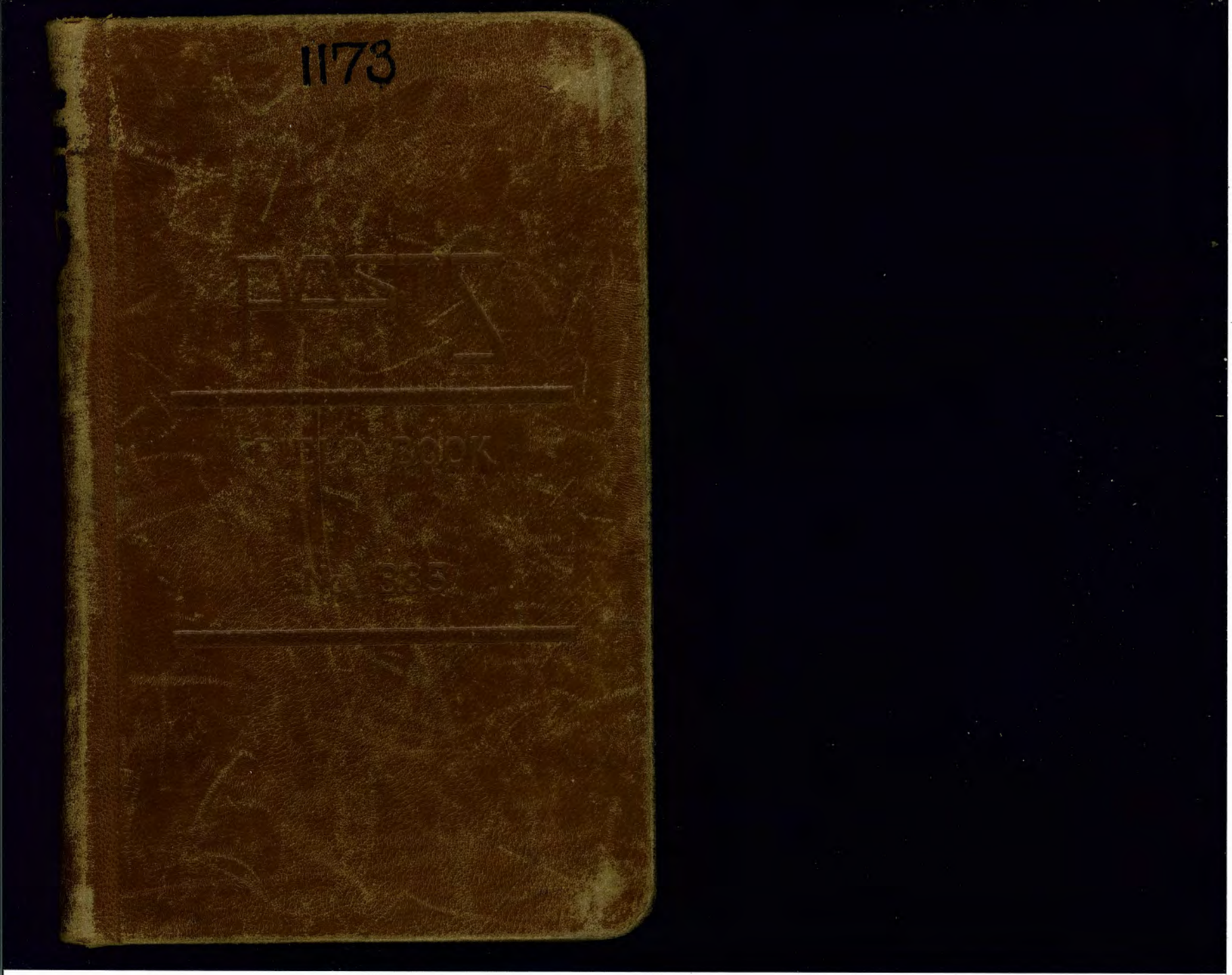
1173

Our Leather Bound Engineers Note Books are carried in the following rulings:

No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.

No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.

No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.

No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

CHICAGO, ILL.

92 FIFTH ST.
PORTLAND, ORE.

75 NEW MONTGOMERY ST.
SAN FRANCISCO, CAL.

AGENTS FOR

"BERGER" TRANSITS and LEVELS
"GURLEY" SURVEYING and HYDRAULIC INSTRUMENTS
"CHICAGO" STEEL TAPES, etc.

Cross Section of Narragansett Ave 80' wide 20' 10' 1/4S

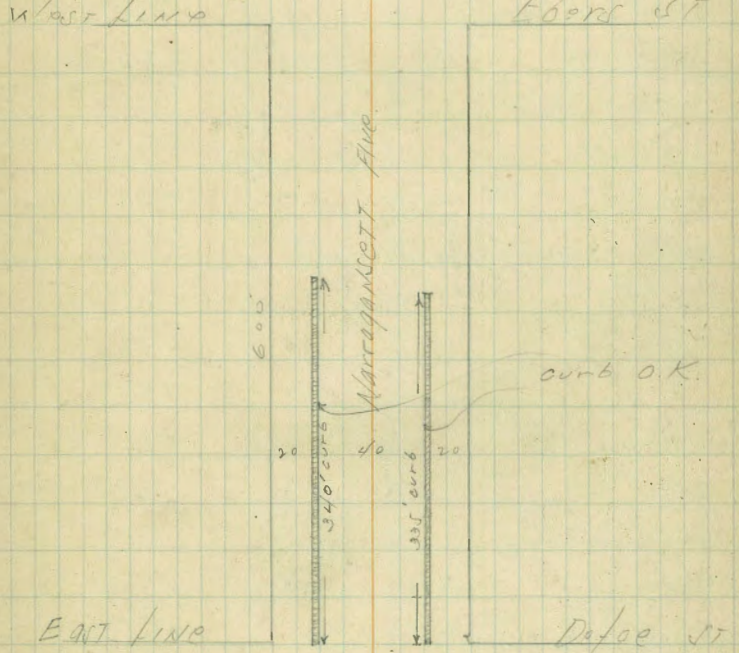
Defoe to Ebers St.

					Datum taken at Defoe
SEBP	12.97	50.07		37.05	
TP	8.07	48.10	10.5	39.48	
	150' E of EL Defoe = 00				
S			11.7	36.4	
cb top cem cb			12.07	36.08	
gut			12.7	35.4	
1/4			12.6	35.5	
c			12.8	35.3	
1/4			13.3	34.8	
gut			13.8	34.3	
cb top cem cb			13.10	35.00	
N			12.4	35.7	
	700' E Defoe				
N			10.7	37.4	
cb top cem cb			11.7	36.36	
gut			12.4	35.7	
1/4			12.0	36.1	
c			11.5	36.6	
1/4			11.3	36.8	
gut			11.6	36.5	
cb top cem cb			10.71	37.39	
S			10.0	36.1	
	250' E Defoe				
S			8.4	39.7	
cb top cem cb			9.39	38.71	

Yardage was not used. Street was graded & surf. with. D.G. in 1911.

Tolman Dec 15, 1926

Moore 12 1/15/26



Sidewalks have never been laid.

48.10

Sgut		10.1	38.0	
1/4		10.0	38.1	
C		10.3	37.8	
1/4		10.4	37.7	
gut		10.6	37.5	
cb	top cem cb	10.41	36.69	
~/		9.3	38.8	
	275' E Defoe			
~/		8.2	39.9	
+17		8.7	39.4	
cb	top cem cb = buried	9.7	38.36	
gut		9.5	38.6	
1/4		9.3	39.8	
C		9.3	39.8	
1/4		9.2	39.9	
gut		9.3	39.8	
cb	top cem cb	8.74	39.36	
+10		8.5	39.6	
S		7.2	40.9	
	300' E Defoe = Break in grade			
S		6.6	41.5	
+6		7.3	40.8	
cb	top cem cb	8.07	39.93	
gut		8.2	39.9	
1/4		8.1	40.0	
C		8.3	39.8	

48.10 Nonragansett

1/4		8.2	39.9
gut		8.3	39.8
cb	top cem cb	9.01	38.99
~/		8.3	39.8
	350' E of Defoe		
~/		J.4	42.7
cb	gone	J.7	42.4
1/4		J.6	42.5
C		J.1	43.0
1/4		J.2	42.9
cb	gone	J.7	42.4
+1		4.9	43.2
S		4.3	43.8
	397' E Defoe		
S		1.2	46.9
+17		1.3	46.8
cb		1.9	46.2
1/4		2.1	46.0
C		2.2	45.9
1/4		2.4	45.7
+9		3.3	44.8
cb		2.4	45.7
~/		3.3	44.8
	400' E Defoe		
~/		1.5	46.6
cb		2.0	46.1

		48.10					59.59	Narragansett T 3	
+1			3.0	45.1			500' E		
1/4			2.2	45.9		S		1.6	58.0
C			2.0	46.1		cb		2.4	57.2
1/4			1.9	46.2		1/4		2.8	56.8
cb			1.8	46.3		C		3.0	56.6
+4			1.1	47.0		+1		4.2	55.4
S			0.9	47.2		+5		4.2	55.4
T.P.	12.13	59.59	0.6	47.46		+6		3.3	56.3
	450' E of Defoe					1/4		3.1	56.5
S			8.7	50.9		cb		2.9	56.7
+18			9.1	50.5		N		2.6	57.0
cb			9.8	49.8		TP	4.68	63.46	0.81 58.78
1/4			9.7	49.9			585' E Defoe		
C			9.9	49.7		N		4.0	39.5
1/4			10.1	49.5		cb		4.3	59.2
cb			10.4	49.2		1/4		4.6	58.9
N			9.8	49.8		C		4.4	59.1
	500' E					+1		6.1	57.4
N			6.2	53.4		+3		6.2	57.3
cb			6.9	52.7		+7		4.2	59.3
1/4			6.9	52.7		1/4		4.0	59.5
C			6.7	52.9		cb		3.8	59.7
1/4			6.2	53.4		+10		2.8	60.7
cb			5.8	53.8		S		2.2	61.3
S			5.4	54.2			600' E = WL Ebers		
						S		1.8	61.7

6346 Narragansett

+10			2.4	61.1	
cb			3.3	60.2	
1/4			3.8	59.7	
+3			5.4	58.1	
+6			5.2	58.3	
+7			3.4	60.1	
C			3.2	60.3	
1/4			3.9	59.6	
+3			3.4	60.1	
cb			3.0	60.5	
+13			3.2	60.3	
N			4.2	59.3	
T.P.	3.2	5411	12.57	50.89	
T.P.	2.13	4948	6.76	47.35	
check to BM			17.42	37.06	37.05

Levels for ridge on Narr. Narragansett
curb. Defoe EAST 150'

	2.9	37.9	Top cb at 150' E of Defoe on N side 35.00
	EL Defoe		
1/4			6.2
+18			6.3
cb	top cb		6.9
	5' East		
cb	top cb		6.8
+2			5.2
N			4.7
	50' E		
N			4.6
+17			4.6
cb	top cb		5.5
	100' E		
cb	top cb		4.2
+3			3.3
N			3.7

See page 1 for Sta. 1+50

Cross Section of Street Intersections to the Moore
New paving on Univ. Ave Extention 12/27/26

Top of curb Nw cor. Univ. Ave

18th St North side of Univ. Ave			
	5.10	350-15	345.05
N.L. Univ.			350.1
w/ gut. on paving		5.8	344.3
N 1/4 " "		5.5	344.6
C " "		5.3	344.8
E 1/4		5.2	344.9
E gut		5.1	345.0
1'N			
E cb natural grd.		2.1	348.0
1/4		5.1	345.0
C		5.3	344.8
1/4		5.4	344.7
+4		4.5	345.6
W cb		2.2	347.9
20' N = Natural grd			
W cb		2.2	347.9
W 1/4		2.5	347.6
C		2.5	347.6
E 1/4		2.6	347.5
E. cb		1.4	348.7

Estrella at S.L. Univ. 17th e. 5

Top cb Sw cor Estrella & Univ

330	330.30	326.50
S L Univ 17th e		330.3
w/ gut. on paving	5.2	325.1
W 1/4 " "	5.3	325.0
C " "	5.4	324.9
E 1/4 " "	5.8	324.5
E gut. " "	6.3	324.0
" " +05	5.4	324.9
E.L. Natural grd.	3.1	327.2
30' S. on Natural grd		
E.L.	2.2	328.1
cb	2.2	328.1
1/4	2.3	328.0
C	2.3	328.0
1/4	2.2	328.1
W gut	1.2	329.1

Moore

Estrella at NL Univ Ave

	4.10	333.60		3x9.50 Tob c6 NW Estrella x Univ
	NL Univ			333.6
WL			3.8	329.8
w/ gut	on paving		3.4	328.4
1/4	"	"	3.3	328.3
c	"	"	3.5	328.1
1/4	"	"	3.9	327.8
E gut	"	"	6.4	327.2
E			6.1	327.5
	1' N			
E	Natural grd		2.7	330.9
+5	"	"	2.9	330.7
+6	"	"	3.1	328.5
c6	Ecol.		3.8	327.8
1/4	"		3.7	327.9
c	"		3.4	328.2
1/4	"		3.3	328.3
w/c6	"		3.0	328.6
+6	Natural grd		3.8	329.8
	30' N =	Natural grd		
WL +6			3.4	330.2
c6			3.7	329.9
1/4			4.5	329.1
c			4.4	329.2
1/4			4.5	329.1
c6			4.8	328.8
EL			3.4	330.2

Light = Vine Court SL Univ Ave

6

	8.80	3x7.30	318.50 Tob c6 Vine Court
	SL Univ.		327.3
w/ gut	on paving	9.4	317.9
1/4	" "	8.5	318.8
c	" "	8.1	319.2
1/4	" "	8.0	319.3
E gut	" "	8.1	319.2
	2' S		
E c6	= Natural grd	1.4	325.9
+2		6.7	320.6
1/4		7.2	320.1
c		7.3	320.0
1/4		8.0	319.3
+4		8.0	319.3
+5	Natural grd	4.0	323.3
w/c6		4.0	323.3
	3' S =	Natural grd	
w/c6		2.0	325.3
1/4		2.3	325.0
c		2.6	324.9
1/4		2.4	324.9
E c6		1.0	326.3

Light at NL Univ.

No EXCAVATION

Approx. 20 cu. yds necessary for approach

Winona at St Univ Five

				Totals Set for
	335.10	335.10	3330	
St Univ			338.2	
E gut		6.10	331.0	
1/4		6.4	331.8	
c		6.6	331.6	
1/4		7.10	331.0	
W gut		7.9	330.3	
2'S				
W c6	Natural grd	0.2	337.5	
+S		6.5	331.7	
1/4		7.0	331.2	
c		6.8	331.4	
1/4		6.6	331.6	
+S		6.6	331.6	
+S	Not grd	1.4	336.8	
c6	" "	1.0	337.2	
4'	S = Natural grd			
E c6		1.10	337.0	
1/4		1.10	337.0	
c		1.10	337.0	
1/4		1.3	336.9	
W c6		0.7	337.5	

Winona at NE Univ. Five 7

			Totals Set for Winter
6.10	334.10	335.0	
NE Univ		334.1	
W gut		6.7	327.4
1/4		6.6	328.1
c		10.4	328.7
1/4		10.3	328.8
E gut		10.2	328.9
2'N			
E C6	Natural grd	1.0	333.1
+1	" "	1.2	332.9
+3		3.6	330.5
1/4		4.6	329.5
c		4.8	329.3
1/4		4.9	329.2
+6		4.4	329.7
W c6	Natural grd	1.3	332.8
25'N = Natural grd			
W c6		1.8	332.3
1/4		2.4	331.7
c		2.1	332.0
1/4		2.1	332.0
E C6		1.7	332.7

50th ST at NL Univ Ave

approx. 90 cu yds EXCAVATION for approach

52nd ST on SL Univ Ave
320 cu. yds EXCAVATION

Shiloh Road on SL Univ Ave
15 cu. yds EXCAVATION

80' w. d.e
23' cls
8.5 1/4 S

Jackdaw ST X Sec
Walnut to Brookes

1-18-27

BM.	4.44	251.98		247.50	Jackdaw N.W. & Brooks
		00 = S. Line Brookes			
W			3.7	248.3	
cl			4.0	248.0	
1/4			4.1	247.9	
c			4.2	247.8	
1/4			4.1	247.9	
cl			4.4	247.6	
E			4.2	247.8	
		4' S			
E			3.3	248.7	
+5			4.3	247.7	
cl			4.2	247.8	
1/4			4.0	248.0	
c			4.1	247.9	
1/4			4.0	248.0	
cl			3.8	248.2	
+13			3.6	248.4	
W			3.1	248.9	
		45' S			
W			2.5	249.5	
+4			3.4	248.6	
cl			3.0	249.0	
1/4			3.0	249.0	
c			3.0	249.0	
1/4			2.4	249.6	

PLOTTED

251.98

cl		3.0	249.0
+10		3.1	248.9
+18		2.4	249.6
E		1.2	250.8
	75' S		
E		0.8	251.2
+5		2.2	249.8
+13		2.6	249.4
cl		2.8	249.2
1/4		2.5	249.5
c		2.8	249.2
1/4		3.1	248.9
cl		3.4	248.6
W		4.1	247.9
	100' S		
W		4.5	247.5
cl		3.8	248.2
1/4		3.3	248.7
c		3.2	248.8
1/4		3.0	249.0
cl		3.2	248.8
+13		2.7	249.3
E		1.2	250.8

		251.98		
		128' S.		
E			1.5	250.5
+7			3.1	248.9
cl			3.8	248.2
1/4			3.3	248.7
E			3.9	248.1
1/4			4.1	247.9
cl			4.3	247.7
W			5.1	246.9
		165' S		
W			6.9	245.1
cl			6.0	246.0
1/4			5.8	246.2
E			5.3	246.7
1/4			4.7	247.3
cl			4.7	247.3
+13			4.4	247.5
			3.0	249.0
		200' S		
E			6.6	246.0
+6			6.8	245.2
cl			7.1	244.9
1/4			7.1	244.9
E			7.1	244.9
1/4			7.3	244.7
cl			7.7	244.3
+20			8.1	243.9
W			9.4	242.6

	251.98		
	225' S		
W		10.1	241.9
+13		11.0	241.0
cl		9.9	242.1
1/4		9.5	242.6
E		9.1	242.9
1/4		8.7	243.3
cl		9.1	242.9
+16		9.3	242.7
E		8.7	243.3
	228' S		
E		9.0	243.0
+7		9.5	242.5
cl		9.3	242.7
1/4		9.0	243.0
E		9.4	242.6
1/4		9.9	242.1
cl		10.3	241.7
+10		11.1	240.9
W		12.0	240.0
	240' S		
W		12.4	239.6
+13		11.9	240.1
cl		11.5	240.5
1/4		11.1	240.9
E		10.8	241.2
1/4		10.5	241.5

