1151

DIETZGEN

ENGINEER'S

LEVEL BOOK

No. 340

EUGENE DIETZGEN CO.

Distances from Center of Roadway for Cross-Sectioning

Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be 30.6+(20—16)÷2 or 2 ft. added to 30.6 =32.6. For slopes of 1 on 1½ see inside of back cover.

Park Row

Culvert

157.70

				℄	152.00
00 = S. el Park Row					152.40
Δ 0+35.08			7.3		150.40
TT	3.87	154.27	7.30		150.40
0+82.28			4.04		150.23
1+29.49			5.11		149.16
1+76.10			5.35		148.92
W. line Ivanhoe					
2+23.91			5.41		148.86
℄ Rd. line Ivanhoe			℄ 5.29		148.98
2+37.76			gutter 5.94		148.33
2+46.20			℄ 5.87		
14' W of N el Ivanhoe			gutter 6.52		147.75

Park Row Grades

	N. line	N. el	S. el	S. line
00				
W. line Torrey Pradeons			152.87	153.12
+24' W = 00				
W. line Torrey of N	154.29	154.04		52.188
+50'	54.14			52.52
1+00	53.42			52.16
1+22.8	153.50	153.25	152.15	152.40
28				
1+50	53.86			52.90
2+00	54.51			54.50
End of on N				
2+18	154.75	154.50		
end of on S				
2+24			155.00	155.25

157.7

℄ Grades B

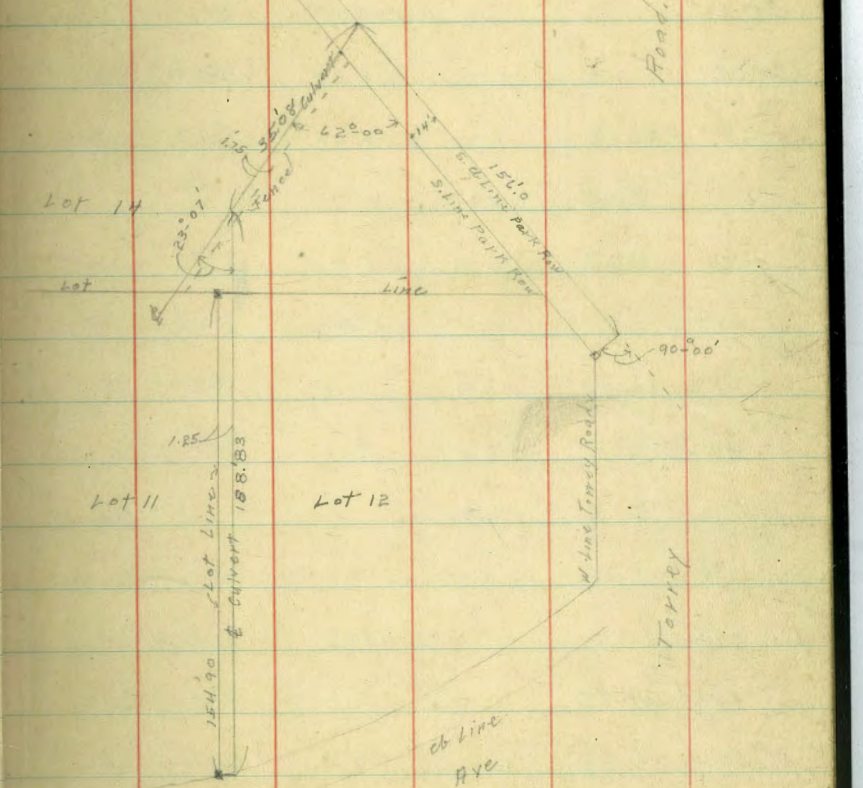
3/12/26

50

N	54.14	53.82	53.50	53.86	54.51
	3.6	3.9	4.2	3.8	3.2
	4.1	4.1	3.9	3.8	3.4
	-0.5	-0.2	+0.3	00	-0.2

40

S	52.88	52.32	52.16	52.00	52.90	54.50
	4.8	5.2	5.5	5.7	4.8	3.2
	5.5	5.9	6.6	6.0	5.7	3.8
	-0.7	-0.7	-1.1	-0.3	-0.9	-0.6
	-0.8	-0.9	-1.4	-0.7	-1.2	-0.8



cb Elevations Coast Blvd 3/18/26

		Blk			
BM	0.19	29.26		29.07	S.E.C. Blvd & La Jolla Pkwy
00± Sec of 00					
Book 1149-25			9.60	19.66	Book 114 1967 Page 25
750N on cb			9.40	19.8	
110'N " "			9.25	20.0	
150'N " "			9.05	20.2	
200'N " "			8.85	20.4	
250'N			8.65	20.6	
289'N P.C.			8.48	20.8	
		300'N			
cb			8.44	20.8	
gutter			9.2	20.1	
15'W			9.5	19.8	
30'W			9.1	20.2	
		350'N			
cb			8.22	21.1	
gutter			9.3	20.0	
15'W			9.2	20.1	
30'W			9.0	20.3	

Plotted JB 3/19/26

Road way O.K.

		29.26		
		400'N		
cb			7.98	21.28
gutter			9.1	20.2
15'W			8.9	20.4
30'W			8.4	20.7
T.P.	11.43	32.71	7.98	21.28
		450'N		
cb			10.60	22.11
gutter			11.6	21.1
15'W			11.8	20.9
30'W			11.8	20.9
		500'N		
cb			9.61	23.10
gutter			10.8	21.9
15'W			10.9	21.8
30'W			10.6	22.1
		550'N		
cb			8.75	23.96
gutter			10.0	22.7
15'W			9.7	23.0
30'W			9.4	23.1

1½

32.71

600' N on el

el	7.71	25.0	
gutter	8.6	24.1	
15' W	8.6	24.1	
30' W	7.9	24.8	

650' N

el	6.66	26.05	
gutter	7.2	25.5	
15' W	7.3	25.4	
30' W	6.8	25.9	

662' N - catch Basin
10" cmt pipe W. cmt 35' W. of el

el	6.25	26.46	
grating	7.3	25.41	To be raised .4 feet in

700' N

el	4.44	28.05	
gutter	5.5	27.2	
15' W	5.7	27.0	
30' W	5.4	27.3	

32.71

750' N

el	2.47	30.24
gutter	3.5	29.2
15' W	3.5	29.2
30' W	3.4	29.3

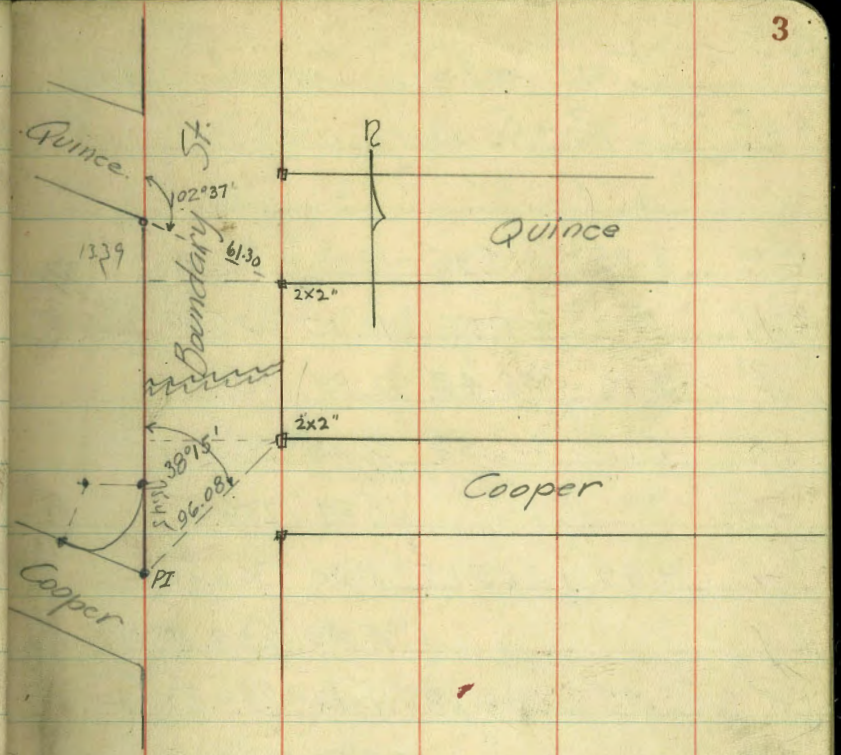
768' N R.C.E. in C.B.S.

el.	1.72	30.99
gutter	2.5	30.2
15' W	2.5	30.2
30' W	2.3	30.4

P.R.E. in C.B.S.

el	0.17	32.54

Ties at Boundary Street between Carmel Hgths Extension and City Heights.



BM. - Redwood & Felton - N.W. Brass Plug 313.01
BM - Redwood & 33rd N.W. " " 311.61

Cross Sections - Carmel Heights Extension

Pacific Bldg. Co.

Tom J. Allen. April 9, 1926.

	+		−	Elev.	
BM.	2.95	315.96		313.01	
BM	0.00	305.86	10.10	305.86	
TP	9.16	302.43	12.59	293.27	
BM.	7.11	302.56	6.98	295.45	
BM			5.91	296.65	
BM.	4.49	305.15	1.90	300.66	✓
BM.			5.89	299.26	
TP	3.05	296.78	11.42	293.73	
BM.			3.82	29296	✓
BM	11.25	300.74	7.29	289.49	✓
BM	9.44	310.15	0.03	300.71	✓
BM.			1.79	308.36	✓
TP	8.46	315.29	3.32	306.83	
BM.			2.35	312.94	

Redwood & Felton - Br. Plug. N.W. Cor.

Pipe N.W. Lot 4 - Bk A.

Pipe N.E. Lot 1 Bk C ✓

" NE Lot 1 - Bk D.

Lot Stake - Lot 1 - Bk E

Pipe NE. Lot 1 - Bk F

Lot Stake S.E Lot 18 - Bk E.

Pipe S.W. Lot 12 - Bk E

Pipe S.E. Lot 39 - Bk F.

" SW Lot 30 - Bk F

Top Fire Hyd NE. Palm & Felton

E Curb. Felton

Redwood & Felton - Br. Plug. N.W. Cor.

Boundary St.

	+			
BM.	6.72	305.98	299.26	
Sect. A S.E. Cor. Lot 1, Bk. F			(PI)	
		306.0		
W. P.		7.25	298.73	✓
W. Curb		7.0	299.0	✓
¼		6.85	299.13	
℄		6.45	299.53	✓
¼		6.50	299.5	✓
E. Curb		6.20	299.8	✓
E P		5.90	300.1	✓
	45' north			
W P.		6.9	299.1	✓
Curb		6.50	299.5	✓
¼		6.50	299.5	✓
℄		5.95	300.03	✓
¼		5.7	300.3	✓
E. Curb		5.4	300.6	✓
E. P.		5.0	301.0	✓

NE. Cor Lot 1, Bk F

305.98
306.0

W P.	6.70	299.3	✓
W. Curb	6.25	299.73	✓
¼	6.20	299.8	✓
℄	5.70	300.3	✓
¼	5.50	300.5	✓
E. Curb	5.0	301.0	✓
E P.	4.60	301.4	✓

SW. Cor Lot xx, Bk E. (PI)

W. P.	4.60	301.4	✓
Curb	4.70	301.3	✓
¼	4.90	301.1	✓
℄	5.25	300.73	✓
¼	5.9	300.1	✓
Curb	5.95	300.05	✓
E. P.	6.30	299.7	✓

E. C. Lot xx, Bk E.

W P.	6.00	300.0	✓
Curb	5.80	300.2	✓
¼	5.40	300.6	✓

	305.98		
	306.00		
℄	5.20	300.8	✓
¼	5.00	301.0	✓
Curb	4.80	301.2	✓
E. R.	4.50	301.5	✓
N.E. Cor Lot 22, Bk E			
W. R.	6.00	300.0	✓
Curb	5.70	300.3	✓
¼	5.50	300.5	✓
℄	5.20	300.8	✓
¼	5.20	300.8	✓
Curb	5.00	301.0	✓
E. R.	4.85	301.13	✓
10'	4.85	301.0	
50' north			✓
W. R.	5.85	300.13	
Curb	5.60	300.4	✓
¼	5.80	300.2	✓
℄	5.50	300.5	✓
¼	5.30	300.7	✓
Curb	5.20	300.8	✓
E. R.	5.25	300.75	✓
E+10'	5.25	300.7	

	305.98		
	306.00		
N.E. cor. Lot 1, Bk. E			
W. R.	5.75	300.13	✓
Curb	5.55	300.43	✓
¼	6.20	299.8	✓
℄	5.70	300.3	✓
¼	5.80	300.2	✓
Curb	5.85	300.13	✓
E. R.	6.00	300.00	✓
E+10	5.80	300.2	
S.E. cor. Lot 24, Bk. D (PI)			
W R.	6.40	299.6	✓
Curb	6.20	299.8	✓
¼	6.25	299.73	✓
℄	6.20	299.8	✓
¼	6.50	299.5	✓
C.	6.65	299.33	✓
E. R.	6.90	299.1	✓
E+10	7.20	298.8	
N.E. Cor Lot 24, Bk. D.			
W R.	8.05	297.93	✓
Curb	8.40	297.6	✓

	+	305.98	305.98 306.20 –		
¼			9.30	✓96 7.	✓
℄			9.25	✓96 73	✓
¼			9.80	✓96 ✓	✓
Curb.			10.65	✓95 33	✓
E. PL. E+10 H			11.40	✓94 6	✓
			1200	✓94 0	
	5.30	300.81	10.47	295.51	
	50' north.		300.8		
W. R.			3.60	✓97 ✓	✓
C.			4.00	✓96 8	✓
¼			5.10	✓95 7	✓
℄			5.20	✓95 6	✓
¼			6.10	✓94 7	✓
C.			7.30	✓93 5	✓
E R. E+10			8.20	✓91 6	✓
	N.E. Lot 1, Bk D		9.20	✓91 6	
W. PL.			4.16	296.65	
Curb.			5.0	✓95 8	✓
¼			6.35	✓94 46	✓

		300 81	
℄		6.75	✓94 06 ✓
¼		7.30	✓93 5 ✓
C.		8.80	✓91 0 ✓
E. R. E+10		10.00	✓90 8 ✓
		11.30	✓89 5
	S.E. Cor. Lot 12 - Bk. C (PL)		
W. R.		4.60	✓96 ✓ ✓
C		6.90	✓93 9 ✓
¼		7.10	✓93 7 ✓
℄		7.40	✓93 4 ✓
¼		7.80	✓93 0 ✓
C.		10.40	✓90 4 ✓
E. R. E+10 +V0		11.40	✓89 4 ✓
		12.40	✓88 4
	50'. north.	14.30	✓86 5
W. R.		4.50	✓96 3 ✓
C		5.20	✓95 1 ✓
¼		6.50	✓94 3 ✓
℄		7.40	✓93 4 ✓
¼		8.0	✓92 8 ✓
C		10.50	✓90 2 ✓
E. R. 10 V0		11.70	✓89 1 ✓
		13 60	✓87.8
		14.30	✓86 5

