

1153

FIELD BOOK

361

CITY OF
SAN DIEGO - CALIFORNIA
ADDITIONAL WATER SUPPLY
EL CAPITAN DAMSIT

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.
FOR SINGLE TRACK EXCAVATION.

" Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

FOR KEITH'S RAILROAD CURVE TABLES SEE END OF BOOK.

1126

CITY OF
SAN DIEGO - CALIFORNIA
ADDITIONAL WATER SUPPLY

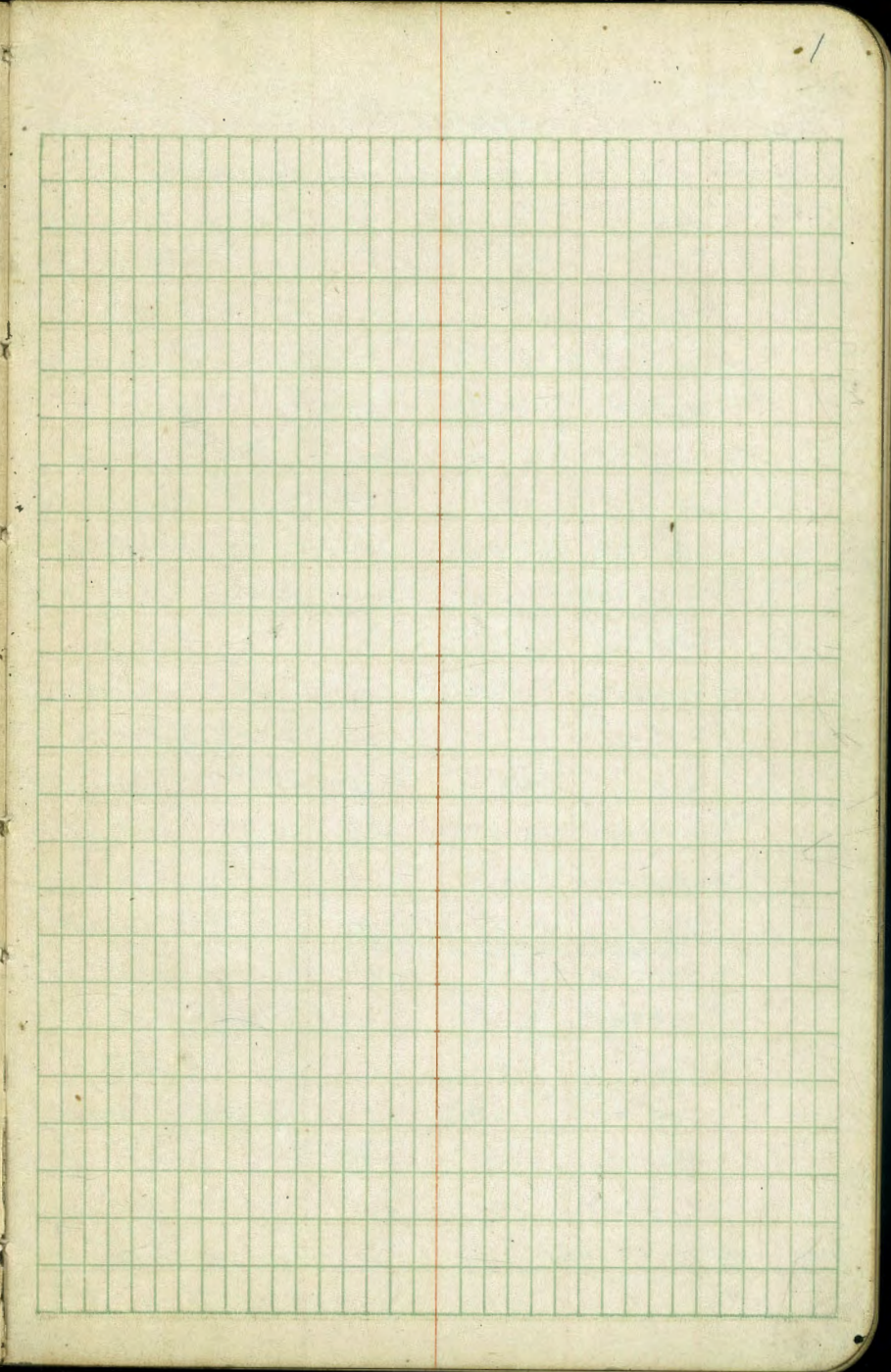
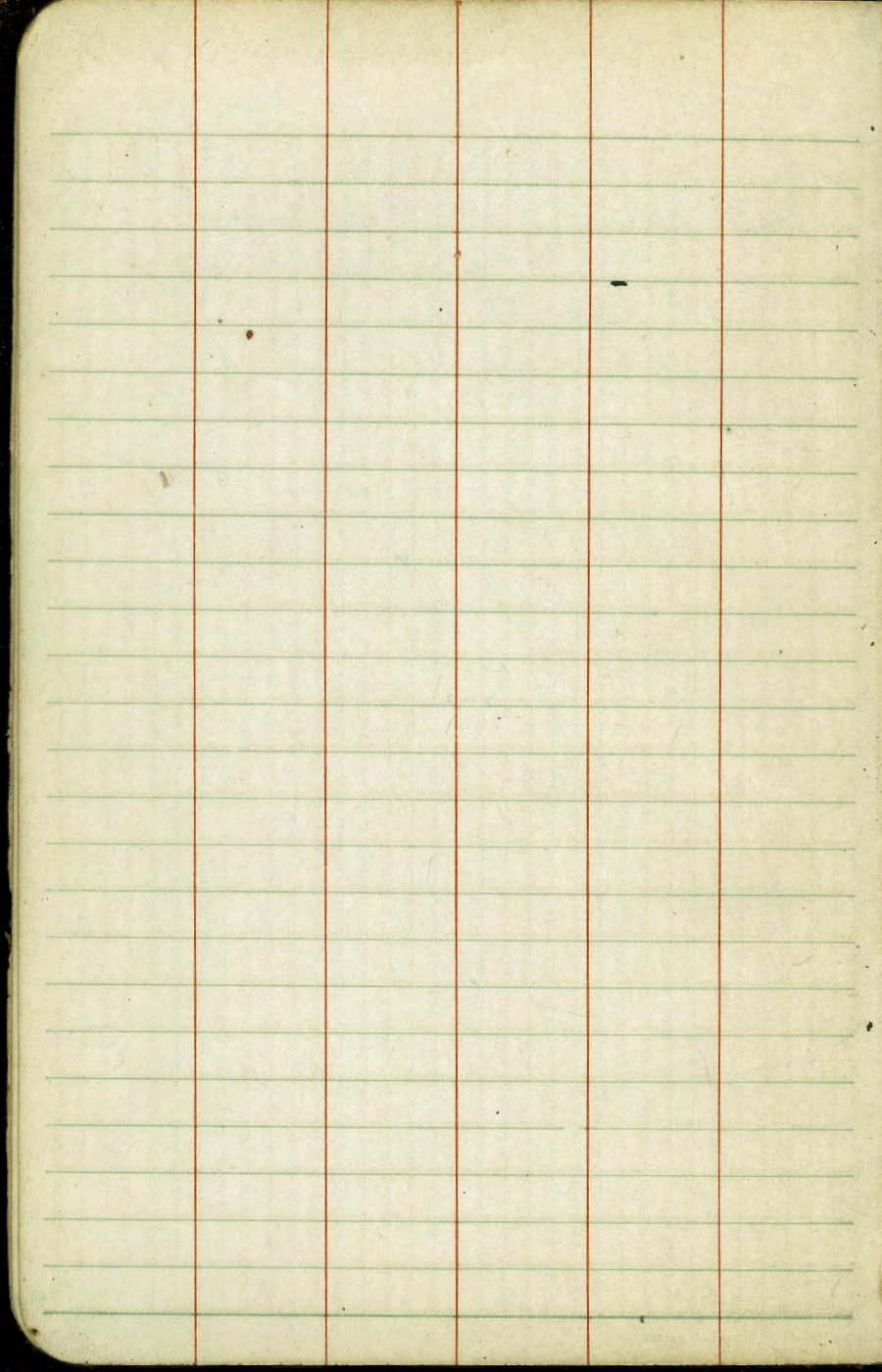
Aug - 1921

H.N. Savage
Hydraulic Engineer

No. 1000

MICROFILMED

Tunnel Line - Eucalyptus Pass	2-14
El Capitan Dam site #2 - Additional Topography	15-28
" " #2 Location of Core Drill holes	29-30
List of BIMs - County Highway	60



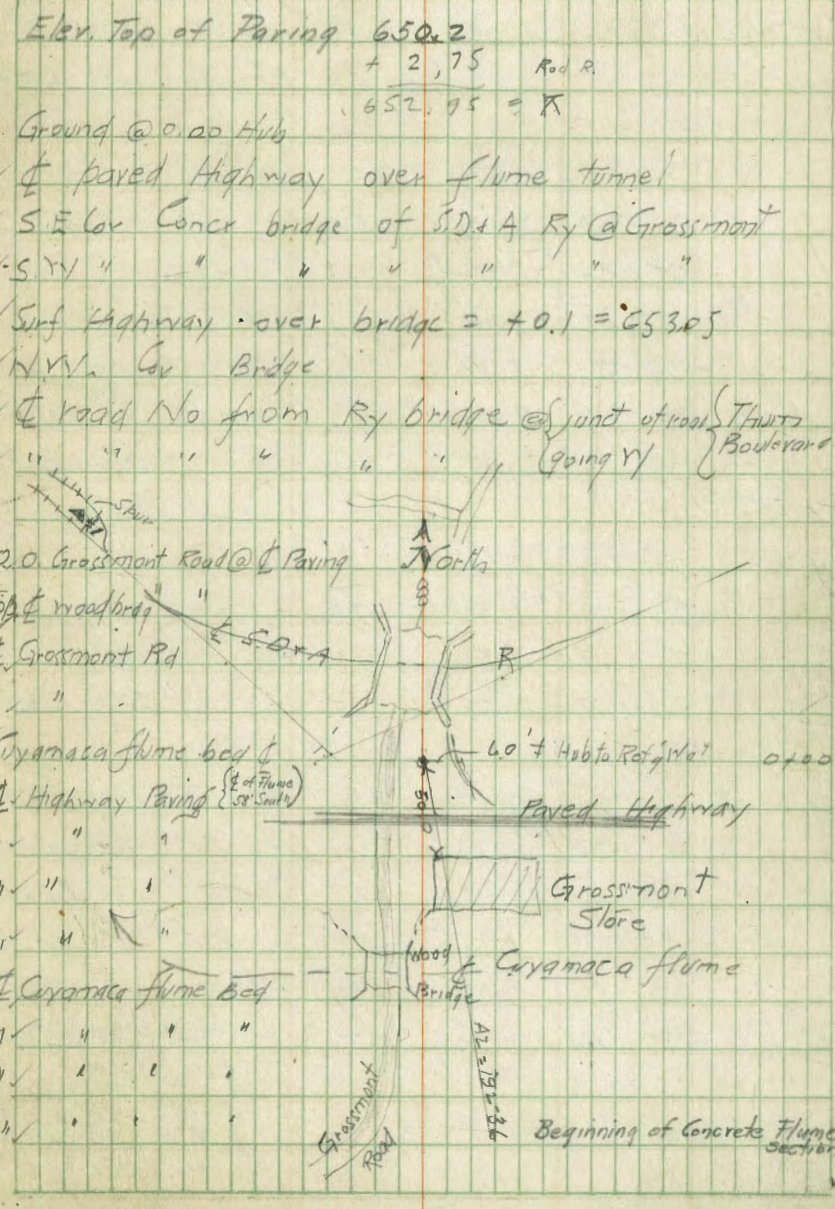
Az Rod Hor Dist Vert \angle

Hayler Multiply Rod Readings by 1.025 (const) 2
 Franklin +c = 1.04
 Williams
 True - North = 0 of Azimuth. Var. = 14° 30' 8-26-21