		251.98		
		240'S (EOH)		
eb			10.2	241.8
E			9.7	242.3
T.P.	0.74	240.18	12.54	239.44
		270'S.		
E			1.8	239.4
eb			2.6	237.6
1/4			2.8	237.4
C			3.2	237.0
1/4			3.5	236.7
eb			3.7	236.5
+10			4.1	236.1
W			4.9	235.3
		285'S.		
W			6.9	233.3
+13			4.2	234.0
eb			4.2	234.0
1/4			6.0	232.2
C			5.4	234.8
1/4			4.9	235.3
eb			4.7	235.5
+10			4.4	235.8
E			3.4	236.8

240.18 Jackdaw 11

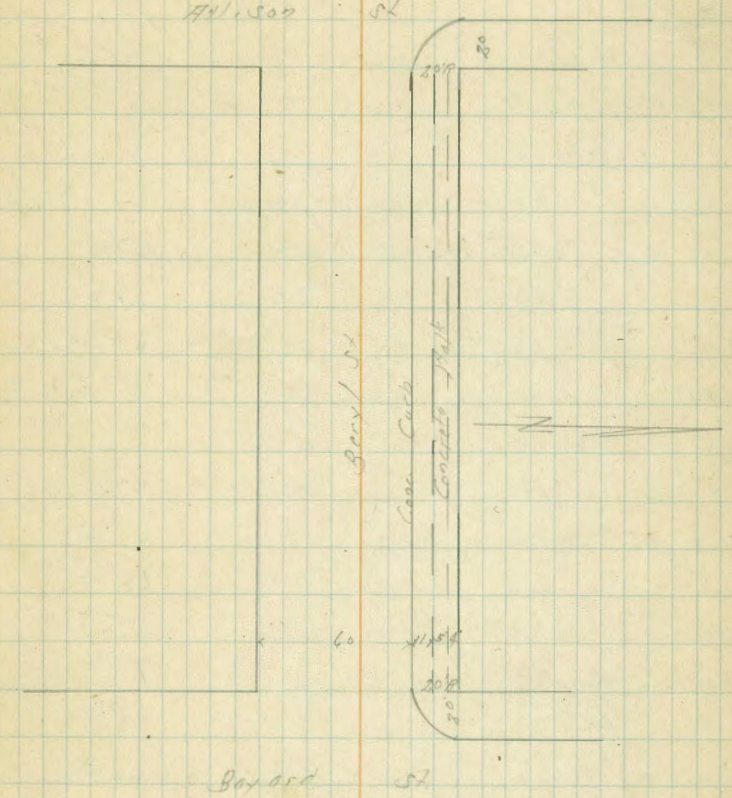
300'S-N. Line Walnut

E	6.0	234.2
+16	7.5	232.7
eb	8.1	232.1
1/4	8.7	231.5
C	8.5	231.7
1/4	8.2	232.0
eb	8.0	232.2
W	7.6	232.6
	310'S.	
W	10.4	229.8
eb	10.1	230.1
1/4	10.7	229.5
C	11.7	228.5
1/4	11.8	228.4
eb	10.7	229.5
+10	9.5	230.7
E	7.6	232.6

Cross Section Beryl St.
Bayard to Allison

80' Wide
20 Cbs
10 QLs

BM	1.10	90.12 ✓		88.02	NE Mon SP Lavina & Bayard
TP	0.63	78.60 ✓	12.15	77.97 ✓	
TP	1.61	68.24 ✓	11.47	67.13 ✓	NW Cor Beryl & Bayard NEad Reland
		W/L Bayard			
N			0.6	68.1	
+3	PLOTTED		1.6	67.1	
+12			1.5	67.2	
+18			1.5	67.2	
Cb	Top & Gutter		1.85	66.89	
¼			0.9	67.8	
½			0.4	68.3	
¼			1.9	66.8	
Cb			2.4	66.3	
+6			2.5	66.2	
+8			3.1	65.6	
+17			2.6	66.1	
S			2.8	65.9	
		50' W of NW/L Bayard			
S			2.9	65.8	
+3			3.3	65.4	
+7			3.4	65.3	
+9			2.7	66.0	
+18			2.5	66.2	
Cb			3.2	65.5	
+4			2.5	66.2	



Beryl St.

68.74

¼		2.0	66.7
E		1.6	67.1
¼		1.2	67.5
+6		1.6	67.1
Cb	Top of Ground	2.99	66.2
+2		1.6	67.1
+8		1.4	67.3
+11		2.3	66.4
+16		2.1	66.6
N		1.1	67.6
	100' W		
N		0.9	67.8
+2		1.8	66.9
+4		2.7	66.0
+9		3.0	65.7
+14		2.0	66.7
+18		2.1	66.6
Cb		2.7	66.0
Top Conc.		3.16	65.58
¼		1.4	67.3
E		1.8	66.9
¼		2.3	66.4
Cb		3.1	65.6
+2		2.7	66.0
+7		3.9	65.8
+13		3.6	65.1

68.74

S		3.3	65.5
	150' W		
S		3.2	65.5
+3		3.7	65.0
+8		3.8	64.9
+10		3.6	65.1
+11		3.2	65.5
+18		3.0	65.7
Cb		4.2	64.5
+8		2.5	66.2
¼		2.5	66.2
E		2.0	66.7
¼		1.8	66.9
+5		2.2	66.5
Cb		3.1	65.6
Top Conc		3.75	65.0
+2		2.1	66.6
+7		2.1	66.6
+10		3.5	65.2
+17		3.4	65.3
+18		2.1	66.6
N		1.9	66.8
	200' W		
N		2.3	66.4
+3		3.2	65.5
+4		4.0	64.7

Beryl St.

68.74

+10		12	64.5
+14		3.6	65.1
+19		3.4	65.3
cb	+Ground	4.20	64.5
+8		3.0	65.7
¼		3.0	65.7
+5		2.6	66.1
℄		2.7	66.0
¼		3.3	65.4
+9		4.0	64.7
cb		4.7	64.0
+2		3.9	64.8
+8		4.0	64.7
+10		4.7	64.0
+17		4.8	63.9
S.		4.1	64.6
	7.50'W		
S		5.3	63.4
+3		5.9	62.8
+6		5.8	62.9
+10		5.2	63.5
+18		5.1	63.6
cb		5.7	62.8
+2		5.3	63.4
+7		4.8	63.9
¼		4.9	63.8

14

68.74

℄		4.2	64.5
¼		4.0	64.7
Gutter		5.1	63.6
cb Top		4.90	63.8
+16		4.7	64.0
N		4.2	64.5
	3.00' W		
N		5.0	63.7
cb Top		5.70	63.0
Gutter		6.1	62.6
¼		5.0	63.7
℄		5.0	63.7
¼		5.7	63.0
+7		6.3	62.4
cb		6.6	62.1
+2		6.0	62.7
+8		6.0	62.7
+11		6.6	62.1
+17		4.8	61.9
S.		6.4	62.3
	3.50'W		
S		7.4	61.3
+3		8.0	60.7
+8		7.9	60.8
+13		7.0	61.7
+18		7.0	61.7

Beryl St.

1874

Cb		75	61.2
¼		68	61.9
½		60	62.7
¼		60	62.7
+8		66	62.1
Gutter		66	62.1
Cb Top		611	62.6
+8		66	62.1
+10		64	62.3
+11		60	62.7
+16		63	62.4
N		61	62.6
	400'N		
N		72	61.5
+4		66	62.1
+8		66	62.1
+11		75	61.2
+17		75	61.2
Cb		682	61.9
Gutter		73	61.4
¼		69	61.8
½		72	61.5
¼		79	60.8
Cb		86	60.1
+3		81	60.6
+10		82	60.5

1874

+12		87	60.0
+18		87	60.0
S		87	60.0
	456'N		
S		92	59.5
+5		87	60.0
+10		92	59.5
Cb		95	59.2
¼		89	59.8
½		85	60.2
¾		82	60.5
Gutter		84	60.3
Cbs Top		744	61.3
+2		82	60.5
+6		80	60.7
+11		72	61.5
+16		72	61.5
N		80	60.7
	500'N = E.L. Allison		
N		84	60.3
+4		78	60.9
+9		78	60.9
+14		83	60.4
+18		85	60.2
Cb Top		800	60.7
Gutter		87	60.0

15

Beryl St.

		68.7 ℄		
¼			8.7	60.0
8			9.0	59.7
¼			9.4	59.3
ob			9.7	59.0
+3			9.6	59.1
+10			9.6	59.1
+15			9.4	59.3
S			10.0	58.7
TP	9.13	62.57 ✓	10.60	58.14

Cross Section Lamont
Bayard to Allison

80' wide
20' CBs
10' Qds

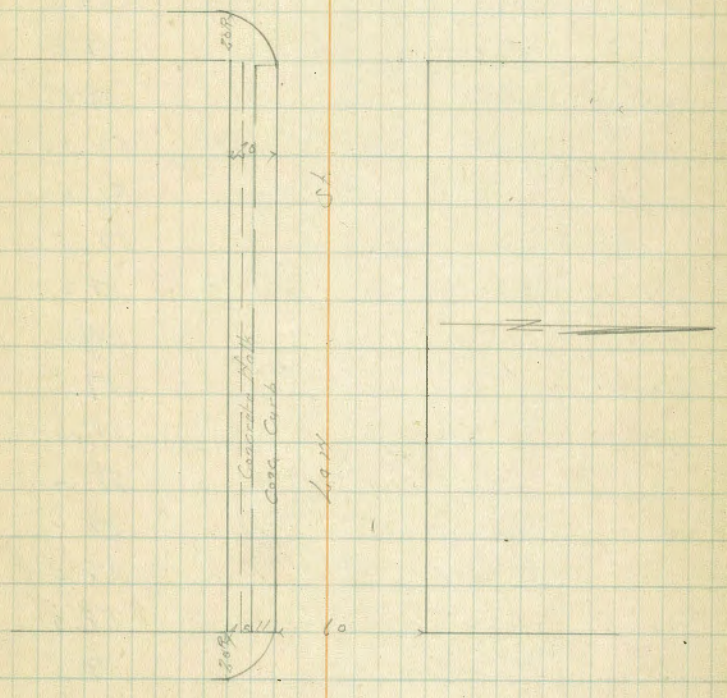
62.57 Bl Ford

W.L. Bayard

S		4.0	58.6
Cb	Top rGround	4.40	58.2
¼		3.2	59.4
½		3.4	59.2
¼		3.3	59.3
+7		3.4	58.7
+8		4.0	58.6
Cb		3.8	58.8
+3		3.3	59.3
N		3.9	59.7
	50' N of W.L. Bayard		
N		3.3	59.3
+12		3.4	59.2
+17		3.7	58.9
+18		4.3	58.3
Cb		4.4	58.2
+3		3.7	58.9
¼		3.6	59.0
½		3.4	59.2
¼		3.9	58.7
+5		4.2	58.4
+8		4.8	57.8
Gutter		5.2	57.4
Cb	Top	4.91	57.66

PLOTTED

17
S. Allison
Bl. 55
Sanborn



Low St. 62.57

+3	4.2	58.3
+8	4.5	58.1
S	4.5	58.1
100' W		
S	5.0	57.6
+9	5.3	57.3
+12	4.8	57.8
+17	4.6	58.0
CL Top	5.42	57.15
Gutter	5.7	56.9
+2	5.1	57.5
¼	4.0	57.6
℄	3.6	59.0
¼	3.5	59.1
+7	3.7	58.6
+8	4.4	58.2
CL	4.4	57.2
+2	4.2	57.4
+2	3.7	58.9
N	3.2	59.4
150' W		
N	2.8	59.8
+9	3.2	59.4
+12	4.1	58.5
+16	3.1	59.0
+17	4.1	58.5

62.57

CL	4.2	58.4
+2	4.2	58.4
+3	3.5	59.1
¼	3.2	59.4
℄	3.4	59.2
¼	3.9	58.7
+8	5.2	57.4
CL Top & Ground	5.89	56.68
+3	4.7	57.9
+9	5.0	57.6
+10	5.7	56.9
+17	5.7	56.9
S	4.9	57.8
200' W		
S	5.3	57.3
+3	6.1	56.5
+9	6.1	56.5
+10	5.7	56.9
+12	5.3	57.3
+18	5.1	57.5
CL Top & Ground	6.30	56.3
+2	5.7	56.9
¼	4.5	58.1
℄	4.1	58.5
¼	3.8	58.8
+9	3.8	58.8

Low St

(2.57)

+8		4.3	58.3
Cb		4.4	58.2
+2		4.4	58.2
+3		3.8	58.8
+7		4.1	58.0
+11		3.4	59.2
N		2.7	59.9
	350' N		
N		3.9	59.2
+8		3.1	59.0
+11		5.0	57.6
+16		4.3	58.3
+17		5.0	57.6
Cb		5.1	57.5
+2		5.1	57.5
+3		4.4	58.2
1/4		4.3	58.3
S		4.4	58.2
1/4		4.8	57.8
+9		6.0	56.6
Gutter		6.9	55.7
Cb Top		6.78	55.79
+3		5.4	57.2
+10		5.8	56.8
+12		6.6	56.0
+17		6.6	56.0

(2.57)

S		5.9	56.7
	300' N		
S		6.4	56.2
+3		7.0	55.6
+9		7.0	55.6
+11		6.0	56.6
+18		6.3	56.3
Cb Top		7.21	55.36
Gutter		7.4	55.2
+2		6.4	56.2
1/2		5.4	57.2
S		4.8	57.8
1/2		4.8	57.8
+7		4.8	57.8
+8		5.9	56.7
Cb		5.8	56.8
+2		5.5	57.1
+3		4.7	57.9
+12		4.5	58.1
N		4.5	58.1
	350' N		
N		5.1	57.5
+8		5.5	57.1
+9		6.2	56.4
+12		6.2	56.4
+17		5.5	57.1

Line 57

6.7.57

Cb	64	56.7
+3	65	56.1
+4	56	57.0
1/4	55	57.1
2	54	57.7
1/4	57	56.9
+8	66	56.0
Cb + Gu Hor	7.69	54.86
+2	60	56.6
+6	63	56.3
+11	75	55.1
+17	74	55.2
5	62	56.4
400' W		
5	69	55.7
+4	79	54.7
+11	80	54.6
+13	77	55.4
+19	72	55.4
Cb Top	8.16	54.41
Gu Hor	81	54.0
+2	80	54.6
1/4	70	55.6
2	65	56.1
1/4	64	56.7
+7	64	56.7

6.7.57

+8	70	55.6
Cb	72	55.4
+2	71	55.5
+3	63	56.3
+10	71	55.5
+11	79	54.7
+13	60	56.6
N	61	56.5
450' N		
N	72	55.4
+6	73	55.3
+7	78	54.8
+12	78	54.8
+18	78	54.8
Cb	83	54.3
2	83	54.3
+3	75	55.1
1/4	74	55.0
2	78	54.8
1/4	82	54.4
+7	85	54.1
Gu Hor	91	53.5
Cb Top	8.57	54.0
+2	82	54.4
+16	84	54.2
+18	87	53.9

Low St

62.57

S		8.3	54.3
	500'N = EL Hibson		
S		9.9	52.7
+4		8.8	53.8
+10		8.8	53.8
+12		9.3	53.3
Cb Top		8.85	53.62
Gutter		9.6	53.0
+4		9.0	53.6
℄		8.1	54.0
+6		8.1	54.0
+9		8.7	53.6
Cb		9.1	53.5
+2		8.5	54.1
N		8.5	54.1

Levels on Dirt Curb Returns
29th & Franklin Ave

Woolman + 29th				
N.E. B.P.	2.25	99.70		97.45
	100' S S.L. Franklin			
E on Dirt			5.8	93.9
W " "			5.0	94.7
	50' S S.L. Franklin			
W " "			7.4	92.3
E " "			9.0	90.7
	S.L. Franklin			
E " "			11.5	87.8
W " "			9.8	89.9
T.P. " "	7.75	94.56	12.89	86.81
	N.L. Franklin			
W " "			7.7	86.9
E " "			9.6	85.0
	50' N			94.6
E			10.7	83.9
W			9.0	85.6
	100' N			
W			10.6	84.0
E			11.9	87.7
	Levels on Franklin			
	100' E. E.L. 29th			
N			8.9	85.7
S			6.2	88.4
	50' E. E.L.			
S			6.3	88.3

94.56

				94.6
N			8.9	85.7
	E.L. 29th			
N			8.9	85.7
S			6.0	88.0
	W.L. 29th			
S			5.2	89.4
N			7.9	86.7
	50' W. W.L.			
N			6.3	88.3
S			3.7	90.9
	100' W W.L.			
S			7.4	92.2
N			5.4	89.2
T.P.	9.91	107.70	2.27	92.28
			9.78	97.42
				97.45 - Bm.
				+0.03

22

X Section Boundary St 50 wide 10 cb 7.5 1/4 5

From N.L. Redwood to S.L. Myrtle on West.

(W.L. Stations to S.L. Thorn on E.)