	+	−		
	56' north.	300.81		
W R.			4.50	×963 ✓
C.			5.30	×955 ✓
¼			7.10	×937 ✓
℄			7.00	×938 ✓
¼			8.05	×976 ✓
C			10.30	×905 ✓
E. R. 14			11.50	×893 ✓
×0	N.E. Cor. Lot 1, Bk C		13.00	×878
			14.50	×863
W. R.			5.40	×954
C.			6.15	×946 ✓
¼			8.00	×918 ✓
℄			8.50	×913 ✓
¼			9.15	×9166 ✓
C			11.65	×8916 ✓
E. R. 11			13.25	×8756 ✓
×0			14.60	×8622
			16.30	×835
B.M.	1.69	297.14		295.45

	+		×971/4		
	SE. Cor. Lot 10, Bk. B		(PI)		
W R.			3.30	×938	✓
C.			4.80	×923	✓
¼			6.25	×908	✓
℄			6.55	×905	✓
¼			7.80	×893	✓
C			10.20	×869	✓
E. R. 10			11.50	×856	✓
×0	50' north.		13.00	×841	
			14.50	×826	
W R.			7.20	×899	✓
C.			8.10	×890	✓
¼			10.80	×863	✓
℄			10.70	×864	✓
¼			11.40	×857	✓
C			13.65	×8349	✓
E. R. 10			15.50	×816	✓
×0			16.70	×804	
			18.00	×791	
TP	0.88	285.77	12.25	284.89	

	285.77	785 8		
	50' north.			
W R.		4.55	781	✓
C.		5.20	806	✓
1/4		5.80	800	✓
℄		6.60	792	✓
1/4		7.40	784	✓
C.		8.40	774	✓
E. R.		9.60	762	✓
10		10.80	750	
20	25' north.	12.60	733	
W R.		14.0	718	✓
C		14.0	718	✓
1/4		13.7	711	✓
℄		14.1	713	✓
1/4		15.2	706	✓
C		18.3	675	✓
E. R.		20.5	653	✓
10		22.00	638	
20		23.00	628	
	30' north. Creek Bottom			
W R.		30.4	554	✓
C.		31.0	548	✓

		785 8		
1/4		32.1	537	✓
℄		32.0	538	✓
1/4		31.0	548	✓
C		32.0	538	✓
E. R.		33.3	521	✓
	13' north.			
W. R.		23.0	618	✓
C		28.0	578	✓
1/4		29.7	561	✓
℄		32.0	538	✓
1/4		32.7	531	✓
C		33.2	516	✓
E. R.		34.2	516	✓
10		35.00	508	✓
20		33.2	516	✓
	(P.C.) 17' north.	N ℄ E Cor. Lot 1 BK B.		
W R.		12.5	783	✓
C		13.2	776	✓
1/4		13.5	773	✓
℄		13.5	773	✓
1/4		14.4	714	✓

	+	285.77	13.8		
E. Curb			13.0	708	✓
E. Pt			15.3	705	✓
10			16.8	698	
20			17.0	688	
	25' north N.E. Cor. Lot 1 Bk. B (P.T.)				
W. Pt			7.5	783	✓
C			7.6	778	✓
¼			8.3	775	✓
E			8.8	770	✓
¼			9.6	762	✓
C			10.2	756	✓
E. Pt			10.8	750	
10			11.4	744	✓
20	28' north		12.1	737	
W. Pt.			0.0	285 8	✓
C			1.60	284	✓
¼			2.10	283	✓
E			2.40	282	✓
¼			3.90	819	✓
C			4.70	811	✓
E. Pt			4.80	810	✓
10			6.09	798	
TP 20	11.33	297.09	6.88	790	
			0.01	285.76	

		297.09	297 1		
	E. Cor. Lot 8 - Bk. A (P.C.)				
W. Pt.			6.40	907	✓
C			8.00	891	✓
¼			9.30	878	✓
E			10.00	871	✓
¼			11.90	855	✓
C			13.70	834	✓
E. Pt			14.80	823	✓
10			15.80	813	
20	50' north		16.60	805	
W. Pt.			3.70	934	✓
C			5.20	919	✓
¼			8.20	889	✓
E			7.85	897	✓
¼			9.70	871	✓
C			11.10	860	✓
E. Pt			13.10	840	✓
10			14.00	831	
20	N.E. Cor. Lot 1, Bk. A		15.20	819	
W. Pt.			2.30	948	✓
C			3.55	935	✓

Boundary St.

297'

¼	5.70	291	✓
C	5.60	2915	✓
¼	8.00	2891	✓
C	9.90	287x	✓
E. Pt. 10 20	12.20	2749	✓
	13.70	2834	
	15.20	2819	

62' north - (North Side Redwood St.)

W. Pt.	1.20	2959	✓
C	3.00	2941	✓
¼	5.55	2915	✓
C	6.00	2911	✓
¼	7.10	2900	✓
C	9.20	2879	✓
E. Pt. 11 20	10.90	286x	✓
	12.10	2850	
	14.10	2830	

end Boundary

Redwood St

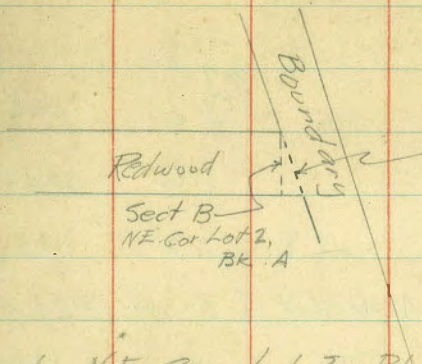
Starting at Boundary St. and working west.

Sect A.

		297.09	297		
S. Pl.			2.30	294.8	✓
C			1.80	295.3	✓
1/4			3.40	293.7	✓
¢			2.70	294.4	✓
1/4			1.70	295.4	✓
C			2.40	294.7	✓
N. Pl.			1.20	295.9	✓
PP	11.22	307.80	0.51	296.58	

Sect B. N.E. Cor Lot 2 Blk A

			307.8		
S. Pl.			10.2	297.6	✓
C.			10.0	297.8	✓
1/4			9.6	298	
¢			11.4	296.4	✓
1/4			10.3	297.5	✓
C			10.7	297.1	✓
N Pl			9.0	298	



55' west N.E. Cor. Lot 3 Blk. A.

			307.8		
S. Pl.			5.4	302	✓
C.			5.2	302.6	✓
1/4			5.3	302.5	✓
¢			5.6	302.2	✓
1/4			5.4	302.4	✓
C			6.2	301.6	✓
N Pl			4.8	303.0	✓

55' west N.E. Cor. Lot 4, Blk A.

S. Pl.			3.3	302.5	✓
C.			3.2	302.6	✓
1/4			3.0	302.8	✓
¢			3.3	302.5	✓

Redwood.

307.80

		307.8		
1/4		3.0	3048	✓
C		3.6	3042	✓
N. PL.		2.3	3055	✓
55' west. N.W. Lot 4 Blk A (PZ)				
S PL.		1.7	3061	✓
C		1.3	3065	✓
1/4		1.5	3063	✓
℄		1.7	3061	✓
1/4		1.3	3065	✓
C		2.1	3057	✓
N. PL		0.30	3075	✓
B.M.	9.85 315.70	1.95	305.85	
50' west. (west side McKinley St.)				
		315.7		
S. PL.	—	8.3	307 ℄	✓
C		8.1	3076	✓
1/4		7.8	3079	✓
℄		8.0	3077	✓
1/4		7.8	3079	✓

	315.7		
C	8.20	3075	✓
N. PL.	7.20	3085	✓
50' west.			
S. PL.	7.70	3080	✓
C.	7.30	3084	✓
1/4	6.85	3088	✓
℄	7.80	3079	✓
1/4	7.20	3085	✓
C.	6.60	3091	✓
N. PL.	5.80	3099	✓
50' west.			
S. PL.	7.80	3079	✓
C.	7.30	3084	✓
1/4	7.00	3087	✓
℄	7.20	3085	✓
1/4	7.0	3087	✓
C	6.1	3096	✓
N. PL.	5.8	3099	✓

315.70

50' west

S. PL.	315.7 / 10.80	3089	✓
C.	9.70	3060	✓
1/4	8.10	3076	✓
℄	7.4	3083	✓
1/4	6.7	3090	✓
C	6.8	3089	✓
N PL	6.3	3094	✓

50' west.

S. PL.	6.80	3089	✓
C	6.65	3090	✓
1/4	6.60	3091	✓
℄	6.50	3094	✓
1/4	6.30	3094	✓
C.	6.00	3097	✓
N. PL.	5.25	3104	✓

50' west

S PL.	5.10	3106	✓
C.	4.85	3108	✓

Redwood Jt.

315.7 / 4.70 — 3110 ✓

℄	5.30	3104	✓
1/4	5.10	3106	✓
C	4.60	3114	✓
N. PL.	4.15	3118	✓

50' west.

S. PL.	4.60	3111	✓
C	4.45	3114	✓
1/4	4.35	3113	✓
℄	4.50	3112	✓
1/4	4.50	3117	✓
C.	4.10	3116	✓
N. PL.	3.90	3118	✓

50' west.

S. PL.	3.90	3118	✓
C	3.80	3119	✓
1/4	3.60	3121	✓
℄	3.90	3118	✓
1/4	3.65	3120	✓

315.7

C.	3.40	313 ✓
N. PL.	2.95	312.7 ✓
50' West.		
S. PL.	3.35	313 ✓
C.	3.00	312.7 ✓
1/4	3.00	312.7 ✓
℄	3.30	312.4 ✓
1/4	3.10	312.6 ✓
C.	2.60	3131 ✓
N PL.	2.40	3133 ✓
50' west.		
S. PL.	3.00	312.7 ✓
C.	2.85	312.8 ✓
1/4	2.55	3131 ✓
℄	2.80	312.9 ✓
1/4	2.60	3131 ✓
C	2.45	313 ✓ ✓
N. PL.	2.00	313 ✓

315.70

50' west.	315.7	
S. PL.	2.75	313 ✓
C	2.70	3130 ✓
1/4	2.60	3131 ✓
℄	2.95	312.7 ✓
1/4	2.60	3131 ✓
C	2.40	3133 ✓
N. PL.	2.00	3137 ✓
50' west.		
S. PL.	3.25	312.4 ✓
C	3.20	312.5 ✓
1/4	3.05	312.6 ✓
℄	3.20	312.5 ✓
1/4	3.20	312.5 ✓
C	3.00	312.7 ✓
N. PL.	2.30	313.7 ✓
B.M.	2.73	312.97 ✓

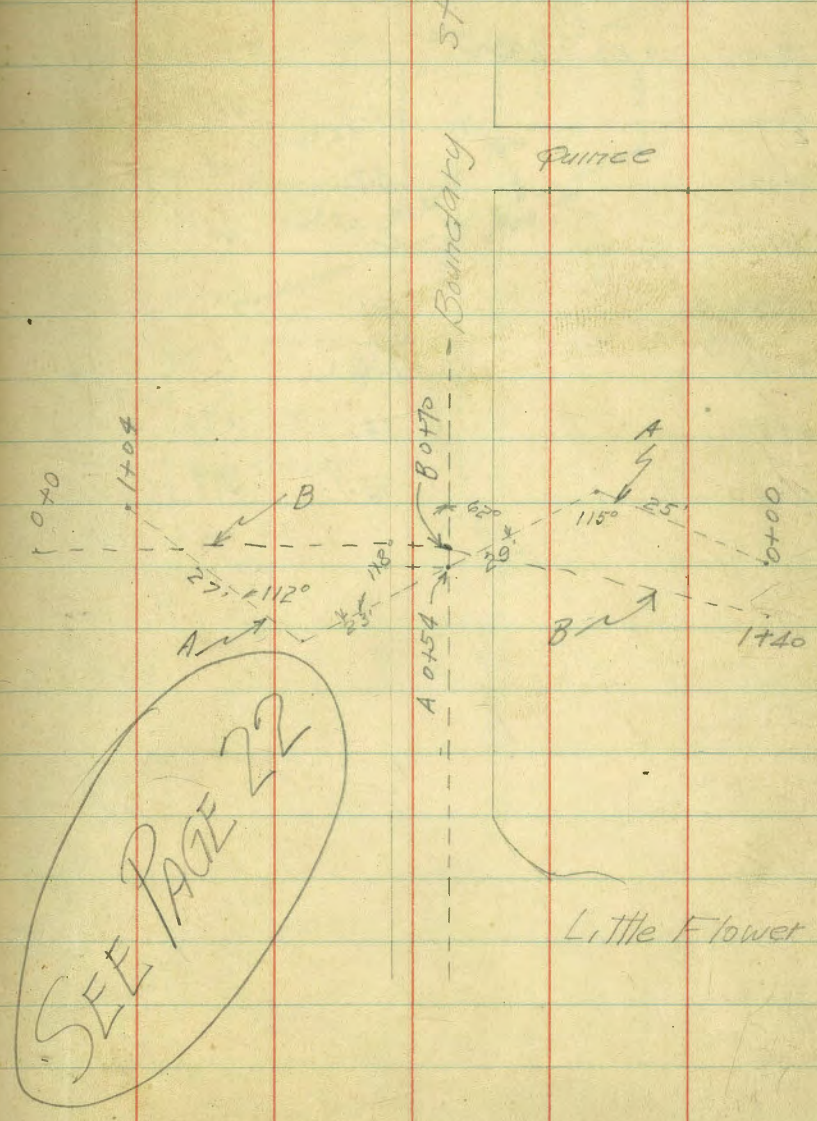
E.L. Felton
end Redwood.

Cross Sections for Culvert on Boundary St between Quince and Little Flower.

