

117A

EDS

FIELD BOOK

No. 385

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300 Eddie

Advised to 77

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5124
61021
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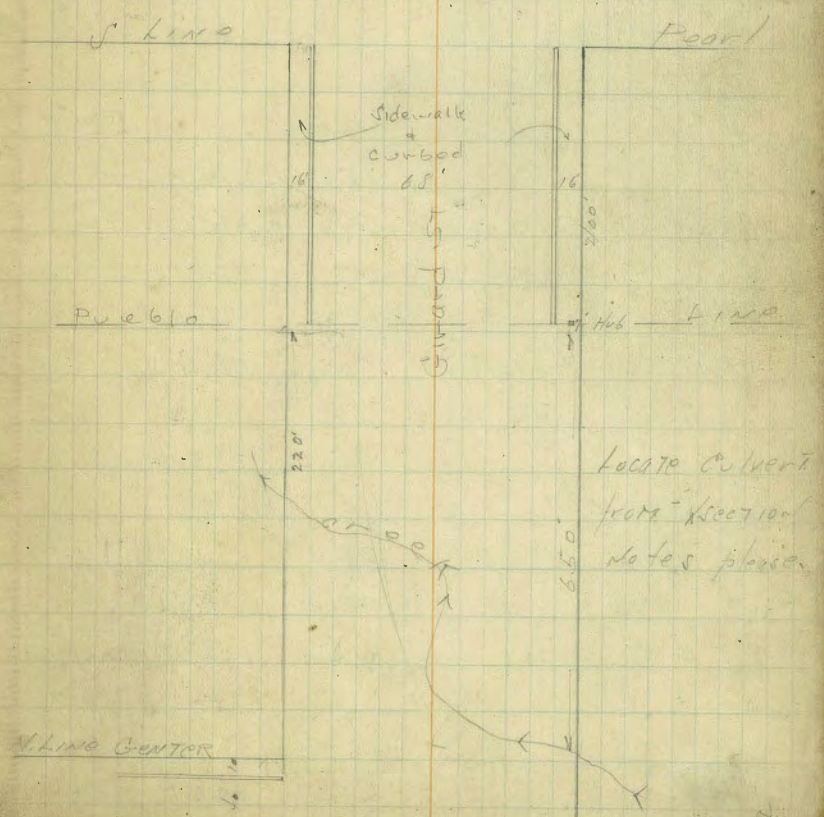
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GIRARD ST. Cross Section
 Part to Center
 100' wide
 15' curb
 17' 17 1/2' curb
 Part to Girard

SEBP	12.82	127.88	115.05
T.P.	12.60	140.44	0.0
100' S. of Part to Pueblo line = 0.0			
w		10.4	130.0
cb	tap	10.46	129.98
put		10.9	129.5
1/4		10.7	129.7
e		10.5	129.9
1/4		10.9	129.5
put		11.0	129.4
cb	11.11	10.4	130.00
E		10.3	130.1
0+50			
E		8.7	131.7
cb		8.7	131.7
1/4		8.8	131.6
e		8.9	131.5
1/4		8.9	131.5
cb		8.6	131.8
w		8.3	132.1
1+00			
w		5.7	134.7
cb		5.7	134.7
1/4		5.8	134.6
e		6.4	134.2
1/4		6.3	134.1

Plotted by Tolman 2-25-27.



120.44

cb	6.4	134.0
E	6.2	134.2
1+25		
E	5.3	135.1
cb	5.1	135.3
1/4	5.1	135.3
c	5.1	135.3
1/4	4.4	136.0
cb	4.6	135.8
w	5.5	134.9
1+40		
-10	9.2	131.2
w	8.4	132.0
cb	5.1	135.3
1/4	2.7	136.7
c	4.2	136.1
1/4	4.3	136.1
cb	4.2	136.2
E	4.5	135.9
2+00		
E	1.1	139.3
cb	0.6	139.8
1/4	2.2	138.2
c	1.3	139.1
1/2	2.4	138.0
43	4.0	136.4

140.44

Barard

cb	5.2	135.1	
w	6.7	133.7	
+10	6.7	133.7	
2+10			
-10	8.0	132.4	
w	6.4	134.2	
+13	5.4	135.0	
cb	7.8	132.6	
+2	4.7	135.7	
+10	4.3	136.1	
1/4	1.2	139.2	
c	1.0	139.4	
+5	2.7	137.7	
1/4	2.1	138.3	
+10	0.0	140.4	
T.P. 1077	151.05	0.16	140.48
cb	10.5	140.6	
E	10.7	140.4	
2+20			
E	11.5	139.6	
cb	10.4	140.7	
+9	10.5	140.6	
1/4	12.6	138.5	
c	12.8	137.3	
+6	11.6	139.5	
1/4	11.8	139.3	

15/05

1/4 + 3	12.1	139.0
48	14.6	136.5
+ 13	15.3	135.8
cb	18.4	133.9
w / Middle creek	19.3	131.8
+ 10	19.3	131.8
2 + 53		
- 10	15.1	136.0
w /	15.1	136.0
+ 10	15.2	135.9
cb	12.2	138.9
+ 3	11.5	139.7
1/4	11.2	139.8
+ 5	13.5	137.6
c	13.6	137.5
+ 1.2	13.3	137.8
1/5	11.6	139.5
+ 6	9.4	141.7
cb	8.7	142.4
E	9.0	142.1
v + 70		
E	8.5	142.6
cb	8.1	143.0
+ 9	8.5	142.6
1/4	10.8	140.3
C	13.2	137.8

15/05

Girard

1/4	13.7	137.4
+ 4	11.4	139.7
cb	11.0	140.1
w /	9.8	141.3
3 + 00		
v /	8.7	142.4
cb	9.4	141.7
1/4	9.5	141.6
+ 13	12.3	138.8
c	14.2	136.8
1/4	12.4	138.7
cb	9.7	141.4
E	9.0	142.1
3 + 50 = 7 + 50 Book 1446 p. 69		
E	9.2	141.5
cb	9.9	141.2
1/4	10.3	140.8
C	8.7	142.4
1/4	6.2	142.9
cb	6.0	145.1
w /	6.0	145.1
3 + 57		
w / # corr walk 3 inside	5.55	14.550 corr line
3 + 75		
w /	4.6	146.5
cb	4.8	146.3