NW. BP					
Thorn & Gregory	0.45	318.46		315.01	
T.P.	2.26	307.86	12.8 V	305.64	
T.P.	1.37	296.7 V	10.5 I	V 295.35	
	N.L. Redwood Section Parallel With N.L.				
W			3.3	293.4	L
cb.			4.9	291.8	L
1/4	Plotted - J.H.		5.3	291.4	L
E	3-12-27		5.6	291.1	L
1/4			5.6	291.1	L
cb.			5.8	290.9	L
+3			5.8	290.9	L
+5			4.9	291.8	L
E			5.5	291.1	L
+15			12.8	283.9	L
	N.L. Redwood Section at Rt. Angles to N.W.P.L.				
-15			12.2	284.5	L
E			9.2	287.5	L
cb.			7.1	289.6	L
1/4			6.4	290.3	L
E			5.9	290.8	L
1/4			5.5	291.2	L
cb.			4.9	291.8	L
W			3.4	293.3	L
		50' N			
W			2.1	294.6	L

296.7 V

+5	4.5	292.2	L
cb.	5.0	291.7	L
+5	6.0	290.7	L
1/4	6.0	290.7	L
E	6.4	290.3	L
1/4	6.6	290.1	L
cb.	8.2	288.5	L
E	10.1	286.6	L
+15	12.8	283.9	L
	100' N		
-15	12.0	284.7	L
E	10.1	286.6	L
cb.	8.6	288.1	L
1/4	7.3	289.4	L
E	6.9	289.8	L
+4	6.5	290.2	L
1/4	5.9	290.8	L
cb.	4.6	292.1	L
+5	3.6	293.1	L
W	1.1	295.6	L
	125' N		
W	1.9	294.8	L
cb.	5.2	291.5	L
+6	5.9	290.8	L
1/4	6.4	290.3	L
E	7.2	289.5	L

E96.72

¼		7.6	289.1	⌐
cb.		8.7	288.0	⌐
E		10.3	286.4	⌐
+15		13.6	283.1	⌐
	150' N			
-15		13.9	282.8	⌐
E		11.0	285.7	⌐
cb.		9.0	287.7	⌐
+3		7.9	288.8	⌐
¼		7.6	289.1	⌐
E		7.5	289.2	⌐
¼		6.8	289.9	⌐
+3		5.3	291.4	⌐
cb.		5.0	291.7	⌐
W		2.7	294.0	⌐
	200' N			
W		1.4	295.3	⌐
+8		4.7	292.0	⌐
cb.		4.7	292.0	⌐
+5		5.5	291.2	⌐
¼		6.8	289.9	⌐
E		7.3	289.4	⌐
¼		7.6	289.1	⌐
+5		7.7	289.0	⌐
cb.		9.2	287.5	⌐
E		11.6	285.1	⌐

E96.72

+25		E35'	273.2	⌐
	E50' N			
-25		30.0	276.7	⌐
E		13.0	283.7	⌐
cb.		9.2	287.5	⌐
+3		7.7	289.0	⌐
¼		7.2	289.5	⌐
E		7.1	289.6	⌐
+3		6.6	290.1	⌐
¼		5.0	291.7	⌐
cb.		4.8	291.9	⌐
+3		4.8	291.9	⌐
W		1.7	295.0	⌐
	300' N			
W		1.3	295.4	⌐
+6		3.6	293.1	⌐
+8		4.7	292.0	⌐
cb		4.7	292.0	⌐
+4		5.2	291.5	⌐
¼		6.4	290.3	⌐
E		7.3	289.4	⌐
¼		7.3	289.4	⌐
+2		7.6	289.1	⌐
cb		9.5	287.2	⌐
E		12.4	284.3	⌐
+25		19.5	277.2	⌐

E96.72

330' N

-25		21.8	274.9	↵
E		13.2	283.5	↵
cb.		9.2	287.5	↵
+3		7.7	289.0	↵
¼		7.2	289.5	↵
℄		7.1	289.6	↵
¼		6.5	290.2	↵
+3		4.9	290.8	↵
cb.		4.4	292.3	↵
+3		4.4	292.3	↵
+5		3.0	293.7	↵
W		1.0	295.7	↵

355' N

W		1.8	294.9	↵
+5		3.0	293.7	↵
+7		4.7	292.0	↵
cb.		4.7	292.0	↵
+5		5.1	291.6	↵
¼		7.9	288.8	↵
℄		8.5	288.2	↵
¼		8.7	288.0	↵
+3		9.1	287.6	↵
cb.		12.1	284.6	↵
E		15.5	281.2	↵
+25		26.0	270.7	↵

E96.72

+27			330	263.7 ↵
TP	7.96	293.14	11.54	285.18

400' N

-25			26.0	267.1 ↵
E			19.7	273.4 ↵
cb.			13.0	280.1 ↵
¼			8.3	284.8 ↵
℄			7.6	285.5 ↵
+6			7.3	285.8 ↵
¼			5.3	287.8 ↵
+3			3.8	289.3 ↵
cb.			3.8	289.3 ↵
+4			3.5	289.6 ↵
W			0.3	292.8 ↵

425' N

W			0.1	293.0 ↵
+5			2.1	291.0 ↵
+6			3.7	289.4 ↵
cb			3.7	289.4 ↵
+5			5.2	287.9 ↵
¼			6.5	286.6 ↵
+3			7.8	285.3 ↵
℄			8.1	285.0 ↵
¼			8.4	284.7 ↵
cb.			12.2	280.9 ↵
E			17.3	275.8 ↵

+8		20.9	272.2	✓	
+25		24.4	268.7	✓	
	460' N				
-25		19.7	273.4	✓	
E		13.8	279.3	✓	
cb.		10.0	283.1	✓	
¼		8.6	284.5	✓	
S		8.4	284.7	✓	
+3		8.1	284.7	✓	
¼		6.4	286.7	✓	
+3		5.4	287.7	✓	
cb.		5.0	288.1	✓	
W		0.7	292.4	✓	
	500' N				
W		0.2	292.9	✓	
cb.		6.1	287.0	✓	
+5		7.0	286.1	✓	
¼		7.9	285.2	✓	
+3		8.8	284.3	✓	
S		9.2	283.9	✓	
¼		9.4	283.7	✓	
cb.		10.5	282.6	✓	
E		12.5	280.8	✓	
+15		14.6	278.5	✓	
+25		19.4	273.7	✓	
	550' N				

-25		19.2	273.9	✓	
-10		15.2	277.9	✓	
E		14.3	278.8	✓	
cb.		11.5	281.6	✓	
¼		10.0	283.1	✓	
S		9.5	283.6	✓	
¼		8.6	284.5	✓	
cb.		7.3	285.8	✓	
W		3.2	289.9	✓	
	600' N				
W		4.8	288.3	✓	
+5		8.4	284.7	✓	
cb.		9.0	284.1	✓	
¼		9.6	283.5	✓	
S		12.1	281.0	✓	
¼		12.1	281.0	✓	
cb.		13.0	280.1	✓	
E		15.7	277.4	✓	
+14		19.3	273.8	✓	
+20		21.2	271.9	✓	
	610' N				
-20		21.1	272.0	✓	
E		20.5	272.6	✓	
+4		19.5	273.6	✓	
cb.		16.0	277.1	✓	
¼		13.0	280.1	✓	

		293.14			
℄			13.0	280.1	⌐
¼			11.2	281.9	⌐
+3			10.2	282.9	⌐
cb.			9.9	283.2	⌐
+6			9.5	283.6	⌐
W			6.6	286.5	⌐
T.P.	6.08	286.37	12.85	280.29	
		460' N			
W			3.5	282.9	⌐
cb.			6.1	280.3	⌐
¼			7.9	278.5	⌐
℄			8.4	278.0	⌐
¼			8.4	278.0	⌐
+5			10.1	276.3	⌐
cb.			12.7	273.7	⌐
E			12.1	274.3	⌐
+7			10.8	275.6	⌐
+15			9.0	277.4	⌐
		700' N			
-15			8.7	277.7	⌐
-10			10.7	275.7	⌐
-9			11.7	274.7	⌐
E			11.3	275.1	⌐
+4			11.4	275.0	⌐
+5			10.1	276.3	⌐
cb.			9.1	277.3	⌐

		286.37			
¼			8.2	278.2	⌐
℄			7.9	278.5	⌐
¼			7.4	279.0	⌐
cb.			5.5	280.9	⌐
+5			3.8	282.6	⌐
W			1.5	284.9	⌐
		725' N			
W			2.3	284.1	⌐
cb.			4.6	281.8	⌐
¼			6.5	279.9	⌐
℄			7.4	279.0	⌐
¼			7.9	278.5	⌐
cb.			9.0	277.4	⌐
E			10.7	275.7	⌐
+7			10.3	276.1	⌐
+8			9.2	277.2	⌐
+15			7.4	279.0	⌐
		742' N			
-15			6.1	280.3	⌐
-1			8.3	278.1	⌐
E			10.1	276.3	⌐
cb.			10.0	276.4	⌐
+1			8.4	278.0	⌐
¼			7.6	278.8	⌐
℄			7.0	279.4	⌐
¼			6.5	279.9	⌐

cb.			5.4	281.0	⌐
+6			3.7	282.7	⌐
W			1.9	284.5	⌐
		7+44			
W			1.9	284.5	⌐
+4			3.7	282.7	⌐
cb.			5.4	281.0	⌐
¼			6.5	279.9	⌐
E			7.0	279.4	⌐
¼			7.9	278.5	⌐
+6			8.7	277.7	⌐
cb.			9.9	276.5	⌐
+9			9.9	276.5	⌐
E			8.6	277.8	⌐
+15			5.4	281.0	⌐
		7+55			
-15			3.1	283.3	⌐
E			6.9	279.5	⌐
+4			7.8	278.6	⌐
+5			9.4	277.0	⌐
cb.			9.3	277.1	⌐
+3			9.3	277.1	⌐
+4			8.1	278.3	⌐
¼			8.0	278.4	⌐
E			7.0	279.4	⌐
¼			6.0	280.4	⌐

cb.			5.1	281.3	⌐
+6			3.8	282.6	⌐
W			1.8	284.6	⌐
		750'N			
W			4.5	281.9	⌐
cb.			5.6	280.8	⌐
¼			5.0	281.4	⌐
E			4.8	281.6	⌐
+6			6.4	280.0	⌐
¼			8.8	277.6	⌐
+4			9.3	277.1	⌐
cb.			7.5	278.9	⌐
+3			4.8	281.6	⌐
E			3.0	283.4	⌐
+5			2.1	284.3	⌐
		800'N			
-5			0.4	286.0	⌐
E			1.5	284.9	⌐
+5			2.9	283.5	⌐
cb.			5.3	281.1	⌐
+5			6.2	280.2	⌐
¼			7.6	278.8	⌐
E			8.0	278.4	⌐
+6			7.8	278.6	⌐
¼			4.7	281.7	⌐
cb.			4.8	281.6	⌐

286.37

W			5.0	281.4	⌐
+15			1.7	284.7	⌐
818.7 N = S.L. McKinley on W					
-15			3.1	283.3	⌐
W			4.3	282.1	⌐
+5			4.7	281.7	⌐
+7			6.3	280.1	⌐
cb.			6.3	280.1	⌐
¼			6.5	279.9	⌐
+3			6.7	279.7	⌐
+4			5.2	281.2	⌐
℄			4.9	281.5	⌐
+5			3.9	282.5	⌐
¼			2.3	284.1	⌐
cb.			1.5	284.9	⌐
+5			1.2	285.2	⌐
E			+1.2	285.2	⌐
+5			+3.2	283.2	⌐
T.P.	12.09	297.35	1.21	285.14	
		828 N			
-5			6.8	290.6	⌐
E			8.2	289.2	⌐
cb.			10.2	287.2	⌐
¼			10.8	286.6	⌐
+1			12.4	285.0	⌐
℄			16.0	281.4	⌐

297.35

+5		14.7	282.7	⌐
¼		16.3	281.1	⌐
cb.		16.7	280.7	⌐
+3		16.7	280.7	⌐
+5		14.9	282.5	⌐
W		14.4	283.0	⌐
+15		9.3	288.1	⌐
840.8 = S.L. Thornston E		10 cbs. 12.5 ¼s		
-10		4.4	292.0	
W		10.7	286.7	⌐
+6		15.9	281.5	⌐
cb.		16.3	281.1	⌐
¼		15.5	281.9	⌐
℄		12.8	284.6	⌐
+2		14.1	283.3	⌐
+5		14.1	283.3	⌐
+6		9.7	287.7	⌐
¼		9.7	287.7	⌐
cb.		8.8	288.6	⌐
E		7.0	290.4	⌐
+5		5.4	292.0	⌐
S.L. THORNE on E +8'				
E		5.0	292.4	⌐
cb.		6.7	290.7	⌐
℄		9.7	287.7	⌐
+1		12.5	284.9	⌐

297.35

E		12.4	285.0	L
+5		13.2	284.2	L
+6		14.8	282.6	L
¼		15.4	282.0	L
cb.		15.3	282.1	L
+5		15.3	282.1	L
+8		5.0	292.4	L
W		5.0	292.4	L
	5 cb.			
W		5.0	292.4	L
+2		5.0	292.4	L
+5		14.8	282.6	L
cb.		14.8	282.6	L
¼		10.9	283.5	L
E		5.7	291.7	L
¼		5.5	291.9	L
cb.		4.9	292.5	L
E		4.9	292.5	L
	+10'			
E		4.7	292.7	L
cb.		5.0	292.4	L
¼		5.3	292.1	L
E		5.1	292.0	L
¼		5.6	291.8	L
+3		9.5	287.9	L
cb.		10.5	286.9	L

297.35

60

+5		10.5	286.9	L
+6		5.5	291.9	L
W		5.4	292.0	L
	S ¼			
W		5.6	291.8	L
cb.		5.7	291.7	L
¼		5.6	291.8	L
E		5.2	292.2	L
¼		5.2	292.2	L
cb.		5.0	292.4	L
E		4.7	292.7	L
	E thorn			
E		4.8	292.6	L
cb.		5.0	292.4	L
¼		5.1	292.3	L
E		5.4	292.0	L
¼		5.7	291.7	L
cb.		6.9	290.5	L
W		9.9	287.5	L
+15		13.6	283.8	L
	N ¼			
-15		14.1	283.3	L
W		12.1	285.3	L
cb.		9.7	287.7	L
¼		7.0	290.4	L
E		6.1	291.3	L

¼		5.8	291.6	⌐
cb.		5.5	291.9	⌐
E		4.8	292.6	⌐
	N cb.			
E		4.2	293.2	⌐
+7		4.6	292.8	⌐
cb.		5.7	291.7	⌐
¼		5.7	291.7	⌐
d.		6.0	291.4	⌐
¼		8.9	288.5	⌐
cb.		12.7	284.7	⌐
W		13.9	283.5	⌐
+15		15.9	281.5	⌐
	N.L. Thurn one E = 0+00			
-15		15.0	282.4	⌐
W		15.0	282.4	⌐
cb.		13.2	284.2	⌐
¼		9.9	287.5	⌐
d.		5.8	291.6	⌐
¼		5.5	291.9	⌐
cb.		5.4	292.0	⌐
+3		4.0	293.4	⌐
E		3.7	293.7	⌐
	50' N			
E		0.6	296.8	⌐
+7		1.7	295.7	⌐

cb.		2.6	294.8	⌐
¼		3.3	294.1	⌐
d.		3.4	294.0	⌐
+4		3.0	294.4	⌐
¼		3.9	293.5	⌐
cb.		9.9	287.5	⌐
W		12.1	285.3	⌐
+15		12.3	285.1	⌐ on Rock Appr ox. 75' N of C
T.P. K16	307.28	2.23	295.12	
	75' N			
-15		20.5	286.8	⌐
W		17.2	290.1	⌐
cb.		15.0	292.3	⌐
¼		11.7	295.6	⌐
d.		11.8	295.5	⌐
¼		11.4	295.9	⌐
cb.		10.2	297.1	⌐
E		9.0	298.3	⌐
	100' N			
E		7.1	300.2	⌐
cb.		8.0	299.3	⌐
¼		9.5	297.8	⌐
d.		9.5	297.8	⌐
¼		9.8	297.5	⌐
cb.		9.5	297.8	⌐
W		10.7	296.6	⌐

+15		14.1	293.2	
	150'N			
÷10		8.1	299.2	⌐
W		7.3	300.0	⌐
cb.		6.6	300.7	⌐
¼		6.7	300.6	⌐
℄		6.8	300.5	⌐
¼		6.7	300.6	⌐
cb.		5.8	301.5	⌐
E		4.9	302.4	⌐
187'N = ℄ Con. Ribbon. Dr. on W 5' in St.				
E		3.0	304.3	⌐
cb.		1.2	303.1	⌐
¼		5.0	302.3	⌐
℄		5.3	302.0	⌐
¼		5.2	302.1	⌐
cb.		5.2	302.1	⌐
~~#~~ 5 on Dr.		5.20	302.08	⌐
W		5.40	301.9	⌐
+5		5.7	301.6	⌐
	242'N			
-5		3.4	303.9	⌐
W		3.4	303.9	⌐
cb.		3.1	304.2	⌐
¼		3.0	304.3	⌐
℄		2.6	304.7	⌐

¼		2.6	304.7	⌐
cb.		1.9	305.4	⌐
E		1.1	306.2	⌐
TP 8.56	315.37	9.47	306.81	
282'N = ℄ Garage on W. Con. Ribbons Floor				
E		8.0	307.4	⌐
cb.		8.5	306.9	⌐
¼		9.1	306.3	⌐
℄		9.3	306.1	⌐
¼		9.6	305.8	⌐
cb.		9.6	305.8	⌐
W		10.1	305.3	⌐
+4' = Garage Floor		10.18	305.19	⌐
296'N = ℄ Con. Walk 2.0 West to house		9.45	305.92	⌐
310'N = ℄ Acacia tree on E 16" dia. 25' High 1.5' in St.				
W		8.6	306.8	⌐
cb.		8.3	307.1	⌐
¼		8.7	306.7	⌐
℄		8.4	307.0	⌐
¼		8.5	306.9	⌐
cb.		7.7	307.7	⌐
E		7.0	308.4	⌐
350' = ℄ Acacia tree on E 1' dia. 1.5' in St. 30' tall				
E		6.2	309.2	⌐
cb.		6.6	308.8	⌐
¼		7.1	308.3	⌐

℄	7.2	308.2	⌐
¼	7.5	307.9	⌐
cb.	7.3	308.1	⌐
W	7.3	308.1	⌐
373'N = ℄ con. walk on E. to house	5.40	4'in st.	
400'N = Section at approx Rt. Angles to sb. upas st. on W			
W.	6.3	309.1	⌐
cb.	6.3	309.1	⌐
¼	6.2	309.2	⌐
℄	5.9	309.5	⌐
¼	5.9	309.5	⌐
cb	5.3	310.1	⌐
E	4.9	310.5	⌐
417.7'N = N.L. UPAS ST Produced Easterly = Approx. dist.	Section Parallel with N.L.	Upas	5.9 5.5 4.9.
E	4.2	311.2	⌐
cb.	4.3	311.1	⌐
℄	4.8	310.6	⌐
¼	5.2	310.2	⌐
cb.	4.9	310.5	⌐
W	4.9	310.5	⌐
450'N N.L. of Thorn			
W	4.0	311.4	⌐
cb.	3.9	311.5	⌐
¼	3.7	311.7	⌐
℄	3.7	311.7	⌐
¼	3.5	311.9	⌐

cb.	3.1	312.3	⌐
E	3.1	312.3	⌐
500'N			
E	2.0	313.4	⌐
cb.	2.3	313.1	⌐
¼	2.4	313.0	⌐
℄	2.5	312.9	⌐
¼	2.5	312.9	⌐
cb.	2.5	312.9	⌐
W	2.5	312.9	⌐
550'N			
W	1.2	314.2	⌐
cb.	1.4	314.0	⌐
¼	1.3	314.1	⌐
℄	1.3	314.1	⌐
¼	1.3	314.1	⌐
cb.	1.1	314.3	⌐
E	1.0	314.4	⌐
	1.0 cb S.		
610'N = S.L. Myrtle on E.	1.0 ¼ S.		
E	0.0	315.4	⌐
cb.	0.0	315.4	⌐
¼	0.1	315.3	⌐
℄	0.2	315.2	⌐
¼	0.2	315.2	⌐
cb.	0.4	315.0	⌐
W	0.1	315.3	⌐

		315.37			
T.P.	5.80	321.13	0.04	315.33	
	↓ cb. Myrtle on E				
W			5.7	315.4	↵
cb.			5.8	315.3	↵
¼			5.9	315.2	↵
E			5.9	315.2	↵
¼			5.7	315.4	↵
cb.			5.6	315.5	↵
E			5.3	315.8	↵
	↓ ¼				
E			5.0	316.1	↵
cb.			5.2	315.9	↵
¼			5.7	315.4	↵
E			5.6	315.5	↵
¼			5.8	315.3	↵
cb.			5.5	315.6	↵
W			5.8	315.3	↵
	E				
W			5.7	315.4	↵
cb.			5.6	315.5	↵
¼			5.8	315.3	↵
E			5.5	315.6	↵
¼			5.6	315.5	↵
cb.			5.2	315.9	↵
E			4.6	316.5	↵
	N ¼				

		321.13		
E		4.7	316.4	↵
cb.		4.9	316.2	↵
¼		5.1	316.0	↵
E		5.4	315.7	↵
¼		5.5	315.6	↵
cb.		5.8	315.3	↵
W		5.5	315.6	↵
	N cb.			
W		5.0	316.1	↵
cb.		5.7	315.4	↵
¼		5.4	315.7	↵
E		5.1	316.0	↵
¼		4.9	316.2	↵
cb.		4.7	316.4	↵
E		4.5	316.6	↵
	N.L. Myrtle on E			
E		4.3	316.8	↵
cb.		4.7	316.4	↵
¼		4.8	316.3	↵
E		5.0	316.1	↵
¼		5.5	315.6	↵
cb.		5.2	315.9	↵
W		5.0	316.1	↵
	N.L. + 10' = old N.L. Myrtle = end of existing cb. on E.			
W		4.9	316.2	↵
cb.		4.9	316.2	↵

	321.13			
¼		5.1	316.0	⌐
℄		5.0	316.1	⌐
¼		5.0	316.1	⌐
Gut		4.8	316.3	⌐
℄ top cb		4.52	316.61	⌐
℄		4.6	316.5	⌐
61.3' N. of old section parallel with ℄ cb line on W. Produced Myrtle on ℄ = ℄ cb. Line Myrtle on West Factory				
℄		4.2	316.9	⌐
top cb.		4.31	316.82	⌐
Gut		5.0	316.1	⌐
¼		5.0	316.1	⌐
℄		4.8	316.3	⌐
¼		4.8	316.3	⌐
Gut		5.4	315.7	⌐
W top cb.		5.15	315.98	⌐
T.P.	1.88	324.94	5.07	316.06
T.P. on BM. Myrtle +331d N.E. P.P.			2.85	322.09 322.06 = BM. .03

Walker 2-27

X. Section Thorn St. 70' wide 10' Cbs. 12.5' 1/4 S

From E.L. Boundary to E.L. ~~Jefferson St.~~ Haller St.

