1148

DIETZGEN

TRADE MARK

ENGINEERS

LEVEL BOOK

No. 410

EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

28th St. X Sec of the W. 50' ft of 100' St from S. Line of B. to N. Line C. 1/22/26 mills

B.M.	0.64	207.62		206.98	N.W. cor & A
T.P.	1.15	198.09	10.66	196.94	
W. Line 28th S. ch of B St			1.20	196.89	on cmt ch
		00=S Line B. St			
N			1.0	197.1	
+25' E			0.7	197.4	
+50' E = ℄ 100' St = W ch of graded st			1.13	196.96	on return
		10' S			
℄			2.0	196.1	
+10			1.7	196.4	
+20			2.7	195.4	
+30			2.9	195.2	
+35			5.0	193.1	
+50 = W			8.3	189.8	
		18' S			
W			10.4	187.7	
+7			8.8	189.3	
+20			3.9	194.2	
+35			3.0	195.1	

198.09

+40	2.2	195.9
+50 = ℄	2.5	195.6
	30' S	
℄	3.4	194.7
+12	3.0	195.1
+18	4.5	193.6
+30	5.4	192.7
+35	6.7	191.4
+45	8.1	190.0
+50 = W	11.8	186.3
	40' S	
W	11.6	186.5
+3	9.2	188.9
+17	7.7	190.4
+20	5.5	192.6
+32	4.9	193.2
+37	3.6	194.5
+50 = ℄	4.0	194.1

1

	198.09		
	50' S		
℄		4.8	193.3
+12		4.3	193.8
+13		5.3	192.8
+30		5.8	192.3
+47		10.2	187.9
+50 = W		12.6	185.5
	60' S		
W		13.1	185.0
+4		10.4	187.7
+15		8.7	189.4
+24		4.3	191.8
+39		5.3	192.8
+50 = ℄		5.8	192.3
	70' S		
℄		6.3	191.8
+12		6.2	191.9
+16		7.5	190.6
+25		8.1	190.0
+40		10.9	187.2
+50 = W		15.8	182.3

	198.09		
	82' S		
W		20.9	177.2
+20		14.1	184.0
+25		11.6	186.5
+32		11.1	187.0
+36		7.2	190.9
+50 = ℄		7.2	190.9
	100' S		
℄		8.6	189.5
+11		8.5	189.6
T.P.	246	12.73	185.36
+22		5.0	183.0
+27		5.5	182.5
+30		6.9	181.1
+50 = W		12.3	175.7
	125' S		
W		15.3	172.7
+19		9.8	178.2
+22		9.5	178.5
+24		8.1	179.9
+39		0.1	187.9
+50 = ℄		0.4	187.6

188.02

150' S

℄	2.2	185.8
+10	2.1	185.9
+17	5.7	182.3
+22	7.9	180.1
+26	10.7	177.3
+33	13.2	174.8
+50: W	16.8	171.2

175' S

W	20.0	168.0
+4	19.1	168.9
+10	19.1	168.9
+13	17.0	171.0
+22	14.0	174.0
+32	9.0	179.0
+40	3.8	184.2
+50: ℄	4.0 4.6	184.0 183.4

200' S

℄	5.9	182.1
+10	5.9	182.1
+20	12.7	175.3

188.02

+29	17.6	170.4
+32	18.2	169.8
+33	19.8	168.2
+40	19.6	168.4
+50: W	22.1	165.9

225' S

W	23.4	164.6
+7	22.6	165.4
+14	21.4	166.6
+15	20.0	168.0
+22	19.9	168.1
+23	18.5	169.5
+34	12.1	175.9
+40	7.6	180.4
+50: ℄	7.8	180.2

250' S

℄	9.7	178.3
+10	9.7	178.3
+19	16.3	171.7
+20	18.9	169.1

188.02

R50 S (con)

+28	18.2	169.8 ✓
+36	23.6	164.4 ✓
+40	24.1	163.9 ✓
+50 = W	25.0	163.0 ✓

R68.' S

W	25.0	163.0 ✓
+14	23.9	164.1 ✓
+24	16.4	171.6 ✓
+33	17.2	170.8 ✓
+40	10.9	177.1 ✓
+50 = ℄	11.0	177.0 ✓

R78.' S

℄	11.7	176.3 ✓
+10	11.8	176.2 ✓
+14	15.3	172.7 ✓
+21	14.7	173.3 ✓
+31	15.1	172.9 ✓
+50 = W	20.0	168.0 ✓

R87.' S

W	14.3	173.7 ✓
+17	13.8	174.2 ✓

188.02

28th

4

+18	14.4	173.6 ✓
+37	13.8	174.2 ✓
+40	12.4	175.6 ✓
+50 = ℄	12.3	175.7 ✓

295.' S

℄	12.9	175.1 ✓
+10	12.7	175.3 ✓
+25	13.5	174.5 ✓
+50 = W	14.0	174.0 ✓

300.' S = N. Line : E St.

W	14.1	173.9 ✓
+25	13.6	174.4 ✓
+40	13.0	175.0 ✓
+50 = ℄	13.1	174.9 ✓
chk BM	12.05	175.97 = 175.98

N.E. 28.4 E

20' Wide. Alley Blk 60 City Hts 1/22/26
bet 35th & Wilson. Univ. to Wightman N.W. Univ & 35th

B.M.	3.51	365.06		361.55	
	Rotten	00= S. Line Univ Ave			
W			4.23	360.83	cpt paving
C			4.53	360.53	Paving
E			4.45	360.61	cl+paving
		20' S			
E			4.6	360.5	
C			5.2	59.9	
W			4.5	60.6	
		50' S = double Garage on W. dirt floor 7.5 Back			
-7.5			5.0	60.1	
W			5.3	59.8	
C			5.2	59.9	
E			5.2	59.9	
		100' S			
E			5.8	59.3	
C			6.0	59.1	
W			6.2	58.9	
		120' S			
W			6.6	58.5	
C			6.4	58.7	

5

365.06

E		6.5	58.6	
145' S Garage on W cmt floor 7' Back				
" " E dirt " 8' "				
E		7.2	57.9	
C		7.1	58.0	
W		7.2	57.9	
215' S garage on W cmt floor 7' Back				
W		8.2	56.9	
C		8.0	57.1	
E		7.9	57.2	
	359.95			357.18
T.P.	2.77 (259.95)	7.88	257.18	
225' S Garage on E dirt floor 8' Back				
	250' S			
E		3.5	56.5	
C		3.2	56.8	
W		3.7	56.3	
280' S garage on W cmt floor 9' Back				
" " E dirt " 8' "				
W		3.7	56.3	
C		3.4	56.6	
E		3.8	56.2	

259.95

300.'S

E		3.7	56.3 ✓
C		3.9	56.1 ✓
W		3.9	56.1 ✓

325'S garage on E dirt floor 8' Back

340'S double " " W " " 3' "

W-3		3.9	56.1 ✓
W		3.9	56.1 ✓
C		4.0	56.0 ✓
E		4.4	55.6 ✓

370'S

E		4.6	55.4 ✓
C		4.6	55.4 ✓
W		4.6	55.4 ✓

400'S

W		5.0	55.0 ✓
C		5.1	54.9 ✓
+5		4.8	55.2 ✓
E		5.4	54.6 ✓

450'S

E		5.7	54.3 ✓
C		5.6	54.4 ✓
W		5.6	54.4 ✓

fence 1.1 in alley

259.95

4.85'S

Blk 60 CityHts

6

W		6.4	53.6 ✓
C		6.3	53.7 ✓
E		6.7	53.3 ✓ Fence 1.4 in alley

510'S. garage on W dirt floor 10' back

530'S " " " " " 8' back

E		6.9	53.1 ✓
C		7.2	52.8 ✓
W		7.1	52.9 ✓

565'S

W		7.5	52.5 ✓
C		7.5	52.5 ✓
E		7.4	52.6 ✓

592'S

E		7.5	52.5 ✓
C		7.7	52.3 ✓
W		7.7	52.3 ✓

600'S = N. Line Wightman

W		8.20	51.75 ✓ cmt el.
C		8.2	51.8 ✓
E		8.50	51.45 ✓

40' wide GEORGIA COURT X Sec from E. Line Georgia st to W Line Florida St

B.M.	0.14	312.13		311.99	1/22/26 Muller S W Georgia & Robinson
T.P.	0.49	299.77	12.85	299.28	
	E. ¢ Line Georgia				
N			4.88	294.89 ✓	cmt cb
	00 = E. Line Georgia				
N			4.6	295.2 ✓	
+10			5.6	294.2 ✓	
+20			5.8	294.0 ✓	
+30			6.3	293.5 ✓	
+40 = S			6.9	292.9 ✓	
T.P.	5.65	292.42	13.00	286.77 ✓	
		15' E			
S-20			12.1	280.3 ✓	
S-15			11.6	280.8 ✓	
S			3.4	289.0 ✓	
+2			2.6	289.8 ✓	
+10			2.3	290.1 ✓	
+20			1.5	290.9 ✓	
+30			1.1	291.3 ✓	
+40=N			0.4	292.0 ✓	

		292.42		
		50' E		
N			7.0	285.4 ✓
+10			7.3	285.1 ✓
+20			8.3	284.1 ✓
+30			9.4	283.0 ✓
+38			9.5	282.9 ✓
+40=S			10.1	282.3 ✓
T.P.	3.21	283.34	12.29	280.13 ✓
+15			8.3	275.0 ✓
+25			9.0	274.3 ✓
		70' E		
S-25			11.9	271.4 ✓
S-15			10.2	273.1 ✓
S			4.2	279.1 ✓
+1			3.5	279.8 ✓
+10			3.3	280.0 ✓
+20			2.1	281.2 ✓
+30			1.2	282.1 ✓
+40=N			0.7	282.6 ✓

		283.34		
		100' E		
N			3.9	279.4 ✓
+10			4.6	278.7 ✓
+20			5.3	278.0 ✓
+30			6.2	277.1 ✓
+40=S			6.2	277.1 ✓
		150' E		
S			11.6	271.7 ✓
+10			11.3	272.0 ✓
+20			10.5	272.8 ✓
+30			10.0	273.3 ✓
+40=N			9.3	274.0 ✓
T.P.	0.16	270.50	13.00	270.34 ✓
		195' E		
N			0.9	269.6 ✓
+10			1.8	268.7 ✓
+20			2.1	268.4 ✓
+30			3.1	267.4 ✓
+40=S			3.5	267.0 ✓

Georgia Court

		270.50		
		206' E garage on ^(& Fence) S 1.0 in street		
S			4.4	266.1 ✓
+10			4.4	266.1 ✓
+20			3.3	267.2 ✓
+30			2.8	267.7 ✓
+40=N			2.1	268.4 ✓
		230' E		
N			4.4	266.1 ✓
+10			4.9	265.6 ✓
+20			5.4	265.1 ✓
+30			6.4	264.1 ✓
+40=S			6.3	264.2 ✓
		250' E		
S			7.3	263.2 ✓
+10			7.3	263.2 ✓
+20			6.6	263.9 ✓
+30			6.2	264.3 ✓
+40=N			5.6	264.9 ✓
		280' E		
N			6.7	263.8 ✓
+10			7.0	263.5 ✓

	270.50		
	280' E (com)		
+20		7.6	262.9
+30		8.4	262.1
+40=S		8.5	262.0
	295' E		
S		8.8	261.7
+10		8.8	261.7
+20		8.1	262.4
+30		7.7	262.8
+38		7.5	263.0
+40=N		8.5	262.0
+10		13.0	257.5
+20		14.0	256.5
	310' E		
N-20		14.7	255.8
-7		14.1	256.4
N		12.8	257.7
+8		11.1	259.4
+10		11.1	259.4
+20		11.6	258.9
+23		11.5	259.0

	270.50		Georgia Court
+30		9.4	261.1
+40=S		9.2	261.3
	320' E = W. Line Florida		
S		9.2	261.3
+10		8.9	261.6
+20		8.4	262.1
+30		7.9	262.6
+40=N		7.3	263.2
	W. ch Line Florida		
N		7.62	262.88 on cmt ch
S		9.62	260.88 " " "

80' wide
14' cls
13' 1/4s

Market St X Sec. from 41st to 43rd — 2/16/26 mille

B.M.	1.63	135.51		133.88	Old Boundary Line Mon 170' N. of Market
T.P.	8.08	139.43	4.16	131.35	
B.M. Spk Tel Pole E7930T			0.61	138.82	N.W. Raven & Market
T.P.	0.95	127.33	13.05	126.38	
BM Spike Elec Pole 7L704			4.05	123.28	S.E. Market & 41st St.