157.05

1/4	5.7	145.4
1/2	6.5	144.6
2	8.2	142.9
+9	9.1	142.0
1/2 creek	11.4	139.7
+4	9.1	142.0
cb	9.7	141.4
E	8.6	142.5
✓ 4+05		
E	7.4	143.7
+5	9.8	141.3
cb	9.3	141.8
+10	9.8	141.3
1/4	7.6	143.5
2	7.3	143.8
+8	7.1	144.0
+11	8.9	142.2
1/2	7.1	144.0
+8	4.2	146.6
cb	3.8	147.3
w	3.8	147.3
4+25		
w	3.4	147.9
cb	4.2	146.9
+7	5.7	145.4
+14	7.0	144.1

151.05

Girard

1/4	6.3	144.8
+4	6.0	145.1
17 creek	8.7	142.4
+12	5.6	145.5
2	5.6	145.5
+16	5.9	145.2
1/4	7.2	143.9
+3	5.8	145.3
+8	6.0	145.1
+10	9.8	141.3
cb	9.8	140.3
+10	8.5	142.6
E	4.9	146.2
TP 9.6	158.66	2.0
4+50		149.04
E	11.3	147.2
cb	13.0	145.7
+5	13.1	145.6
+7	16.6	142.1
1/4	17.1	141.6
+2	13.2	145.5
+12	13.0	145.7
25		
C creek	16.6	142.1
+5	13.6	145.1
+10	13.0	145.7
1/4	13.1	145.6

15866

1/11		11.8	146.9
cb		10.1	148.6
w		9.8	148.9
	4+25		
w		8.0	150.7
cb		8.2	150.5
1/4		9.3	149.2
+7		11.5	147.2
✓ c		11.8	146.9
+10		12.0	146.7
212		12.2	146.5
+15		16.0	142.7
1/4	Creek	16.0	142.7
+5		15.4	143.3
+9		11.9	146.8
cb		11.4	147.3
E		10.2	148.5
	5+25		
E		9.0	149.7
cb		8.8	149.9
+10		9.8	148.9
+11		11.7	147.0
+15		12.5	146.2
1/4		15.7	143.0
+9	Creek	15.3	143.4
+11		9.6	149.1

15866

Girard

5

✓ c		9.8	148.9
+8		8.5	150.3
1/4		6.5	152.2
+5		5.8	152.9
cb		5.8	152.9
w		5.4	153.8
	5+50		
w		4.5	154.2
cb		5.2	153.5
+10		5.4	153.3
1/4		7.8	150.9
+1		12.0	146.7
+3	Creek	12.7	146.0
✓ c		14.3	144.4
+6		9.2	149.3
1/4		8.6	150.1
cb		8.7	150.0
E		8.6	150.1
TP	7.8	16.2.48	4.03 154.63 Meter bar
	5+75		
E		7.4	155.1
cb		9.2	153.3
1/4		11.4	151.1
+8		11.2	151.3
+13		11.8	150.7
✓ c		10.7	151.8

162.48

10 + 5		10.8	151.7
+ 6		16.2	146.3
+ 10	creek	16.0	146.5
1/4		15.2	147.3
+ 12		8.1	154.4
cb		7.9	154.6
w/		8.2	154.3
	6+00		
w/		7.2	155.1
cb		6.5	156.0
+ 12		6.6	155.9
1/4		8.5	154.0
+ 13		10.6	151.9
+ 15		11.7	147.8
✓ e	creek	11.7	147.8
+ 8		11.7	147.8
+ 11		10.1	152.4
1/4		9.7	152.8
cb		9.2	153.3
+ 4		8.8	153.7
E		5.3	157.2
	6+25		
E		6.6	155.9
cb		9.2	153.3
+ 3		11.1	153.1
+ 1		11.1	146.1

162.48

Girard 6

+ 14 creek		11.1	148.1
+ 15		10.2	152.3
1/4		10.0	152.5
✓ e		9.2	153.1
+ 10		8.8	153.7
1/4		5.3	157.2
cb		5.2	157.1
w/		5.5	159.0
	6+44		
w/		4.7	157.8
cb		4.5	158.0
1/4		4.0	158.5
✓ e		5.9	156.6
1/4		8.2	154.2
+ 15		8.8	153.7
cb		11.1	151.1
+ 6		13.6	148.9
+ 14 creek		13.9	148.6
E		8.8	153.7
	6+50		
E	creek	13.8	148.7
+ 5		13.8	148.7
+ 7		8.2	154.3
cb		5.3	154.2
1/4		6.8	155.7
✓ e		4.8	157.7

165.78

1/4			3.8	158.7
cb			4.1	158.4
w/			4.5	158.0
	6+60			
w/			5.2	158.3
cb			3.5	158.7
1/4			3.2	159.3
c			4.0	158.5
T.P.	5.74	165.13	3.07	159.41
1/4			7.4	157.7
+10			10.5	154.6
cb			10.6	154.5
E			10.6	154.5
+5	creek		16.6	148.5
	6+75.4 = NL	Center		60' width
-5			11.4	153.7 10' cds
E			10.0	155.1 10' cds
+6			8.0	157.1
cb			7.0	158.1
1/4			5.8	159.3
c			5.5	159.6
1/4			5.5	159.6
cb			6.3	158.8
w/			6.4	158.7
	n/cb			
w/	top cem. cb.		6.31	158.82

165.79

Cinard

w/	for ydps		6.9	158.2
cb			6.0	159.1
1/4			5.5	159.6
c			5.4	159.7
1/4			4.8	160.3
+7			5.6	159.5
cb			7.1	158.0
E			8.5	156.6
	n/1/4			
E			7.4	157.7
cb			6.7	158.4
+7			4.8	160.3
1/4			4.4	160.7
c			5.0	160.1
1/4			5.2	159.9
cb			5.4	159.7
w/			6.3	158.8
	♀			
w/			5.9	159.2
cb			5.3	159.8
1/4			5.0	160.1
c			4.5	160.6
1/4			4.1	161.0
cb			5.0	160.1
E			7.4	157.7