N.L. Station's

Note: All sections at Rt. Angles N.L. Thorn St.

9.73 304.85 295.12 = Elev. Rock T.P. Page 31

E (W) L.

N			7.4	297.4	
cb.			7.8	297.0	
1/4			12.3	292.5	
+8			13.0	291.8	
d	Platted 3-10-27 J.H.L.		12.2	292.6	
1/4			12.2	292.6	
cb.			12.4	292.4	
S			14.3	290.5	
		20' E			
S			11.4	293.4	
cb.			11.2	293.6	
1/4			11.3	293.5	
d			10.9	293.9	
+5			11.2	293.6	
+8			9.7	295.1	
1/4			9.4	295.4	
cb.			8.4	296.4	
N			8.0	296.8	
		50' E			
N			6.1	298.7	
cb.			6.6	298.2	
1/4			7.2	297.6	
+2			7.5	297.3	

304.85

+4		8.6	296.2
d		8.6	296.2
1/4		9.0	295.8
cb.		8.9	295.9
S		8.5	296.3
	100' E		
S		7.0	297.8
cb.		6.4	298.2
1/4		6.6	298.2
d		6.1	298.7
+8		6.0	298.8
1/4		5.0	299.8
d		4.2	300.6
N		3.9	300.9
	150' E		
N		2.7	302.1
cb.		2.9	301.9
1/4		4.0	300.8
+3		5.0	299.8
d		5.1	299.7
1/4		5.7	299.1
cb.		6.1	298.7
S		6.8	298.0
+10		7.7	297.1
	200' E		
-10		6.7	298.1

304.85

S			5.8	299.0	
cb			5.3	299.5	
¼			4.9	299.9	
℄			4.4	300.4	
+8			4.2	300.6	
¼			3.1	301.7	
cb			2.1	302.7	
N			1.2	303.6	
		250'E			
N			1.7	303.1	
cb.			1.9	302.9	
¼			2.6	302.2	
+4			3.8	301.0	
℄			3.8	301.0	
¼			4.2	300.6	
cb.			4.8	300.0	
8S			5.6	299.2	
+10			6.7	298.1	
		296'E = W.L. Nike on N			14 cbs 13 ¼'s
-10			4.5	300.3	
S			4.4	300.4	
cb.			4.0	300.8	
¼			3.7	301.1	
℄			3.1	301.7	
+8			3.4	301.4	
¼			2.6	302.8 ✓	

304.85

cb.		2.0	302.8
N		1.6	303.2
TP 797	31134	1.48	303.37
N = top cb.	W cb.	2.14	303.2
Cut		8.5	302.8
cb.		9.0	302.3
¼		9.5	301.8
℄		9.4	301.9
¼		9.7	301.6
cb.		10.0	301.3
S		9.9	301.4
	N ½		
S		9.5	301.8
cb.		9.3	302.0
¼		9.1	302.2
℄		8.7	302.6
¼		9.3	302.0
cb.		8.7	302.6
N		8.4	302.9
	℄		
N		7.8	303.5
cb.		8.0	303.3
¼		8.5	302.8
℄		8.2	303.1
½		8.6	302.7
cb.		8.8	302.5

S	9.0	302.3
E ¼		
S	8.5	302.8
cb.	8.4	302.9
¼	8.1	303.2
℄	7.7	303.6
¼	7.8	303.5
cb.	7.9	303.4
N	7.7	303.6
E cb.		
N=top cb.	7.64	303.7
Gut	7.7	303.6
cb.	7.9	303.4
¼	7.9	303.4
℄	7.6	303.7
¼	7.8	303.5
cb.	8.3	303.0
S	8.5	302.8
E ⊗ L. Nile on N. = 0+00		
S	8.2	303.1
cb.	8.2	303.1
¼	7.6	303.7
℄	7.4	303.9
¼	7.6	303.7
cb.	7.1	304.2
N	7.5	303.8

✗ 10' E		
N	5.9	305.9
cb.	6.0	305.3
¼	7.0	304.3
℄	7.0	304.3
¼	7.1	304.2
cb.	7.9	303.4
S	7.7	303.6
50' E		
S	6.1	305.2
cb.	6.1	305.2
¼	5.8	305.5
℄	5.8	305.5
¼	5.8	305.5
cb.	5.3	306.0
N	5.2	306.1
100' E		
N	4.5	306.8
cb.	4.5	306.8
¼	5.0	306.3
℄	4.7	306.6
¼	4.8	306.5
cb.	5.2	306.1
S	4.8	306.5
150' E		
S	4.2	307.1

cb.			4.0	307.3
¼			4.0	307.3
℄			3.6	307.7
¼			3.7	307.6
cb.			3.5	307.8
N			3.5	307.8
		200' E		
N			2.9	308.4
cb.			2.9	308.4
¼			3.3	308.0
℄			3.2	308.1
¼			3.5	307.8
cb.			3.4	307.9
S			3.6	307.7
		250' E		
S			3.1	308.2
cb.			2.9	308.4
¼			2.9	308.4
℄			2.7	308.6
¼			2.9	308.4
cb.			2.5	308.8
N			2.4	308.9
		300' E = W.L.	VANCOUVER Jefferson	
N			2.4	308.9
cb			2.2	309.1
¼			2.6	308.7

℄		2.5	308.8
¼		2.8	308.5
cb.		2.9	308.4
S		2.7	308.6
T.P. 181	303.14	10.01	301.33
T.P. on Rock		7.99	295.15
			295.12 = Rock.
			0.03

Note. T.P. on Rock Noted on Page 31 was carried on up to N.E.B.P. Myrtle +33'9 for chk. See Page 35

Plotted - 3-10-27
J.T.H.

Walker

X. Section Newton Ave. 80 W. side
From 36th to 34th St 14' cbs.
13' 1/4 S

S.E. BP. Nat. 36th	10.79	47.77		36.98
	E.L. = 20'			
-10			9.4	38.4
N			8.5	39.3
cb.			7.3	40.4
1/4			6.2	41.6
d.			5.9	41.9
1/4			4.5	43.3
cb.			4.9	42.9
S			4.9	42.9
				10' cbs
	E.L. 36th			10' 1/4 S.
S			1.3	46.5
cb.			1.8	46.0
1/4			2.3	45.5
d.			2.8	45.8
1/4			3.0	44.8
cb.			3.3	44.5
N			3.7	44.1
+10			4.5	43.3
T.P.	7.6	55.23	0.19	47.58
-10			10.1	45.1
N		E cb.	9.1	46.1
cb.			9.0	46.0
1/4			8.7	46.5
d.			8.5	46.7

55.23

40

1/4		8.0	47.2
cb.		7.6	47.7
S		6.7	48.7
	E 1/4		
S		6.1	49.1
cb.		6.5	48.7
1/4		7.1	48.1
d.		7.5	47.7
1/4		7.8	47.4
cb.		7.8	47.4
N.		8.1	47.1
+10.		9.4	45.8
	d.		
N		7.1	48.1
cb.		6.6	48.6
1/4		6.7	48.5
d.		6.1	49.1
1/4		5.9	49.3
cb.		5.5	49.7
S		5.6	49.4
	W 1/4		
S		4.9	50.3
cb.		4.7	50.5
1/4		5.1	50.1
d.		4.9	50.3
1/4		5.7	49.5

5523

cb.	5.4	49.8
N	5.7	49.5
W cb.		
N	4.5	50.7
cb.	4.5	50.7
¼	4.9	50.3
2	4.4	50.8
¼	4.6	50.6
cb.	4.2	51.0
S	4.3	50.9
W 6. 36 +b		
S	4.8	50.4
cb.	4.3	50.9
¼	4.1	51.1
2	3.9	51.3
¼	4.0	51.2
cb.	3.8	51.4
N	3.6	51.6
30' W		
N	2.8	52.4
cb.	2.4	52.8
+8	2.7	52.5
+10	3.4	51.8
¼	3.4	51.8
2	3.7	51.5
¼	4.3	50.9

5523

4

cb.	4.6	50.6
S	4.9	50.9
85' W		
S	5.9	49.3
cb.	5.6	49.6
¼	5.3	49.9
2	4.7	50.5
¼	4.7	50.5
+2	4.9	50.3
+6	4.6	50.6
cb.	4.5	50.7
N	4.3	50.9
150' W		
N	4.6	50.6
cb.	4.8	50.4
+8	5.6	49.6
+10	6.5	48.7
¼	6.1	49.1
2	6.2	49.0
¼	7.1	48.1
cb.	7.7	47.5
S	8.0	47.2
180' W		
S	8.6	46.6
cb.	8.2	47.0
¼	7.8	47.4

55.23

℄	7.0	48.2	
¼	7.0	48.2	
+8	5.8	49.4	
cb.	5.3	49.9	
N	4.6	50.6	
200' W			
N	5.9	49.3	
cb.	6.7	48.5	
+6	7.1	48.1	
¼	7.9	47.3	
℄	7.4	47.8	
¼	8.3	46.9	
cb.	8.8	46.4	
S	8.9	46.3	
255' W			
S	9.9	45.3	
cb.	9.4	45.8	
¼	9.4	45.8	
℄	8.8	46.4	
¼	9.3	45.9	
cb.	8.7	47.0	
N	7.8	47.4	
300' W			
N	9.2	46.0	
cb.	9.6	45.6	
¼	10.3	44.9	

55.23

82

℄	10.1	45.1
¼	10.8	44.4
cb.	11.1	44.1
S	11.3	43.9
320' W = ℄ on Walton South	1.50 on line	43.73
345' W = ℄ " " " South	11.85	43.28
S	11.9	43.3
cb.	12.2	43.0
¼	12.0	43.2
℄	11.3	43.9
¼	11.0	44.2
cb.	11.1	44.1
N	10.7	44.5
393' W = ℄ on Walton S. to house		
N	11.7	43.5
cb.	12.3	42.9
¼	12.6	42.6
℄	12.5	42.7
¼	13.0	42.2
cb.	12.8	42.4
S on Walk	12.46	42.77
T.P. 2.47 45.23	12.97	42.76
450' W		
S	4.7	40.5
cb.	4.7	40.5
¼	4.9	40.3

4523

℄	4.3	40.9
¼	4.2	41.0
cb.	4.3	40.9
N	4.1	41.1
500'W		
N	6.7	38.5
cb.	6.4	38.8
¼	6.1	39.1
℄	5.8	39.4
¼	6.4	38.8
cb.	6.4	38.8
S	7.0	38.2
550'W		
S	7.4	37.8
cb.	7.1	38.1
+10	6.7	38.5
+11	7.7	37.5
¼	7.7	37.5
℄	6.9	38.3
¼	6.9	38.3
cb.	7.1	38.1
N	7.3	37.9
575'W		
N	7.7	37.5
cb.	6.7	38.5
+9	6.5	38.7

4525

+11	7.5	37.7
¼	7.5	37.7
℄	7.7	37.5
¼	8.1	36.2
+2	6.3	38.9
cb.	6.8	38.4
S	7.7	37.5
600'W = W.L. 35th		
S	8.2	37.0
cb.	8.0	37.2
+9	8.3	36.9
¼	8.1	36.1
℄	8.6	36.6
¼	8.7	36.5
+4	8.0	37.2
cb.	8.3	36.9
N	8.1	37.1
W.L. 35th = 0+00		
N	11.1	34.1
cb.	11.3	33.9
¼	11.6	33.6
℄	11.5	33.7
¼	11.9	33.3
cb.	10.3	34.9
S	10.7	35.0
20'W		

		45.23		
S			11.6	33.6
cb.			12.0	33.2
+9			12.4	32.8
¼			13.6	31.6
℄			13.1	32.1
¼			13.8	31.4
+6			12.2	33.0
cb.			12.1	33.1
N			11.2	34.0
		45' W		
T.P.	173	34.44	12.52	32.71
N			2.9	31.5
cb.			3.3	31.1
+8			4.1	30.3
¼			5.1	29.3
℄			4.2	30.2
¼			4.2	30.2
cb.			3.5	30.9
S			2.3	32.1
		100' W		
S			7.6	26.8
cb.			8.0	26.4
¼			7.5	26.9
℄			7.1	27.3
¼			7.4	27.0
cb			6.9	27.5

	34.44		42
N		6.2	28.2
+5		5.5	28.9
135' W = ℄ Con. Wall to N			
N = top Walk		3.33	31.11
cb		4.3	30.1
¼		7.2	27.2
℄		7.8	26.8
¼		7.6	26.6
cb.		8.8	25.6
S		8.8	25.6
	145' W		
S		9.0	25.4
+11		8.7	25.7
cb.		10.0	24.4
¼		7.8	26.6
℄		7.3	27.1
¼		7.1	27.3
+2		7.0	27.4
+6		4.3	30.1
cb.		3.6	30.8
N		2.7	31.7
	163' W		
N		2.6	31.8
cb.		3.8	30.6
+7		4.7	29.7
¼		6.9	28.5

℄	7.1	27.3
¼	7.3	27.1
cb.	9.7	24.7
+1	11.2	23.2
+5	9.9	24.5
S	10.0	24.4 ✓
180'W = ℄ Con. Walk on N		
S	12.2	22.2
+10	10.8	23.6
cb.	10.8	23.6
¼	10.2	24.2
+4	7.3	27.1
℄	7.4	27.0
¼	7.2	27.2
+2	7.1	27.3
+7	4.9	29.5
cb.	4.3	30.1
N	3.1	31.3
N+1' = top of Walk	3.04	31.46
205'W = ℄ Con. Ribbon Dr. on North		
N = top Dr.	3.72	30.72
cb.	5.3	29.1
+7	5.4	29.0
¼	7.2	27.2
℄	7.4	27.0
+10	7.6	26.8

¼	8.5	25.9
cb.	11.8	22.6
S	13.2	21.2
+10	13.5	20.9
257'W = ℄ Con. Walk on N		
-10	12.9	22.5
S	11.3	23.1
cb.	9.7	24.7
¼	7.8	26.6
+3	7.5	26.9
℄	7.4	27.0
¼	7.2	27.2
+6	5.9	28.5
cb.	5.5	28.9
N	4.8	29.6
+1 = top of Walk	4.66	29.78
300'W		
N	8.3	26.1
cb.	8.4	26.0
¼	8.4	26.0
℄	8.0	26.4
¼	8.6	25.8
cb.	9.6	24.8
S	11.6	22.8
+10	12.9	21.5
350'W		

3444

-10		11.5	22.9
S		10.4	24.0
cb.		9.8	24.6
¼		9.2	25.2
℄		8.5	25.9
¼		8.9	25.5
cb.		8.7	25.7
N		8.6	25.8
	400' W		
N		9.3	25.1
cb.		8.7	25.7
¼		9.2	25.2
℄		8.8	25.6
¼		8.9	25.5
cb.		8.5	25.9
S.		8.8	25.6
	433		
S		11.1	23.3
cb.		11.1	23.3
¼		10.8	23.6
℄		10.1	24.3
¼		10.0	24.4
cb.		10.4	24.0
N		11.6	22.8
+10		13.6	20.8
	438' W		

3444

-10		15.0	19.4
N		13.0	21.4
cb.		11.3	23.1
¼		11.0	23.4
℄		10.7	23.7
¼		11.6	22.8
cb.		11.7	22.7
*5		11.9	22.5
+10		11.9	22.5
T.P. 1.13	22.48	13.09	21.35
	471' W		
-10		11.7	10.5
S		11.1	11.1
cb.		10.5	12.0
¼		10.4	12.1
℄ = Rim of M.H.		10.36	12.12
¼		9.8	12.7
cb.		9.4	13.1
N		10.4	12.1
+10		10.8	11.7
+15		12.2	10.3
T.P. 0.10	10.86	11.72	10.76
	485' W		
-15		3.7	7.2
N		0.9	10.8
*cb.		1.4	9.5

¼		1.4	9.5
℄		1.9	9.0
¼		3.5	7.4
cb.		4.0	6.9
S		4.8	6.1
+15		4.8	6.1
	505' W		
−15		8.5	2.5
S		8.0	2.9
cb.		7.3	3.6
¼		6.4	4.5
℄		5.4	5.5
¼		4.6	6.3
cb.		4.0	6.9
N		4.6	6.3
+15		5.9	5.0
	522' W		
N−10		7.7	3.2
N		8.0	2.9
cb.		8.0	2.9
¼		8.3	2.6
℄		9.0	1.9
¼		10.2	0.7
cb.		10.7	0.2
S		10.7	0.2
+10		10.7	0.2

	550' W	
−10	10.5	0.4
S	10.5	0.4
cb.	10.5	0.4
¼	10.4	0.5
℄	10.4	0.5
¼	10.3	0.6
cb.	9.8	1.1
N	9.4	1.5
+10	9.4	1.5
599' W = E.L. 34th	(Note; dist. Measured bet. Mon. = 659' this is within 0.1' of being correct as too much water over hub.	
−5	8.0	−2.9
N	10.1	0.8
cb	10.7	0.2
¼	10.6	0.3
℄	10.9	0.0
¼	10.9	0.0
cb.	11.4	−0.5
S	11.5	−0.6
+10	11.5	−0.6
T.P. 7.48 11.52	6.82	4.04
T.P. S.E.B.P. on B.M. Nail. +34th	4.70	6.82

