P.O.T. | 5.57 | 16.8 | on AUB |
| 1455 | | 5.6 | 16.7 | |
| 1500 | | 4.7 | 17.6 | |
| 1550 | | 4.1 | 18.2 | |
| T.P. | 4.94 | 23.77 | 3.43 | 18.83 |
| 1600 | | 5.0 | 18.77 | |
| 1650 | | 4.6 | 19.17 | |
| 1700 | | 4.0 | 19.77 | |
| 1710 | | 4.6 | 19.17 | |
| 1741.47 | = Existing Center | 4.66 | 19.11 | on AUB |
| | 4.4 | 23.25 | | |
| 297.60 | So. = New line of EX. 147. | 12.72 | 10.53 | |

PRELIM. Sewer on HAMILTON

| | | | |
|--|------|-------|-------|
| on H&W Webster + Ek Sewer on 33d | 1013 | 29.24 | 19.1 |
| Flowline Ek. M.H. & of Alley North of Imp. on 33d | | 11.50 | 17.74 |
| on Top of Hyd NE Imperial 33d | | 0.22 | 29.02 |
| HAMILTON + Ek. Sewer on 33d = 0400 | | 7.07 | 22.17 |
| 50' E | | 7.2 | 22.24 |
| 100 | | 7.1 | 22.14 |
| 150 | | 7.2 | 22.04 |
| 200 | | 7.1 | 22.14 |
| 250 | | 7.1 | 22.14 |
| 300 | | 8.3 | 20.94 |
| 350 | | 8.1 | 21.14 |
| 400 | | 8.2 | 21.04 |
| 443 | | 7.8 | 21.44 |
| 478 | | 10.5 | 18.74 |
| 475 | | 11.6 | 18.64 |
| 496 | | 12.7 | 16.54 |
| 500 | | 13.0 | 16.24 |
| 505 | | 11.0 | 18.24 |
| 550 | | 11.7 | 17.54 |
| 600 | | 12.0 | 17.24 |

Plot

✓



2924
34
238

L

L

| | | | | |
|------------------|-------|-------|-------|-------|
| 625 | | | 11.3 | 17.94 |
| 649 | | | 15.3 | 13.94 |
| 650 | | | 12.5 | 16.74 |
| 655 | | | 11.4 | 17.84 |
| 658 | | | 5.8 | 23.44 |
| 700 | | | 5.4 | 23.8 |
| TP 736.60 | 11.61 | 34.61 | 6.24 | 23.00 |
| 750 | | | 12.5 | 22.11 |
| 763 | | | 18.0 | 16.6 |
| 770 | | | 17.0 | 17.6 |
| 771 | | | 14.1 | 20.5 |
| 800 | | | 11.0 | 23.6 |
| 850 | | | 9.0 | 25.6 |
| 878.70 = FRANCIS | | | 7.57 | 27.04 |
| 895 | | | 6.3 | 28.3 |
| 905 | | | 3.9 | 30.7 |
| 925 | | | 2.5 | 32.1 |
| 950 | | | 1.6 | 33.0 |
| TP 12.58 | 47.19 | 0.00 | 34.61 | |
| 1000 | | | 12.2 | 35.0 |
| | | | 12.1 | 35.1 |

5' N of 1000 = SL PAVING

| | | | | |
|----------|-------|------|-------|------|
| 1050 | | | 9.5 | 37.7 |
| 1100 | | | 6.7 | 40.5 |
| 1129 | | | 5.8 | 41.4 |
| 1150 | | | 2.7 | 44.5 |
| 1168 | | | 1.0 | 46.2 |
| | | | 1.88 | 45.3 |
| TP 12.51 | 59.70 | 0.00 | 47.19 | |
| 1169.50 | | | 12.12 | 47.6 |
| 1190 | | | 12.1 | 47.6 |
| 1191 | | | 14.3 | 45.4 |
| 1200 | | | 14.6 | 45.6 |
| 1204 | | | 13.8 | 45.9 |
| 1205 | | | 12.6 | 47.1 |
| 1250 | | | 9.4 | 50.3 |
| | | | 9.5 | 50.2 |
| 1300 | | | 7.3 | 52.4 |
| | | | 6.7 | 53.0 |
| 1350 | | | 3.8 | 55.9 |
| 1400 | | | 1.7 | 58.0 |
| TP 14.80 | 72.50 | 0.00 | 59.70 | |

2' W of #1 DIX 85

10.8 N of 1168 = SL PAVING

4 1/2' SW LT
#1 3574

on hub

Profile

Profile

2' N = SL PAVING

2.5 N = PAVING

| | | | |
|---------------------------|-------|-------|--------|
| 1450.40 = E of Pardee | 1.82 | 61.62 | on hub |
| 10.5 N of hub = SL paving | 10.00 | 61.8 | |
| 1500 | 7.8 | 64.7 | |
| 1545 = A 33° 12' RT | 4.51 | 68.0 | on hub |
| 1.5 N = SL paving | 4.43 | 68.1 | |
| 1595 | 1.1 | 71.4 | |
| 7.5 N = SL paving | 1.1 | 71.4 | |
| TP 12.99 85.49 | 0.0 | 72.50 | |
| 1645 = A 22° 00' 30" | 10.23 | 74.8 | |
| 1.5 N = SL paving | 10.6 | 74.9 | |
| 1700 | 7.1 | 78.4 | |
| 1750 | 3.9 | 81.6 | |
| 1800 | 0.7 | 84.8 | |
| TP 12.13 97.62 | 0.0 | 85.49 | |
| 18+27.5 = DE. Hub | 11.08 | 86.0 | |
| | 11.01 | 86.0 | |

36 + 6' ^{WEST} to 2' W of E of BIK 85

C

| T.P. | 23' ↓ | 976 ^v = Last page 99.47 - K 0.29 | 97.13 | |
|--------------|------------------------------|--|-------|--------|
| DE. | E of E of Pardee 2000 | 1.80 | 97.7 | on hub |
| 50' W | | 0.7 | 98.8 | |
| 100' W | | 2.8 | 96.7 | |
| 150 | | 7.4 | 92.1 | |
| 200 | | 11.6 | 87.9 | |
| 230 | T.P. 0.21 ON Hub & Pardee | 86.56 | 13.12 | 86.35 |
| 250 | | 1.9 | 84.7 | |
| 300 | | 4.1 | 81.7 | |
| 350 | | 7.5 | 79.1 | |
| 400 | | 9.7 | 76.9 | |
| 450 | | 11.7 | 74.9 | |
| T.P. | 0.11 | 73.73 | 12.94 | 73.62 |
| 500 | | 2.6 | 71.1 | |
| 509.80 | E 35' to north | 3.70 | 70.33 | on hub |
| 550 | | 4.1 | 69.63 | |
| 600 | | 3.9 | 69.83 | |
| 650 | | 4.1 | 69.63 | |
| 700 | | 5.8 | 67.93 | |
| 75' S of 700 | | 10.0 | 63.73 | |
| 75' N | | 8.7 | 65.0 | |

| | | | |
|---------------------------------|-------|-------|--------|
| 730 | 6.8 | 66.9 | |
| 750 | 6.9 | 66.8 | |
| 770 | 6.4 | 67.3 | |
| 790 = E of Francis to north | 6.20 | 67.53 | on hub |
| 825 | 9.8 | 63.9 | |
| T.P. 0.78 | 61.61 | 12.90 | 60.83 |
| 850 | 2.2 | 69.4 | |
| 880 | 7.1 | 64.5 | |
| 900 | 9.4 | 52.2 | |
| 9 + 31.93 = 2' W of E of BIK 85 | 12.94 | 48.67 | |

58 Sewer Levels thru BIK 2 STRADFORD PARK
 Webster to Hamilton + v 85 S.D. Homestead Union

38.19

59
 ✓

| | | | | | | |
|------------------------------|------|-------|-------------|------------------------|------|-------|
| | 1.58 | 50.25 | 48.67 | 400 | 10.3 | 27.9 |
| Webster = STA 10+44.4 = 0+00 | | | 11.40 38.85 | 425 | 11.6 | 26.6 |
| 30' N | | | 11.0 39.25 | TP 41.9 v 9.40 12.98 | | 25.21 |
| 33' N | | | 7.9 42.35 | 450 | 6.3 | 23.1 |
| 60' N | | | 4.1 46.15 | 479 | 8.9 | 20.5 |
| 100' N | | | 2.2 48.25 | 480 | 13.1 | 16.3 |
| 150 | | | 1.5 48.75 | 493 | 12.5 | 16.9 |
| 163.65 = # DURANT | | | 1.58 48.67 | 500 | 9.8 | 19.6 |
| 200 | | | 1.7 48.55 | 503 | 8.6 | 20.8 |
| 235 | | | 3.2 47.05 | 519.65 = # of Hamilton | 6.74 | 22.7 |
| 260 | | | 8.7 41.55 | 522.85 = HAMILTON LINE | 6.43 | 22.97 |
| 275 | | | 12.3 36.95 | | | |
| TP | 0.59 | 38.19 | 12.65 37.60 | | | |
| 300 | | | 5.1 33.1 | | | |
| 325 | | | 7.3 30.9 | | | |
| 350 | | | 8.1 30.1 | | | |
| 362 | | | 8.5 29.7 | | | |
| 363 | | | 9.9 28.3 | | | |
| 380 | | | 11.6 26.6 | | | |
| 385 | | | 9.8 28.4 | | | |

Plotted

Sewer Levels & FRANCIS
DURHAM TO HAMILTON

✓

± DURHAM = $\frac{0+00}{7+90}$ -181

69.34

67.53

on by 6

5.85

11.1 34.26

50' W

6.1 63.24

TP 0.6 33.88 12.1 33.22

85 W

7.7 61.64

300 W 4.9 29.0

1+15

13.1 56.2

307 6.0 27.9

TP

0.21

57.55

12.0 57.22

3+50
27.11

ON AUB
HAMILTON

6.87

27.01

27.0 ✓

125

5.2 52.35

141

12.1 45.45

150

13.7 43.85

156

15.2 42.35

160

18.2 39.35

169

18.6 38.95

175

14.5 43.05

187

12.0 45.55

202

10.2 47.35

208

8.5 49.05

216

7.2 50.15

220

7.2 50.15

235

9.8 48.75

TP

0.48

45.36

12.67 44.88

275

8.2 37.16

A 10 ed.