Tunnel Line - Eucalyptus Pass

Sta 0+00 - B.S. on Center of Paving directly over flume

Sta	Az	Rod	Hor. Dist	Vert. \angle	El. Elev.	El. Elev.
0+00	50°				647.95	
	284-26					
	10-23	0.26	28.			
	342-20	0.33	35.			
	0-23	0.60	62.			
	18-19	0.55	57.			
	18-22	1.84	185.	+1-03	+3.4	651.4
	28-19	4.23	435.	+2-58	+22.5	670.5
	192-36	0.50				
	239-38	0.33	36.	-2-20	-1.5	646.5
	217-18	1.08	112.	+1-28	+2.9	650.9
	214-20	2.32	239.	+1-19	+5.5	653.5
	223-41	3.35	344.	+1-56	+11.6	659.6
	200-27	1.01	104.	-1-40	-3.0	645.0
	112-01	3.45	355.	-1-27	-9.0	639.0
	288-22	1.72	176.	+0-8'	+0.4	648.4
	289-20	2.58	265	+0-21	+1.6	649.6
	278-52	4.40	452	+0-23	+3.0	651.0
	263-35	2.35	242	-0-54	-3.8	644.2
	280-24	3.26	335.	-0-33	-3.2	644.8
	296-12	4.75	488.	-0-25'	-3.5	644.5
	302-52	6.25	642.	-0-23	-4.3	643.7
	308-24	6.23	640.	-1-07	-12.5	635.5



To Δ + 1308-24
 Sec 7

Sta	Ass	Az	Rod	Hor. Dist	Vert	L	Diff. Elev.	Elev.
π@Δ-3		208-58	1.22	125.	-4-29	-9.8	589.3	
		174-05	0.49	47.	-16-56	-14.2	584.9	
		121-27	0.51	47.	-18-32	-15.7	583.4	
		75-0	0.89	88.	-12-55	-20.2	578.9	
		58-27	1.77	179.	-7-25	-23.3	575.8	
		49-0	2.14	218.	-6-28	-24.7	574.4	
		56-104	2.82	287.	-5-41	-28.4	570.7	
		55-25	3.50	356.	-5-25	-33.6	565.5	
		54-33	3.96	403.	-4-54	-34.3	564.8	
Δ-3 1/2 Δ-4		48-58	4.73	483.	-4-0	-33.7	565.4	
		71-35	3.86	396.	-2-49	-19.5	579.6	
		79-36	3.22	330.	-2-34	-14.8	584.3	
		162-47	1.94	200.	+1-52	+6.5	605.6	
		185-42	2.29	235	+2-55	+11.9	611.0	
π@Δ-4	45	266-36	1.54	155.	+8-33	+23.3	588.7	
		340-0	1.29	127.	+11-55	+26.8	592.2	
		17-37	2.45	252	+3-08	+13.8	579.2	
		184-43	0.47	49	-2-04	-1.8	563.6	
		71-13	0.57	57.	-6-48	-6.8	558.6	
		57-45	1.23	125.	-3-49	-8.3	557.1	
		49-20	1.85	190.	-3-0	-10.0	555.4	
		52-27	2.90	298.	-2-25	-12.5	552.9	
Δ-4 7/8 Δ-5		53-29	5.05	520	-1-55	-17.3	548.1	

✓	Wash	Sta-12+26.9	B.S.-9+69.8
✓	"		
✓	"		
✓	"		
✓	on flat		
✓	Wash		
✓	"		
✓	"		
✓	on flat	Sta-17+10.4	(584.4)
✓	Highway		
✓	"	Tarp	
✓	"	EC	
✓	"	POC	
✓	Sta-17+10.4	B.S. Sta-12+26.9	EC Ry POC
✓	POC	Ry.	"
✓	POC	"	"
✓	Wash		
✓	"		
✓	"		
✓	"		
✓	"		
✓	Sta-22+28.5		

Sta	Az	Rod	Hor Dist	Vert. /	Diff	Elev
π@ -5	44				El.	578.1
267-04	2.66	271.	+6-0	+28.5	576.6	✓
291-09	4.72	175.	+5-38	+26.5	574.6	✓
328-11	1.31	191.	+9-25	+21.7	569.8	✓
9-49	1.60	162.	+6-38	+18.9	567.0	✓
32-21	2.30	235.	+3-55	+16.0	564.1	✓
50-20	4.20	431.	+1-52	+14.1	562.2	✓
55-07	5.75	590.	+0-34	+5.9	554.0	✓
131-41	4.37	141.	-1-51	-4.5	548.6	✓
138-31	1.15	119.	-1-50	-3.8	544.3	✓
148-32	1.39	143.	-0-35	-1.6	546.5	✓
29-22	0.67	69.	+3-07	+3.7	551.8	✓
301-27	0.35	36.	+7-11	+4.5	552.6	✓
235-53	1.30	134.	+2-47	+6.5	554.6	✓
247-04	1.20	124.	+1-05	+2.3	550.4	✓
233-18	0.90	93.	+0-50	+1.4	549.5	✓
237-46	0.46	48.	+0-12	+0.2	548.3	✓
69-32	1.44	148.	-1-30	-3.9	544.2	✓
72-03	2.41	247.	-1-47	-7.8	540.3	✓
73-47	3.24	332.	-2-02	-10.9	537.2	✓
73-54	4.35	447.	-1-53	-14.7	533.4	✓
76-19	5.65	580.	-1-56	-19.5	528.6	✓
-576-673-53	6.23	640.	-1-29	-16.5	531.6	✓

Sta-22+285

✓ R.

✓ "

✓ "

✓ "

✓ R.O.T. EC.

✓ RY BC

✓ "

✓ N.E. Cor Twin Bungalow

✓ N.W.

✓ S.W.

✓ Highway

✓ "

✓ "

Low Bridge
Concr Box Coff 3' x 10'

✓ Wash

✓ "

✓ "

✓ "

✓ "

✓ "

Sta-28+67.7 ✓

Sta	Az	Rod	Hor Dist	Vert L	Diff Elev	Elev.
π@A- ⁴²⁵ G	136-31	0.56	.57	-6-25	-6.4	537.6
	103-30	1.25	128.	-3-42	-3.7	527.9
	"	1.82	186.	-3-0	-9.7	521.9
	138-33	1.15	118.	-3-54	-8.1	523.5
	180-05	1.16	119.	-2-27	-5.1	526.5
	212-22	1.90	195.	-0-13	-0.7	530.9
	92-21	2.85	291.	-2-40	-13.5	518.1
	89-03	4.35	446.	-2-05	-16.2	515.4
	80-36	5.72	587.	-1-57	-20.0	511.6
	83-34	6.75	692.	-1-52	-22.7	508.9
	84-28	7.17	735.	-1-46	-22.7	508.9
	85-49	8.00	822.	-1-43	-22.2	509.4
	87-47	8.60	883.	-1-53	-29.0	502.6
	(?) 86-15	9.40	965.	-1-52	-31.5	500.1
38+661	86-54	9.75	1000.	-1-48	-31.4	500.2
	48-30	4.75	488.	-0-19	-2.7	528.9
	47-31	4.45	457.	-0-14	-1.8	529.8

Sta-28+67.7 BS on -22+285 Shot is in Wash

Wash

Wash Junction with Small Wash from So.

Wash from So

" " " "

" " " "

Main Wash

" " "

" " "

" " "

of Earth Road

of Wash

" " "

" " "

" " "

Junct. Ea. Road + Paved Highway

BC Highway Curve to Lt

Eng Line to East

Sta	AZ	Rad	Hor Dist	Vert L	Diff Elev	Elev.
T@A ¹ Sec bot. p ^o 2	50				-12.5	635.5
336-34	0.41	43.	+0-12	+0.2	635.7	
94 0	0.16	17.	+1-15	+0.4	635.9	
131-37	1.37	141.	+0-50	+2.1	637.6	
289-26	0.23	24.	0	0	635.5	
305-40	1.44	148.	-0-46	-2.0	633.5	
289-54	2.16	222.	+2-52	+11.6	647.1	
271-49	1.14	117.	+4-56	+10.1	645.6	
306-54	2.12	225.	-0-55	-3.6	631.9	
307-52	3.82	393.	-0-56	-6.4	629.1	
308-20	4.15	426.	-0-56	-6.9	628.6	
308-37	4.90	504.	-0-57	-8.4	627.1	
308-25	5.96	612.	-1-08	-12.1	623.4	
A ¹ to A ²	313-02	628.	-0-29	-5.4	630.1	
		3.				
T@ 2	177-85	30	301	+3-10	+1.7	631.8
	225-18	261	267.	+3-52	+18.0	648.1
	252-16	2.50	257.	+3-16	+15.2	645.3
	191-07	2.15	221.	-1-30	+5.8	635.9
	214-28	0.61	62.	-8-22	-9.1	621.0
	288-06	0.85	86.	-7-07	-10.7	619.4
	320-36	2.15				
	315-13	2.35	241.	-3-21	-14.1	616.0
	320-35	3.40	349.	-2-31	-15.3	614.8
	322-41	4.60	471.	-2-06	-17.2	612.9

See p. 2. Line r/cst

Sta. 6+39.3 Tack So side Spur on tie

SE Car Grossmont Ry Sta. Par. to tie 18x42

SE " " Freight Platform B' No. 10x30

Frog Point N Rail for Siding spur @ Sta

✓ R₁

✓ " "

Fletcher BM 638.15 on Concr intake to Pipeline (Reservoir)

✓ " " Hume East End Trestle

✓ R₁ P.O.T.

✓ AC

Point frog West End Siding

✓ R₁ P.O.C @ H.B. of Siding

✓ P.I. of Curve on R₁

Sta 12+84.3

✓ End of Dam E

" " " W

✓ West End Trestle

✓ bot elev @ toe of dam

drainage

" end

✓ R₁ BC

drainage + So side ditch R₁

" "

" "

Trestle is Tangent no Curve

Wily Pond

Sta	Az	Rod	Hor. Dist.	Vert L	Diff Elev	Elev.
π @ Δ ^{#2}	326-09	4.87	500.	-1-44	-15.2	630.1 614.9
	324-44	6.20	636.	-1-51	-20.5	609.6
#2 to #3	324-51	7.20	740.	-1-27	-18.7	611.4
+ 3						
π @ Δ ^{#3}	113-41	0.43	45.	-0-41	-0.5	610.9
	0-88	0.50	51.	-5-07	-4.5	606.9
	337-05	0.85	88.	-7-34	-2.4	609.0
	346-55	1.01	104.	-3-35	-6.5	604.9
	326-42	1.81	186.	-1-11	-3.8	607.6
Δ ^{#3} to Δ ^{#4}	323-58	3.12	321.	-0-42	-3.9	607.5
+ 65						
π @ Δ ^{#4}	221-20	0.16	17.	-9-19	-2.8	604.7
	301-14	1.45	149.	-2-03	-5.3	602.2
	95-03	1.68	173.	-1-55	-5.8	601.7
	51-29	1.05	108.	-4-21	-8.2	599.3
	353-42	1.87	192.	-2-55	-9.8	597.7
	317-36	2.32	238.	-2-54	-12.1	595.4
	306-50	2.58	265.	-2-42	-12.5	595.0
	301-36	2.81	289.	-1-31	-7.9	599.6
Δ ^{#4} to Δ ^{#5}	302-00	6.35	652.	-1-00	-11.4	596.1

See p. 9

✓ Ry E.C.
 Drainage
 20722.8 ✓
 " ✓
 ✓ Ry over Bridge #25 = 16' Stringer Bridge (Drainage Crossed to No Side)
 Drainage
 ✓ Ry P.O.C.
 Drainage
 ✓ Ry P.O.C.
 Sta. 23+43.6 ✓
 " ✓
 ✓ Ry P.O.C.
 " " " ✓
 ✓ Drainage
 " ✓
 " ✓
 ✓ " @ Junction Small wash from No.
 Drainage
 ✓ Ry P.O.C.
 Sta 29+95.3 (5859) ✓