Walker 3-8-27

X. Section Thorn St. 70' Wide 10 cbs 12.5, 1/4S
From W.L. Vancouver East

11.19 314.89 303.70 N.E. top of cb Nile & Thorn See Page 38

W cb Line {Note: for Section on W.L. See Page 39

N		6.0	308.9
cb		5.8	309.1
1/4	Plotted 3-10-27 J.T.H.	6.0	308.9
℄		6.0	308.9
1/4		6.2	308.7
cb		6.4	308.5
S		6.5	308.4
	W 1/4		
S		6.5	308.4
cb		6.4	308.5
1/4		6.4	308.5
℄		5.9	309.0
1/4		6.0	308.9
cb		5.8	309.1
N		5.8	309.1
	℄		
N		5.8	309.1
cb		5.8	309.1
1/4		5.9	309.0
℄		5.9	309.0
1/4		6.0	308.9
cb		6.3	308.6
S		6.4	308.5

E 1/4

S		6.4	308.5
cb		6.3	308.6
1/4		6.1	308.8
℄		5.7	309.2
1/4		5.7	309.2
cb		5.7	309.2
N		5.5	309.4
	E cb		
N		5.2	309.7
cb		5.6	309.3
1/4		5.7	309.2
℄		5.8	309.1
1/4		6.1	308.8
cb		6.1	308.8
S		6.1	308.8
	E.L. VANCOUVER on N = 0+00		
S		6.1	308.8
cb		6.0	308.9
1/4		6.0	308.9
℄		5.5	309.4
1/4		5.5	309.4
cb		5.2	309.6
N		5.3	309.6
	50' E		
N		4.9	310.0

		314.89		
cb			5.2	309.7
¼			5.3	309.6
℄			5.3	309.6
¼			5.6	309.3
cb			5.6	309.3
S			5.8	309.1
		100' E		
S			5.0	309.9
cb			5.2	309.7
¼			5.0	309.9
℄			4.8	310.1
¼			4.6	310.3
cb			4.5	310.4
N			4.2	310.7
		150' E		
N			4.4	310.5
cb			4.4	310.5
¼			4.5	310.4
℄			4.4	310.5
¼			4.9	310.0
cb			4.7	310.2
S			4.9	310.0
		200' E		
S			4.8	310.1
cb			4.8	310.1
¼			4.8	310.1

		314.89		
℄			4.8	310.1
¼			4.9	310.0
cb			4.9	310.0
N			5.1	309.8
+10			5.5	309.4
		217' E		
-10			10.3	304.6
N			8.9	306.0
cb			7.3	307.6
¼			6.0	308.9
℄			5.4	309.5
¼			5.1	309.8
cb			4.9	310.0
S			4.9	310.0
		233' E		
S			5.2	309.7
cb			6.1	308.8
¼			6.9	308.0
℄			8.2	306.8
¼			9.0	305.9
cb			10.6	304.3
N			12.6	302.3
+20			17.5	297.4
		253' E		
-20			23.8	289.1
N			19.8	295.1

		314.89		
cb			18.3	296.6
¼			16.4	298.5
℄			14.1	300.8
¼			12.9	302.0
cb			10.5	304.4
S			8.6	306.3
+5			7.7	307.2
T.P.	0.20	302.22	12.87	302.02
		275'E		
-10			0.3	301.9
S			3.0	299.2
cb			5.9	296.3
¼			8.5	293.7
℄			10.8	291.4
¼			12.9	289.3
cb			13.8	288.4
N			17.4	284.8
+30			23.0	279.2
		292'E		
-30			32.0	270.2
N			26.1	276.1
cb			22.8	279.4
¼			21.3	279.9
℄			19.3	282.9
¼			16.1	286.1
cb			12.7	289.5

302.22

50

S		9.9	292.3
+15		4.3	297.9
	310'E = Mk. Haller ~~Jefferson~~ st		
-20		12.3	289.9
S		17.7	284.5
cb		21.3	280.9
¼		27.2	275.0
℄		27.8	274.9
¼		30.2	272.0
cb		31.2	271.0
N		33.4	268.8
+45		44.5	257.7
T.P. 12.58	314.60	0.20	302.02
Ck. on NE top cb. Nile & Thorn sts.		10.91	303.69 303.70 = top cb. +0.01 in Error

Platted
3-10-27
J.T.H.

4/16/71 Cross Section of Washout #1
W Moore on Curlew S of Penn Fire
60' wide 10' curbs

198.00 Penn Curlew

SE Retard	0.86	197.97		197.11
SL Penn on East=00				
W Top paving			1.7	196.3
cb " "			2.2	195.8
0+5 South				
-5			5.5	192.5
W			5.0	193.0
+6			4.0	194.0
+7			2.2	195.8
cb			2.2	195.8
0+10				
-5			6.5	192.5
W			5.8	192.2
+5			5.2	192.8
cb			2.4	195.6
0+17				
-5			6.1	191.9
W			3.0	195.0
cb			2.5	195.5
Washout #2 = 0+20				
W			4.0	194.0
cb			4.4	193.6
1/2			4.4	193.6
C			3.7	194.3
1/2			4.2	193.8
cb			3.6	194.4

197.97

E	4.5	193.5
0+25		
E	4.8	193.2
cb	4.2	193.8
+1	4.7	193.3
+2	5.7	192.3
+7	4.9	193.1
+8	7.1	190.9
1/4	7.1	190.9
+1	7.1	190.9
+2	5.0	193.0
C	4.4	193.6
+7	4.8	193.2
1/4	7.2	190.8
+8	9.0	189.0
cb	5.3	192.7
W	5.3	192.7
0+75		
W	6.1	191.9
+5	6.1	191.9
cb	11.7	186.3
+4	12.6	185.4
+6	12.6	185.4
1/4	9.5	188.5
+2	6.3	191.7
C	5.7	192.3

198.0

		1979		198.0
+5			5.8	192.2
+6			8.0	190.0
1/4			9.0	189.0
+4			6.3	191.7
c6			5.4	192.6
E			6.0	192.0
	0+85			
E			6.5	191.5
c6	Tab east c6		6.4	191.6
+3			8.9	189.1
1/4			10.1	187.9
+4			6.5	192.5 191.5
C			6.4	191.6
+5			6.7	191.3
1/4			10.6	187.4
+8			14.6	183.4
c6			12.0	186.0
+5			7.9	190.1
W			7.8	190.2
	0+9W			
=20			26.0	172.0
-8			23.1	174.9
W			18.2	179.8
+5			12.0	186.0
c6			15.5	182.5
+4			15.4	182.6

	1979	Continued	5.2
			198.0
1/4		9.5	188.5
+5		7.2	190.8
C		7.1	190.9
+5		7.2	190.8
+6		8.7	189.3
1/4		10.7	187.3
+5		9.5	188.5
+6		8.5	189.5
c6		7.0	191.0
E		6.9	191.1
	1+00		
E		7.0	191.0
c6		7.4	190.6
+4		7.8	190.2
+5		11.5	186.5
1/4		10.9	187.1
+2		8.4	189.6
C		7.7	190.3
1/4		8.6	189.4
c6		17.4	180.6
W		19.8	178.2
+8		22.6	175.4
+20		26.2	171.8
	1+08		
-10		17.1	180.9
W		18.0	180.0

		197.97		198.0	
c6			16.6	181.4	
+2			8.9	189.1	
1/4			8.6	189.4	
c			8.2	189.8	
1/4			9.0	189.0	
+1			11.0	187.0	
+5			12.0	186.0	
+7			8.3	189.7	
c6			8.0	190.0	
E			7.4	190.6	
	1+09				
E			7.6	190.4	
c6			8.2	189.8	
+4			8.3	189.7	
+5			11.9	186.1	
+9			11.4	186.6	
1/4			9.1	188.9	
c			8.3	189.7	
1/4			8.9	189.1	
c6			9.0	189.0	
1/4			8.8	189.2	185.50
T.P.	0.18	185.48	12.67	185.30	
	1+50				
E			+4.0	181.5	
c6			+2.1	183.4	
+4			+1.2	184.3	

185.48

Curb 53

185.5

+5	2.7	182.8
+7	2.7	182.8
+9	0.0	185.5
1/4	0.0	185.5
2+00		
E	0.0	185.5
c6	1.0	184.5
+3	1.6	183.9
+4	5.0	180.5
+6	5.0	180.5
+7	2.0	183.5
1/4	2.0	183.5
2+50 Joint		
E	3.2	182.3
c6	4.0	181.5
+4	7.4	178.1
+6	7.4	178.1
+7	5.7	179.8
1/4	5.5	180.0
3+30		
E	7.4	178.1
c6	8.4	177.1
+4	10.3	175.2
+5	13.0	172.5
+6	13.0	172.5
+8	10.8	174.7
1/4	10.5	175.0

		185.48			185.5		173.08		173.1
4+00						4+90			
E			12.5	173.0		E		6.6	166.5
c6			14.8	171.7		c6		8.0	165.1
+6			15.7	169.8		1/4		8.8	164.3
+7			17.2	168.3		+3		9.0	164.1
1/4			17.2	168.3		+4		10.4	162.7
+2			14.9	170.6		C		11.9	161.2
T.P.	0.21	173.08	13.11	172.37	173.1	+4		11.7	161.4
4+50 South						+6		8.3	164.8
E			4.9	168.2		1/4		8.3	164.8
c6			5.8	167.3		5+05			
+7			6.0	167.1		E		8.2	164.9
+8			9.3	163.8		c6		9.1	164.0
1/4			9.3	163.8		1/4		9.8	163.3
+1			9.3	163.8		+1		11.8	161.3
+2			6.3	166.8		+3		12.2	160.9
C			6.2	166.9		+6		9.9	163.2
4+70						C		9.7	163.4
E			5.7	167.4		1/4		9.6	163.5
c6			6.5	166.6		c6		9.8	163.3
1/4			7.8	165.3		+8		9.5	163.6
+1			7.8	165.3		41		10.8	162.3
+2			9.6	163.5		+7		20.1	153.0
C			9.9	163.2		+15	Increek	21.3	151.8
+3			7.0	166.1		T.P.	24.5	164.93	10.60	162.48
1/4			7.0	166.1					

164.93

164.9

Sta 30 = Approx ℄ pt

−15		12.9	152.6
−7	℄ creek	14.4	150.5
W		9.7	155.2
+5		3.1	161.8
cb		2.9	162.0
1/4		3.2	161.7
C		3.2	161.7
+3		5.2	159.7
1/4		5.7	159.2
+2		3.4	161.5
cb		2.4	162.5
E		1.2	163.7
	Sta 55		
E		2.6	162.3
cb		4.2	160.7
1/4		5.5	159.4
+1		6.7	158.2
+2		6.7	158.2
+3		4.5	160.4
C		4.5	160.4
1/4		4.7	160.2
cb		5.1	159.8
W		4.3	160.6
+8	E edge creek	13.0	151.9

Content

164.93

TP	0 x 5	157.09	13.09	151.84
TP	4 x 0	145.59	10.70	141.39

W'ly out - North of ℄ pt 25°08' Lot 18 El Paso Tract 145.6

40'W of ℄ angle pt

−10		10.4	135.2
W		4.3	141.3
cb		3.6	142.0

48' W of ℄ pt

cb		4.1	141.5
+4		4.1	141.5
W		7.0	138.6
+10		12.2	133.4

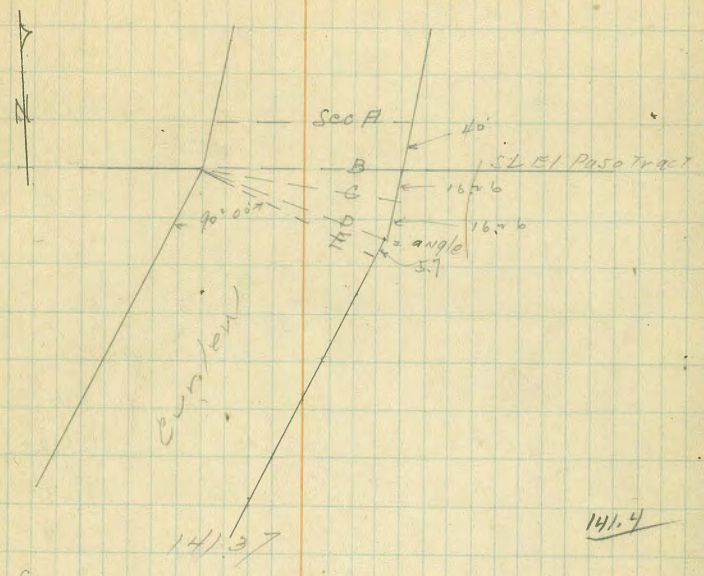
58' W of ℄ pt

−15	east edge creek	16.7	128.9
−10		15.0	130.6
W		11.7	133.9
+3		4.3	141.3
cb		3.8	141.8

63' W

cb		4.2	141.4
+8		4.1	141.5
W		11.1	134.5
+10		15.0	130.6
+15		16.6	129.0

		14.5.59		145.6
	93' N of ℄			
-10			12.2	133.4
w/			3.5	142.1
c6			3.4	142.2
T.P.	3.00	141.37	7.43	138.37
	Cross Section of Cut in Curve			
	S'ly of SL of El Paso Tract			141.4
	Sec A			
E			5.0	139.4
c6			2.8	138.6
1/4			3.4	138.0
C			3.8	137.6
1/4			3.5	137.9
c6			3.6	137.8
w/			4.2	137.2
	Sec B = SL El Paso Tract			
w/			4.5	136.9
c6			5.0	139.4
+2			7.9	133.5
1/4			7.2	134.2
C			6.0	135.4
1/4			5.2	136.0
+1			4.0	137.4
c6			3.0	138.4
E			2.2	139.2



	Sec C		
w/		4.5	136.9
c6		8.4	133.0
1/4		7.3	134.1
C		7.5	133.9
+3		7.0	134.4
+4		4.5	136.9
1/4		3.5	137.9
	Sec D = 4 Line		
w/		4.5	136.9
c6		8.5	132.9
1/4		8.1	133.3
C		7.8	133.6
+2		4.7	136.7
1/4		3.7	137.7

		141.87			141.4
	Sec E = 0+00				
W			4.5	136.9	
CL			8.5	132.9	
1/4			8.4	133.0	
+9			7.9	133.5	
C			4.8	136.6	
T.P.	906	140.3N	10.1	131.96	140.3
	= 0+07				
-10			10.4	129.9	
W			10.1	130.2	
+3			9.6	130.7	
+4			7.5	132.8	
+9			6.0	134.3	
CL			8.N	132.1	
1/4			8.1	132.2	
+3			9.N	131.1	
+9			7.0	133.3	
C			3.4	136.9	
1/4			0.0	140.3	
	0+N4				
-10			13.0	127.3	
-4			9.N	131.1	
W			9.N	131.1	
+1			11.4	129.9	
CL			11.0	129.3	
+7			10.4	129.9	

	140.3N		Curlew	57
				140.3
1/4			6.5	133.8
C			2.9	137.4
	0+N7			
-10			13.3	127.6
-8			9.1	131.2
W			11.7	128.6
CL			11.6	128.7
+5			11.9	128.4
1/4			6.9	133.4
C			2.9	137.4
	0+50			
-14			9.3	131.0
-5N			15.5	124.8
W			14.6	125.7
CL			16.0	124.3
+3			7.0	133.3
1/4			4.5	135.8
C			2.8	137.5
	0+75			
-20			10.6	129.7
-18			17.1	123.2
W			17.N	123.1
+N			17.N	123.1
+5			6.7	133.6
CL			6.N	134.1
1/4			4.9	135.5

140.37 Curlew

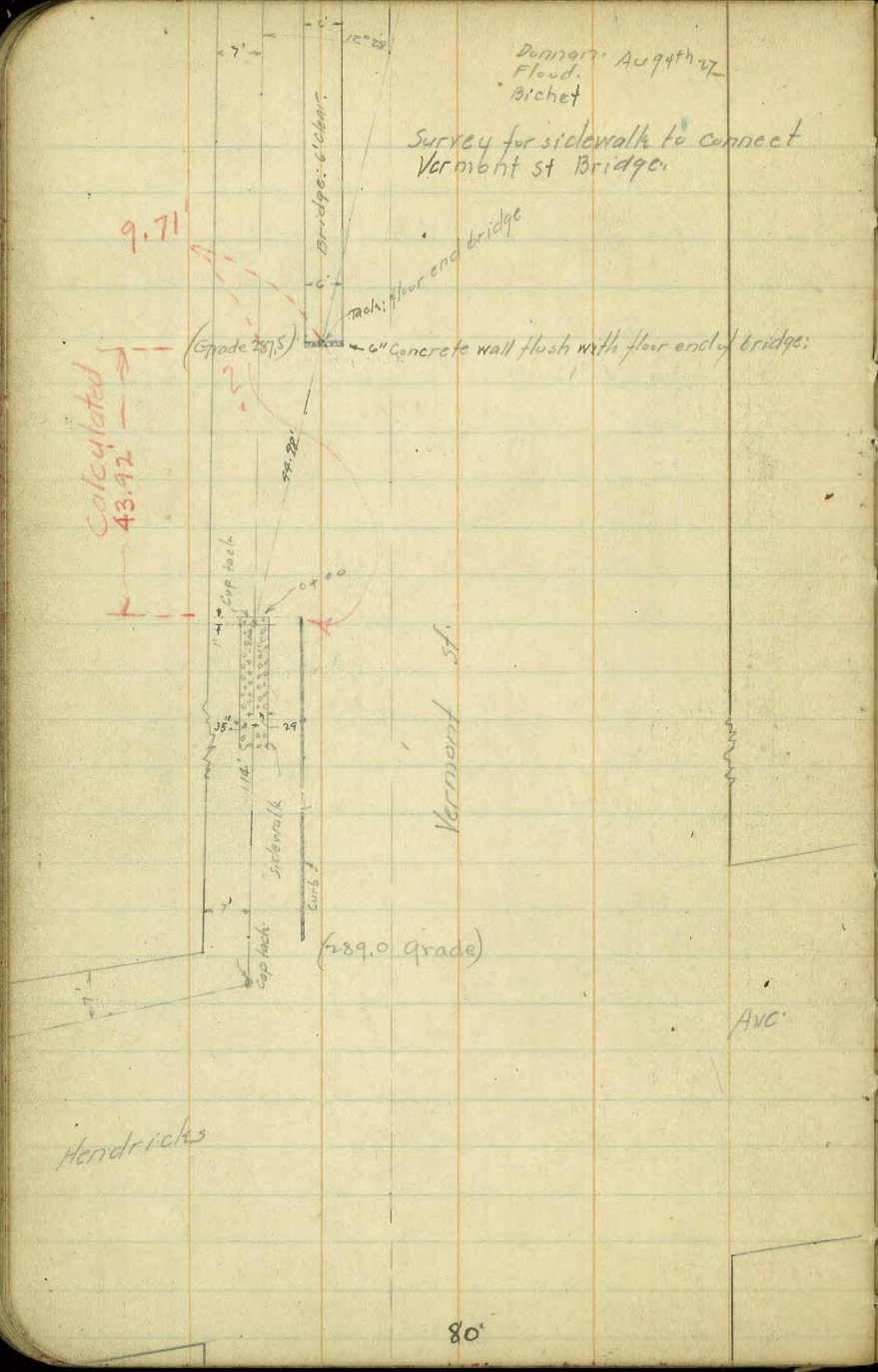
140.3

	0+85			
-25		12.6	127.7	
-22		17.7	122.6	
-5		17.1	123.2	
W/L		8.1	132.2	
cb		6.7	133.6	
1/4		5.1	135.2	
	1+00			
-20		17.8	122.5	
-11		18.0	122.3	
-9		10.5	129.8	
W/L		9.0	131.3	
cb		7.2	133.1	
1/4		5.4	134.9	
	1+75			
-20		19.5	120.8	
-15		13.5	126.8	
W/L		10.5	129.8	
cb		8.7	131.6	
1/4		7.2	133.1	

58

Damage: Aug 4th 27
Flood.
Bichet

Survey for sidewalk to connect Vermont st Bridge.