W. Line 41st St 60' wide 127.3
10' cls
10' 1/4s

S	2.2	125.1
+10	2.4	124.9
cl	3.0	124.3
1/4	3.5	123.8
+5	2.9	124.4
c	2.5	124.8
1/4	2.4	124.9
+5	1.9	125.4
cl	1.3	126.0
N	0.6	126.7

W. cl.

N	0.7	126.6
cl	1.5	125.8
1/4	2.5	124.8

127.33

c	2.8	124.5
+6	3.1	124.2
1/4	3.8	123.5
+5	4.0	123.3
cl	3.6	123.7
S	2.1	125.2

W 1/4

S	2.7	124.6
cl	4.1	123.2
1/4	4.0	123.3
+7	3.2	124.1
c	2.8	124.5
1/4	2.5	124.8
+10	2.2	125.1
cl	1.5	125.8
N	0.8	126.5

8' E. of W 1/4

N	0.9	126.4
cl	1.4	125.9
+3	2.3	125.0

127.33

1/4		2.6	124.7
c		3.0	124.3
1/4		4.1	123.2
cl		4.5	122.8
S		3.3	124.0
	℄		
S		4.1	123.2
cl		4.7	122.6
1/4		4.2	123.1
c		3.0	124.3
1/4		2.8	124.5
cl		2.0	125.3
N		1.7	125.6
	E. 1/4		
N		1.9	125.4
cl		2.0	125.3
1/4		3.2	124.1
c		3.3	124.0
1/4		4.4	122.9
cl		4.2	123.1
S		4.4	122.9

127.33
E. cl

-5		5.0	122.3
S		5.0	122.3
cl		5.3	122.0
1/4		4.6	122.7
c		3.8	123.5
1/4		3.7	123.6
+7		3.6	123.7
cl		3.0	124.3
N		2.5	124.8
	00= E. line 41st St.		
N		3.4	123.9
cl		3.4	123.9
+3		4.4	122.9
1/4		4.2	123.1
c		4.3	123.0
1/4		4.9	122.4
cl		5.7	121.6
S		6.0	121.3
+5		5.8	121.5

127.33

30' E

			127.3
-5		7.3	120.0
S		6.7	120.6
+5		6.5	120.8
el		6.4	120.9
15		6.0	121.3
+8		6.6	120.7
1/4		6.5	120.8
C		6.1	121.2
1/4		6.0	121.3
+11		5.8	121.5
el		4.7	122.6
N		4.6	122.7

50' E

N		5.3	122.0
+12		5.2	122.1
el		6.8	120.5
1/4		6.8	120.5
C		6.9	120.4
1/4		7.7	119.6
el		7.7	119.6

127.33

Mark-et

127.3

S		7.7	119.6
+5		8.6	118.7

65' E

-5		9.7	117.6
S		9.5	117.8
el		9.2	118.1
1/4		8.4	118.9
C		7.7	119.6
1/4		7.6	119.7
el		8.0	119.3
+2		6.4	120.9
N		6.3	121.0

90' E

N		8.0	119.3
+11		7.7	119.6
el		9.1	118.2
1/4		8.5	118.8
C		8.5	118.8
1/4		9.0	118.3
el		10.0	117.3
S		10.5	116.8
+5		10.8	116.5

	127.33		127.3
	112' E		
S-5		10.2	117.1
S		10.1	117.2
℄		11.7	115.6
1/4		10.9	116.4
℄		9.8	117.5
1/4		9.8	117.5
℄		10.4	116.9
N		10.7	116.6
+10		11.1	116.2
	120' E		
-10		12.9	114.4
N		11.8	115.5
℄		10.6	116.7
1/4		10.0	117.3
℄		10.2	117.1
1/4		11.3	116.0
℄		12.0	115.3
+2		11.6	115.7
S		10.3	117.0
+5		10.4	116.9

			Market	
	127.33		127.3	
	142' E		114.3	
-10		13.0		
S		13.2	114.1	
℄		13.1	114.2	
1/4		12.5	114.8	
+5 = S. end 12" Bottom S.I Pipe		12.5	114.8	Flowline no yardage
+8		11.0	116.3	
℄		10.5	116.8	
1/4		10.4	116.9	
+3 = N. end 12" Pipe		12.0	115.3	Flowline no yardage
+3		11.2	116.1	
℄		11.3	116.0	
N		11.6	115.7	
+10		11.0	116.3	
	145' E			
-5		9.8	117.5	
N		10.2	117.1	
℄		11.0	116.3	
1/4		10.5	116.8	
℄		10.9	116.4	
1/4		11.7	115.6	

	127.33		127.3
+9		12.8	114.5
el		13.7	113.6
+9		13.9	113.4
+10		13.3	114.0
S		13.3	114.0
+10		14.1	113.2
	172' E		
-10		14.5	112.8
S		13.8	113.5
el		12.9	114.4
1/4		11.6	115.7
C		10.8	116.5
1/4		10.5	116.8
el		10.6	116.7
+2		9.5	117.8
N		8.8	118.5
+5		8.5	118.8
	190' E		
N		7.1	120.2
+10		7.6	119.7

	127.33		Market 127.3
el		9.8	117.5
1/4		10.0	117.3
C		10.5	116.8
1/4		11.4	115.9
el		12.2	115.1
S		12.7	114.6
+10		13.5	113.8
	210' E		
-10		13.6	113.7
S		12.2	115.1
el		11.7	115.6
1/4		10.9	116.4
C		9.7	117.6
1/4		8.9	118.4
el		9.0	118.3
+4		5.9	121.4
N		5.6	121.7
	236' E = W Line Morrison St		50' Wide 10' els
N		6.1	121.2
+10		6.6	120.7

		127.33		127.3
+11			8.4	118.9
cl			8.3	119.0
1/4			8.9	118.4
c			9.4	117.9
1/4			10.4	116.9
cl			11.3	116.0
S			13.2	114.1
+5			13.0	114.3
+10			10.8	116.5
		3' E		
-5			11.1	116.2
S			11.1	116.2
cl			11.2	116.1
1/4			10.5	116.8
c			9.6	117.7
1/4			8.8	118.5
cl			8.3	119.0
N			7.4	119.9
		W. cl.		
N			7.4	119.9

		127.33		Market 127.3
cl			8.2	119.1
1/4			8.7	118.6
c			9.4	117.9
1/4			10.2	117.1
cl			10.8	116.5
S			10.6	116.7
+5			10.9	116.4
		℄		
-5			10.6	116.7
S			10.5	116.8
cl			10.4	116.9
1/4			9.7	117.6
c			8.8	118.5
1/4			8.8	118.5
cl			8.5	118.8
N			7.8	119.5
		E. cl		
N			8.0	119.3
cl			8.5	118.8
1/4			8.7	118.6

	127.33		127.3
C		8.6	118.7
1/4		9.1	118.2
cl		10.0	117.3
S		10.4	116.9
+5		10.4	116.9
	00 = E. Line Morrison		
S-5		9.6	117.7
S		9.6	117.7
cl		9.2	118.1
1/4		8.4	118.9
C		8.2	119.1
1/4		8.4	118.9
cl		8.8	118.5
N		8.2	119.1
	35' E.		
N-5		8.4	118.9
N		8.3	119.0
cl		7.4	119.9
1/4		6.5	120.8
C		6.0	121.3

	127.33		Market 127.3
1/4		6.4	120.9
cl		6.2	121.1
+1		6.2	121.1
+4		5.6	121.7
S		5.1	122.2
	60' E.		
S		2.1	125.2
+8		2.3	125.0
+12		3.7	123.6
cl		3.7	123.6
1/4		3.7	123.6
C		4.2	123.1
1/4		5.0	122.3
cl		6.3	121.0
N		6.8	120.5
+10		7.3	120.0
	80' E		
-5		5.2	122.1
N		5.1	122.2
cl		5.0	122.3

		127.33		127.3
1/4			3.4	123.9
C			2.3	125.0
1/4			2.5	124.8
cl			2.0	125.3
+3			1.0	126.3
S			0.1	127.2
T.P.	8.97	136.00	0.30	127.03
		120' E		136.9
S			5.5	130.5
cl			8.3	127.7
1/4			8.9	127.1
C			9.0	127.0
1/4			9.9	126.1
+10			10.8	125.2
cl			10.5	125.5
N			11.3	124.7
+10			13.0	123.0
		145' E.		
-10			12.6	123.4
N			11.5	124.5

		136.00		Market 136.0
cl			10.1	125.9
1/4			8.6	127.4
C			7.5	128.5
1/4			6.9	129.1
cl			6.2	129.8
S			4.9	131.1
		160' E		
S			4.7	131.3
cl			5.6	130.4
1/4			4.6	129.4
C			6.9	129.1
1/4			8.1	127.9
cl			9.7	126.3
N			11.4	124.6
+10			12.0	124.0
		200' E		
-10			10.8	125.2
N			9.8	126.2
cl			8.7	127.3
1/4			7.4	128.6

		136.00		136.0
e			4.8	129.2
1/4			6.4	129.6
cl			5.6	130.4
s			4.3	131.7
		R 20' E		
s			3.7	132.3
cl			4.8	131.2
1/4			5.5	130.5
c			5.7	130.3
1/4			6.6	129.4
cl			7.0	129.0
N			7.9	128.1
+5			8.8	127.2
		R 36' E = W Line	H 2nd	St 50' wide 10' cbs
-5			128.1	7.9
N			128.4	7.6
cl			129.4	6.6
1/4			129.8	6.2
c			130.7	5.3
1/4			130.8	5.2

		136.00		Market 136.0
cl			5.1	130.9
s			3.8	132.2
+20			3.0	133.0
		W cl		
s			3.9	132.1
cl			5.0	131.0
1/4			5.2	130.8
c			5.4	130.6
1/4			6.2	129.8
cl			6.7	129.3
N			7.3	128.7
+5			8.0	128.0
		E		
-5			7.6	128.4
N			7.0	129.0
cl			6.3	129.7
1/4			5.9	130.1
c			5.2	130.8
1/4			5.0	131.0
cl			4.6	131.4
s			3.3	132.7

		134.00 E. el.		136.0
S			3.0	133.0
el			4.0	132.0
1/4			4.2	131.8
C			4.5	131.5
1/4			5.4	130.6
el			5.8	130.2
N			6.4	129.6
+5			6.9	129.1
		.00 = E. Line 42nd St.		
-20			7.4	128.6
N			6.0	130.0
el			5.4	130.6
1/4			4.9	131.1
C			4.0	132.0
1/4			3.6	132.4
el			3.7	132.3
S			3.2	132.8
+20			2.5	133.5
		25' E		
S			2.6	133.4

		136.00		136.0
el			2.6	133.4
1/4			2.6	133.4
C			3.3	132.7
1/4			4.1	131.9
el			4.6	131.4
N			5.0	131.0
		62' E.		
N-10			5.6	130.4
N			4.5	131.5
el			4.0	132.0
1/4			3.7	132.3
C			3.3	132.7
1/4			2.8	133.2
el			2.8	133.2
+3			2.4	133.6
S			2.2	133.8
		90' E		
S			1.8	134.2
+11			1.9	134.1
el			2.5	133.5

136.00

				136.0
1/4			3.2	132.8
C			3.4	132.6
1/4			4.0	132.0
cl			3.2	130.8
N			5.4	130.6
+5			5.4	130.6
		125' E		
N			3.8	132.2
cl			4.3	131.7
1/4			3.8	132.2
C			3.4	132.6
1/4			3.3	132.7
cl			3.3	132.7
+2			2.8	133.2
S			2.6	133.4
		140' E		
S			1.6	134.4
+12			2.2	133.8
cl			2.8	133.2
1/4			2.6	133.4

136.00

				136.0
C			2.9	133.1
1/4			3.7	132.3
cl			4.0	132.0
N			3.0	133.0
		165' E		
N-5			3.8	132.2
N			3.9	132.1
cl			3.7	132.3
1/4			3.3	132.7
C			2.4	133.6
1/4			2.0	134.0
cl			2.3	133.7
+2			1.9	134.1
S			1.1	134.9
		185' E		
S			2.0	134.0
+12			2.2	133.8
cl			2.8	133.2
1/4			2.4	133.6
C			2.7	133.3

