Alley Blk 74 Parkville 1-2 cross sections

UPAS-ST. STATE & MORTON 3-7 "

UNION - UPAS TO WALNUT 8-17 "

WALNUT - UNION & STATE 18-21 "

" ST CULVERT " " 19 Levels

STATE - WALNUT & GLEN 22-25 cross section

" CULVERT WALNUT 26 Levels

" " GLENWOOD 27 "

CULVERT BLK 81 Middleton Add 28 "

ALLEY BLK 61 Winders 29 Cross Section

PENNSYLVANIA Kitch & Jack 30-32 "

WALNUT - LARK & UNION 33 Sewer Levels

GLENWOOD DR Thru State ST 37.

STATE - VINE intersect 34

Crosby St. Logan to End. 50-60

Alley Block-1-Palm #Ts. - 46

15' wide X-See Alley Blk 74 Park Villas Landis to Dwight et Arnold + Villa Terrace 11-12-26 Miller

B.M.	12.67	304.52		291.85	SE Arnold & Landis
		00 = S. line Landis			
W			153	302.99	cmt el
C			1.2	303.3	
E			0.6	303.9	dirt
E			0.12	304.40	cmt el
T.P.	0.90	303.60	1.82	302.70	
	44' S. garage on W. cmt floor 3.5 Back				
E			2.1	301.5	
C			2.5	301.1	
W			3.0	300.6	cmt apron
	60' S = garage on W dirt floor 4.5 Back				
W			3.8	299.8	floor
C			3.2	300.4	
E			2.5	301.1	
	100' S				
E			3.7	299.9	
C			3.9	299.7	
W			3.8	299.8	
	140' S				
W			3.6	300.0	
C			4.0	299.6	
E			3.5	300.1	

303.60

157' S garage on W dirt floor 3.5 Back

E	3.7	299.9	
C	4.2	299.4	
W	4.3	299.3	floor
	200' S		
W	3.7	299.9	
C	3.6	300.0	
E	3.2	300.4	
	214' S		
E	3.4	300.2	
C	3.3	300.3	
W	3.5	300.1	
	230' S garage on W. cmt floor 6.5 Back		
W	3.3	300.3	
C	3.4	300.2	
E	3.3	300.3	
	260' S		
E	4.1	299.5	
C	4.2	299.4	
W	4.2	299.4	
	292' S garage on W dirt floor 3.5 Back		
W	5.3	298.3	floor
C	5.0	298.6	
E	4.7	298.9	
	335' S		
E	5.0	298.6	
C	5.4	298.2	
W	5.2	298.4	

303.60

360's

W		6.3	297.3	
C		6.0	297.6	
E		5.4	298.2	
	392's garage on W cmt floor 8.5 Back			
E		6.3	297.3	
C		6.4	297.2	
W		6.7	296.9	
+4.5		6.7	296.9	cmt apron
	408's garage on W dirt floor 10' Back			
	424's garage on E dirt floor 4.5 Back			
W		7.5	296.1	
C		7.4	296.2	
E		7.5	296.1	
+4.5		7.1	296.5	floor
	450's			
E		8.2	295.4	
C		8.1	295.5	
W		8.1	295.5	
	470's			
W		9.5	294.1	
C		9.2	294.4	
E		9.1	294.5	
	492's garage on W cmt floor 7.5 Back			
E		9.7	293.9	
C		9.9	293.7	
W		10.1	293.5	
+7.5		9.6	294.0	floor

Alley Blk 74 P.V. 2

303.60

525's

W		10.7	292.9	
C		10.7	292.9	
E		10.8	292.8	
	545's garage on W dirt floor 0.5 in Alley			
E		11.3	292.3	
C		11.4	292.2	
W		11.1	292.5	floor
	570's			
W		11.6	292.0	
C		11.5	292.1	
E		11.5	292.1	
	600's = N. Line Dwight			
E		11.17	292.43	cl
C		11.62	291.98	Paving
C		11.8	291.8	
W		11.85	291.75	Paving
W		11.70	291.90	cl

Moore 12/3/96 — Ubas St. Cross Section — State to Horton — 50' wide, 10' cbs

℄ Mon	172.90	172.12		159.21	Ubas State
	El State = 0+00				
-15			8.1	164.0	
^/			6.8	165.3	
cb			4.5	167.6	
1/4			3.2	168.9	
c			1.8	170.3	
1/4			1.2	170.9	
cb			0.3	171.8	
TP	172.41	184.52	0.00	172.12	
S			11.7	172.8	
	0+72				
S			7.0	177.5	
cb			7.7	176.8	
1/4			8.8	175.7	
c			10.2	174.3	
1/4			11.6	172.9	
cb			12.4	172.1	
^			14.2	170.3	
+10			15.4	169.1	
	0+37				
-10			12.1	172.4	
^/			11.4	173.1	
cb			10.2	174.3	
1/4			9.2	175.3	
c			8.1	176.4	

184.52

1/4		6.6	177.9
cb		5.6	178.9
S		4.9	179.6
	0+50		
S		2.9	181.6
cb		3.6	180.9
1/4		4.2	180.0
C		5.1	179.4
1/4		6.1	178.4
cb		6.5	178.0
^/		5.0	176.5
+10		9.4	175.1
TP to Bole	172.60	197.12	0.00	184.52
	0+65		
-5		16.2	180.7
^/		16.1	181.0
cb		15.5	181.6
1/4		15.1	182.0
C		14.4	182.7
1/4		14.0	183.1
cb		13.8	183.3
S		13.1	184.0
	0+80		
S		10.9	186.2
cb		11.3	185.8
1/4		11.5	185.6

1971 ✓

C	12.1	185.0 ✓	
1/4	12.5	184.6 ✓	
eb	12.9	184.2 ✓	
✓	13.8	183.3 ✓	
+5	14.0	183.1 ✓	
0+95			
-5	11.5	185.6 ✓	
✓	11.0	186.1 ✓	
eb	11.5	185.6 ✓	
1/5	10.0	187.1 ✓	
C	9.6	187.5 ✓	
1/4	8.8	188.3 ✓	
eb	8.9	188.2 ✓	
S	8.7	188.4 ✓	
1+03			
S	6.5	190.6 ✓	
eb	7.6	189.5 ✓	
1/5	7.8	189.3 ✓	
e	8.1	189.0 ✓	
1/4	8.2	188.9 ✓	
eb	8.2	188.9 ✓	
✓	9.4	187.7 ✓	
+5	10.0	187.1 ✓	
1+10			
S & double garage dirt floor	6.3	190.8 ✓	ON LINE

1971 ✓ Spas 4

1+18			
-5	7.6	189.5 ✓	
✓	7.5	189.6 ✓	
eb	7.2	189.9 ✓	
1/4	7.0	190.1 ✓	
e	5.5	191.6 ✓	
1/4	5.4	191.7 ✓	
eb	5.3	191.8 ✓	
S	5.3	191.8 ✓	
1+35			
S	2.1	195.0 ✓	
eb	2.3	194.8 ✓	
1/5	2.6	194.5 ✓	
e	2.7	194.4 ✓	
1/4	3.1	194.0 ✓	
eb	3.9	193.2 ✓	
✓	4.3	192.8 ✓	
+5	4.5	192.7 ✓	
TP 1197 ✓08.96 ✓	0.13	196.99 ✓	
1+60			
-5	12.0	197.0 ✓	
✓	11.6	197.4 ✓	
eb	11.3	197.7 ✓	
1/4	11.2	197.8 ✓	
e	10.9	198.1 ✓	
1/4	10.7	198.3 ✓	

	20896				
cb		10.0	199.0		
S		9.6	199.4		
	2+00 = WL Union			75' und.	
S		2.3	206.7	in cbs	
cb		2.4	206.6	12:25 11/5	
1/4		2.8	206.2		
e		2.7	206.3		
1/4		2.9	206.1		
cb		3.6	205.4		
~		4.4	204.6		
	w/cb				
~		2.1	206.9		
cb		1.5	207.5		
1/4		1.1	207.9		
c		0.8	208.2		
1/4		0.7	208.3		
cb		0.4	208.6		
TP	12:55	+10.8	208.2	rock	
S		11.7	209.1		
	w/ 1/4				
S		9.1	211.7		
cb		9.8	211.0		
1/4		10.0	210.8		
c		10.5	210.3		
1/4		10.7	210.1		
cb		10.7	210.1		

220.8

Ups

~		10.7	210.1
	℄		
~		8.8	212.0
cb		8.0	212.8
1/4		7.6	213.2
c		7.4	213.4
1/4		7.2	213.6
cb		6.8	214.0
S		6.4	214.4
	E 1/4		
S		5.1	215.7
cb		5.1	215.7
1/4		5.4	215.4
c		5.4	215.4
1/4		5.8	215.0
cb		6.0	214.8
~		6.8	214.0
	E cb		
~		6.0	214.8
cb		5.1	215.7
1/4		4.9	215.9
c		4.5	216.3
1/4		4.5	216.3
cb		4.4	216.4
S		4.5	216.3

220.8

EL UNION = 0+00

S			3.1	217.7
cb			3.4	217.4
1/4			3.6	217.2
P			3.7	217.1
1/4			3.6	217.2
cb			4.5	216.3
∧			5.5	215.3
	0+15			
∧			3.6	217.2
cb			2.8	218.0
1/4			2.5	218.3
C			1.9	218.9
1/4			1.2	219.6
cb			0.5	220.3
S			0.1	220.7
T.P	11.04	3.171	0.15	220.67
	0+32			
S			9.2	222.5
cb			9.0	222.7
+4			9.5	222.2
1/4			10.7	221.0
C			11.3	220.4
1/4			11.6	220.1
cb			11.4	220.3
∧			12.0	219.7

231.7

0+67

∧	9.1	222.6
cb	8.5	223.2
1/4	8.7	223.0
C	8.9	222.8
+3	9.2	222.5
+4	8.3	223.4
1/4	8.0	223.7
+3	7.2	224.5
cb	7.4	224.3
S	7.8	223.9
	1+00	
S	7.7	224.0
cb	6.8	224.9
1/4	6.6	225.1
+3	7.6	224.1
C	7.4	224.3
1/4	6.9	224.8
cb	6.9	224.8
∧	7.3	224.4
	1+25	
∧	5.8	225.9
cb	5.9	225.8
1/4	6.1	225.6
C	6.4	225.3
1/4	7.5	224.2

cb			8.2	223.5 ✓
S			8.4	223.3 ✓
	1+50			
S			8.0	223.7 ✓
cb			7.2	224.5 ✓
1/4			6.1	225.6 ✓
C			5.4	226.3 ✓
1/4			5.2	226.5 ✓
cb.			4.8	226.9 ✓
~/			4.9	226.8 ✓
	1+75			
~/			3.6	228.1 ✓
cb			3.8	227.9 ✓
+5			3.6	228.1 ✓
1/4			4.7	227.0 ✓
C			5.2	226.5 ✓
1/4			6.0	225.7 ✓
cb			6.8	224.9 ✓
S			7.7	224.0 ✓
	1+99.5 = WL HORTON ✓			
S			7.5	224.2 ✓
cb			6.2	225.5 ✓
1/4			5.7	226.0 ✓
+5			4.4	227.3 ✓
C			4.4	227.3 ✓
1/4			4.1	227.6 ✓

cb		3.8	227.9 ✓
~/		2.8	228.9 ✓

Cross Section of Union 57.75 wide
Ubas to Walnut
12 cbs

cb	TP 0.15	↓0.82	220.67	
S	↓ Ubas=00			
	E	-5.6	210.2	
S	cb	6.1	214.7	
cb	1/4	6.9	213.9	
1/4	c	9.0	211.8	
c	1/4	10.9	209.9	
1/4	cb	14.2	206.6	
cb.	w/	16.3	204.5	
w/	0+25			
	-10	20.3	200.5	
w/	w/	18.3	202.5	
cb	cb	14.9	205.9	
+5	1/4	12.7	208.1	
1/4	c	10.2	210.6	
c	1/4 +7	8.7	212.1	
	1/4	8.3	212.5	
c	1/4	8.1	212.7	
cb	+4	8.2	212.4	
S	+10	7.4	213.4	
	E	6.2	214.6	
S	0+50			
cb	E	7.0	213.8	
1/4	+4	8.2	212.6	
+5	+7	9.9	210.9	
c	cb	10.1	210.7	
1/4	1/4	10.4	210.4	

220.82

		14.00+	
		12/3/26	
	+10	10.8	210.0
	c	11.9	208.9
	1/4	15.0	205.8
	cb	17.7	203.1
	w/	19.4	201.4
	+10	21.1	199.7
	0+75		
	-15	24.0	196.8
	w/	21.7	199.1
	+7	21.3	199.5
	+9	19.5	201.3
	cb	19.2	201.6
	1/4	16.8	204.0
	c	13.2	207.6
	1/4	12.5	208.3
	+8	12.7	208.1
	cb	14.1	206.7
	+5	12.5	208.3
	+7	10.6	210.4
	E	9.2	211.6
	1+00		
	E	10.9	209.9
	+10	12.7	208.1
	T.P. 0.95	↓08.99	12.78 ↓08.84
	cb	2.6	206.4
	1/4	3.7	205.3

208.99

1/4+1			2.5	206.5
C			3.1	205.9
+5			3.5	205.5
1/4			5.5	203.5
+10			8.2	200.8
C6			9.6	199.4
+2			10.6	198.4
W/			12.0	197.0
+15			14.1	194.9
	1+35			
-9	& cem drive	Tuvido	15.5	193.5
W/			15.0	194.0
+6			14.1	194.9
+7			13.0	196.0
C6			12.2	196.8
+3			9.4	199.6
1/4			6.6	202.4
+4			5.6	203.4
C			5.1	203.9
+9			5.2	203.8
1/4			5.9	203.1
2			5.0	204.0
+5			4.6	204.4
+7			3.4	205.6
C6			2.6	206.4
+9			1.8	207.2

208.99

E	0.5	208.5
1+59		
E	0.7	208.3
C6	3.7	205.3
1/4	5.9	203.1
7.5	6.7	202.3
C	6.3	202.7
1/4	6.7	202.3
+10	9.7	199.3
C6	12.8	196.2
+6	13.8	195.2
+7	14.8	194.2
W/	15.2	193.8
+11 & Residence	14.4	194.6 for elev.
1+80		
-10	16.0	193.0
W/	15.0	194.0
+5	14.8	194.2
+10	13.3	195.7
C6	11.0	196.0
1/4	8.0	201.0
C	7.5	201.5
+8	7.6	201.4
1/4	4.1	204.6
C6	3.1	205.9
+10	2.2	206.8
E	0.7	208.3

Various 9

		2+00		
E		0.3	208.7	
+5		2.9	206.1	
c6		3.6	205.4	
1/4		4.7	204.3	
+2		5.1	203.9	
+7		9.2	199.8	
C		9.1	199.9	
1/4		9.0	200.0	
+8		9.2	199.8	
c6		11.1	197.9	
+4		14.0	195.0	
W		12.8	194.2	
+10		17.2	191.8	
		2+32		
-10	top bank		18.1	190.9
-10	bottom "	in yard	20.6	188.4
-5	"	" "	20.4	188.6
W			15.4	193.6
+8			14.9	194.1
c6			12.2	196.8
+2			11.3	197.7
1/4			10.8	198.2
C			11.3	197.7
+5			11.8	197.2
+9			5.2	203.8

1/4		4.8	204.2
c6		4.1	204.9
+9		3.1	205.9
E		0.1	208.9
	2+59		
E		0.1	208.9
+2		2.7	206.3
c6		4.5	204.5
1/4		5.7	203.3
+2		7.4	201.6
+7		13.0	196.0
C		13.3	195.7
1/4		12.6	196.4
c6		13.0	196.0
+3		15.6	193.4
W		16.0	193.0
+13 & residence		20.0	189.0 on conc. porch
	2+80		
-10	bottom bank inward	10.2	188.8
-10	top "	18.0	191.0
W		16.3	192.7
c6		14.5	194.5
1/4		14.1	194.9
C		14.0	195.0
+5		13.4	195.6
+10		6.3	202.7

		208.99					208.79	Union	11
1/4			5.8	203.2		c6	5.2	203.6	
c6			5.1	203.9		+8	4.0	204.8	
+8			4.0	205.0		+11	2.2	206.6	
E			+0.3	209.3		E	+0.1	208.9	
T.P.	5.48	208.79	5.68	203.31		+3 top bank	+3.9	212.7	
	3+00					3+45.5 = SL Vine			50' wide
– r	top bank		+3.5	218.3		– r top bank	+2.0	210.8	10' obs
E			+0.5	209.3		E	1.0	207.8	
+r			-2.1	206.4		+r	3.2	205.6	
+5			4.3	204.5		+6	4.8	204.0	
c6			5.3	203.5		c6	5.6	203.2	
1/4			6.1	202.7		1/4	6.8	202.0	
+7			13.8	195.0		+5	16.0	192.8	
C			15.1	193.7		C	18.2	190.6	
1/4			15.7	193.1		1/4	19.6	189.2	
c6			15.5	193.3		c6	19.8	189.0	
w			17.9	190.9		w	19.2	189.6	
+10			19.2	189.6		Sc6 Vine			
	3+15					w	19.9	188.9	
– 10			19.8	189.0		c6	20.7	188.1	
w			17.6	191.2		1/4	20.5	188.3	
c6			16.7	192.1		+10	20.7	188.1	
1/4			17.2	191.6		C	18.5	190.3	
C			16.5	192.3		+9	15.6	193.2	
+8			12.9	195.9		1/4	6.6	202.2	
1/4			6.3	202.5		c6	5.0	202.8	