80'

	+	π	−	Elev	
	4.49	294.22		289.73	B.P.S.W. Cor University and Vermont.
#	5.33	294.90	9.65	289.57	Rock.
	check on return N&E Vermont and Hendricks		6.00	288.9	
	End of curb.		7.61	287.29	Draftsman please check this 287.5
	0+20 Ground.		10.0	284.9	
	Concrete wall end of bridge		12.17	287.73	

Note: E ½' of sidewalk this end 5' buckled by tree: should be removed to make a good job.

Sewer line from 28th and Granada West to connect with line "the Park."

Aug 5th 27

Donnan
Flood
Bichet

"A" line:

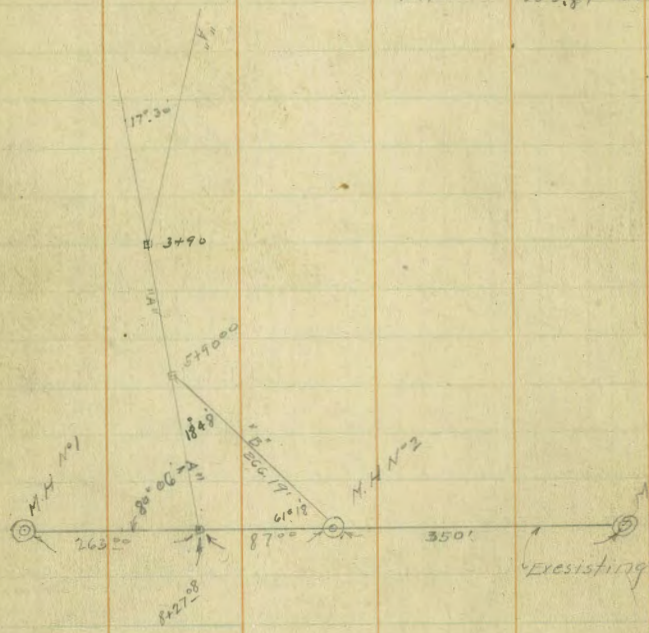
	+	π	−	Ele:
	6.03	238.98 ✓		232.95 B.P.S.E Grape and Granada
	8.01	292.98 ✓	4.01	234.97 End curb W.Side Granada S.C. Hawthorne
0+00 Pine hub & Hawthorn and & Granada			1.12	241.86 ~~234.86~~ Hub 0+00
0+20 W.L. Granada & Hawthorn			5.8	237.18
0+50 & Hawthorn			8.0	234.98
# " "	0.25	230.69 ✓	12.54	230.44 ✓ Rock
1+00 " "			2.2	228.7
1+50 " "			7.5	223.2
1+82 " " P.O.T. Pine hub	3.11	221.97 ✓	11.88	218.81 ✓ Hub
2+00 " "			11.3	210.6
#	0.62	209.99 ✓	12.50 ✓	209.37 ✓ Rock
2+20 " "			10.9	199.1
#	0.44	197.66 ✓	12.77	197.22 ✓ Rock
2+35 & Hawthorne Δ 52°00'R			5.37	192.29 Pine stub
#	0.32	188.50 ✓	10.08	187.58 ✓ Rock
2+80			2.1	186.4
2+90			6.5	182.0
3+05			7.0	181.5
3+20			5.3	183.2
3+35			6.0	182.5
3+50			4.7	184.3
3+65			4.1	184.4
3+80			6.5	182.0
# 3+90 Δ 17°30'LT	1.54	189.24	9.80	178.70 ✓ on Pine stub

Jan 6/1928

60

	+	π 180.24	−	Ele
4+00			4.9	175.34
4+15			7.3	172.94
4+60			5.3	174.94
5+00			5.3	174.94
5+35			7.7	172.54
#1	0.80	168.14 ✓	12.90	167.34 ✓ Rock
5+55			1.4	166.74
6+00			5.2	162.94
6+50			8.4	159.74
6+75			9.5	158.64
7+00			3.6	164.54
7+15			4.0	164.14
7+28			5.7	162.44
#	0.21	155.71 ✓	12.64	155.50 ✓ Rock
7+60			4.3	151.4
7+75			5.8	149.9
8+20			6.0	149.1
8+29			9.9	145.8
8+27.08 = Int sewer line in Park: Bottom				
#	10.49	156.53 ✓	9.67	146.04 ✓ = 8+27.08 Pine stub in Bottom of wash Switzer Canyon
Flow line M.H. to the N.E. N°1			7.28	149.25
Center of M.H. Cover N°1			2.25	154.28
#	3.26	149.30 ✓	10.49	146.04 ✓ 8+27.08 Stub
Flow line M.H. to the S.W. N°3			12.08	137.22
Center of M.H. Cover. " N°3			7.33	141.97
#	11.57	160.80 ✓	0.03	149.27 ✓

	+	℄ 160.84	−	Elc
				"A" Line:
#	11.34	171.78 ✓	0.40	160.44 ✓ Rock
#	12.68	184.28 ✓	0.18	171.60 ✓ Rock
#	11.54	195.63 ✓	0.19	184.09 ✓ Rock
#	12.11	207.34 ✓	0.90	195.23 ✓ Rock
#	12.30	219.43 ✓	0.21	207.13 ✓ Rock
#	11.04	230.47 ✓	0.00	219.43 ✓ Rock
#	8.01	234.58 ✓	3.90	226.57 ✓ Rock
#			1.71	232.87 = 232.94 ✓ B.M.



	+	℄	−	Elc	
	5.49	151.53			146.04 See page 60
	Flow line M.H. N°2			11.30	140.23
	℄ Cover " " "			5.47	146.06

"B" Line:

	0.44	167.78		167.34 Rock see Page 60
0+00 "B" = 5+90 "A"			4.40	163.68 = Pine stub
0+38 Top bank drain flowing to right			8.5	159.3
0+40 Bottom " " " "			10.9	157.9
0+42 Top bank " " " "			8.4	159.4
0+75			8.4	159.4
1+00			10.2	157.6
1+20 Bottom of above drain flowing 7° left.			10.0	153.8
1+40			9.7	158.1
1+65			10.9	156.9
#	0.49	156.18	12.09	155.69 Rock
1+90			4.2	152.0
2+30			6.9	149.3
2+66.9 = Manhole N°2 Center Cover			10.11	146.07 ✓ See above 146.06

Note: Think "B" Line is best in spite of it crossing the drain twice.
Mr Brems
If you can find any place where the damned brush is any higher or thicker or has more thorns - page 45

"B" line used

J.H. 8/10/27

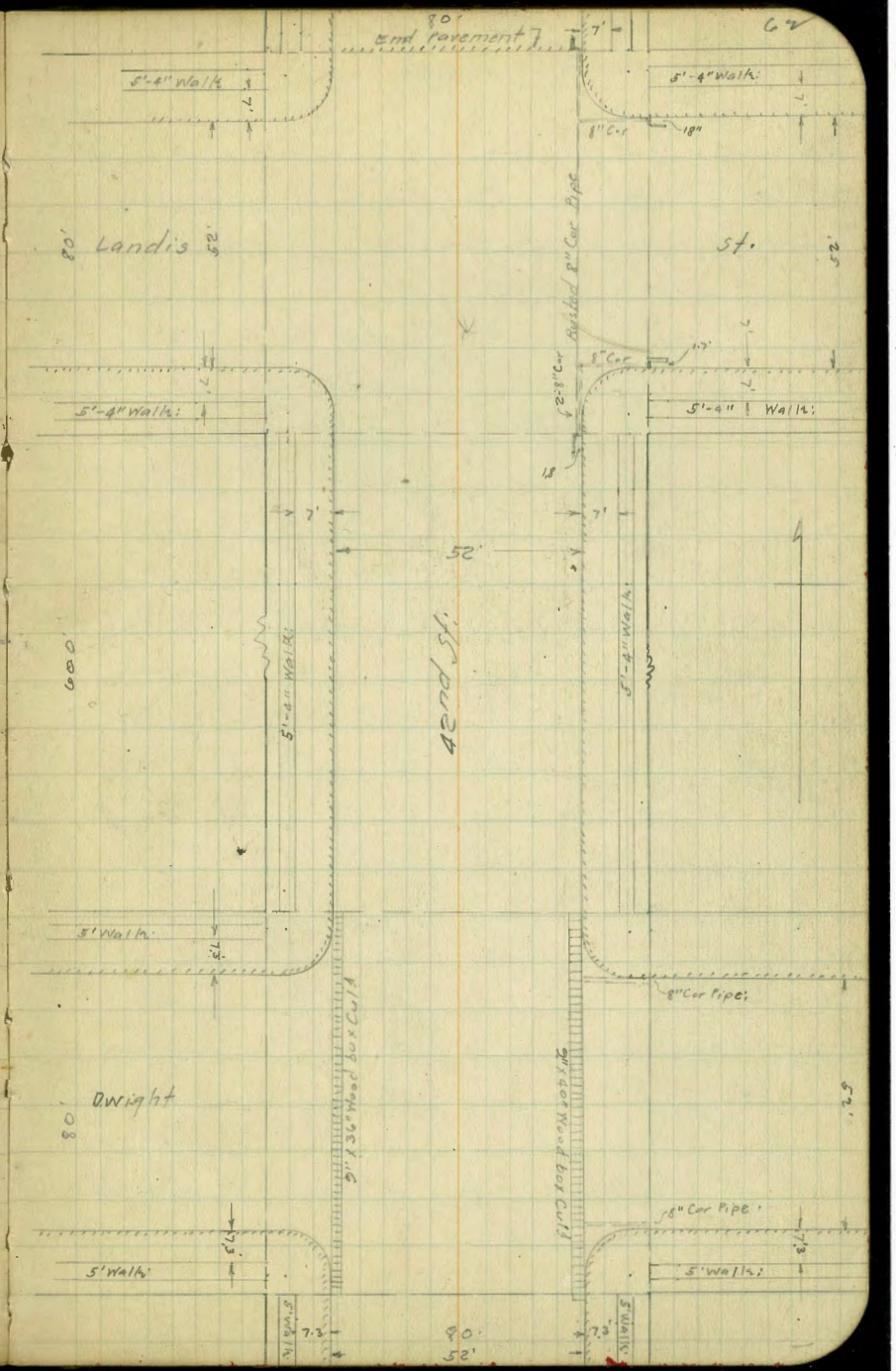
Xsection of 42nd St from Landis to Thorn:

Sep 8th 27

Flood
Bichet
Donnan:

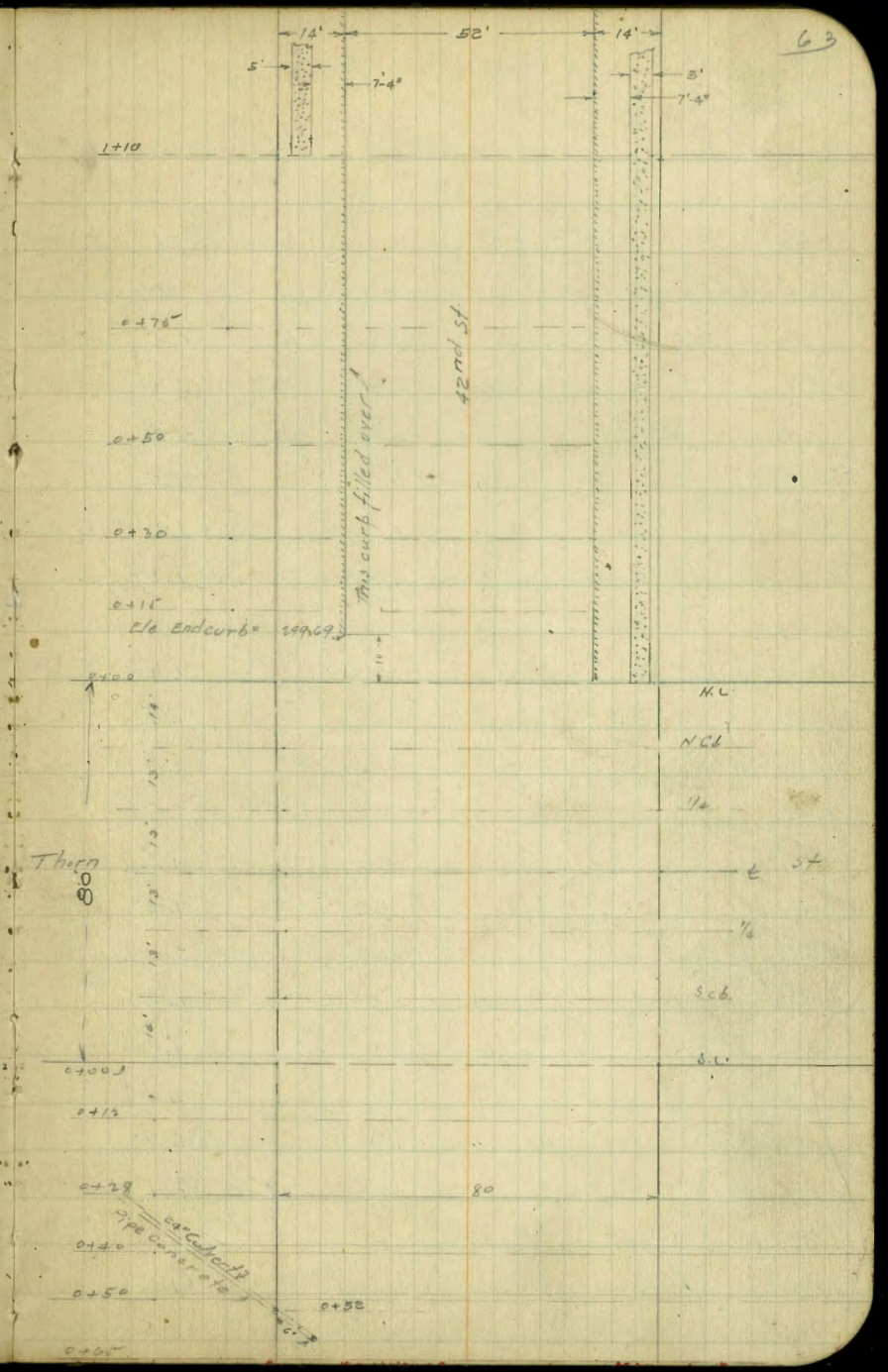
	+	℄	−	Ele
#	1.95	354.52		352.57 B.P.N.W Copeland and Klaubert, 42nd & Wightman;
#	2.26	347.98	8.80	345.72 curb;
#			5.62	342.36 B.P.N.W 42nd & Landis;

Null and Void: Slip called for this but then you never can tell:
See next page:



	+	π	−	Ele:	
42nd at Thorn: See page 67					
#	0.98	322.60		321.62	N.W. B.P. 42nd and Myrtle:
#	0.94	311.74	11.80	310.80	Rock:
#	1.47	305.49	7.72	304.02	End Sidewalk East Cor.
0+00 = N.L. of Thorn St:					
W.L. -15			5.7	0.3	
W.C.			5.5	0.0	
cb			5.7	0.3	
1/a			5.0	0.5	
℄			4.7	0.8	
1/a			4.9	0.7	
cb on end concrete cb			5.22	0.27	
Cb on ground			4.6	0.9	
on end of sidewalk			5.00	0.44	
E.L. ground			4.7	0.8	
0+15					
E curb; gutter flush			4.93	0.56	
1/a			4.3	1.2	
℄			4.7	0.8	
1/a			5.0	0.5	
cb on concrete			5.41	0.58	
cb " Ground			5.1	0.4	
W.L.			5.0	0.5	
W.L. +15 on Thorn st slope:			10.1	94.4	
0+30					
W.L. -30 Toe slope of Thorn st:			22.9	82.6	
W.L. -25 Toe " Thorn and 42nd.			22.1	82.4	

Plotted Sept 14-27



+	π 30ft. 49	−	Ele	80' St.
			42nd St	
W.L.		5.3	0.2	
+2		4.3	1.2	
+11		4.0	1.5	
cb on concrete curb		4.73	0.76	
gutter on ground		5.0	0.5	
+5		4.4	1.1	
1/4		4.9	0.6	
℄		4.7	0.8	
1/2		4.9	1.1	
E Cb on concrete: gutter flush:		4.42	1.07	
0+50				
E Cb on Concrete		3.72	1.47	
gutter		4.1	1.4	
1/4		4.2	1.3	
℄		3.7	1.8	
1/4		4.2	1.3	
+10		4.3	1.2	
cb on concrete		4.08	1.41	
cb " ground		3.6	1.9	
+12		3.9	1.6	
W.L.		5.1	0.4	
W.L +20		24.6	80.9	
W.L +40		28.4	77.1	
0+75				
W.L -40		24.0	81.5	
W.L -25		20.0	85.5	

+	π 30ft. 49	−
W.L.	5.4	0.1
+8	2.7	2.8
cb on concrete	3.12	2.37
cb " ground	2.2	3.3
1/2	3.2	2.3
℄	3.6	1.9
1/2	3.3	2.2
gutter	3.1	2.4
E cb on concrete	2.84	2.65
1+10 see sketch: North end of sections:		
E Curb on concrete	1.66	3.83
gutter	2.0	3.5
1/2	2.2	3.3
℄	1.9	3.6
1/2	2.1	3.4
cb on concrete	1.76	3.74
" " ground	1.8	4.0
End of walk, east side of same	1.97	4.02
W.L.	1.9	4.1
W.L +12	6.6	98.9
W.L +25	14.3	91.2
Intersection of 42nd and Thorn:		
North curb of Thorn St:		
E.L.	5.1	0.4
+4	5.2	0.3
+5	8.7	96.8