	136.00			136.0
1/4		3.2	132.8	
cl		3.5	132.5	
N		3.4	132.6	
+5		3.4	132.6	
	200' E			
-5		3.3	132.7	
N		2.8	133.2	
cl		2.9	133.1	
1/4		3.1	132.9	
c		2.6	133.4	
1/4		2.4	133.6	
cl		2.7	133.3	
+2		2.2	133.8	
S		2.1	133.9	
	215' E			
S		2.7	133.3	
+12		2.1	133.9	
cl		2.6	133.4	
1/4		2.5	133.5	
c		2.6	133.4	

	136.00			Market 136.0
1/4		3.1	132.9	
cl		3.2	132.8	
N		3.0	133.0	
	136' E = W. Line Tayne. 50' wide 10' els			
-20		2.2	133.8	
N		3.2	132.8	
cl		3.2	132.8	
1/4		2.9	133.1	
c		2.8	133.2	
1/4		3.2	132.8	
cl		3.8	132.2	
S		4.0	132.0	
+20		4.3	131.7	
	W. cl			
S		4.4	131.6	
cl		4.0	132.0	
1/4		3.3	132.7	
c		2.8	133.2	
1/4		2.8	133.2	
cl		3.2	132.8	
N		3.2	132.8	

	136.00 ℄		136.0
N		3.3	132.7
cl		3.3	132.7
1/4		3.1	132.9
c		2.8	133.2
1/4		3.3	132.7
cl		4.3	131.7
S		4.7	131.3
	E. cl		
S		4.9	131.1
cl		4.6	131.4
1/4		3.9	132.1
c		3.3	132.7
1/4		3.5	132.5
cl		3.4	132.6
N		3.1	132.9
	00 = Elvington Toyne		
-20		2.6	133.4
N		2.3	133.7
cl		3.2	132.8
1/4		3.6	132.4

	136.00		Market 136.0
C		3.7	132.3
1/4		4.0	132.0
cl		5.2	130.8
S		5.8	130.2
+20		6.0	130.0
	18. E		
-5		6.5	129.5
S		6.3	129.7
+10		6.3	129.7
cl		5.1	130.9
1/4		4.5	131.5
C		4.3	131.7
1/4		3.9	132.1
cl		3.2	132.8
N		2.7	133.3
	20. E		
S-5		6.6	129.4
S		6.4	129.6
+4		6.4	129.6
+7		8.3	127.7
+10		6.1	129.9
S. cl		5.3	130.7

	136.00		136.0
	24' E		
S-5		6.8	129.2
S		6.6	129.4
+3		8.6	127.4
+7		6.3	129.7
S cl		5.3	130.7
	27' E		
S-10		9.2	127.8
S		8.8	127.2
+5		4.2	129.8
S cl		5.3	130.7
	30' E		
N		3.4	132.6
cl		3.9	132.1
1/4		4.4	131.6
C		4.3	131.7
1/4		4.6	131.4
cl		5.1	130.9
S		6.4	129.6
+5		9.1	126.9
+ 15		9.7	126.3

	136.00		136.0
	45' E		
- 10		6.4	129.6
S		5.0	131.0
+10		4.2	131.8
cl		4.8	131.2
1/4		4.5	131.5
C		4.4	131.6
1/4		4.3	131.7
cl		4.0	132.0
N		3.6	132.4
	65' E		
N		2.8	133.2
cl		3.8	132.2
1/4		4.4	131.6
C		4.5	131.5
1/4		4.6	131.4
cl		5.0	131.0
+3		4.4	131.6
S		5.2	130.8
+10		6.7	129.3

Market

		136.00		
		85' E		136.8
-10			6.5	129.5
S			6.0	130.0
+18			5.6	130.4
cl			6.1	129.9
1/4			5.1	130.9
C			4.6	131.4
1/4			4.1	131.9
cl			3.1	132.9
N			2.0	134.0
		100' E		
N			2.2	133.8
cl			2.9	133.1
1/4			4.3	131.7
C			4.6	131.4
1/4			5.2	130.8
cl			5.8	130.2
+2			5.4	130.6
S			6.0	130.0
+5			6.3	129.7
T.P. on Pipe Blk Cor	2.31	132.53	5.78	130.22

S.E. Toy in C
+ Market

		132.53		Market
		140' E		132.5
S			2.0	130.5
+10			1.7	130.8
+11			2.4	130.1
cl			2.0	130.5
1/4			1.4	131.1
C			1.3	131.2
1/4			1.5	131.0
+3			1.6	130.9
+5			0.6	131.9
cl			0.0	132.5
N			+0.3	132.8
		160' E.		
N			+0.3	132.8
cl			0.3	132.2
+6			0.9	131.6
+8			2.2	130.3
1/4			1.9	130.6
C			1.7	130.8
1/4			1.9	130.6
cl			2.5	130.0

	132.53		132.5
+3		2.7	129.8
+4		2.3	130.2
S		3.1	129.4
	180		
S		5.1	127.4
+9		4.2	128.3
cl		3.9	128.6
1/4		3.2	129.3
c		3.0	129.5
1/4		2.9	129.6
+5		2.9	129.6
+7		0.7	131.8
cl		0.6	131.9
N		0.0	132.5
	R00' E		
N		0.1	132.4
cl		1.2	131.3
+6		1.5	131.0
+8		4.0	128.5
1/4		4.0	128.5

			Market
	132.53		132.5
c		4.7	127.8
1/4		5.0	127.5
cl		5.7	126.8
S		7.3	125.2
+5		7.9	124.6
	R20' E		
-10		10.9	121.6
S		9.5	123.0
cl		7.6	124.9
1/4		6.9	125.6
c		5.4	127.1
1/4		4.6	127.9
+4		4.1	128.4
+6		2.3	130.2
cl		1.4	131.1
N		0.2	132.3
	R36' E. = W. line Eugenia St.		50's to 10's
N		0.5	132.0
cl		2.1	130.4
+6		3.0	129.5

	132.53		132.5
+8		5.0	127.5
1/4		5.4	127.1
c		6.6	126.0
1/4		8.1	124.4
cl		9.1	123.4
S		11.4	121.1
+10		13.0	119.5
+25		13.4	119.1
	4' E. of N line		
S		11.9	120.6
cl		9.5	123.0
1/4		8.4	124.1
c		6.9	125.6
1/4		5.6	126.9
cl		3.6	128.9
N		2.1	130.4
	W. cl.		
N		2.4	130.1
cl		4.2	128.3
1/4		6.1	126.4

			Market
	132.53		132.5
c		7.4	125.1
1/4		8.8	123.7
cl		10.0	122.5
S		11.6	120.9
	℄		
S		11.2	121.3
cl		10.5	122.0
1/4		9.5	123.0
c		8.6	123.9
1/4		7.3	125.2
cl		5.3	127.2
N		3.7	128.8
	E. cl		
N		4.4	128.1
cl		7.2	125.3
1/4		9.0	123.5
c		9.8	122.7
1/4		10.1	122.4
cl		11.1	121.4
S		11.8	120.7

132.53

00 = ℄ Line Eugenia St

			132.5
S-20		13.0	119.5
S		12.8	119.7
℄		12.3	120.2
+5		11.1	121.4
1/4		10.6	121.9
E		10.2	122.3
1/4		9.8	122.7
+7		9.5	123.0
℄		8.4	124.1
N		5.5	127.0
+27		1.2	131.3
+30		0.0	132.5
	25' E		
-5		7.7	124.8
N		8.5	124.0
℄		10.3	122.2
1/4		11.2	121.3
+3		11.1	121.4
+4		10.2	122.3
E		10.6	121.9

132.53

Market

			132.5
1/4		10.6	121.9
+7		11.6	120.9
+9 = 5. end 12" Rolled pipe culvert		12.6	119.9
℄		12.4	120.1
S		12.4	120.1
+10		12.1	120.4
	61' E		
-10		10.5	122.0
S		10.5	122.0
℄		10.5	122.0
1/4		10.5	122.0
E		10.2	122.3
+7		10.2	122.3
+10 N. end Pipe culvert		12.6	119.9
+11		11.4	121.1
1/4		11.9	120.6
+3		12.8	119.7
℄		13.1	119.4
+1		12.0	120.5
N		10.9	121.6
+10		9.8	122.7

flow line no yardage

flow line no yardage

	132.53 85' E.		132.5
-10		10.7	121.8
N		11.6	120.9
+2		13.5	119.0
el		13.1	119.4
+2		10.9	121.6
1/4		10.2	122.3
E		9.2	123.3
1/4		9.6	122.9
el		9.1	123.4
S		8.4	124.1
+10		8.1	124.4
	88' E		
-10		7.7	124.8
S		8.0	124.5
el		8.9	123.6
1/4		9.4	123.1
E		9.0	123.5
1/4		9.9	122.6
el		11.1	121.4
+2		13.1	119.4

	132.53		Market 132.5
N		13.2	119.3
+4		11.4	121.1
+14		10.9	121.6
	102' E		
-18		11.2	121.3
-12		12.6	119.9
N		13.2	119.3
+2		10.4	122.1
el		9.6	122.9
1/4		8.6	123.9
E		8.0	124.5
1/4		8.2	124.3
el		8.0	124.5
S		7.0	125.5
+5		6.8	125.7
	108' E		
-5		6.7	125.8
S		6.9	125.6
el		7.6	124.9
1/4		7.7	124.8

		132.53		132.5
C			7.5	125.0
1/4			8.2	124.3
el			9.2	123.3
N			10.1	122.4
+3			13.0	119.5
+15			13.0	119.5
	112' E of W Line H3rd St.			
-20			12.9	119.6
-4			12.9	119.6
-2			10.2	122.3
N			9.5	123.0
el			8.5	124.0
1/4			7.5	125.0
E			7.0	125.5
1/4			7.3	125.2
el			7.1	125.4
S			6.5	126.0
+20			5.7	126.8
Check on B.M. Book 1107 P. 28			5.38	127.15 = 127.14

Market

		132.53		132.5
	12' E of W Line			
S			4.7	127.8
el			5.6	126.9
1/4			6.0	126.5
C			5.8	126.7
1/4			6.1	126.4
el			6.0	126.5
+1			5.2	127.3
N			5.8	126.7
	30' E.			
N			6.0	126.5
el			5.2	127.3
1/4			5.3	127.2
E			4.8	127.7
1/4			4.6	127.9
el			3.7	128.8
S			2.7	129.8

	132.53 40' E		132.5
S		1.9	130.6
cl		3.4	129.1
1/4		4.2	128.3
C		4.6	127.9
1/4		4.8	127.7
cl		5.3	127.2
N		6.5	126.0

Cross Section Ingraham St.
From N L Diamond to N L Beryl

80' Wide
20' Cb's
10' Gts

BM	9.58	86.77		77.19	Nail SE Diamond & Haines E gnd. Back Stop
		0+0 = N L Diamond			
N			3.2	83.6	
Cb			2.7	84.1	
+2			3.7	83.1	
1/4			3.2	83.6	
℄			2.7	84.1	
1/4			2.5	84.3	
Cb			2.9	83.4	
+3			2.9	83.9	
+4			2.0	84.8	
E			1.6	85.2	
		50' N			
E			1.1	85.7	
+13			1.4	85.4	
+17			2.2	84.6	
Cb			2.3	84.5	
1/4			1.8	85.0	
℄			2.1	84.7	
1/4			2.5	84.3	

4-1-26
Sisson
Bliss
Northern

		86.77			
+2			2.7	84.1	
Cb			2.2	84.6	
+7			2.4	84.4	
N			2.6	84.2	
		100' N			
N			1.8	85.0	
Cb			1.6	85.2	
+3			2.1	84.7	
1/4			2.2	84.6	
℄			1.5	85.3	
+2			1.0	85.8	
1/4			1.1	85.7	
Cb			1.3	85.5	
+4			1.4	85.4	
TP	10.38	97.12	0.03	86.74	
+9			10.6	86.5	
E			10.0	87.1	
		135' = ℄ Alley			
E			9.2	87.4	
+4			9.6	87.5	
+8			10.5	86.6	