✓

62

Sewer Levels @ 35th
+ Webster To Hamilton

| | 469 | 75.0V | 70.33 | EDUCANT + 35th on hub |
|---|------|-------|-------|-----------------------------|
| 5482.53 | | | | |
| 0+00 = 4 Webster + 35th to the north | | | 5.3 | 69.87 on hub |
| 50 N | | | 5.3 | 69.7 |
| 100 N | | | 5.3 | 69.7 |
| 159 N = 5+0980 & DURANT | | | 4.69 | 70.3 on hub |
| 200 | | | 3.9 | 71.1 |
| 230 | | | 4.1 | 70.9 |
| 250 | | | 6.8 | 68.2 |
| 300 | | | 8.4 | 66.6 |
| 323 | | | 7.9 | 67.1 |
| 335 | | | 6.1 | 68.9 |
| 350 | | | 5.6 | 69.4 |
| 371 | | | 5.6 | 69.4 |
| 39610 POT. | | | 8.3 | 66.8 on hub |
| TP | 0.25 | 62.79 | 12.48 | 62.54 |
| 420 N | | | 3.6 | 59.2 |
| 421 | | | 7.6 | 55.2 |
| 428 | | | 10.4 | 52.4 |
| 430 | | | 11.7 | 51.1 |
| 434 | | | 12.70 | 50.1 |

6279

4+35.10
11+09.50 on hub 15.23

47.6 = 47.58

63

64

Sewer Levels @ PARDEE
& DURANT TO HAMILTON

| | | | | |
|--------------------------|--------|--------|-------|--------|
| 0+00 | 487 | | 86.35 | on bub |
| 1+30 = @ Pardee & Durant | 9.22 | | | |
| 50 W | | 4.4 | 86.8 | |
| 100 | | 5.9 | 85.3 | |
| 150 W | | 5.9 | 85.8 | |
| 100 W of 1+50 | | 9.1 | 82.1 | |
| 200 | | 4.5 | 86.7 | |
| 212.65 = POT | | 5.99 | 85.2 | |
| 230 | | 9.6 | 81.6 | |
| TP | 0.14 | 78.48 | 1288 | 78.34 |
| 250 | | | 5.1 | 73.38 |
| 255 | | | 8.6 | 69.88 |
| 2+60 | | | | 61.78 |
| 1+50.00 = Hamilton | ROSTER | 216.70 | | 61.68 |

Plotted

65

66

Sewer Levels @ ALLEY *Belvedere* C
35th + Pardee Webster So to E of 10' Alley
betw Woolman & Minerva

87.75

87

outlet
DUGOUT
PARDEE

-1.40 87.75 8025 600 S 11.5 76.25

⁰⁺⁰⁰
416.50 Webster 6.5 81.24 T.P. 207 78.75 11.10 76.65

30' S of Webster 5.7 82.05 650 S 2.6 76.12

60 S 2.5 85.25 685 S 3.0 75.72

100 S 3.6 84.15 690 = 75 4.2 74.52

60' W of 100 9.0 78.75 700 4.6 74.12

150 S 6.0 81.75 702 S 5.1 73.62

200 S 8.7 79.05 714.20 = 2 Minerva 4.9 73.82

60' W of 200 12.5 75.25 740 5.1 73.62 914.20

210 S 9.5 78.25 744 S 3.9 74.82

227 S 9.5 78.25 750 4.3 74.42

260 S 8.0 79.05 800 S 4.6 74.12

300 S 8.9 78.85 850 S 3.2 75.52

60' W of 300 11.7 76.05 60' E of 850 6.7 72.02

335 8.2 79.55 900 3.5 75.22

400 S 9.7 78.05 950 4.2 74.52

80' W of 400 11.9 75.85 974.80 = E of 10' Alley 4.6 74.12

450 S 9.2 78.55

500 S 10.6 77.15

550 10.9 76.85

betw Woolman &
Minerva

10

68 Sewer Levels E of 10' Alley between
Woolman & MINERVA. 35th to 36th

169

78.74

2

| | | |
|---|-------|-----------|
| 0+00 = EL 35th | 3.7 | 75.02 |
| 50 E | 2.6 | 76.12 |
| 100 E | 3.8 | 74.92 |
| 122.3 = E. of Alley to W betw Pardee + 35th | 4.6 | 74.12 |
| 150 | 6.5 | 72.22 |
| 175 | 9.5 | 69.22 |
| 225 | 10.4 | 68.32 |
| 250 | 11.4 | 67.32 |
| 269.60 | 11.2 | 67.52 |
| 300 | 11.9 | 66.82 |
| 350 | 9.6 | 69.12 |
| T.P. 1204 | 82.76 | 850 70.24 |
| 400 | 12.0 | 70.26 |
| betw Pardee + 36th 416.75 = E. of Alley to north | 11.2 | 71.06 |
| 450 E | 10.0 | 72.26 |
| 500 | 6.7 | 75.56 |
| 539 = WL 36th | 3.1 | 79.26 |
| T.P. nail in pole WL 36th + alley | 0.00 | 82.76 |

Potted.

850

70 Sewer Levels ϕ of Alley betw. Woolman +
 Minerva + Pardee + 36th = 517 $\frac{416.75}{0.00}$ ✓

96.62

71

| | | | |
|----------------------------------|-------|---------------|---------------------------|
| -27v | 84.98 | 82.26 = 11.72 | 450v |
| 416.75 ϕ of Alley = 0.00 | 14.0 | 70.98 | 500v |
| 50' w | 12.5 | 72.48 | 60' w of 500 |
| 100' w | 10.0 | 74.78 | 550' w |
| 60' w of 100 | 13.0 | 72.98 | 600 |
| 150' w | 8.0 | 76.78 | 650 |
| 200' w | 6.0 | 78.98 | 50' w of 650 |
| 230' w | 5.5 | 79.48 | 700 |
| 236 | 6' | 78.88 | 750 |
| 245 | 6.6 | 78.38 | 800 |
| 260 = ϕ Minerva | 5.7 | 79.28 | T.P. 6.85 102.09 13.8 |
| 274 | 5.9 | 79.08 | 850 |
| 276 | 5.3 | 79.68 | 900 |
| 283 | 5.6 | 79.38 | 950 |
| 285 | 4.8 | 80.18 | 975 = Webster |
| 300' w | 4.5 | 80.48 | TP 2.0' 92.49 11.6 |
| 350 | 3.1 | 81.88 | check to Duranit + Pardee |
| 400 | 2.0 | 82.98 | 61v |
| 60' w of 400 | 4.4 | 80.58 | 86.37 |
| T.P. | 11.90 | 96.62 | 86.35 |

| | |
|------|-------|
| 10.9 | 85.72 |
| 8.2 | 88.42 |
| 11.8 | 84.82 |
| 5.9 | 90.72 |
| 4.2 | 92.42 |
| 2.7 | 93.92 |
| 6.7 | 89.92 |
| 3.0 | 93.62 |
| 2.6 | 94.00 |
| 2.3 | 94.32 |
| 13.8 | 95.24 |
| 8.0 | 94.00 |
| 6.6 | 95.49 |
| 5.1 | 96.89 |
| 4.58 | 97.51 |
| 11.6 | 90.45 |
| 61v | 86.37 |

L

| | | | | | |
|---|-------|---|-----------------|-----------|-------|
| 131 | 69.34 | 67.53 <small>on 455 @ between FRANCIS</small> | 4.50 | 6.2 | 63.14 |
| $\frac{73.59^N}{+100} = \text{E Webster}$ | 10.5 | 58.84 <small>on 455 @ between FRANCIS</small> | 5.00 | 6.0 | 63.34 |
| + 3 S | 9.1 | 60.24 | 60' w of | 12.0 | 57.34 |
| 13 S | 9.5 | 58.84 | 550 S | 2.6 | 66.74 |
| 17 S | 11.5 | 57.84 | TP 371 | 71.59 096 | 68.38 |
| 22 S | 9.6 | 59.74 | 600 | 1.9 | 70.69 |
| 36 S = E Webster | 9.9 | 59.44 | 60' w of 600 | 5.7 | 65.89 |
| 50 S | 10.7 | 58.64 | 650 | 2.8 | 66.79 |
| 100 S | 9.4 | 59.94 | 687 | 3.5 | 68.09 |
| 150 | 6.3 | 63.34 | 700 | 4.7 | 66.89 |
| 200 S | 7.5 | 64.84 | 700 | 5.4 | 66.19 |
| 250 | 4.0 | 65.34 | 715 = E Minerva | 4.8 | 66.79 |
| 300 S | 3.5 | 65.84 | 728 | 5.5 | 66.09 |
| 340 | 4.2 | 65.14 | 740 | 5.1 | 66.49 |
| 382 | 9.0 | 60.34 | 750 | 4.1 | 67.49 |
| 388 | 11.2 | 58.14 | 800 | 3.7 | 67.89 |
| 400 | 11.7 | 57.64 | 60' w of 800 | 5.8 | 65.79 |
| 50' w of 400 | 15.7 | 53.64 | 850 | 2.2 | 69.39 |
| 415 | 11.7 | 57.64 | 900 | 1.0 | 70.59 |
| 422 | 9.2 | 60.14 | TP 2.27 | 72.14 082 | 70.77 |