20879

cb +9		2.9	204.9
E		1.1	207.7
+v	tob bank	+1.5	210.3
	N/L		
-3	tob bank	+1.2	210.1
E		2.0	206.8
+4		4.8	204.0
cb		6.0	202.8
1/4		6.7	202.1
+3		15.6	203.2
E		18.4	190.6
+3		19.0	189.8
+5		21.4	187.6
1/4		21.3	187.5
cb		21.3	187.5
4		20.6	188.2
	E line		
4		21.3	187.5
cb		22.2	186.6
1/4		22.3	186.5
E		21.1	187.7
+9		16.5	192.3
1/4		7.1	201.7
cb		6.7	202.1
+7		5.5	203.3
E		2.6	206.2
+3	tob bank	+0.9	209.7

20879

	N 1/4 line		
-3		+0.6	209.4
E		2.6	206.2
+5		5.6	203.2
cb		7.1	201.7
+11		7.5	201.3
1/4		17.9	190.9
C		22.3	186.5
1/4		22.9	185.9
.6		23.1	185.7
4		22.3	186.5
	N. cb line		
4		23.	185.4
cb		24.1	184.7
1/4		23.9	184.9
C		22.7	186.1
1/4		20.0	188.8
+1		8.0	200.8
cb		7.4	201.4
+4		6.8	202.0
E		3.3	205.5
+3	tob bank	0.0	208.8
	N/L line = 0400		
-3		2.2	206.6
E		3.2	205.6
+4		5.9	202.9

		208.79		
E +8		7.5	201.3	
c6		7.8	201.0	
1/4		9.0	199.8	
+4		20.9	187.9	
C		24.4	184.4	
1/4		25.2	183.6	
c6		25.4	183.4	
w/		25.0	183.8	
	0+14			
-5	to bank	23	185.4	
w/		26.8	182.0	
c6		27.3	181.5	
1/4		27.4	181.4	
C		26.8	182.0	
+11		21.6	187.2	
1/4		14.8	194.0	
+2		10.1	198.7	
c6		8.7	200.1	
+7		7.1	201.7	
E		4.5	204.0	
+3	top bank	3.0	205.8	
	0+35			
E		8.8	200.0	
c6		11.6	197.2	
+9		13.1	195.7	
1/4		15.6	193.2	

		208.79		
1/4 +1		17.0	191.8	
+11		18.4	190.4	
C		29.0	179.8	
1/4		29.2	179.4	
c6		29.7	179.1	
w/		29.3	179.5	
+6	top bank	25.7	183.1	
	0+60			
-10		32.0	176.8	
w/		32.5	176.3	
c6		33.2	175.4	
1/4		33.2	175.6	
+7		32.9	175.9	
+11		31.2	177.4	
C		29.1	179.7	
+3		20.2	188.4	
1/4		18.3	190.3	
+4		16.3	192.3	
c6		15.0	193.8	
+6		15.1	193.7	
E		13.2	195.4	
T.P.	0.06	195.58	13.7	195.5
	0+80			
E		4.5	191.1	
c6		5.2	190.4	
+3		5.6	190.0	

		1958									
1/4			11.3	184.3							
+11			14.2	181.4							
C			17.3	178.3							
+8			23.6	172.0							
1/4			23.1	172.5							
c6			23.2	172.4							
W			20.8	174.8							
+10			22.2	173.4							
	1+12										
-10			28.6	167.0							
W			27.2	168.9							
c6			26.4	169.2							
1/4			27.8	167.8							
C			28.1	167.5							
+5			28.0	167.6							
+9			19.8	175.8							
1/4			18.2	177.2							
+4			17.1	178.5							
c6			11.6	184.0							
+4			8.9	186.7							
E			7.3	188.3							
	1+28										
E			9.0	186.6							
+3			9.5	186.1							
c6			15.5	180.1							
1/4			23.5	172.1							

		1958									
1/4 +4			29.5	166.1							
C			30.0	165.6							
1/4			29.2	166.4							
+7			29.0	166.6							
c6			30.7	164.9							
W			34.2	161.2							
+10			35.1	160.5							
		1+46									
-15			43.5	152.1							
W			41.3	154.3							
c6			37.1	158.5							
1/4			32.0	163.6							
C			31.7	163.9							
+11			33.1	162.5							
1/4			31.6	164.0							
+3			26.1	169.5							
c6			21.6	174.0							
E			15.2	180.2							
TP Hook Nail		048	183.75	17.3							
		1+57									
E			10.1	173.7							
T.P.		058	172.58	11.75							
c6			2.5	170.1							
+7			4.1	168.5							
1/4			11.5	161.1							
+2			10.8	161.8							

		172.58					159.45		15
C			10.3	162.3 ✓ ✓		1/4		10.9	148.6 ✓
1/4			10.3	162.3 ✓		C6		16.7	142.8 ✓
C6			16.7	155.9 ✓		W		20.4	139.1 ✓
W			21.7	150.9 ✓ ✓		+20		25.0	134.5 ✓ ✓
+15			25.0	147.6 ✓		2+15			
	1+70					−20		30.1	129.4 ✓
−15			30.1	142.5 ✓		W		25.8	133.7 ✓ ✓
W			25.8	146.8 ✓ ✓		C6		23.3	136.2 ✓
C6			22.0	150.6 ✓		1/4		19.4	140.1 ✓
1/4			15.8	156.8 ✓		C		13.6	145.9 ✓ ✓
+7			12.1	160.5 ✓		1/4		6.9	152.6 ✓
C			12.3	160.3 ✓ ✓		C6		7.3	152.2 ✓
1/4			12.9	159.7 ✓		E		6.5	153.0 ✓ ✓
+4			13.0	159.6 ✓		2+30			
+7			6.0	166.6 ✓		E		9.0	150.5 ✓ ✓
C6			4.7	167.9 ✓		C6		9.4	150.1 ✓
E			1.8	170.8 ✓ ✓		+8		9.0	150.5 ✓
	1+93					1/4		11.9	147.6 ✓
E			11.1	161.5 ✓ ✓		C		19.6	139.9 ✓ ✓
T.P.	0.13	159.45	13.26	159.32 ✓ ✓		1/4		24.1	135.1 ✓
+10			3.8	155.7 ✓		C6		25.4	134.3 ✓
C6			3.8	155.7 ✓		W		28.3	131.2 ✓ ✓
1/4			3.7	155.8 ✓		TP 3.71	151.63 ✓	11.53	147.9 ✓ ✓
+10			3.4	156.1 ✓		W+20		23.6	128.0 ✓
C			2.0	157.5 ✓ ✓		2+50 = wash			
+4			4.6	155.9 ✓		−20		23.3	128.3 ✓

15.63

w/	21.3	130.3	✓ ✓
c6	19.4	132.7	✓
1/4	17.4	134.2	✓
C	15.8	135.8	✓ ✓
+6	14.6	137.0	✓
1/4	9.9	141.7	✓
+9	4.0	147.6	✓
c6	4.1	147.5	✓
E	3.3	148.3	✓ ✓
	x+75		
E	15.5	146.1	✓ ✓
c6	15.6	146.0	✓
+3	15.7	145.9	✓
1/4	11.8	139.8	✓
C	14.6	137.0	✓ ✓
1/4	15.7	135.9	✓
c6	17.5	134.1	✓
w/	20.4	131.2	✓ ✓
+15	22.9	128.7	✓
	x+95		
-10	19.8	131.8	✓
w/	18.2	133.4	✓ ✓
c6	16.2	135.4	✓
1/4	13.9	137.7	✓
C	11.1	140.5	✓ ✓
1/4	8.2	143.4	✓

15.63

Vallon 16

c6	7.5	144.1	✓
E	7.3	144.3	✓ ✓
3+17 = 5% Walnut			to wide
E	5.7	145.9	1/4 c6
+3	7.5	144.1	✓ 1.3' 1/4 S
c6	8.9	142.7	✓
1/4	8.9	142.7	✓
+4	8.4	143.2	✓
C	10.7	140.9	✓ ✓
1/4	12.9	138.7	✓
c6	15.2	136.4	✓
w/	17.9	133.7	✓ ✓
S c6			
w/	18.9	132.7	✓ ✓
c6	16.6	135.0	✓
1/4	14.9	136.7	✓
C	11.4	140.2	✓ ✓
1/4	10.8	140.8	✓
c6	9.0	142.6	✓
+7	8.2	143.4	✓
E	1.1	150.5	✓ ✓
S 1/4			
E	2.6	149.0	✓ ✓
+7	4.7	146.9	✓
c6	9.9	141.7	✓
1/4	11.3	140.3	✓

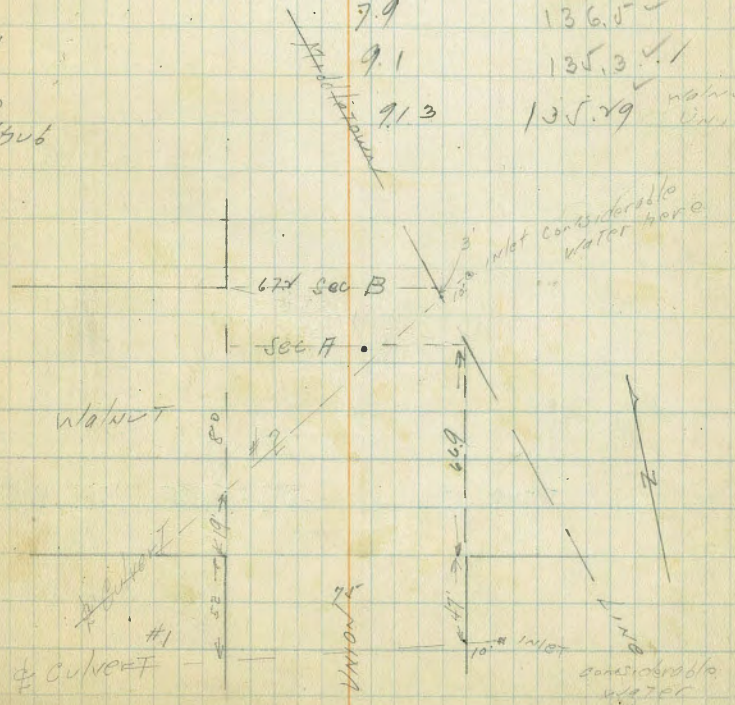
1511.63

C		13.6	138.0
1/4		15.8	135.8
cb		17.7	133.9
w/		18.7	132.9
	℄ walnut		
w/		18.3	133.3
cb		16.5	135.1
1/4		15.1	136.5
C		13.8	137.8
1/4		12.3	139.3
+10		10.0	141.6
cb		8.8	142.8
E		4.6	147.0
	N 1/4		
E		6.9	144.7
cb		10.4	141.2
1/4		11.8	139.8
C		12.0	137.6
1/4		15.6	136.0
cb		16.5	135.1
w/		17.3	134.3
TP	4.54	144.42	11.75	139.88
	0.9 N of NCb = Sec A		
w/		10.2	134.0
cb		9.5	134.9
1/4		7.8	136.6

1444 N

C		7.5	136.9
1/4		5.9	138.5
cb		4.9	139.5
+10		3.6	140.8
E		2.2	142.2
	N1 walnut - Sec B		
cb - 7.8		3.6	140.8
cb		3.8	140.6
1/4		4.9	139.5
C		6.0	138.4
1/4		6.8	137.6
cb		7.9	136.5
w/		9.1	135.3
T.P. N 1/4 Sec 6		9.13	135.29

walnut

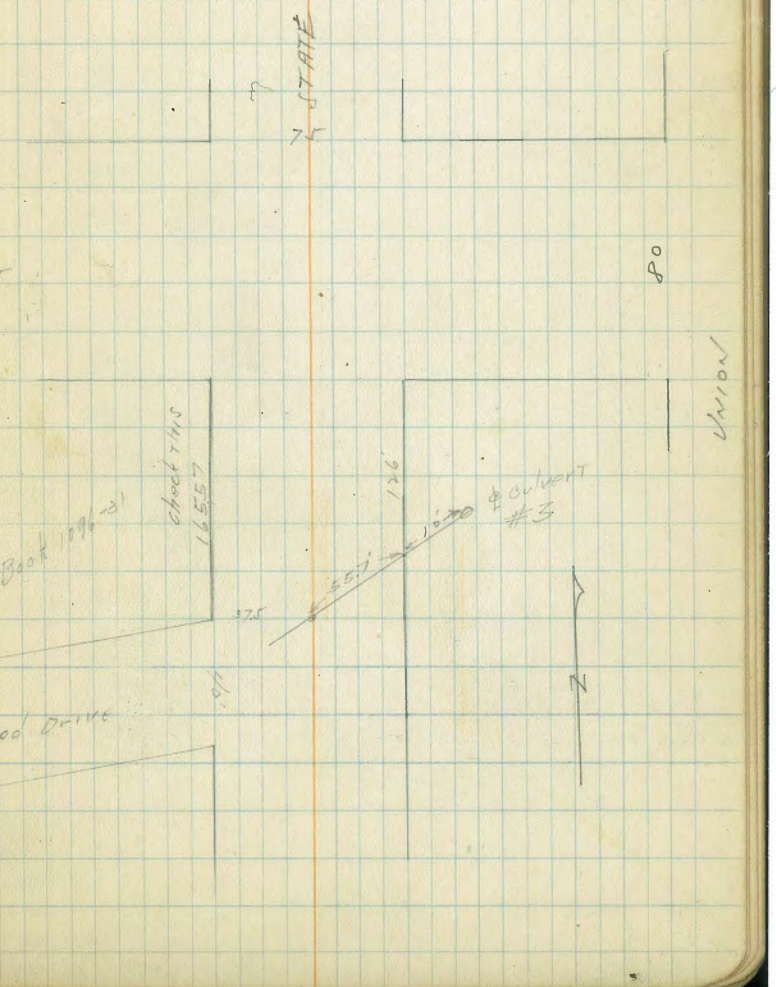


Cross Section of Walnut
Union to State

80' wide
14' cbs
13' 1/2S

NW Hub	3.3	138.4		135.1	Walnut Union
W L Union = 0+00					
℄			3.1	135.3	
cb			4.2	134.2	
1/4			4.1	134.3	
e			3.0	133.4	
1/4			5.5	132.9	
cb			5.7	132.7	
S			4.6	133.8	
	0+25				
-10			9.5	128.9	
S			10.0	128.4	
cb			8.6	129.8	
1/4			7.8	130.6	
e			7.2	131.2	
+9			6.8	131.6	
1/4			5.8	132.6	
cb			5.5	132.6	
℄			5.1	133.3	
	0+50				
℄			6.7	131.7	
cb			7.2	131.2	
1/4			7.7	130.7	
c			9.3	129.1	
1/4			10.1	128.3	
cb			10.8	127.6	

cont. page 20



Levels for Culvert #1

Seabago 17

NW Hub	147.53		135.29	Walnut Union
10' E of EL Union = 00 = inlet		0.0	147.5	
0+10 = EL Union		1.3	146.2	
0+24		0.8	146.7	
0+40		9.6	137.9	
0+60		13.6	133.9	
0+85		16.5	131.0	
1+05 = outlet		19.2	128.3	

Levels for Culvert #2

10' E of L Middleton Inlet line = 00	147.53	6.1	141.4
0+10		7.2	140.3
0+45		9.2	138.3
0+75		11.4	136.1
1+00 approx 19' N of SL Walnut W/L Union		15.2	132.3
1+55 = outlet approx 16' South of SL Walnut		21.4	126.0

Levels for Culvert #3

117.28

19

10' E of EL = 00 = inlet	9.7	107.6	Some water
+30	8.4	108.9	
+60	10.7	106.6	
+65.7 = opposite W.L elev Wood	13.7	103.6	
+70	16.7	100.6	Bottom Ditch

		138.4✓		
S		11.6	126.8	✓ ✓
+10		12.2	126.2	✓
	0+75			
-10		13.9	124.5	✓
S		13.1	125.3	✓ ✓
cb		12.1	126.3	✓
1/J		11.2	127.2	✓
c		10.2	128.2	✓ ✓
1/4		9.0	129.4	✓
cb		8.5	129.9	✓
∧/		7.5	130.9	✓ ✓
	1+00			
∧/		7.2	131.2	✓ ✓
+4		8.5	129.9	✓
cb		9.5	128.9	✓
+9		10.1	128.3	✓
+10		8.7	129.7	✓
1/J		9.2	129.2	✓
c		10.4	128.0	✓ ✓
1/4		10.8	127.6	✓
cb		12.8	125.6	✓
S		14.9	123.5	✓ ✓
+10		15.1	123.3	✓
	1+15			
-10		16.1	122.3	✓
S		15.6	122.8	✓ ✓

Planted 4@1½ #4

		138.4✓		
cb		14.0	124.4	✓
+7		11.6	126.8	✓
1/J		11.0	127.4	✓
c		11.0	127.4	✓ ✓
1/J		10.4	128.0	✓
4/		11.1	127.3	✓
cb		10.0	128.4	✓
+8		9.6	128.8	✓
∧/		3.4	135.0	✓ ✓
	1+35			
∧/		0.5	137.9	✓
+4		2.5	135.9	✓
+7		7.1	131.3	✓
+10		8.4	130.0	✓
+11		11.0	127.4	✓
cb		11.5	126.9	✓
1/4		11.6	126.8	✓
+8		12.6	125.8	✓
+9		11.2	127.2	✓
c		11.1	127.3	✓ ✓
1/J		11.1	127.3	✓
cb		11.4	127.0	✓
S		17.4	121.0	✓ ✓
+10		17.8	120.6	✓
	1+55			
-10		19.1	119.3	✓