	+	H.I.	−	Elev.
B.M.	0.01	295.46		295.45
	0.45	283.28	12.63	282.83
	0.32	271.05	1255	270.73
	0.71	260.00	1176	259.29

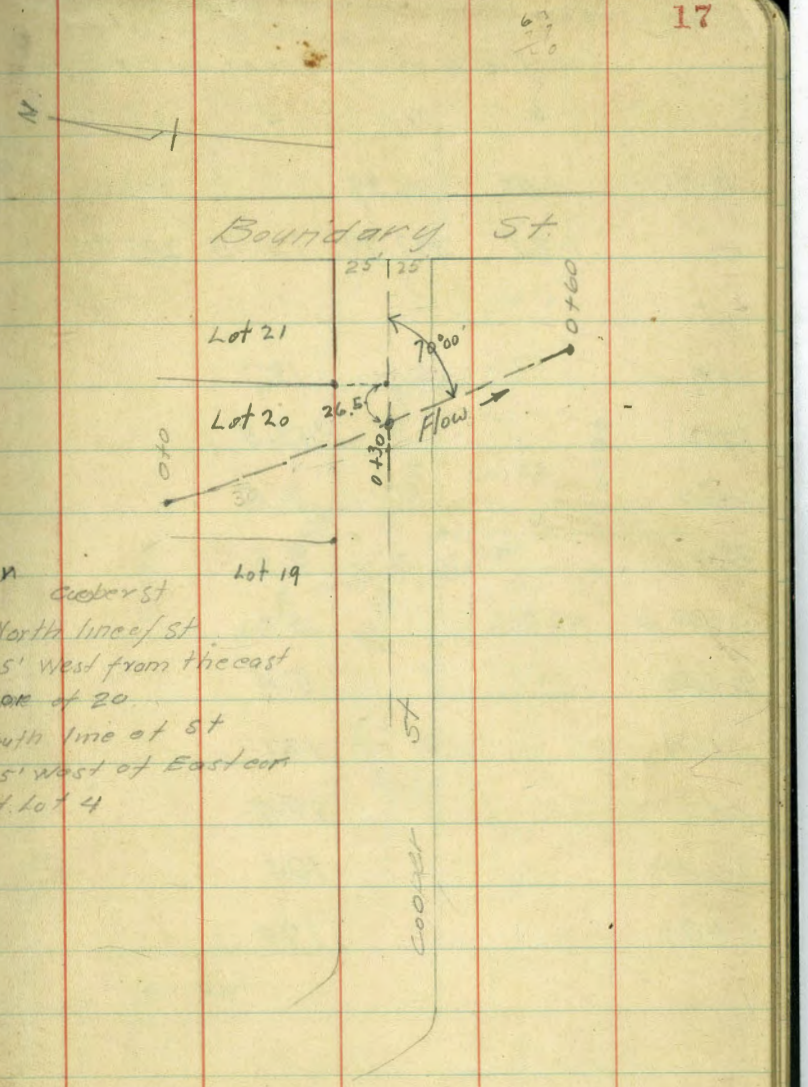
	A	B	B'	A
0+0	0+0	12.6	4.3	√47 ✓
0+10	0+15	11.0.4	4.5	√49 ✓
0+20	0+20	10.0	4.9	√50 ✓
0+25 Angle	0+30	9.6	5.2	√50 ✓
0+35	0+40	7.3	5.6	√57 ✓
0+45	0+50	5.7	6.4	√63 ✓
0+54 ℄	0+60	5.1	6.6 (53.4)	√59 ✓
0+66	0+70 ℄	5.4	6.9	√56 ✓
0+70 ℄	0+80	5.7	7.3	√54 ✓
0+87	0+90	3.0	7.9	√70 ✓
0+97	1+00	1.4	8.5	√86 ✓
	1+10	1.3		√87 ✓
1+04	1+20	3.1	9.5	√69 ✓

B	B'		
1+30	4.1	√59	✓
1+40	3.3	√62	



On Cooper between Boundary St and Angle Point on Cooper

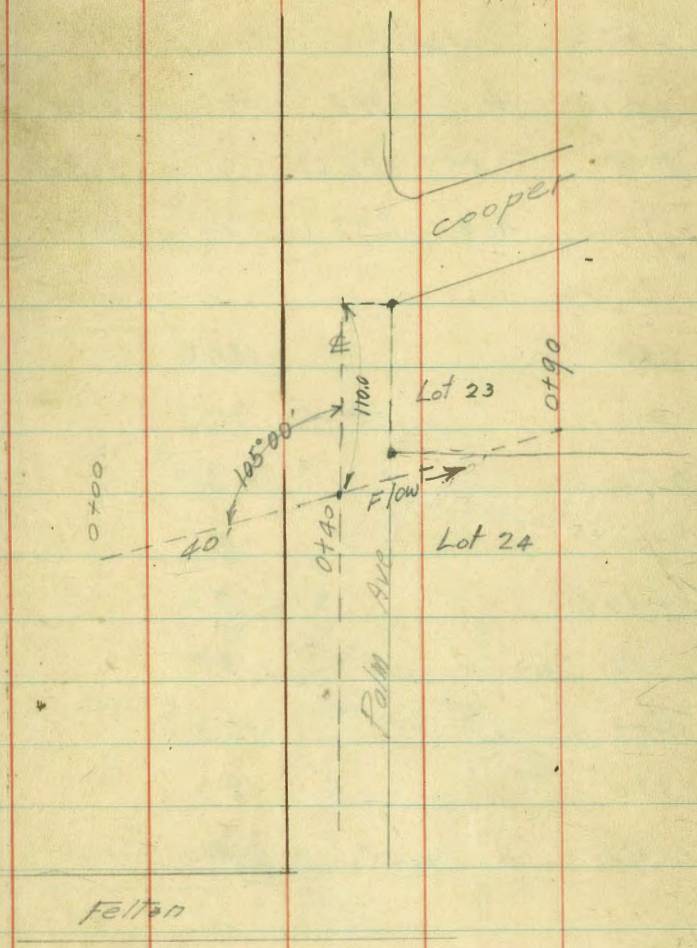
	+	H.I.	−	Elev
B.M.	0.27	294.00		293.73
0+0			9.7	284.3 ✓
0+10			8.7	285.3 ✓
0+20			8.3	285.7 ✓
0+30 ℄			11.1	282.9 ✓
0+40			13.2	280.8 ✓
0+50			14.5	279.5 ✓
0+60			15.7	278.3 ✓



N Cooper St
North line of St 35' West from the east cor of 20
South line of St 15' West of East cor of Lot 4

On Palm bet. Cooper and Felton.

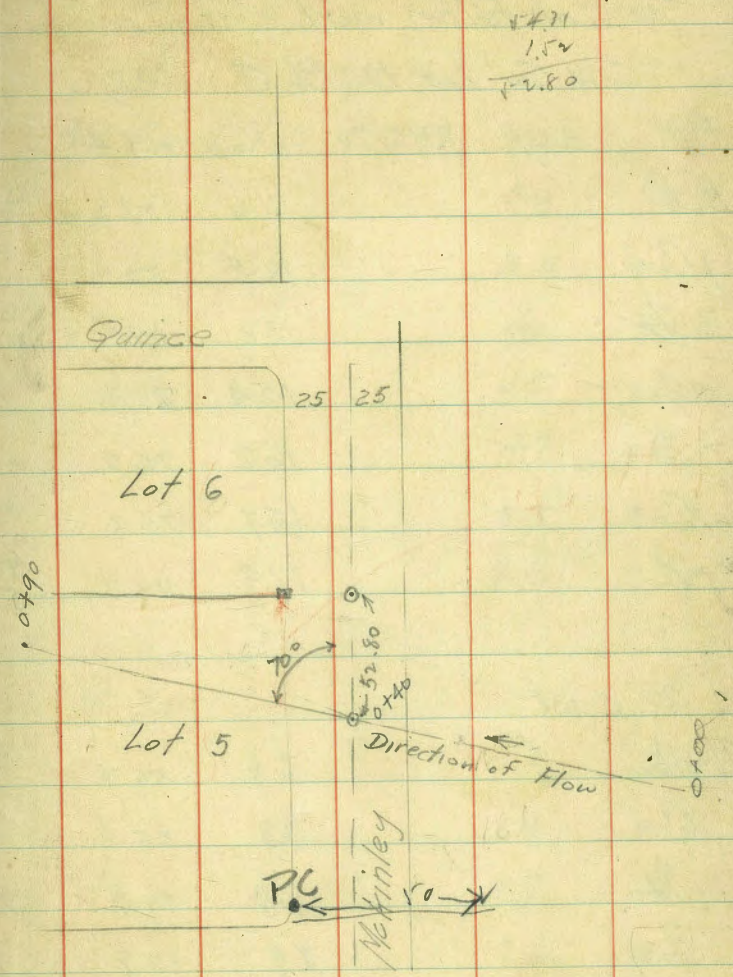
	+	HI	−	Elev
B.M.	0.01	308.37		308.36
	1.95	297.77	12.55	295.82
0+0			13.7	
0+10			13.5	
0+20			11.6	
0+30			5.5	
0+40 ℄			5.2	
0+46			5.4	
0+54			10.1	
0+70			12.5	
0+80			16.1	
0+90			17.0	



On McKinley bet. Quince and Little Flower.

	+	HI	−	Elev
B.M.	2.55	308.41		305.86
	4.8	292.7	—	288.3

0+0	10.6
0+10	10.3
0+20	9.0
0+30	4.9
0+40 ℄	5.0
0+47 Edge of Bank	6.3
0+58	16.5
0+70	18.3
0+90	20.9



Cross-Sections Nutmeg St.
Start at Felton, work east to Teresita

S.W. Cor. Lot 12, Blk. G. (P.I.)

BM	3.29	292.78		289.49
N Pl.			11.6	81.2
Curb			12.8	80.0
¼			13.8	79.0
℄			15.4	77.4
¼			16.2	76.6
Curb			16.7	76.1
S. Pl.			17.9	74.9

50' east

N Pl.			6.6	86.2
C			7.3	85.5
¼			7.9	84.9
℄			8.9	83.9
¼			9.7	83.1
C			10.7	82.1
S Pl.			11.4	81.4

T.J. ALLEN
April 22, 1926

292.78

S.E. Cor Lot 12, Blk. G.

N Pl.			3.0	89.8
C.			3.5	89.3
¼			4.0	88.8
℄			4.5	88.3
¼			4.7	88.1
C			5.5	87.3
Pl.			6.0	86.8

50' east

N Pl.			1.1	91.9
C			1.4	91.4
¼			1.7	91.1
℄			2.2	90.6
¼			2.4	90.4
C			2.5	90.3
Pl.			3.1	89.7

292.7+

S.E. Cor Lot 1, Bk. G. (P1)

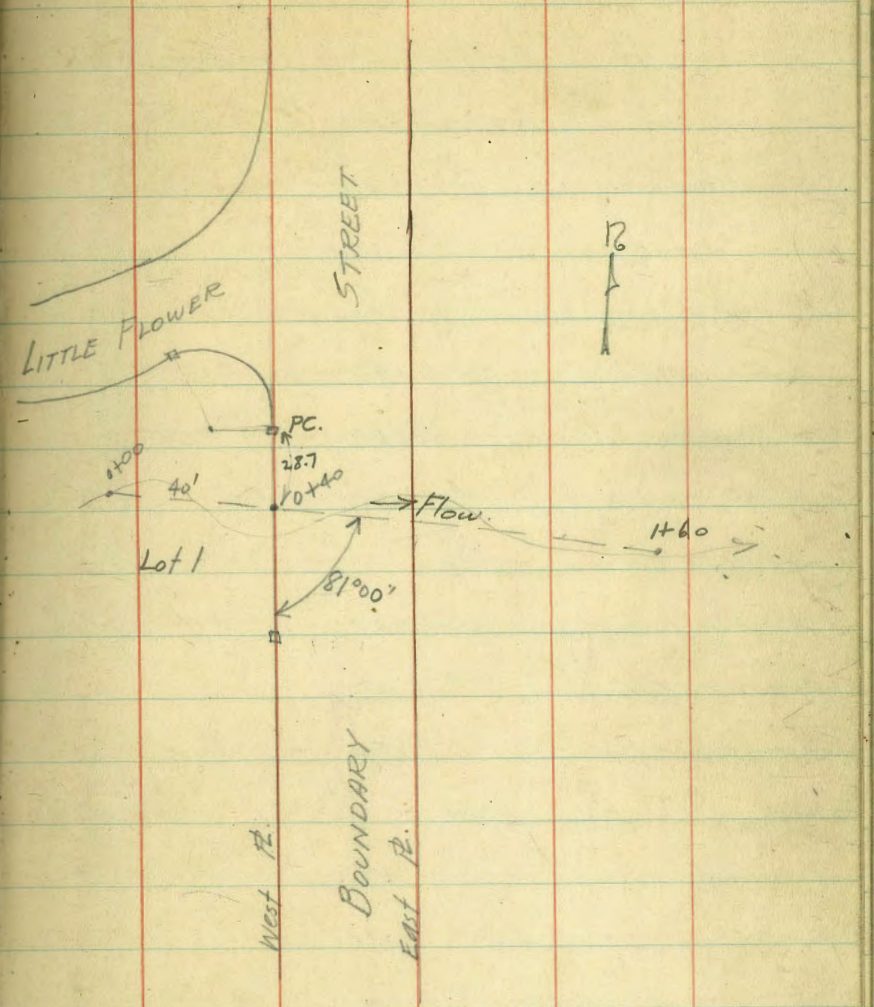
N Pt.	1.1	91.7
Curb	1.3	91.5
1/4	1.2	91.6
℄	1.3	91.5
1/4	1.5	91.3
Curb	1.6	91.2
S Pt.	1.8	91.0

S.W. Cor. Lot 39 Bk F

N Pt.	2.0	90.8
C.	2.1	90.7
1/4	2.4	90.4
℄	2.7	90.1
1/4	2.8	90.0
C	3.0	89.8
S Pt.	3.1	89.7

Culvert on Boundary between Little Flower & Quince.

TP.	6.00	259.4		253.4
			~~259.4~~	
1+60			13.0	246.4 ✓
1+40			11.3	248.1 ✓
1+10			8.8	250.6 ✓
0+85			5.2	254.4 ✓
0+70			5.8	253.6 ✓
	10.00	263.4	~~263.4~~	253.4
0+56			6.1	257.3 ✓
0+40			3.7	259.7 ✓
0+27			4.2	259.2 ✓
0+15			7.5	255.9 ✓
0+04			4.8	258.6 ✓
0+00			6.0	257.4 ✓



Cross Section Alley Block 16 Univ. Hgts.
From Madison to Adams Between Hamilton & Osgood 20' Wide

B.M.	4.80	38.379		37.899	SE Madison & Hamilton
		N.L. Madison			
E	Top Curb		3.24		
	Ground		3.7		
L			4.0		
+ 5			4.3		
W	Ground		3.8		
W	Top Curb		3.41		
		25' N			
W			3.3		
S			3.8		
E			3.0		
		50' N			
E			3.2		
S			3.6		
+ 5			3.5		
W			2.9		
		75' N			
W			3.0		
+ 5			3.4		

		38.379			S.P. 2.24 Sl. Floor No. Floor
S			3.1		
E			3.2		
		100' N			
E			4.8		
S			4.1		
W			3.0		
TP	5.80	38.654	3.05	38.074	
		125' N			110' N Garage 6" F.L. Conc. Floor
-7	Garage Dirt Floor		5.5		5.24
W			5.7		
S			5.9		192' N Garage Conc. Floor on W.L.
E			5.4		5.55
		150' N			
-6	Garage Conc. Floor		5.17		
E			5.7		
S			5.9		
W			5.8		
		175' N			
W			5.5		
S			5.5		
E			5.5		

		381.54			
		190'N			
-6 Garage Conc Floor			5.00		
E			5.5		
L			5.3		
W Fence 0.5 in Alley			5.3		
		235'N			
W			4.7		250'N on W.L. Concrete 435
S			4.6		
E			5.0		
		275'N			
E			4.9		
L			5.0		
W Fence 0.5 in Alley			5.0		
		300'N			
W Fence 0.5 in Alley			4.6		
Top N.H.			4.6		
L			4.7		
E			4.9		
		330'N			
E			4.8		
L			4.8		

		381.54			
W			4.5		
+2 Garage Conc Floor			4.24		
		360'N			
W			4.3		
L			4.2		
E			3.4		
+5.7 Garage Conc Floor			6.43		360'N Garage Conc Floor 2'W.L. 3.90
		400'N			
E			3.5		
L			3.6		407'N Garage Conc Floor 4'E.L. 3.4
W			3.6		
		430'N			
W			3.5		
L			3.7		
E			3.9		
		475			
-5.5 Garage			2.37		
E			2.7		
L			2.8		
W			3.0		
		490'N			

8&C 54

=2 De Garage Conc Floor		2.25		
N		2.9		
E		2.8	525 N S.S. F.F.L. 3 Garages Dirt Floors	
E		2.7		2.1
+5.5 De Garage Dirt Floor		2.3		
	540' N			
E		2.0		
S		2.2		
N		2.6		
	580' N			
W		1.8		
S		2.2		
+5		2.4		
E		1.7		
	597' N			
E		2.1		
+2		2.1		
+5		3.3		
S		3.4		
+5		3.5		
+8		2.5		

8&C 54

N		7.5		
600' N = C.L. Adams				
N Top Curb		4.58		
" Paving + Ground		4.03		
E " "		4.21		
E " "		3.93		
E " Curb		3.73		

LOCATION of NEW CUTOFF

Top Biological Grade. 0+00 = STA 145+00.6↓

P.R.C. Biological PAVING WEST ON N LINE

P.O.T 12+98 to STA.