16513

S 1/4

E		7.5	157.6
+10		4.7	160.4
cb		4.0	161.1
1/4		3.8	161.3
✓ C		4.3	160.8
1/4		4.9	160.2
cb		5.6	159.5
w/		6.4	158.7
f cb			
w/	top cent cb	5.5	159.8 ✓
w/	10go	6.4	158.9
cb		5.6	159.5
1/4		4.4	160.7
✓ C		3.6	161.5
1/4		3.3	161.8
cb		2.9	162.2
E		3.9	161.2
SL			
E		2.4	162.7
cb		2.4	162.7
1/4		3.3	161.8
e		3.6	161.5
1/4		4.3	160.8
cb		5.1	160.0
w/		5.3	159.8

Girard

7

16513
~~157.1~~
~~157.4~~
 0.66
 153.08
 4.97
 148.11

148.11 ✓ SETop Hyd
 Fay & Genter

0.03 error
 (terrible!!)

X Section Brant St. 50' wide 10' cbs.
 From N.L. Nutmeg St N to P.C. as shown in sketch
 Also Olive St. from E.C. East

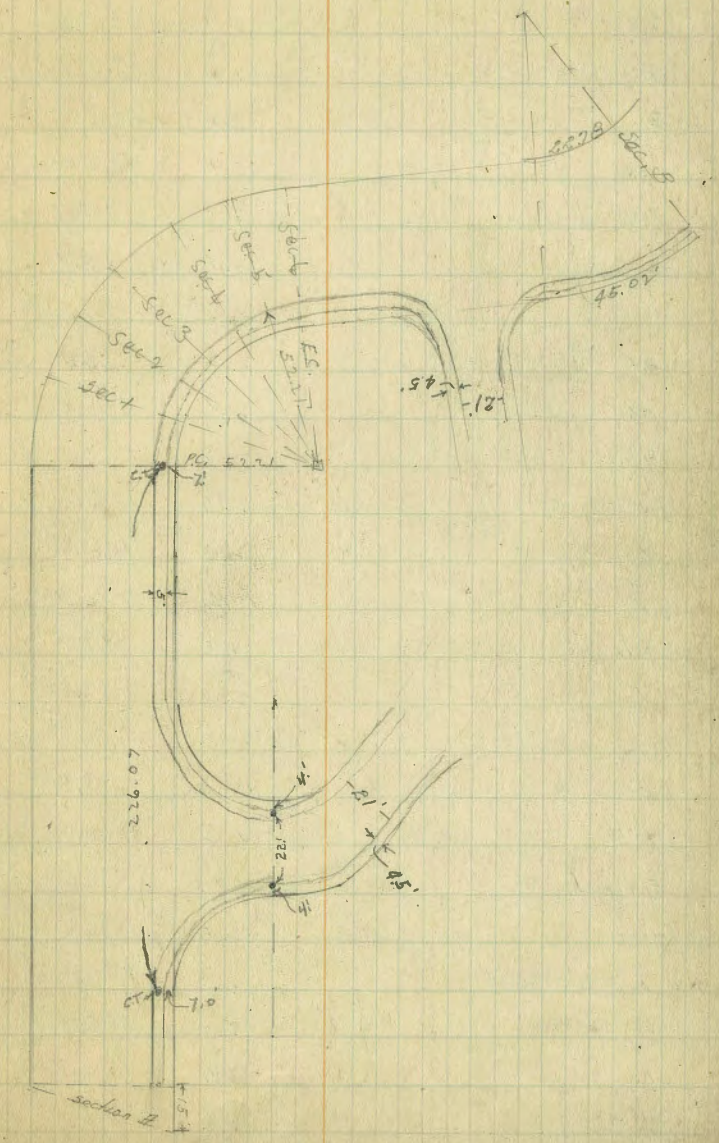
1.25 188.50 187.24
 Nail in Pole
 See sketch
 111 - Page 4

Section #1

to	5.8	182.7
+5	5.2	183.3
+7	9.0	179.5
cb.	8.2	180.3
+5	5.0	183.5
$\frac{1}{4}$	4.8	183.7
$\frac{1}{4}$	4.7	183.8
$\frac{1}{4}$	4.4	184.1
cb.	5.0	183.5
+2	3.8	184.7
N	3.4	185.1

N.L. Nutmeg

N	3.4	185.1
cb.	4.0	184.5
+2	4.4	184.1
$\frac{1}{4}$	4.0	184.5
$\frac{1}{4}$	3.5	185.0
$\frac{1}{4}$	3.5	185.0
Gut	3.8	184.7
E top cb.	2.67	185.86
E	2.9	185.6
30' N		
to	1.6	186.7



Nutmeg St.

186.53

186.53

9

E topcb	2.22	186.31
out	3.1	185.4
$\frac{1}{4}$	2.9	185.6
$\frac{1}{4}$	2.9	185.6
$\frac{1}{4}$	3.0	185.5
cb	3.5	185.0
+2	2.8	185.7
N	2.8	185.7
	50' N	
N	2.4	186.1
cb	2.1	186.1
+2	2.9	185.6
$\frac{1}{4}$	2.5	186.0
$\frac{1}{4}$	2.3	186.2
$\frac{1}{4}$	2.4	186.1
cb	2.5	186.0
E	2.3	186.2
	101' N	
E	0.0	186.5
+5	1.6	186.9
E topcb	1.72	186.81
Gut	2.5	186.0
$\frac{1}{4}$	2.3	186.2
$\frac{1}{4}$	2.0	186.5
$\frac{1}{4}$	2.2	186.3
+5	2.7	185.8
cb	2.0	186.5

N	2.2	186.3	
T.P. 5.94	192.54	1.95	186.58
	110' N		
-15	9.6	182.9	
-13	9.2	183.3	
-10	7.1	185.4	
N	5.9	186.2	
cb	6.2	186.3	
+1	6.6	185.9	
$\frac{1}{4}$	6.0	186.5	
$\frac{1}{4}$	5.9	186.6	
$\frac{1}{4}$	6.2	186.3	
Gut.	6.5	186.0	
E topcb	5.68	186.84	
+5	5.5	187.0	
E	3.6	188.9	
	150' N		
E	3.5	189.0	
+5	5.3	187.2	
topcb	5.4	187.12	
Gut.	6.5	186.0	
$\frac{1}{4}$	5.9	186.6	
$\frac{1}{4}$	5.5	187.0	
$\frac{1}{4}$	5.6	186.9	
cb	6.3	186.2	
+2	5.5	187.0	