Sta	Az	Rod	Hor. Dist.	Vert L	Diff Elev	Elev
^{A*4} T@23+436						607.5
89-35	12.17	✓	1247.	+1-56	+42.0	649.5
66-28	13.45		1380.	+1-54	+45.7	653.2
79-A2	11.50		1180.	+0-33	+11.2	618.7
77-35	4.50		462.	+0-36	+4.8	612.3
169-09	6.00		615.	+3-34	+38.3	645.8
181-54	4.90			Not Visible		
191-50	3.32		336.	+6-25	+37.8	645.3
210-02	2.80		283.	+7-30	+37.3	644.8
233-39	3.03		306.	+6-54	+37.1	644.6
257-0	4.83		494.	+4-14	+32.5	644.0
						<u>Elev Δ5 = 596.1</u>
^{A*5} T@ Δ5	121-13	1.57	162.	-1-20	-3.8	592.3
	131-06	1.63	168.	+0-14	+0.7	596.8
	181-08	0.65	67.	-1-06	-1.3	594.8
	180-08	0.43	44.	-7-03	-5.4	590.7
	253-35	0.26	99.	-3-52	-6.7	589.4
	245-30	1.04	107.	-1-36	-3.0	593.1
	201-10	4.35	441.	+6-19	+48.8	644.9
	218-10	5.25	534.	+5-20	+49.6	645.7
	274-22	2.20	226.	-2-24	-9.5	586.6
	271-31	3.75	385.	-1-35	-10.6	585.5
	278-56	5.55	570.	-1-17	-12.8	583.3
	281-37	7.45	765.	-1-16	-17.0	579.1
	282-36	9.20	944.	-1-07	-18.5	577.6

Side Line East or to Rt for Reservoir S.8 9
11.6

BS on 20+225

Sat 7/27/21

✓ On So of End of Top of Dam

✓ " No " " " " "

✓ Drainage @ lower side W Toe of Dam { 15' W. of T
2.1' Slopes
Both Sides

✓ " from Dam

✓ Fletcher Flume P.O.C. →

" " " " "

" " " " "

" " " " "

" " " " "

" " " " "

SI

SI 29+953 No side Ditch @ Ry = Drainage

✓ Ry P.O.C.

✓ " " " " "

No side Ditch at Ry

" " " " "

✓ BC on of Ry

✓ Fletcher flume

" " " " "

" " " " "

Drainage

✓ " " " " "

✓ " " " " "

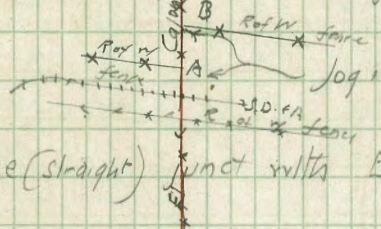
✓ " " " " "

✓ " " " " "

Sta	Az	Rod	Hor Dist	Vert	P.H. Elev	Elev
π@ #5						596.1
#5 to #6	272-47	9.74	998.	-1-04	-18.6	577.5
π@ #6 5'						
	348-07	Δ6 is on line of fence whose Az = 344-07				
"	0.15	15.	-9-55	-2.6	574.9	
"	0.25	26.	+1-0	+0.5	578.0	
"	0.22	75.	+2-0	+2.6	586.1	
	168-07	0.42	44.	+0-31	+0.4	577.9
	255-18	0.33	35.	+4-33	+2.8	580.3
	287-48	1.27	131.	-1-39	-3.8	573.7
	275-14	1.34	138.	+0-32	+1.3	578.8
	275-46	3.21	330.	+0-20	+1.9	579.4
	286-52	3.23	332.	-0-57	-5.5	572.0
	292-14	4.32	443.	-1-0	-2.7	569.8
	281-29	5.90	605.	-0-58	-10.2	567.3
#6 to #7	270-20	10.20	1046.	-0-08	-2.4	575.1

Sta	Az	Rod	Hor Dist	Vert	P.H. Elev	Elev
π@ #7 44						
	90-55	2.50	257.	-2-34	-11.5	563.6
	87-31	5.82	596.	-0-04	-0.7	574.4
	88-12	4.15	426.	-0-33	-4.1	571.0
	97-59	2.50	257.	-1-27	-6.5	568.6
	131-45	1.35	139.	-3-50	-9.3	565.8
	138-43	1.08	110.	-5-40	-10.9	564.2
	209-16	1.66	169.	-6-09	-18.2	556.9
	230-29	2.80	285.	-3-58	-19.7	555.4

Sta 39+95.3						
Sta 39+94.3	Ry Spike	El Cajon Trail	W. State 4 1/2 No			
"	Drainage	No 16'				
Fence Line	W boundary	Line El Cajon Rancho				
Drainage						
fence Cor. #A						
" "	#B					
So Rd of fence (straight)		Junct with	El Cajon Rancho Line			
E.C. of Ry						
Drainage						
P.O.C Ry						
" "						
Drainage						
" "						
" "						
Sta. 50+40.8					564.9	
"						
Drainage						
Ry P.O.C						
" "						
" "						
" "						
" "						
Drainage						
" "						
" "						



Sta	Az	Red	Hor Dist	Vert %	Diff. Elev.	Elev.
						575.1
	231-23	3.85	390.	-3-0	-20.4	554.7
	229-42	4.12	423.	-2-21	-17.8	557.3
#7 to #8	250-16	6.10	625.8	-1-38	-17.8	557.3
K @ #8		1				
	124-33 ⁴²⁵	1.18	122.	-2-15	-4.8	552.5
	187-30	1.15	118.	-3-04	-6.3	551.0
	195-46	0.96	98.	-4-54	-8.4	548.9
	214-05	1.28	131.	-3-52	-8.7	548.4
	235-22	2.06	213.	-2-55	-10.9	546.4
	247-08	3.25	334.	-2-06	-12.3	545.0
#8 to #9	251-35	7.48	767.7	-0-3	-0.7	556.6
K @ #9	435					
	83-02	2.85	293.	-2-25	-12.4	544.2
	107-40	"	293.	-2-34	-13.1	543.5
	126-54	2.14	219.	-4-14	-16.2	540.4
	128-36	2.45	252.	-2-32	-11.1	545.5
	75-22	0.75	78.	0	0	556.6
	167-13	1.93	197.	-4-55	-16.9	539.7
	202-05	2.80	286.	-3-57	-19.7	536.9
	214-47	3.55	363.	-3-02	-19.3	537.3
	230-55	4.80	492.	-2-41	-23.0	533.6
#9 to #10	251-24	7.06	724.6	-0-44	-9.3	547.3
K @ #10 ⁴²⁵						
	94-19	1.08	108.	-2-10	-17.4	529.9
	210-55	1.14	114.	-2-56	-20.0	527.3

Drainage
 Ry P.O.T.
 Sta 56+66.6
 " BS #7 5040E
 Drainage called wash hence easier to write
 wash So side
 " No "
 " " " So Side Invisible brush
 " " " " "
 " " " " "
 Sta 64+34.3
 " "
 Wash coming in from North
 Main Wash
 " "
 Intensed of 17ftch of 36" Rbel inc + Ry of
 of Top Fletcher 36" RL.
 Wash
 "
 "
 "
 Sta. 71+58.9
 "
 Main Wash
 "

Ry Long Tang

Sta	A2	Red	Hor Dist	Vert	Cor. Elev	Elev.
T@ *13 4 ⁹						<u>591.9</u>
*13 to *14	<u>141-15</u>	4.02	420.2	+0-39	+4.7	596.6
T@ *14 4 ¹		5.00				
*14 to *15	<u>173-13</u>	5.00	508.4	-5-46	-5.4	<u>595.2</u>
T@ *15 4 ¹						
	98-32	6.10	626.	+0-58	+10.6	555.8
	99-53	4.85	498.	+0-46	+6.7	551.9
	102-12	3.60	370.	+0-27	+3.0	548.2
	107-0	2.18	224.	-0-22	-1.4	543.8
	120-46	1.05	108.	-2-17	-4.3	540.9
	223-27	0.74	76.	-6-22	-8.5	536.7
	247-43	2.00	205.	-3-04	-11.0	534.2
	252-29	3.21	330.	-2-29	-14.3	530.9
	254-33	4.97	510.	-1-58	-17.5	527.7
	253-37	6.60	677.	-1-48	-21.3	523.9
	252-33	8.00	820.	-1-38	-23.4	521.8
*15 to *16	<u>251-56</u>	9.48	972.4	-1-02	-17.5	<u>527.7</u>
T@ *16 4 ³						
	89-35	0.73	75.	-6-14	-8.2	519.5
	176-22	4.15	117.	-5-42	-11.6	516.1
	183-17	1.95	200.	-4-06	-14.3	513.4
	198-52	2.45	251.	-3-31	-15.4	512.3
	218-44	3.40	349.	-3-12	-19.5	508.2
	232-17	3.75	385.	-3-08	-21.0	506.7
	244-39	4.25	435.	-3-19	-25.1	502.6

Sta 90+04.5	
Sta 94+24.7	F.S. N side Stand Pipe ✓
"	
Sta 99+33.1	(545.0) ✓
✓ & slash 1st shot in this wash	
✓ " "	
✓ " "	
✓ " "	
✓ " "	
✓ " "	
✓ " "	
✓ " "	
✓ " "	
✓ " "	
✓ " "	
Sta 109+05.5	✓
✓ & same slash	
✓ " "	
✓ " "	
✓ " "	
✓ Main Wash junction ends above reach	
✓ " " below junct	
✓ " " " "	

"X" E1 CAPITAIN Damsite #2
Additional Topography H.I.

Sta	Az	Rod	Hor Dist	Vert L
π@ 76+288 Williams station				
0+00 "X" 4.87		4.87	563.25	558.38
	2.05	2.04	+3°-39'	+13.70R 571.46
				592 557.33
to ✓ 0+91-18	4.82	4.74	+20°-02'	1/2 155.55
to ✓ 0+11-18	5.80	5.34	+16°-22'	+15.71
to 0+37.5 0+11-18	0.365	36.4		2.22 561.03
to -0+66 0+191-18	0.67	65	+9°-34'	+11.15 562.53
				563.25
✓ 249-22	1.47	147		4.1 559.2
✓ 262-07	1.17	117		7.1 556.4
✓ 269-31	3.38	338	-10°-03'	-6.4 552.2
✓ 280-13	3.50	350	-10°-0'	-6.1 552.3
✓ 291-09	3.20	320		4.9 558.1
✓ 302-51	4.00	400		2.1 561.1
✓ 305-58	4.02	402	+0°-58'	+6.8 565.2
✓ 326-28	2.30	230	+1°-33'	+6.2 564.6
✓ 322-53	1.81	181		8.3 555.0
✓ 297-53	1.21	121		10.1 553.2
✓ 191-18	0.45	45		6.85 556.4
✓ 11-18	0.72	72		8.5 554.8
✓ "	1.72	172		9.2 554.1
✓ "	2.33	233		0.1 563.2
π@ 0+66		5.01	574.35	2.89 569.35

Hayler Loc 180
Franklin π 88-11
Williams Rod 71-49

571.46
13.08
558.38

15

Nov 4/21

FS. up S.O.R to 86+55.7 S. 88-11 E 42 91-49

Comp " 0-40E

BM #20 Damsite #2

0+00 - 76+34 Williams

71393 71317 So side SDR 160 Contour

71342 " No " " " " "

561.03 " " in " " " Bed

569.35 So " top bank

Topog

Toe So Bank

In R Bottom

So edge Channel

No " "

R Bot

R Bank No Side

No Side toe Mt

" " R Channel

" " "

Toe bank R bot

So side Channel

No side Channel

" " toe Mt

BM #20 571.46 - 2.89

571.46

+ 2.89

574.35

Plotted
Nov 9
R.B.