P.O.T 14+11.0

E.C. 12+41.1

PI = 10+82.57

P.C 8+65.21

Δ = 71°51' RT.

D = 30°00'

T = 217.36

L = 376.20

det = 5°01'55

tab 61°53.67

P.O.T. 7+86.83

0+00 = P.R.C. 145+00.6↓

− 22.73 = P.I.

Δ = 71° 22.1'

T = 22.73

T = 311.35

2 x 2

3 x 3

3 x 3 hub

2 x 2 Hub

x 50 appr.↓ x 45.1↓ ⊕ TACK IN PAVING

STUB

11/19/26 Moore

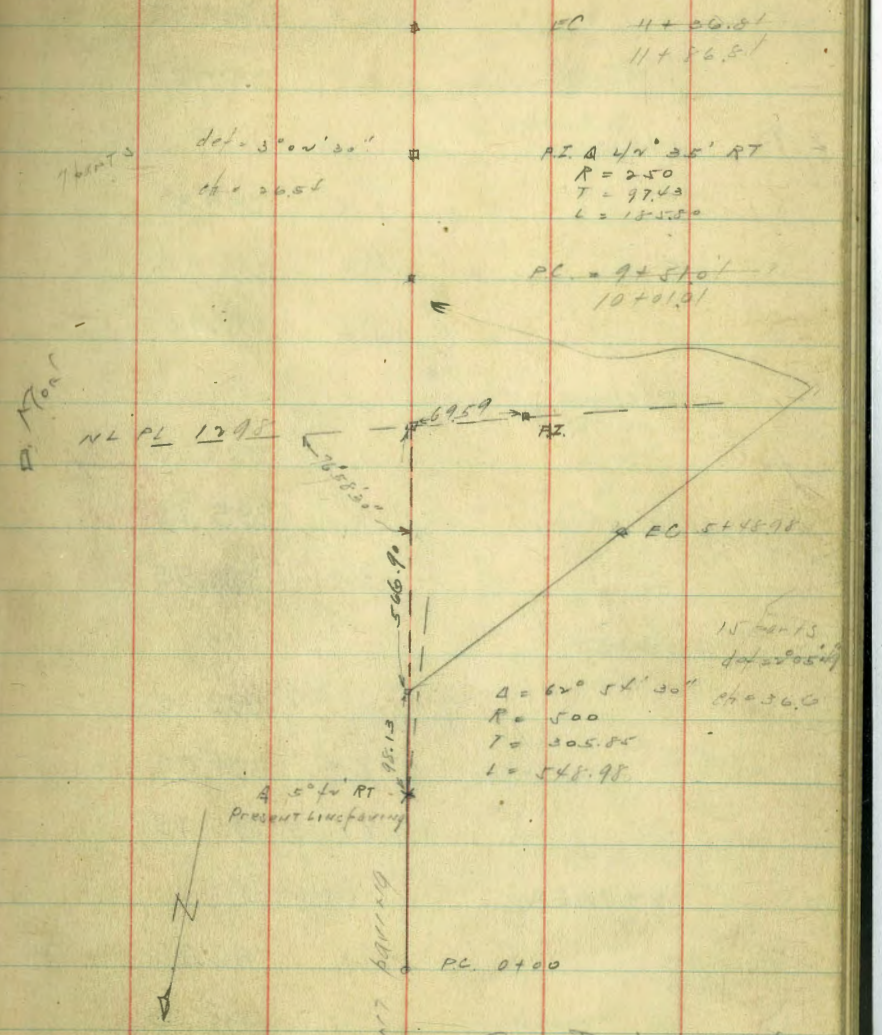
New Cut-off Tot Biology-ol proofs

PC = 2077N North of old Angle pt. (5°45') STA?

	1N5	40 1N5	400.00	assumed at PC & bearing
-50	℄ paving	0.8N	400.43	
	PC = 0+00			
E		1.1	400.15	
C	on bearing	1.1N	400.0	
W		1.1	399.85	
	0+36.6			
W		1.6	399.65	
C	on bearing	1.8	399.75	
E		1.3	399.5	
	0+73.2			
E		1.9	399.35	
C		1.7	399.55	
W		2.2N	399.05	
	1+09.8			
W		2.3	397.95	
C		2.1	399.15	
E		2.0	399.25	

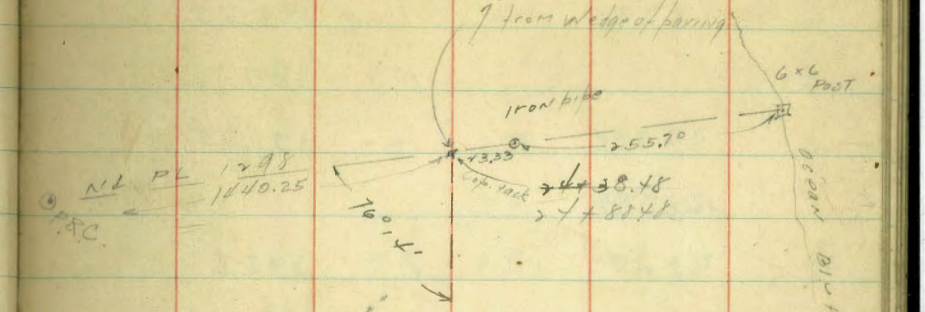
27

Cross Sectioned 30' wide



See Books 1039
99
1010

		1+01.5		
	1+46.4			
IE			2.3	398.95
C			2.9	398.35
W			3.3	397.95
	1+82			
W			3.9	397.35
D			4.3	396.95
IE			3.3	397.95
	2+19.6			
IE			5.3	395.95
C			6.0	395.25
W			6.7	394.55
	2+56.4			
W			8.1	393.15
C			7.4	394.05
IE			6.1	395.15
	2+94.8			
E			7.5	393.75
C			9.5	392.05
W			12.5	388.75



	3+29.4			
W		12.5	388.75	
C		11.1	390.15	
E		10.2	391.05	
	3+66			
E		8.7	392.55	
C		8.7	392.55	
W		9.1	392.15	
	3+92			
E	approx. location of wood stairs	7.1	394.15	26.1
	4+00.6			
W		7.4	393.85	
C		6.9	394.35	
E		6.9	394.35	
	4+39.2			
E		3.9	397.35	
C		4.2	397.05	
W		5.0	396.25	
	4+75.8			
W		4.1	397.15	

C		3.2	397.95	
E		2.9	398.35	
	5+14.4			
E		2.2	398.05	
C		3.8	397.45	
W		4.8	396.45	
	5+48.98 = E.C.			
W		6.2	395.05	
C	on 5+46	5.32	395.93	
E		4.6	396.65	
	6+00			
E		7.2	394.05	
C		8.1	393.15	
W		8.7	392.55	
	6+50			
W		12.0	389.25	
C		11.1	390.15	
E		10.3	390.95	
T.P.	189	390.67	12.47	388.78

390.67

	7+00			
E		3.0	387.67	
C		3.8	386.87	
W		4.1	386.57	
	7+50			
W		6.3	384.37	
C		5.5	385.17	
E		5.1	385.57	
	8+00			
E		6.8	383.87	
C		7.5	383.17	
W		8.1	382.57	
	8+50			
W		9.0	381.67	
C		8.5	382.17	
E		8.0	382.67	
	9+00			
E		9.7	381.97	
C		9.6	381.07	
W		10.4	380.27	

390.67

	9+50			
W			11.5	379.17
C			11.1	379.57
E			10.9	379.77
	10+01.01		From base on 1 stove	
	9+51.01 = P.C.		stas up 50	
E			12.9	377.77
T.P.	1.77	379.54	12.90	377.77
Concrete			2.6	376.94
W			3.7	375.84
	9+77.55			
	10+27			
W			6.3	373.24
C			6.8	374.74
E			3.3	376.24
	10+54.09			
	10+04.09			
E			11.2	368.34
C			10.8	369.14
W			13.8	356.14
T.P.	0.80	367.45	14.89	366.65
	1+80			
	10+30.63			
W			7.2	360.25

		367.45		
C			7.7	359.75
E			7.6	359.85
	10+57.17			
E			12.5	354.95
C			16.0	351.45
W			18.0	349.45
T.P	11+	356.78	13.16	343.62
	10+83.7	= Culvert + Hydro ?		
	11 33			
W			16.0	340.78
C			12.9	343.88
E			5.7	348.08
	11+10.25			
	11+60.25			
E			9.6	347.18
C			15.7	341.1
W			18.7	338.08
	11+86.81			
	11+36.81 = E.C.			
W			20.5	336.28
C			15.5	341.3
E			9.6	347.18

	5	356.78		
	11+90			
	12+40			
E			9.3	347.48
C			14.8	342.0
W			21.6	335.18
	12+85			
W			28.0	328.78
C			18.5	338.3
E			8.5	348.28
	13+65			
	13+15			
E			5.7	351.08
C			12.1	344.7
W			22.5	334.38
	13+80			
	13+30			
W			18.0	338.78
C			9.6	347.2
E			-2.5	354.28
	13+00			
	13+50			
E			+1.7	358.48
C			-5.6	51.2
W			-11.2	395.58

		356.78			
	13+35				
	13+85				
W			17.0	339.78	
C			-6.6	50.2	
E			+3.4	350.18	
	13+75				
	14+25				
E			+6.1	362.88	
C			-3.9	52.9	
W			13.9	392.9	
T.P.	5.71	358.98	3.51	353.27	
	14+21.22	=P.C.			
	14+31.22				
W			20.8	338.18	
C			-7.8	351.2	
E			+0.7	359.68	
	14+51.22				
	15+01.22				
E			-0.3	358.68	
C			8.5	50.5	
W			18.4	340.58	
	14+81.22				
	15+31.22				
W			17.0	341.98	
C			10.9	331.1	

		358.98			
E			4.6	354.38	
	15+11.22				
	15+61.22				
E			9.7	349.18	
C			15.3	43.7	
W			21.1	337.88	
T.P.	0.47	347.13	1.32	346.66	
	15+41.22				
	15+91.32				
W			31.0	316.13	
C			19.9	301.2	
E			7.0	340.13	
	15+71.32	=E.C.			
	16+21.32				
E			9.4	337.73	
T.P.	0.14	334.30	1.95	334.18	
C			8.3	26.0	
W			19.3	315.0	
	16+14				
	16+62				
W			22.8	311.5	
C			9.6	24.7	
E			2.7	331.6	

		334.20			
	16+70				
	17+20				
E			17.9	316.4	
C			27.0	07.3	
W			34.8	299.5	
	17+05				
	17+55				
W			35.0	299.3	
C			26.0	08.3	
E			17.✓	316,9	
	17+70				
	17+90				
E			5.✓	328.9	
C			13.✓	11.1	
W			22.3	312.0	
	17+70				
	18+20				
W			17.✓	317.1	
C			8.0	26.3	
E			3.✓	331.1	
	17+96.22 = POT				
E			4.✓	330.1	
C = POT STUB			9.✓	26.1	
W			17.✓	318.8	
T.P	0.09	321.32✓	1807	321.23✓	

		321.32			
	18+52.40 = PC				
	1902.40				
W			12.0	309.32	
C			8.✓	17.9	
E			4.1	317.22	
T.P	0.41	308.85✓	12.88	308.44✓	
	18+84.72				
	1934.72				
E			0.0	308.85	
C			4.9	03.9	
W			6.3	302.55	
	19+17.0				
	1967.04				
W			8.✓	300.35	
C			6.✓	02.5	
E			3.9	304.95	
	19+39.36				
	19+99.32				
E			4.6	304.25	
C			7.✓	1.4	
W			10.8	298.0	
	19+81.68				
	20+31.68				
W		308.8	9.✓	299.65	
C			7.1	301.8	
E			5.✓	303.65	

		308.85		
	20+16			
	20+64			
E			7.3	301.55
C			8.8	00.1
W			10.0	298.85
	20+46.32			
	20+96.32			
W			12.9	295.9
C			11.8	99.1
E			11.4	297.45
	20+756			
	21 28.6		308.35	
E			14.9	293.9
C			15.5	293.4
W			17.1	291.75
T.P	179	292.66	12.98	295.87
	21+10.96			
	21+60.36			
W			10.6	287.06
C			9.8	89.9
E			8.4	289.26
T.P	193	287.85	12.74	284.96
	21+53.28			
	21+93.28			
E			4.9	282.95

		287.85		
C			5.3	82.6
W			6.4	281.45
	21+75.81 = EC			
	2225.81			
W			10.1	277.75
C			5.90	80.0
E			5.4	282.65
	22+67.5			
	W +17.4 = W edge bearing			
E	edge bearing		7.4	280.45
C	" "		6.1	281.8
W			6.7	281.15
	23+00			
	23+50			
W			10.5	277.35
C	E edge bearing		10.7	99.2
E			11.4	276.15
T.P	331	285.26	5.90	281.95
	W+38.48 ℄ bearing		17.05	268.21
	24+88.48			

	Meade Idaho to Texas	Ave	Xsec	80 wide 14" cob	
SEB	3.86	381.09		377.23	Meade Oregon
WL Idaho=00					
S			5.0	76.1	
tob con cb			√1.7	75.92	
gut			√.√	75.6	
1/4			√.√	75.7	
C			√.3	75.8	
1/4			√.6	75.5	
gut			√.√	75.7	
tob con cb			√.√	75.7	
N			1.9	76.2	
gut w					
N			√.3	75.8	
cb			√.6	75.5	
1/4			√.4	75.7	
C			√.N	75.9	
1/4			√.√	75.6	
cb			√.3	75.8	
S			1.9	76.2	

SW & NW cb curbs on both sides of street. Cut sidewalk NOT IN. SE Return must be rebuilt. Sunnan Engineering Co. Engineer of Meade Oregon. Control point = 20.00