100
 150
 200
 250
 300
 340
 382
 388
 400
 415
 422

L

L

| | | | |
|--------------------------|-----|------|-------------|
| 950.5 of Webster | | 27 | 70.44 |
| 1000 | | 3.1 | 70.04 |
| 60' w/ob 1000 | | 6.0 | 67.14 |
| 1050 | | 4.1 | 69.04 |
| 1100 | | 4.5 | 68.64 |
| 1125 | | 4.9 | 68.24 |
| 1129.3 = NW corner | | 16.6 | 56.54 |
| T.P. | 248 | 659 | 970 63.44 |
| check to Pol Sta. 167.00 | | 958 | 56.34 56.30 |

| | | | |
|-------------------|-------|------|-------|
| | 91.51 | 8226 | 90.8 |
| WL 36th = 0+00 | | 1.7 | 84.5 |
| 50 | | 7.0 | 80.8 |
| 100 | | 10.7 | 79.5 |
| 12215 = # Alley | | 12.0 | 78.80 |
| TP | 132 | 8012 | 77.92 |
| 150 | | 2.2 | 75.82 |
| 200 | | 4.3 | 74.42 |
| 250 | | 5.7 | 73.92 |
| 269.30 = # Pardee | | 6.2 | 73.72 |
| 300 | | 6.4 | 73.52 |
| 350 | | 6.6 | 73.62 |
| 400 | | 6.5 | 73.82 |
| 416.60 = # Alley | | 6.3 | 74.42 |
| 450 | | 5.7 | 74.02 |
| 500 | | 6.1 | 73.22 |
| 550 | | 6.9 | 72.92 |
| 568.90 = # 34th | | 7.2 | 71.82 |
| 600 | | 8.3 | 70.22 |
| 650 | | 9.9 | |

P10 H d

| | | | |
|------------------------------|------|-------|-------|
| 700 | T | 11.8 | 68.32 |
| TP | 0.71 | 68.30 | 12.53 |
| 736.39 = # Alley | | 1.5 | 66.8 |
| 750 | | 2.0 | 66.30 |
| 800 | | 4.5 | 63.80 |
| 850 | | 6.4 | 61.5 |
| 898.88 = # FRANCIS ST | | 8.4 | 59.9 |
| 925 | | 11.6 | 56.7 |
| TP | 0.49 | 56.54 | 12.25 |
| 986 | | 3.8 | 52.74 |
| 1000 | | 6.0 | 50.54 |
| 1026 | | 11.2 | 45.34 |
| TP | 0.4 | 43.89 | 12.79 |
| 1060.90 = STA 727.55 # Alley | | 3.0 | 40.86 |
| 1100 | | 11.3 | 32.59 |
| TP | 0.05 | 31.46 | 12.48 |
| 1123 | | 3.6 | 28.86 |
| 1138 | | 8.2 | 23.26 |
| TP | 161 | 20.14 | 12.93 |
| 1155 | | 3.5 | 12.64 |

on hole 40.80

3.5

| | | | |
|--|------|-------|-------|
| 1185 E edge of channel | 5.0 | 15.14 | |
| 1190 | 6.6 | 13.54 | |
| 1194 | 8.3 | 11.84 | |
| 1218 | 9.5 | 10.64 | |
| 1227.4v = E 3' ditto = E of hole creek | 11.4 | 8.74 | |
| 25' W = wedge of channel | 5.2 | 14.94 | |
| T.P. 18' 2187 | 0.8 | 20.06 | |
| back to 2nd 23rd wheel road | 4.58 | 17.29 | 17.22 |

Sewer Levels on Line 15' E of E of 34th
& Woolman to & Webster

2/20/26
Moore

| Station | Offset | Elevation | Notes |
|----------------------|--------|-----------|-------------------------------|
| ON Ht. Exh. Man | 17.4 | 216.5 | 1993 = STA 170 = Woolman Line |
| 40' N = N.W. Wool | 2.5 | 219.15 | |
| 1 + 00 N | 4.4 | 217.25 | |
| +50 | 4.9 | 216.75 | |
| 7 | 5.0 | 216.65 | |
| +50 | 4.9 | 216.75 | |
| 3 | 4.9 | 216.75 | |
| +50 | 6.5 | 215.15 | |
| +85 = Cholla Creek | 9.5 | 212.15 | |
| 4 | 10.2 | 211.35 | |
| 4 + 54.5 = & MINORVA | 10.70 | 210.95 | in bit |
| 5 | 11.6 | 210.05 | |
| +16 | 12.2 | 209.35 | |
| +47 | 11.7 | 209.95 | |
| +50 | 11.2 | 210.45 | |
| 6 | 10.2 | 211.45 | |
| +30 | 9.6 | 212.05 | |
| +50 | 10.6 | 211.05 | |
| 7 | 10.7 | 210.95 | |
| +65 | 9.8 | 211.85 | |

EXISTING Sewer in 33rd St
EXISTING M.H.

HUB 124135 = STA. of & Webster from DIST

H116933 ← ← & Webster

45' 15'

HUB 8490.93

00.00

H118415 = 12 + 4.92 = STA. of & MINORVA from DIST

H118415 ← ← & MINORVA

N

EL. 304.4

EL. 311.4

45' 15'

HUB 80400
170.25

& Woolman

TO EXISTING M.H.
& Alley South of Woolman
15' W of E. of 34th

| | | |
|--------------------------|------|-------|
| 7 +75 | 7.6 | 14.05 |
| 8 +00 | 7.8 | 13.85 |
| +50 | 6.5 | 15.15 |
| 8 +70.93 Hub of P 487 | 4.96 | 16.67 |
| 9 | 4.1 | 17.44 |
| +50 | 5.3 | 16.24 |
| 10 | 5.1 | 16.44 |
| +50 | 6.4 | 15.14 |
| +55 | 8.0 | 13.54 |
| 11 | 8.4 | 13.14 |
| +25 | 8.1 | 13.44 |
| +35 | 11.1 | 10.44 |
| +55 | 10.6 | 10.94 |
| +69.70 on Hub of Webster | 9.25 | 12.29 |

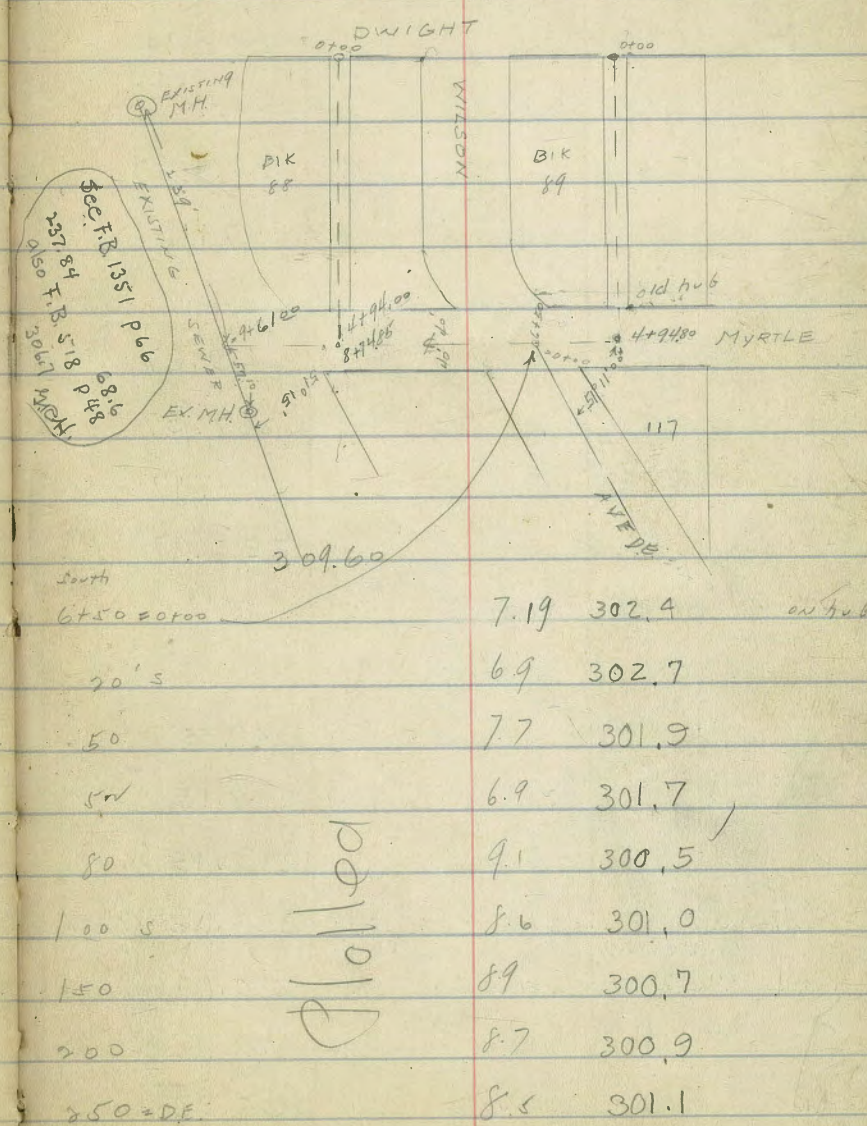
| | | |
|---------------------------|-------|---------------|
| 8 +70.93 = 0 +00 | 487 | 16.67 |
| +15 West | 9.7 | 11.84 |
| +50 | 10.1 | 11.44 |
| +75 E. edge of pond water | 10.4 | 11.14 |
| +76 | 11.6 | 9.94 |
| +720 | 12.5 | 9.04 |
| +73 | 11.6 | 9.94 |
| +24 W. edge of pond water | 10.4 | 11.14 |
| +26 | 9.4 | 12.14 |
| +29 | 4.9 | 16.64 |
| 2 +00 | 5.4 | 16.14 |
| +50 | 6.0 | 15.54 |
| 3 | 4.1 | 17.44 |
| +50 | 3.4 | 18.14 |
| 4 | 3.5 | 18.04 |
| +50 | 3.5 | 18.04 |
| 5 +00 | 3.7 | 17.84 |
| 5 +33 = EX. M.H. RIM | 3.8 | 17.74 |
| 1 - 1 = flow line | 11.05 | 10.49 = 10.83 |