Ingraham		97.12		
cb			11.1	86.0
¼			11.0	86.1
℄			11.3	85.8
+5			11.9	85.2
¼			11.9	85.2
+3			11.7	85.4
Cb			12.2	84.9
W			12.7	84.4
		N50'W		
W			12.0	85.1
Cb			11.5	85.6
¼			11.4	85.7
+4			11.3	85.8
℄			10.9	86.2
¼			10.7	86.4
Cb			10.8	86.3
+8			10.6	86.5
E			9.3	87.8
		200'N		
E			8.0	89.1
+4			9.0	88.1

		97.12		
+15			9.9	87.2
Cb			9.7	87.4
¼			9.7	87.4
℄			10.0	87.1
¼			10.4	86.7
Cb			10.8	86.3
W			11.2	85.9
		250'N		
W			10.0	87.1
+14			9.3	87.8
cb			9.4	87.7
¼			9.0	88.1
℄			8.7	88.4
¼			8.4	88.7
cb			8.3	88.8
+8			8.5	88.6
+9			8.0	89.1
E			7.2	89.9
		N65'E		
E			6.8	90.3
+14			8.0	89.1

Ingraham		97.12			
Cb			7.8	89.3	
1/4			8.0	89.1	
℄			8.2	88.9	
1/4			8.4	88.7	
Cb			8.9	88.2	
+4			8.4	88.7	
W			8.7	88.4	
		270'W = ℄ Missouri			Missouri 80' Wide 20 Cbs 10' Qts
W			7.0	90.1	
+11			7.1	90.0	
+17			8.1	89.0	
Cb			8.3	88.8	
+6			8.7	88.4	
1/4			8.3	88.8	
℄			8.1	89.0	
1/4			7.9	89.2	
Gutter			8.0	89.1	
Cb Top			7.20	89.92	Cb Return
E			7.0	90.1	
		S Cb			
E			7.03	90.09	on Cb Return

		97.12			
Gutter			7.8	89.3	
Cb			7.7	89.4	
1/4			7.4	89.8	
℄			7.5	89.7	
1/4			7.8	89.3	
+6			8.1	89.0	
Cb			7.6	89.5	
W			7.7	89.4	
		S 1/4			
W			7.4	89.7	
Cb			7.2	89.9	
+5			7.9	89.2	
1/4			7.5	89.6	
℄			7.0	90.1	
1/4			7.0	90.4	
Cb			7.5	89.6	
E			7.0	90.1	
		℄ Missouri			
E			6.5	90.6	
Cb			7.2	89.9	
+5			7.2	89.9	

Ingraham

97.12

1/4			6.7	90.4	
℄			6.8	90.3	
1/4			7.2	89.9	
+5			7.4	89.7	
Cb			7.0	90.1	
W			7.3	89.8	
		N 1/4			
W			7.1	90.0	
Cb			6.8	90.3	
+5			7.2	89.9	
1/4			6.9	90.2	
℄			6.6	90.5	
1/4			6.8	90.3	
+6			7.1	90.0	
Cb			7.1	90.0	
E			6.5	90.6	
		N Cb			
E			6.06	91.06	on Cb Rel
Gutter			6.7	90.4	
Cb			7.0	90.1	
1/4			6.4	90.7	

97.12

℄			6.2	90.9	
1/4			6.6	90.5	
+5			6.9	90.2	
Cb			6.8	90.3	
W			7.0	90.1	
		N℄ Missouri			
W			6.7	90.4	
Cb			6.0	91.1	
+5			6.2	90.9	
1/4			5.8	91.3	
℄			5.3	91.8	
77			5.1	92.0	
1/4			5.4	91.7	
+5			6.1	91.0	
Gutter			6.5	90.6	
Cb			6.08	91.04	on Cb Return
E			5.7	91.4	
		2' N			
E			3.8	93.3	
Cb			5.0	92.1	
71			5.7	91.4	

Ingraham		97.12					97.12		
+5			5.8	91.3		¼		1.7	95.4
¼			5.2	91.9		℄		2.0	95.1
+3			5.0	92.1		+5		2.1	95.0
℄			5.2	91.9		¼		2.7	94.4
¼			5.6	91.5		Cb		3.0	94.1
+5			6.2	90.9		N		3.8	94.3
Cb			6.1	91.0				135'N = ℄ Alley	
N			6.6	90.5		N		2.6	94.5
		50'N				Cb		2.1	95.0
N			5.4	91.7		+4		2.2	94.9
Cb			4.7	92.4		¼		1.7	95.4
¼			4.2	92.9		+6		1.3	95.8
℄			3.4	93.7		℄		1.0	96.1
¼			3.5	93.6		¼		0.9	96.2
Cb			3.4	93.7		Cb		1.1	96.0
+4			3.3	93.8		+3		1.0	96.1
E			2.2	94.9		TP	11.62	108.39	0.05 97.07
		100'N				E			10.6 97.8
E			0.8	96.3				150'N	
Cb			1.8	95.3		E			10.2 98.2
+6			1.7	95.4		Cb			11.7 96.7

Ingraham	108.39			
¼		11.9	96.5	
E		11.7	96.6	
¼		12.4	96.0	
Cb		12.8	95.6	
+5		12.7	95.7	
W		13.3	96.1	
	200'N			
W		11.7	96.7	
+15		11.0	97.4	
Cb		11.0	97.4	
¼		10.7	97.7	
+9		10.7	97.7	
E		10.1	98.3	
¼		10.1	98.3	
Cb		10.0	98.4	
+9		9.4	99.0	
E		9.0	99.4	
	250'N			
E		7.1	101.3	
+16		7.4	101.0	
Cb		8.3	100.1	

	108.39			
¼		8.4	100.0	
E		8.2	100.2	
+6		8.9	99.5	
¼		9.2	99.2	
Cb		9.4	99.0	
+8		9.5	99.9	
W		10.4	98.0	
	275'N -SL Chalcedony			
W		9.2	99.2	Chalcedony 80'W.de 20'Cbs 10'Qtz
+12		9.0	99.4	
Cb		8.8	99.6	
¼		8.4	100.0	
E		7.5	100.9	
¼		7.7	100.7	
Gutter		8.2	100.2	
		6.9	101.5	
Cb top		6.92	101.47	on Cb Rock
E		6.5	101.9	
	5 Cb			
E		6.72	101.67	
Gutter		7.5	100.9	
Cb		7.4	101.0	
¼		7.1	101.3	

Ingraham		108.39		
E			7.0	101.4
+5			7.1	101.3
1/4			7.5	100.9
Cb			7.9	100.4
W			8.8	99.6
		5 1/4		
W			8.0	100.4
Cb			7.5	100.9
1/4			7.1	101.3
+5			6.8	101.6
E			6.7	101.7
1/4			6.8	101.6
Cb			6.9	101.5
E			6.5	101.9
		E Chalcedony		
E			6.3	102.1
Cb			6.5	101.9
1/4			6.5	101.9
E			6.5	101.9
1/4			6.9	101.5
Cb			7.2	101.2

		108.39		
W			7.7	100.7
		N 1/4		
W			7.5	100.9
Cb			6.8	101.6
1/4			6.2	102.2
E			5.9	102.5
1/4			6.0	102.4
Cb			6.2	102.2
E			6.2	102.2
		N Cb		
E			5.7	102.7
Cb			6.2	102.2
1/4			5.8	102.6
E			5.4	103.00
1/4			5.8	102.6
Cb			6.4	102.0
W			7.3	101.1
		W Chalcedony		
W			7.1	101.3
Cb			5.7	102.7
1/4			5.0	103.4

Ingraham

		108.39		
+5			4.5	103.9
E			4.5	103.9
¼			4.6	103.8
+3			4.5	103.9
Cb			5.3	103.1
E			5.4	103.0
		8'N		
E			3.0	105.4
Cb			3.8	104.6
¼			4.5	103.9
E			4.4	104.0
¼			4.8	103.6
Cb			5.6	102.8
N			7.0	101.4
		25'N		
W			6.1	102.3
+13			4.9	103.5
Cb			4.6	103.8
¼			4.0	104.4
E			3.3	105.1
+3			3.2	105.2

		108.39		
¼			3.7	104.7
Cb			3.0	105.4
+11			1.7	106.7
E			1.5	106.9
		50'N		
E			0.8	107.6
Cb			1.7	106.7
+6			2.3	106.1
¼			2.9	105.5
+6			3.0	105.4
E			2.7	105.7
¼			3.1	105.3
Cb			3.6	104.8
+8			3.8	104.6
N			5.0	103.4
		100'N		
N			5.0	103.4
+4			5.0	103.4
+5			4.3	104.1
+15			3.6	104.8
Cb			3.4	105.0

Ingraham

		108.39			
1/4			3.1	105.3	
+4			3.2	105.2	
℄			2.2	106.2	
1/4			1.7	106.7	
Cb			1.5	106.9	
E			1.0	107.4	
TP	12.37	118.91 ✓	1.85	106.54	
		135 N = ℄ Alley			
E		11.0		107.9	
Cb		11.4		107.5	
+3		12.1		106.8	
1/4		11.9		107.0	
℄		12.5		106.4	
1/4		13.0		105.9	
+7		13.3		105.6	
Cb		14.0		104.9	
+5		14.4		104.5	
+9		13.5		105.4	
W		14.4		104.5	
		150' N			
W		14.3		104.6	

+16			14.1	104.8	
Cb			13.5	105.4	
1/4			12.9	106.0	
+4			12.6	106.3	
+5			12.2	106.7	
℄			12.0	106.9	
1/4			11.5	107.4	
Cb			11.1	107.8	
E			10.4	108.5	
		200' N			
E			8.6	110.3	
+15			9.6	109.3	
Cb			9.6	109.3	
1/4			10.2	108.7	
℄			11.0	107.9	
+4			11.0	107.9	
+5			11.5	107.4	
1/4			11.6	107.3	
Cb			12.0	106.9	
+2			12.4	106.5	
+9			13.3	105.6	

Topographer

W			139	105.0	
		250 N			
W			13.0	105.9	
cb			12.5	106.4	
+5			11.3	107.6	
1/4			11.1	107.8	
℄			10.7	108.2	
1/4			10.0	108.9	
cb			9.1	109.8	
+7			8.9	110.0	
E			7.4	111.5	
		270 N = SL Low			Low 80' wide 20 cbs 10 Qts
E			7.0	111.9	
+12			8.5	110.4	
cb			8.9	110.0	
1/4			9.5	109.4	
℄			10.2	108.7	
1/4			10.5	108.4	
+5			11.0	107.9	
cb			12.0	106.9	
W			12.8	106.1	

		S cb			
W			12.1	106.8	
cb			11.3	107.6	
+5			10.7	108.2	
1/4			10.2	108.7	
℄			9.5	109.4	
1/4			9.0	109.9	
+5			8.2	110.7	
cb			8.3	110.6	
+3			8.1	110.8	
E			6.6	112.3	
		S 1/4			
E			6.2	112.7	
+16			8.0	110.9	
cb			7.8	111.1	
+5			7.9	111.0	
1/4			8.7	110.2	
℄			9.3	109.6	
1/4			10.0	108.9	
+5			10.4	108.3	
cb			10.8	108.1	

Ingraham 11891

W		11.9	107.0
	℄ Low W		
W		11.6	107.3
Cb		10.6	108.3
+5		10.2	108.7
¼		9.8	109.1
℄		9.0	109.9
¼		8.7	110.2
+7		7.6	111.3
Cb		7.6	111.3
+5		7.6	111.3
E		5.9	113.0
	N ¼		
E		5.6	113.3
+15		7.2	111.7
Cb		7.3	111.6
+3		7.4	111.5
¼		8.2	110.7
℄		8.9	110.0
¼		9.4	109.5
+5		9.8	109.1

Cb		10.3	108.6
W		11.2	107.7
	N Cb		
W		11.1	107.8
Cb		10.0	108.9
+5		9.4	109.5
¼		9.1	109.8
℄		8.6	110.3
¼		7.6	111.3
+8		6.7	112.2
Cb		6.8	112.1
+5		6.8	112.1
E		5.1	113.8
	040 = N ℄ Low		
E		4.1	114.8
+15		6.1	112.8
Cb		6.0	112.9
+3		6.0	112.9
¼		7.0	111.9
+8		7.5	111.4
℄		8.2	110.7