Meade Idaho to Texas		381.09			
	35' in				
S			3.6	77.5	
cb			√.0	76.1	
1/4			√.√	75.6	
C			√.√	75.6	
1/4			√.1	76.0	
cb			√.√	75.6	
N			√.N	75.9	
	10' in				
N			√.1	76.0	
cb			√.√	75.6	
1/4			√.N	75.9	
C			√.1	76.0	
1/4			√.7	75.4	
cb			√.4	75.7	
S			√.0	76.1	
	75' w				
S			√.3	75.8	
cb			√.3	75.8	
1/4			√.4	75.7	

		38109		
C			1.4	75.7
1/4			1.1	76.0
CB			1.3	75.8
℄			4.8	76.3
	100' N			
℄			4.6	76.5
CB			1.0	76.1
1/4			1.3	75.8
C			1.3	75.8
1/4			1.3	75.8
CB			4.8	76.3
S			4.9	76.2
	175' N			
S			1.N	75.9
CB			1.0	76.1
1/4			1.0	76.1
C			4.7	76.4
1/4			4.5	76.6
CB			4.6	76.5
℄			4.6	76.5

	1450	38109		Mondo 36
℄			4.5	76.6
CB			4.5	76.6
1/4			4.8	76.3
C to ℄	Sewer MH Rim		4.6	76.44
1/4			4.8	76.3
CB			1.N	75.9
S			1.1	76.0
	200 N			
S			4.7	76.4
CB			4.7	76.4
1/4			4.9	76.2
C			4.9	76.2
1/4			1.0	76.1
CB			4.7	76.4
℄			4.5	76.6
	250 N			
℄			4.6	76.5
CB			4.7	76.4
1/4			4.7	76.4

c		4.7	76.4	
1/4		4.7	76.4	
cb		4.7	76.4	
S		4.5	76.6	
	2.75 in			
S		4.4	76.7	
cb		4.6	76.5	
1/4		4.6	76.5	
c		4.8	76.3	
1/4		5.0	76.1	
cb		4.7	76.4	
R		4.5	76.6	
	2.95 in			
R		4.6	76.5	
cb		4.8	76.3	
1/4		4.6	76.5	
c		4.8	76.3	
1/4		4.9	76.2	
cb		4.6	76.5	
S		3.8	77.3	

381.09 Meade

300' W. of Ft. Oregon

S	3.7	77.4	Oregon has 14 cbs.
Tobacco cb	3.9 W	77.17	to cut corn in 0
gut	4.3	76.8	sidewalk
1/4	4.6	76.5	
c	4.6	76.5	
1/4	4.6	76.5	
gut	4.3	76.8	
tobacco cb	3.90	77.19	
R	3.8	77.3	
W. Oregon 00			
R	4.1	77.0	
Tobacco cb	4.38	76.71	
gut	4.8	76.3	
1/4	5.0	76.1	
c	5.0	76.1	
1/4	5.0	76.1	
gut	4.8	76.3	
tobacco cb	4.47	76.62	
S	4.1	76.9	

381.09

S			4.6	76.5
cb			5.0	76.1
1/4			5.0	76.1
C			5.1	76.0
1/4			5.0	76.1
cb			4.9	76.2
R			4.3	76.8
	50' R			
R			4.5	76.6
cb			4.4	76.7
1/4			5.2	75.9
C			5.2	75.9
1/4			5.1	76.0
cb			5.0	76.1
S			4.9	76.2
	75' R			
S			5.1	76.0
cb			5.1	76.0
1/4			5.0	76.1

381.09

Moody

C			5.4	75.7
1/4			5.5	75.6
cb			5.3	75.8
R			4.8	76.3
T.P.	4.05	379.51	5.63	375.46
	100' R			
R			3.3	76.2
cb			4.0	75.5
1/4			4.0	75.5
C			4.0	75.5
1/4			4.0	75.5
cb			3.9	75.6
S			3.7	75.8
	125' R			
S			3.9	75.6
cb			4.1	75.4
1/4			4.1	75.4
C			4.4	75.1
1/4			4.3	75.2
cb			4.4	75.3

	379.5'			
N		3.8	75.7	
	150' W			
N		4.3	75.2	
cb		4.5-	75.0	
1/4		4.5-	75.0	
C on Sewer 19 H.P.M		3.0	76.5	
C for ydge		3.7	75.8	
1/4		4.4	75.1	
cb		4.3	75.2	
S		4.W	75.3	
	177' W			
S & H'com walk		3.95-	75.56	on line
S for ydge		4.3	75.2	
cb		4.8	74.7	
1/4		4.7	74.8	
C		4.5-	75.0	
1/4		4.6	74.9	
cb		4.W	75.3	
N		4.5	75.0	

	379.5'		Moore	39
	210' W			
N		5.W	74.3	
cb		5.3	74.2	
1/4		5.3	74.2	
C		4.5-	75.0	
1/4		4.7	74.8	
cb -		4.9	74.6	
S		4.7	74.8	
S & com double strip auto		4.50	75.01	drive out W
	231' W			
S & H'com walk		4.65-	74.86	" "
S for ydge		5.0	74.5	
cb		5.8	73.7	
1/4		5.7	73.8	
C		5.3	74.2	
1/4		5.4	74.1	
cb		5.4	74.1	
N		4.4	75.1	
	450' W			
N		4.6	74.9	

		3795'				3795'		Moodo 40
cb			J-9	73.6	cb		6.✓	73.3
1/4			J-6	73.9	S		6.4	73.1
c			J-7	73.8	300'W = EL Ham.		Returns all o K.	
1/4			J-9	73.6	S		7.9	71.6
cb			J-9	73.6	Top com cb good for ridge		8.37	71.14
S			J-✓	74.3	1/4		8.✓	71.3
	295'W				c		8.3	71.2
S			J-J-	74.0	1/4		8.✓	71.1
cb			J-8	73.7	gut		7.8	71.7
1/4			6.J-	73.0	top com cb		7.J-✓	71.99
c			6.7	72.8	W		7.✓	72.3
1/4			6.8	72.7	WL Ham = 00			
cb			6.1	73.4	W		8.8	70.7
W			4.J-	75.0	top com cb		9.1✓	70.39
	295'W				gut		9.4	70.1
W			6.3	73.2	1/J.		9.7	69.8
cb			6.J-	73.0	C		9.6	69.9
1/J			8.0	71.5	1/4.		9.9	69.6
c			7.8	71.7	Top com cb		10.0	69.5 for ridge
1/4			7.8	71.7	S		9.7	69.8

		379.51					
S'nl of Ham							
S			8.8	70.7			
cb			8.9	70.6			
1/4			9.5	70.0			
c			9.4	70.1			
1/4			9.7	69.8			
cb			8.9	70.6			
N/			8.7	70.8			
50'w/							
N/			8.9	70.6			
cb			9.0	70.5			
1/4			9.4	70.1			
c			8.9	70.6			
1/4			9.0	70.5			
cb			8.8	70.7			
S			9.3	70.2			
50'w/							
S			10.4	69.1			
cb			9.6	69.9			
1/4			9.7	69.8			

		379.51					
C			9.5	70.0			
1/4			9.7	69.8			
cb			9.8	69.7			
N/			9.6	69.9			
80'w/							
-3.5	E. garage	conc floor	10.6	68.91	9'w rdo floor level		
N/			11.3	68.2			
cb			11.4	68.1			
1/4			11.4	68.1			
c			11.2	68.3			
1/4			11.4	68.1			
cb			11.8	67.7			
S			12.2	67.3			
F.P.	1.39	369.00	11.90	367.61			
110'w/							
S			4.1	64.9			
cb			4.8	64.2			
1/4			3.2	65.8			
c			2.6	66.4			
1/4			2.7	66.3			

		369.00		
cb			2.6	66.4
N			2.5	66.5
	127'W			
N			3.6	65.4
cb			4.8	64.2
1/4			5.8	63.2
C			5.8	63.2
1/4			6.3	62.7
cb			6.0	63.0
S			5.4	63.6
+ W & corn walk 4' wide			5.7	63.3
	150'W			
S.			8.1	60.9
cb			8.5	60.5
1/4			8.8	60.2
C Sewer I.P. H/Rim			8.90	60.10
1/4			8.9	60.1
cb			9.1	59.9
N			8.6	60.4

		369.00		Inside
	175'W			
N			11.1	57.9
cb			11.3	57.7
1/4			9.9	59.1
C			10.1	58.9
1/4			11.1	57.9
cb			11.6	57.4
S			11.1	57.9
T.P.	0.63	356.43	18.50	350.80
	200'W			
S			1.3	55.1
cb			1.7	54.3
1/4			1.6	54.8
C			1.5	54.9
1/4			1.8	54.2
cb			1.0	54.4
N			1.9	54.5
	130'W			
N			4.4	52.0
cb			5.0	51.4

		356.43		
1/4			4.1	52.3
c			3.7	50.7
1/4			4.1	52.3
cb			4.4	52.2
s			3.3	51.1
	2.45 in			
s			7.3	49.1
cb			7.4	49.0
1/4			7.6	48.8
c			7.4	49.0
1/4			7.6	48.8
cb			7.4	49.2
n			3.5	50.9
	2.60 in			
n			7.6	48.8
cb			7.7	48.7
1/4			8.1	48.3
c			8.4	48.0
1/4			8.7	47.7
cb			8.7	47.7

		356.43		Moved
s			9.4	47.2
	2.75 in			
s			9.0	47.4
cb			8.7	47.7
1/4			9.1	47.3
c			9.0	47.4
1/4			8.4	48.0
cb			8.7	47.7
n			8.9	47.5
	2.95 in			
n			10.6	45.8
cb			11.9	44.5
t3			12.9	43.5
1/4			11.2	45.2
c			11.0	46.4
1/4			11.3	46.1
cb			10.9	45.5
s			10.6	45.9
TP	3.60	41.11	12.3	34.11

	347.77			
300 w/ EL Horiz.		all returns	O.K.	
S		S-3	42.5	
Top com cb	for type	S-66	42.11	
1/4		S-S	42.3	
C		S-0	42.8	
1/4		7.6	43.2	
gut		7.7	43.4	
top com cb		7.2	43.6	
N		3.7	44.1	
Wt Horiz=00				
N		S-S	42.3	
top com cb		S-68	42.09	
gut		6.6	41.2	
1/4		6.7	41.1	
C		6.4	41.4	
1/4		7.1	40.7	
gut		7.0	40.8	
top com cb		6.72	41.05	
S		6.4	41.4	
T.P.	18	347.86	6.72	341.05

	347.86		Mondo	
25 w				
S		3.1	39.8	
cb		4.0	38.9	
1/4		3.S-	39.4	
C		3.6	39.3	
1/4		3.9	39.0	
cb		4.0	38.9	
N		3.7	39.2	
+S		3.6	39.3	
50 w				
-S		4.2	38.7	
N		4.3	38.6	
cb		4.1	38.8	
1/4		4.4	38.5	
C		S.3	37.6	
1/4		S.1	37.8	
cb		S-0	37.9	
S		4.7	38.2	
65 w				
0.7 S of SL & Com Apron		4.00	38.86	8' wide

		3/7.86		
	75'w/			
S			3.8	39.1
cb			4.3	38.6
1/4			5.6	37.3
c			5.5	37.6
1/4			5.1	37.8
cb			4.6	38.3
w/			4.7	38.2
	85'w/			
-1.5 E con. double drive strip			4.80	38.06
w/			5.1	37.8
cb			4.8	38.1
1/4			6.0	36.9
c			6.2	36.7
1/4			6.1	36.8
cb			6.2	36.7
S			5.8	37.1
	100'w/			
S			6.3	36.6
cb			6.3	36.6

		3/7.86		Meade
1/4			6.6	36.3
c			6.9	36.0
1/4			6.9	36.0
cb			6.7	36.7
w/			5.7	37.2
110'w/ 1 upper true 10" diam 3' N of w/ cb				
115'w/				
w/			5.9	37.0
cb			6.3	36.6
1/4			6.6	36.3
c			6.5	36.4
1/4			5.1	37.8
cb			5.5	37.1
S			7.3	35.6
	135'w/			
S			8.0	34.9
cb			7.9	35.0
1/4			7.4	35.5
c			7.2	35.7
1/4			7.4	35.5

		34x86		
cb			7.1	35.8
✓			6.3	36.6
	150'w			
✓			6.8	36.1
cb			6.9	36.0
1/4			7.0	35.9
c = Tap Sewer MH/RIM			7.5	35.4
c			6.6	36.3
1/4			7.✓	35.7
cb			8.1	34.8
S			8.3	34.6
	175'w			
S			8.8	34.1
cb			9.0	33.9
1/4			8.6	34.3
c			8.0	34.9
1/4			8.✓	34.5
cb			8.5	34.4
✓			7.6	35.3

		34x86		
	200'w			
✓			8.✓	34.7
cb			9.0	33.9
1/4			9.1	33.8
c			9.0	33.9
1/4			8.9	34.0
cb			8.4	34.5
S			8.3	34.6
	225'w			
S			9.8	33.1
cb			8.9	34.0
1/4			7.8	35.1
c			7.7	35.2
1/4			8.9	34.0
cb			9.1	33.8
✓			8.6	34.3
	237'w			
✓			8.8	34.1
+10			7.5	35.3
cb			7.7	35.2