N	5.6	186.9
+1	5.6	186.9
+5	9.3	183.2
+10	10.4	182.1
+12	12.1	180.4
+15	12.1	180.4

157' N

-15	13.0	179.5
-12	13.0	179.5
-10	11.0	181.5
-5	9.8	182.7

N	5.6	186.9
+9	5.6	186.9
cb	6.2	186.3
$\frac{1}{2}$	5.7	186.8
$\frac{2}{4}$	5.5	187.0
$\frac{1}{4}$	5.8	186.7
Gut	6.2	186.3
E top cb	5.29	187.23
E	4.8	187.7

220' N

E	4.3	188.2
E top cb	4.85	187.67
Gut	5.7	186.8
$\frac{1}{2}$	5.4	187.1
$\frac{2}{4}$	5.2	187.3
$\frac{1}{4}$	5.4	187.1

cb	5.8	186.7
+2	5.2	187.3
+8	5.4	187.1
N	6.4	186.1
+5	10.8	181.7
+9	12.6	179.6
+15	14.7	177.8

247' N

-15	19.0	173.5
-12	14.6	177.9
-6	12.3	180.2
N	7.2	185.3
+3	4.9	187.6
+8	4.7	187.6
cb	5.5	187.0
$\frac{1}{2}$	5.3	187.2
$\frac{2}{4}$	5.0	187.5
$\frac{1}{4}$	5.2	187.3
Gut	5.2	187.3
cb	4.62	187.90
E	4.0	188.5

248' N

E	4.0	188.5
top cb	4.61	187.91
Gut	5.2	187.3
$\frac{1}{2}$	5.2	187.3

19252

L	5.0	187.5
$\frac{1}{4}$	5.3	187.2
cb	5.5	187.0
+2	4.9	187.6
+7	4.9	187.6
N	7.2	185.3
+6	12.6	179.9
+12	14.3	178.2
+15	16.2	176.3
+17	25.2	167.3
+25	25.8	166.7
261' N = PC.		
-25	26.3	166.2
-17	26.2	166.3
-12	15.2	177.3
-6	12.7	179.8
N	8.3	184.2
+4	4.9	187.6
cb	4.9	187.6
+1	5.4	187.1
$\frac{1}{4}$	5.1	187.4
$\frac{1}{2}$	4.8	187.7
$\frac{1}{4}$	4.9	187.6
Gut	5.0	187.5
E top cb	4.52	188.0
E	4.1	188.4

19252

11

Section 1

E	3.7	188.6
E top cb	4.03	188.49
Gut	4.9	187.6
$\frac{1}{4}$	4.5	188.1
$\frac{1}{2}$	4.3	188.2
$\frac{1}{4}$	4.6	187.9
+5	4.9	187.6
cb	4.2	188.5
+5	4.4	188.1
N	8.6	183.9
+5	13.0	179.5
+15	15.5	177.0
+17	26.3	166.2
+25	26.5	166.0

Sec. B

-25	26.7	165.8
-17	26.3	166.2
-15	17.4	175.1
-9	15.7	176.8
-7	13.0	179.5
N	8.5	184.0
+7	3.8	188.7
cb	3.8	188.7
+1	3.7	188.8
+2	4.5	188.0

192.52

$\frac{1}{4}$	4.1	188.4
$\frac{1}{2}$	3.7	188.8
$\frac{3}{4}$	4.0	188.5
Gut	4.6	187.9
E top cb	3.62	188.90
E	3.4	189.1

Sec. 3

E	3.0	189.5
E top cb	3.20	189.32
Gut	4.1	188.4
$\frac{1}{4}$	3.7	188.8
$\frac{1}{2}$	3.3	189.2
$\frac{3}{4}$	3.5	189.0
25	3.9	188.6
cb	3.3	189.2
+3	3.3	189.2
W	8.5	184.0
+18	20.6	171.9
+25	21.3	171.2

Sec. 4

-25	22.7	170.3
W	4.8	187.7
+4	24	190.1
cb	28	189.7
+1	34	189.1
$\frac{1}{4}$	29	189.6

192.52

12

$\frac{1}{4}$	2.8	189.7	
$\frac{1}{2}$	3.3	189.2	
Gut	3.7	188.8	
E top cb	2.81	189.71	
E	2.6	189.9	
T.P. 8.27	198.49	2.30	190.22

Sec. 5

E	7.9	190.6
E top cb	5.20	190.29
Gut	9.1	189.4
$\frac{1}{4}$	8.5	190.0
$\frac{1}{2}$	8.1	190.4
$\frac{3}{4}$	10	190.2
cb	8.5	190.0
+1	8.0	190.5
+8	7.8	190.7
W	9.1	189.4
+20	24.9	173.6

Sec. 6 = EC

-20	12.7	172.8
W	7.2	191.3
cb	7.1	191.4
+1	7.6	190.9
$\frac{1}{4}$	7.4	191.1
$\frac{1}{2}$	7.4	191.1
$\frac{3}{4}$	7.7	190.8

19849

Gut	84	190.1
E top cb.	7.47	191.02
Fo	7.1	191.4
28' E of E.C.		
S	5.1	193.4
S top cb.	5.70	192.79
S Gut	6.6	191.9
S 1/2	6.0	192.5
L	5.6	192.9
1/4	5.8	192.7
cb.	5.9	192.6
+2	5.6	192.9
N	6.7	191.8
+10	11.6	186.9
45' E		
-10	6.0	192.5
N	4.1	194.4
+8	4.4	194.1
cb.	4.9	193.6
1/4	4.7	193.8
L	4.4	194.1
1/2	4.6	193.9
Gut	5.5	193.0
S top cb.	4.39	194.10
S	3.9	194.6