11.05 10.49 = 10.83 See page 49

Sewer Levels THRU BIKs 88 + 89
Wilson + MYRTLE (EAST SAN Diego)

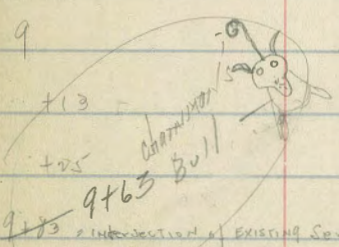
| | | | | |
|----------------------|------|--------|--------|------------------------------|
| NWBP | 129 | 328.84 | 327.55 | Howard=Dwight storey=36th |
| Thru BIK 89 | | | 4.4 | 324.44 |
| SL DWIGHT=0+00 | | | 6.1 | 322.74 |
| +50 South | | | 8.7 | 320.14 |
| 1 | | | 11.3 | 317.54 |
| +50 | | | 12.9 | 315.94 |
| T.P. | 0.70 | 316.64 | 19 | 314.74 |
| ✓ | | | 4.6 | 312.04 |
| +50 | | | 7.6 | 308.84 |
| 3 | | | 13.2 | 303.44 |
| +45 = gully | | | 11.5 | 305.14 |
| +85 | | | 10.3 | 306.34 |
| 4 | | | 9.9 | 306.74 |
| +50 | | | 9.55 | 307.14 |
| 5 + 04.80 = A 90° RT | | | 7.48 | 309.16 |
| +50 T.P. | 0.44 | 309.60 | 1.6 | 308.0 |
| 6 | | | 7.9 | 301.70 |
| +50 = A S on Wilson | | | 9.2 | 300.40 |
| +55 | | | 11.0 | 298.60 |
| +65 | | | 14.1 | 295.50 |
| +75 | | | 12.54 | 297.06 |
| T.P. | 0.35 | 297.44 | | |

Plotted



Plotted

| | | | | |
|------------|--|------------|------------|--------------|
| 7+00 | | 6.1 | 291.34 | |
| +06 | | 7.1 | 290.34 | |
| +35 | | 15.3 | 282.14 | |
| T.P. | 006 | 284.77 | 12.73 | 284.71 |
| +70 | | 9.5 | 275.27 | |
| +90 | | 12.4 | 271.37 | |
| T.P. | 082 | 272.87 | 12.72 | 272.05 |
| 8 | | 3.2 | 269.67 | |
| +15 | | 5.3 | 267.57 | |
| +35 | | 9.7 | 263.17 | |
| +65 | | 16.0 | 255.87 | |
| T.P. | 017 | 260.16 | 12.88 | 259.99 |
| 2+84.85 | T.P. | 132 | 248.45 | 1303 247.13 |
| 9 | | 7.1 | 241.35 | |
| +13 | | 10.3 | 238.15 | |
| +25 | | 12.0 | 236.45 | |
| 9+63 | | 12.49 | 235.96 | ent hub |
| 9+73 | intersection of existing sewer in water center | | | |
| EX.M.H. 29 | 57.5 | of 9+63 | = Flowline | 18.25 230.10 |
| T.P. | 10.59 | 246.55 | 12.19 | 235.96 |
| EX.M.H. 29 | N. of 9+63 | = Flowline | 10.17 | 236.38 |



| | | | | | |
|------------------|-----|--------|-------|--------|---------|
| 49744 | 065 | 278.20 | | 327.55 | 28.74 |
| SL Dright = 0200 | | | 7.80 | 320.4 | ent hub |
| +50 South | | | 9.3 | 318.9 | |
| | | | 11.5 | 316.7 | |
| +50 | | | 14.5 | 313.7 | |
| T.P. | 110 | 216.96 | 12.24 | 315.86 | |
| | | | 7.4 | 309.56 | |
| +50 | | | 12.4 | 304.56 | |
| T.P. | 016 | 304.19 | 12.93 | 304.03 | |
| +35 | | | 6.4 | 297.8 | |
| 3 | | | 9.4 | 294.8 | |
| +15 | | | 12.4 | 291.8 | |
| T.P. | 026 | 291.94 | 12.51 | 291.68 | |
| +50 | | | 11.6 | 280.34 | |
| T.P. | 085 | 279.93 | 12.85 | 279.09 | |
| +80 | | | 5.0 | 274.93 | |
| 4+00 | | | 9.1 | 270.83 | |
| T.P. | 122 | 268.17 | 12.98 | 266.95 | |
| +40 | | | 4.7 | 263.47 | |
| +80 | | | 8.9 | 259.27 | |

Pio Fed

268.17 x

4+85

10.2 257.97

T.P.

218

258.28

1207

256.10

4+90

7.2 254.08

5+0400

1118

24710

24712

8+8485

90 CROSS SECTION of
 DWIGHT ST & 47th ST South
 to Myrtle to deep cañon S of Myrtle

3/10/26
 Moore

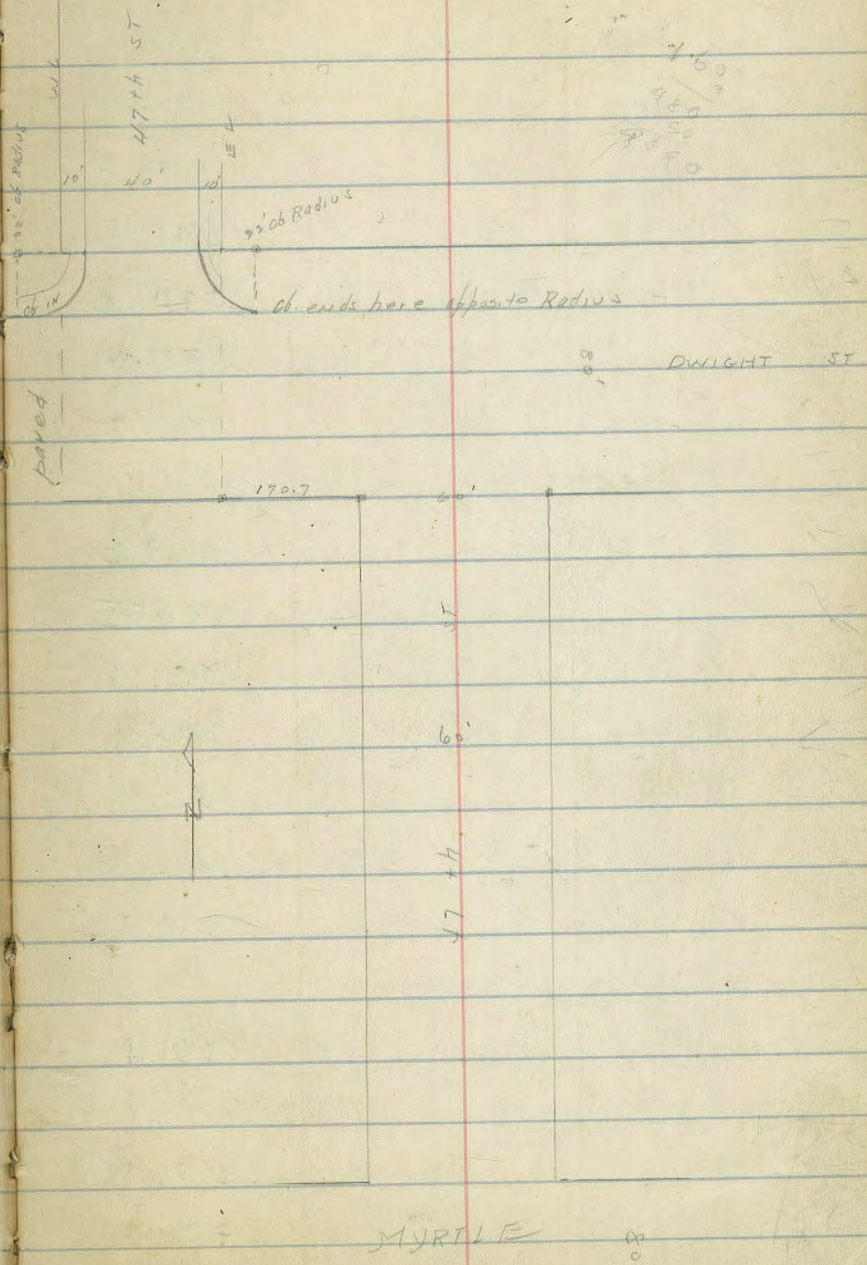
NWBP 1110 336.10 324.00 Charanne + Dwight

TP 937 344.4v 005 335.05

wl of 47th to the North = 0 + 100

| | | |
|--------------------------|------|--------|
| S | 5.9 | 338.5 |
| tr + cement cb | 6.05 | 338.4 |
| gutter on paving | 6.71 | 337.7 |
| 1/4 ✓ ✓ | 5.78 | 338.6 |
| C ✓ ✓ | 5.35 | 339.1 |
| 1/4 ✓ ✓ | 5.20 | 339.22 |
| cb on paving | 5.20 | 339.2 |
| + 3.5 = gutter pav | 5.18 | 339.2 |
| + 3.5 = cem. cb on Curve | 4.54 | 339.9 |
| N | 4.2 | 340.2 |
| wl cb | | |
| NL on cem. cb | 4.45 | 340.0 |
| 1/2 S = cb | 4.7 | 339.7 |
| 1/4 | 4.6 | 339.8 |
| e | 4.8 | 339.6 |
| 1/4 | 4.9 | 338.5 |
| cb | 5.2 | 339.2 |
| S | 5.7 | 338.7 |

Dwight = 80' wide w/cbs 9' 1/4's
 47th = 60' ✓ 10' cbs 10' 1/4's



7.60
 4.60
 9.70

80' DWIGHT ST

60'
 17
 4

MYRTLE ST

47th 344.4v

| | | |
|-----|-----|-------|
| S | 5.3 | 339.1 |
| cb | 4.9 | 339.5 |
| 1/4 | 4.6 | 338.8 |
| C | 4.4 | 340.0 |
| 1/4 | 4.4 | 340.0 |
| cb | 4.6 | 339.8 |
| N | 4.4 | 340.0 |