X Axis

El Cap Damsite #2. Topog

Sta	Az	Rod	Hbr	Dist	Vert	L
TA-0+66				574	35	569.34
✓ 269-22		3.29	329		+1-05	+6.5755
✓ 271-22		2.56				5.4 569.0
✓ 268-36		1.55				8.1 566.3
✓ 274-26		0.86				6.5 567.9
✓ 84-41		0.97				4.6 569.8
✓ 90-25		2.32				4.3 570.1
✓ 91-08		4.75				3.3 571.1
✓ 85-35		4.70	470		-1-05	-8.8 560.5
✓ 77-38		4.90	490		-0-55	-7.8 561.5
✓ 71-29		5.20				9.2 565.2
✓ 60-34		3.65				9.1 565.3
✓ 57-39		3.29	329		-1-23	-7.9 561.4
✓ 77-40		3.11	310		-1-56	-10.4 558.9
✓ 83-39		3.05	304		-2-0	-10.6 558.7
✓ 82-18		1.25				16.0 558.4
✓ 66-38		1.38	137		-5-18	-12.7 556.6
✓ 61-34		1.53	154		-3-02	-8.4 560.9
✓ 106-40		1.35				4.1 570.3
AXIS ✓ 191-18		0.48				5.6 568.8
✓ 267-19		2.18				6.2 568.2
✓ 220-32		1.04				2.5 571.9
" ✓ 191-18		0.94				0.7 573.7
✓ 142-04		1.35	135		+3-19	+7.8 577.1
✓ 124-23		1.86	185		+3-18	+10.7 580

16

Topog Damsite #2 X Axis

						574.35
						5.01
						569.34
No edge road						
lower 1st slope						
Top Cut Bank So side						
" " " "						
" " " "						
On So Bench						
1st R So side Channel						
" " " "						
" " Bot						
" " " on bar						
" " " "						
" " " "						
" " " "						
Top Cut Bank So side						
1st R Bot						
" " " "						
On Bench						
" " " "						
1st Wagon road						
" " " "						
" " " "						
" " " "						
" " " "						

Plotted
11/19/21
HRB

El Cap Dom #2 Topog

Sta	Az	Rod	Hor Dist	Vert	Σ
to @-04660	Ans	5	01	57435	56934
✓ 103-43		2.68	267	+1-59	+90 5286
✓ 108-21		4.88	480	+7-10	+60.5 6298
✓ 120-13		3.20	380	+9-17	+60.2 6313
✓ 129-25		3.80	370	+9-24	+60.8 6301
✓ 136-03		3.25	314	+10-26	+58 6273
✓ 147-54		2.93	276	+12-12	+60.3 6296
✓ 156-55		2.40	274	+12-56	+55 6213
to 'C					
✓ 338-18		6.41	617	+11-30	+116 6953
✓ 319-20		5.23	514	+3-20	+30.5 5998
✓ 330-41		5.57	550	+7-27	+71.5 6408
✓ 345-35		5.14	487	+13-24	+116 6853
✓ 351-19		4.90	460	+14-03	+115.3 6846
✓ 359-54		4.74	449	+13-28	+107 6763
✓ 5-21		4.79	456	+12-41	+104.8 6721
✓ 7-47		4.31	417	+10-34	+77.3 6466
✓ 357-52		4.12	395	+11-25	+79.7 6490
✓ 342-55		4.45	430	+10-33	+80 6493
✓ 338-38		4.75	462	+9-13	+75 6403
✓ 353-08		3.42	337	+7-28	+44 6133
✓ 342-50		3.51	348	+6-19	+38.4 6077
to 'D					
✓ 60-54		4.14	414	-0-31.8	55 56580

to Wagon Road					
On Mt side	Sw				
"	"				
"	"				E of small gulch
"	"				"
"	"				"
"	"				"
On Hogback	P.O. Rock	6.47		+11-37	Surf - 20 ft
On hogback	No side				
"	"				
On Mt	"				
"	"				Under Cliff
"	"				"
"	"				"
"	"				"
"	"				"
"	"				"
"	"				"
"	"				"
"	"				"
"	"				"
"	"				"
"	"				"

Platted
Nov 9 1921
H.R.B.

Ri. Cap. Dam #2 Topog

Sta	Az	Red H	Dist	Vert L	Diff	E1
T@D			502	570.62		565.80
					1.47	569.35
✓ 264-35	1.25				7.0	563.8
✓ 273-45	1.35	134	-3	-55	-9.4	556.4
✓ 301-0	1.32	131	-5	-02	-11.5	554.3
✓ 317-0	2.33				4.1	566.7
✓ 340-06	1.82				6.3	564.5
✓ 11-50	1.78				3.4	567.4
✓ 49-23	2.50				1.8	569.0
✓ 52-35	2.08		-2	-11	-8.0	557.8
✓ 52-53	0.80	79	-6	-56	-9.6	556.2
✓ "	0.37				6.0	567.5
✓ 305-29	0.28				5.0	565.8
✓ 322-08	0.49	48	-8	-23	-7.1	558.7
✓ 336-58	0.78	75	-11	-42	-14.9	550.9
✓ 345-36	1.47	147	-3	-45	-9.6	556.2
✓ 48-43	2.85	284	+2	-57	+14.6	580.4
✓ 34-08	2.54	249	+8	-53	+38.7	604.5
✓ 10-33	2.30	225	+7	-35	+3.0	595.8
✓ 6-12	2.42	240	+5	-29	+1.3	588.8
✓ 30-46	4.75	459	+10	-25	+8.4	649.8
✓ 21-58	4.05	384	+13	-33	+9.4	657.8
✓ 341-38	2.39	234	+9	-0	+3.7	602.8
✓ 22-13	5.21	488	+14	-43	+12.8	693.8
✓ 330-43	3.33	317	+12	-41	+11.5	637.3

57.46
1.47
572.93

565.80
502
570.62

569.35
1.47
570.82

BS on -0766 4-14 + 0-28
 On -0766 + 0-28
 In R. Bed on bar
 " " So side Channel
 Channel
 On toe Mt No side
 " " " " " " Up 10'
 " " " " " " " "
 In Channel N side
 " " " " " " " "
 Top of Bar in R Bed
 " " " " " " " "
 So edge Channel
 " " " " " " " "
 No " " " " " " " "
 Top of cut bank Toe Mt
 " " " " " " " "
 " " " " " " " "
 " " " " " " " "
 Small ^{20' deep} gulch Same as ^{6-10'} sup No side
 " " 30' farther East
 On ridge between gulches
 " Mt
 On ridge @ break E into gulch =
 On Mt

Plotted
Nov 9, 1921
J.E.B.

Sta	Az	Rod	H. Dist	Vert	∠	Diff	EI
π@D		5.02	570	±			565.8
14-20	4.98	470	+13	-57	+116	681.8	
341-03	4.17	39	+14	-35	+104	667.8	
6-10	4.85	46	+12	-50	+105	671.3	
358-54	4.62	43	+14	-28	+111	677.3	
348-55	4.48	47	+15	-17	+114	679.8	
0-25	3.85	367	+12	-54	+84	649.8	
6-10	3.94	380	+10	-52	+73	638.8	
345-40	4.83	450	+18	-05	+111	686.8	

On ridge
" MT
In gulch
On MT
" "
" "
In T
In gulch
On MT

Sta	Az	Rod	H. Dist	Vert	∠	Diff	EI
π@C	4.98					695.3	
140-41	0.61	60	-7	-40	-8.1	687.7	
114-12	1.46	140	+8	-27	+21	716.5	
115-40	1.90	187	+7	-40	+15	720.5	
69-21	0.82	68	+24	-06	+30	725.9	
77-10	1.54	127	+24	-31	+58	753.5	
91-29	1.80	158	+20	-22	+58	753.7	
55-24	2.33	204	+21	-11	+78	773.5	
31-58	3.04	29	+11	-19	+58	754.1	
24-36	4.35	425	+8	-22	+65	757.8	
14-39	4.95	48	+9	-12	+76	773.3	
358-29	4.05	405	+1	-45	+12	707.7	
12-27	3.40	340	+1	-31	+90	704.3	
12-44	2.74	444	+1	-08	+44	699.7	

647
On MT
" "
Surt above cliff with trap
On MT
" "
" @ galv l. tank
" "
" " In gulch 10' deep
" "
" "
In gulch same

Plotted Nov 7 1921
ARB

K1 Cap Dam #2 Topog
+ H.I.

Sta	Az	Red	Vert	EL
K@9+54	Old Aris	5.05		856.7
✓	225-28	4.11	407	-8-45 618 794.4
✓	225-24	2.82	468	-12-08 58 798.7
to B	250-02	1.63	161	-7-22 406 835.6
to A	22-11	0.92	91	+7-40 417 868.5
K@IB		4.50		835.6
✓	210-57	0.52	49	-14-40 418 824.8
✓	216-19	1.35	148	-12-49 494 826.4
✓	"	2.25	418	-9-22 360 899.6
✓	237-26	2.40	444	-15-50 634 774.4
✓	237-56	1.44	134	-16-28 390 796.6
✓	305-38	0.60	60	+2-22 415 838.1
✓	13-15	0.52	48	+16-21 440 849.6
✓	348-02	0.98	93	+12-54 423 856.9
✓	47-0	1.63	143	+20-31 535 889.1
✓	31-14	2.33	188	+25-58 498 927.4
✓	21-25	2.68	213	+27-12 409.5 945.1
to TE	20-17	2.12	188	+19-56 468.0 903.6

Sta	Az	Red	Vert	EL
K@TE		5.11		903.6
✓	280-06	1.81	144	-31-38 508 824.8
✓	261-0	1.46	115	-27-17 594 844.2
✓	288-29	1.90	175	-16-19 517 852.4

362-17
150
182-17

21

On Mt

SP

Old Hub B for Core Hole Location

" " A " " " "

BS on 9+54.7 Old Aris 161 +7-20

Topog Shots No Side

On Mt top Hogback

" " " "

" " " "

" " " "

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" " " "

" " " "

217 -19-57

BS on IB

On Mt W side Hogback

" " W of " Main Slope

Old Topog
Hogback
192

Page 15

7	Topog 375	X	4.94	565.97		561.03
	281-31	0.71	71		12.05	553.92
to	Axis	191-18	6.93	534	+ 19 - 45	+ 19.0° 753.0
to	#768	170-12	5.60	515	+ 16 - 28	+ 15.0° 713.0
to	#767	156-31	6.16	575	+ 14 - 50	+ 15.0° 713.0
	150-32	6.60	618	+ 22 - 58	+ 14.0°	705.0
to	#766	145-07	7.10	675	+ 12 - 56	+ 15.0° 713.0
	142-05	6.18	588	+ 12 - 50	+ 13.0°	695.0
	135-58	5.55	530	+ 12 - 09	+ 11.0°	675.0
	148-01	5.61	540	+ 11 - 40	+ 11.5°	674.5
	153-06	4.98	475	+ 12 - 06	+ 10.0°	663.0
	176-16	4.96	460	+ 15 - 30	+ 12.0°	689.0
	181-08	4.32	401	+ 15 - 26	+ 11.0°	674.0
	187-39	3.95	368	+ 15 - 09	+ 9.5°	660.5
	198-49	4.00	371	+ 15 - 49	+ 10.5°	666.0
	198-42	3.58	340	+ 13 - 0	+ 7.5°	639.5
	203-46	3.50	334	+ 12 - 38	+ 7.5°	635.5
	223-51	3.45	323	+ 10 - 08	+ 5.5°	620.5

FS. on Williams Hub @ El 713.17 = 160 Contour
A2 191-18 So Side

Core Hole #14 River Channel

On flume Bench So Side

Hub on 160 Contour Williams So side

On Mt Slope

Hub on 160 Contour

On Mt Hogback top East Axis

" " Slope

" " "

" " "

" " "

" " "

" " "

" " "

" " "

" " "