Ingrahams		118.91			
¼			8.3	110.6	
+5			8.8	110.1	
cb			9.3	109.6	
W			10.2	108.7	
TP	9.41	126.36	19.6	116.95	Nail, Pole SW Cor Ingrahams Alley Bet. Lane & Barry 116.88 No 1193 Page 15
		50'N			
W			15.5	110.9	
cb			14.7	111.7	
+5			14.5	111.9	
+8			13.6	112.8	
¼			13.8	112.6	
℄			13.3	113.1	
+3			12.3	114.1	
¼			12.1	114.3	
+6			11.3	115.1	
cb			11.3	115.1	
+5			11.3	115.1	
E			9.4	116.5	
		100'N			
E			6.7	119.2	
+12			8.4	118.0	

		126.36		
cb			8.4	118.0
¼			9.4	117.0
℄			10.6	115.8
¼			11.3	115.1
+5			11.5	114.9
cb			12.0	114.4
W			12.6	113.8
		135'N ℄ Alley		
W			10.1	116.3
cb			9.5	116.9
+5			8.5	117.9
¼			8.8	117.6
℄			8.5	117.9
+3			7.4	119.0
¼			7.1	119.3
+8			6.3	120.1
cb			5.9	120.5
+8			5.8	120.6
E			3.9	122.5
		150'N		
E			2.1	124.3

Ingrahom		126.36					126.36		
+15			4.5	121.9	TP	13.07	138.88 ✓	0.55	125.81
Cb			4.6	121.8			250'N		
+5			5.0	121.4	E			10.0	128.9
¼			5.6	120.8	+15			11.4	127.5
E			6.8	119.6	Cb			11.2	127.7
+1			7.4	119.0	¼			12.1	126.8
¼			7.7	118.7	+8			12.3	126.6
+8			7.7	118.7	~~Cb~~ E			13.0	125.9
Cb			8.2	118.2	+2			13.4	125.5
W			9.1	117.3	¼			13.4	125.5
		200'N			Cb			14.5	124.4
W			5.3	121.1	W			15.4	123.5
Cb			4.4	122.0			270'N = SL Beryl		
¼			3.7	122.7	W			14.2	124.7
E			3.4	123.0	Cb			13.0	125.9
+2			2.5	123.9	¼			12.4	126.5
¼			2.2	124.2	E			12.1	126.8
+6			1.7	124.7	¼			11.0	127.9
Cb			1.4	125.0	Cb			10.4	128.5
+6			1.7	124.7	+5			10.3	128.6
E			0.1	126.3	E			8.7	130.2

Beryl
80'wide
20'Obs
10'Qts

Ingraham

138.88

SCb

E		7.2	131.6
+15		9.3	129.6
Cb		9.3	129.6
1/4		10.1	128.5
+5		10.6	128.3
℄		10.6	128.3
1/4		11.5	127.4
+5		12.0	126.9
Cb		12.0	126.9
W		12.7	126.2
	5 1/4		
W		12.2	126.7
Cb		11.5	127.4
+5		11.3	127.6
1/4		10.8	128.1
℄		10.1	128.8
1/4		9.2	128.7
Cb		8.4	130.5
+5		7.9	131.0
E		6.2	132.7

℄ Beryl

E		5.1	133.8
+11		5.5	133.4
Cb		6.8	132.1
1/4		8.3	130.6
℄		9.1	129.8
1/4		9.9	129.0
+5		10.5	128.4
Cb		10.5	128.4
W		11.5	127.4
	N 1/4		
W		10.7	128.2
Cb		10.0	128.9
+5		9.8	129.1
1/4		9.2	129.7
℄		8.3	130.6
+7		7.6	131.3
1/4		7.6	131.7
Cb		5.7	133.2
+6		4.1	134.8
E		3.6	135.3
	N Cb		

Ingraham	138.88		
E		2.3	136.6
+/2		3.5	135.4
Cb		4.5	134.4
1/4		5.7	133.2
2		7.0	131.9
1/4		8.2	130.6
Cb		8.8	130.1
+C		9.0	129.9
M		9.9	129.0
	NL Sery/		
M		8.0	130.9
Cb		6.8	132.1
+C		6.4	132.5
1/4		6.0	132.9
2		4.5	134.4
1/4		3.5	135.4
Cb		1.9	137.0
E		0.0	138.9

Cross Section Ingraham St
75' Wide From West Line
From Diamond to Moorland

75' Wide
12' Cbs
12.75 Qts

BM	8.10	85.29		77.19	Nail SE Diamond + Haines Fendback Stop
		S.L. Diamond			
W			4.1	81.2	
Cb			3.4	81.9	
1/4			3.6	81.7	
℄			3.2	82.1	
1/4			3.1	82.2	
Cb			3.1	82.2	
E +5			2.9	82.4 / 83.3	
		45' S			
-5 E			4.0	82.5 / 81.3	
Cb			4.0	81.3	
1/4			3.6	81.7	
℄			4.1	81.2	
+10			4.9	80.3	
1/4			3.8	81.5	
Cb			4.3	81.0	
W			5.2	80.1	
		90' S			
W			6.2	79.1	

		85.29			4-2-26 Sisson Bliss Northern
Cb			5.9	79.4	
1/4			5.2	80.1	
+1			6.1	79.2	
℄			5.3	80.0	
1/4			4.8	80.5	
Cb			4.8	80.5	
E -5			4.9	80.4 / 81.6	
		135' S ℄ Alley			
+5 E			5.8	80.6 / 79.5	
Cb			5.7	79.6	
1/4			5.9	79.6	
℄			6.1	79.2	
+10			7.0	78.3	
1/4			6.3	79.0	
Cb			6.5	78.8	
W			7.0	78.3	
		180' S			
W			8.2	77.1	
Cb			7.5	77.8	
1/4			7.4	77.9	
+1			8.3	77.0	

Ingraham

85.29

℄			7.2	78.1	
¼			6.6	78.7	
cb			7.0	78.3	
E			7.0	78.3	
+5				79.6	
		225'			
-5				78.8	
E			7.8	77.5	
cb			7.7	77.6	
¼			7.6	77.7	
℄			8.2	77.1	
+10			9.0	76.3	
¼			8.5	76.8	
cb			8.4	76.9	
W			9.4	75.9	
		270'S - NL Emerald			Emerald 86' Wide 20' Cbs 10' Qts
W			10.0	75.3	
cb			9.6	75.7	
¼			8.8	76.5	
+2			9.6	75.7	
℄			9.2	76.1	
¼			8.7	76.6	
cb			9.0	76.3	

85.29

E			9.1	76.2	
+5				77.4	
		N Cb			
-5				76.3	
E			9.5	75.8	
cb			9.4	75.9	
¼			9.3	76.0	
℄			9.7	75.6	
+10			10.0	75.3	
¼			9.7	75.6	
cb			9.9	75.4	
W			10.2	75.1	
		N ¼			
W			10.6	74.7	
cb			10.2	75.1	
¼			10.0	75.3	
+2			10.3	75.0	
℄			10.0	75.3	
¼			9.5	75.8	
cb			9.6	75.7	
E			9.5	75.8	
+5				76.0	
		℄ Emerald			
-5				76.0	
E			9.5	75.8	
cb			9.8	75.5	

Ingraham		85.29					85.29		
¼			9.6	75.7		¼	10.0	75.3	
℄			10.2	75.1		+2	10.3	75.0	
+10			10.5	74.8		cb	10.3	75.0	
¼			10.2	75.1		N	10.7	74.6	
cb			10.0	75.3			St. Emerald		
N			10.2	75.1		N	10.9	74.4	
		S ¼				cb	10.2	75.1	
N			10.5	74.8		+2	10.8	74.5	
cb			10.2	75.1		¼	10.3	75.0	
¼			10.0	75.3		+2	11.3	74.0	
+3			10.8	74.5		℄	10.8	74.5	
℄			10.4	74.9		¼	10.4	74.9	
¼			9.8	75.5		cb	10.7	74.6	
cb			10.0	75.3		E +5	11.0	74.3	75.7
E +5			10.1	75.2 74.4 ✓		TP	249	7653	11.45	73.84
		S cb		75.2				45 S		73.8
-5 E			10.3	75.0		-5 E	3.0		79.5
cb			10.1	75.2		cb	2.7		73.8
¼			10.0	75.3		¼	2.4		74.1
℄			10.6	74.7		S	2.0		74.5
4/10			11.0	74.3		+10	3.8		73.2

Ingraham

		76.53		
¼			2.0	74.5
Cb			2.7	73.8
¼			3.1	73.4
		90.'S		
¼			3.8	72.7
+10			3.0	73.5
Cb			4.0	72.5
¼			3.3	73.2
+2			4.4	72.1
℄			4.0	72.5
¼			3.3	73.2
+2			3.1	73.4
Cb			3.6	72.9
E +5 -2.5			3.7	72.8 73.2
		135'S = ℄ Alley		72.7
E			5.0	71.5
Cb			4.7	71.8
¼			4.2	72.3
℄			5.1	71.4
+7			5.2	71.2
¼			4.9	71.6

		76.53		
Cb			4.5	72.0
¼			4.7	71.8
		180'S		
¼			5.3	71.2
Cb			5.4	71.1
¼			5.5	71.0
+3			5.4	71.1
+5			6.1	70.4
℄			6.0	70.5
¼			5.1	71.4
Cb			5.8	70.7
E +2.5			5.9	70.6 71.0
		225'S		70.1
E			6.9	69.6
Cb			6.6	69.9
+9			6.0	70.5
¼			6.1	70.4
℄			6.6	69.9
+7			6.9	69.6
+9			6.1	70.4
¼			6.1	70.4

Ingraham 76.53

Cb			5.8	70.7	
M			5.6	70.9	
		270'S = ¼ Feldspar			Feldspar 80' M.de 20' Cbs 10' Qts
M			6.2	70.3	
Cb			6.4	70.1	
¼			6.5	70.0	
+4			6.8	69.7	
+6			7.5	69.0	
E			7.5	69.0	
¼			7.0	69.5	
Cb			7.5	69.0	
E			7.6	68.9	
+35				69.4	
		M. Cb			
-35				68.6	
E			8.0	68.5	
Cb			7.8	68.7	
¼			7.2	69.3	
E			7.9	68.6	
+3			8.1	68.4	
+8			7.4	69.1	
¼			7.4	69.1	
Cb			7.4	69.1	

76.53

M	7.5	69.0	
N ¼			
M	8.3	68.2	
Cb	8.4	68.3	
¼	8.1	68.4	
E	8.0	68.5	
¼	7.3	69.2	
Cb	8.0	68.5	
E	8.3	68.2	
+35		68.6	
E Feldspar			
-35		68.4	
E	8.4	68.1	
Cb	8.1	68.4	
¼	7.4	69.1	
E	8.3	68.2	
+5	8.3	68.2	
¼	7.9	68.6	
Cb	8.0	68.5	
M	8.2	68.3	
S ¼			
M	8.0	68.5	
Cb	8.2	68.3	

Ingraham		76.53		
1/4			85	68.0
E			8.7	67.8
1/4			7.8	68.7
+2			7.6	68.9
Cb			8.3	68.2
E			8.7	67.8
+2.5				68.2
		3 Cb		
-2.5				68.4
E			8.8	67.7
Cb			8.5	68.0
1/4			7.9	68.6
E			8.6	67.9
+5			9.0	67.5
+9			8.0	68.5
1/4			7.8	68.7
Cb			7.9	68.6
W			7.9	68.6
		SL. Feldspar		
W			8.2	68.3
Cb			8.3	68.2
1/4			8.5	68.0
+5			8.4	68.1

		76.53		
+7			9.5	67.0
E			9.1	67.4
1/4			8.6	67.9
+4			8.5	68.0
Cb			9.0	67.5
E			9.5	67.0
+2.5				67.8
		45'S		
-2.5				66.5
E			10.5	66.0
Cb			9.9	66.6
1/4			9.5	67.0
E			10.2	66.3
+5			10.5	66.0
+7			9.5	67.0
1/4			9.4	67.1
Cb			9.2	67.3
W			9.2	67.3
TP	2.10	68.34	10.29	66.24
		90'S		
W			2.1	66.2
Cb			2.0	66.3
1/4			2.2	66.1