Planted 4@1½ #4

		138.4			
S			17.2	121.2	
cb			11.2	127.2	
1/4			12.2	126.2	
+8			12.3	126.1	
+9			13.5	124.9	
C			13.6	124.8	
1/4			13.5	124.9	
+9			12.5	125.6	
+10			11.5	126.9	
cb			9.7	128.7	
+8			3.0	135.4	
T.P.	70.80	149.21	0.0	138.41	
+9			10.4	138.8	
N			8.2	141.0	
	1+75				
N			4.3	144.9	
cb			9.1	140.1	
+1			16.0	133.2	
1/4			22.7	126.5	
+6			23.2	126.0	
C			26.3	122.9	
1/4			26.5	122.7	
+3			26.2	123.0	
+5			23.4	125.8	
cb			23.2	126.0	
+7			23.2	126.0	

Planted 4 poles

		149.21			Walnut 21
S			27.1	122.14	
+10			29.2	120.0	
	2+00 = EL. STATE				75' wide
S			24.7	124.5	12' cb
+4			29.7	119.5	1/4S
cb			29.4	119.8	
1/4			28.1	121.1	
C			21.8	127.4	
+10			15.8	130.4	
1/4			8.0	141.2	
+1			6.5	142.7	
cb			2.5	146.7	
T.P.	5.0	153.69	0.5-C	145.65	
N			3.9	149.8	
T.P.			8.1	145.58	Walnut & Mon. State

Planted 4 poles

Cross Section of STATE ST
Walnut to Glenwood Drive

25' wide
12 cbs
IN 7.5" 1/45
ubas STATE

℄ Mon	0.0	159.33		159.33	
	℄ walnut = 80' wide 14' cbs 13'				
E			9.5	149.8	
cb			7.9	151.4	
1/4			6.4	152.9	
C			4.5	154.8	
1/4			3.0	156.3	
cb			1.6	157.7	
W			0.8	158.5	
	W cb				
W			2.6	156.7	
cb			3.9	155.4	
1/4			5.1	154.2	
C			7.4	151.9	
1/4			8.9	150.4	
cb			10.7	148.6	
E			12.6	146.7	
	N 1/4				
E			17.4	141.9	
cb			13.8	145.5	
1/4			11.8	147.5	
C			9.9	149.4	
1/4			7.6	151.7	
cb			6.1	153.2	
W			5.0	154.3	

Moore 159.33 = Profile Platted M.N.P. DEC 28-1926

N 1/4 ℄ 3		
W	15.5	153.8
cb	6.9	152.4
1/4	8.6	150.7
C	11.0	148.3
1/4	13.1	146.2
cb	15.1	144.2
℄	17.4	141.9
E	28.7	130.6
℄ walnut		
E	32.4	127.1
℄ 10	28.7	130.6
cb	26.0	133.3
℄	17.6	141.7
1/4	16.3	143.0 check
℄ on Mon	13.7	145.59 1.55
1/4	11.1	148.2
cb	9.4	149.9
W	7.9	151.4
S 1/4		
W	12.6	146.7
T.P. 0.58	12.3	147.0 147.60
cb	2.1	145.5
1/4	3.7	143.9
C	5.9	141.7
℄	8.7	138.9

+10		14.2	133.4
1/4		14.9	132.7
cb		19.1	128.5
E		26.1	121.5
S cb			
E		28.0	119.6
cb		28.1	119.5
+5		33.7	123.9
1/4		21.6	126.0
C		16.2	131.4
+1		16.0	131.6
+2		10.7	136.9
1/4		7.4	140.2
cb		6.2	141.4
+7		4.5	143.1
2/		1.4	146.2
S cb +10			
2/		7.0	140.6
+10		8.2	139.4
cb		10.5	137.1
1/4		11.4	136.2
+1		15.1	132.5
C		19.7	127.9
1/4		24.5	123.1
+3		25.4	122.2
+4		28.9	118.7

cb		29.5	117.1
E		28.0	119.6
SLIGHT CUT = 0+00			
E		22.7	124.9
+5		28.4	119.2
cb		30.0	117.6
1/4		32.0	115.6
+3		26.0	121.6
C		22.1	125.5
1/4		17.2	130.4
+3		16.5	131.1
+6		11.3	136.3
cb		10.7	136.9
2/		10.6	137.0
0+11.			
2/		11.1	136.5
cb		12.7	134.9
T.P. 0.15	135.8	12.93	134.67
+2		2.10	132.2
1/4		9.6	125.2
C		14.3	120.5
+4		15.4	119.4
+5		19.1	115.7
1/4		19.3	115.5
cb		18.0	116.8
+2		11.5	123.3

		134.8		
E		13.1	121.7	✓
+5		14.2	120.6	✓
	0+14			
-5		15.1	119.7	✓
E		14.3	120.5	✓
+9		11.3	123.5	✓
cb		12.0	122.8	✓
+2		18.3	116.5	✓
1/4		19.6	115.2	✓
+10		19.3	115.5	✓
C		15. ✓	119.6	✓
1/2		10.5	124.3	✓
cb		4.3	130.5	✓
+1		3.3	131.5	✓
w/		3.3	131.5	✓
	0+35			
1-17 E edge residence		4.5	130.3	✓
w/ " " terrace in yard		4.6	130.2	✓
+6		10.9	123.9	✓
cb		12.6	122.2	✓
1/4		15.0	116.8	✓
+2		20.5	114.3	✓
C		21.2	113.5	✓
+11		20.8	114.0	✓
1/4		16.1	118.7	✓
cb		13.7	121.1	✓

		134.8		
E		18.0	116.8	✓
+5		18.4	116.2	✓
T.P.	3.70	145.57	12.9	131.87 ✓
	0+50			
-5		16.1	114.5	✓
E		10.4	115.2	✓
cb		6.4	119.2	✓
1/4		8.8	116.8	✓
+5		10.1	115.5	✓
+6		13.8	111.8	✓
C		13.9	111.7	✓
1/4		13.6	112.0	✓
+6		12.8	112.8	✓
+8		10.1	115.5	✓
cb		7.1	118.5	✓
+8		2.1	123.5	✓
w/		2.1	123.5	✓
	0+77			
w/ w/ east edge conc. stairs		11.6	114.0	at landing
T.P.	4.55	117.28	12.5	112.73 ✓
+5		4.1	113.2	✓
cb		7.5	109.5	✓
1/4		8.8	108.5	✓
C		8.7	108.6	✓
+6		5.1	112.2	✓
1/4		2.9	114.4	✓

11.7.28

1/4 +6		12.0	115.3
c6		11.4	117.9
+6		6.6	110.7
E		6.6	110.7
+5		6.6	110.7
	0+90		
-5		8.3	109.0
E		7.7	109.6
c6		7.1	110.2
+6		4.4	113.1
1/4		4.8	112.5
+8		6.9	110.4
+9		9.9	107.4
C		9.8	107.5
1/4		9.9	107.4
c6		9.6	107.7
+8 & corn Hpron		9.1	108.2
W		9.0	108.3
+3 Garage corn floor		8.9	108.4
	1+31		
W -1' & garage dirt floor		12.4	105.1
	1+31		
W on corn walk parallel with	north end street	13.7	103.6
c6		13.7	103.6
1/4		13.6	103.7
C		12.8	104.5

11.7.28 STATE 75

+5	14.4	103.1	117.28
1/4	10.4	106.9	-12.36
c6	9.6	107.7	104.92
E	8.8	108.5	+0.91
	1+44		105.83
E	7.7	109.6	-12.69
+5	9.3	108.0	93.14
c6	10.2	107.1	091
1/4	10.4	106.9	94.05
+5	11.0	106.3	12.10
+6	12.5	104.8	51.95
C	14.3	103.0	3.00
+3	13.3	104.0	54.95
1/4	14.4	102.9	2.40
c6	14.8	102.5	76.75
+11 edge corn walk	14.4	102.9	
16.5.57 = N/L Glenwood Drive			763
W & edge corn walk	16.5	100.8	1' in street
c6	16.3	101.0	
1/4	14.7	102.6	
+16	16.7	100.6	
C	13.7	103.6	
+7 Junction c of s strobings of	13.3	104.0	draftsman/ water. take a look
+8	9.9	107.4	Seebago 18 for
1/4	8.9	108.4	location
c6	5.3	112.0	19 for levels
E	2.1	115.2	

MAP Glenwood 1.4.19

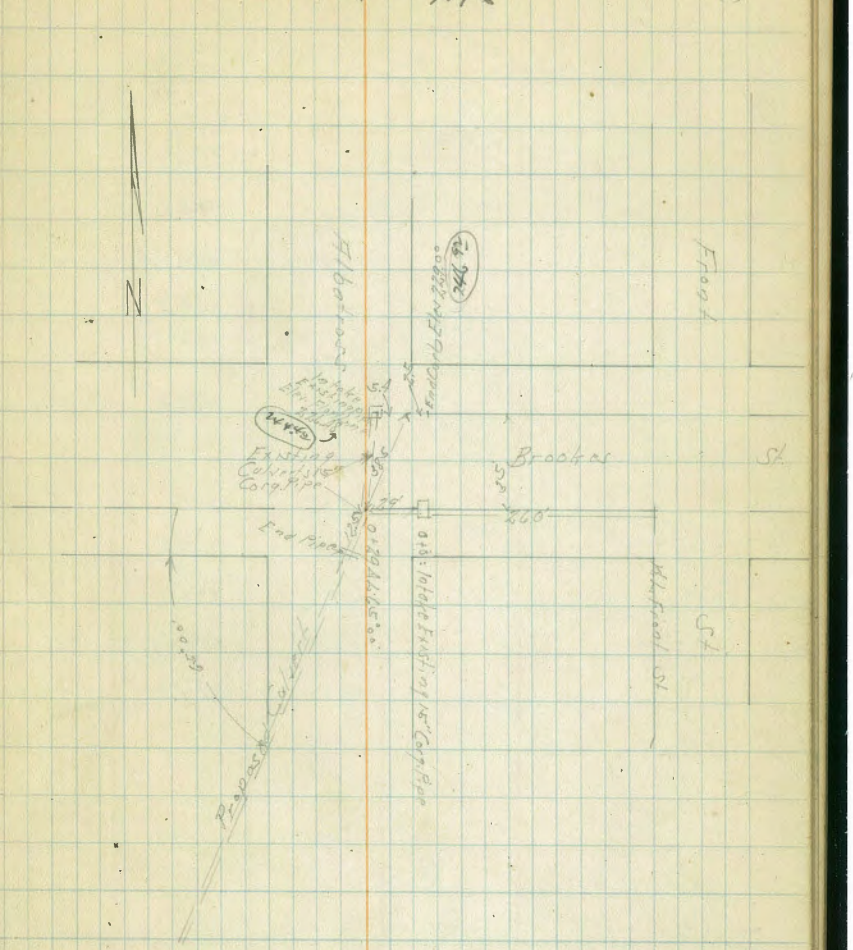
Levels For Proposed Culvert
Albatross + Brookes

BM	9.34	278.16 260.24 ✓		268.82 250.90	N.W. S.P Walnut 1st St
TP	0.36	265.72 247.90 ✓	12.70	265.46 247.54 ✓	
TP	0.29	255.63 237.71 ✓	10.48	255.34 237.42 ✓	
0+0 =		Flow Line	9.44	246.19	
+15	End Curb on Top		7.81	247.82	
+29	Δ∠ 65°00'		11.6	244.0	
TP	0.36	242.43 225.51 ✓	12.56	242.07 225.15 ✓	
+41.5	= End of Existing Pipe Flow Line		5.20	237.23	
+47			11.2	231.2	
TP	1.21	231.28 214.36 ✓	12.36	230.07 213.15 ✓	
+53			6.5	224.8	
+73			11.0	220.3	
+74			18.6	212.7	
TP	0.30	219.30 202.38 ✓	12.28	219.00 202.08 ✓	
+93			7.9	211.4	
TP	0.21	207.42 190.50 ✓	12.09	207.21 190.29 ✓	
1+08			1.8	205.6	
+28			12.1	195.3	
+43			18.9	188.5	
TP	0.35	195.97 179.05 ✓	11.80	195.62 178.70 ✓	
+65	= Bottom Gulch		11.80	184.17	

Plotted 1/4/7 HPL

Note This Bench should have been 268.82
follow revised TPs. HPL

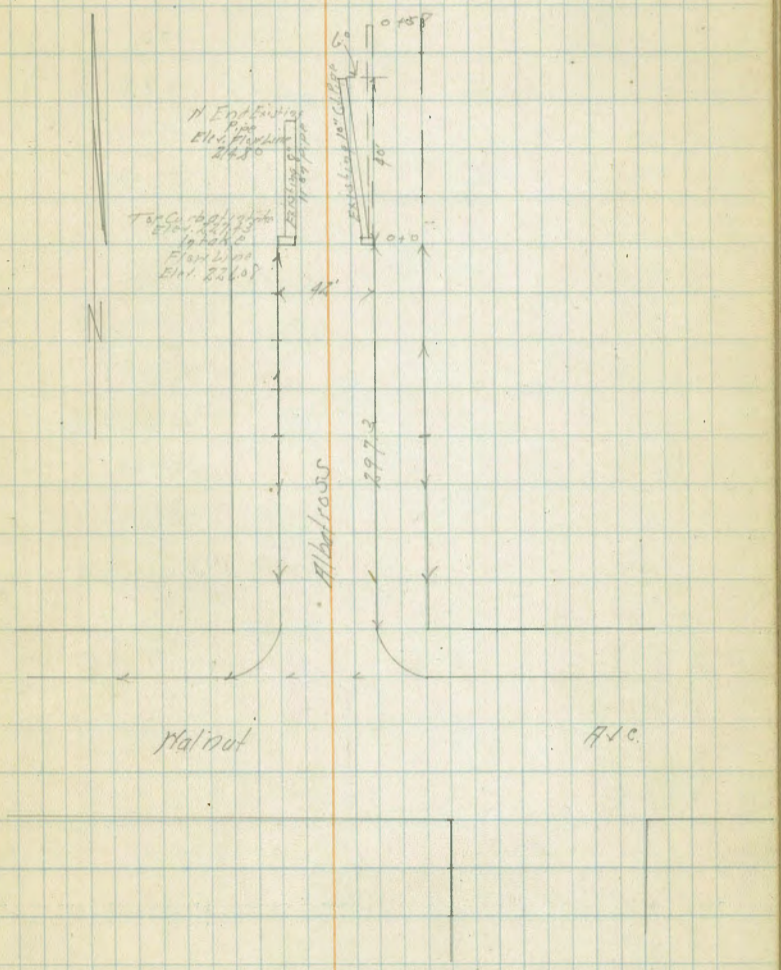
12-30-26
3-5-27
31-32
Hoffman
1/6



Levels For Proposed Culvert
E Curb Line of Albatross N of Walnut

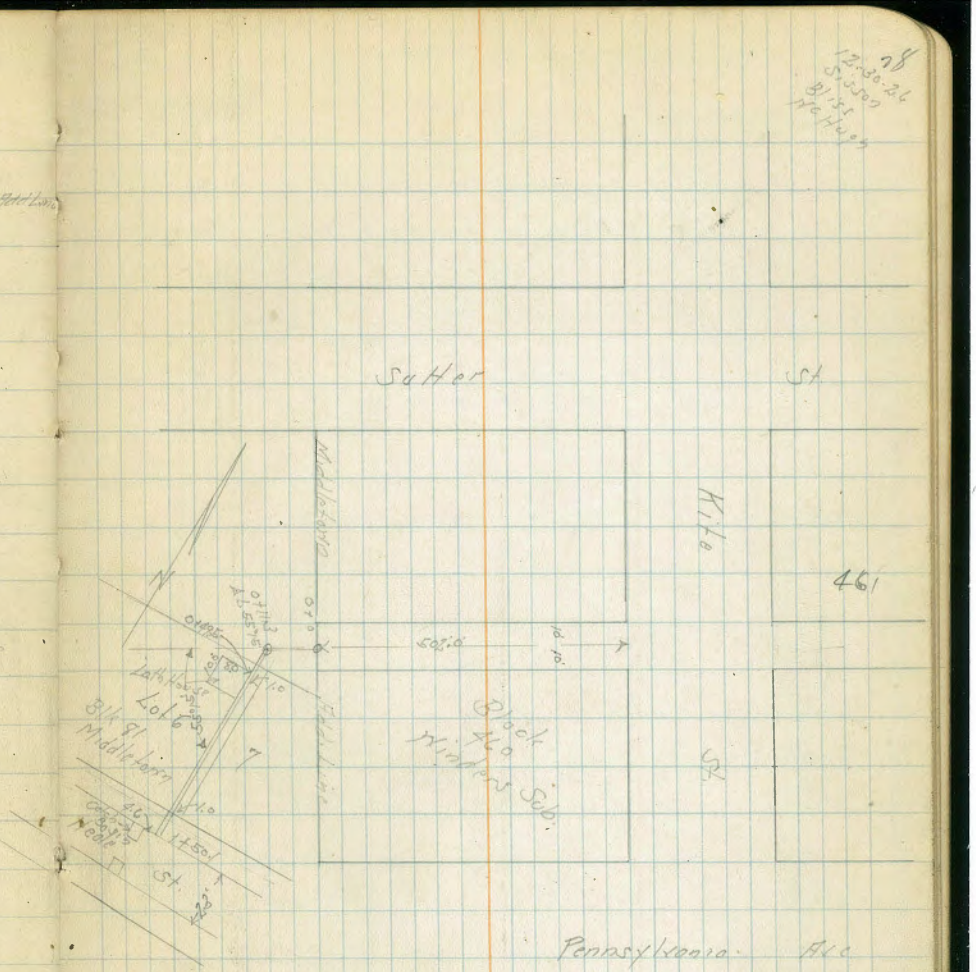
		269.68		268.87	N.W.B.P.
B.M.	0.86	251.76		250.90	Walnut & Albatross
		257.70		257.37	
T.P.	0.33	238.78	18.81	238.45	
		247.87		246.97	N.E.B.P.
B.M. set	4.85	233.90	10.73	229.05	Walnut & Albatross
0+0	Top Curb		7.71	244.05	
	Flow Line		9.04	242.78	
+10			7.3	244.5	
		239.50		239.49	
T.P.	0.01	221.58	12.33	227.17	
+17			2.6	236.9	
		227.91		227.13	
T.P.	0.78	208.88	12.37	208.00	
+29			2.0	225.9	
+38			5.3	222.6	
+40	= C.L. of N End of Pipe		8.8	219.1	
	Flow Line		7.94	219.97	
+58	= Bottom of Gutter		14.9	213.0	