Plotted
Nov 9 1921
HRB

Axis No 0 + 37.5	494	565	97	561.03
✓ 209-35	2.96	289	+ 8-41	+140 6050
✓ 224-51	5.00	480	+ 11-30	+175 6585
✓ 228-22	5.54	534	+ 11-29	+1080 6690
✓ 219-56	5.01	484	+ 11-19	+162 6572
✓ 226-10	6.11	578	+ 13-31	+1490 7100
✓ 217-14	5.13	494	+ 12-02	+1050 6660
✓ 220-47	6.00	567	+ 13-55	+1400 7010

to ~~TH~~ ✓ 213-49 440 416 + 13-12 +940 + 659.07

Axis No 0 + 37.5	496	664.03	659.1
✓ 322-04	1.98	184	- 16-36 -540 6051
✓ 305-28	1.50	139	- 15-46 -393 619.8
✓ 317-04	1.23	105	- 22-05 -438 6153
✓ 310-0	0.78	59	- 29-28 -333 6258
✓ 253-44	0.53	45	- 22-52 -190 640.1
✓ 225-30	1.67	158	+ 13-11 +370 6961
✓ 210-20	1.48	137	+ 15-49 +387 6978
✓ 213-20	0.75	74	+ 10-07 +190 672.1
✓ 186-17	0.54	45	+ 24-26 +103 6794
✓ 125-19	1.47	134	+ 17-26 +120 7011

On Mt Slope
"
"
"
"
"
"

440 -13-16

BS. on 0 + 37.5 New Axis X

On Mt lower slope
"
"
In gully
"
On Mt slope - 30' of gully
"
"
"
"

Nov 7-21

Plotted
Nov 9 21
HRB

Sta	Az	Rod	Vert	L	E
AXIS ^{50 side}					
AXIS		4.93	757.09		752.16
B.M.				3.915	753.47
AXIS	✓ 191-18	0.39	34	+ 25-30	+55 767.4
"	✓ "	1.51	106	+ 82-02	+89 820.2
"	"	0.85	?	0	3.22 753.27
	✓ 253-59	0.33			3.26 753.83
	✓ 258-42	1.01			3.36 753.73
old AXIS to 5+50	✓ 262-50	1.60			4.84 752.25
	✓ 263-45	1.99			3.56 753.53
	✓ 274-31	3.60			3.63 753.46
	✓ 274-21	3.95			3.72 753.37
to "G"	✓ 273-33	2.95		- 0°-12	6.26 750.83
	✓ 266-52	2.90	190	+ 0-48	+40 756.2
	✓ 259-06	2.78	278	+ 3-02	+148 767.0
	✓ 255-08	3.31	516	+ 7-52	+148 797.0
	✓ 257-10	3.67	358	+ 8-13	+548 807.0
	✓ 255-25	4.10	396	+ 10-33	+140 826.2
	✓ 252-55	3.60	350	+ 9-36	+590 811.2
	✓ 262-04	4.23	412	+ 8-0	+582 810.4
	✓ 267-52	3.67	365	+ 4-43	+300 782.2
	✓ 125-52	0.17	17		3.21 753.88
	✓ 109-21	1.74	174	+ 0-34	+17 753.9
	✓ 117-15	3.10	310	+ 0-21	+19 754.1

F.S. to 160 Hub No Side
H.I. from f.S. on 200' Contour

On Fletcher flume bench on Axis X p 24
on 200 ft Contour Nail in Sill of flume

⊕ Fletcher flume ? should be about 8

" " " B.C. stars called + up R

" " " E.C.

Hub on flume bench former Axis

⊕ Fletcher "

" " "

" " "

" " "

Hub on Fletcher flume bench W of treadle

On Mt W of gulch

" " " "

" " " "

" " " "

" " " "

" " " "

" " " "

" " " "

" " " "

⊕ Fletcher flume E.C.

" " " B.C.

" " " "

Plot 10' 9 192
T.B.

Sta	Az	Rod	Vert L	Σ
Axis π@X	✓	+ 93	757.09	752.16
to 'II'	106-35	1.07	107	-0-06 5.10 751.29
to 'II'	105-59	3.22	322	+0-05 4.29 752.80
π@'H'		5.06	757.05	751.99
✓	197-26	0.45	35	+ 27-56 4.16 770.6
✓	202-25	0.67	49	+ 31-27 4.17 781.7
π@ 'I'		5.03	757.83	752.80
✓	243-46	1.97	167	+ 22-58 4.08 823.6
✓	171-10	2.42	216	+ 19-24 4.55 828.3
✓	194-57	0.50	41	+ 24-45 4.92 771.8
✓	146-0	2.72	255	+ 14-54 4.68 820.6
✓	140-50	4.26	170	+ 10-58 4.33 785.6
✓	120-17	1.62	167	+ 0-30 4.14 754.2
✓	155-34	4.57	147	+ 14-28 4.37 790.6
✓	108-12	1.07	107	- 1-52 3.5 749.3
π@ G		4.95	755.78	750.83
✓	25-30	0.42	28	- 35-20 4.18 731.0
✓	106-43	4.03	107	- 6-59 4.14 736.4
✓	72-53	0.73	59	- 25-58 4.87 722.1
✓	125-42	0.74	74	3.0 752.8

Hub on Fletcher Flume Bench
 ' ' ' ' ' ' E of Axis for topog

R
1.07

B.S. on Hub @ Axis on Fletcher Flume Base
 On Mt
 " "

B.S. Hub on Axis @ Fletcher Flume bench
 R
3.22

On Mt

" "

" "

" "

" "

Flume B.C

On Mt

" "

R
2.95

B.S. on hub on Axis @ Fletcher Flume Base

Flume below tralte

On Mt below Tualte

" "

Sta	Az	Rod	Vert	EI
N @ G		4.95	755.78	750.83
146-16	1.10	104	+ 13-28	+ 487756
121-54	1.93	187	+ 10-34	+ 346 7954
171-0	2.06	178	+ 21-33	+ 705 821 3
157-35	2.04	186	+ 17-12	+ 515 8083
141-18	2.53	127	+ 19-20	+ 792 830.0
Old Axis to 5+50	105-49	1.11	+ 0-33	3 50 752.28 + 135 752.18

On Mt above Trestle
 ' ' ' flume
 ' ' ' W of gulch
 ' ' ' E ' '
 ' ' ' " "

Hub on Old Axis on flume bench E of Trestle

El Capitan Dam site No 2
CORE DRILL HOLES

G.R.H
11-30-21

29

Hole No	Elev. of Ground Surf.	Estimated Elev. of Bed Rock
1	568.5	511
2	652.0	—
3	651.3	575
4	757.0	—
5	756.8	626
6	838.8	703
7	875.9	768
8	870.9	740
9	978.4	757
10	941.7	816
11	783.6	690
12	727.3	630
13	555.4	500
14	553.9	504
15	554.7	
16	552.6	



El Capitan Dam site #2

Location of Core Drill Holes

Sta	Azi.	Red	Hor. Dist	Vert L	Elevation
T@ -1+33.3A		5.13			569.00
BS on 5+21.6	20°46'	6.25		+ 11°00'	+74.56
	30°14½'	6.60	653	+ 6°31'	643.6
	35°20'	4.10	411	- 2°28'	-17.68 551.3
	152-40	0.81	79	+ 11-05	+ 15.57 584.5
AK	152°-26	1.48		+ 16-39	+41.3
T@ AK		4.87	138	Average	610.3
BS on 1+33.3A	332°-26	1.51		- 16-35	+38.3
	194°-21	0.91	72	+ 28-02	648.6

Hole # 21 is 2.5' Northerly of hub on bench near flume on Williams

4-19-22

On Axis of Dam Site #2

Hole # 22

17 (?) Post in River

19

AK

Hole # 20

Axis and 6" lower than hub. Elev

Cross Section Eadid Ave
From University to El Cajon

60' wide
18' cbs
9' qts

347.45

410.21
515.50
315.5
North

15ft. of Center Paved

Hyd

Univ. & Eadid

BM 6.77 347.45 340.68

N.L. University

W 6.5 341.0

cb Top 6.77 340.68 End Return

Gutter Top Paving 7.49 339.6

W 7.17 340.24

E 6.90 340.55

W 7.12 340.33

Gutter " " 7.42 340.03

cb Top 6.72 340.73 on Return

E 6.9 340.6

50'N

E 6.9 340.6

cb 7.2 340.2

W 7.9 339.6

+1.5 E Edge Paving 7.82 339.63

E 7.59 339.86

+7.5 W El Pav 7.76 339.69

W 8.0 339.5

cb 7.2 340.3

W 6.9 340.6

52'N

W 6.8 340.7

cb 7.2 340.3

W 7.9 339.6

+1.5 W El Pav 7.77 339.68

6	7.63	339.87
+7.5 E El Pav	7.88	339.57
W	8.1	339.4
cb	7.2	340.3
E	6.5	340.3
	6.77	
E	7.2	345.3
W	7.9	343.6
cb	7.6	339.9
W	8.2	339.3
+1.5 E El Pav	7.87	339.48
E Paving	7.72	339.73
+7.5 W El Pav	7.91	339.54
W	8.0	339.5
cb	7.2	340.7
W	6.8	340.7
	100'N	
W	6.9	340.6
cb	7.5	340.0
W	8.2	339.3
+1.5 W El Pav	8.00	339.3
E	8.00	339.5
+7.5 E El Pav	8.21	339.24
W	8.3	339.2
cb	8.2	338.7
+3	7.5	340.0
+5	4.3	343.2

110' X 100' Paved Garage
Cone Floor
6551-34084

F	2.3	345.2
	150'H	
F	2.0	345.5
+4	2.8	344.7
+8	8.6	338.9
Cb	9.5	338.0
1/4	8.7	338.8
+1.5 F Ed P	8.62	338.83
2	8.50	339.0
+7.5 W Ed P	8.71	338.74
1/4	8.6	338.9
Cb	8.5	339.0
W	8.3	339.2
	180'H	
W	8.5	339.0
Cb	8.8	338.7
1/4	9.0	338.0
+1.5 W Ed P	9.02	338.43
2	8.82	338.63
+7.5 F Ed P	9.02	338.43
1/4	9.0	338.5
Cb	9.2	338.2
+5	9.7	337.8
+9	4.6	347.9
F	4.0	343.5
	200'H	
F	5.1	341.9

+7	7.1	340.4
+10	9.5	338.0
Cb	9.8	337.7
1/4	9.2	338.2
+1.5 F Ed P	9.21	338.24
2	9.00	338.5
+7.5 W Ed P	9.21	338.24
1/4	9.0	338.5
Cb	9.1	338.4
W	8.8	338.7
30' Ed Top Conc Wall	5.84	341.61
	250'H	
W Ed Top Conc Wall	5.77	341.68
W	9.0	338.5
Cb	9.4	338.1
1/4	9.7	337.8
+1.5 W Ed P	9.55	337.90
2	9.43	338.02
+7.5 F Ed P	9.58	337.86
1/4	9.6	337.9
Cb	9.9	337.6
F	9.2	338.2
TP	3.31	341.2
F	3.31	341.2
Cb	3.31	341.2
+3	3.5	337.4
1/4	3.8	337.3

341.12

+1.5 E Ed Pav	361	337.51
E	335	337.77
+7.5 W Ed Pav	358	327.54
1/4	36	337.5
cb	34	337.7
W	33	337.9

300 W

W Top Conc Wall	168	339.42	314 W on W Conc Dr. 321
W	25	337.6	
cb	36	337.5	
1/4	52	327.3	
+1.5 W Ed Pav	323	327.79	
E	362	327.45	
+7.5 E Ed Pav	391	327.21	
1/4	41	327.0	
cb	44	326.7	
+5	57	325.2	
+7	53	325.8	
+8	47	326.4	
F	47	326.2	

315 W

F	57	335.4
+10	48	326.3
cb	42	326.9
1/4	41	327.0
+1.5 E Ed Pav	109	327.08
E	379	327.33

341.12

32

+7.5 W Ed Pav	396	337.16
1/4	38	327.3
cb	36	327.5
W	33	327.8
	340 W	
W	57	327.4
cb	37	327.4
1/4	39	327.2
+1.5 W Ed Pav	395	327.17
E	377	327.35
+7.5 E Ed Pav	400	327.4
1/4	40	327.0
cb	39	327.2
F	39	327.2
+10	61	325.0