E of 47th

| | | |
|-----------|-----|-------|
| N cem. cb | 4.8 | 339.9 |
| rv = cb | 4.5 | 338.9 |
| 1/4 | 4.2 | 340.2 |
| C | 4.0 | 340.4 |
| 1/4 | 3.6 | 340.8 |
| cb | 4.0 | 340.4 |
| S | 5.2 | 339.2 |

EL 47th = 0+00

| | | |
|-----|-----|--------|
| S | 5.0 | 339.4 |
| cb | 3.7 | 340.7 |
| 1/4 | 3.6 | 340.8 |
| C | 4.0 | 340.42 |

| | | |
|---------------------------|------|--------|
| 1/4 | 4.1 | 340.3 |
| cb | 4.3 | 340.1 |
| + 3.5 on cem. cb on curve | 4.45 | 339.97 |
| + 10 | 4.3 | 340.0 |
| N | 4.0 | 340.42 |
| N | 3.5 | 341.1 |

+ 12 EAST

| | | |
|-------------------|------|-------|
| + 16 | 3.8 | 340.6 |
| cb end of cem. cb | 4.48 | 340.0 |
| 1/4 | 3.9 | 340.5 |
| C | 4.2 | 340.2 |
| 1/4 | 4.1 | 340.3 |
| cb | 4.2 | 340.2 |
| S | 4.5 | 339.9 |

+ 23

| | | |
|-----|-----|-------|
| S | 4.0 | 340.4 |
| cb | 4.3 | 340.1 |
| 1/4 | 4.1 | 340.3 |
| C | 4.0 | 340.4 |
| 1/4 | 3.7 | 340.7 |

390
in 6mils
check this to
of file 9410
Please

| | | |
|----------------------------|------|-------|
| cb | 3.6 | 340.8 |
| N | 3.0 | 341.4 |
| +46 | | |
| N | 3.9 | 340.5 |
| cb | 3.7 | 340.7 |
| 1/4 | 3.4 | 341.0 |
| C | 3.8 | 340.6 |
| 1/4 | 4.1 | 340.3 |
| cb | 4.1 | 340.3 |
| +18 | 4.2 | 340.2 |
| S on con platform to stone | 38.2 | 340.6 |
| +70 | | |
| -3 on con platform | 36.3 | 340.8 |
| S | 4.3 | 340.1 |
| cb | 4.3 | 340.1 |
| 1/4 | 4.4 | 340.0 |
| C | 4.2 | 340.2 |
| 1/4 | 4.4 | 340.0 |
| cb | 4.3 | 340.1 |
| N | 4.3 | 340.1 |

| | | |
|-----------------------------------|-----|---------|
| +81 | | |
| 1/2 | 4.5 | 338.9 |
| cb | 4.9 | 339.5 |
| 1/4 | 4.6 | 339.8 |
| C | 4.5 | 339.9 |
| 1/4 | 4.6 | 339.8 |
| cb | 4.3 | 340.1 |
| S | 4.3 | 340.1 |
| +8 sidewalk to residence | 4.3 | 3' wide |
| +100 | | |
| S | 4.8 | 339.6 |
| cb | 4.7 | 339.7 |
| 1/4 | 4.7 | 339.7 |
| C | 4.4 | 339.0 |
| 1/4 | 4.6 | 339.8 |
| cb | 5.0 | 338.4 |
| +5 | 4.9 | 339.5 |
| N | 4.6 | 339.8 |
| +105 | | |
| -1 = Residence under construction | 5.3 | 339.1 |
| N | 5.4 | 339.0 |

| | | | |
|------|-------------------------------|-----|-----------------------------|
| +16 | | 5.7 | 338.7 |
| d | | 5.7 | 338.7 |
| 1/4 | | 5.7 | 338.7 |
| e | | 5.5 | 338.9 |
| 1/4 | | 5.6 | 338.8 |
| d | | 6.0 | 338.4 |
| s | | 5.6 | 338.8 |
| | 1 + 70.7 = w. 47 + 6 to south | | 60' wide 10' obs & 1/4 s |
| s | | 7.5 | 336.9 |
| d | | 7.2 | 337.2 |
| 1/4 | | 6.9 | 337.5 |
| e | | 7.1 | 337.3 |
| 1/4 | | 7.3 | 337.1 |
| +1 | | 7.4 | 337.0 |
| d | | 7.0 | 337.4 |
| +1 | | 7.0 | 337.4 |
| N | | 7.5 | 336.9 |
| T.P. | 193 340.34 | 6.0 | 338.4 |
| | w/ct | | |
| N | | 4.5 | 335.8 |

| | | | |
|-----|---------|-----|--------|
| ct | | 3.9 | 336.4 |
| 1/4 | | 3.5 | 336.8 |
| e | | 3.1 | 337.2 |
| 1/4 | | 2.7 | 337.6 |
| d | | 3.2 | 337.1 |
| s | | 3.4 | 336.9 |
| | 2 w/1/4 | | |
| s | | 3.4 | 336.9 |
| d | | 3.6 | 336.7 |
| 1/4 | | 3.6 | 336.7 |
| e | | 3.7 | 336.6 |
| 1/4 | | 4.2 | 336.1 |
| d | | 4.4 | 335.9 |
| N | | 4.9 | 335.4 |
| | Φ | | |
| N | | 8.0 | 332.34 |
| +10 | | 5.9 | 334.44 |
| d | | 5.5 | 334.8 |
| 1/4 | | 5.0 | 335.3 |
| e | | 4.5 | 335.8 |

| | | | | | |
|-------|------|-------|-----|------------------|--------|
| 1/4 | 4.3 | 336.0 | S | 4.7 | 335.6 |
| cb | 4.2 | 336.1 | | EL 47th To South | |
| S | 3.7 | 336.6 | S | 5.6 | 334.7 |
| E 1/4 | | | cb | 6.2 | 334.1 |
| S | 4.3 | 336.0 | 1/4 | 7.3 | 333.0 |
| A | 4.6 | 335.7 | c | 8.4 | 331.9 |
| 1/4 | 4.8 | 335.5 | 1/4 | 10.7 | 329.6 |
| C | 5.1 | 335.2 | cb | 12.0 | 328.3 |
| 1/4 | 6.0 | 334.3 | N | 16.6 | 323.7 |
| cb | 7.4 | 332.9 | +10 | 17.7 | 322.6 |
| N | 10.5 | 329.8 | | 20' E of EL | |
| +10 | 11.0 | 329.3 | -15 | 25.0 | 315.34 |
| E cb | | | N | 23.7 | 316.6 |
| -10 | 14.2 | 326.1 | cb | 18.8 | 321.5 |
| N | 14.0 | 326.3 | 1/4 | 16.0 | 324.3 |
| cb | 8.8 | 331.5 | c | 13.3 | 327.0 |
| 1/4 | 6.7 | 333.6 | 1/4 | 11.2 | 329.1 |
| C | 5.4 | 334.9 | cb | 9.0 | 331.3 |
| 1/4 | 5.4 | 334.9 | S | 7.4 | 332.9 |
| cb | 5.4 | 335.1 | | | |

100

Cross Section of \bar{v} = 60' wide
10' obs
47th St Dwight to Myrtle

340.34

101

| St Dwight = 0+00 340.34 X | | | | | |
|---------------------------|-----|-------|-----------|--------|--------|
| | | | c | 3.8 | 336.5 |
| E | 5.7 | 334.0 | 1/4 | 3.1 | 337.2 |
| cb | 4.7 | 335.6 | cb | 2.6 | 337.7 |
| 1/4 | 4.3 | 336.0 | w | 2.4 | 337.9 |
| c | 3.7 | 336.6 | | | |
| 1/4 | 3.5 | 336.8 | w | 2.8 | 337.5 |
| cb | 3.3 | 337.0 | cb | 2.9 | 337.4 |
| w | 3.4 | 336.9 | 1/4 | 3.3 | 337.0 |
| +2.5 S | | | c | 3.7 | 336.6 |
| w | 2.8 | 337.5 | 1/4 | 4.0 | 336.3 |
| cb | 2.7 | 337.6 | cb | 4.3 | 336.0 |
| 1/4 | 3.2 | 337.1 | E | 4.2 | 336.1 |
| c | 3.9 | 336.4 | | | |
| 1/4 | 3.9 | 336.4 | E | 3.8 | 336.5 |
| cb | 3.9 | 336.4 | cb | 3.3 | 337.0 |
| E | 4.6 | 335.7 | 1/4 | 3.2 | 337.1 |
| +1.50 | | | c | 3.2 | 337.1 |
| E | 4.7 | 335.6 | 1/4 | 3.0 | 337.3 |
| cb | 4.1 | 336.2 | cb | 2.5 | 337.8 |
| 1/4 | 4.0 | 336.2 | w | 2.0 | 338.34 |
| | | | T.P. 0.52 | 338.98 | 1.88 |
| | | | | | 338.46 |