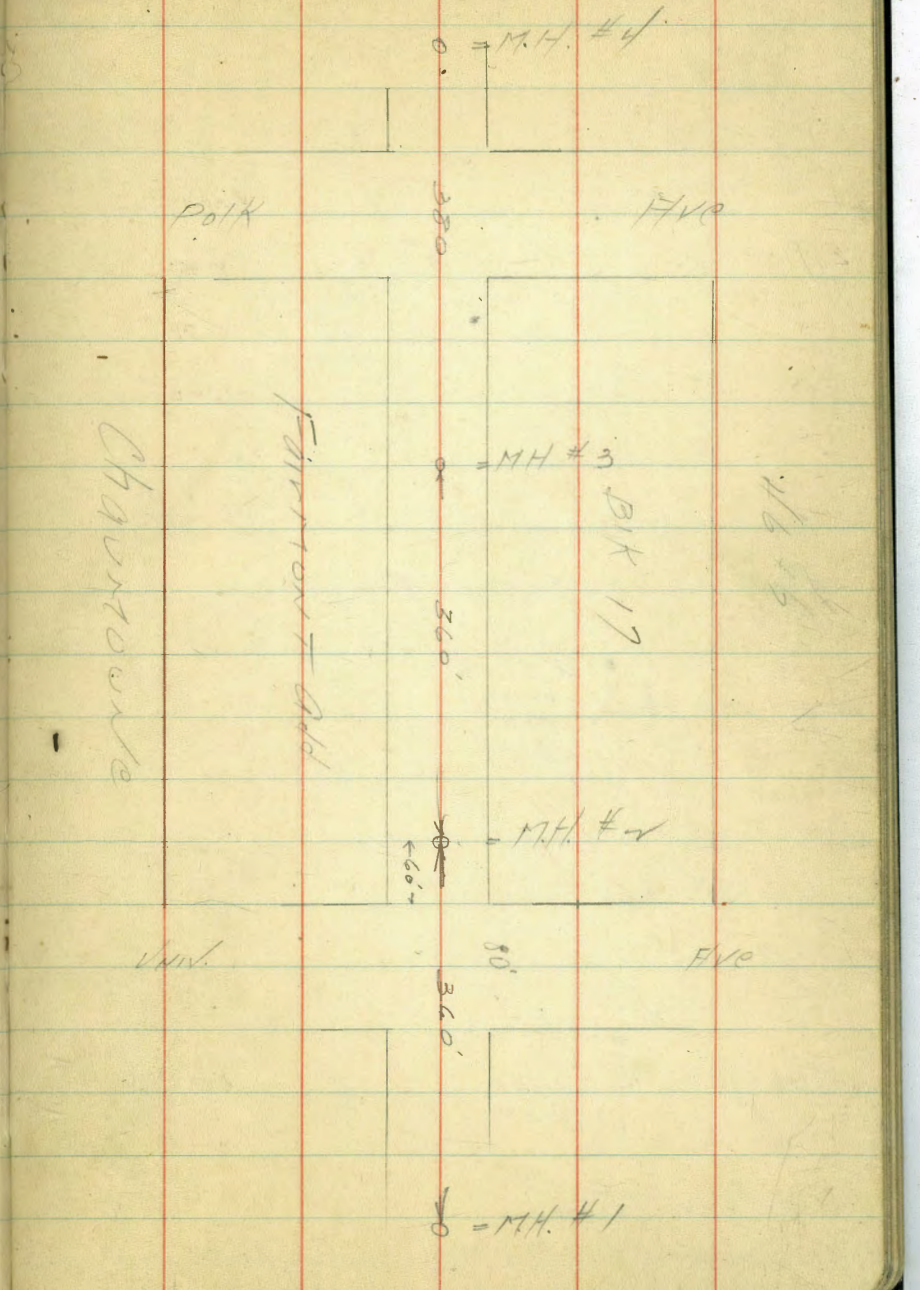
		3+286		
1/4			10.3	32.6
e			8.8	34.1
1/4			9.1	33.8
cb			9.9	33.0
S			9.5	33.4
	x50'w			
S			9.3	33.6
cb			10.1	32.8
1/4			10.0	32.9
e			9.9	33.0
1/4			10.0	32.9
cb			9.6	33.3
N			9.7	33.7
	x75'w			
N			9.6	33.3
cb			10.1	32.8
1/4			10.2	32.5
e			10.2	32.7
1/4			10.2	32.7
cb			9.8	33.1

		3+286		Meade	47
S			9.3	33.6	
	300'w = EL Tebb		Return w/l o.k.		
S			11.1	31.8	
top cor cb			11.33	31.53	
gut			11.6	31.3	
1/4			11.6	31.3	
e			11.4	31.5	
1/4			11.0	31.9	
gut			10.7	32.2	
top cor cb			10.40	32.46	
N			10.1	32.8	
SEBP Meade Texas 331.41			11.35	331.51	0.10 Error

Levels on Sewer M.H.'s Moore 1/14/17

BLK 17 Fairmont Add.

	4.58	356.98	352.40
Howline Sewer M.H. 2 ft S. of St. W.		15.7	= M.H. #1
Howline Sewer M.H. 60 N. of NL	"	14.5	342.46 = " #2
Rim	"	4.07	352.91 = " "
"	"	6.10	350.88 = " #3
Howline	"	13.5	343.46 = " "
"	"	12.75	344.73 = " #4



Sta. 1 Change of Line at West Biological Grade
Moore Cut off.

See page 28

xx+10.34 = old EC. = STA. xx+xx.81 old STA.

Δ = 61°46' LT
20+84.67 = P.I. R = 260.03
T = 156.2x
L = 28x.47

19+x7.95 = PC.

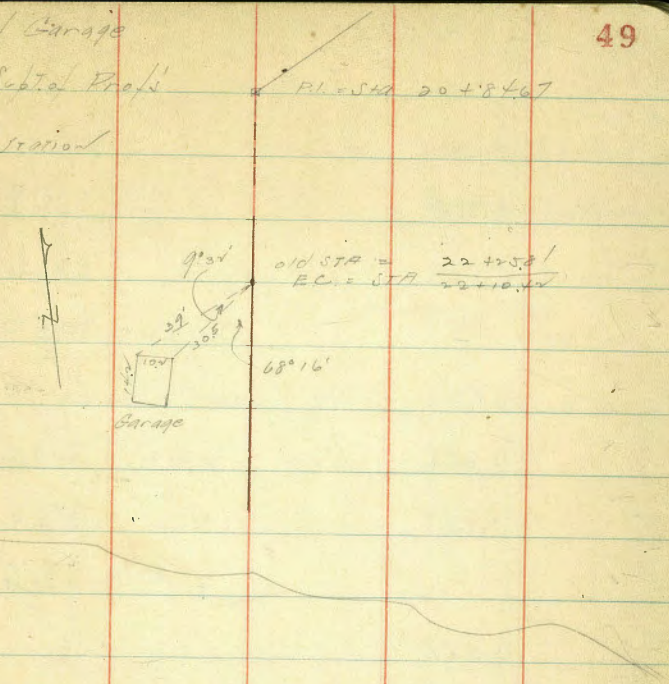
18+40 = P.C.T.

15+91.99 = E.C.

Δ = 43°00' LT
15+x0.67 = PI. R = 200'
T = 78.78
L = 150.1

14+41.89 = 0+00 = Change in Line

Location of Garage
property of Sch. of Prof.
at Biological Station



Cross section of new line on Biological Cut off 30 inside.

12+71 on sub station	12+45	363.65		351.20
12+48 = Sec. E			0.9	362.8
C			10.1	353.6
W			18.5	345.2
Sec F	Curve in 5 parts chords = 29.98			
W			23.2	340.4
C			11.3	352.4
E			1.8	361.8
Sec B				
E			1.9	360.8
C			9.7	354.0
W			18.4	345.2
Sec C				
W			16.5	347.2
C			11.5	352.2
E			6.5	357.2
Sec D				
E			10.0	353.6
C			15.1	348.4
W			22.2	341.4
18	333	354.15	12.33	350.82

354.15

Sec C = EC. 15+91.99

W			22.1	332.0
C			10.1	344.0
E			3.9	350.2
16+25				
E			7.2	347.0
C			14.7	339.4
W			26.0	328.2
16+50				
W			28.6	325.6
C			18.0	336.2
E			9.4	344.8
16+75				
E			15.2	339.0
T.P.	0.5	341.82	12.84	341.31
C			12.3	329.5
W			23.0	318.8
17+25				
W			32.5	309.3
C			23.1	318.7
E			12.1	329.7

	17+55	321.8			
E			11.4	330.4	
C			21.8	320.0	
W			31.4	310.6	
	17+75				
W			22.5	319.3	
C			13.2	327.6	
E			6.4	335.4	
	18+00				
E			5.0	336.8	
C			9.2	332.6	
W			15.6	326.2	
	18+40 = P.O.T.				
W			15.1	326.7	
C			11.2	330.6	
E			8.1	333.7	
T.P.	0.14	329.24	12.74	329.10	
	18+70				
E			1.0	328.2	
C			4.7	324.5	
W			9.9	319.3	

		329.24			
	19+00				
W			16.3	312.9	
C			12.2	317.0	
E			8.4	320.8	
	19+20				
E			12.7	316.5	
T.P.	0.60	316.91	12.92	316.31	
C			4.4	312.5	
W			7.9	309.0	
	19+27.9 = P.C.		Curve is 10 bars		Chord = 28.2
W			12.8	304.1	
C			9.6	307.3	
E			5.5	311.4	
	19+37 = Top of	bank on old road	on South		
E			10.0	306.9	
C			12.3	304.6	
W			13.7	303.2	
T.P.	3.38	307.67	12.64	304.29	
	See H = Top of bank				
W			5.2	307.3	

		307.67		
C			2.5	305.2
E			1.1	306.6
	Sec B			
E			0.9	306.8
C			4.1	303.6
W			7.3	300.4
	Sec C			
W			7.2	300.5
C			4.7	303.0
E			2.3	305.4
	Sec D			
E			4.3	303.4
C			6.1	301.6
W			8.1	299.6
	Sec E			
W			10.2	297.5
C			8.7	299.0
E			7.3	300.4
	Sec F			
E			10.7	297.0

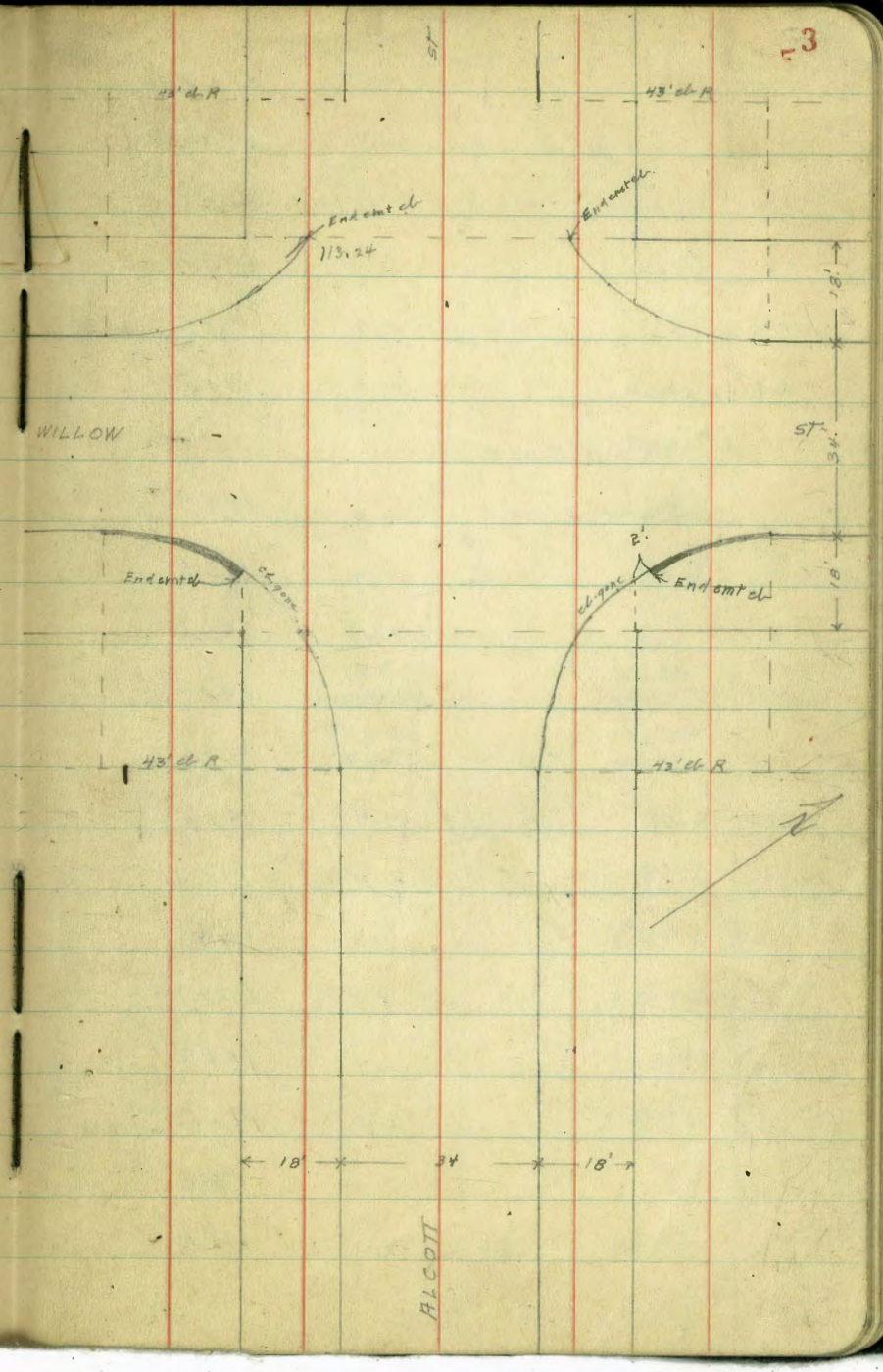
		307.67			
					50
E			11.9	295.8	
W			14.4	293.3	
TP	103	295.85	12.85	297.85	
	Sec G				
W			6.6	289.2	
C			4.3	291.5	
E			2.8	293.0	
	Sec H				
E			7.1	288.7	
			9.1	286.7	
W			13.0	282.8	
	Sec I				
W			15.2	280.6	
C			13.4	282.4	
E			14.9	282.9	
	Sec J = EC				
E			13.1	282.7	
C			13.83	287.0 = 287.0	
W			15.6	277.2	

70' ST S
18' cbs
34' Roadway

See Inlet Section of Willow & Alcott.

S-28-R7 Mills.

			V 112.64	SW. Alcott & Willow
			+113.26	
BM.	3.52	116.16	112.64	
		W Line Willow		
N. end ch Return on S 10' W. of S Line Alcot		3.54	112.62	
" " " " " N 10' S " N. Line Alcot		2.20	113.96	
		10' E. of W. Line Willow		
N. Line Alcott emt ch		1.48	114.28	
S " " " "		3.53	112.63	
		E. ch Willow ST		
S Line Alcot		3.8	1124	
S ch		4.2	1120	
℄		4.0	1122	
N. ch		3.0	1132	
N. Line		2.6	113.6	
		4' E. of E. ch		
N		3.0	1132	
ch		2.9	113.3	
℄		4.4	111.8	
+4		4.4	111.8	
+5		14.5	101.7	
+12		11.6	1046	
+13		4.5	111.7	



4' E of E el (con)

S el		4.5	111.7
+2		4.4	111.6
+4		11.1	1059
+8		11.0	105.2
+10		4.9	111.3
S. Line Alcott		4.5	111.7

8' E. of E. el

S Line = E end emt el ret		4.3	111.9
+9		6.0	1102
+10		12.3	103.9
+13		12.0	104.2
+15		4.7	111.5
el		4.4	111.8
+4		4.5	111.7
+5		11.3	1049
+12		15.5	1007
℄		10.0	1062
+5		4.5	111.7
+10		3.2	113.0
el		3.6	112.6

N. Line		2.9	1133

18' E. of E el of Willow = E. Line Willow

N Line Alcott		2.9	113.3
+10		6.0	1102
N. el		3.4	1128
+4		3.7	112.5
+5		6.3	109.9
+14		7.2	109.0
℄		16.5	99.7 (96.8)

Continued by Talman - 6-21-27.