Plotted 1/3/11 RJK



Levels for Proposed Culvert Across Block 81 Middletown Add

B.M.	7.55	27693		269.38	G.P. N.E. Sather & Middletown Add Line
0+0			5.7	271.2	
+11.3 = Δ L55°15'			6.4	270.5	
+33.8 = Fence			9.0	267.9	
+50			10.5	266.4	
TP	2.42	267.29	12.06	264.87	
1+0			8.6	263.7	
+40			4.0	263.3	
+44.3 = N Edge Walk			6.17	261.12	
+50.1 = Top Cb			6.30	261.0	
Gutter Top Paving			6.95	260.34	
Grading Catch Basin 4.6 W of Top of Line			7.33	259.96	
Flow Line			9.10	258.19	



X See Alley Jackdaw to Kite
20'. wide. Bet Penn Ave + Sutter

2-18-24
mill

B.M.	1.30	263.30 ✓		262.00	N.W. Sutter + Jackdaw
	00 = W. Line Jackdaw St				
N			3.90	259.4	cmt el
N			4.29	259.0	Paving ✓
℄			4.56	258.7	"
S			4.12	259.2	"
S			4.01	259.3	cmt el
85' W = E. end garage on S cmt floor			3.5 Bank		
S - 3.5			1.95	261.4	✓ floor
S			2.4	260.9	
E			2.5	260.8	
N			1.8	261.5	
40' W = W. end above garage				~~26~~	
N			1.0	262.3	✓
E			1.6	261.7	
S			2.1	261.2	
+3.5			2.00	261.3	cmt floor
64' W = E. end cmt drive to garage Facing West.					
S			1.00	262.3	cmt drive
℄			0.7	262.6	cmt drive
N			0.2	263.1	
T.P.	8.64	271.22 ✓	0.72	262.58 ✓	
86' W = W. end above cmt drive to garage					
N			6.5	264.7	
E			6.7	264.5 ✓	
S			7.1	264.1	cmt drive

271.22

91.' W

79

S			5.5	265.7	
E			5.8	265.4	
N			5.6	265.6	
98' W = E. Line Kite St					
N.			4.53	266.69	cmt el
N.			5.0	266.2	dirt
E.			5.1	266.1	"
S.			5.2	266.0	"
S.			4.61	266.61	cmt el
T.P.	2.02	268.04 ✓	5.20	266.02 ✓	

80' wide
14' ells
13 1/4s

X. Sec. Pennsylvania Ave
E. Line Kite to W.L Jackdaw

2-18-27
Miller

2.68.04 Page 29

00 = E. line Kite

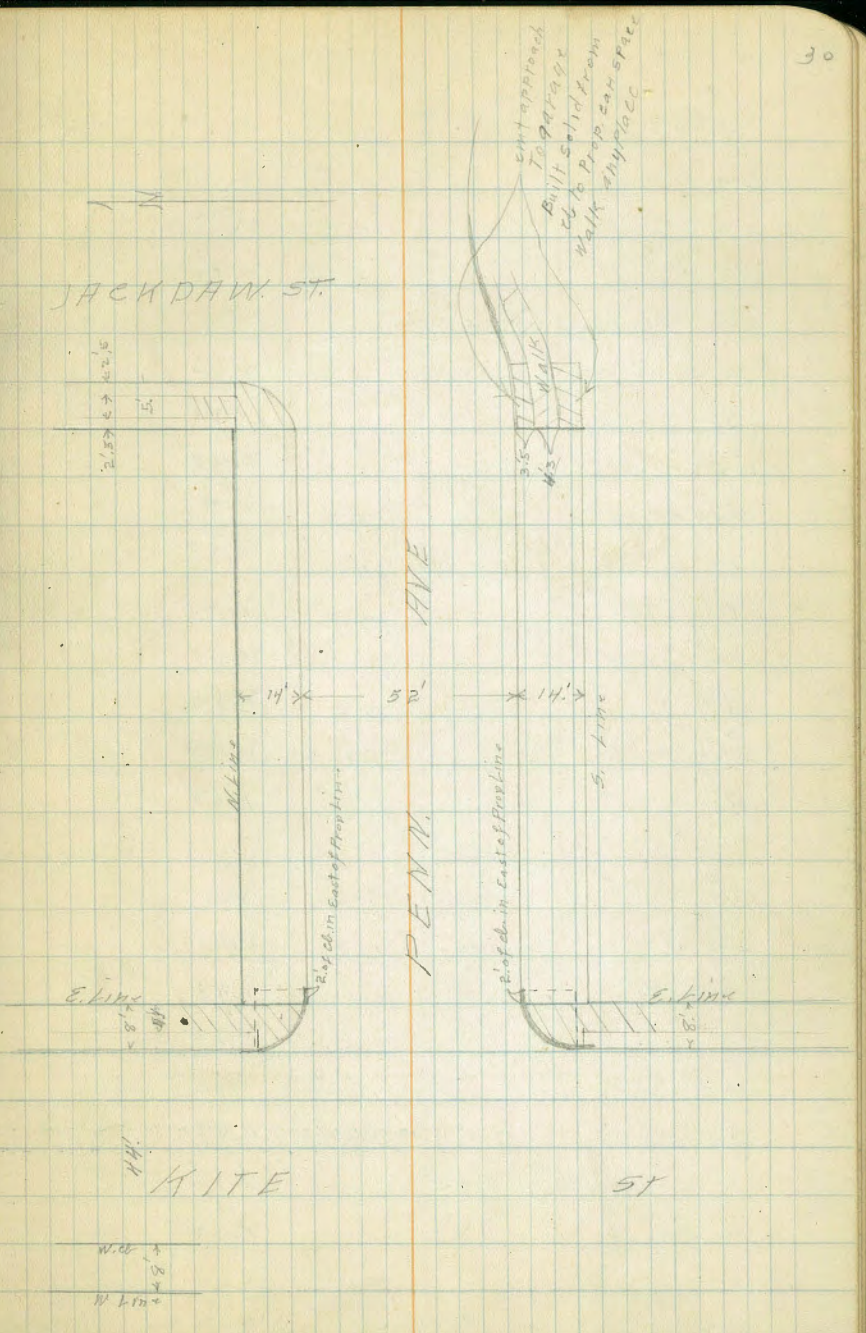
N		1.7	26.3	
el		2.22	25.82	cmt el
1/4		2.2	25.8	
e		2.4	25.6	
1/4		2.5	25.5	
el		2.70	25.34	cmt el
S		2.4	25.6	

2'E. = E. End 10'R. Returns curbs completed walks on prop line

S		0.0	28.0	
+7		0.1	27.9	
el		1.6	26.4	(dirt) for yardage
el		2.70	25.34	cmt el No yardage
1/4		1.8	26.2	
e		1.6	26.4	
1/4		1.4	26.6	
el		2.22	25.82	cmt el No. yardage
el		1.5	26.3	use for (dirt) yardage
N		1.5	26.3	

20' E

N		1.8	26.2	
el		1.8	26.2	
1/4		2.1	25.9	
e		2.4	25.7	
1/4		2.6	25.4	



	268.04		
	20 E. (con)		
el		2.5	265.5
+4		2.3	265.7
+8		0.6	267.4
S		0.4	267.6
	35' E		
S		0.5	267.5
+2		0.6	267.4
+8		3.2	264.8
el		3.3	264.7
1/4		4.2	263.8
e		4.0	264.0
1/4		2.9	265.1
el		3.0	265.0
+3		1.7	266.3
N		1.7	266.3
	50' E.		
N		1.8	266.2
+9		1.9	266.1
el		4.0	263.9
+4		4.8	263.2
1/4		4.8	263.2
e		5.3	262.7
1/4		5.5	262.5
el		4.8	263.2
+4		5.0	263.0
+12		2.4	265.6
S		0.9	267.1

	268.04		
	70' E		
S		2.2	265.8
+2		4.8	263.2
+7		6.7	261.3
+8		7.6	260.4
el		7.5	260.5
1/4		7.5	260.5
e		7.2	260.8
1/4		6.8	261.2
+9		6.8	261.2
el		5.7	262.3
+7		2.1	265.9
N		2.4	265.6
	87' E		
N		3.3	264.7
+8		3.7	264.3
el		8.3	259.7
+4		9.0	259.0
1/4		8.4	259.6
e		8.6	259.4
1/4		8.7	259.3
el		9.4	258.6
+7		8.2	259.8
+13		6.2	261.8
S		3.3	264.7

		268.04 96' E			
S			7.0	261.0	
cl			10.2	258.8	
1/4			9.9	258.1	
C			9.5	258.5	
1/4			9.7	258.3	
cl			9.7	258.3	
+3			8.3	259.7	
+7			4.5	263.5	
N			4.7	263.3	
	98' E = W Line Jackdaw				
N			9.4	258.6	
cl			10.02	258.02	cm+cl
1/4			10.0	258.0	
C			9.8	258.2	
1/4			10.1	257.9	
cl			10.50	257.54	cm+cl
S			10.3	257.7	
T.P.	4.23	263.27 ✓	8.90	259.04 ✓	
T.P.			1.27	262.00	BM.

Sewer Levels 10' N. of ℄ Walnut Produced from 2-18-27
East from ℄ Lark to ℄ Union

BM. Pag 17	12.37	147.66		135.29	NW cor Union + Walnut
00 = ℄ Union	32.2 N of ℄ Walnut to W		8.8	137.9	
+20			7.0	138.7	
+50			0.7	146.9	
T.P.	13.10	160.44	0.32	147.34	
+70			7.6	152.8	
+75			8.7	151.7	
+80 = Top Bank			2.9	157.5	
6' S. of above			8.8	151.6	
+90 Top Bank			2.0	158.4	
8' S. of above			9.4	151.6	
1+00 Top Bank			+0.2	160.6	
4' S. of above			8.4	152.0	
T.P.	12.70	173.11	0.03	160.41	
1+15			8.1	165.0	
10' S. of above = Top Bank			10.2	162.9	
1+35			4.3	168.8	
T.P.	12.49	185.31	0.27	172.82	
1+55			12.5	172.8	
1+75			10.5	174.8	
1+90			8.6	176.7	
2+00			8.8	176.5	
2+15			8.2	177.1	
2+27			1.1	184.2	
T.P.	12.46	197.69	0.08	185.23	

197.69

T.P.	12.72	210.00	0.41	197.28
2+57			6.3	203.7
2+72			1.6	208.4
T.P.	12.52	222.49	0.03	209.97
2+78			10.4	212.1
3+00			6.3	216.2
3+14 = ℄ Lark			5.7	216.8
T.P.	12.60	233.89	1.40	221.09
chk. on BM.			1.18	232.71 NE. Blk Hub Lark + Walnut

See Page 73. for Profile 2' N. of ℄ Walnut

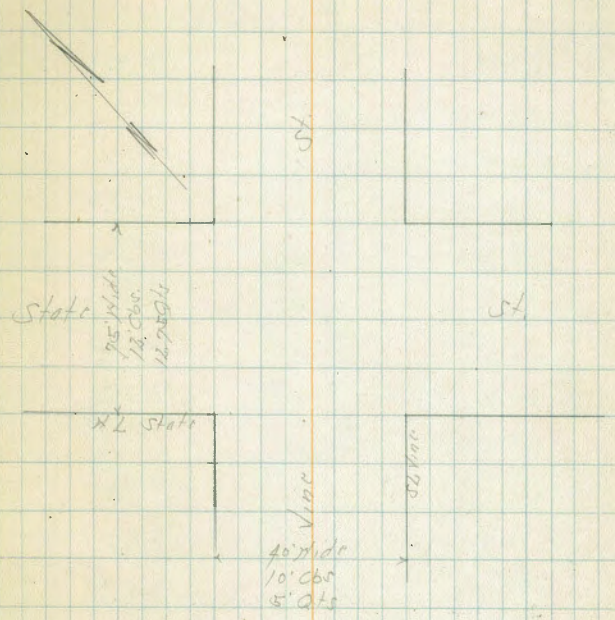
Cross Section State St. & Vine
Intersection

Vine 40' Wide 10' Cbs 5' Qts | State St 75' Wide 12' Cbs 12.75 Qts

BM	139	160.60		139.71
TP	0.36	149.05	11.91	148.69
		WL State		
S			60	143.0
Cb	Top Cb End		66	142.41
Gutter	on Paving		736	141.69
¼	" "		729	141.76
½	" "		731	141.74
¼	" "		754	141.51
Gutter	" "		781	141.24
Cb	" "		730	141.85
+3			78	141.1
N			188	135.2
+10			205	128.5
+20			268	122.2
+30			340	118.0
+37			341	114.9
+50			378	111.2
		W Cb		
-45			318	117.2
-35			313	117.7
-10			227	126.3
N			147	134.3
Cb			71	141.9
+3			58	143.2

Started Chain 4/17/11

8 Mar. Elev. State



149.05

¼	5.7	1433
E	6.1	1429
¼	6.2	1428
Cb	5.9	1431
S	5.9	1440
	W ¼	
S	3.9	1457
Cb	4.1	1446
¼	4.8	1442
E	4.8	1442
+4	3.9	1457
¼	4.7	1443
Cb	8.5	1405
N	16.0	1370
+8	20.7	1283
+20	25.3	1237
+27	28.2	1203
+42	29.4	1196
	E State St	
-40	21.7	1243
-25	24.7	1223
-15	21.9	1271
N	15.0	1340
Cb	8.1	1409
¼	2.4	1456
E	0.0	1469

Revised Chart 4/1/37

149.05

¼	3.3	1457
Cb	3.3	1457
S	1.9	1471
	E ¼	
S	0.4	1486
+4	1.8	1472
Cb	2.5	1465
¼	2.0	1470
E	1.7	1473
+3	1.8	1472
¼	2.7	1463
Cb	7.0	1420
N	14.0	1350
+10	18.9	1301
+16	22.1	1266
+21	23.3	1257
+30	21.9	1271
	E Cb	
-30	18.2	1308
-20	20.0	1290
-14	19.6	1294
N	12.2	1368
Cb	5.3	1438
¼	1.2	1478
E	0.7	1483
E	0.9	1481

		149.05		
¼			1.2	147.8
Cb			1.4	147.6
+2			1.9	147.1
+7			1.2	147.8
S			0.0	149.0
		FL State St		
S			0.0	149.0
+5			0.8	148.2
Cb			0.4	148.6
¼			0.0	149.0
TP	1.50	150.15	0.40	148.65
S			0.8	149.3
+4			0.5	149.6
¼			1.0	149.1
Cb			4.9	145.2
H			11.0	139.1
+10			16.0	134.1
+14			17.5	132.6
+30			16.6	133.5
End of Curb 5' Left of FL of State			1.02	149.13

Revised Elevations 11-21-17

Cross Section Intersection Glenwood & State St.