	+	π	−	Elε	80' St.
		305.49			
				42nd St	
cb			12.0	93.5	
+12			4.0	01.5	
1/4			4.3	01.2	
℄			5.0	0.5	
1/4			5.2	0.3	
cb			6.2	99.3	
+7			5.6	99.9	
W.L.			5.8	99.7	
			North 1/2 Thorn St		
W.L.			5.7	99.8	
+3			4.6	0.9	
+9			11.2	94.3	
cb			11.6	93.9	
+4			11.7	93.8	
+10			6.8	98.7	
1/4			7.0	98.5	
+4			6.2	99.3	
℄			6.5	99.0	
+10			7.7	97.8	
1/4			6.7	98.8	
+2			7.0	98.5	
+3			18.3	87.2	
cb			16.5	89.0	
+3			16.1	89.4	
+8			10.3	95.2	
E.L.			8.3	97.2	

	+	π	−	Elε	65
		305.99			
E.L+20			4.9	0.6	
			℄ Thorn St.		
E.L-20			6.2	99.3	
E.L-13			6.8	98.7	
E.L.			14.8	90.7	
cb			21.0	84.5	
+9			20.7	84.8	
1/4			20.0	84.5	
+2			13.9	91.6	
℄			11.6	93.9	
1/4			10.4	95.1	
+9			11.6	93.9	
+11			16.6	88.9	
cb			16.6	88.9	
+3			11.8	93.7	
W.L.			5.6	99.9	
W.L+10			6.4	99.1	
			S 1/2 of Thorn St		
W.L.-15			6.5	99.0	
WL-8 on Rock pile			4.7	0.8	
W.L.			7.2	97.8	
+7			10.7	94.8	
cb			14.0	91.5	
+2			17.6	87.9	
+9			18.2	87.3	
1/4			16.6	88.9	

	+	π 305.49	−	Ele	80'St:
				42nd St	
℄			18.4	87.9	
1/4			19.3	86.2	
+3			19.5	86.0	
+5			24.3	81.2	
cb			23.4	82.1	
+3			23.0	82.5	
E.L.			16.5	89.0	
+11			8.0	97.5	
+20			6.0	99.5	
Scurb Thorn St:					
E.L-20			7.7	97.8	
E.L-10			8.4	97.1	
E.L.			14.2	91.1	
+2			19.7	85.8	
+10			22.8	82.7	
cb			23.1	82.4	
+5			24.4	81.1	
+6			27.5	78.0	
1/2			28.8	76.7	
+2			24.8	80.7	
℄			25.2	80.3	
+11			22.7	82.8	
1/2			20.5	85.0	
cb			16.3	89.2	
W.L.			9.7	95.8	
W.L. +15			6.9	98.6	

	+	π 305.49	−	Ele:	44
S.L. Thorn St					
W.L. -15			6.9		98.6
W.L.			8.2		97.3
cb.			14.8		90.7
+8			19.9		85.6
1/4			22.0		83.5
+4			23.0		82.5
+8			30.4		75.1
℄			29.7		75.8
+7			31.1		74.4
1/2			29.7		75.8
+6			24.1		81.4
cb			22.6		82.9
E.L.			14.6		90.9
E.L +12			9.5		96.0
E.L +20			8.2		97.3
			0+12		
E.L-20			8.4		97.1
E.L-10			11.2		94.3
E.L			15.9		89.6
#	2.80	295.53	12.76	292.73 Rock:	
+6			9.1		86.4
cb			10.9		84.6
1/4			14.3		81.2
+14			17.4		78.1
℄			22.2		73.3

	+	⊼ 29√.53	−	Ele	80'St.
					42nd St
E+3			23.8	71.7	
+6			22.8	71.7	
1/4			12.8	82.7	
+8			8.1	87.4	
C6			5.4	90.1	
+10			1.2	94.3	
W.L.			1.3	94.2	
W.L +15			2.1	93.4	
	0+28				
W.L -15			12.3	83.2	
W.L.			11.7	83.8	
C6			12.8	82.7	
1/4			15.2	80.3	
+4			27.0	68.5	
E			26.0	69.5	
+3			17.4	78.1	
1/4			13.9	81.6	
C6			10.5	85.0	
E.L.			6.1	89.4	
E.L +10			1.9	93.6	
	0+40				
E.L -10			3.8	91.7	
E.L.			6.7	88.8	
C6			11.1	84.4	
1/4			14.0	81.5	
E			19.3	76.2	

	+	⊼ 29√.53	−	Ele	67
+3			20.7	74.8	
+4			27.7	67.8	
1/4			28.8	66.7	
+7			28.8	66.7	
+9			28.9	66.6	
C6			26.4	69.1	
+7			24.0	71.5	
+12			19.5	76.0	
W.L.			20.0	75.5	
W.L +20			21.5	74.0	
	0+60				
W.L -20			24.0	71.5	
W.L -3			25.5	70.0	
W.L.			28.9	66.6	
+8			30.4	65.1	
C6			30.0	65.5	
+7			28.7	66.8	
1/4			25.2	70.3	
E			19.6	75.9	
1/4			15.1	80.4	
C6			12.2	83.3	
E.L.			8.0	87.5	
E.L. +10			5.8	89.7	
	0+65				
E.L -10			9.5	86.0	
E.L.			11.8	83.7	

	+	π 29√√3	−	℄ℓe 42nd St	80' St.
℄b			14.7	80.8	
½			16.8	78.7	
℄			20.7	74.8	
½			26.4	69.1	
℄b			31.4	64.1	
W.L			30.√	65.0	
W.L +10			29.7	66.3	
W.L +20			26.8	68.7	
Flow line 24"con Culvert			32.3	62.2	

Note: Cul ⅔ full of dirt but functions

#	12.45	305.18	E.80	292.73	Rock
#	12.45	316.48	1.15	304.03	End sidewalk
#	9.23	325.37	0.49	315.99	Rock
#			3.67	321.65 = Initial B.M. 321.62	

X See Alley Blk 65 Park Villas 10-10-27 Miller

15' wide Myrtle to Dwight Bet 28th & Pershing Ave

				S.E. Dwight	
B.M.	9.64	333.69		324.01	& Pershing Ave
	00 = S. Line Dwight				
W			4.27		cmt cl
W			4.41		pavmt
C			4.55		Pavmt
E			4.13		pavmt
E			3.64		cmt cl
		5' S.			
E			3.3		
C			3.C		
W			3.8		
		25' S			
W			4.0		
C			3.6		
E			2.9		
		50' S			
E			3.8		
C			4.2		
W			4.4		
			+ Fence		

From 50'S. to 100's. cmt wall on E. 0.5 in Alley at 30.S. on Line at 100' S.

		100' S.			
W			4.5		
C			4.4		
E			3.7		
			333.49		
		150' S.			
E				3.9	
C				4.0	
W				4.2	
		200' S			
W				3.9	
C				3.5	
E				3.5	
		250'S			
E				2.8	
C				3.1	
W				3.2	

290' S. double gar apr on W cmt floor 6' Back

W-L				3.2	
W				2.7	
C				2.6	
E				2.6	
T.P.	4.44	335.61		2.52	331.17
		330'S			
— 2				4.7	
E				4.4	
E				4.2	
W				4.5	
		365'S			
W				4.5	
C				4.3	
E				4.3	

335.41

400' S.

E	4.4
C	4.7
W	4.7

443.5' garage on E cmt floor 5' Back

W	5.2	
+2	4.6	
E	4.8	
E	4.5	
+1 edge cmt apron	4.5	
+5	4.2	floor

492' S garage on E 5' Back

E-5	4.7	
E	4.9	
C	4.8	
+5	4.8	
W	5.5	

510' S

W	5.6	
+1	5.6	
+1.5	4.6	fence
C	4.7	
E	4.7	

3

335.41

Alley 65 Park Villas

70

540' S

E	3.9
C	4.7
+5	5.0
W	5.4

560' S garage on W cmt floor 3.3 Back

W-33	5.3	floor
W	5.3	
C	4.9	
E	4.7	

590.5

E	4.8	
C	5.3	
W	5.2	

599.5 = N. Line Myrtle

W	5.70	cmt el.
C	5.7	
E	5.35	cmt el.

T.P.	1.62	331.36	5.87	329.74
T.P.	3.23	326.57	8.02	323.34

X Sec Alley Blk 71. Park Villas — 10-18-27 Miller

Myrtle to Upas Bet Pershing Ave & Villa Terrace — 15' wide

326.57 H.I. Page 70

00 = S. Line Myrtle.

E		2.9	323.7	
C		3.1	323.5	
W		3.4	323.2	
32'.5. garage on E emt floor				
W		3.8	322.8	
C		3.4	323.2	
E		3.2	323.4	
+1.5		2.9	323.7.	emt apron
+7.5		2.4	324.2.	floor
74'.5. garage on E emt floor				
-7.5		2.4	324.2.	floor
-1.0		3.1	323.5.	emt apron
E		3.7	322.9	
C		4.0	322.6	
W E?		4.2	322.4	
91'.5. garage on E emt floor				
W		4.8	321.8	
C		4.3	3223	
E		3.3	323.3	
+0.5		3.1	323.5.	apron
+9		2.7	323.9.	floor

326.57

115'.5

E		4.2	322.4
C		4.8	321.8
W		5.0	321.6

1435. to 152'.5 shed on E. 1.8 in alley

165'.5

W		5.8	320.8
C		5.2	321.4
E		5.0	321.6

175'.5 to 187'.5 shed on E 1.5' in alley

200'.5

E		6.1	320.5
C		6.5	320.1
W		6.9	319.7

213'.5. to 225'.5 Wood garage on E dirt floor 1.5 in alley

225'.5

W-5		8.6	318.0
W		8.3	318.3
+2		7.2	319.4
C		7.0	319.6
E		6.8	319.8

245'.5.

E		8.0	318.6
C		8.9	317.7
+6		9.1	317.5
W		9.7	316.9
+5		10.1	316.5.

326.57

269' N. = N. End 3 garages on W cmt floors 9.5 Back

W - 9.5		10.6	316.0	floor
W - 2.3		10.4	316.2	cmt apron
W		10.2	316.4	
C		9.4	317.2	
+4		8.9	317.7	
+5		8.4	318.2	
E		8.2	318.4	

300' S = S end above garages

E		9.2	317.4	
+3		9.4	317.2	
+4		10.3	316.3	
C		10.5	316.1	
W		11.1	315.5	
+2.3		11.1	315.5	cmt apron
+9.5		11.0	315.6	floor

330' S

W		10.9	315.7	
C		11.8	314.8	
+3		11.6	315.0	
+4		9.9	316.7	
E		9.7	316.9	

253' E

E		10.5	316.1	
+3		10.7	315.9	
+4		12.5	314.1	
C		12.7	313.9	

326.57

Alley Blk 71 Park Villas

72

W		12.6	314.0	

357.5 = N. Line 2 lpas.

W		12.93	313.64	cmt el
W		12.99	313.58	Paving
C		13.10	313.47	"
E		12.62	313.95	"
E		12.00	314.57	cmt el
T.P.	11.78	326.35	12.00	314.57
T.P.	5.79	331.41	0.73	325.62
			2.61	328.80 = 328.80

chkd on Bm S.E. 28" + 2 lpas

Plotted 11/1/27
H. McCarty

Survey of W. 50' of Lots 1 & 2 Blk D. Southlook.

11-12-27 Miller

For S. D. Fire Dept.

9-24-48 Hardin Allen Decker

N.E. 7.37
N.W. 5.07
2.30

S.E. 9.53

7.84
3.67
1.17

3.67
1.78
5.42

4.47

BM. Top Hydt S.E. Woolman 436'

Inside walk

64.27
2.63
66.90

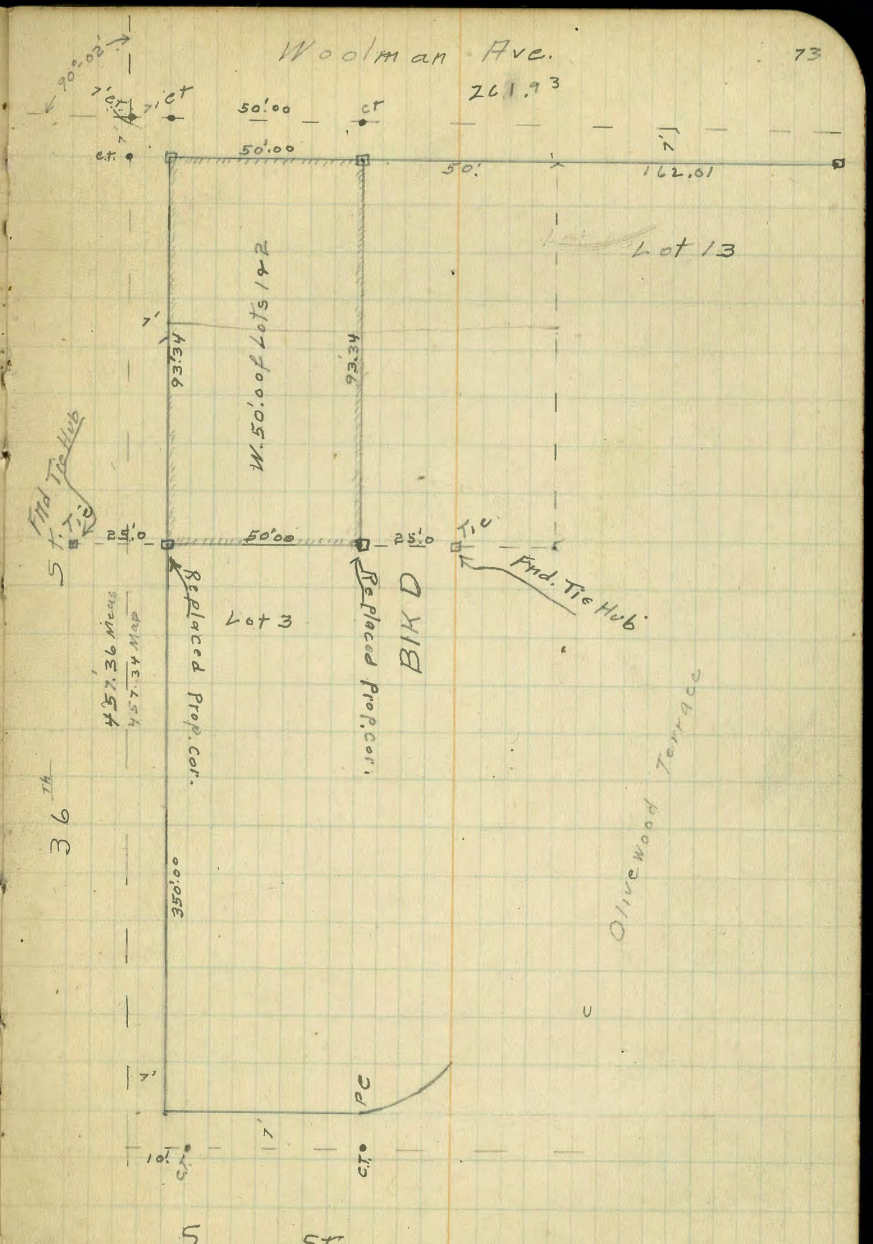
E. Drive 5.38 / 61.52 ℄ Door 5.13 / 61.77 W. Door 4.86 / 62.04 Prop Line 4.70 / 62.20 ct 4.90 / 62.00 grade