Ingraham

6834

+5			2.4	65.9	
+7			2.2	65.1	
℄			2.9	65.4	
¼			2.3	66.0	
+4			2.2	66.1	
Cb			2.6	65.7	
E			3.0	65.3	
+25				65.1	
		135' S - ℄ Hillary			
-25				64.7	
E			4.3	64.0	
Cb			3.6	64.7	
+8			3.3	65.0	
¼			3.4	64.9	
℄			4.1	64.2	
+5			4.0	64.3	
+7			3.4	64.9	
¼			3.4	64.9	
Cb			3.0	65.3	
M			3.1	65.2	
		180' S			
M			4.3	64.0	
Cb			4.2	64.1	

6834

¼			4.6	63.7	
+6			4.5	63.8	
+8			4.9	63.4	
℄			4.8	63.5	
¼			4.7	63.6	
+4			4.4	63.9	
Cb			4.6	63.7	
E			4.7	63.6	
+25				63.8	
		225 S			
-25				63.9	
E			5.2	63.1	
Cb			5.3	63.0	
+8			5.1	63.2	
¼			5.4	62.9	
℄			5.6	62.7	
+2			5.4	62.7	
¼			5.6	62.7	
+9			5.8	62.5	
Cb			5.2	63.1	
M			5.5	62.8	
		270' S : N.L. Garnet			Garnet Paved
M			5.1	63.2	

Ingraham

Cb		68.34	5.2	63.1	
+8			5.01	63.33	on Cb Return
Old Gutter			5.7	62.6	
1/4			5.7	62.6	
℄			5.8	62.5	
1/4			5.6	62.7	
Cb			5.5	62.8	
E			5.7	62.6	
+25				63.1	S.W. Spk Garnet + Ingraham
TP	3.49	66.79	5.04	63.30	
		S∠ Garnet			
-25				62.9	
E			4.7	62.1	
Cb			4.5	62.3	
1/4			4.5	62.3	
℄			4.6	62.2	
1/4			4.9	61.9	
+3 Old Gutter			5.0	61.8	
			4.63	62.16	on Cb Return
Cb			4.4	62.4	
W			4.3	62.5	
		45 S			
W			4.8	62.0	

		66.79			
Cb			5.0	61.8	
1/4			5.1	61.7	
℄			5.2	61.6	
1/4			4.7	62.1	
Cb			4.8	62.0	
E			4.8	62.0	
+25				62.8	
		90 S			
-25				63.1	
E			4.8	62.0	
Cb			4.9	61.9	
1/4			4.8	62.0	
℄			5.4	61.4	
1/4			5.2	61.6	
Cb			4.9	61.9	
W			5.0	61.8	
		135 S - ℄ Alley			
W			5.6	61.2	
Cb			5.6	61.2	
1/4			5.5	61.3	
℄			5.4	61.4	
1/4			4.8	62.0	
Cb			4.9	61.9	

Ingraham		6679							
E			4.6	62.2					
+25				63.2					
		180°S							
-25				64.8					
E			3.5	63.3					
Cb			4.2	62.6					
1/4			3.6	63.2					
Z			4.5	62.3					
+10			5.3	61.5					
1/4			5.0	61.8					
Cb			5.5	61.3					
+8			4.5	62.3					
N			4.6	62.2					
		225°S							
N			4.3	62.5					
Cb			3.9	62.9					
1/4			3.8	63.0					
+3			4.3	62.5					
Z			3.6	63.2					
1/4			2.8	64.0					
Cb			3.4	63.4					
+10			2.5	64.3					
E			1.6	65.2					
+25				65.4					

		6679			
		220°S = N L Hornblend		65.2	
-25				65.0	
-7					
E			3.1	63.7	Hornblend 80% Nido 20% Cbs 10% Qtz
+4			3.6	63.2	
Cb			3.6	63.2	
1/4			3.2	63.6	
Z			3.7	63.1	
+8			4.3	62.5	
1/4			4.2	62.6	
Cb			3.6	63.2	
N			2.9	63.9	
TP	119	65.45	2.53	64.26	Nail N of Pole Ingraham + Hornblend
		N Cb			
N			2.5	63.0	
Cb			2.7	62.8	
1/4			3.2	62.3	
Z			2.1	62.9	
1/4			2.0	63.5	
Cb			2.5	63.0	
E			3.8	62.7	
		N 1/4			
E			2.1	62.9	
Cb			2.5	63.0	

Ingraham

+8		63.2	
¼		63.0	63.5
E		62.6	62.9
¼		62.9	62.6
Cb		62.8	62.7
W		62.7	62.8
	E Hornblend		
W		62.9	62.6
Cb		63.1	62.4
¼		63.2	62.3
E		62.7	62.8
¼		62.2	63.3
+5		63.5	63.0
Cb		62.6	62.9
E		62.7	62.8
	S ¼		
E		62.6	62.9
Cb		62.6	62.9
+6		62.6	62.9
¼		62.2	63.3
E		62.8	62.7

65.45

¼		63.0	62.5
Cb		62.9	62.6
W		62.9	62.6
	S Cb		
W		63.2	62.3
Cb		63.1	62.4
¼		63.2	62.3
E		62.8	62.7
+5		62.6	62.9
¼		62.2	63.3
+5		62.6	62.9
Cb		62.8	62.7
E		62.8	62.7
	SE Hornblend		
-25		62.6	62.2
E		62.6	62.9
+5		62.6	62.9
+7		63.0	62.5
Cb		63.0	62.5
+6		63.0	62.5
¼		62.5	63.0
E		62.8	62.7
¼		63.0	62.5

Ingraham		65.45				65.45		
+3			25	63.0			43	61.2
Cb			24	63.1	¼		45	61.0
¼			23	63.2	¼		39	61.6
		45.5			Cb		35	62.0
¼			21	62.9	¼		33	62.2
Cb			29	62.6		135.5		
¼			29	62.6	¼		39	61.6
+2			30	62.5	Cb		42	61.3
+3			35	62.0	¼		46	60.9
¢			34	62.1	+3		52	60.1
¼			32	62.3	¢		53	60.2
+5			37	61.8	¼		51	60.4
Cb			39	61.6	+7		59	59.6
+4			37	61.8	Cb		58	59.7
+7			38	62.7	+4		58	59.7
E			30	62.5	+7		54	60.1
+25				62.0				
		90.5			E		54	59.9
-25				61.2	+25			60.0
E			46	60.9		180.5		59.4
+5			41	61.4	-25			
					E		65	59.0
Cb			50	60.5	+5		65	59.0
+5			48	60.7	+7		70	58.5

Ingraham		65.45				65.45		
Cb			6.9	58.6				
+5			7.1	58.4				
1/4			6.6	58.9				
+5			7.1	58.4				
E			7.3	58.2				
+7			7.2	58.3				
1/4			6.5	59.0				
+7			5.4	60.1				
Cb			5.0	60.5				
N			4.8	60.7				
		225'S						
N			5.6	59.9				
Cb			5.7	59.8				
+8			6.0	59.5				
1/4			8.2	57.3				
E			8.3	57.2				
+7			8.1	57.4				
1/4			7.8	57.7				
+5			8.3	59.2				
Cb			8.1	57.4				
+5			8.5	57.0				
+6					8.0	57.5		
E					8.0	57.5		
+25						58.5		
			265'S			"		
-25						56.5		
E					9.6	55.9		
Cb					9.6	55.9		
+5					9.5	56.0		
1/4					9.0	56.5		
E					9.3	56.2		
1/4					9.2	56.3		
+5					6.7	58.8		
Cb					6.6	58.9		
N					6.0	59.5		
			270'S = N. Grand Ave.				Grand 125'N 20'Cbs 2125'9+s	
N					8.1	57.4		
Cb					8.4	57.1		
1/4					9.1	56.4		
+2					9.4	56.1		
E					9.4	56.1		
1/4					9.1	56.4		
+9					9.7	55.8		
Cb					9.7	55.8		

Ingraham

E		9.5	56.0
+25			56.3
	N Cb		
-25			54.9
E		10.1	55.4
cb		9.9	55.6
¼		9.5	56.0
℄		9.7	55.8
¼		9.7	55.8
cb		9.7	55.8
W		9.8	55.7
	N ¼		
W		9.2	56.3
cb		9.3	56.2
¼		9.6	55.9
℄		9.6	55.9
¼		9.6	55.9
cb		9.6	55.9
E		9.7	55.8
+25			55.2
	℄ Grand Ave		
-25			55.2
E		9.7	55.8
cb		9.4	56.1
¼		9.4	56.1

65.45

℄		9.8	55.7
¼		9.5	56.0
cb		9.3	56.2
W		9.0	56.5
	S ¼		
W		10.0	55.5
cb		10.2	55.3
¼		10.3	55.2
℄		10.4	55.1
¼		10.4	55.1
cb		10.4	55.1
E		10.9	54.6
+25			54.1
	S cb		
-25			53.3
E		11.2	54.3
cb		11.0	54.5
¼		10.9	54.6
℄		10.7	54.8
¼		10.6	54.9
cb		10.1	55.4
W		10.1	55.4
	St. Grand		

Ingraham		65.45				55.45		
W			9.7	55.8	W		0.3	55.2
cb			9.8	55.7		90°S		
+8			10.0	55.5	W		1.2	54.3
+9			10.6	54.9	cb		1.4	54.1
1/4			10.4	55.1	+8		1.8	53.7
E			10.9	54.6	1/4		2.3	53.2
+6			10.8	54.7	E		2.4	53.1
1/4			10.5	55.0	+7		2.4	53.1
+5			10.9	54.6	1/4		1.9	53.6
cb			11.0	54.5	cb		3.0	52.5
E			11.3	54.2	E		3.5	52.0
+25				54.1	+25			52.9
		45°S			135°E			
-25				53.9	-25			51.7
E			12.0	53.5	E		4.7	50.8
TP	0.91	55.45	10.91	54.54	cb		3.9	51.6
+5			2.2	53.3	1/4		3.0	52.5
cb			1.8	53.7	E		3.3	52.2
1/4			1.2	54.3	1/4		2.9	52.6
E			1.3	54.2	+5		3.0	52.5
1/4			1.3	54.2	+6		2.5	53.0
+3			1.1	54.4	cb		2.2	53.3
+8			0.4	55.1	W		2.1	53.4

Rain

152°S

Top Cam Stop 5" High 0.88

Ingraham

55.45

180° S

W			3.3	52.2	
Cb			3.6	51.9	
+6			3.8	51.7	
+7			4.3	51.2	
1/4			4.0	51.5	
℄			4.1	51.4	
1/4			4.0	51.5	
Cb			4.9	50.6	
E +25			5.5	50.0	
				50.7	
		275° S			
-25 E			6.5	49.8 49.0	
Cb			5.5	50.0	
1/4			4.8	50.7	
℄			5.0	50.5	
1/4			5.1	50.4	
+5			5.1	50.4	755 S Code Drive
+6			4.6	50.9	4.65
Cb			4.3	51.2	
W			4.0	51.5	
		270° S: NL Thomas			

55.45

TP	0.82	51.30	4.97	50.48	
W			1.1	50.2	Thomas 80' Wide 20' Obs 10' Qtz
Cb			1.2	50.1	
1/4			1.6	49.7	
℄			1.6	49.7	
1/4			1.3	50.0	
Cb			2.0	49.3	
E +25			2.6	48.7 48.8	
		N Cb			
-25 E			2.7	49.0 48.6	
Cb			2.3	49.0	
1/4			1.5	49.8	
℄			1.7	49.6	
1/4			2.0	49.3	
Cb			1.8	49.5	
W			1.6	49.7	
		N 1/4			
W			1.6	49.7	
Cb			2.1	49.2	
1/4			2.3	49.0	
℄			1.8	49.5	

Ingraham

		51.30			
1/4			1.6	49.7	
Cb			2.3	49.0	
E +25			2.6	48.7	
				48.9	
		E Thomas			
-25 E			3.0	48.7 48.3	
Cb			2.6	48.7	
1/4			1.6	49.7	
℄			2.0	49.3	
1/4			2.4	48.9	
Cb			1.7	49.6	
W			1.7	49.6	
BM			2.88	48.42	on W7 Ingraham E Thomas Mon
		S 1/4			
W			1.7	49.6	
+5			2.4	48.9	
Cb			2.5	48.8	
1/4			2.7	48.6	
℄			2.1	49.2	
1/4			1.7	49.6	
Cb			2.7	48.6	
E +25			3.3	48.0	
				48.5	