60' E

19849

15

S	2.7	195.9	
S top cb.	3.18	195.31	
Gut	4.0	194.5	
1/4	4.6	193.9	
L	5.3	195.2	
1/2	3.5	195.0	
+6	4.0	194.5	
cb.	3.4	194.9	
N	2.9	195.6	
100' E			
T.P. 11.87	21913	0.25	198.29
N	10.1	200.0	
+2	11.4	198.7	
cb.	14.0	198.1	
1/4	11.7	198.4	
L	11.5	198.6	
1/2	11.7	198.4	
Gut	12.1	198.0	
S top cb.	11.28	198.85	
S	11.1	199.0	
150' E = R.C.			
S	7.3	202.8	
S top cb.	7.48	202.45	
Gut	8.1	201.4	
1/4	8.5	201.6	
L	8.1	202.0	

$\frac{1}{2}$		25	201.6
cb.		9.0	201.1
+3		8.2	201.9
N		7.9	202.2
	Sec. B		
N		6.6	203.5
cb.		7.1	203.0
$\frac{1}{2}$		6.4	203.7
$\frac{1}{2}$		6.2	203.9
$\frac{1}{2}$		6.4	203.7
Gut		6.8	203.3
S = Existing cb. on S		6.67	203.46
S		6.3	203.8
T.P.	9.92 212.15	0.90	209.23
chk. on B.M. Mon. Palm + H/batross		4.47	214.68
			214.76 = B.M.
			+ 0.08

Darker
6-2-27

7. Section 9th St. 50' wide 10' deep
From N.W. 10th to N.W. Robinson Ave
(See sketch page 16)

262.39

15

STAMP			
Unit 1 10th	0.37	262.39	262.02
	0-18 = section on top 109		
Rt on Paving	6.80	275.59	
+9 = 1/8 Catch Basin ^{30' Curved Iron} on First line Pt	13.01	69.38	
cb on top of Gate & Ck Basin	6.97	75.47	
1/2 " " Paving	6.74	75.65	
1/2 " " "	6.39	76.00	
1/2 " " "	6.11	76.28	
cb " " "	5.86	76.53	
Left " " "	5.48	76.91	
	0-18 on top cb		
cb " " "	4.97	77.47	
cb " " "	5.21	77.18	
1/2 " " "	5.41	76.98	
1/2 " " "	5.60	76.79	
1/2 " " "	5.80	76.59	
cb " " "	5.18	76.51	
Rt. " " "	5.81	76.58	
	0-5		
Rt	5.3	77.1	
cb	5.6	76.8	
1/2	5.3	77.1	
1/2	5.5	76.9	
1/2	5.6	76.8	
cb	4.8	77.6	

Plotted
9/11-1927
D.S.P.

Lt.	4.6	277.8
	0+00	
Lt.	4.9	77.5
cb	5.4	77.0
1/2	7.0	75.4
1/2	7.3	75.1
1/2	8.0	74.4
cb	7.7	74.7
+4	7.6	74.8
+6	5.4	75.0
Rt.	5.3	75.1
	0+10	
Rt.	10.3	72.1
+4	15.3	67.1
cb	16.2	66.2
1/2	14.1	68.3
1/2	13.3	69.1
1/2	13.0	69.4
cb	13.6	68.8
Lt.	12.1	70.3
+5	12.1	70.3
T.P. 222	2/963	1208
	269.31	
	0+28	
-5 = top Rt. Wall	+2.0	68.2
-5 at bottom of Wall	3.8	66.4
Lt.	3.8	66.4

See Page 35 + See Page 59.

Cross in City Walk on East 7' line 8th and South 7' line Robinson Ave
8th St.

9th St.

Sec I

□ = 2" x 2" REDWOOD Hubs.

Robinson Ave

9076

879

9039

1035

1199

1199

199.61

186.51

153.31

153.51

101.25

101.25

101.25

101.25

101.25

101.25

101.25

101.25

101.25

101.25

101.25

101.25

101.25

ONE SIDE

Change here

PLACE

10th St.

8th St.



Curve 1
Chords = 23.43
R = 400.07
ST = 7.97
Curve 2

Curve 3
Chords = 20.01
R = 300.07
ST = 5.97
Curve 4

Curve 5
Chords = 20.01
R = 300.07
ST = 5.97
Curve 6

Curve 7
Chords = 23.10
R = 375.07
ST = 6.46

Curve 8
Chords = 20.01
R = 300.07
ST = 5.97

Curve 9
Chords = 20.01
R = 300.07
ST = 5.97

Curve 10
Chords = 20.01
R = 300.07
ST = 5.97

Curve 11
Chords = 20.01
R = 300.07
ST = 5.97

Curve 12
Chords = 20.01
R = 300.07
ST = 5.97

RIGHT SIDE

Place

10th St.

27023

cb	7.8	262.4
1/2	8.3	61.9
3/4	8.9	61.3
1	11.3	58.9
+4	14.1	56.1
cb	14.4	56.0
+6	11.0	59.2
+7	9.1	61.1
Rt.	9.1	61.1
+10	5.7	64.5

0437

-15	6.1	64.1
Rt.	11.7	58.5
cb	13.6	56.6
1/2	12.7	57.5
1/4	14.3	57.9
1/2	11.8	58.4
cb	8.9	61.3
lt.	5.1	65.1
+5 at Ret. Wall	4.1	66.1
+5 on top "	+1.5	71.7

0493

-6 = top Wall	0.0	70.2
-6 = Bottom of Wall	5.3	64.9
lt.	7.7	62.5
cb	10.0	60.2

27023

1/2	13.3	256.9
1/4	15.6	54.6
1/2	15.0	55.2
cb	15.5	54.7
Rt.	14.2	55.8
+15	8.6	61.6
T.P. 084	26213	894 261.79

16.1 in face SW
Cor. oneida pl
+ 9.3 St.

Note: beginning at station 0423 on left there is 11 Eucalyptus trees 7.5' apart
"3" dia, 10' tall, 2" ^{50'} in St.