		Glenwood 40' Wide 5 Cbs 75 Pk	State 75' Wide 13 Cbs 123.75 Pk	
				NE 8 P
BM	10.28	86.72 ✓	76.34	Glenwood & Locke
TP	12.47	98.70 ✓	0.50 / 86.23 ✓	
TP	9.33	107.83 ✓	0.20 / 98.50 ✓	
		W L State		
N			8.0 / 99.8	
Cb			8.3 / 99.5	
¼			8.2 / 99.6	
S			8.3 / 99.5	
¼			8.0 / 99.8	
+3			8.3 / 99.5	
+6			14.0 / 93.8	
Cb			6.8 / 101.0	
S			3.9 / 104.9	
		W Cb		
S			0.0 / 107.8	
Cb			6.2 / 101.6	
+5			11.4 / 96.4	
½			10.3 / 97.5	
S			7.3 / 94.3	
¼			2.1 / 100.5	
Cb			7.0 / 100.6	
N			6.8 / 100.7	
TP	12.50	120.11 ✓	0.22 / 107.11 ✓	
		W ½		
N			1.78 / 102.3	

Started Chase 4/4/37

120.11

Cb	17.9	102.2
+5	18.3	101.8
¼	20.2	99.9
½	23.1	97.0
+3	21.1	99.0
S	18.5	101.6
+3	18.5	101.6
+6	11.3	108.8
¼	9.9	110.2
Cb	7.5	112.6
S	5.1	114.7
	8' Est W ½	
S	2.9	117.2
Cb	1.7	118.4
¼	7.8	112.3
S	10.5	109.6
+3	11.5	108.6
¼	18.2	101.9
+1	20.5	99.6
Cb	21.0	99.1
N	20.4	99.7
	S State St	~~103.0~~
N	17.1	103.0
Cb	16.0	104.1
+5	14.9	105.2
¼	10.9	109.2

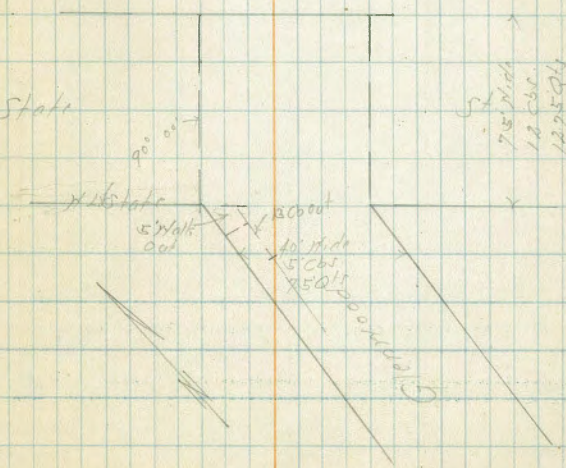
120.11

℄			9.5	110.6
¼			6.0	114.1
cb			2.9	1181
S			1.4	118.7
TP	12.15	131.39 ✓	0.87	119.24 ✓
		5' E of ℄ of State		~~4.9~~
S			11.5	1199
cb			18.3	1181
¼			15.8	1156
℄			18.7	1127
℄			21.2	100.1
cb			23.1	108.3
N			24.2	107.2
		E ¼		10
N			22.7	108.7
cb			21.0	110.4
¼			18.5	112.9
℄			15.9	115.5
¼			13.3	118.2
cb			10.9	120.5
S.			9.0	122.4
		E cb		
S			6.2	125.2
cb			7.9	123.5
¼			10.2	121.2
℄			12.6	118.8

Pulled Stake 4 ½/21 Stone

131.39

¼		14.9	116.5
cb		16.5	114.9
N		19.0	112.4
E ℄ State St.			~~111.0~~
N		14.4	115.0
cb		12.9	117.7
¼		11.1	1203
℄		9.3	122.1
¼		6.7	124.7
cb		4.5	126.9
S		3.0	128.4



Cross Section Alley Block 12 City Heights Tract No 2
From Thorn to Myrtle
Between Chamoune & 45th St. 20' W. do

B.M	580	338.78		332.98	N.W. St. Thorn & Chamoune						
		NL Thorn									
E	Top Cb & Ground		8.3	330.55							
&			8.7	30.1							
W	Top Cb & Ground		8.0	29.8							
		2' N of NL Thorn		32.6							
W			6.2	32.6							
+2			6.1	32.7							
+3			7.8	31.0							
&			8.0	30.8							
+5			7.7	31.1							
+6			6.0	32.8							
E			5.8	33.0							
		25' N									
E			5.4	33.4							
&			6.1	32.7							
W			5.8	33.0							
		50' N									
W			5.4	33.4							
&			5.4	33.4							
E			5.0	33.8							
		100' N									
E			4.9	33.9							
&			5.0	33.8							
W			5.0	33.8							

Plotted 9-23-27 by DC Wilcox

338.78

150' N

W	4.9	33 4.1		
&	4.4	34.4		
E	4.5	34.3		
	200' N			
E	3.6	35.2	Shed 0.5 in Alley out	
&	3.7	35.1		
W	3.5	35.3		
	250' N			
W	3.4	35.4	2.5 E & Garage 0.5 W of NL	
&	3.4	35.4	Conc Floor 4.75 = 336.0	
E	3.4	35.4	Shed on Alley out	
	300' N			
E	2.8	36.0	Shed 0.5 in Alley out	
&	3.1	35.7		
W	2.9	35.9		
TP	6.95	342.9	3.02	335.76
	350' N			
W	6.8	3 35.9	3.18' NL Garage 0.4 E Floor 0.4 W of NL 6.80 = 335.9	
&	6.7	36.0		
E	6.3	36.4	3.6' W & Garage 0.5' Floor	
	400' N		3.5' W of NL 6.52 = 336.15	
E	6.1	36.6	3.2' W & Garage Conc Floor Apron on NL 6.12 = 336.5	
&	6.2	36.5		
W	6.4	36.3		
	450' N			

	342.71			
W		5.9	336.8	457' N & Garage Conc. Floor 2.0' of PL 5.07 = 337.3
℄		6.0	36.7	
E		6.1	36.6	
	493' N			
-1 ℄ Garage Conc Floor		5.84	37.5	
E		5.3	37.4	
℄		5.6	37.1	
W		5.6	37.1	
+3.6 ℄ Garage Dirt Floor		5.5	37.2	
	530' N			
W		4.8	37.9	
℄		5.3	37.4	
E		5.3	37.4	
	542' N			
E		5.0	37.7	
℄		5.0	37.7	
+5		4.9	37.8	
W = Conc Apron		4.15	38.6	
	570' N			
W		4.2	38.5	
℄		4.6	38.1	
E		4.8	37.9	
	590' N			
E		4.7	38.0	
℄		4.8	37.9	

	342.71			
W		4.3	338.4	
680' N = S.L. Myrtle				
W Top Cb & Ground		5.07	37.6	
℄		5.5	37.2	
E Top Cb & Ground		5.59	37.1	
BM		6.81	335.90	N.W. & P Myrtle & Curbline 335.89

CoHanwood St.
Cross Section Woden to Yoma

80' wide
14' Cbs
13.9 Qts

BM	4.95	17.07		12.12	
TP	7.67	24.37	0.37	16.70	
BM			3.31	22.16	
		EL Woden			
S			46	20.0	
Cb Top End Return			4.30	20.1	
Gutter			4.9	19.5	
¼			4.1	20.0	
½			3.8	20.6	
¼			3.7	20.7	
Gutter			3.5	20.9	
Cb Top End Return			2.89	21.5	
N			2.3	22.2	
		50' E of EL Woden			
N			3.4	21.0	
Cb			3.6	20.8	
+3			4.0	20.4	
+5			5.0	19.4	
¼			4.8	19.6	
½			4.8	19.6	
¼			4.9	19.5	
+7			5.2	19.2	
Cb			4.9	19.5	
S			5.3	19.1	
		100' E			

N W Spk
Main St Woden

SE Top Hyd
CoHanwood St Woden

24.4

24.37

S		54	19.0
Cb		55	18.9
+6		54	19.0
+7		58	18.6
¼		56	18.8
½		55	18.9
¼		54	19.0
+5		59	18.5
Cb		40	20.4
N		34	21.0
	150' E		
N		43	20.1
Cb		47	19.7
+5		58	18.6
¼		61	18.3
½		65	17.9
¾		66	17.8
Cb		71	17.3
S		80	16.4
	200' E		
S		81	16.3
Cb		76	16.8
¼		67	17.7
½		65	17.9
¼		64	17.0
+7		68	17.6

9-19-37
S. Ser 47
81.55
Santiam

Cottonwood St. 24.4

24.37

Cb		48	18.6	
N		44	20.0	
	250'E			
N		41	20.3	
Cb		43	20.1	
+6		6.7	17.7	
1/4		5.9	18.5	
1/2		6.0	18.4	
1/4		6.1	18.3	
Cb		6.9	17.5	
S		7.3	17.1	
	300'E	= N of 7 Small Trees 11.5' S of N.		
S		7.3	17.1	
Cb		7.0	17.4	322'E of NL Top of 1st Step 417 of 8
1/4		6.2	18.2	
1/2		6.0	18.4	
1/4		5.9	18.5	
+7		5.4	19.0	
Cb		4.9	19.5	
N		4.0	20.4	
	350'E			
N		5.0	19.4	
Cb		6.1	18.3	
+6		6.7	17.7	
1/4		7.2	17.2	
1/2		7.2	17.2	

24.4 42

24.37

1/4	7.4	17.0	
Cb	7.9	16.5	345'E of NL Top of 1st Step of 8
S	8.6	15.8	
	400'E		
S	10.9	13.5	
Cb	9.5	14.9	
1/4	8.6	15.8	
1/2	8.5	15.9	
1/4	8.7	15.7	
+9	8.0	16.4	
Cb	7.0	17.4	
N	6.3	18.1	
	435'E		
N	8.4	16.0	
Cb	8.3	16.1	
+3	9.1	15.3	
1/4	9.0	15.4	
1/2	9.3	15.1	
1/4	9.4	15.0	
Cb	10.0	14.4	
S	11.6	12.8	
TP	240 16.64	10.13 14.34	16.6
	450'E	= E of 7 Trees 13' S of N.	
S	4.0	12.6	
Cb	3.2	13.4	

Co Hanwood St.

16.6

16.64

+3		21	13.5
+6		24	14.2
¼		25	14.1
⅛		26	14.0
¼		27	14.2
+9		25	14.1
Cb		19	14.7
N		19	14.7
	S 495'E		
N		20	14.6
Cb		25	14.1
+3		33	13.3
¼		34	13.2
⅛		38	12.8
¼		38	12.8
Cb		41	12.5
S		47	11.5
	500'E		
S		54	11.2
Cb		49	11.7
¼		51	11.5
⅛		53	11.3
¼		50	11.6
+7		54	11.2
Cb		44	12.2
N		52	11.4

16.6

16.64

532'E

N		74	9.2
49		74	9.2
Cb		69	9.7
¼		67	9.9
⅛		69	9.7
¼		70	9.6
Cb		74	9.2
S		82	8.4
	550'E		9.2
S		87	
Cb		83	8.3
¼		75	9.1
⅛		74	9.2
¼		75	9.1
Cb		76	9.0
N = Conc Walk		740	9.2
	600'E = N.L. Yama		Yama 6'x16' 10'Cbs 10'Ftr
N		76	9.0
Cb		79	8.7
¼		80	8.6
⅛		81	8.5
¼		80	8.6
Cl		80	8.6
S		82	8.4
	WCb		

Cathonwood St. 16.6

16.64

S		8.3	8.3
Cb		8.0	8.6
¼		8.1	8.5
⅛		8.0	8.6
¼		7.9	8.7
Cb		7.9	8.7
N		7.8	8.8
	W ¼		
N		7.8	8.8
Cb		7.8	8.8
¼		7.9	8.7
⅛		8.1	8.5
¼		8.2	8.4
Cb		8.0	8.6
S		8.1	8.5
	½ Yama		
S		8.5	8.1
Cb		8.7	7.9
¼		8.5	8.1
⅛		8.2	8.4
¼		8.0	8.6
Cb		7.9	8.7
N		7.8	8.8
	E ¼		
N = Garage Dirt Floor		7.9	8.7
Cb		7.9	8.7

Cathonwood St. Yama Intersection Tolerances Regular

16.6 #4

16.64

¼		8.2	8.4
⅛		8.2	8.4
¼		8.1	8.0
Cb		8.1	8.0
S		8.9	7.7
	E Cb		
S		8.2	8.4
Cb		8.3	8.3
¼		8.4	8.2
⅛		8.4	8.2
¼		8.2	8.4
Cb		8.1	8.5
N		8.0	8.6
	E ¼ Yama		
N		7.9	8.7
¼ N		8.4	8.2
Cb		7.9	8.7
¼		8.3	8.3
⅛		8.5	8.1
¼		8.5	8.1
Cb		8.3	8.4
S		8.1	8.5
BM		4.54	11.10

SE Top Nut Cathonwood St Yama

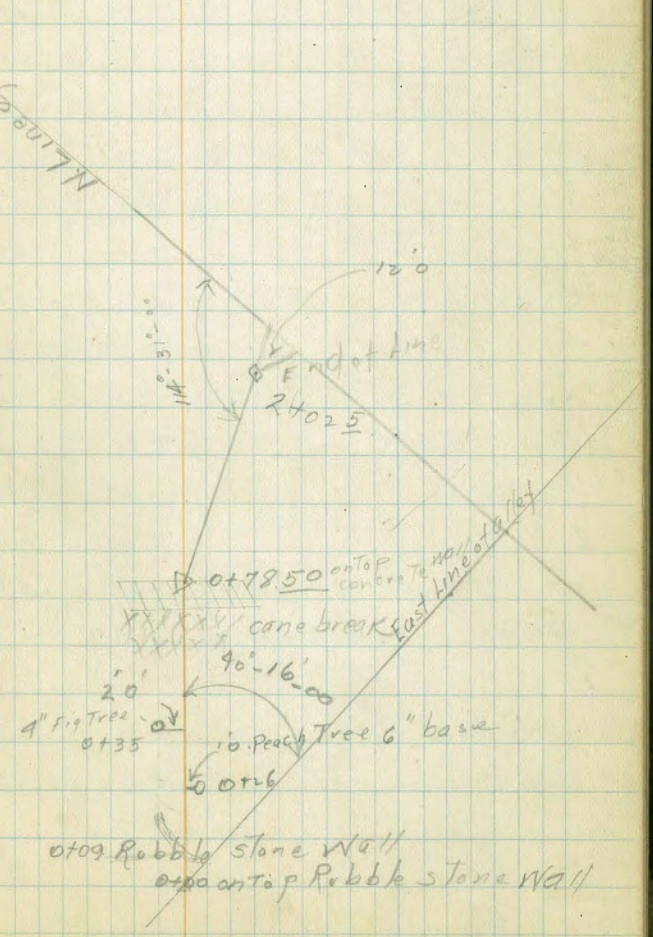
Levels for Culvert Block 31

Fairmount Addition, to City Heights Map 1035

Bliss
10/20/27

	+	T	−	Elev	BM
	0.38	348.83			348.45
T.P.	1.39	337.69	12.53	336.30	
T.P.	5.54	330.18	13.05	324.64	
0+00	T.P. Rubble Masonry wall		9.21	325.37	
0+2			6.9	323.8	
0+09	Wall		6.56	323.62	
0+10			8.5	321.7	
0+26	Peach Tree		9.0	321.2	
0+35	Fig Tree		9.2	321.0	
0+50			9.7	320.5	
0+78.50	△ on Concrete retaining wall		9.33	320.75	
0+79			12.3	317.9	
0+86			11.8	318.4	
1+03			10.2	320.0	
1+28			10.8	319.4	
1+53			13.1	317.1	
1+63			14.2	316.0	
1+73			13.6	316.6	
1+83			14.9	315.3	
2+02.5	End of line		15.9	314.8	
			16.83	Flow line existing	Appeal Pole

Step at church Garage + Estrella



Walker Mrs. Virgil Shaw Sheen 11-30-37

N. Section 15' Alley Blk (1) Dalby Hts.

277.79

SW B.P.			
Douglas + Albatross T.26	277.79		270.53
0+00 = N.L. Douglas			
E top cb		587	271.92
E Gut on Par.		620	271.59
℄ " "		654	271.25
W " " "		660	271.19
W top cb		630	271.49
18' North N.L. Douglas			
W		57	272.1
+2		54	272.4
℄		52	272.6
E		49	272.9
44' N = ℄ Con. Walk on E 36' Back 1.5' Wide			
-.36 = top Walk		430	273.49
E		450	273.29
℄		450	273.29
W		46	273.2
R = 4.10			273.69
53' N = South End dble. Garage on E 1' Back Con. Floor			
67' " = N " " " " " " " " "			
-1' = top Con Floor		438	273.41
E		44	273.4
℄		45	273.3
W		47	273.1
90' N			
W		54	272.4

℄	50	272.8
E	44	273.4
Rad = 45		
113' N = ℄ Euc. Tree on E 2' dia. 50' High ℄ Tree on E Line		273.3
128' N = ℄ Garage on E. on Line dirt Floor		
E	51	272.7
℄	55	272.3
W	59	271.9
132' N = South End Dble Garage on E. Con. Floor With Con. Apron		
W	58	272.0
℄	55	272.3
+69 = toe of Con Apron	476	273.03
E +0.10 = Garage Floor	464	273.15
1+49 = N end of Above Garage		
-.10 = Garage Floor	454	273.25
E +0.7 = toe of Apron	468	273.11
℄	48	273.0
W	49	272.9
0.3' in Alley		
1+55.15 = South Line of East + West Alley = ℄ Garage on E Wood Floor		
W	48	273.0
℄	47	273.1
+7.2 = Garage	46	273.2
Note, EAST LINE of North + South Alley = 0+00 of E + West Alley		
0+00.30 = West edge of Garage		
S	46	273.2
℄	50	272.8
N	48	273.0

Con Floor
on North 3' Back

5' West of E.L. of North + South Alley = ℄ Garage

-3' = Garage Floor		4.46	273.33
7.5' N = ℄ M.H. on RIM		5.20	272.59
15' West			
N		4.9	272.9
℄		4.8	273.0
S		4.8	273.0
20' N			
S		5.0	272.8
℄		4.6	273.2
N		4.8	273.0
38' N			
N		5.1	272.7
℄		5.2	272.6
S		6.0	271.8
+10		6.5	271.3
T.P	1.55 272.65	6.69	271.10
66' N			
S		2.3	270.3
℄		2.1	270.4
N		2.5	270.1

85' N = ℄ Garage on N dirt Floor 55' Back.

-55 on Floor		3.2	269.4
N		3.8	268.8
℄		4.2	268.4 ✓
S		4.0	268.6

96' N = ℄ Garage on North dirt Floor 55' Back

S	4.7	267.9
℄	4.7	267.9
N	4.3	268.3
+5.5 = Garage Floor	4.0	268.6

104' N = ℄ Garage on North + South dirt Floors

-4' = Garage Floor	4.3	268.3
N	4.6	268.0 ✓
℄	4.8	267.8
S = Garage Floor	4.9	267.7
115' N		
S	4.9	267.7
℄	5.2	267.4
N	5.3	267.3

dirt for 73' North of N.L.
125' West = ℄ Private drive on North Entrance at Washington St.