		51.30			
		S Cb			
-25 E			3.6	48.6 47.7	
Cb			2.9	48.4	
1/4			1.8	49.5	
℄			2.2	49.1	
1/4			2.9	48.4	
+10			2.8	48.5	
Cb			2.1	49.2	
W			2.0	49.3	
		S E Thomas			
W			1.2	50.1	
+3			2.3	49.0	
Cb			2.4	48.9	
+7			2.6	48.7	
+9			3.2	48.1	
1/4			3.3	48.0	
℄			2.5	48.8	
1/4			2.2	49.1	
Cb			3.2	48.1	
E +35		45'5	4.0	47.3 48.3	

Ingraham

-25	5130		47.6	
E		4.7	46.6	
cb		4.0	47.3	
1/4		3.2	48.1	
℄		3.2	48.1	
+3		3.2	48.1	
1/4		4.0	47.3	
+2		4.0	47.3	
+8		3.2	48.1	
cb		3.1	48.2	
W		2.6	48.7	
	90' S			
W		3.5	47.8	
cb		3.8	47.5	
+8		4.0	47.3	
+10		4.4	46.9	
1/4		4.5	46.8	
+10		3.9	47.4	
℄		3.8	47.5	
1/4		3.9	47.4	
cb		4.6	46.7	
E		5.4	45.9	
+25			47.2	

		5130		
		135 S ℄ Alley		
-25			46.4	
E		5.8	45.5	
cb		5.3	46.0	
+8		4.5	46.8	
1/4		4.5	46.8	
℄		4.6	46.7	
1/4		5.3	46.0	
+4		5.2	46.1	
+6		4.4	46.9	
cb		4.4	46.9	
W		4.2	47.1	
		180 S		
W		4.9	46.4	
cb		5.2	46.1	
+8		5.5	45.8	
+11		6.0	45.5	
1/4		5.8	45.7	
℄		5.5	45.0	
1/4		5.3	46.2	
cb		6.1	45.2	
E		6.5	44.8	
+50			45.8	

Ingraham 5/30

		225 s		45.4	
-25 E			6.8	44.5	
Cb			6.2	45.1	
1/4			5.8	45.5	
₵			5.8	45.5	
1/4			6.6	44.7	
+4			6.6	44.7	
+6			6.1	45.2	
Cb			6.0	45.3	
W			5.6	45.7	
		270's	: NL Reed		Reed 80' wide 20' Cbs 10' Qts
W			6.0	45.3	
Cb			6.4	44.9	
+7			6.5	44.8	
+10			7.0	44.5	
1/4			7.1	44.2	
₵			6.3	45.0	
1/4			6.1	45.2	
Cb			6.2	45.1	
E			6.9	44.4	
+25		N Cb		44.0	

5/30

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-25 E			7.0	44.4 44.3	
+10			6.3	45.0	
Cb			6.2	45.1	
1/4			5.9	45.4	
₵			6.3	45.0	
+5			6.8	44.5	
1/4			6.9	44.4	
Cb			6.9	44.4	
W			6.6	44.7	
		N 1/4			
W			6.7	44.7	
Cb			7.0	44.3	
1/4			6.8	44.5	
+6			6.8	44.5	
₵			6.2	45.1	
1/4			5.9	45.4	
Cb			6.2	45.1	
E			6.8	44.5	
+25				44.0	
		₵	Reed		
-25 E			6.5	44.1 44.8	
Cb			6.2	45.1	

Ingraham		5130		
1/4			6.0	45.3
¢			6.3	45.0
+5			6.8	44.5
1/4			6.8	44.5
Cb			7.0	44.3
W			6.7	44.6
		s 1/4		
W			7.0	44.3
Cb			7.2	44.1
1/4			7.0	44.3
¢			6.5	44.8
1/4			6.2	45.1
Cb			6.4	44.9
E +2.5			6.8	44.5 44.0
		s Cb		
−2.5 E			6.5	44.6 44.8
Cb			6.1	45.2
1/4			5.8	45.5
¢			6.1	45.2
+5			6.7	44.6
1/4			7.0	44.3

		5130		
Cb			7.1	44.2
W			6.8	44.5
		SL Hood		
W			6.2	45.1
Cb			6.5	44.8
+7			6.8	44.5
1/4			7.3	44.0
¢			6.5	44.8
1/4			6.1	45.2
Cb			6.4	44.9
E +2.5			6.6	44.7 44.3
		45.5		
−2.5 E			6.4	44.5 44.9
Cb			5.9	45.4
1/4			5.6	45.7
¢			5.8	45.5
+5			6.7	45.6
1/4			7.0	44.3
+2			7.0	44.3
+6			6.1	45.2
Cb			6.1	45.2

Ingraham

		51.30			
W			5.8	45.5	
		90's			
W			5.0	46.3	
Cb			5.6	45.7	
+7			5.6	45.7	
1/4			6.5	44.8	
E			5.4	45.9	
1/4			5.0	46.3	
Cb			5.2	46.1	
E			5.7	45.6	
+25				45.4	
		135's			
-25				46.0	
E			5.0	46.3	
Cb			4.7	46.6	
1/4			4.5	45.8	
E			4.7	45.6	
1/4			5.4	45.9	
+3			5.7	45.6	
+7			5.0	46.0	
Cb			4.7	46.6	
W			4.3	47.0	
TP	4.54	52.31	8.53	47.77	

		52.31			
		180's			
W			4.9	47.4	
Cb			5.2	47.1	
+7			5.2	47.1	
+10			5.9	46.4	
1/4			5.7	46.6	
E			4.8	47.5	
1/4			4.8	47.8	
Cb			5.0	47.3	
E			5.4	46.9	
+25				47.5	
		225's			
-25				48.1	
E			4.8	47.5	
Cb			4.2	48.1	
1/4			4.2	48.1	
E			4.4	47.9	
1/4			5.3	47.0	
+3			5.4	46.9	
+7			4.6	47.7	
Cb			4.5	47.8	
W			4.1	48.2	
		270's = NL Oliver			

Ingraham 52.31

W	2.8	49.5	Oliver 80' wide 20' Cbs 10' Gts
+3	3.9	48.4	
Cb	4.0	48.3	
+5	4.2	48.1	
+10	5.0	47.3	
1/4	4.8	47.5	
℄	4.0	48.3	
1/4	3.8	48.5	
Cb	4.0	48.3	
E	4.5	47.8	
+25		48.6	
N Cb			
-25		48.6	
E	4.6	47.7	
Cb	4.1	48.2	
1/4	3.9	48.4	
℄	4.2	48.1	
1/4	4.8	47.5	
+3	4.9	47.4	
+7	4.2	48.1	
Cb	4.0	48.3	
+9	3.7	48.6	
W	2.9	49.4	

N 1/4

52.31

W	2.1	50.2	
+4	3.5	48.8	
Cb	4.1	48.2	
+7	4.2	48.1	
1/4	4.9	47.4	
℄	4.2	48.1	
1/4	4.0	48.3	
Cb	4.2	48.1	
E	4.4	47.9	
+25		48.7	
℄ Oliver			
-25		48.7	
E	4.5	47.8	
Cb	4.2	48.1	
1/4	4.1	48.2	
℄	4.2	48.1	
1/4	4.9	47.4	
+7	4.2	48.1	
Cb	3.9	48.4	
+9	3.4	48.9	
W	2.1	50.2	Mon W'L Ingraham
BM	4.85	47.46	& Oliver

S 1/4

Ingraham		5231	5 1/4		
W			2.5	49.8	
+3			3.7	48.6	
Cb			4.0	48.3	
+7			4.2	48.1	
1/4			4.9	47.4	
℄			4.1	48.2	
1/4			4.0	48.3	
Cb			4.2	48.1	
E			4.5	47.8	
+2.5				48.5	
		S Cb			
-2.5				48.3	
E			4.5	47.8	
Cb			4.2	48.1	
1/4			4.0	48.3	
℄			4.0	48.3	
1/4			5.0	47.3	
+7			4.3	48.0	
Cb			4.0	48.3	
+9			3.8	48.5	
W			2.7	49.6	
		S.L. Oliver			
W			2.3	50.0	

		5231			
+3			3.7	48.6	
Cb			4.1	48.2	
+7			4.2	48.1	
1/4			4.8	47.5	
℄			4.0	48.3	
1/4			4.1	48.2	
Cb			4.2	48.1	
E			4.5	47.8	
+2.5				48.6	
		45.5			
-2.5				48.7	
E			4.8	47.5	
Cb			4.4	47.9	
1/4			4.4	47.9	
℄			4.1	48.2	
1/4			4.8	47.5	
+2			5.0	47.3	
+7			4.3	48.0	
Cb			4.2	48.1	
+9			3.7	48.6	
W			2.8	49.5	
		90.5			
W			2.9	49.4	

Ingraham

5231

+3			44	47.9
Cb			46	47.7
+7			47	47.6
+10			53	47.0
1/4			51	47.2
E			44	47.9
1/4			44	47.9
Cb			45	47.8
E			47	47.6
+25				48.0
		125's		
-25				47.4
E			49	47.4
Cb			47	47.6
1/4			46	47.7
E			48	47.5
1/4			54	46.9
+7			49	47.4
Cb			48	47.5
+9			45	47.8
W			36	48.7
		170's		
W			40	48.3

5231

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+3	48	47.5	
Cb	48	47.5	
+6	48	47.5	
+10	55	46.8	
1/4	54	46.9	
E	48	47.5	
1/4	47	47.6	
Cb	51	47.2	
E	56	46.7	
+25		47.1	
	215's		
-25		46.5	
E	61	46.2	
Cb	55	46.8	
1/4	51	47.2	
E	51	47.2	
1/4	57	46.6	
+5	57	46.6	
+8	52	47.1	
Cb	50	47.3	
M	47	47.6	
	250's NL Pacific		
W	57	46.6	

4-9-26

Ingraham		52.31			
Cb			5.9	46.4	Pacific 149' wide 20' Cbs 27.25 gts
1/4			6.2	46.1	
℄			5.6	46.7	
1/4			5.2	47.1	
Cb			5.7	46.6	
E			6.3	46.0	
+25				46.1	
B.M.	3.61	49.12	6.80	45.51	Mon N 1/2 Ingraham N.L. Pacific
		N Cb			
-25				46.4	
E			3.4	45.7	
Cb			3.0	46.1	
1/4			2.1	47.0	
℄			2.4	46.7	
1/4			2.9	46.2	
+5			3.3	45.8	
Cb			2.8	46.3	
W			2.8	46.3	
		N 1/4			
W			3.1	46.0	
Cb			3.0	46.1	
+8			3.6	45.5	
1/4			3.3	45.8	

		49.12			
℄			2.7	46.4	
1/4			2.3	46.8	
Cb			3.0	46.1	
E			3.6	45.5	
+25				45.8	
		℄ Pacific			
-25				45.9	
E			3.4	45.7	
Cb			3.3	45.8	
1/4			2.7	46.4	
℄			3.1	46.0	
1/4			3.5	45.6	
+5			3.6	45.5	
Cb			3.1	46.0	
W			3.2	45.9	
		S 1/4			
W			3.5	45.6	
Cb			3.3	45.8	
+8			3.8	45.3	
1/4			3.6	45.5	
℄			3.2	45.9	
1/4			2.8	46.3	
Cb			3.5	45.6	

Ingraham		49.12					49.12		
E			3.5	45.6			50's		
-2.5				45.8					
		SCb				E		3.3	45.8
-2.5				45.6		Cb		3.4	45.7
E			3.7	45.4		-1/4		4.0	45.1
Cb			2.5	45.6		Z		3.7	45.4
1/4			3.3	45.8		1/4		3.9	45.2
Z			3.3	45.8		+5		4.2	44.9
1/4			4.0	45.1		+10		3.4	45.7
+5			4.3	44.8		Cb		3.3	45.8
Cb			3.7	45.4		W		3.1	46.0
W			3.5	45.6		100's			
		SL Pacific				W		3.4	45.7
W			3.6	45.5		Cb		3.5	45.6
Cb			3.4	45.7		+8		4.6	44.5
+3			3.4	45.7		1/4		4.3	44.8
+8			4.2	44.9		Z		4.2	44.9
1/4			4.0	45.1		1/4		4.3	44.8
Z			3.4	45.7		Cb		3.5	45.6
1/4			3.7	45.4		E		3.3	45.8
+5			3.7	45.4		150's			
Cb			3.4	45.9		E		3.5	45.6
E			3.2	45.9		Cb		3.6	45.5
+25				46.1					