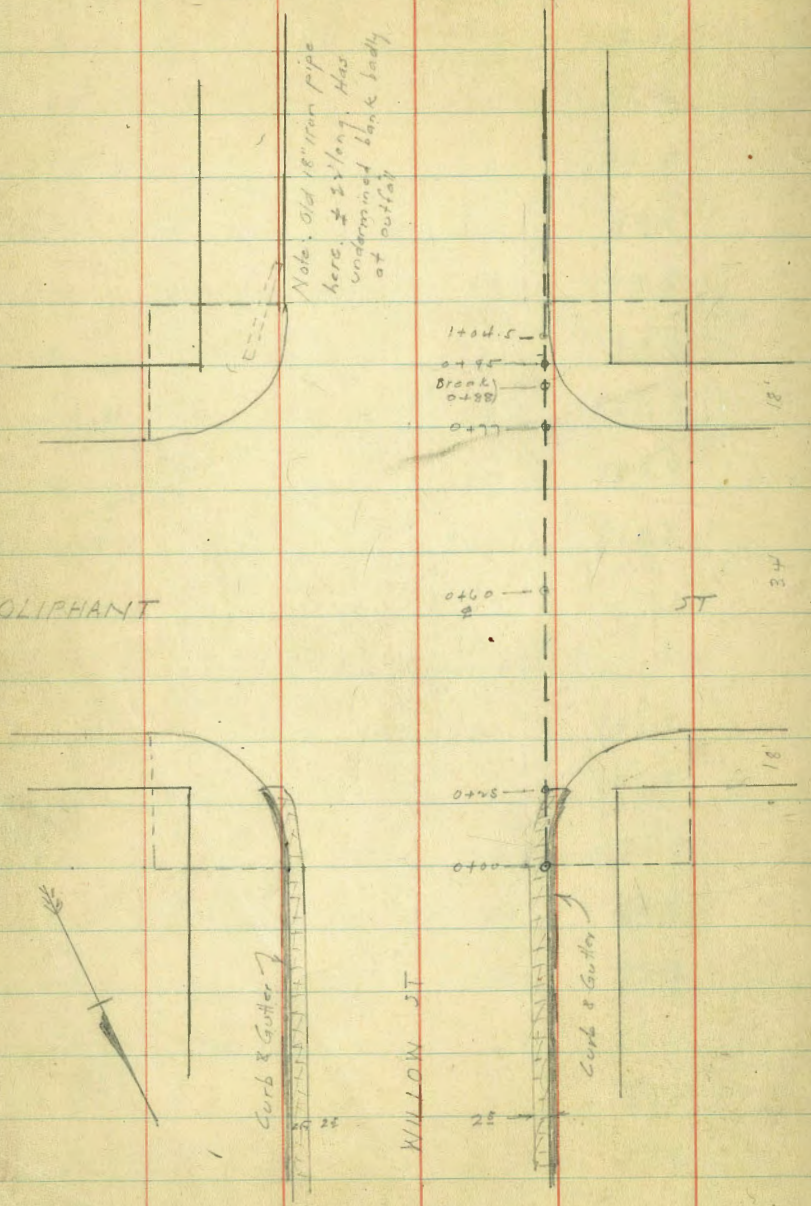
	1.90	114.54 ~~+15 +6~~	~~112.64~~ B.M Willow + Alcott
	1.10	102.76 ✓ 103.38	101.66 ~~102.28~~
℄		12.88	96.2
+2		-7.8	95.0
+9		+1.4	1042
+10		+7.0	1098
+16		+1.0	103.8
el		-4.✓	98.6
+1		0.7	102.1
+10		+2.0	104.8
S. PL Alcott		+9.0	111.8

	E.L. Willow +8		
S.L. Allcott		0.7	102.1
+5		1.6	101.2
+15		6.8	96.0
cb		6.2	96.6
+9		3.3	99.5
℄		9.6	93.4
+7		1.1	101.7
cb		0.7	102.1
N.L. Alcott		+8.0	110.8
	E.L. Willow +36		
N.L. Alcott		0.7	102.1
cb		7.3	95.5
+15		14.0	88.8
℄		17.9	84.9
+4		15.6	87.2
+8		16.2	86.6
+13		19.3	83.5
cb+8		15.2	87.6
S.L. Alcott		10.3	92.6

Elevline 12" conc. culvert Also end of it

Tolman
6-21-27

Culvert at Oliphant & Willow

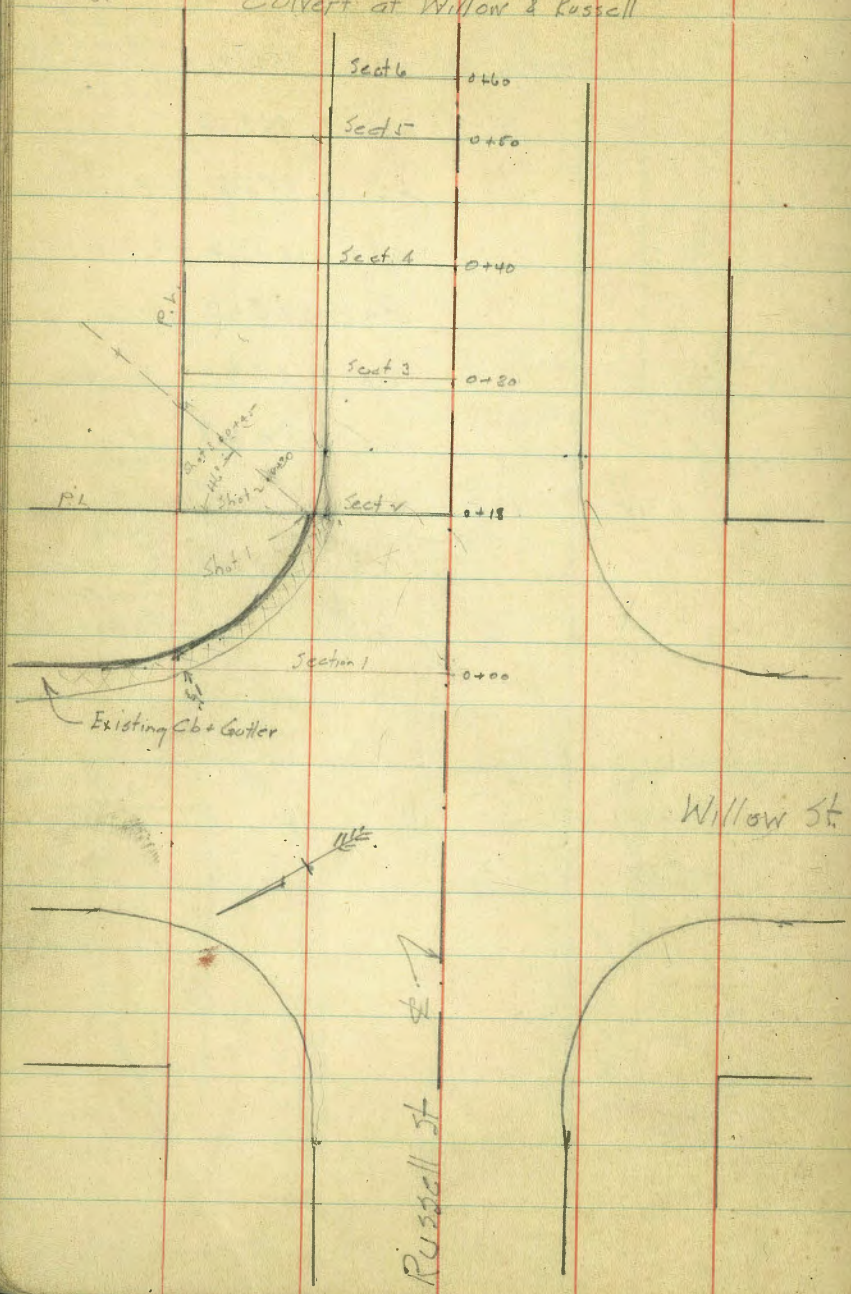


Levels

				152.81	B.M. N.W. Oliphant & Willow
	4.20	157.01			Rad. Line
0+00			1.38	155.63	Top Curb
0+25			4.2	152.8	P. Line
0+60			5.8	151.2	& Oliphant
0+77			5.7	151.3	Curb
0+88			6.0	151.0	Break
0+95			10.3	146.7	P.L.
TP	4.45	154.65	6.81	150.20	
1+04.5			15.3	139.3	Note: Same slope for 50'

Tolman
6/21-27

Culvert at Willow & Russell



Levels

	0.7 ±	161.57 ~~161.57~~	161.33 ~~161.53~~	BM SW Russell + Willow
		Section 1 = 0+00		
℄		1.2	160.4	
17' left		1.4	160.2	Cb line
35' left		1.4	160.2	P.L.
43' left		0.00	161.6	Top Curb
		Section 2 = 0+18		
℄		1.6	160.0	
17' left		2.8	158.8	Cb line
35' left		2.8	158.8	P.L.
		Section 3 = 0+30		
℄		2.2	159.4	
17' lft.		4.0	157.6	
35' lft.		5.8	155.8	
		Section 4 = 0+40		
℄		2.7	158.9	
17' lft.		5.0	156.6	
35' lft.		7.4	154.2	

	Sect 5 = 0+50			
℄		3.5	158.1	
17' Lft		5.9	155.7	
35' Lft		8.8	152.8	
	Section 6 = 0+60			
℄		4.2	157.4	
17' Lft		6.8	154.8	
35' Lft		10.0	151.6	
	Line from end of existing curb into canon. Shortest Route			
	2.08 163.41 ~~169.41~~		161.33 ~~167.33~~	BM
Shot 1 0+30		3.31	160.1	Top C6
Shot 2 0+45		10.1	153.3	
Shot 3		16.3	147.1	

1

Palmer Engineering

X section of Xenophon St bet. S.E. line of Willow St. & the N.W. line of Rosecrans.

	1x.07	148.84		136.77	B.M. Zola + Willow S.E
	10.37	158.95	0.x6	148.58	
		S.E. Line Willow St. = 0+00			
S.W.			5.1	53.8	
Tp Cb			6.07	52.88	
Gutter 3ft wide			6.68	52.27	
1/4			6.9	52.0	
℄			6.9	52.0	
1/4			7.x	51.7	
Gutter 3ft wide			7.71	51.24	
Tp Cb			7.05	51.90	
N.E line			7.4	51.5	
		+ 0x			
N.E. line			6.0	52.9	
+7			4.9	54.0	
+13			7.0	51.9	
Cb			7.0	51.9	
+2			6.9	52.0	

70' Street 19" CBS 85 %

158.95

+4		4.4	54.5
1/4		3.9	55.0
℄		3.4	55.5
1/4		3.3	55.6
Cb		3.1	55.8
S.W line		2.0	56.9
	0+60		
S.W.		2.9	56.0
Cb		3.9	55.0
1/4		4.4	54.5
℄		4.8	54.1
1/4		5.7	53.2
Cb		6.0	52.9
N.E		7.5	51.4
	1+00		
N.E		8.8	50.1
Cb		7.6	51.3
1/4		6.7	52.2

158.95

±		5.9	53.0
¼		4.6	54.3
cb		3.9	55.0
S.W.		3.2	55.7
	1+40		
S.W		5.6	53.3
cb		6.5	52.4
¼		7.1	51.8
±		7.6	51.3
¼		8.2	50.7
cb		8.3	50.6
N.E		9.8	49.1
	1+80		
N.E		11.0	47.9
cb		9.6	49.3
¼		9.8	49.1
±		9.4	49.5
¼		8.6	50.3
cb		8.7	50.2

158.95 Xenophon St 61

S.W.		7.9	51.0
	2+00		
S.W.		9.3	49.6
cb		9.7	49.2
¼		9.7	49.2
+7		10.2	48.7
±		10.7	48.2
¼		10.8	48.1
+6		11.6	47.3
cb		11.0	47.9
N.E		12.1	46.8
	1.00 147.95	12.00	146.95
	2+40		
N.E		3.8	44.1
cb		2.7	45.2
+4		3.2	44.7
1/4		2.6	45.3
±		2.5	45.4

147.95		
¼	1.8	46.1
cb	1.6	46.3
S.W	0b	47.3
	2+60	
S.W	1.9	46.0
cb	3.4	44.5
¼	3.5	44.4
+7	3.5	44.4
℄	4.2	43.7
¼	4.2	43.7
+4.5	4.4	43.5
+5.5	3.9	44.0
cb	4.3	43.6
N.E	5.4	42.5
	2+80	
N.E	6.8	41.1
cb	5.7	42.2
+3	5.9	42.0
¼	5.8	42.1

147.95	Xenophon St.	
℄	5.8	42.1
+1.5	5.3	42.6
¼	5.0	42.9
cb	4.9	43.0
S.W.	4.3	43.6
	+300 = Evergreen St. P.L.	
S.W	6.0	41.9
cb	7.0	40.9
1¼	7.0	40.9
+7	6.9	41.0
℄	7.4	40.5
¼	7.5	40.4
+5	7.8	40.1
+6	7.1	40.8
cb	7.4	40.5
N.E	7.0	38.9
	cb. Line - 18'	
S.W	10.1	37.8
cb	9.1	38.8

		147.95		
+ 3			8.9	39.1
+ 5			9.2	38.7
¼			9.1	38.8
℄			9.1	38.8
+ 1			8.7	39.2
¼			8.7	39.2
cb			8.9	39.0
N.E			8.2	39.7
T.P.	1.04	139.39	9.60	138.35
		1/4		
N.E			2.5	36.9
cb			1.5	37.9
+ 3			1.2	38.2
+ 4			1.7	37.7
¼			1.4	38.0
℄			1.4	38.0
¼			1.0	38.4
cb			1.0	38.4
S.W			1.0	38.4

		394. Xenophon St.	63
		℄ Evergreen St	
S.W		0.8	38.6
cb		1.6	37.8
¼		1.7	37.7
+ 7		1.5	37.9
℄		2.4	37.0
¼		2.1	37.3
cb		2.1	37.3
N.E		3.3	36.1
		¼	
NE		4.0	35.4
cb		2.9	36.5
+ 1		3.3	36.1
¼		3.1	36.3
℄		3.2	36.2
+ 2		2.6	36.8
¼		2.6	36.8
cb		2.4	37.0
S.W.		1.9	37.5

	139.39		
	Cb.		
S.W.		2.3	37.1
cb		3.3	36.1
1/4		3.3	36.1
+6		3.3	36.1
℄		4.0	35.4
1/4		3.9	35.5
+5		4.2	35.2
+6		3.7	35.7
cb		4.0	35.4
N.E		5.1	34.3
	P.L. Evergreen St = 0+00		
N.E		6.8	32.6
cb		5.5	33.9
+3		5.4	34.0
+5		6.0	33.4
1/4		5.8	33.6
℄		5.6	33.8
1/4		5.2	34.2
cb		5.2	34.2

	394	Xenophon St.	
S.W		4.5	34.9
	0+30		
S.W		8.0	31.4
cb		9.2	30.2
1/4		8.8	30.6
℄		9.3	30.1
1/4		9.2	30.2
+3		9.3	30.1
+5		8.6	30.8
cb		9.0	30.4
N.E		9.9	29.5
	0+50		
N.E		12.1	27.3
cb		11.3	28.1
+4		11.0	28.4
+6		11.6	27.8
1/4		11.4	28.0
℄		11.5	27.9
1/4		12.1	27.3