-73 on Con. drive	9.7	262.9
-15	8.1	264.5
N	7.5	265.1
℄	6.9	265.7
S	6.3	266.3

{Wood Floor}
East Ent. 16' Wide 0.5' in Alley
143' N = East edge Garage on North East Entrance to Above Private drive

-5	6.4	266.2
-4	6.6	266.0
S	8.4	264.2
℄	8.8	263.8
N	8.8	263.8 ✓

+8' = ℄ East End.	9.4	263.2
160' West = West end Above Garage 1' in Alley		
-16' = N end Above Garage		
Floor of Garage =	9.1	263.5
Ground at Base of Garage	18.5	254.1
N +1' at Floor	9.1	263.5
" " " on Ground	11.3	261.3
+4	10.0	262.6
℄	10.1	262.5
+4	9.5	263.1
S	9.0	263.6
+1	7.1	265.5
+5	7.1	265.5
Note: No Pipe Needed South of N.L.		
178' N = This Section may be Used for drain		
-5'	9.1	263.5
-2	9.7	262.9
S	10.6	262.0
+1	11.0	261.6
℄	11.1	261.5
+3	11.3	261.3
N	13.6	259.0
+13	16.0	256.6
+26	19.7	252.9
+40	24.6	248.0
205' N		
-15	13.7	258.9

N	11.1	261.5
+5	9.7	263.4
℄	9.1	263.5
S	8.6	264.0
+5	7.0	265.6
225' N		
S	6.6	266.0
℄	6.7	265.9
+4	6.8	265.8
N	8.4	264.2
+10	10.1	262.5 ✓
2+52 = ℄ Board Fence on N 08' in Alley 28' Wide		
265' N		
N-10	5.7	266.9
N	4.7	267.9
℄	5.1	267.5
S	5.7	267.4
T.P. 570 77345	4.90	267.75
274' N = ℄ Garage on N	6.26	267.19 Con. Floor 8.6' Back.
286' N = " " " "	6.7	267.2 Dirt Floor 10' Back
313.5' N = ℄ M.H.		
S	5.3	268.1
℄ on Rim of M.H.	5.26	268.19
N	5.3	268.1
	R= 5.07	268.43
324' N = East edge 4 Garages Con Floor With Con. Apron 4.3' Back		
327' N = ℄ Garage on N Con. Floor With Con. Apron		

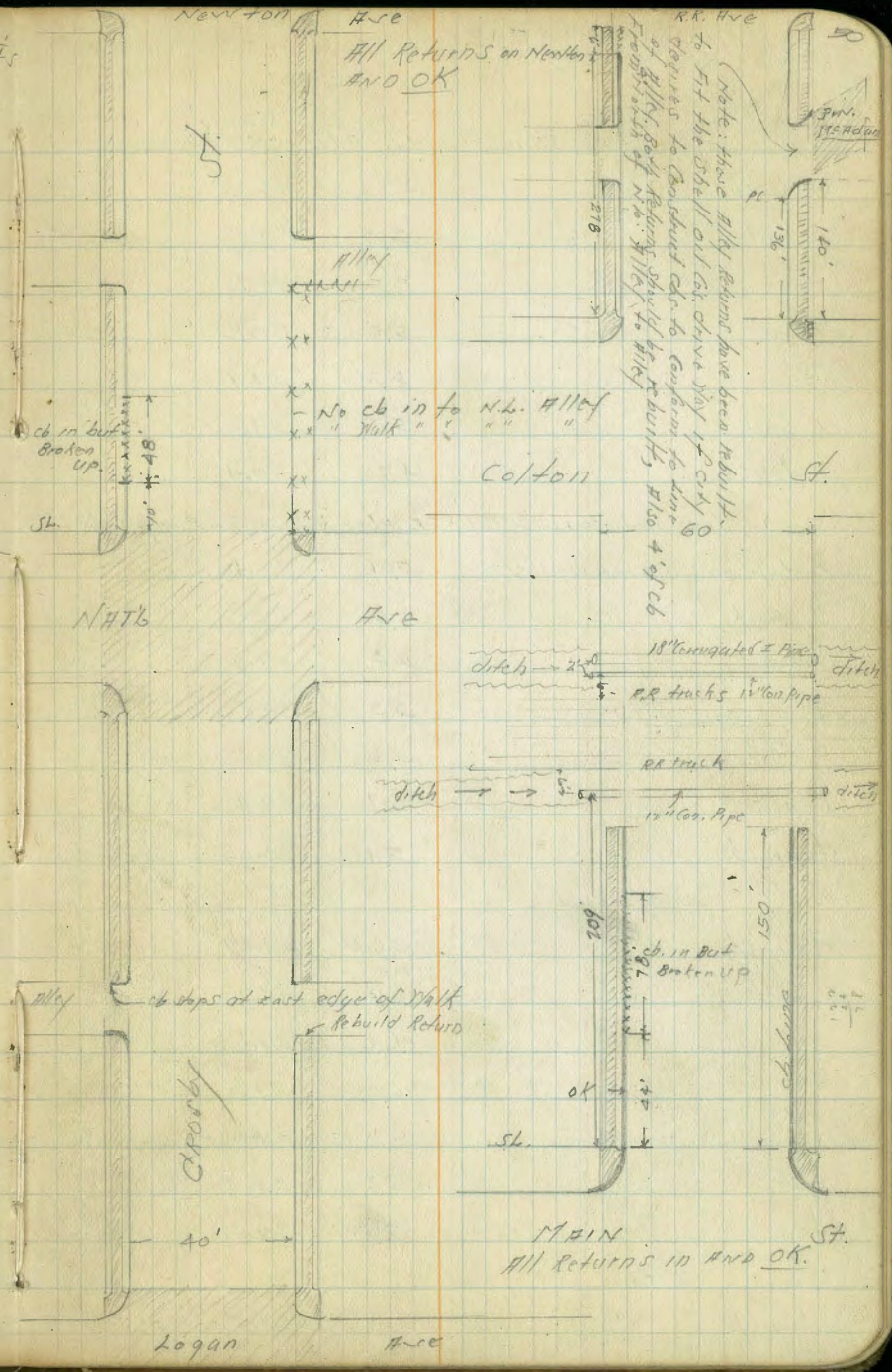
-6' = Garage Floor	5.41	268.04
N	5.41	268.04
+0.5' = Toe of Apron	5.41	268.04
℄	5.42	268.2
S	5.42	268.2
+4.3 on Apron	5.02	268.43
Rod on Apron	5.13	268.32
340' W = ℄ 4 Garages on South		
357' W = West end 4 Garages on South	4.3' Back Con Floors	Con Apron
-4.3 = Toe of Apron	5.18	268.27
S	5.3	268.1
℄	5.4	268.0
N	5.5	267.9
360' W = East end 4 Garages on South	5.18 4.3' Con Floor	268.27 Con Apron
394' W = W " " " "	" " " "	" " " "
-4.3' = Toe of Apron	5.21	268.24
S	5.8	267.6
℄	6.0	267.4
N = ℄ Garage dirt Floor	6.10	267.35
R= 5.77		267.73 8' Back.
402' W = ℄ Garage on South Con Floor		
R= 6.00		267.45
406' W = ℄ Garage on N Con Floor on line	5.80	267.65 8' Back
413' W = ℄ Garage on South Con Floor		
423' W = ℄ Garage on South Con Floor		8' Back.
N	6.0	267.4
℄	6.0	267.4
S	5.8	267.6
+8' on Garage Floor	5.76	267.69

R= 5.81	267.64	Con Floor 8' Back
434' W = ℄ Garage on South		
446' W = " " " " 5.82	267.63	" " Con Floor
T.P. 5.76	272.77 6.24	267.21
455' W = ℄ Garage on South Con Floor 12' Back.		
-12' on Garage Floor	5.38	267.59
S	5.6	267.4
℄	5.7	267.3
N	5.5	267.5
465' W = ℄ Private dirt Drive Way on South Entrance on Douglas ℄		
485' W = ℄ Garage on North Con. Floor 2' Back.		
-2' on Con. Floor	5.71	267.26
N	5.7	267.3
℄	6.0	267.0
S	5.7	267.3
+50'	5.4	267.6
+100'	6.0	267.0
+140'	6.7	266.3
+165.5 Gutter Line on Pav.	9.30	263.67
470.10 W = End of Alley		
S	5.7	267.3
℄	6.0	267.0
N	5.7	267.3
T.P. 7.25	271.37 8.85	264.12
Chi on N.W. BR Douglas & Grant	3.39	267.98
		268.00 = B.M.
		0.02 in Error.

Yds Taken from Shaw's Sheet (1-30-27)

X. Section Crosby St. 60' Wide 10' cbs 10' ½s
From Sh. Logan to S.L.Y. Termination

N.E. BP			
Nat'l. & Crosby	7.13	45.13	38.00
S.L. Logan Ave = 0+00			
E top cb.		2.67	42.46
E Gut on Pav.		2.67	42.46
" ¼		2.85	42.28
½ " "		2.85	42.28
W ¼ " "		2.91	42.22
W Gut " "		3.16	41.97
W top Cb.		2.74	42.39
50' South			
W top cb		3.47	41.66
" Gut on Ground		4.0	41.1
¼		4.0	41.1
½	12/29/27	3.9	41.2
¼	D.C.M. Book 16	3.9	41.2
E Gut	Yardage Book 12/30/27.	3.9	41.2
E top cb		3.39	41.74
100' South			
E top cb		4.17	41.01
E Gut		4.6	40.5
¼		4.8	40.3
½		4.5	40.6
¼		4.7	40.4
Gut		5.0	40.1
W top cb		4.20	40.9



140' South = N.L. Alley Rebuilt "N.W. Alley Return

W top cb	4.76	40.37
W Gut	5.3	39.8
¼	5.0	40.1
℄	5.0	40.1
¼	5.2	39.9
E Gut	5.3	39.8
E top cb	4.70	40.4

160' South = S.L. Alley Built "S.E. Alley Return From E edge Walk to Pl.

E top on cb line Crosby	5.06	40.1
" Gut	5.4	39.7
" ¼	5.4	39.7
℄	5.3	39.8
W ¼	5.5	39.6
W Gut	5.7	39.4
W top cb	5.10	40.03
2.00' South		
W top cb	5.64	39.49
W Gut	6.4	38.7
" ¼	6.0	39.1
℄	6.0	39.1
E ¼	6.1	39.0
" Gut	6.3	38.8
E top cb	5.67	39.51
2+50		
E top cb	6.76	38.77

E Gut	6.9	38.2
" ¼	6.7	38.4
℄	6.6	38.5
¼	6.7	38.4
W Gut	7.1	38.0
W top cb.	6.40	38.7
300' South = N.L. Natl Ave		
W top cb	7.19	37.94
" Gut on Par.	7.61	37.52
" ¼ " "	7.34	37.79
℄ " "	7.25	37.88
E ¼ " "	7.40	37.70
E Gut	7.68	37.45
E top cb.	7.17	37.96
S.L. Natl = 0+00		
E top cb	8.17	36.96
" Gut on Par.	8.82	36.31
" ¼ " "	8.53	36.60
℄ " "	8.35	36.78
W ¼ " "	8.52	36.61
W Gut " "	8.81	36.32
W top cb	8.28	36.85
T.P. 1.94	39.94 7.13	38.00
10' South		
W.L.	3.0	36.9
W cb.	3.5	36.4

+1	3.8	36.1
¼	3.6	36.3
℄	3.3	36.6
¼	3.5	36.4
E Gut	3.8	36.1
E top cb.	3.22	36.72
58' South		
E top cb.	4.35	35.59
" Gut	5.3	34.6
" ¼	5.0	34.9
℄	4.9	35.0
¼	5.0	34.9
+8	5.0	34.9
cb	4.6	35.3
W	4.0	35.9
100' South		
W	4.9	35.0
cb.	5.6	34.3
+3	6.3	33.6
¼	6.1	33.8
℄	6.0	33.9
¼	6.1	33.8
E Gut	6.0	33.9
E top cb.	5.30	34.64
160' South = S.L. Alley	N.E. SE & S.W. Returns in	
E top cb	6.75	33.19

Gut	7.4	32.5
¼	7.3	32.6
℄	7.3	32.6
¼	7.4	32.5
W Gut	7.4	32.5
W top cb. no cb Line Colby	6.74	33.20
200' South		
W top cb	7.63	32.31
W Gut	8.0	31.9
" ¼	8.3	31.6
℄	8.2	31.7
E ¼	8.2	31.7
E Gut	8.1	31.8
" top cb.	7.69	32.25
250' South		
E top cb	8.82	31.12
" Gut	9.2	30.2
" ¼	9.2	30.2
℄	9.2	30.2
¼	9.2	30.0
W Gut	9.3	30.1
" top cb.	8.77	31.17
300' South = N.L. Newton 80' Wide 14' Cbs 13¾s.		
T.P. 122	31.61 9.55	30.39
W top cb	1.58	30.03
W Gut	1.7	29.9

W ¼	1.6	30.0
d	1.4	30.2
E ¼	1.6	30.0
E Gut	1.4	30.2
E top cb.	1.62	29.99
N cb.		
E top cb.	1.74	29.87
" Gut	1.7	29.9
cb	1.5	30.1
¼	1.7	29.9
d	1.6	30.0
¼	1.4	30.2
cb	1.7	29.9
Gut	1.4	30.2
W top cb	1.64	29.97
N ¼		
W	1.7	29.9
cb.	1.7	29.9
¼	1.8	29.8
d	1.8	29.8
¼	1.6	30.0
cb	1.6	30.0
E	1.6	30.0
d Newton		
E.	1.7	29.9
cb.	1.8	29.8

¼	1.9	29.7
d	2.1	29.5
¼	1.8	29.8
cb.	1.8	29.8
W	2.0	29.6
S ¼		
W	1.9	29.7
cb	2.3	29.3
¼	2.3	29.3
d	2.6	29.0
¼	2.2	29.4
cb	2.2	29.4
E.	2.1	29.5
S cb.		
E top cb on Eb. Crosby	2.64	28.97
E Gut	2.8	28.8
E cb.	2.7	28.9
" ¼	2.6	29.0
d	2.6	29.0
W ¼	2.9	28.7
W cb	2.9	28.7
W Gut	2.9	28.7
W top cb. on W.b. Crosby	2.70	28.9
S.b. Newton = 0700		
W top cb.	2.62	28.99
" Gut	3.3	28.3

W ¼	3.5	28.1
℄	3.4	28.2
¼	3.1	28.5
E Gut	3.2	28.4
E top cb.	2.65	28.96
50' South		
E line	2.3	29.3
+2	3.0	28.6
+3	3.3	28.3
E top cb.	3.50	28.1
" Gut	4.0	27.6
" ¼	4.4	27.2
℄	4.1	27.5
W ¼	4.3	27.3
" Gut	4.2	27.4
" top cb.	3.65	27.96
W	3.0	
100' South		
W	4.1	27.5
" top cb	4.56	27.05
" Gut	5.5	26.1
" ¼	5.1	26.5
℄	5.0	26.6
¼	5.0	26.6
E Gut	5.0	26.6
E top cb	4.59	27.02

+7	4.0	27.6	
E	3.1	28.5	
140' South = N.L. Alley			
E on Ground (Return covered up)	4.5	27.1	Returns All in
+3	5.2	26.4	
E top cb.	5.39	26.22	
" Gut	6.0	25.6	
" ¼	5.8	25.8	
℄	5.8	25.8	
W ¼	6.1	25.5	
W Gut	6.2	25.4	
W top cb.	5.39	26.22	
W	5.2	26.4	
160' South = S.L. Alley			
W	5.6	26.0	
+3	5.3	26.3	
W top cb	5.87	25.74	
" Gut	6.6	25.0	
" ½	6.6	25.0	
℄	6.3	25.3	
E ¼	6.3	25.3	
" Gut	6.3	25.3	
" Top cb.	5.86	25.75	
200' South			
E top cb	6.70	2491	
E Gut	7.4	24.2	
" ½	7.2	24.4	

℄		7.2	24.4
W ¼		7.5	24.1
W Gut		7.6	24.0
W top cb.		6.63	24.98
+7		6.4	25.2
W		5.9	25.7
	2.50' South		
W		7.0	24.6
+7		7.2	24.4
W top cb.		7.68	23.93
" Gut		8.4	23.2
" ¼		8.5	23.1
℄		8.2	23.4
E ¼		8.1	23.5
" Gut		8.5	23.1
E top cb.		7.65	23.96
	300' South = N.W. MAIN St. 80' Wide 14'cb 13' ⅛		
E top cb.		8.66	22.95
" Gut		9.1	22.5
" ¼		9.1	22.5
℄		9.1	22.5
W ¼		9.1	22.5
" Gut		9.1	22.5
" top cb.		8.62	22.99
T.P.	2.40 24.70	9.31	22.30
	N cb.		

W top cb on W.L. Crosby	1.74	22.96
" Gut " " "	1.8	22.9
W cb.	2.6	22.1
" ¼	2.5	22.2
℄	2.5	22.2
E ¼	2.1	22.6
E cb.	2.2	22.5
E Gut on E.L. Crosby	2.2	22.5
E top cb. " " "	1.78	22.92
	North cb	
E	2.2	22.5
cb	2.3	22.4
¼	2.4	22.3
℄	2.5	22.2
¼	2.8	21.9
cb	2.6	22.1
W	2.5	22.2
	N ¼	
W	2.6	22.1
cb	2.9	21.8
¼	2.9	21.8
E	2.8	21.9
¼	2.6	22.1
cb	2.6	22.1
E	2.4	22.3
	℄	

E	27	22.0
cb	29	21.8
¼	30	21.7
℄	31	21.6
¼	34	21.3
cb	33	21.4
W	3.2	21.5
South cb		
W top cb on W.L. Crosby	274	21.96
" Gut	29	21.8
" cb	35	21.2
¼	35	21.2
℄	33	21.4
¼	31	21.6
cb	3.2	21.5
Gut on E.L. Crosby	29	21.8
E top cb on E.L. Crosby	270	22.0
S.L. Main = 0+00		
E top cb.	274	21.96
" Gut	34	21.3
" ¼	36	21.1
℄	35	21.2
W ¼	34	21.3
W Gut	37	21.0
" top cb.	276	21.94
44' South.		