350 W

+5	114	329.7
F	57	325.4
+1	36	327.5
cb	37	327.6
1/4	38	327.3
+1.5 E Ed Pav	371	327.21
E	377	327.35
+7.5 W Ed Pav	385	327.27
1/4	36	327.5
cb	33	327.8
+7	55	325.6

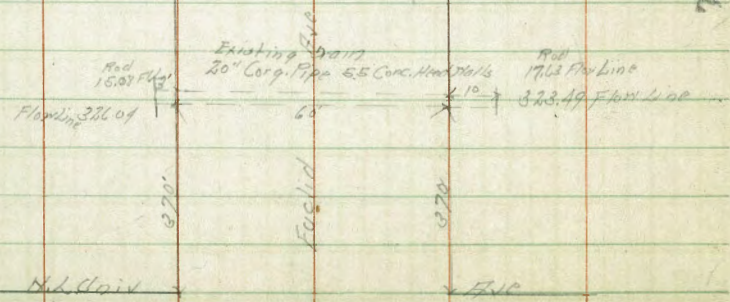
341.12

+8	4.0	337.1
M	4.0	337.1
N End Conc Hall	2.29	338.73
	320'N	
-10	2.9	332.2
M	8.5	332.6
+3	9.3	331.4
+6	8.0	332.1
cb	3.6	337.5
14	3.5	337.6
+1.5 N Ed Par	3.85	337.27
E	3.72	337.40
+7.5 E Ed Par	3.82	337.30
14	3.7	337.4
cb	3.6	337.5
+2	3.7	337.4
E	9.7	331.7
+7	13.4	327.7
125	17.8	323.3

Polk

lotland

Use 10' sidewalk



University

341.12

	370'N	
-2.5	12.3	328.8
-10	12.6	328.5
-8	15.1	326.0
E	9.8	331.3
cb	3.9	337.2
+2	3.5	337.6
14	3.5	337.6
+1.5 E Ed Par	3.75	337.37
E	3.63	337.49
+7.5 N Ed Par	3.74	337.28
14	3.5	337.6
cb	3.3	337.8
M	10.6	330.5
+2.5	12.6	328.5
+3	15.1	326.0
+7	13.5	327.6
+1.5	12.2	328.9
TP	4.36	343.09
	400'N	
-20	15.7	327.7
-10	14.9	328.2
M	12.1	331.0
cb	5.1	338.0
+2	4.1	339.0
14	4.9	338.2
+1.5 N Ed Par	4.12	338.27

Top Hall
32.50' off H.L.

34309

B	462	339.47
+7.5 F Ed Pav	487	338.22
1/4	49	338.2
Cb	46	338.5
+1	45	338.6
F	110	337.1
+9	152	327.9
+20	158	327.3

430'N

-20	112	331.9
-2	105	332.6
F	91	334.0
+10	36	339.5
Cb	38	339.3
1/4	39	339.2
+1.5 F Ed	386	339.23
B	361	339.48
+7.5 N Ed	388	339.21
1/4	40	339.1
+7	36	339.5
Cb	46	338.5
N	117	331.4
+20	133	329.8

450'N

-20	107	332.4
N	96	333.5
Cb	32	339.9

34309

5-12-26 34

1/4	32	339.9
+1.5 N Ed Pav	321	339.88
B	321	340.13
+7.5 F Ed Pav	344	339.85
1/4	34	339.7
Cb	32	339.9
+2	31	340.0
F	72	335.9
So. End Top Cook Hall	547	337.62
+10	69	336.2

475'

F	42	338.9
+7	39	339.2
Cb	25	340.6
1/4	24	340.7
+1.5 F Ed Pav	237	340.72
B	209	341.0
+7.5 N Ed	239	340.70
1/4	23	340.8
Cb	23	340.8
+2	25	340.6
N	71	336.0
+10	80	335.1

500

-10	62	336.9
N	49	338.2
+1	40	339.1

343.09

+7		18	341.3
Cb		17	341.4
74		15	341.6
+1.5 WED		158	341.51
Z		1.32	341.77
+7.5 EED		1.58	341.51
74		1.6	341.5
Cb		1.5	341.6
E		1.5	341.6

510'N

E		0.2	343.1	
+2		0.1	343.0	
+5		0.8	342.3	
Cb		1.1	342.0	
74		1.2	341.9	
+1.5 EEDP		1.26	341.83	
Z		1.01	342.08	
+7.5 WEDP		1.26	341.83	
74		1.2	341.9	
Cb		1.1	342.0	
74		1.5	341.6	
TP	9.73	<u>352.08</u>	0.74	342.35
		5.50'N		
74		8.6	342.5	
Cb		8.0	342.1	
74		7.7	344.4	
76		9.5	342.6	

352.08

85

74		9.2	342.9
+1.5 WEDP		9.0	343.4
Z		8.73	343.35
+7.5 EED		8.98	343.10
74		9.0	342.1
72		9.5	342.6
78		6.5	345.6
Cb		6.2	345.9
E		5.5	346.6

575'N

E		5.5	348.6
Cb		3.9	348.2
+1		4.2	347.9
+7		8.3	343.8
74		8.2	343.9
+1.5 EEDP		8.11	343.92
Z		9.90	344.18
+7.5 WEDP		8.12	343.96
74		8.2	343.8
+3		8.8	343.3
+5		5.2	346.9
Cb		5.1	347.0
+2		5.6	346.5
74		6.0	346.1
			6.00'N = 51. Fells (Bona)
74		4.2	347.9
Cb		3.3	349.8

352.08

7.4			3.7	348.4	
7.6			7.9	344.2	Palk
7.4			7.5	344.6	80' Wide
7.15	NEEP		7.38	344.7	65 Cbs
8			7.15	344.93	6.75 94
7.5	E Ed Pav		7.38	344.7	
7.4			7.4	344.7	
7.2			7.4	344.7	
cb			2.2	349.9	
E			2.2	349.6	
TP	4.95	355.51	1.58	350.86	Hail Palk SE Cor App. at Euclid
		5 Cb			
E			5.5	350.0	
cb			5.8	349.7	
7.6			10.5	345.0	
7.4			10.7	344.8	
7.15	E Ed Pav		10.65	344.86	
8			10.47	345.04	
7.5	NEEP		10.28	344.79	
7.4			10.8	344.7	
7.3			10.9	344.6	
7.7			6.5	349.0	
cb			6.2	349.0	
7.4			6.7	348.8	
		3' N Cb			
7.4			6.4	349.1	
cb			6.2	349.3	

355.51

5" Mac Pav
2" Asp Top

34

7.7			6.5	349.0	
7.6			10.1	344.7	
7.4			10.7	344.8	
7.15	NEEP		10.68	344.83	
8			10.46	345.05	
7.5	E Ed Pav		10.65	344.86	
7.4			10.7	344.8	
7.2			10.4	345.1	
cb			6.2	349.3	
7.4			5.5	350.0	
7			5.5	350.0	
		5' 7/4			
7			8.0	347.5	
cb			9.2	346.3	
7.4			10.3	345.2	
7.4			10.4	345.1	
7.15	E Ed Pav		10.65	344.86	
8			10.45	345.06	
7.5	E Ed Pav		10.68	344.89	
7.4			10.6	344.9	
cb			9.8	345.7	
7.4			9.0	346.5	
		8' Palk			
7.4			9.1	346.4	
cb			9.9	345.6	
7.4			10.2	345.2	
7.15	NEEP		10.56	344.95	

355.51

2		10.33	345.18
+7.5	F Ed Pav	10.55	344.96
1/4		10.25	345.16
+5		10.2	345.3
cb		9.7	345.8
F		8.1	347.4
	N 1/4		
F		8.5	347.0
cb		9.7	345.8
1/4		10.3	345.2
+1.5	F Ed P	10.50	345.2
2		10.25	345.26
+7.5	N Ed P	10.44	345.07
1/4		10.3	345.2
+3		9.8	345.7
cb		9.7	345.8
N		8.8	346.7
	Ncb		
N		7.7	347.8
cb		8.4	347.1
+2		8.6	346.9
+6		10.0	345.5
1/4		10.2	345.3
+1.5	N Ed Pav	10.38	346.13
2		10.21	345.30
+7.5	F Ed Pav	10.45	345.06
1/4		10.3	345.2

355.51

37

+5		9.8	345.7
cb		8.6	346.9
F		9.3	349.2
	35' N N.C.		
F		4.1	351.4
cb		5.3	350.2
+1		5.8	349.7
+3		9.7	345.8
1/4		10.3	345.2
+1.5	F Ed Pav	10.39	345.12
2		10.19	345.32
+7.5	N Ed P	10.39	345.12
1/4		10.2	345.3
+3		10.0	345.5
cb		6.4	349.1
N		5.8	349.7
	N. L. Pav		
N		5.7	349.8
cb		6.4	349.1
+6		10.0	345.5
1/4		10.2	345.3
+1.5	N Ed Pav	10.39	345.12
2		10.19	345.32
+7.5	F Ed P	10.39	345.12
1/4		10.3	345.2
+6		9.7	345.8
+8		5.8	349.7

355.51

Cb		5.3	350.2
F		9.1	351.4
		50%	
F		8.8	351.7
Cb		3.2	352.3
+6		9.7	345.8
1/4		10.0	345.5
+1.5	FFDP	9.88	345.63
2		9.58	345.93
+7.5	WEDP	9.82	345.69
1/4		9.9	345.6
+2		9.3	346.2
Cb		4.8	350.7
+5		3.2	352.3
1/4		3.4	352.1
		100%	
1/4		3.1	352.4
Cb		2.6	352.9
+2		2.9	352.6
+6		8.8	346.7
1/4		9.4	346.1
+1.5	WEDP	9.37	346.14
2		9.23	346.28
+7.5	FFDP	9.48	346.13
1/4		9.5	346.0
+3		9.1	346.4
Cb		3.9	351.8

355.51

38

7-11-26

F		3.5	352.0
B/W	7.31	352.22	352.56
		135%	
F		6.2	351.7
Cb		6.2	351.7
+2		11.1	346.8
1/4		11.5	346.4
+1.5	FFDP	11.5°	346.37
2		11.3°	346.57
+7.5	WEDP	11.52	346.35
1/4		11.4	346.55
+2		11.3	346.6
Cb		5.2	352.7
1/4		5.2	352.7
		137%	
1/4		5.0	352.9
Cb		5.1	352.8
+2		11.2	346.6
1/4		11.9	346.5
+1.5	WEDP	11.55	346.32
2		11.5°	346.57
+7.5	FFDP	11.51	346.33
1/4		11.5	346.4
Cb		11.2	346.7
F on Conc Drive		10.81	347.01
		150%	
F		10.9	347.2

Nail pole
SE from
Euclid

35787

Cb	10.9	347.0
1/4	11.4	346.5
+1.5 Ed P	11.39	346.48
E	11.18	346.69
+7.5 Ed P	11.42	346.45
1/4	11.4	346.5
+2	11.2	346.7
Cb	4.9	353.0
H	5.8	352.9
152'H		
H	5.1	352.8
Cb	5.1	352.8
+7	11.0	346.9
1/4	11.4	346.5
+1.5 Ed P	11.34	346.51
E	11.15	346.72
+7.5 Ed P	11.37	346.50
1/4	11.4	346.5
+6	10.8	346.1
Cb	7.8	350.1
F	7.3	350.6
195'		
F	8.8	349.1
+10	7.7	350.2
Cb	8.8	349.1
+5	10.7	347.2
1/4	10.9	347.0

35787

+1.5 Ed P	10.95	346.92
E	10.74	347.13
+7.5 Ed P	11.00	346.87
1/4	11.0	346.9
+2	10.6	347.3
Cb	5.1	352.8
H	5.4	352.5
195'H		
H	5.2	352.7
Cb	5.1	352.8
+7	10.7	347.2
1/4	11.0	346.9
+1.5 Ed P	10.97	346.90
E	10.23	347.14
+7.5 Ed P	10.84	346.93
1/4	10.9	347.0
Cb	10.1	347.8
F	9.2	348.7
200'H		
F	9.0	348.9
+3	7.4	350.5
Cb	6.6	351.3
+4	10.7	347.2
1/4	10.8	347.1
+1.5 Ed P	10.92	346.95
E	10.70	347.17
+7.5 Ed P	10.93	346.94