1+12.67 = E.l. oneida place $\left. \begin{array}{l} 4.75' \text{ cbs} \\ 7.17' \text{ 1/2} \end{array} \right\} \text{ see sketch}$

-15	1.7	60.4
Rt.	7.2	54.9
cb	7.8	54.3
1/2	7.6	54.5
1/4	7.6	54.5
1/2	7.4	54.7
cb	4.4	57.7
lt.	0.8	61.3
+5 = Bottom Ret. Wall	+1.2	63.3
+5 = top " "	+7.0	69.1

E. cb line oneida pl.

lt.	1.7	60.4
cb	3.4	56.9
1/4	7.4	54.6
1/2	7.4	54.5
1/4	7.8	54.3

866.13

cb	80	254.1
Rt.	73	54.8
+10	35	58.6
	54	
-10	97	58.4
Rt.	73	54.8
cb	81	54.0
$\frac{1}{2}$	81	54.0
$\frac{1}{2}$	77	54.4
$\frac{1}{2}$	70	55.1
cb	45	57.6
Lt.	09	61.2
	8	
bt.	09	61.7
cb	44	57.7
$\frac{1}{2}$	68	55.3
$\frac{1}{2}$	81	54.0
$\frac{1}{2}$	83	53.8
cb	85	53.6
Rt.	79	54.2
+10	43	57.8
	84	
-10	49	57.2
Rt.	84	53.9
cb	86	53.5
$\frac{1}{2}$	85	53.6

868.13

8	84	253.7
$\frac{1}{2}$	66	55.5
cb	39	58.2
bt.	05	61.6
	Wcb.	
Lt.	05	61.6
cb	41	58.0
$\frac{1}{2}$	71	55.0
$\frac{1}{2}$	86	53.5
$\frac{1}{2}$	88	53.3
cb	87	53.4
Rt.	85	53.6
+10	60	56.1
	Ylume oneida #1 = 0+00	
-10	62	55.9
Rt.	89	53.2
cb	89	53.2
$\frac{1}{2}$	91	53.0
$\frac{1}{2}$	89	53.2
$\frac{1}{2}$	71	55.0
cb	40	58.1
Lt.	07	61.9
T.P. 0.13	202.17 084	261.79
PC = $\frac{1}{2}$ Euc. Tree ^{on lat} 12" diam. 40' tall 6' in st.		
Lt.	+0.3	62.4
+6 at tree	2.0	60.1

cb.	38	258.3
$\frac{1}{4}$	40	56.1
8	10.1	52.0
7	9.5	52.6
cb	9.5	52.6
Rt	9.4	52.7
+15	5.6	56.5

PC + 20' on left = 2 Euc. tree 10' diam 40' tall 9.5' inst.

PART 1

-15	7.3	54.8
-5	10.3	51.8
Rt	10.3	51.8
cb	10.3	51.8
$\frac{1}{2}$	11.1	51.0
+5	12.9	51.2
cb line	9.6	52.5
$\frac{1}{4}$	6.5	55.6
cb.	3.5	58.6
Lt.	0.0	62.1

R = + 1.0

PART 1 + 5' on left = 2 Euc. tree 3' back 16' dia. 50' tall

R = 0.4 61.7

PART 2 = 2 Euc. tree on left 12' dia. 45' tall 1.5' back

R = 4.8 57.3

" " + 7' " " " 9' inst. 4.8 10' dia. 30' tall

R = 10 61.1

" " + 15' " " " 2' back cluster of 7 trees approx 5' dia 45' tall

R = 6.0 56.1

" " + 21' " " " 9' inst. " 3' " " 6' " 35' "

R = 15 60.5

" 3' + 3' " " " 3' back " of 7 tree " 6' " 10' "

R = 3.8 58.3

" " + 7' " " " on line = cluster of 4 trees " 5' " 35' "

R = 8.4 253.7

PC Curve # 2 + 6' = 2 Euc. tree on left 15' inst. cluster 2 trees 15' dia 45'

PART 2 Curve # 1

Lt.	1.1	61.0
cb	5.4	56.9
$\frac{1}{2}$	8.3	53.8
$\frac{1}{4}$	11.3	50.8
$\frac{1}{2}$	12.4	49.9
cb	11.8	50.3
Rt	7.4	50.7
7.8	11.5	50.6
+15	8.6	53.5

PART 3

-15	7.0	55.1
-5	12.3	49.8
Rt	12.1	50.0
cb	12.5	49.6
$\frac{1}{2}$	12.6	49.5
$\frac{1}{4}$	12.3	49.8
$\frac{1}{2}$	10.4	51.7
cb	7.0	55.1
Lt.	7.5	59.6

PART 4 = EC. Curve # 1

Lt.	9.4	54.7
$\frac{1}{4}$	10.8	51.3
$\frac{1}{2}$	13.4	48.7
$\frac{1}{4}$	13.5	48.6

26212

7	13.5	248.6
cb	13.4	248.7
RT	11.5	50.7
+15	6.6	55.5

PK. Curve #4

-15	6.3	55.8
RT	10.4	51.7
cb	13.3	48.8
7	14.0	48.1
8	13.7	48.4
7	13.8	48.3
cb	12.2	49.9
LT	7.2	54.9

Sec 1

LT	11.2	50.9
cb	14.7	47.4
7	15.3	46.8
8	15.1	47.0
7	15.1	47.0
cb	13.9	48.2
RT	11.6	50.5
+10	8.4	53.9

Sec 2

-15	13.3	48.8
RT	14.8	47.3
cb	14.5	45.6

26212

20

7	16.5	245.6
2	16.3	45.8
7	16.2	45.9
cb	14.2	47.9
LT	10.8	51.3
TP	7.1	251.53
	12.30	219.82

Sec 3

LT	1.3	53.2
cb	5.5	49.0
7	8.4	46.1
8	9.9	44.6
7	10.2	44.3
cb	10.2	44.3
RT	10.1	44.4
+20	8.6	45.9

Sec 4 = EC, Curve #6 = 0+00

-15	5.9	48.6
RT	11.3	43.2
cb	10.8	43.7
7	11.1	43.4
8	10.3	44.2
7	8.3	46.2
cb	6.7	48.3
LT	2.8	51.7

0+50

LT = East	8.0	46.5
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mt. Elmore
2100

cb.	10.8	43.7
$\frac{1}{2}$	12.7	41.8
2	12.7	42.1
$\frac{1}{4}$	12.7	42.1
cb	11.9	42.6
St. = West	10.2	44.3
+5	8.7	45.8