1+25

| | | |
|--------------------------------|-----|--------|
| w | 0.8 | 338.18 |
| cb | 1.0 | 337.98 |
| 1/4 | 1.0 | 337.78 |
| C | 1.4 | 337.58 |
| 1/4 | 1.8 | 337.18 |
| cb | 2.1 | 336.88 |
| E | 2.4 | 336.58 |
| 1+50 | | |
| E | 1.7 | 337.28 |
| d | 1.3 | 337.68 |
| 1/4 | 1.0 | 337.98 |
| C | 1.1 | 337.88 |
| 1/4 | 1.0 | 337.78 |
| dr | 1.0 | 337.78 |
| w | 1.3 | 337.68 |
| 1+69 = ϕ w wide sidewalk | | |
| w on Cem walk to house | 1.3 | 337.68 |
| + r. ^{walk} 14 street | 1.3 | 337.68 |
| cb | 1.6 | 337.38 |
| 1/4 | 1.1 | 337.88 |

| | | |
|------|-----|--------|
| e | 1.0 | 337.98 |
| 1/4 | 1.3 | 337.68 |
| dr | 1.3 | 337.68 |
| E | 1.3 | 337.68 |
| 200 | | |
| E | 1.9 | 337.08 |
| dr | 1.9 | 337.08 |
| 1/4 | 2.0 | 336.98 |
| e | 1.6 | 337.38 |
| 1/4 | 1.9 | 337.08 |
| dr | 2.2 | 336.78 |
| w | 1.7 | 337.28 |
| 2+25 | | |
| w | 2.9 | 336.08 |
| dr | 2.9 | 336.08 |
| 1/4 | 2.7 | 336.28 |
| C | 2.6 | 336.38 |
| 1/4 | 2.6 | 336.38 |
| cb | 2.5 | 336.48 |
| E | 2.3 | 336.68 |

| | | | |
|-----|------|-----|--------|
| E | 2+60 | 3.5 | 335.48 |
| cb | | 3.0 | 335.98 |
| 1/4 | | 3.1 | 335.88 |
| e | | 3.8 | 335.18 |
| 1/4 | | 3.8 | 335.18 |
| d | | 4.0 | 335.98 |
| w | | 4.0 | 335.98 |
| | 3+00 | | |
| w | | 5.4 | 333.58 |
| cb | | 5.4 | 333.58 |
| 1/4 | | 5.3 | 333.68 |
| c | | 5.1 | 333.88 |
| 1/4 | | 4.9 | 334.08 |
| cb | | 4.7 | 334.28 |
| E | | 4.3 | 334.68 |
| | 3+50 | | |
| E | | 6.0 | 332.98 |
| d | | 6.3 | 332.68 |
| 1/4 | | 6.4 | 332.58 |
| c | | 6.5 | 332.18 |

| | | | |
|-----|------|------|--------|
| 1/4 | | 6.8 | 332.18 |
| cb | | 7.4 | 331.58 |
| w | | 7.1 | 331.88 |
| | 5+00 | | |
| w | | 9.1 | 329.88 |
| cb | | 9.2 | 329.78 |
| 1/4 | | 8.4 | 330.58 |
| c | | 8.0 | 330.98 |
| 1/4 | | 8.0 | 330.98 |
| cb | | 7.8 | 331.18 |
| E | | 7.5 | 331.48 |
| | 5+35 | | |
| E | | 8.5 | 330.48 |
| d | | 8.9 | 330.08 |
| 1/4 | | 9.3 | 329.68 |
| c | | 9.7 | 329.28 |
| 1/4 | | 10.3 | 328.68 |
| d | | 10.3 | 328.68 |
| w | | 10.3 | 328.68 |

4+70

| | | |
|------|------|--------|
| w | 10.9 | 328.08 |
| cb | 11.3 | 327.68 |
| 1/4 | 10.9 | 328.08 |
| c | 10.5 | 328.48 |
| 1/4 | 10.1 | 328.88 |
| cb | 9.5 | 329.48 |
| E | 9.5 | 329.48 |
| 5+00 | | |
| E | 10.4 | 328.58 |
| cb | 10.7 | 328.28 |
| 1/4 | 10.8 | 328.18 |
| c | 11.4 | 327.78 |
| 1/4 | 11.7 | 327.28 |
| cb | 12.3 | 326.68 |
| w | 12.7 | 326.28 |
| 5+50 | | |
| w | 13.6 | 325.38 |
| cb | 13.5 | 325.48 |
| 1/4 | 12.6 | 326.38 |
| c | 12.3 | 326.68 |

| | | |
|---|------|--------|
| 1/4 | 12.4 | 326.58 |
| cb | 12.3 | 326.68 |
| E | 12.0 | 326.98 |
| T.P. 0.28 326.71 12.65 326.33 | | |
| FIELDS = N.E. MYTLE - 20' wide 10' 1/2 | | |
| E | 0.9 | 325.8 |
| cb | 1.0 | 324.7 |
| 1/4 | 1.3 | 325.4 |
| c | 1.7 | 325.0 |
| 1/4 | 2.1 | 324.6 |
| cb | 2.4 | 324.3 |
| w | 2.9 | 323.8 |
| Nct | | |
| w | 3.1 | 323.6 |
| cb | 3.1 | 323.6 |
| 1/4 | 2.8 | 323.9 |
| c | 2.3 | 324.4 |
| 1/4 | 1.7 | 325.0 |
| cb | 1.9 | 324.8 |
| E | 1.9 | 324.8 |

N 1/4

| | | |
|-------|-----|--------|
| E | 2.3 | 324.4 |
| cb | 2.4 | 324.3 |
| 1/4 | 2.6 | 324.1 |
| C | 2.9 | 323.8 |
| 1/4 | 3.2 | 323.5 |
| cb | 3.2 | 323.5 |
| w | 3.8 | 322.9 |
| ♀ | | |
| w | 4.2 | 322.5 |
| cb | 3.7 | 323.0 |
| 1/4 | 3.5 | 323.2 |
| C | 3.3 | 323.4 |
| 1/4 | 3.1 | 323.6 |
| cb | 2.9 | 323.8 |
| E | 2.6 | 324.1 |
| S 1/4 | | |
| E | 2.7 | 324.0 |
| cb | 2.6 | 324.11 |
| 1/4 | 3.2 | 323.5 |
| C | 3.8 | 322.9 |

| | | |
|------------------|-----|-------|
| 1/4 | 3.9 | 322.8 |
| cb | 4.1 | 322.6 |
| w | 4.6 | 322.1 |
| Sch | | |
| w | 4.9 | 321.8 |
| cb | 4.5 | 322.2 |
| 1/4 | 4.3 | 322.4 |
| e | 4.2 | 322.5 |
| 1/4 | 3.7 | 323.3 |
| cb | 2.6 | 324.1 |
| E | 3.0 | 323.7 |
| SL Myrtle = 0+00 | | |
| E | 3.2 | 323.5 |
| cb | 4.1 | 322.6 |
| 1/4 | 4.6 | 322.1 |
| C | 4.8 | 321.9 |
| 1/4 | 4.6 | 322.1 |
| cb | 5.1 | 321.6 |
| w | 5.7 | 321.0 |

at 50 - S of St. Mur + 10

| | | |
|------|------|--------|
| w | 7.4 | 319.31 |
| cb | 6.9 | 319.8 |
| 1/4 | 6.8 | 319.9 |
| c | 6.8 | 319.9 |
| 1/4 | 6.4 | 320.5 |
| cb | 5.7 | 321.0 |
| E | 5.5 | 321.2 |
| +100 | | |
| E | 8.0 | 318.71 |
| cb | 8.3 | 318.4 |
| 1/4 | 8.5 | 318.2 |
| c | 8.7 | 318.0 |
| 1/4 | 8.9 | 317.8 |
| cb | 8.9 | 317.8 |
| w | 9.3 | 317.4 |
| +200 | | |
| w | 11.4 | 315.5 |
| cb | 11.1 | 315.6 |
| 1/4 | 10.8 | 315.9 |

| | | |
|------|------|-------|
| c | 10.4 | 316.5 |
| 1/4 | 9.9 | 316.8 |
| cb | 9.7 | 317.0 |
| E | 8.9 | 317.8 |
| +750 | | |
| E | 9.9 | 316.8 |
| cb | 10.5 | 316.2 |
| 1/4 | 11.0 | 315.7 |
| c | 11.8 | 314.9 |
| 1/4 | 12.5 | 314.2 |
| cb | 14.4 | 312.3 |
| w | 15.1 | 311.6 |
| +5 | 15.4 | 311.3 |
| +775 | | |
| -10 | 21.4 | 305.5 |
| w | 20.0 | 306.7 |
| cb | 17.5 | 309.2 |
| 1/4 | 15.3 | 311.4 |
| c | 12.0 | 314.7 |
| 1/4 | 11.5 | 315.2 |

| | | |
|-----|------|-------|
| cb | 11.0 | 315.7 |
| E | 10.3 | 316.4 |
| | 2+00 | |
| E | 10.8 | 315.9 |
| cb | 11.7 | 315.0 |
| 1/4 | 12.1 | 314.6 |
| C | 13.9 | 312.8 |
| 1/4 | 15.9 | 310.8 |
| cb | 18.2 | 308.5 |
| w | 20.9 | 305.8 |
| +10 | 23.2 | 303.5 |
| | 2+25 | |
| -10 | 23.5 | 303.2 |
| w | 22.0 | 304.7 |
| cb | 19.8 | 306.9 |
| 1/4 | 16.9 | 309.8 |
| C | 15.4 | 311.3 |
| 1/4 | 14.5 | 312.2 |
| cb | 13.0 | 313.7 |
| 1/4 | 12.0 | 314.7 |

| | | | |
|---------------|--------|--------|--------|
| | 2+50 | | |
| F | 14.0 | 312.71 | |
| cb | 15.0 | 311.71 | |
| 1/4 | 16.1 | 310.61 | |
| C | 17.0 | 309.71 | |
| 1/4 | 19.0 | 307.71 | |
| cb | 21.0 | 305.71 | |
| w | 23.0 | 303.71 | |
| +10 | 25.5 | 301.21 | |
| | at +65 | | |
| T.P. | 6.85 | 326.29 | 7.7 |
| | | | 319.4 |
| check to B.M. | 22.9 | 324.00 | 324.00 |