35787

74		11.0	346.9
+2		10.7	347.2
Cb		51	352.8
H		54	352.5
	220'N		
H		56	352.3
Cb		55	352.4
+7		10.6	347.3
74		10.8	347.1
71.5	HEDP	10.72	347.14
E		10.51	347.36
+7.5	EDP	10.74	347.13
71		10.5	347.37
+3		10.4	347.47
+7		6.4	351.5
Cb		6.4	351.5
+9		7.9	350.0
F		9.4	348.5
	222'N		
F		9.5	348.4
Cb		9.9	348.0
74		10.6	347.3
71.5	EDP	10.70	347.2
E		10.50	347.4
+7.5	HEDP	10.72	347.15
74		10.8	347.1
+2		10.6	347.3

35787

Cb		54	352.5
H		56	352.3
	224'		
H		58	352.1
Cb		54	352.5
+7		10.5	347.4
74		10.7	347.2
71.5	HEDP	10.62	347.25
E		10.43	347.44
+7.5	HEDP	10.69	347.18
74		10.6	347.3
Cb		9.7	348.2
F		9.5	348.4
	221'N		
F		9.4	348.5
H		9.2	348.7
+3		9.8	350.1
Cb		6.5	351.4
+6		10.2	347.7
74		10.6	347.3
71.5	HEDP	10.65	347.22
E		10.36	347.51
+7.5	HEDP	10.60	347.27
74		10.7	347.2
+2		10.7	347.2
Cb		54	352.5
H		57	352.2

35787

N		66	351.3	
CB		76	350.3	
+7		9.2	348.7	
1/4		9.4	348.5	
+1.5 HEDP		9.57	348.29	
8		9.55	348.52	
+7.5 FEDP		9.54	348.33	
1/4		9.6	348.3	
CB		9.5	348.4	
F		9.3	348.6	
Top Conc Wall		9.15	348.72	
TP	4.84	<u>353.21</u>	9.50	348.37
		400		
Top Wall		4.20	349.01	
F		4.6	348.6	
CB		4.8	349.4	
1/4		4.5	348.5	
+1.5 FEDP		4.48	348.73	
8		4.61	348.97	
+7.5 HEDP		4.46	348.79	
1/4		4.3	348.9	
+2		4.3	348.9	
CB		3.0	350.2	
N		1.7	351.3	
		450		
N		2.6	350.6	
+7		3.0	350.2	

35321

46

CB		3.8	349.4	
1/4		4.0	349.2	
+1.5 HEDP		4.07	349.15	
8		3.83	349.38	
+7.5 FEDP		4.05	349.16	
1/4		4.1	349.1	
CB		4.4	348.8	
F		4.3	348.9	
Top Wall		3.76	349.45	
		500		
Conc Wall		3.55	349.66	
F		3.6	349.6	
CB		3.6	349.6	
1/4		3.6	349.6	
+1.5 FEDP		3.57	349.64	
8		3.36	349.85	
+7.5 HEDP		3.57	349.64	
1/4		3.7	349.5	
CB		3.8	349.4	
+5		3.5	349.7	
+2		3.8	350.4	
N		3.5	350.7	
		550		
N		2.2	351.0	
+5		2.5	350.7	
+8		3.5	349.7	
CB		3.6	349.6	
1/4		3.3	349.7	

35321

+1.5	WEAR	3.23	349.98	
z		3.01	350.20	
+7.5	FEED	3.22	349.99	
1/4		3.2	350.0	
CB		3.5	349.7	
E		3.4	349.8	
Top Wall		3.03	350.18	
	577X = 52 Orange			Orange 80' wide 15' deep 12.59 ft
Top Wall		2.69	350.52	
E		3.5	349.7	
CB		3.3	349.9	
1/4		2.9	350.3	
+1.5	FEED	2.95	350.26	
z		2.72	350.49	
+7.5	WEAR	2.94	350.77	
1/4		3.0	350.2	
CB		3.0	350.2	
X		2.6	350.6	
	CL			
		2.59	350.62	OO CB End
X		2.8	350.4	
CB		3.1	350.1	
1/4		2.9	350.3	
+1.5	WEAR	2.90	350.31	
E		2.72	350.49	
+7.5	FEED	2.95	350.76	
1/4		2.9	350.3	

35321

4-13-26 73

CB		3.9	350.3		
E		4.1	348.6		
BM	3.27	<u>353.99</u>	2.99	350.72	NE Orange Euclid 350.69
		5 1/4			
E		5.3	348.7		
CB		4.4	349.6		
1/4		3.7	350.3		
1/4		3.1	350.4		
+1.5	FEED	3.71	350.78		
z		3.50	350.49		
+7.5	WEAR	3.71	350.78		
1/4		3.6	350.4		
CB		3.7	350.3		
X		3.1	350.4		
		z			
X		3.5	350.5		
CB		3.5	350.5		
1/4		3.1	350.4		
+1.5	WEAR	3.64	350.33		
z		3.45	350.54		
+7.5	FEED	3.65	350.34		
1/4		3.5	350.5		
1/4		3.7	350.3		
CB		4.1	349.9		
E		5.0	349.0		
		X 1/4			
E		4.8	349.2		

353.89

1/4		48	349.2	
CB		49	349.1	109' HOURLY CONC DRIVE
H		48	349.2	516
Top of Wall		150' N		
H		570	348.3	135' HOURLY CONC WALK
		57	348.3	516
CB		57	348.3	516
1/4		55	348.5	
+1.5	W EDP	542	348.57	
2		520	348.8	
+7.5	E EDP	540	348.6	
1/4		54	348.6	
+6		58	348.7	
CB		58	348.2	
F		56	348.4	
		200' N		Fence Posts
F		76	346.8	
CB		67	347.3	
1/4		68	347.8	
+1.5	E EDP	613	347.86	
2		588	348.11	
+7.5	W EDP	610	347.89	192' HOURLY CONC DR. 649
1/4		61	347.9	
+6		66	347.4	
CB		68	349.2	220' HOURLY CONC WALK 710
H		71	346.9	
		250' N		241' HOURLY CONC DRIVE 760
H		80	346.0	

353.99

+6		77	346.3	
CB		71	346.9	
1/4		69	347.1	
+1.5	W EDP	666	347.33	
2		645	347.56	
+7.5	E EDP	668	347.31	
1/4		68	347.2	
CB		74	346.4	
F		77	346.3	
		300' N		
F		80	346.0	
CB		80	346.0	
1/4		74	346.6	
+1.5	E EDP	733	346.66	
2		710	346.89	
+7.5	W EDP	733	346.66	
1/4		75	346.5	
+5		79	346.1	
CB		80	346.0	
H		82	345.8	
		300' N		
H		81	345.9	
CB		79	346.1	
+4		80	346.0	
1/4		75	346.5	
+1.5	W EDP	726	346.63	
2		715	346.84	

353.99

+7.5	FEHP	7.38	346.61
1/4		7.4	346.6
+5		7.8	346.7
+6		9.0	345.0
cb		9.3	344.7
+5		9.3	344.7
+6		8.3	345.7
F		8.8	345.2

350.11

E		9.3	344.7
+5		9.0	345.0
+6		9.9	344.1
cb		9.1	344.4
+2		9.4	344.6
+3		8.6	345.4
1/4		8.0	346.0
+15	FEHP	7.95	346.14
Z		7.69	346.30
+7.5	WEP	7.93	346.06
1/4		8.0	346.0
+6		8.6	345.4
cb		8.7	345.3
1/4		8.9	345.1

400.11

1/4		9.0	345.0
cb		9.2	344.8
1/4		8.5	345.5

353.99

+15	WEP	8.05	345.44	
Z		8.33	345.66	
+7.5	FEHP	8.54	345.45	
1/4		8.6	345.4	
+5		8.9	345.1	
cb		10.2	345.8	
+5		10.2	343.8	
+7		9.3	344.7	
F		9.3	344.7	
TP	4.80	349.33	9.46	344.53

450.11

F		4.7	344.6
+6		4.8	344.5
+7		5.8	343.5
cb		5.7	343.6
+2		5.5	343.8
+4		4.7	344.6
1/4		4.5	344.8
+15	FEHP	4.47	344.86
Z		4.80	345.13
+7.5	WEP	4.43	344.90
1/4		4.5	344.8
cb		4.5	344.8
1/4		4.3	345.1

500.11

1/4		4.8	345.1
+5		4.1	345.2

349.33

cb	5.1	344.2
1/4	5.0	344.3
+1.5 HEDP	5.03	344.30
±	4.83	344.50
+7.5 FEHP	5.05	344.28
1/4	5.1	344.2
cb	5.2	344.1
+9	5.1	343.9
F	5.0	344.3
550'N		
F	5.6	343.7
+1	5.9	343.4
cb	5.9	343.4
1/4	5.7	343.6
+1.5 FEHP	5.73	343.60
±	5.53	343.80
+7.5 HEDP	5.73	343.70
1/4	5.7	343.6
cb	5.6	343.7
1/4	4.8	344.5
Trojan Ave 600'N = 5.2 (Florence) From East		
1/4	4.7	344.6
+5	5.1	344.4
cb	5.8	343.5
1/4	6.1	343.4
+1.5 HEDP	6.15	343.18
±	6.02	343.21

Florence
6' deep
12' x 25'
9' x 15'

349.33

+7.5 FEHP	6.29	343.04
1/4	6.2	343.1
+1	5.8	343.5
cb	5.7	343.6
F	6.3	343.0
+14 (5 cb)?		
F	6.6	342.7
12' Corp Drain	6.09	343.24
Flow Line	7.95	341.38
+7	6.0	343.3
cb	5.6	343.7
+3	6.0	343.3
1/4	6.2	343.1
+1.5 FEHP	6.21	343.07
±	5.99	343.34
+7.5 HEDP	6.13	343.20
1/4	6.2	343.1
+6	6.09	343.24
Flow Line	7.76	341.57
cb	6.8	342.5
+2	6.6	342.7
+3	5.0	342.3
1/4	5.0	342.3
+27 (1/4)?		
1/4	5.3	342.0
+7	5.0	342.3
+10	6.1	342.9

Existing 12' Corp
Drain
on S Chloffe Florence
Top Handrail

Top Handrail

349.33

Cb		15	342.8
+3		55	343.8
+5		59	343.6
1/4		61	343.2
+1.5	W E P	67	343.21
2		597	343.36
+7.5	F E P	622	343.11
1/4		68	343.1
+1		62	343.1
Cb		59	343.4
F		67	343.6
	+40 ? (2) Fiacco) TROJAN AIF		
F		63	343.0
Cb		61	343.2
1/4		60	343.3
+1.5	F E P	618	343.17
2		592	343.41
+7.5	W E P	610	343.23
1/4		60	343.3
+4		58	343.5
+5		52	344.1
+7		56	343.7
Cb		68	342.5
+2		67	342.6
+3		56	343.7
X		59	343.9

+53

(12)?