Ingraham

		49.12		
+8			4.2	44.9
¼			4.1	45.0
Z			4.0	45.1
¼			4.3	44.8
+5			4.4	44.7
cb			3.7	45.4
M			3.6	45.5
		200'S		
M			3.6	45.5
cb			3.8	45.3
+3			3.8	45.3
+8			4.5	44.6
¼			4.2	44.9
Z			4.0	45.1
¼			4.2	44.9
+5			4.3	44.8
cb			3.8	45.3
E			3.4	45.5
		250'S		
E			3.8	45.3
cb			3.8	45.3

		49.12		
+8			4.4	44.7
¼			4.2	44.9
Z			4.1	45.0
¼			4.2	44.9
+7			4.4	44.7
cb			3.8	45.3
M			3.7	45.4
		300'S		
M			3.5	45.6
cb			3.7	45.4
+3			3.6	45.5
+8			4.4	44.7
¼			4.1	45.0
Z			4.0	45.1
¼			4.1	45.0
+5			4.2	44.9
cb			3.7	45.4
E			3.4	45.7
		350'S		
E			3.3	45.8
+5			3.9	45.2

Ingraham

Cb		3.9	45.2
+8		4.4	44.7
1/4		4.1	45.0
E		4.0	45.1
1/4		4.3	44.8
+5		4.5	44.6
+9		3.7	45.4
Cb		3.5	45.6
W		3.0	46.1
	400's		
W		3.1	46.0
+3		3.5	45.6
Cb		3.6	45.5
+8		4.4	44.7
1/4		4.6	44.5
E		4.3	44.8
1/4		4.5	44.6
+5		4.4	44.7
Cb		3.7	45.4
+7		3.7	45.4
E		2.4	46.7

49.12

		450's	
E		2.8	46.3
+7		3.7	45.4
Cb		4.0	45.1
+5		4.5	44.6
1/4		4.4	44.7
E		4.2	44.9
1/4		4.5	44.6
+7		4.7	44.4
+10		4.0	45.1
Cb		3.8	45.3
W		3.6	45.5
	500's		
W		3.3	45.8
+2		4.0	45.1
Cb		3.8	45.3
+3		4.0	45.1
+8		4.6	44.5
1/4		4.6	44.5
E		4.4	44.7
1/4		4.6	44.5

Ingraham		49.12			
+5			4.5	44.6	
Cb			4.1	45.0	
E			3.8	45.3	
BM	2.23	45.90	5.45	43.67	E Mon Sunset + Ingraham
		550'S - N L Sunset			
E			0.4	45.5	Sunset 75' wide 12' Cbs 12.75 Gts
Cb			0.9	45.0	
+5			1.3	44.6	
1/4			1.6	44.3	
℄			1.2	44.7	
1/4			1.5	44.4	
+6			1.5	44.4	
+7			1.0	44.9	
Cb			0.9	45.0	
+10			0.5	45.4	
W			0.0	45.9	
		N Cb			
W			0.0	45.9	
+2			0.9	45.0	
Cb			1.0	44.9	
+6			1.7	44.2	

		45.90			
1/4			1.5	44.4	
℄			1.2	44.7	
1/4			1.5	44.4	
+7			1.6	44.3	
Cb			1.0	44.9	
E			0.9	45.0	
		N 1/4			
E			1.5	44.4	
Cb			1.6	44.3	
1/4			1.5	44.4	
℄			1.2	44.7	
1/4			1.6	44.3	
Cb			1.5	44.4	
+8			1.0	44.9	
W			0.0	45.9	
		℄ Sunset			
W			0.2	45.7	
Cb			1.3	44.6	
+4			1.5	44.4	
1/4			1.5	44.4	
℄			1.4	44.5	
1/4			1.3	44.6	

Ingraham

45.90

Cb			1.5	44.4
E			1.5	44.4
		5 1/4		
E			2.2	43.7
Cb			2.0	43.9
1/4			1.8	44.1
E			1.4	44.5
1/4			1.5	44.4
Cb			1.8	44.1
+8			1.5	44.4
W			0.0	45.9
		5 Cb		
W			0.0	45.9
+5			1.3	44.6
Cb			1.6	44.3
+8			2.1	43.8
1/4			18	44.1
E			1.5	44.4
1/4			2.0	43.9
+9			2.0	43.9
Cb			1.4	44.5

45.90

E		1.3	44.6
	SL Sunset		
E		1.3	44.6
Cb		1.3	44.6
+3		1.5	44.4
+8		2.2	43.7
1/4		2.1	43.8
E		1.6	44.3
1/4		2.1	43.8
+5		2.2	43.7
+10		1.3	44.6
Cb		1.3	44.6
+8		0.7	45.2
W		0.0	45.9
	50's		
W		0.7	45.2
+2		1.8	44.1
Cb		2.1	43.8
+3		2.1	43.8
+7		2.9	43.0
1/4		2.8	43.1

Ingraham

45.90

+6			2.6	43.3
8			2.0	43.9
1/4			2.5	43.4
+5			2.7	43.2
cb			2.1	43.8
E			2.0	43.9
		100's		
E			2.7	43.2
cb			3.0	42.9
+8			3.7	42.2
1/4			3.5	42.4
8			3.1	42.8
1/4			3.5	42.4
+9			3.1	42.8
cb			2.8	43.1
+9			2.6	43.3
W			1.1	44.8
		150's		
W			2.3	43.7
+3			3.5	42.4
cb			3.6	42.3

45.90

+3			3.6	42.3
+7			4.1	41.8
1/4			4.4	41.5
8			3.8	42.1
1/4			4.2	41.9
+4			4.4	41.5
+8			3.7	42.2
cb			3.8	42.1
E			3.4	42.5
		200's		
E			3.8	42.1
cb			4.4	41.5
+4			4.3	41.6
+9			5.1	40.8
1/4			4.2	41.2
8			4.3	41.6
1/4			4.8	41.1
+6			4.9	41.0
+10			4.1	41.8
cb			4.1	41.8
+9			4.0	41.9

Ingraham

	45.90		
W		2.9	43.0
	250'S		
W		3.1	42.3
+5		5.1	40.8
Cb		5.2	40.7
+3		5.0	40.9
+8		5.9	40.2
1/4		5.6	40.3
E		4.8	41.1
+6		5.4	40.5
1/4		5.3	40.6
+6		5.8	40.1
+7		5.2	40.7
Cb		5.0	40.9
E		4.9	41.0
	300'S		
E		5.0	40.9
+4		5.8	40.1
Cb		5.8	40.8
+4		5.6	40.3
+8		6.5	39.4
1/4		6.2	39.7

	45.90		
+4		6.1	39.8
E		5.4	40.5
+8		6.1	39.8
1/4		6.2	39.7
+5		6.3	39.6
+9		5.8	40.1
Cb		5.6	40.3
+8		5.5	40.4
W		4.3	41.6
	350'S		
W		4.7	41.2
+4		6.2	39.7
Cb		6.4	39.5
+4		6.4	39.5
+8		7.2	38.7
1/4		7.0	38.9
E		6.3	39.6
1/4		6.6	39.3
+5		7.0	38.9
+6		6.5	39.4
Cb		6.5	39.4

Ingraham

		45.90		
+7			6.3	39.6
E			5.4	40.5
		400'S		
E			6.2	39.7
+4			6.9	39.0
Cb			7.0	38.9
+5			7.0	38.9
+8			7.7	38.2
1/4			7.4	38.5
E			6.8	39.1
1/4			7.5	38.4
+6			7.7	38.2
+9			7.2	38.7
Cb			7.1	38.8
+9			6.9	39.0
W			5.5	40.4
		450'S		
W			6.4	39.5
+3			7.5	38.4
Cb			7.8	38.1
+4			8.0	37.0

		45.90		
+8			8.5	37.4
1/4			8.4	37.5
E			7.7	38.2
1/4			8.1	37.8
+5			8.4	37.5
+8			7.6	38.3
Cb			7.7	38.2
+8			7.9	38.0
E			6.9	39.0
		500'S		
E			7.4	38.5
+4			8.3	37.6
Cb			8.4	37.5
+4			8.4	37.5
+8			9.1	36.8
1/4			9.0	36.9
E			8.5	37.4
1/4			9.0	36.9
+6			9.1	36.8
+9			8.6	37.3
Cb			8.3	37.6
+9			8.1	37.8

Ingraham

4590

W	9.0	38.7	
	550's		
W	7.8	38.1	
+3	9.1	36.8	
Cb	9.2	36.7	
+4	9.2	36.7	
+8	10.0	35.9	
1/4	9.7	36.2	
E	9.0	36.9	
1/4	9.5	36.4	
+6	9.8	36.1	
+8	9.1	36.8	
Cb	9.1	36.8	
+8	8.9	37.0	
E	8.1	37.8	
	600's = N.L. Roosevelt		
E	9.1	36.8	Roosevelt 95' wide 12 Cbs 12.75 qls
+4	9.4	36.5	
Cb	9.6	36.3	
+3	9.7	36.2	
+7	10.2	35.6	

4590

1/4	10.0	35.9
E	9.7	36.2
1/4	10.2	35.7
+6	10.6	35.3
+8	9.9	36.0
Cb	9.7	36.2
+9	9.6	36.3
W	8.3	37.6
	N Cb	
W	8.5	37.4
+3	9.7	36.2
Cb	9.9	36.0
+8	10.2	35.7
1/4	10.2	35.7
E	9.9	36.0
1/4	10.0	35.9
+6	10.3	35.6
Cb	10.0	35.9
E	9.4	36.5
	N 1/4	
E	9.6	36.3

Ingraham		45.90			
Cb			10.2	35,7	
¼			10.1	35,8	
℄			9.9	36.0	
¼			10.1	35.8	
Cb			10.1	35,8	
+9			9.8	36,1	
W			8.9	37,0	
BM	3.38	38.18	11.10	34.80	℄ Mon Roosevelt & Ingraham
		℄ Roosevelt			
W			1.8	36,4	
+4			2.2	36.0	
Cb			2.5	35,7	
¼			2.6	35.6	
℄			2.4	35,8	
¼			2.7	35,5	
Cb			2.6	35.6	
E			2.3	35.9	
		S ¼			
E			2.9	35,3	
Cb			3.3	34,9	
¼			3.0	35,2	

		38.18			
℄			2.6	35,6	
¼			2.9	35,3	
Cb			3.0	35,2	
+8			2.6	35,6	
W			1.7	36,5	
		S Cb			
W			1.9	36,3	
+4			2.9	35,3	
Cb			3.0	35,2	
¼			3.0	35,2	
℄			2.6	35,6	
¼			3.3	34,9	
+5			3.5	34,7	
+8			3.0	35,2	
Cb			3.1	35,1	
E			2.9	35,3	
		SL Roosevelt			
E			2.8	35,4	
Cb			3.2	35,0	
+6			3.2	35,0	
+8			3.8	34,4	

Ingraham

75' Wide From H.L. 38.18

				75' Wide 12' Cbs 12.25' Qts
1/4			2.7	35.5
Z			2.3	35.9
1/4			3.2	35.0
+6			3.5	34.7
+9			2.7	35.5
Cb			2.9	35.3
+9			2.6	35.6
W			2.2	36.0
		50' S		
W			3.3	34.9
Cb			3.6	34.6
+3			3.6	34.6
+8			4.5	33.7
1/4			4.3	33.9
Z			3.4	34.8
1/4			4.3	33.9
+5			4.5	33.7
+8			3.8	34.4
Cb			3.7	34.5
E			3.6	34.6

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Table IX.—Calculation of Earthwork.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w =16.2 and h =5.3, cu. yds. =1.48+.028+.089 =1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =h, and ½ the roadbed =w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56 8	56 9	57.1	57.2	57.4	32
33	57.5	57 7	57.8	58 0	58.1	58 3	58.4	58 6	58 7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.