		139.39		
cb			11.3	28.1
S.W			11.4	28.0
T.P	1.20	12 8.71	11.88	12 7.51
		0+70		
S.W			2.1	26.6
+2			3.0	25.7
+4			4.8	23.9
+6			3.0	25.7
cb			3.6	25.1
℄			3.5	25.2
1/4			3.3	25.4
+2			3.6	25.1
+3			2.7	26.0
cb			3.0	25.7
N.E			3.6	25.1
		0+90		
N.E			6.4	22.3
cb			5.6	23.1

		28.7	Xenephon St.	
+5			5.5	23.2
+6			6.2	22.5
1/4			6.0	22.7
℄			6.1	22.6
+3			5.6	23.1
+5			7.0	21.7
1/4			5.4	23.3
cb			5.7	23.0
+1			7.3	21.4
+2			5.7	23.0
S.W.			4.9	23.8
		1+10		
S.W			7.5	21 2
cb			8.6	20.1
+3			8.5	20 2
+5			9.5	19.2
1/4			8.0	20.7
+1			8.2	20 5
+4			9.8	18.9
℄			8.6	20.1

		128.71		
¼			9.0	19.7
+¼			9.2	19.5
+4			8.3	20.4
C6			8.3	20.4
NE			8.6	20.1
		1+30		
NE			11.3	17.4
C6			10.9	17.8
½			11.2	17.5
¾			11.5	17.2
½			11.2	17.5
+2			12.0	16.7
C6			11.7	17.0
+1			10.6	18.1
S.W.			9.8	18.9
TP	0.18	118.33	10.56	118.15
		1+50		
S.W			2.8	15.5

		18.3	Xenophon St.	66
+3			4.2	14.1
C6			4.7	13.6
½			4.0	14.3
¼			3.4	14.9
½			3.5	14.8
C6			3.7	14.6
NE			2.5	15.8
		1+53		
NE			4.1	14.2
C6			4.5	13.8
½			4.4	13.9
¼			4.2	14.1
¼			4.7	13.6
C6			4.5	13.8
S.W			5.3	13.0
		1+70		
S.W.			6.8	11.5
C6			6.9	11.4
¼			7.2	11.1
¼			7.3	11.0

		118.33		
¼			6.6	11.7
cb			6.2	12.1
N E			6.1	12.2
		1+90		
N.E			8.7	09.6
cb			9.1	9.2
¼			10.8	7.5
℄			10.0	8.3
¼			10.1	8.2
cb			9.0	9.3
S.W			8.8	9.5
		2+10		
S.W.			12.6	5.7
cb			13.2	5.1
¼			13.2	5.1
℄			13.3	5.0
¼			13.1	5.2
cb			12.7	5.6
N.E.			12.4	5.9

3+00 to 1+90 Const. Ret. Wall on S.W. line

		118.33	Xenophon St	
TP	0.15	106.35	12.13	106.20
		2+50		
N E			8.6	95.8
cb			8.7	97.7
¼			9.4	97.0
℄			10.0	96.4
¼			11.0	95.4
+v			10.6	95.8
cb			10.7	95.7
S.W			9.0	97.4
TP	0.50	93.83	13.0v	93.33
		3400 - Locust St		
N E			7.0	86.8
cb			7.3	86.5
¼			7.8	86.0
℄			8.3	85.5
¼			9.3	84.5
cb			8.9	84.9
S.W			7.6	86.2

93.83

cb (18')

N.E			9.9	84.0
cb			10.6	83.2
1/4			10.9	82.9
℄			12.0	81.8
1/4			12.8	81.0
cb			12.2	81.6
S.W			11.6	82.2
T.P	0.33	81.21	12.95	80.88
		1/4		
S.W			0.3	80.9
cb			1.7	79.5
1/4			2.2	79.0
℄			1.4	79.8
1/4			0.7	80.5
cb			0.1	81.1
N.E			0.0	81.2

81.2 Xenophon St

68

℄ Locust

N.E		1.3	79.9
cb		1.5	79.7
1/4		1.9	79.3
℄		3.1	78.1
1/4		3.9	77.3
+1.5		4.8	76.4
+4		3.8	77.4
cb		3.3	77.9
S.W		2.1	79.1
	1/4		
S.W		3.8	77.4
cb		6.1	75.1
1/4		6.2	75.0
℄		5.0	76.2
1/4		4.2	77.0
cb		3.6	77.6
N.E		4.5	76.7
	cb		
N.E		5.4	75.8

		81.21		
cb			5.6	75.6
1/4			6.3	74.9
℄			7.3	73.9
1/4			7.8	73.4
cb			7.9	73.3
S.W.			5.8	75.4
		Pl Locust St. = 0+00		
SW			9.3	71.9
+14			11.6	69.6
+16.6			11.2	70.0
+17.6			14.2	67.0
cb			11.7	69.5
1/4			11.6	69.6
℄			11.1	70.1
1/4			10.7	70.5
cb			10.1	71.1
N.E.			9.6	71.6
T.P	0.63	695.2	12.32	68.89

Xenophon St

		69.52		
		0+40		
N.E			6.0	63.5
cb			6.4	63.1
1/4			8.0	61.5
℄			7.9	61.6
1/4			8.7	60.8
+3			11.3	58.2
+5			9.0	60.5
cb			8.6	60.9
S.W.			6.2	63.3
T.P	2.18	59.85	11.85	57.67
		0+80		
S.W			5.0	54.8
+16			7.2	52.6
cb			10.0	49.8
+3			7.2	52.6
1/4			7.0	52.8
℄			6.7	53.1
+1			5.4	54.4

		59.85		
¼			4.7	55.1
cb			4.1	55.7
NE			3.6	56.2
TP	1.88	49.26	12.47	47.38
		1+20		
NE			4.5	44.8
cb			4.4	44.9
¼			4.5	44.8
℄			5.0	44.3
¼			5.2	44.1
+4			5.0	45.3
+6			7.2	42.1
cb			5.6	43.7
+7			4.4	44.9
S.W			4.0	45.3
T.P	0.18	37.31	12.13	37.13

37.3 Xenophon 54

		1+60	
SW		3.3	34.0
+14		2.9	35.4
cb		2.2	35.1
+2		1.8	35.5
¼		1.4	35.9
℄		1.5	35.8
¼		1.2	36.1
cb		0.9	36.4
N.E.		0.9	36.4
	2+00		
NE		5.9	31.4
cb		6.3	31.0
¼		6.2	31.1
℄		6.2	31.1
¼		6.1	31.2
+4		6.4	30.9
+6		7.2	30.1
cb		7.6	29.7
N.E.		7.4	29.9

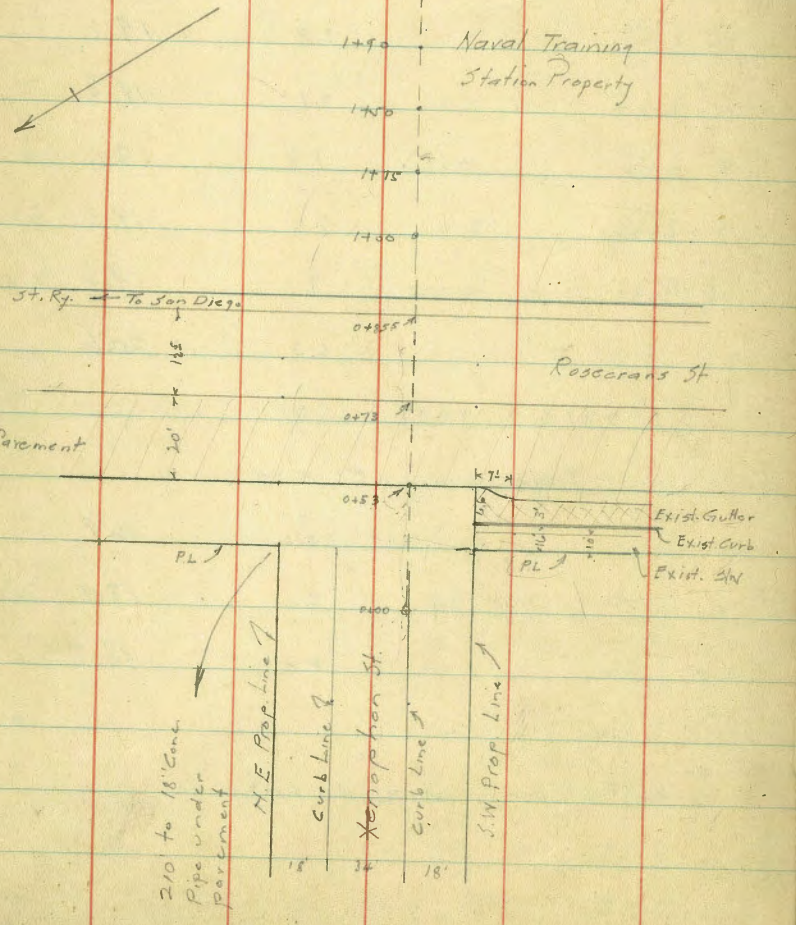
1+75 to 3+00 Rubble Wall on SW. line

		37.31		
		2+40		
SW			12.4	24.9
℄ 14			12.9	24.4
+ 15			13.9	23.4
+17			12.5	24.8
cb			12.1	25.2
1/4			11.5	25.8
℄			10.9	26.4
1/4			10.7	26.6
cb			10.5	26.8
N.E			10.4	26.9
TP	0.43	36.92	10.87	26.49
		2+85		
XE			3.5	23.4
cb			4.1	22.8
1/4			4.3	22.6
℄			5.5	21.4
1/4			5.5	21.4
+2			6.4	20.5

26.9 Xenophon St

cb	7.5	19.4
SW	6.6	20.3
P.L. Rosecrans St = 3+00		
SW	8.7	18.2
cb	8.3	18.6
+2	7.8	19.1
1/4	7.1	19.8
℄	7.3	19.6
1/4	7.6	19.3
cb	7.3	19.6
NE	6.3	20.6
Edge paving = P.L. + 20'		
SW	10.0	16.9
℄	9.0	17.9
N.E	8.2	18.7
See drainage on next page		

Drainage at Rosecrans & Xenophon



	4.36	12.87		18.01	BM Rosecrans & Xenophon
0+00			1.3	21.1	
0+53			4.7 ±	17.65	Top Paving
0+73			4.80	17.6	" "
0+85.5			5.0 ±	17.35	Top Rail
1+00			6.0	16.4	
1+15			7.2	15.2	
1+50			6.7	15.7	
1+90			10.1	12.3	

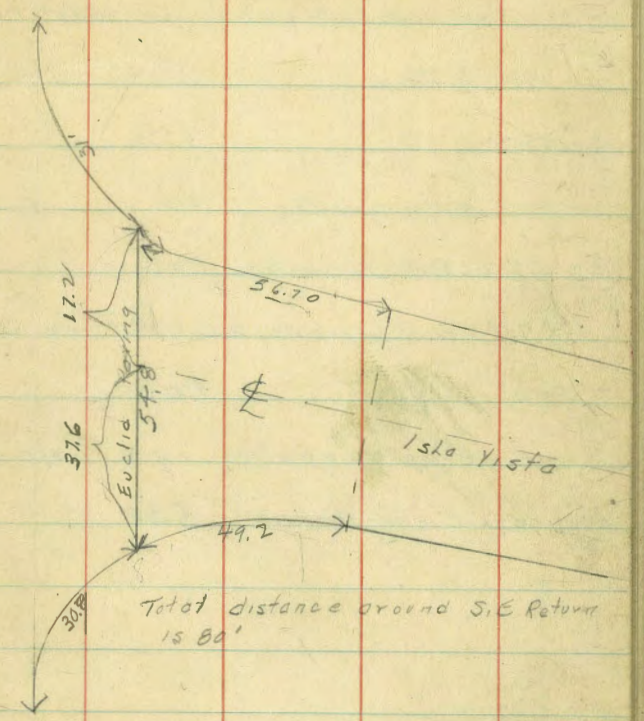
9-26-28
J.C. Bliss
Dreber
Rauner

Levels at Intersection of Euclid and Isla Vista - Sketch next page

B.M. N.E. B.P. - Lantana + Euclid			340.46
	+7.98	348.44	
		-8.56	339.88
	+0.61	340.49	
		-8.03	332.46
	+4.95		
		T 337.41	

Levels around S.E. Return, beginning 0+00 at South P.C.

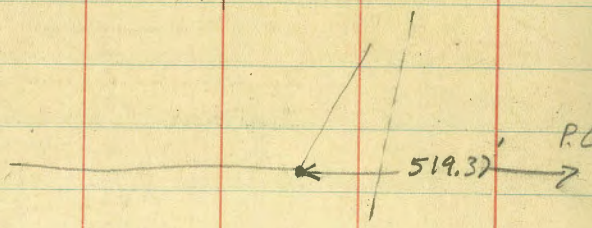
0+00 Top	3.98	333.43
Gutter	4.44	332.97
0+20 Top	3.96	333.45
Gutter	4.43	332.98
0+30.8 = East edge Euclid Parking Top	3.97	333.44
Gutter	4.23	333.18
0+40 Top	3.95	333.46
0+60 Top	3.97	333.44
0+80 = East P.C. Return	4.00	333.41
N.E. Return 0+00 = North P.C.		~~331.96~~
0+00 Top	5.45	331.96
Gutter	5.89	331.52



T 337.41

0+15.5 = center N.W. Return-Top	5.40	332.01
Gutter	5.71	331.70
0+31 = East edge Euclid paving and East P.C. of Return-Top	5.49	331.92
Gutter	5.72	331.69
0+48.5 - Brk in curb-Top	4.41	333.00
0+68.6 = Brk in curb-Top	3.95	333.05
0+87.7 = Point opposite East P.C. of S.E Return Top	4.03	333.38
Shot at intersection of ℄ Isla Vista and East edge Euclid Paving	5.30	332.11

2172.98 — Recovd.
2135 — approx. asrun.



66.0 No 4

26.9
9.1
11.80

18.01
17.8
.21

93.83
12.95
80.88
33
81.21
12.32
68.89
63
69.52
11.85
57.67
2.18
59.85
12.47
47.38
1.88
49.26
12.13
37.13
18
37.31
10.8
26.49

173

118.6

59.3

118.33
13.02
105.31

105.81
4.90
100.91

13.26
1.90
15.16
12.98
0228

10
√0
25
30
40
25
28

Eureka Springs

Keokuk

Waterloo - Rochester

Table IX.—Calculation of Earthwork.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if w =16.2 and h =5.3, cu. yds. =1.48+.028+.089 =1.597 cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) =h, and ½ the roadbed =w, add the triangles formed by taking the distance out to each break in turn (=w's) by the difference between the cuts (or fills) on each side of it (=h's) always subtracting the outer from the inner.

Distances from Center of Roadway for Cross-Sectioning.

Roadway 16 feet wide. Side Slopes 1 on 1½.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	25.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be 41.9+(20—16)÷2 or 2 ft. added to 41.9 =43.9. For slopes of 1 on 1 see inside of front cover.

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