349.33

X		58	343.5
+9		57	343.6
+11		69	342.4
Cb		68	342.7
+2		53	344.0
+1		51	344.2
+5		58	343.5
1/4		59	343.4
+1.5	W E P	600	343.33
2		582	343.51
+7.5	F E P	607	343.26
1/4		61	343.2
Cb		59	343.4
F		64	342.9
	NL + 6 (Cb)?		
F		64	342.9
Cb		60	343.3
1/4		59	343.4
+1.5	F E P	600	343.33
2		574	343.59
+7.5	W E P	593	343.40
1/4		60	343.3
+1		57	343.6
+5		51	344.2
Cb		66	342.7
X		57	343.6

NL + 70

(NL)

349.33

W		57	343.6
Cb		57	343.6
+5		53	344.0
+6		56	343.7
1/4		59	343.4
+1.5	WEDP	58.2	343.51
±		56.3	343.70
+2.5	FFAP	57.9	343.44
1/4		59	343.4
Cb		59	343.4
F		62	343.1
	40 120N		
F		57	343.6
Cb		60	343.3
+5		55	343.8
1/4		57	343.6
+1.5	FFAP	56.8	343.65
±		57.7	343.82
+2.5	WEDP	56.7	343.66
1/4		58	343.5
+6		57	343.6
Cb		63	343.0
+2		65	342.8
+3		60	343.3
W		56	343.7
	90 120N		
W		61	343.2

349.33

+6		63	343.0
+7		68	342.5
Cb		67	342.6
+1		60	343.3
1/4		59	343.9
+1.5	WEDP	58.8	343.95
±		58.0	344.13
+2.5	FFAP	57.4	343.89
1/4		55	343.8
+2		54	343.9
Cb		58	343.5
F		55	343.8
	140 120N	80	
F		52	344.1
Cb		53	344.0
1/4		53	344.0
+1.5	FFAP	51.6	344.17
±		48.8	344.45
+2.5	WEDP	50.7	344.76
1/4		51	344.2
+4		52	344.1
Cb		57	343.6
+3		62	343.1
W		59	343.4
	190 120N		
W		54	343.9
Cb		58	343.5

349.33

+3		51	344.2
1/4		49	344.4
11.5	NEAP	486	344.49
Z		464	344.69
17.5	FEAP	489	344.44
1/4		5.2	344.1
CB		5.0	344.3
F		5.0	344.3
	240 22077		
F		41	345.2
CB		48	344.5
1/4		4.6	344.7
11.5	FEAP	453	344.80
Z		412	345.21
17.5	NEAP	419	345.14
1/4		4.2	345.1
12.		4.2	345.1
CB		5.3	344.0
15		5.2	344.1
X		48	344.5
	290 27077		
X		41	345.2
CB		43	345.0
16		38	345.5
1/4		3.7	345.6
11.5	NEP	363	345.70
Z		367	345.66

349.33

50

17.5 FEAP		4.07	345.26
1/4		4.2	345.1
16		4.3	345.1
CB		4.0	345.3
F		3.5	345.8
	314.3 294.3 N-SL E/Cajon coast		
F		3.6	345.7
19		4.1	345.1
CB		4.1	345.2
13 FEAP		3.84	345.45
1/4		3.55	345.78
Z		3.41	345.87
1/4		3.74	345.63
Gutter		4.01	345.09
CB Top		3.57	345.76 on CB top
X		3.6	345.7
B.M		1.18	348.21
	314.3 294.3 N-SL E/Cajon on Diagonal		
	325.3 305.3 N-SL E		
X		3.6	345.7
CB Top		3.57	345.76
Gutter Tapping		4.24	345.09
1/4		3.62	345.71
Z		3.38	345.95
1/4		3.65	345.68
CB		4.18	345.45
F		3.50	345.83

Gross Section Alley Block 224 SD Land & Town Co.
 Between Julian & Irving
 From Evans to Simpson

Roofside

BN	547	8748	8201	117	Julian + Evans
		010 = F.L. Evans			
S		35	840		
Top Ch		368	8380	00	Palacio
S		323	842		
+4		32	843		
+6		26	849		
N		31	844		
Top Ch		384	8354	02	Ch. Palacio
TP	654	9297	8623		
		8' F			
N		40	88.8		
+3		44	88.4		
+7		70	85.8		
S		75	85.3		
+6		70	85.8		
S		45	88.3		
		28' F			
S		397	88.80	02	Con. Plak
S		41	88.4		
S		54	87.4		
+4		52	87.6	41' E	Top Plak
N		37	89.1	4.33	41' Plak
		45' F			
N		34	89.4		
S		42	88.6		

92.97

51
 4-14-24
 S. 2507
 Glass
 Harbans

S	100' Floor	42	88.6		
S	Garage 2nd Floor	3.88	88.89		
	75' F				Do Garage 2nd Floor 60' E
S		3.8	89.0		11' 11"
S		4.2	88.6		3.8 90'
N		3.8	89.0		
	100' F				18' E Garage 2nd Floor on S.L.
N		3.8	89.0		4.6 80'
S		4.6	88.2		
S		4.5	88.3		
	125' F				
S		5.0	87.8		
S		4.8	88.0		
N		4.5	88.3		
	150' F				
N		4.2	88.6		
+6		5.0	87.8		
S		5.0	87.8		
+5		4.8	88.0		
S		4.9	87.9		
	175' F				
S		4.9	87.9		Do Garage 2nd Floor 187' E on N.L.
+4		4.9	87.9		4.70 40'
S		5.2	87.6		
N		4.5	88.3		Garage 2nd Floor 194' E on S.L.
	200' F				5.20 50'
S		5.7	87.6		

92.77

Z		54	87.4	
+3		54	87.4	
N		47	88.2	
		2.25 F		
-1	Garage Dirt Floor	49	87.9	218 F on S1 Garage Dirt 5.70 W
N		50	87.8	
+6		58	87.0	
Z		58	87.0	
S		56	87.2	
		2.50 F		
S		61	86.7	
Z		60	86.8	
N		52	87.5	
		2.75 F		
N		58	87.0	
+6		65	86.3	
Z		64	86.4	
S		66	86.2	
		3.00 F		
	Conc Walk	650	87.9	288 F Garage Dirt Floor 2.50 W 6.70 W
S		68	86.0	
Z		71	85.7	295 F on N1 Garage Dirt Floor 6.20 W
N		61	86.7	
		3.25 F		
N		69	85.9	320 F Top Man Hole 7.53 W
Z		78	85.0	
+3		78	85.0	

92.77

S		73	85.5	
		3.50 F		
S		81	84.7	
+5		89	83.9	
Z		84	84.4	358 F on N1 Garage Wood Floor 7.40 W
N		79	84.9	
		3.75 F		
N		92	83.6	
Z		97	83.1	
+3		98	83.0	
S		90	83.8	
		4.00 F		
S		97	83.1	
Z		100	82.8	
N		96	83.7	
TP	5.67	88.25	10.04	82.73
		4.35 F		
-4	Do Garage Dirt Floor.	53	83.1	
N		51	83.0	
Z		57	82.7	
S		58	82.6	
		4.55 F		
S		52	83.7	
Z		54	83.0	
N		52	83.7	
		4.75 F		
N		51	83.3	

52

88.35

E		51	83.3	
+7		54	83.0	
S		50	83.4	487' E
	500' E			558' E Garage Dirt Floor 540' 83.15
S		52	83.2	
Z		57	87.7	
N		55	87.9	
	575' E			
N		51	83.0	540' E 355' S 50' Garage Dirt Floor
Z		53	83.1	57' 83.1
S		55	82.9	
	560' E			
S	Garage Dirt Floor	51	83.3	
Z		49	83.5	
N		50	83.4	
	600' E = H.L. Sampson			
N		50	83.4	
	Top Curb	430	84.05	on Cb Return
Z	Top M.Hole	499	83.36	
S		51	83.3	
	Top Curb	472	83.53	on Cb Return
B/N		778	80.57	N of Station 4 Sampson 80.57

^{NAS}
 Crosswalk Block 3 S Garwell Hights
 Between 30th & 31st From Palm to Ounce 16' wide

312.60

54
 4-15-21
 3-5-20
 9-1-17
 Harbor

	11.60	312.60	301.00	SW 30th x Palm
				010 - N x Palm
H Top Cb Rd		5.45	307.15	
Top Parking		5.51	307.09	
2 "		5.74	306.86	
F "		5.51	307.06	
E Top Cb Rd		5.46	307.14	
		4.11		
E		4.7	307.9	
2		5.0	307.6	
+6		5.2	307.4	
H		5.0	307.6	
		25.11		
H		4.8	307.8	
2		4.4	308.0	
E		4.4	308.0	
Top Conc Walk		4.57	308.03	
		5.0.11		
Top Conc Walk				
		4.77	307.83	
E		4.8	307.8	
2		4.7	307.9	
H		4.6	308.0	
		7.0.11		
H		4.4	308.0	
2		4.6	308.0	

E		4.7	308.1	
		8.1.11		
E		4.8	307.8	
2		4.4	308.2	
2		4.0	308.6	
2.6		4.5	308.1	Garage Driv Floor 10.5' x 11.4'
H		4.6	308.0	4.24 - 308.26
		10.0.11		
H		4.7	308.2	
2		4.4	308.2	
E		4.7	307.9	Dr Garage Driv Floor 11.5' x 11.4'
		12.7.11		4.8
E		4.9	307.7	
2		4.8	307.8	
H		4.9	307.7	
		13.5.11		
H		4.7	307.9	
2		4.6	308.0	
2.5		4.6	308.0	
E		5.0	307.6	
		14.3.11		
E		4.6	308.0	
2		4.6	308.0	
H		4.7	307.9	
TP	4.97	312.75	4.32	308.28
			16.0.11	
			3.8	308.77

2.5 4.0 1.9 4.0 Conc Floor

3.8

312.75

N		44	308.4
+	Conc # 7 pro	46	308.49
±		45	308.3
E		44	308.4
	S. End 7 Ga. rapids Conc Floor	47	307.98
	175 No		
E		44	308.0
±		47	308.1
N		46	308.2
	205 N		
N		48	308.0
±		48	308.0
E		48	308.0
	213 N		
-16	N End 7 Ga rapids Conc Floor	47	307.97
E		46	308.2
±		45	308.3
N		44	308.4
	217 No		
	230 N		
N		44	308.4
±		47	308.1
+4		47	308.1
E		45	308.3
	252 N		
E		49	308.1
±		48	308.0
+4		49	307.9

312.75

55

N		47	308.1
	270 N = S.L. Quince		
N	Top Ch Bed	50	307.71
N		52	307.5
+3		57	307.1
±		56	307.2
+3		53	307.5
E		51	307.4
	Top Ch Bed	53	307.87

Goos Section East Alley Block 3 S Ger Well Hpts
From E.L. N + S Alley to 300' East

312.75

0 + 0 = E.L. Has Alley

S	51
E	51
N	49

15'E

N	50
E	52
S	52

21'E

S	54
E	51
N	49

Conc Apron

99

+5 Dr Garage Conc Floor	98
-------------------------	----

50'E

N	51
E	55
S	55

6'E
Garage Dirt Floor

55.5

75'E

S	55
E	56
N	51

100'E

N	55
E	53
S	51

312.75

125'E

S	52
E	51
N	51

141'E

141'E

N	50
E	50
S	51

+3 Garage Conc Floor	500
----------------------	-----

160'E

S	54
E	52
N	51

+3 Garage Dirt Floor	52
----------------------	----

190'E

N	62
E	62
S	66

200'E

S	73
E	74
N	74

225'E

N	98
E	98
S	97

31275

250'E

S 118

E 118

H 120

275'E

H 146

E 148

S 149

290'E

S 163

E 162

+4 162

H 166

+ L Garage Dirt Floor 167

300'E

H 185

E 182

S 182

TP 489 31244 520 307.55

BM 11.43 301.01 514
Elevat. 301.01

57

8/25/21 G.C.

60

Elevations on State Highway near
Grossmont.

1. Top of Pavment at Cuyamaca Flume
Xing near Grossmont Store Elev = 650.2 ±
U.S.G.S. Datum.
2. B.M. #1 N.Ely. City Limits of La Mesa
Nail in tel. pole 40' left of sta. 0+08.
Elev = 613.09
3. B.M. #3 at Summit of Grade 21' left
of Sta 19+64 Nail in tel. pole. El. = 713.95
all U.S.G.S. Datum.
Info. from Co. Surveyors Office. (G.C.)

Elevations on State Highway near
Santee

1. Top of parment at low point in curve
near Santee junction Elev = 363.93 U.S.G.S.
2. Top of Pavment 2600' N. of Santee
Lowest point in highway bet. El Cajon
and Lakeside. Elev. 361.30 U.S.G.S.
Info. from Co. Highway Com. (G.C.)

254.26
150
104-26

5687

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1½ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

123
26
2