1+00

W-5	9.1	45.4
W	10.2	44.3
cb	13.1	41.4
$\frac{1}{4}$	14.1	40.4
8	14.1	40.4
$\frac{1}{2}$	13.7	40.8
cb	12.7	41.8
E	8.4	46.1

1+30

E	4.4	50.1
cb	5.1	46.4
$\frac{1}{4}$	12.3	42.2
2	13.5	40.0
$\frac{1}{2}$	14.5	40.0
cb	14.5	40.0
W	12.3	42.2
+5	10.5	44.0

1+50

-10	10.4	44.1
W	14.4	40.1
cb	14.6	39.7
$\frac{1}{4}$	14.7	39.8
2	15.0	39.5
$\frac{1}{2}$	12.8	41.7
cb	10.5	44.0
E	6.5	48.0

1+65

E	7.3	47.2
cb	12.0	42.5
$\frac{1}{4}$	13.3	41.2
8	15.1	39.3
$\frac{1}{2}$	15.0	39.5
cb	15.3	39.2
W	14.5	40.0
+10	11.1	43.4

1+99.61 on E = PL.

-10	15.5	39.0
W	15.6	38.9
cb	15.5	39.0
$\frac{1}{2}$	15.4	39.1
2	15.6	38.9
$\frac{1}{4}$	16.3	38.2
cb	15.1	38.7
E	13.9	40.6

T.P.	8.07	251.26	1129	243.14
	Section A	$cbs = 1.55'$	$\frac{1}{2}s = 7.78'$	$= 5218$
E-10		9.0	42.3	
E		10.6	40.7	
cb		13.0	38.3	
$\frac{1}{2}$		12.7	38.6	
$\frac{1}{2}$		12.4	38.9	
$\frac{1}{2}$		12.5	38.8	
cb		12.4	38.9	
W		12.6	38.7	
	Section B	$cbs = 1.04'$	$\frac{1}{2}s = 9.03'$	
N		12.6	38.7	
cb		10.3	41.0	
$\frac{1}{2}$		7.2	44.1	
$\frac{1}{2}$		3.7	47.6	
+6		1.3	50.0	
$\frac{1}{2}$		1.3	50.0	
cb		1.5	49.8	
+7		1.4	49.9	
+8		4.0	47.3	
+9		4.0	47.3	
S		+23	53.6	
	Sec. C	$= 7.74'$		
South W		51	46.2	
+26		45	46.8	
+46		13.7	37.6	

+77 = NE Prop.	12.3	38.0
NE +10	13.3	38.0
+25	9.5	41.8
Sec. D = 68.0'		
NE Prop = 35'	10.1	41.2
" " = 20	13.9	37.4
N " = 0+00	14.1	37.2
+23	14.2	37.1
+33	11.7	39.6
+41	7.2	44.1
+68 = SW Prop.	7.6	43.7
Sec. E = 78'		
SW Prop	9.3	42.0
+23	10.0	41.3
+33	12.8	38.5
+78 = NE Prop	14.8	36.5
NE +17	13.0	38.3
" +37	4.7	46.6
Sec. F = 54.1' = 109' cbs 8.17' $\frac{1}{2}s$		
NE	15.3	36.0
cb	14.6	36.7
$\frac{1}{2}$	12.8	38.5
$\frac{1}{2}$	12.1	38.2
$\frac{1}{2}$	11.5	39.8
cb	10.3	41.0
SW = E6 on South	9.5	41.8

Section G = 50' approx. 10' ch 7.5' ds

N	9.5	
cb	10.9	
1/2	11.6	
8	12.4	
1/2	12.8	
cb	12.8	
E	13.7	

This section
outSection 189 North of S.L. Robinson at Rt. Angle to N.W. 9th S^{outh} PC on N

E	17.8	38.6
cb	15.5	35.8
1/2	12.9	38.4
E	12.1	39.2
1/2	11.7	39.6
cb	9.5	41.8
N	9.5	41.8

T.P. 441 244.96 10.71 240.55

Section I = 0+00

N	4.4	40.5
cb	4.9	40.0
1/2	6.4	38.5
1/2	8.5	36.5
1/2	10.6	34.3
71	15.1	29.9
14	15.7	29.9
15	13.1	31.9

E	13.1	31.9
+15	13.1	31.9
	13.1	31.9
	0+5'	
20	12.7	32.3
E	14.7	30.3
cb	15.1	29.9
+1	13.5	31.7
1/2	12.4	32.5
1/2	11.3	33.6
1/2	6.9	38.0
cb	6.6	38.3
+3	5.3	39.6
N	4.7	40.2
	0+11	
N	4.7	40.2
+3	4.9	40.0
cb	4.9	40.0
1/2	5.3	39.6
1/2	12.7	32.2
+5	13.8	31.1
1/2	15.6	29.3
1/2	15.1	29.2
cb	14.6	30.3
E	13.0	31.9
+25	10.1	34.8

Marker
8.3.21

N. Section Robinson Hill 50' wide
From N. to 10th to E. to S. to S.F.
10' cbs
75' 4.5

28443

75

S.F. BP
Robinson + 10th 241 284.43 282.01

0400 = N. to 10th Section Parallel N. to S. 18' 2' 1/2

N	34	81.0
+5 = top cb	376	80.97
+5 = gutter on paving	403	80.4
cb on " "	393	80.5
1/4 " "	371	80.69
d " "	368	80.75
1/2 " "	373	80.70
cb " "	389	80.54
+5 " "	414	80.29
+5 on top cb	349	80.94
S	34	81.0

Plotted 8-11-27
CBH

04323 on North = A.P. - Sec A

S	44	80.0
cb	46	79.8
1/2	47	79.7
d	48	79.6
1/4	53	79.1
cb	51	79.3
N	50	79.4

sec. B

N	50	79.4
cb	53	79.1
1/4	53	79.1

1/2	50	79.4
1/4	50	79.4
cb	50	79.4
S	50	79.4

Section C
Note: Garage on South of Hill Sec. E Ent. 5V
10' 5" South of Hill 55

S	5V	79.2
S	55	78.9
cb	58	78.6
1/2	55	78.9
d	54	79.0
1/4	54	79.0
cb	53	79.1
N	50	79.4