E. Door gutter 1.30 / 60.60

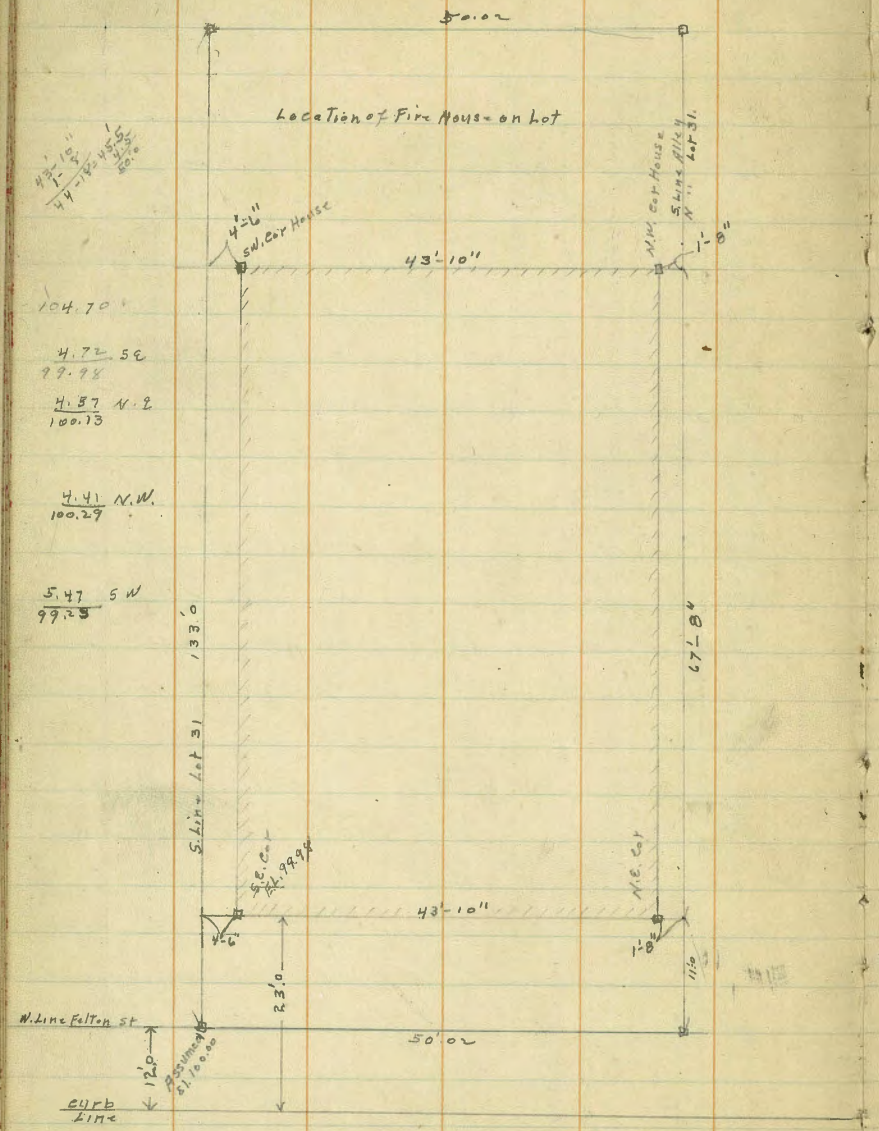
W. Door gutter 5.83 / 61.07

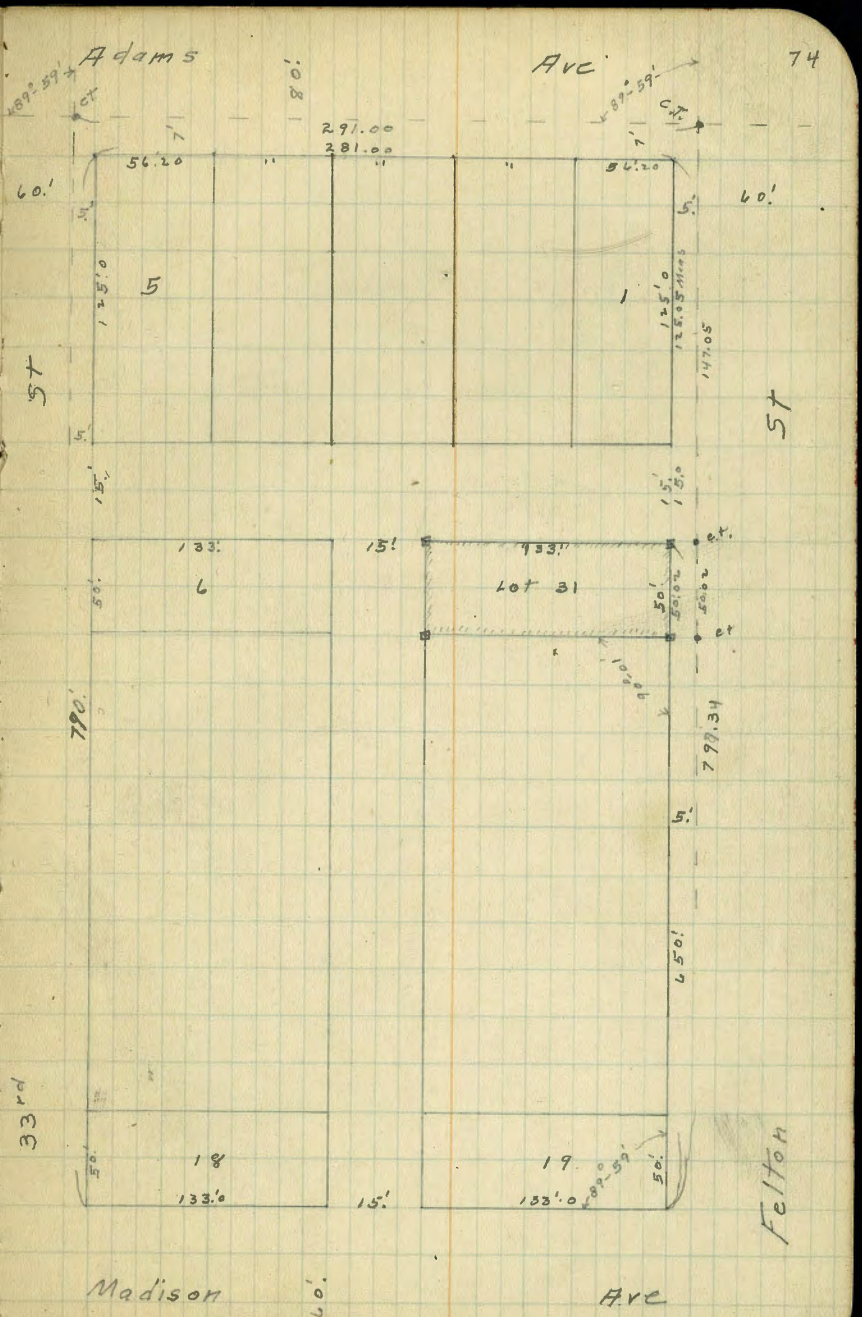
36.57 Gutter 36.44 S.F. Prop Line 5.70 / 61.20

Floor Elev est.	N.W.	N.E.	S.E.	S.W.
	62.00	62.00	62.00	62.00
	4.90	4.90	4.90	4.90
	4.50	6.65	9.18	6.11
	+0.40	-1.75	-4.24	-1.21
64.27	N.W.	N.E.	S.E.	S.W.
1.40	62.00	62.00	62.00	62.00
65.67	3.67	3.67	3.67	3.67
	1.64	4.31	6.43	4.30
	+2.103	-0.64	-2.76	-0.63



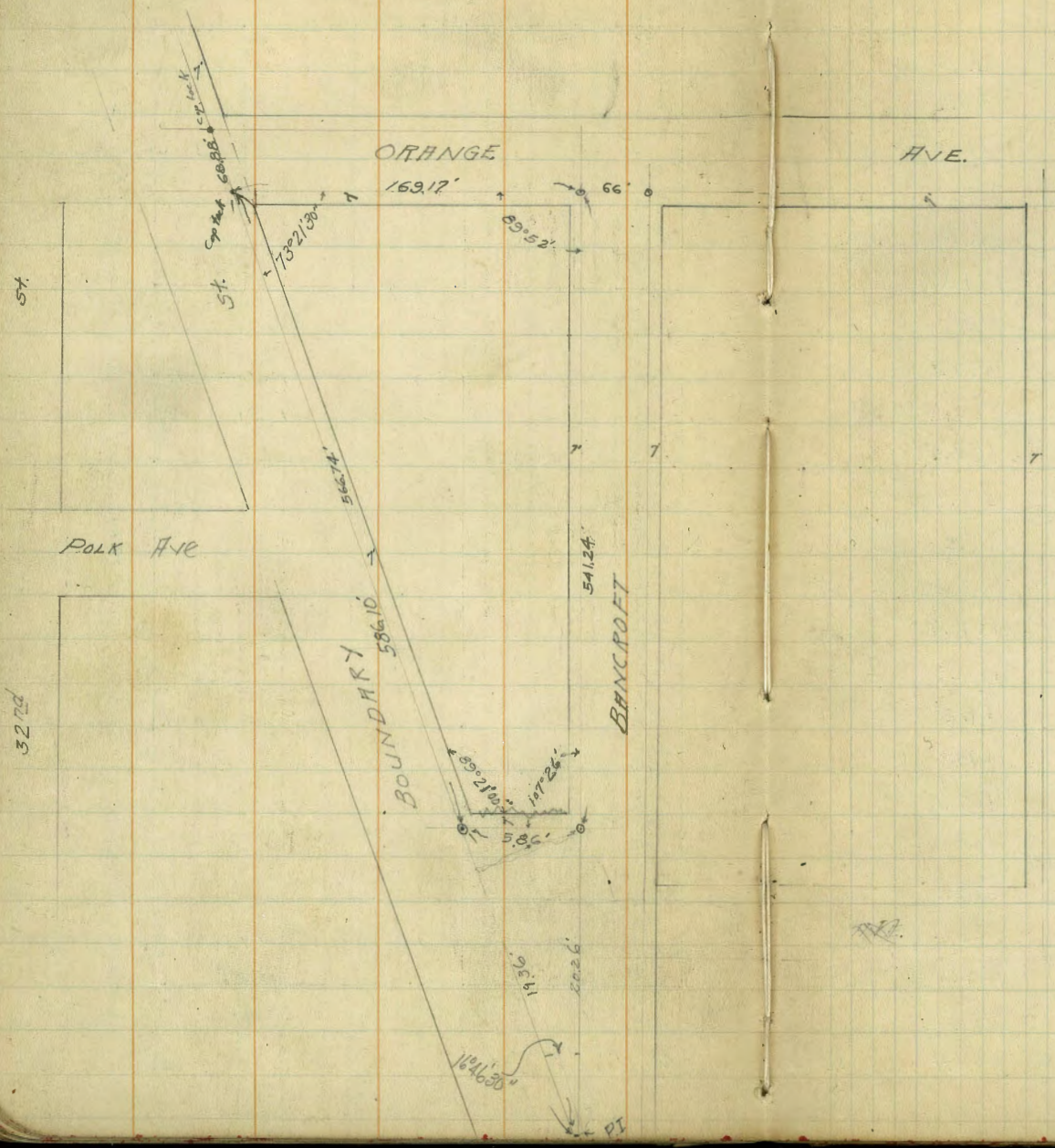
Survey of Lot 31 - Blk. 61. 11-14-27 Mills
Resub. of Blks. 39 & 56 Normal Hts.
For S.D. Fire Department.





Stalker
Ruplinger
Shea
1-12-28

THE POINTS
AS PER SKETCH

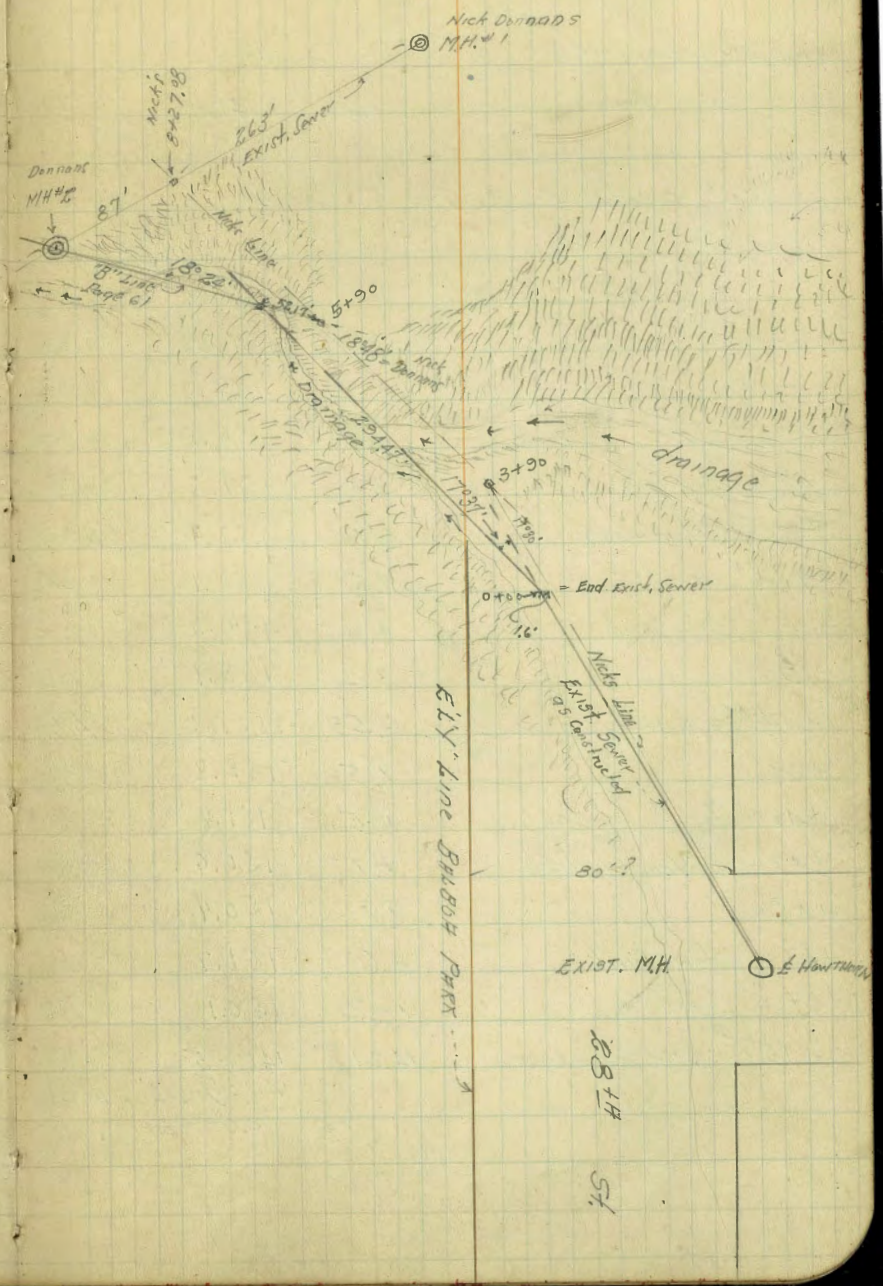


Walker Preliminary Levels Map 10-24-88

PRELIM. LEVELS for Line as Located on opposite Page

			Elev. cut Stob	
	1.05	186.19		185.14
0+00			5.00	181.2
+20			5.2	181.0
+40			11.5	174.7
+58			12.6	173.6
+71	Note. 0+76 = ℄ Wash from East drains about 3' Stocks		14.6	171.6
T.P.	1.01	175.60	11.60	174.59
1+00			3.8	171.8
+28			4.8	170.8
+55			6.4	169.2
+82			7.3	168.3
2+17			10.6	165.0
T.P	1.72	165.28	12.04	163.56
2+30 on top Bank of ditch			2.6	162.7
+32 = Bottom ditch			4.0	161.3
+36 = " "			4.0	161.3
+40 = top Bank			3.0	162.3
+48 (ditch 5' Rt.)			2.7	162.6
+63 = top Bank of ditch			4.7	160.6
+65 = Bottom of ditch			6.5	158.8
+76 = " " "			7.1	158.2
+78 = top Bank			6.0	159.3
2+9447 = Δ Lt. 18°24'			5.97	159.31
Nicks "B" Line Page 61 0+75			5.9	159.4 on Ground
TP	1.09	153.57	12.80	152.48

Prelim. Location Sewer As Per. sketch



Chk. on Flow Line MH #2	13.32	140.25
" " Cover Page 61	7.52	146.05
		146.07 = Nicks
		0.02 = difference

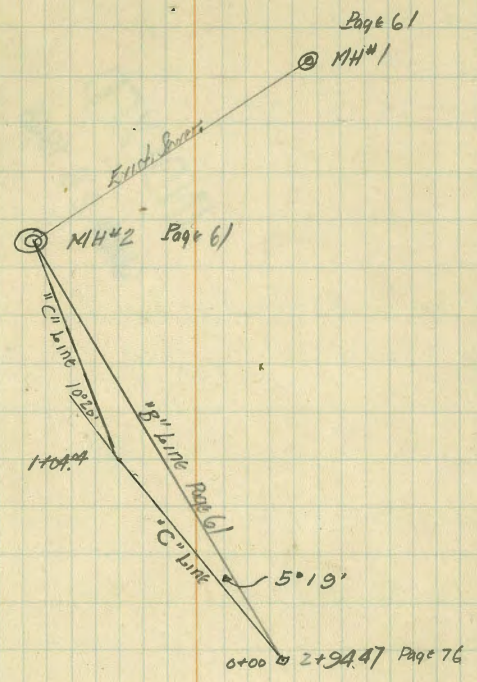
Walker 10-24-28

LEVELS For "C" Line

			Sta 2+94.47	
	0.95	160.76	159.31	Page 76
0+00		0.95	159.31	2+94.47
+25		0.8	159.5	3+19.47
+55		3.8	156.5	3+49.47
+67 = top Bank		5.8	154.5	3+61.47
+70 = Bottom ditch		6.9	153.4	3+64.47
+75 = " "		7.2	153.1	3+69.47
+78 = top Bank		6.0	154.3	3+72.47
+90		5.2	155.1	3+84.47
1+04.04 = △ Rt. 10°20'		6.53	153.73	on Stub. 3+98.51
+26		7.5	152.8	4+20.47
+40 = top Bank at ditch		8.5	151.8	4+34.47
+42 = Bottom of ditch		9.7	150.6	4+36.47
+45 = " " "		9.9	150.4	4+39.47
+47 = top Bank		8.6	151.7	4+41.47
+67		10.2	150.1	4+61.47
2+15.35 = ℄ MH #2 on Cover		14.21	146.05	5+09.82
			146.05 = Cover Above	
			0.00 = Error.	

Prelim.

Location sewer Line as per sketch.



Traeger

Grade Stakes for 100' of 6" V.C. Sewer - N. of M.H in Adams - along ℄ of Felton

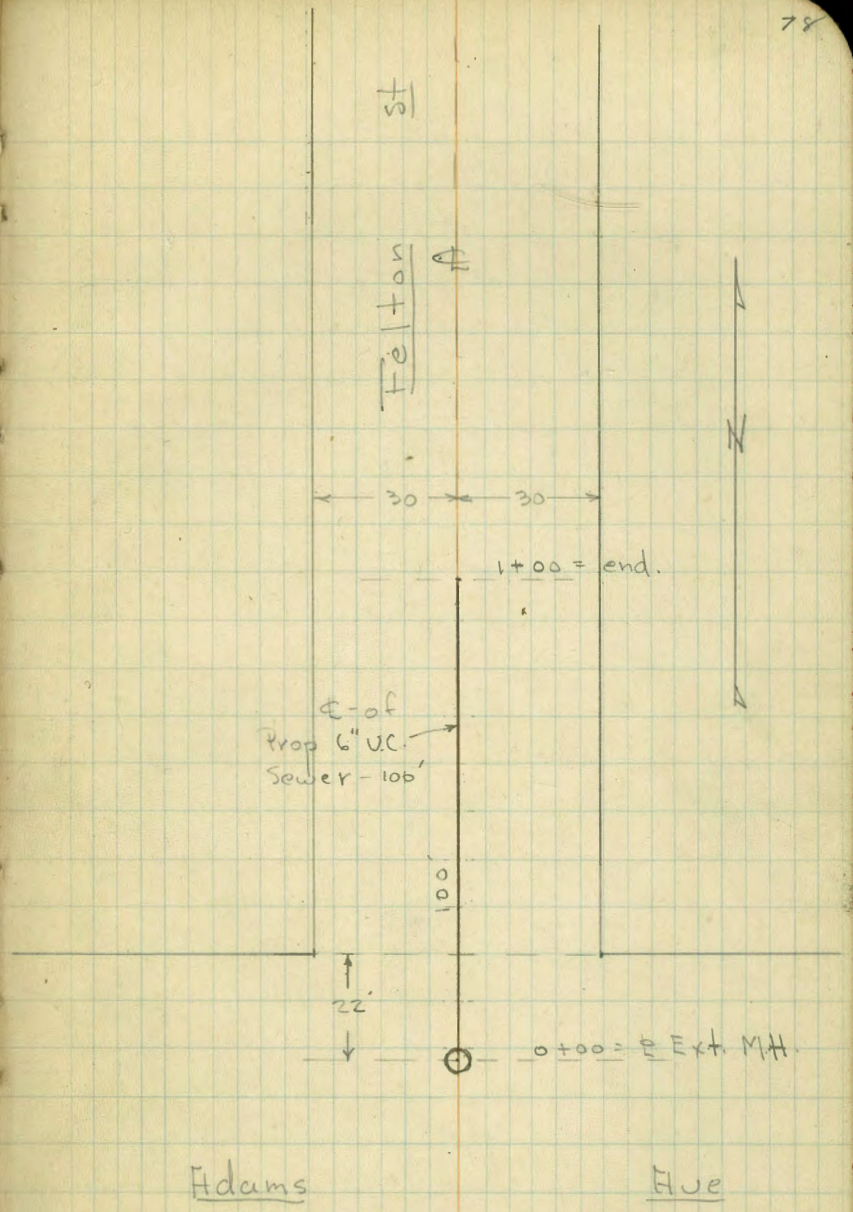
1-23-48

W.O. 60231

7.0

B.M.	4.13	393.38	389.25	SW. 34 ± ℄ Adams

		Grade	
Roof. Nails - 4' Rt.			
0+00 = ℄ Ext. M.H.	on Rim 5.02 / 88.36	375.00	= Ext. F.L.
0+00 = F.L. of Drop	88.36	380.40	C 7.96
+25	4.92 / 88.46	80.95	7.51
+50	4.82 / 88.56	81.50	7.06
+75	4.75 / 88.63	82.05	6.58
1+00 = End.	4.74 / 88.64	382.60	C 6.04



IMPROVED TABLES
AND
INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.