114 Sewer Levels & Alley BIK 89 City Limits
West to Existing Sewer in Watah Canyon
on the E of Myrtle St 80' wide

4/16/66
Moore 310.03

815

| | | | | | | |
|---|--------|--------|------------------------------|--------|--------|--------|
| 289 | 310.03 | 307.14 | 6+57 | 11.1 | 298.93 | |
| √294.80 = φ Alley BIK 89 | 309 | 306.94 | +59 | 12.5 | 297.53 | |
| 5+25 | 1.0 | 309.03 | T.P. 018 | √97.56 | 12.65 | √97.38 |
| +50 | 0.4 | 309.63 | 6+96 | 5.0 | 292.56 | |
| +75 | 0.4 | 309.63 | 7+00 | 6.6 | 290.96 | |
| 6 | 1.9 | 308.13 | +12 | 9.8 | 287.66 | |
| +15 | 2.8 | 307.23 | +3√ | 15.1 | 282.46 | |
| +50 on hub A | 8.90 | 301.13 | T.P. 011 | 284.93 | 12.7√ | √84.81 |
| Sewer levels W/coal & Myrtle South 300' | | | 7+60 | 7.5 | 277.43 | |
| 0+00 = 6+50 = Junction φ Myrtle | 8.90 | 301.13 | 8+00 | 14.6 | 270.33 | |
| +25 S | 7.8 | 302.23 | T.P. 190 | √73.80 | 13.03 | √71.90 |
| +70 | 8.7 | 301.33 | 8+19 | 6.6 | 267.2 | |
| +71 | 7.7 | 302.33 | +41 | 11.7 | 262.1 | |
| +75 | 8.6 | 301.43 | T.P. 102 | 261.70 | 13.12 | √60.68 |
| +96 | 9.6 | 300.43 | +63 | 4.0 | 257.7 | |
| +98 | 9.0 | 301.03 | +74.85 = φ Alley BIK 89 C.H. | 9.2√ | 252.48 | |
| 1+40 | 9.0 | 301.03 | +85 | 14.1 | 247.60 | |
| 1985 | 9.6 | 300.43 | T.P. 359 | √84.93 | 17.36 | √49.34 |
| 2+35 | 9.2 | 300.83 | 9+00 | 9.2 | 243.73 | |
| 2+65 | 9.1 | 300.93 | T.P. 395 | √47.9 | 12.09 | √40.84 |
| 3+00 = DE | 9.0 | 301.03 | | | | |

244.79

Sawyer levels
& Myrtle

9+17 5.9 238, 89

+40 77 237, 09

9+61 at stub Existing source 142 236, 37

CROSS SECTION of ^N BIK 198 City Hqts.
(Loverne Place) ALLEY 20' wide

Between 34th & Swift + Univ. Ave + Park

| | | | | |
|---------------------------|--------|--------|--------|-----------------|
| NW. CP | 190 | 360.76 | 358.86 | Univ + Swift |
| N. UNIV. AVE = 0+00 | | | | |
| E on paving | | 5.7 | 355.04 | |
| E " " | | 6.6 | 354.50 | |
| W " " | | 6.0 | 354.36 | |
| | 11' N | | | |
| W' | | 5.0 | 355.8 | |
| C | | 5.3 | 355.5 | |
| E | | 4.7 | 356.1 | |
| | 4.5' N | | | |
| E | | 3.0 | 357.8 | |
| C | | 3.8 | 357.0 | |
| W' | | 3.8 | 357.0 | |
| | 8.3' N | | | |
| W + 0.4 | | 2.0 | 358.8 | |
| C | | 2.0 | 358.6 | |
| E | | 1.6 | 359.2 | |
| + 2.3 & Garage dirt/floor | | 1.2 | 359.5 | |

Whole
Floor 360.76

9.5' N

| | | | | |
|---------------------------------|---------|------|--------|--------------|
| E | | 1.3 | 359.5 | |
| C | | 1.6 | 359.2 | |
| + 9' & Garage dirt/floor | | 1.9 | 358.9 | in alley 1' |
| | 11.5' N | | | |
| W + 1.3 = Dwelling-plumbing etc | | 0.9 | 360.0 | in Alley 1.3 |
| e | | 0.9 | 360.0 | |
| E | | 0.7 | 360.1 | |
| + 2.8 & Garage dirt/floor | | 0.5 | 360.3 | |
| T.P. 663 (366.81) | | 0.58 | 360.18 | |
| | 12.6' N | | | |
| - 2.8 & Garage Cem./floor | | 5.8 | 361.0 | |
| E | | 6.1 | 360.7 | |
| e | | 6.5 | 360.3 | |
| + 8.7 fence | | 6.5 | 360.3 | in alley 1.3 |
| | 14.3' N | | | |
| W + 1.3 Garage cem./floor | | 6.4 | 360.4 | v v 1.3 |
| e | | 6.2 | 360.6 | |
| + 9.5 = Dwelling w/alley | | 6.0 | 360.8 | |

| | | | | | |
|-----------|---|-----|-------|--|--|
| | 160' N | | | | |
| E | ♀ Garage ^{can} Apron on line | 5.4 | 361.4 | | |
| e | | 5.8 | 361.0 | | |
| W | | 6.0 | 360.8 | | |
| underside | 160' N. St. Dwelling plumbing etc. valley 1.2 | | | | |
| | 196' N. W. r. r. r. 0.2 back of alley line | | | | |
| | 200' N | | | | |
| W | | 5.4 | 361.4 | | |
| e | | 5.1 | 361.2 | | |
| E | | 5.6 | 361.2 | | |
| | 250' N | | | | |
| E | | 4.4 | 362.4 | | |
| C | | 5.0 | 361.8 | | |
| W | | 5.1 | 361.7 | | |
| | 275' N | | | | |
| W | | 5.1 | 361.7 | | |
| C | | 5.0 | 361.8 | | |
| E | | 4.7 | 362.1 | | |
| | 306' N | | | | |
| E | | 4.3 | 362.5 | | |

| | | | | | |
|----|---------------------|-----|--------|--|--|
| e | | 4.9 | 361.9 | | |
| W | ♀ Garage Comp floor | 4.7 | 362.1 | | |
| | 350' N | | | | |
| W | | 3.8 | 363.0 | | |
| C | | 3.4 | 362.4 | | |
| E | | 3.5 | 363.3 | | |
| | 378' N | | | | |
| E | | 2.8 | 364.0 | | |
| C | | 2.7 | 364.1 | | |
| W | | 3.3 | 363.5 | | |
| | 400' N | | | | |
| W | | 2.5 | 364.3 | | |
| C | | 2.5 | 364.3 | | |
| E | | 2.2 | 364.6 | | |
| | 450' N | | | | |
| E | | 1.5 | 365.3 | | |
| C | | 1.2 | 365.6 | | |
| W | | 1.7 | 365.1 | | |
| TP | 666 372.64 0.83 | | 365.98 | | |

500' ✓

W 6.6 366.0

E 6.6 366.0

E 6.5 366.1

550' ✓

E 5.7 367.2

C 5.7 367.2

W 5.6 367.0

590' ✓

W 5.0 367.6

C 5.1 367.5

E 5.1 367.5

599.6' ✓ - SL Pk

E top Alley return 5.7 366.67

C on paving w/ks of Alley paved 6.8 366.06

W ✓ ✓ 6.40 366.24

W top Alley return 6.13 366.51

TP 0.4 369.31 3.47 369.17

check to BM 10.43 358.88 358.86

124

125

128

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140

141

142

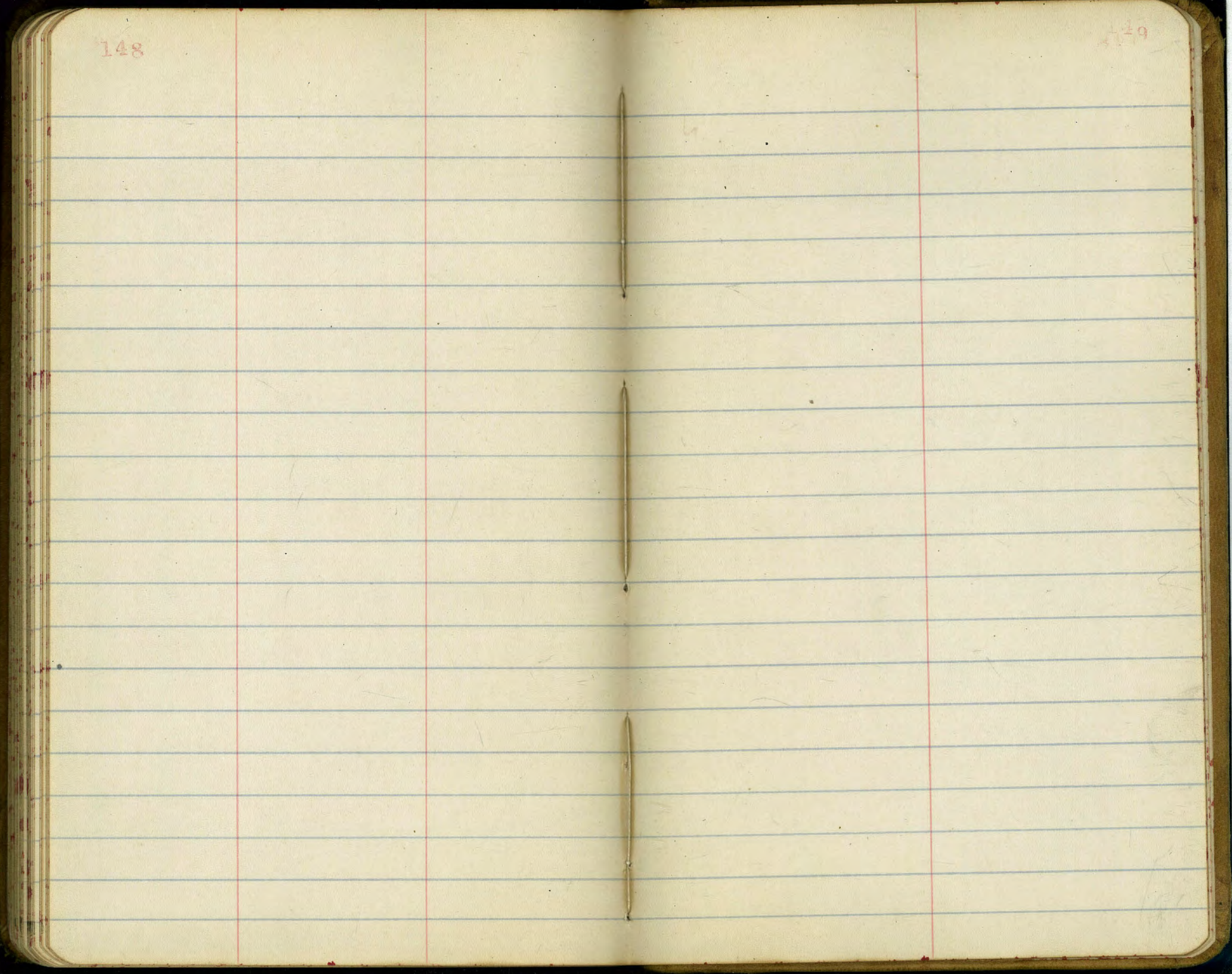
143

144

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152

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$$\begin{array}{r} 198.4 \\ 16.1 \\ \hline 182.3 \end{array}$$
$$\begin{array}{r} 182.3 \\ 21.7 \\ \hline 160.6 \end{array}$$
$$\begin{array}{r} 160.6 \\ 27.1 \\ \hline 133.5 \end{array}$$
$$\begin{array}{r} 133.5 \\ 20.8 \\ \hline 112.7 \end{array}$$

| | |
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8226
 883
 88.09 = 117.