W top cb.	378	20.92	
" Gut	47	20.0	
" ¼	45	20.2	
℄	44	20.3	
¼	43	20.4	
E Gut	44	20.3	
E top cb	381	20.89	
0+56 E top cb	431	20.39	See sketch Page 50
0+71 " " "	447	20.28	
0+85 " " "	477	19.93	
100' South.			
E top cb	568	19.08	
" Gut	60	18.7	
" ¼	54	19.3	
℄	55	19.2	
¼	58	18.9	
W Gut	60	18.7	
W top cb.	508	19.62	
1+22 E top cb	564	19.06	
150' South = End of Exist. Walk Exc Curb on East + West.			
W top cb	624	18.46	
W Gut	71	17.6	
" ¼	72	17.5	
℄	67	18.0	
E ¼	66	18.1	
E Gut	70	17.7	

E top Cb.	6.76	18.44
1+98		
E	6.7	18.0
cb	6.4	18.3
+2	7.2	17.5
¼	7.7	17.0
2	7.8	16.9
½	7.8	16.9
cb	7.6	17.1
W	7.2	17.5
2+09 = 2 Con Pipe Parallel with R.R. tracks		
-3' = Flow Line 12" Con. Pipe	10.83	13.87
W	7.9	16.8
cb	7.9	16.8
¼	8.0	16.7
2	8.0	16.7
¾	8.1	16.6
cb	7.7	17.0
E	7.1	17.6
+3 on Exist Flow line 12" Con Pipe	10.09	14.61
T.P. 4.79	7.44 805	16.65 13.39
216' South = N Rail of R.R. track.		
E Top of Rail	4.85	16.59
W.L. " " Rail	5.00	16.44
243.50' South = South Rail of R.R. track		
W.L. top of Rail	5.00	16.44
E.L. " " "	4.92	16.52

250' South = 2 12" Con. Pipe Parallel with R.R. tracks		
-3' Flow Line	7.05	14.36
E	5.0	16.4
cb	5.3	16.1
¼	5.2	16.2
2	5.2	16.2
½	5.0	16.4
cb.	5.2	16.2
W	5.3	16.1
+3 = Flow Line	7.29	14.11
252' South = 2 18" Corrugated Iron Pipe Parallel with track		
W.L. = Flow Line	7.54	13.90
E+2' = " "	7.38	14.16
290' South		
W	6.1	15.3
cb	6.3	15.1
¼	6.6	14.8
2	6.4	15.0
¾	6.8	14.6
cb	6.5	14.9
E.	6.1	15.3
300' South = N.L. Colton st 80' Wide 14' Cbs 13½ 85		
E	6.2	15.2
cb	6.1	14.6
¼	6.7	14.7
2	6.7	14.7

¼		6.8	14.6
cb		6.4	15.0
W		6.2	15.2
	N cb		
W		6.5	14.9
cb		6.6	14.8
¼		6.8	14.6
℄		6.9	14.5
¼		6.9	14.5
cb		6.8	14.6
E		6.5	14.9
	N ¼		
E		6.6	14.8
cb		6.8	14.6
¼		7.2	14.2
℄		7.1	14.3
¼		7.0	14.4
cb		6.8	14.6
W		6.7	14.9
	℄		
W		6.9	14.5
cb		7.0	14.4
¼		7.3	14.1
℄		7.3	14.1
¼		7.4	14.0
cb		7.1	14.3

E		6.8	14.6
	S ¼		
E		7.5	13.9
cb		7.5	13.9
¼		7.7	13.7
℄		7.4	14.0
¼		7.6	13.8
cb		7.2	14.2
W		7.0	14.4
	S cb		
W top cb		7.43	14.01
W Gut		7.4	14.0
" cb		7.8	13.6
" ¼		8.0	13.4
℄		7.7	13.7
E ¼		7.8	13.6
" cb		7.8	13.6
" Gut		7.5	13.9
E top cb		7.45	13.99
	S.L. Cb/ton st = 0400		
E top cb		7.43	14.01
Gut		7.8	13.6
¼		8.2	13.2
℄		7.9	13.5
¼		8.1	13.3
Gut		8.1	13.3

21.44

W top Cb.			7.35	14.09
T.P.	5.04	18.28	8.20	13.24
	30' South			
W top Cb			5.16	13.12
" Gut			5.70	12.6
" ¼			5.8	12.5
℄			5.8	12.5
¼			6.1	12.2
E Gut			6.8	11.5
E top Cb			5.12	13.16
	100' South			
E top Cb.			5.90	12.38
" Gut			6.5	11.8
" ¼			7.0	11.3
℄			6.8	11.5
¼			7.1	11.2
W Gut			7.0	11.3
W top Cb			4.07	12.21
	140' S = N.L. Hwy			
W top Cb.			6.70	11.58
W Gut			7.3	11.0
W ¼			7.5	10.8
℄			7.6	10.7
¼			7.5	10.8
E Gut			7.2	11.1
E top Cb			6.59	11.69

18.28

160' ??

59

E top Cb	6.93	11.35
" Gut	7.3	11.0
" ¼	7.8	10.5
℄	8.0	10.3
W ¼	8.0	10.3
W Gut	7.7	10.6
W top Cb	7.15	11.13
	200' South	
W on Drive Way Approach	8.64	9.64
W Gut	8.6	9.7
W ¼	8.7	9.6
℄	8.7	9.6
¼	8.6	9.7
E Gut	8.4	9.9
E top Cb	7.63	10.65
	250' South	
E top Cb.	8.40	9.88
E Gut	9.0	9.3
¼	9.2	9.1
℄	9.3	9.0
¼	9.7	8.6
Gut	9.7	8.6
W top Cb	8.84	9.44
T.P. 4.41	13.40 +3.41 R= 4.01	9.99 4.00

278' South = End of Good Curb on East.

284' " " " Walk on East

W top cb.	4.62	8.78
W Gut	5.4	8.0
" ¼	5.5	7.9
℄	5.7	8.2
¼	5.0	8.4
E Gut	4.8	8.6
E top cb.	4.28	9.12
300' South = N.L. R.R. Fence 80 wide 14 cbs		13'.45
E	4.7	8.7
cb	5.2	8.2
½	5.3	8.1
℄	5.5	7.9
¼	5.7	7.7
cb	5.7	7.7
Gut.	5.7	7.7
W top cb.	4.86	8.54
North cb		
W top cb. on W.L. Crosby	4.86	8.54
W Gut " " "	5.1	8.3
+8	5.2	8.2
cb.	5.7	7.7
+2	6.1	7.3
¼	6.1	7.3
℄	5.8	7.6
¼	5.8	7.6
cb.	5.5	7.9

134D

E	5.0	8.4
T.P. on N.W. top cb	4.84	8.54 ~~8.55~~

McHugh Flood Rauner 1/9/28

X Section Hyacinth from RR to Cass St. Intersection at Allison excepted.

B.M. Nails in RR trolley pole north of Lawring St. Elev. 70.90

	+	x	−	
T.R.	5.73	76.63		70.90
		15' cbs.	10' quarters	
		0+00 =	Rail Road	
0+00				
NL			1.6	75.0
+7			2.2	74.4
+12			3.4	73.2
cb			2.5	74.1
¼			1.8	74.8
℄			3.0	73.6
¾			1.9	74.7
cb			2.0	74.6
SL			2.1	74.5
0+49.70				
SL			1.4	75.2
cb			1.3	75.3
¼			1.1	75.5
℄			1.1	75.5
¼			1.1	75.5
cb			1.9	74.7
NL			0.3	76.3
0+99.70				
T.P.	11.73	87.50	0.86	75.77
0+99.70				
N.L.			9.6	77.9

87.5

	+	x	−	
cb			7.3	80.2
+4			10.3	77.2
¼			10.7	76.8
℄			11.1	76.4
+8			11.2	76.3
¾			12.4	75.1
cb			11.9	75.6
SL			11.0	76.5
1+49.70 = WL. Allison				
SL			9.4	78.1
cb			9.6	77.9
¼			11.6	75.9
+2			9.7	77.8
℄			9.6	77.9
¼			9.3	78.2
cb			9.4	78.1
+2			10.2	77.3
NL			8.7	78.8
0+00 = EL. Allison				
NL			5.6	81.9
+12			5.8	81.7
cb			8.7	78.8
¼			5.8	81.7
℄			5.8	81.7
¼			6.6	80.9

87.5

	+	-	
Cb		6.5	81.0
SL		6.7	80.8 ✓
0+50			
SL		5.8	81.7 ✓
Cb		5.7	81.8
¼		5.8	81.7
℄		4.9	82.6 ✓
¼		4.8	82.7
Cb		5.2	82.3
NL		4.6	81.9 ✓
1+00			
NL		3.6	83.0 ✓
Cb		4.3	83.2
¼		3.7	83.8
℄		3.9	83.6 ✓
¼		4.7	82.8
Cb		4.7	82.8
SL		4.6	82.9 ✓
1+50			
SL		3.5	84.0 ✓
Cb		3.4	84.1
¼		3.3	84.2
℄		2.5	85.0 ✓
¼		2.4	85.1
Cb		2.8	84.7

87.5

	+	-	
NL		2.2	85.3 ✓
2+00			
NL		1.4	86.1 ✓
Cb		1.7	85.8
¼		1.6	85.9
℄		2.0	85.5 ✓
¼		2.7	84.8
Cb		3.0	84.5
SL		3.2	84.3 ✓
2+50			
SL		2.3	85.2 ✓
Cb		1.8	85.7
¼		2.2	85.3
℄		1.3	86.2 ✓
¼		1.2	86.3
Cb		1.7	85.8
NL		0.9	86.6 ✓
3+00			
NL		0.1	87.4 ✓
Cb		0.9	86.6
¼		0.0	87.5
℄		0.2	87.3 ✓
¼		1.1	86.4
Cb		1.0	86.5
SL		1.5	86.0 ✓

	+	π	−	
T.P.	9.69	95.75	1.44	86.06
SL 3+50			8.8	87.0
CB			8.4	87.4
¼			8.4	87.4
℄			7.6	88.2
¼			7.6	88.2
CB			8.2	87.6
+5			7.3	88.5
NL			7.1	88.7
4+00				
NL			6.5	89.3
+10			6.6	89.2
CB			7.1	88.7
¼			6.5	89.3
℄			6.6	89.2
¼			7.5	88.3
CB			7.2	88.5
+2			7.0	88.8
SL			7.4	88.4
4+50				
SL			6.4	89.4
CB			6.0	89.8
+5			6.6	89.2
¼			6.2	89.6
℄			5.5	90.3

95.8

	+	π	−	
¼			5.3	90.5
CB			6.0	89.8
NL			5.3	90.5
5+00				
NL			3.7	92.1
+8			3.9	91.9
CB			4.4	91.4
¼			3.6	92.2
CL			3.6	92.2
¼			4.4	91.4
+5			4.8	91.0
CB			4.4	91.4
SL			5.1	90.7
5+50				
SL			4.1	91.7
CB			3.8	92.0
¼			3.8	92.0
℄			2.8	93.0
¼			2.6	93.2
CB			3.2	92.6
+7			2.7	93.7
NL			2.5	93.3
6+00				
NL			1.6	94.2
+10			1.9	93.4

95.8

	+	x	−	
cb			2.3	93.5
¼			1.4	94.9
℄			1.5	94.3 ✓
¼			2.4	93.4
cb			2.7	93.1
SL			3.1	92.7 ✓
6+58.50 = W.L. Bayard St. 40' wide				
SL			2.0	93.8 ✓
cb			1.8	94.0
¼			1.8	94.0
℄			1.0	94.8 ✓
¼			1.0	94.8
℄ b.			1.2	94.6
NL			0.6	95.2 ✓
℄ Bayard St.				
NL			0.5	95.3
cb			0.7	95.1
¼			0.9	94.9
℄			1.4	94.9
¼			1.6	94.2
cb			1.8	94.0
SL			2.0	93.8
T.P.	958	104.07	1.26	94.49
EL Bayard St = 0+00				
SL			9.6	94.5 ✓

104.1

	+	x	−	
cb			9.5	94.6
¼			9.3	94.8
℄			8.8	95.3 ✓
¼			8.3	95.8
cb			8.7	95.4
NL			8.5	95.6 ✓
0+50				
NL			6.5	97.6 ✓
+8			6.7	97.4
cb			7.5	96.6
¼			6.9	97.2
℄			7.0	97.1 ✓
¼			8.1	95.9
℄			8.1	95.9
SL			8.0	96.1 ✓
1+00				
SL			7.0	97.1 ✓
cb			6.3	97.8
+5			6.3	97.8
¼			6.6	97.5
℄			5.4	98.7 ✓
¼			5.4	98.7
cb			6.2	97.9
NL			5.2	98.9 ✓
1+50				

104'

	+	x	−	
NL			4.3	99.8 ✓
cb			5.0	99.1
¼			4.5	99.6
℄			4.5	99.6 ✓
¼			5.5	98.6
cb			5.6	98.5
SL			6.6	97.5 ✓
2+00				
SL			5.5	98.4 ✓
cb			4.9	99.2
¼			5.1	99.0
℄			4.1	100.0 ✓
¼			4.1	100.0
cb			4.2	99.9
NL			3.4	100.7 ✓
2+50				
NL			2.6	101.5 ✓
cb			3.7	100.4
¼			3.3	100.8
℄			3.5	100.6 ✓
¼			4.6	100.5
+5			4.0	100.1
cb			4.1	100.0
SL			3.9	100.2 ✓
3+00				

100'

	+	x	−	
SL			4.2	99.9 ✓
cb			4.0	100.1
¼			3.8	100.3
℄			2.9	101.2 ✓
¼			2.4	101.7
cb			2.7	101.4
NL			2.1	102.0 ✓
3+50				
NL			1.6	102.5 ✓
cb			2.5	101.6
¼			2.0	102.1
℄			2.3	101.8 ✓
¼			3.3	100.8
cb			3.6	100.5
SL			4.0	100.1 ✓
3+79.6 = NL Cass St.				
SL			3.6	100.5 ✓
cb			3.1	101.0
¼			3.0	101.1
℄			2.2	101.9 ✓
¼			1.7	102.4
cb			2.1	102.0
NL			1.4	102.7 ✓

NL Cass St. +23' = Edge of unpaved strip on W. side of Cass

1041

	+		−	
NL			2.5	101.6
cb			2.9	101.2
¼			3.3	100.8
℄			3.7	1004
¼			4.0	100.1
cb			4.3	1998
SL			4.7	994
WL Cass St		+34' = Edge of Pavement		
SL			3.71	
cb			3.27	
¼			3.05	
℄			2.82	
¼			2.49	
cb			2.22	
NL			1.75	
T.P.	8.41	111.91	0.57	10350

X section of Tourmaline

from WL. Cass to R.R.

0+00 = WL Cass

111.91

+ 15' cbs 10' quarters −

H.I. carried over from Preceding page

WL. Cass St − 32' = Edge of pavement

SL	2.14	10977
cb	1.70	11021
¼	1.35	11056
℄	1.10	11081
¼	0.87	11104
cb	0.72	11119
NL	0.28	11163

WL Cass St − 26' = Edge of unpaved strip on west side of Cass St.

NL	0.6	1113
cb	0.9	1110
¼	1.0	1109
℄	1.3	1106
¼	1.6	1103
cb	1.9	1100
SL	2.2	1097
0+00		
SL	1.8	1101
cb	1.7	1102
¼	1.2	1107
℄	0.4	1115
¼	0.5	1114
cb	0.4	1115

	+	℄ 111.91	−	
NL			0.8	111 1
0+29 ↵				
NL			0.5	111 6
cb			1.0	110 9
¼			1.2	110 7
℄			1.3	110 6
¼			1.8	110 1
cb			2.5	109 4
SL			2.0	109 9
0+79 ↵				
SL			3.4	108 5
cb			3.4	108 5
¼			2.9	109 0
℄			2.5	109 4
¼			2.5	109 4
cb			2.5	109 4
NL			2.0	109 9
1+29 ↵				
NL			4.5	107 4
cb			4.4	107 5
¼			4.0	107 9
℄			3.7	108 2
¼			4.2	107 7
cb			4.8	107 1
SL			4.3	107 6

	+	℄ 111.91	−	
1+54 ↵				
SL			5.1	106 8
cb			5.3	106 6
¼			5.1	106 8
℄			5.0	106 9
¼			5.5	106 4
cb			6.1	105 8
NL			6.5	105 4
1+79 ↵				
NL			7.5	104 4
cb			7.4	104 5
¼			6.8	105 1
℄			6.1	105 8
¼			6.0	105 9
cb			6.4	105 5
SL			5.9	106 0
2+29 ↵				
SL			7.5	104 4
cb			7.8	104 1
¼			7.0	104 9
℄			6.7	105 2
¼			7.4	104 5
cb			8.3	103 6
NL			8.3	103 6
2+79 ↵				

	+	℄ 111.91	−	
NL			9.1	102 8
cb			9.1	102 8
¼			8.9	103 0
℄			8.5	103 4
¼			8.3	103 6
cb			8.5	103 4
SL			8.4	103 5
3+04				
SL			9.0	102 9
cb			9.2	102 7
¼			9.2	102 7
℄			9.2	102 7
¼			9.4	102 5
cb			9.7	102 2
NL			9.9	102 0
T.P.	0.82	105.06	7.67	104.24
329				
NL			3.1	102 0
cb			3.6	101 5
¼			3.5	101 6
℄			3.4	101 7
¼			3.6	101 5
cb			3.9	101 2
SL			3.4	101 7
3+79 = E.L. Bayard				

	+	℄ 105.06	−	
SL			5.4	100 7
cb			5.0	100 1
¼			4.9	100 2
℄			4.7	100 4
¼			4.6	100 5
cb			4.8	100 3
NL			4.4	100 7
℄ Bayard st				
NL			4.2	100 9
cb			4.7	100 4
¼			5.0	100 1
℄			5.1	100 0
¼			5.2	99 9
cb			5.2	99 9
SL			5.3	99 8
0+00 = WL Bayard				
SL			5.1	99 4
cb			5.6	99 5
¼			5.6	99 5
℄			5.5	99 6
¼			5.4	99 7
cb			5.1	100 0
NL			4.8	100 3
0+58				
NL			6.1	99 0