1256
 2.07
 15.43

974.8
 70.48
 260.0

504
 30
 474

44.00
 448
 39.70

14.07
 1.26
 13.81
 480
 18.35

227
 1128
 1128

1700
 1500
 320.4

512
 850
 13.96

8900 2' 30"
 878.70

97.00
 200
 95.00
 96.06
 24

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 TO 1. ROADWAY OF ANY WIDTH.

| | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | |
|----|------|------|------|------|------|------|------|------|------|------|----|
| 0 | 0 | .1 | .2 | .3 | .4 | .5 | .6 | .7 | .8 | .9 | 0 |
| 1 | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.6 | 1.7 | 1.8 | 1.9 | 1 |
| 2 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 2 |
| 3 | 3.0 | 3.1 | 3.2 | 3.3 | 3.4 | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 3 |
| 4 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 4 |
| 5 | 5.0 | 5.1 | 5.2 | 5.3 | 5.4 | 5.5 | 5.6 | 5.7 | 5.8 | 5.9 | 5 |
| 6 | 6.0 | 6.1 | 6.2 | 6.3 | 6.4 | 6.5 | 6.6 | 6.7 | 6.8 | 6.9 | 6 |
| 7 | 7.0 | 7.1 | 7.2 | 7.3 | 7.4 | 7.5 | 7.6 | 7.7 | 7.8 | 7.9 | 7 |
| 8 | 8.0 | 8.1 | 8.2 | 8.3 | 8.4 | 8.5 | 8.6 | 8.7 | 8.8 | 8.9 | 8 |
| 9 | 9.0 | 9.1 | 9.2 | 9.3 | 9.4 | 9.5 | 9.6 | 9.7 | 9.8 | 9.9 | 9 |
| 10 | 10.0 | 10.1 | 10.2 | 10.3 | 10.4 | 10.5 | 10.6 | 10.7 | 10.8 | 10.9 | 10 |
| 11 | 11.0 | 11.1 | 11.2 | 11.3 | 11.4 | 11.5 | 11.6 | 11.7 | 11.8 | 11.9 | 11 |
| 12 | 12.0 | 12.1 | 12.2 | 12.3 | 12.4 | 12.5 | 12.6 | 12.7 | 12.8 | 12.9 | 12 |
| 13 | 13.0 | 13.1 | 13.2 | 13.3 | 13.4 | 13.5 | 13.6 | 13.7 | 13.8 | 13.9 | 13 |
| 14 | 14.0 | 14.1 | 14.2 | 14.3 | 14.4 | 14.5 | 14.6 | 14.7 | 14.8 | 14.9 | 14 |
| 15 | 15.0 | 15.1 | 15.2 | 15.3 | 15.4 | 15.5 | 15.6 | 15.7 | 15.8 | 15.9 | 15 |
| 16 | 16.0 | 16.1 | 16.2 | 16.3 | 16.4 | 16.5 | 16.6 | 16.7 | 16.8 | 16.9 | 16 |
| 17 | 17.0 | 17.1 | 17.2 | 17.3 | 17.4 | 17.5 | 17.6 | 17.7 | 17.8 | 17.9 | 17 |
| 18 | 18.0 | 18.1 | 18.2 | 18.3 | 18.4 | 18.5 | 18.6 | 18.7 | 18.8 | 18.9 | 18 |
| 19 | 19.0 | 19.1 | 19.2 | 19.3 | 19.4 | 19.5 | 19.6 | 19.7 | 19.8 | 19.9 | 19 |
| 20 | 20.0 | 20.1 | 20.2 | 20.3 | 20.4 | 20.5 | 20.6 | 20.7 | 20.8 | 20.9 | 20 |
| 21 | 21.0 | 21.1 | 21.2 | 21.3 | 21.4 | 21.5 | 21.6 | 21.7 | 21.8 | 21.9 | 21 |
| 22 | 22.0 | 22.1 | 22.2 | 22.3 | 22.4 | 22.5 | 22.6 | 22.7 | 22.8 | 22.9 | 22 |
| 23 | 23.0 | 23.1 | 23.2 | 23.3 | 23.4 | 23.5 | 23.6 | 23.7 | 23.8 | 23.9 | 23 |
| 24 | 24.0 | 24.1 | 24.2 | 24.3 | 24.4 | 24.5 | 24.6 | 24.7 | 24.8 | 24.9 | 24 |
| 25 | 25.0 | 25.1 | 25.2 | 25.3 | 25.4 | 25.5 | 25.6 | 25.7 | 25.8 | 25.9 | 25 |
| 26 | 26.0 | 26.1 | 26.2 | 26.3 | 26.4 | 26.5 | 26.6 | 26.7 | 26.8 | 26.9 | 26 |
| 27 | 27.0 | 27.1 | 27.2 | 27.3 | 27.4 | 27.5 | 27.6 | 27.7 | 27.8 | 27.9 | 27 |
| 28 | 28.0 | 28.1 | 28.2 | 28.3 | 28.4 | 28.5 | 28.6 | 28.7 | 28.8 | 28.9 | 28 |
| 29 | 29.0 | 29.1 | 29.2 | 29.3 | 29.4 | 29.5 | 29.6 | 29.7 | 29.8 | 29.9 | 29 |
| 30 | 30.0 | 30.1 | 30.2 | 30.3 | 30.4 | 30.5 | 30.6 | 30.7 | 30.8 | 30.9 | 30 |
| 31 | 31.0 | 31.1 | 31.2 | 31.3 | 31.4 | 31.5 | 31.6 | 31.7 | 31.8 | 31.9 | 31 |
| 32 | 32.0 | 32.1 | 32.2 | 32.3 | 32.4 | 32.5 | 32.6 | 32.7 | 32.8 | 32.9 | 32 |
| 33 | 33.0 | 33.1 | 33.2 | 33.3 | 33.4 | 33.5 | 33.6 | 33.7 | 33.8 | 33.9 | 33 |
| 34 | 34.0 | 34.1 | 34.2 | 34.3 | 34.4 | 34.5 | 34.6 | 34.7 | 34.8 | 34.9 | 34 |
| 35 | 35.0 | 35.1 | 35.2 | 35.3 | 35.4 | 35.5 | 35.6 | 35.7 | 35.8 | 35.9 | 35 |
| 36 | 36.0 | 36.1 | 36.2 | 36.3 | 36.4 | 36.5 | 36.6 | 36.7 | 36.8 | 36.9 | 36 |
| 37 | 37.0 | 37.1 | 37.2 | 37.3 | 37.4 | 37.5 | 37.6 | 37.7 | 37.8 | 37.9 | 37 |
| 38 | 38.0 | 38.1 | 38.2 | 38.3 | 38.4 | 38.5 | 38.6 | 38.7 | 38.8 | 38.9 | 38 |
| 39 | 39.0 | 39.1 | 39.2 | 39.3 | 39.4 | 39.5 | 39.6 | 39.7 | 39.8 | 39.9 | 39 |
| 40 | 40.0 | 40.1 | 40.2 | 40.3 | 40.4 | 40.5 | 40.6 | 40.7 | 40.8 | 40.9 | 40 |
| 41 | 41.0 | 41.1 | 41.2 | 41.3 | 41.4 | 41.5 | 41.6 | 41.7 | 41.8 | 41.9 | 41 |
| 42 | 42.0 | 42.1 | 42.2 | 42.3 | 42.4 | 42.5 | 42.6 | 42.7 | 42.8 | 42.9 | 42 |
| 43 | 43.0 | 43.1 | 43.2 | 43.3 | 43.4 | 43.5 | 43.6 | 43.7 | 43.8 | 43.9 | 43 |
| 44 | 44.0 | 44.1 | 44.2 | 44.3 | 44.4 | 44.5 | 44.6 | 44.7 | 44.8 | 44.9 | 44 |
| 45 | 45.0 | 45.1 | 45.2 | 45.3 | 45.4 | 45.5 | 45.6 | 45.7 | 45.8 | 45.9 | 45 |
| 46 | 46.0 | 46.1 | 46.2 | 46.3 | 46.4 | 46.5 | 46.6 | 46.7 | 46.8 | 46.9 | 46 |
| 47 | 47.0 | 47.1 | 47.2 | 47.3 | 47.4 | 47.5 | 47.6 | 47.7 | 47.8 | 47.9 | 47 |
| 48 | 48.0 | 48.1 | 48.2 | 48.3 | 48.4 | 48.5 | 48.6 | 48.7 | 48.8 | 48.9 | 48 |
| 49 | 49.0 | 49.1 | 49.2 | 49.3 | 49.4 | 49.5 | 49.6 | 49.7 | 49.8 | 49.9 | 49 |
| 50 | 50.0 | 50.1 | 50.2 | 50.3 | 50.4 | 50.5 | 50.6 | 50.7 | 50.8 | 50.9 | 50 |