	+	π 105.06	−		
cb			7.0	98	1
¼			7.2	97	9
℄			7.5	97	6
¼			7.5	97	6
cb			7.7	97	4
SL			7.5	97	6
1+08 5					
SL			9.2	95	9
cb			9.2	95	9
¼			9.1	96	0
℄			9.0	96	1
¼			8.6	96	3
cb			8.2	96	9
NL			7.9	97	2
1+58 50					
NL			8.0	97	1
cb			8.9	96	2
¼			9.4	95	7
℄			9.7	95	4
¼			10.0	95	1
cb			10.1	95	0
SL			10.6	94	5
2+08 5					
SL			11.3	93	8
cb			10.9	94	2

	+	π 105.06	−		
¼			10.5	94	6
℄			10.1	95	0
¼			9.5	95	6
cb			9.1	96	0
NL			8.4	96	7
2+58 5					
NL			10.5	94	6
cb			10.5	94	6
¼			10.7	94	4
℄			10.9	94	2
¼			11.2	93	9
cb			11.1	94	0
SL			11.3	93	8
3+08 5					
SL			11.9	93	2
cb			11.7	93	4
¼			11.3	93	8
℄			11.2	93	9
¼			10.7	94	4
cb			10.7	94	4
NL			10.4	94	7
3+58 5					
NL			10.6	94	5
cb			11.0	94	1
¼			11.5	93	6

	+	105.06	−		
℄			11.7	93	4
¼			11.9	93	2
cb			12.1	93	0
SL			12.4	92	7
T.P.	0.44	93.65	11.85	93.21	
4+08.5					
SL			1.8	91	8
cb			1.5	92	1
¼			1.3	92	3
℄			1.0	92	6
¼			0.7	92	9
cb			0.6	93	0
NL			0.0	93	6
4+58.5					
NL			0.3	93	3
cb			0.6	93	0
¼			1.0	92	6
℄			1.1	92	5
¼			1.5	92	1
cb			1.8	91	8
SL			2.4	91	2
5+08.5					
SL			2.7	90	9
cb			2.4	91	2
¼			1.8	91	8

	+	93.65	−		
℄			1.8	91	8
¼			1.4	92	2
cb			1.3	92	3
NL			0.8	92	8
5+68.5					
NL			1.8	91	8
cb			2.1	91	5
¼			2.3	91	3
℄			2.5	91	1
¼			2.7	90	9
cb			3.0	90	6
SL			3.4	90	2
6+08.5					
SL			4.0	89	6
cb			3.8	89	8
¼			3.4	90	2
℄			3.3	90	3
¼			3.1	90	5
cb			2.6	91	0
NL			2.7	90	9
6+58.5 = Right Ls to Tourmaline					
NL			8.0	85	6
cb			8.4	85	2
¼			8.4	85	2
℄			8.1	85	5

	+	↑ 9365	−	
¼			7.1	86 5
cb			5.5	88 1
+6			5.0	88 6
SL			5.0	88 6
6+58⁵ = EL Allison taken on diagonal				
SL			5.0	88 6
+12			5.3	88 3
cb			6.1	87 5
¼			8.4	85 2
℄			9.4	84 2
¼			9.4	84 2
cb			8.6	85 0
NL			6.9	86 7
0+00 = WL Allison taken on diagonal				
NL			4.5	89 1
cb			6.2	87 4
¼			7.1	86 5
℄			8.0	85 6
¼			9.1	84 5
cb			10.1	83 5
SL			12.1	81 5
0+20.4 = R+Ls to Tourmaline				
SL			11.7	81 9
cb			9.9	83 7
¼			8.6	85 0

	+	↑ 9365	−	
℄			7.7	85 9
¼			6.7	86 9
cb			5.6	88 0
NL			4.3	89 3
0+50				
NL			5.1	88 5
cb			5.5	88.1
¼			6.1	87 5
℄			6.6	87 0
¼			7.6	86 0
cb			8.5	85 1
SL			9.9	83 7
0+95				
SL			8.7	85 4
cb			7.5	86 1
¼			6.9	86 7
℄			6.5	87 1
¼			6.0	87 6
cb			5.7	87 9
NL			5.3	88 3
1+20				
NL			5.9	88 2
cb			6.0	87 6
¼			6.4	87 2
℄			6.7	86 9

	+	↑ 93.65	−	
¼			7.1	86 5
cb			7.5	85 1
S L			8.0	85 6
1+70				
S L			9.6	84 0
cb			9.1	84 5
¼			8.8	84 4
℄			8.5	85 1
¼			8.1	85 1
cb			7.6	86 0
N L			7.1	86 5
2+09.8				
N L			8.1	85 5
cb			8.7	84 9
¼			9.1	84 5
℄			9.4	84 2
¼			9.7	83 9
cb			10.0	83 6
S L			10.7	82 9
T.P.	3.79	85.86 ✓	11.58	82.07
2+59.8				
S L			4.9	81 0
cb			3.8	82 1
¼			3.6	82 3
℄			3.6	82 3

	+	↑ 85.86	−	
¼			3.2	82 7
cb			3.0	82 9
N L			2.5	83 4
3+09.8 = Rt ∠s to Tourmaline				
N L			3.7	82 2
cb			4.2	81 7
¼			4.3	81 6
+5			4.2	81 7
℄			6.5	79 4
¼			7.0	78 9
cb			6.3	79 6
S L			6.7	79 2
3+09.8 on diag. to 3+30 ± N L station				
S L			6.7	79 2
cb			6.7	79 2
¼			7.1	79 8
℄			8.6	77 3
¼			7.0	78 9
+2			4.6	81 3
cb			4.6	81 3
N L			4.2	81 7
T.P.	2.51	76.20 ✓	12.17	73 69
T.P.			5.50	70.70 ✓
		70.90		
		70.70		
		.20		

Levels for Drain on line 2 N. of ℄ Walnut from ℄ Union to ℄ Lark

2-21-28 Miller.

BM N.W. Blk Cr	12.54	147.83		135.29	Union & Walnut
00 = ℄ Union			11.1	136.7	
+25			7.0	140.8	
T.P.	12.31	159.94	0.20	147.63	
+50			10.8	149.1	
+68			6.3	153.6	✓
+73			8.1	151.8	
1+06			9.3	150.6	✓
T.P.	12.44	172.56	0.22	159.72	
1+08			9.4	163.1	✓
1+35			5.0	167.5	✓
1+55			2.9	169.6	✓
T.P.	12.66	182.34	2.88	169.68	
1+87			10.0	172.3	
1+90			10.3	172.0	
2+02			88. (?)	173.5	✓
2+14			0.5	181.8	✓
T.P.	12.51	194.53	0.32	182.02	
2+33			0.4	194.1	✓
T.P.	12.72	206.38	0.86	193.67	
2+50			3.0	203.4	✓
T.P.	12.27	218.51	0.15	206.24	
2+65			10.2	208.3	
2+69 approx W line Lark			8.4	210.1	
2+75			5.0	213.5	
2+85			3.3	215.2	

219.51

T.P.	12.53	228.76	2.28	216.23
3+00			12.9	215.9
3+09 ℄ Lark			12.7	216.1
T.P.	10.41	235.42	3.75	225.01
Chk on BM.			2.60	232.82

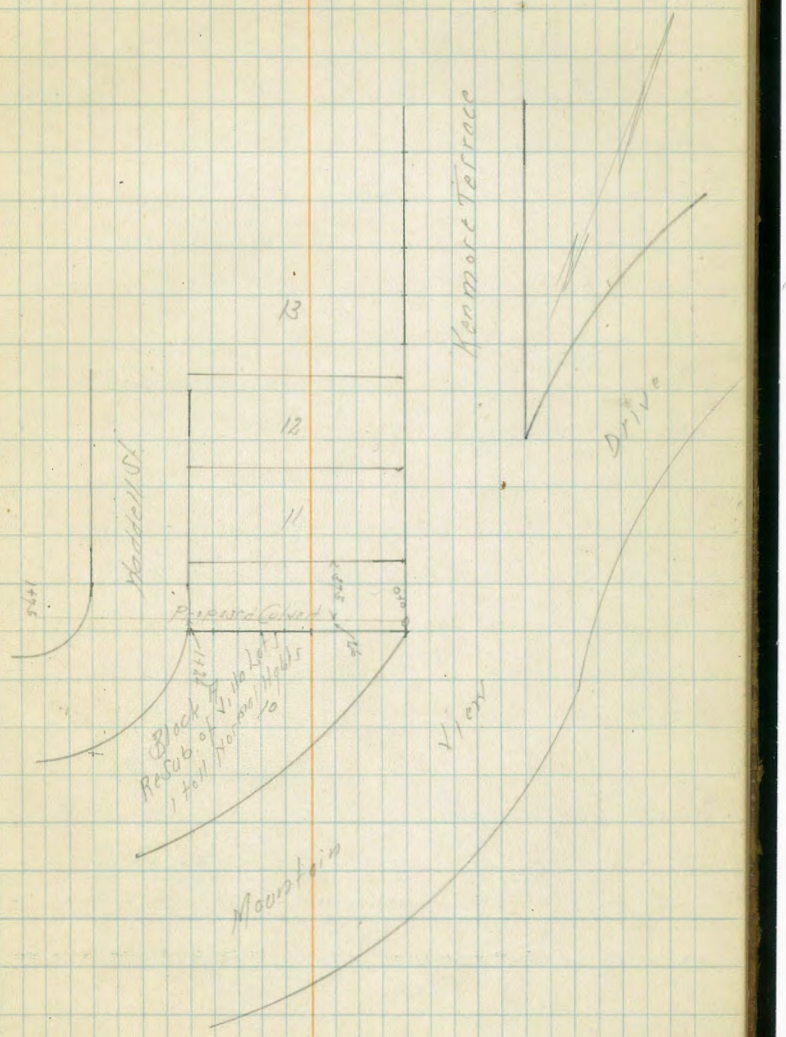
NE. Blk for Lark & Walnut.

See Page 33 for Profile 10' N of ℄ Walnut

S.P. 38
S.A.C.
Bliss
Koogler

Levels For Proposed Culvert
Kenmore Terrace to Haddell St

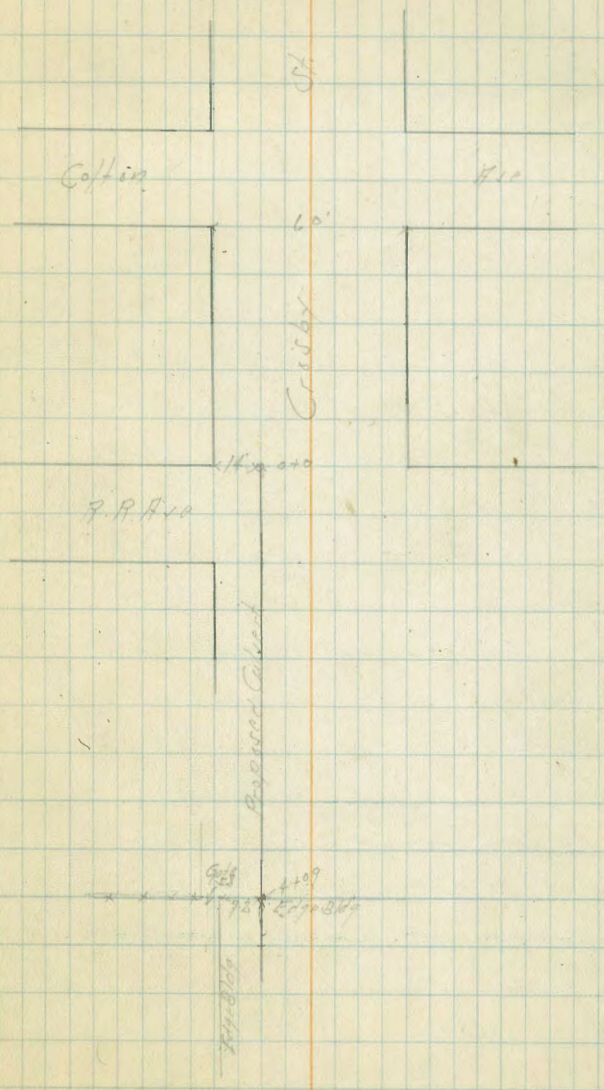
BM	471	393.80		389.09	H.I. 8.7 Adams HM & View
0+0 = H.I. Kenmore			53		
0+Top Curb			54.5		
+8			65		
+25			71		
+50			82		
+75			9.2		
1+0			82		
+34 = E.L. Haddell St			88		
+55			97		
+75			103		



5-7-78
S. Fenton
D.I.S.S.
Ramsey

Levels For Proposed Culvert In Crosby St. Rail Road Ave to Bay

					SE Mon.
BM	1.07	23.25		22.18	Main-Crosby
TP	2.27	15.09	10.43	12.82	
					N.W. Track
BM			1.52	13.57	Crosby St Rail Road Ave
0+0 = N.L. of P.R.R. Ave			7.7	7.4	
+50			8.0	7.1	
1+0			8.3	6.8	
+50			9.0	6.1	
+77 = on Top Rail of Siding B Track			9.08	6.01	
2+0			9.2	5.9	
+32 = on Top Rail of Mainline A Track			9.39	5.80	
+50			10.2	4.9	
TP	3.12	9.01	9.20	5.89	
3+0			9.4	4.6	
+50			9.7	3.5	
4+0			6.6	2.4	
+9 = Edge Bldg on Floor			6.87	2.14	
TP	5.00	6.89	7.16	1.89	
+15 Appox. Under Bldg			6.9	0.00	
+50 " " "			9.1	— 2.12	

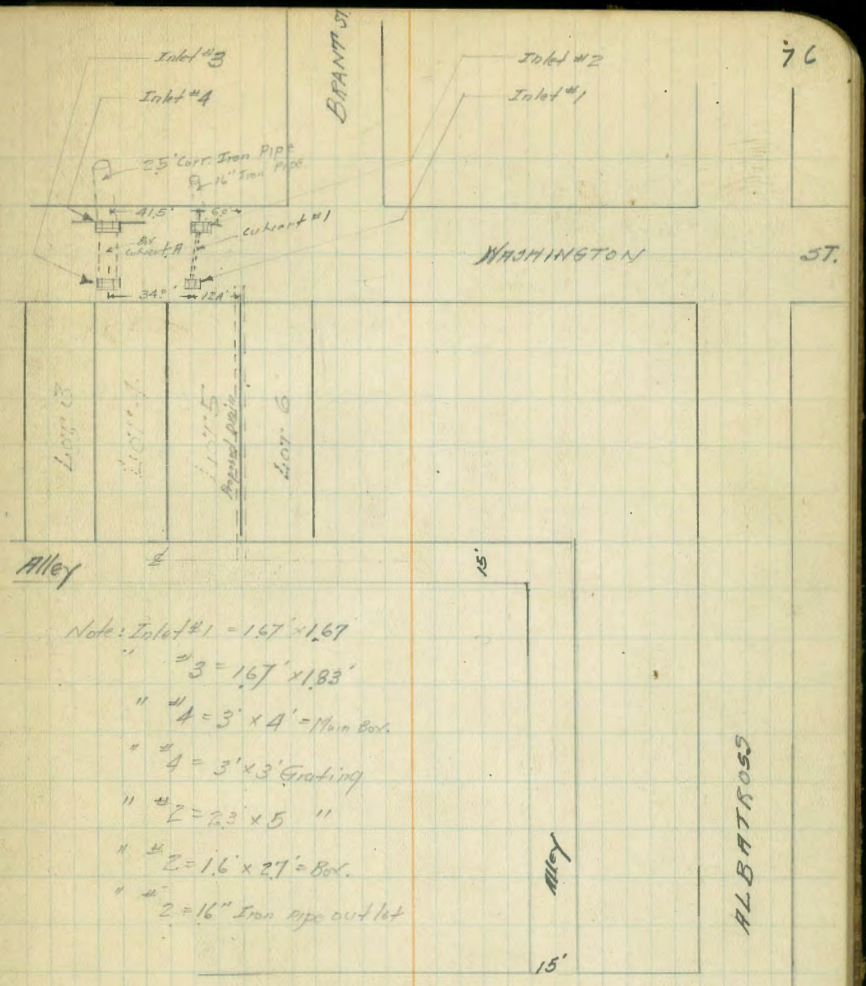


Walker McHugh. McHood Leakey 7-3-29

LEVELS FOR CULVERT

as located on Lot Lines #5 and 6

	2.08	266.55		264.47	N.W. & P. Washington and Dove St.
T.P.	4.88	263.90	7.53	259.02	
T.P.	9.43	270.88	2.45	261.45	
130.86' S.Sly. Washington on Line Lots 5 and 6 = 8+00 = S Alley			4.6	266.3	
+04			4.7	266.2	
+08			6.0	264.9	
+50			10.5	260.4	
+75			11.4	259.5	3' Rt. = 1.5 Lower.
1+00			11.7	259.2	3' Rt. = 0.5 Lower.
+30.36 = St. Washington			12.7	258.7	
T.P.	4.61	263.58	11.91	251.97	
1+40.36 = S. ch. Washington		on ch.	5.23	258.35	
+40.36 = "		" Av.	5.57	258.01	
Inlet #1 on Grating			5.67	257.91	
" #1 " Flow line		Culvert #1 6" Iron Pipe.	8.62	254.96	
" #3 " Grating			5.96	257.62	
" #3 " Flow line		Box Culvert A	8.11	255.47	
" #4 " Grating			5.88	257.70	
" #4 " Flow line		of Box Culvert A	11.85	251.73	
" #4 " " "		2.5' Corr. Iron pipe outlet.	21.33	242.35	
" #2 " Grating			5.57	258.01	
" #2 " Flow line		Culvert #1	10.67	262.91	252.91 ??
" #2 " " "		16" outlet	10.8	262.78	252.78
T.P.	6.77	266.79	3.56	260.02	
ch. on Above B.M.			2.31	264.48 264.47 = B.M.	



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Location of Stucco Residence & Garage N E Cor of Campus Ave & Golden Gate Drive

1/8/16 Moore