14' N of Sec. C

N	5V	79.2
cb	58	78.6
1/4	62	78.2
1/2	60	78.4
1/4	60	78.4
cb	60	78.4
S	60	78.4

Section 1

S-10	87	75.7
S	100	74.4
cb	119	72.5
1/4	116	72.8
d	110	72.4

i	110	73.4
cb	7.5	76.9
ts	5.2	79.2
N	5.7	78.7
Section 2 = 52.80		
N	5.8	78.6
cb	9.6	74.8
z	12.2	72.2
z	13.8	70.6
z	13.4	71.0
cb	13.1	71.4
S	10.0	74.4
+10	8.7	75.7
Section 3 = 3.67 W of E.L. oneida Pl. ^{no' tree} ^{6' cbs} ^{7' z}		
-10	8.7	75.7
S	10.0	74.4
cb	13.5	70.9
z	15.1	69.3
z	15.6	68.8
z	15.1	68.3
cb	15.6	68.8
N	13.6	70.8
TP	29.8	74.29
E 1/2 oneida Pl. Rt Δ to Robinson		
N	1.0	66.7
cb	1.6	66.7

i	7.4	66.9
z	8.2	66.1
z	7.8	66.5
cb	4.1	68.2
S	2.6	71.7
+10	+1.0	75.3
E oneida Pl. Rt Δ to Robinson		
-10	1.6	72.7
S	4.9	69.4
cb	7.7	66.6
z	10.2	64.1
z	10.2	64.1
+5	10.6	63.7
z	9.4	64.9
cb	8.7	65.6
N	8.6	65.7
N 1/2 = E Luc. tree on South 10' in st. 8" dia 40' tall		
N	9.3	65.0
cb	9.6	64.7
z	10.3	64.0
z	13.7	60.6
z	14.0	62.3
cb at tree	10.1	64.2
S	6.9	67.4
+10	3.8	70.5
N cb = E Luc. tree 13' in st 10" dia 50' tall		

274.29

-10	5.8	68.5
S	9.7	64.6
cb	13.1	61.2
+3 = Base of tree	13.7	60.6
$\frac{1}{2}$	14.8	59.5
d	13.5	58.8
$\frac{1}{4}$	12.9	61.4
+2	10.5	63.8
cb	10.5	63.8
N	9.7	64.6

Y. l. oneida Pl. = 0400

N-5	6.6	67.7
N	10.2	64.1
+3	11.2	63.1
+5	12.6	61.7
+8	11.1	63.2
cb	11.1	63.2
+3	11.2	63.1
$\frac{1}{4}$	13.3	61.0
d	16.0	58.3
$\frac{1}{2}$	15.1	58.4
cb	13.4	60.9
S	10.7	63.6
+10	7.0	67.3

2' Y. l. oneida = E tree on S $R=15.3$ 15' inst 10' dia, 35' tall
 1' " " " " " " " $R=14.1$ 6' " " " " " " " 61' tall

274.29

27

0+10 = E tree on S 2' back $R=12.9$ 7" dia 40' tall	61.4
" " " " " 10' inst $R=16.0$ 5" " 30' "	58.3
TP 114 $R=12.9$ 261.20	58.4
0+16 = E tree on South $R=4.1$ 4' inst 9" dia 40' tall	59.6
0+20 = " " 2' back 5" dia 2.9	57.5
0+31 = " " 4' " 5" dia 5.0	53.1
" " = " " 6' inst 10' " 9.4	54.3
0+38 = " " on line 3' " 8.2	
0+40 = section	

-10	3.8	58.7
S	8.4	56.1
cb	10.3	52.2
$\frac{1}{4}$	10.1	52.4
d	8.2	54.3
$\frac{1}{2}$	4.7	57.8
cb	5.3	57.2
N	0.6	61.9
0+60		
N	2.0	60.5
cb	8.4	54.1
$\frac{1}{4}$	1.8	54.7
+2	7.1	54.8
d	10.5	52.0
$\frac{1}{2}$	13.8	48.7
cb	14.3	48.2
S	10.8	51.7

+10	4.5	58.0
0+46 = ^{South} Euc. tree 7" in st. 8" dia	11.2	51.3
+59 = " " " on line	9.7	52.8
+58 = " " " 7" in st. 5" dia	13.3	49.2
+70 = " " " 6" " " 6" "	15.3	47.2
+78 = " " " on line 5" "	12.7	49.8

0+90 = Section

-10	8.5	54.0
S	14.5	48.0
cb	17.8	44.7
$\frac{1}{4}$	15.7	46.8
$\frac{1}{2}$	12.7	49.6
$\frac{3}{4}$	12.3	50.2
cb	12.9	49.6
N	6.0	56.5

T.P. 11.2 253.63 1003 254.51
 on South 8.9
 0+95 = Euc. tree on South 6" in st. 6" dia 44.7

1+05 = Section

N	0.0	53.6
cb	3.7	50.4
+4	7.8	46.4
$\frac{1}{4}$	6.1	47.5
$\frac{1}{2}$	6.3	47.3
+8	6.3	47.3
$\frac{3}{4}$	8.9	44.7
cb	10.8	42.8

S	7.7	45.9
+5	5.3	48.3
	1+15	
-5	7.3	45.8
S	8.8	44.8
cb	12.2	41.4
$\frac{1}{4}$	9.7	43.9
+3	7.9	45.7
cb	8.0	45.6
$\frac{1}{2}$	7.9	45.7
+1	9.0	44.6
+2	7.6	47.0
cb	6.8	46.8
N	12.2	51.2
	R=12.2	41.4
	1+13 = Euc. tree on South 5" dia 4" in st.	

1+40

N	7.2	46.4
cb	10.6	43.0
+5	13.7	39.9
$\frac{1}{4}$	11.8	41.8
$\frac{1}{2}$	12.3	41.3
+3	12.1	41.5
$\frac{3}{4}$	14.1	39.5
cb	15.4	38.2
S	12.4	41.2
+2	10.0	43.6

R=108

1+37 = d. Euc. tree on South 15' Back 4" dia 42.5

1+46 = " " " " " 1' Back 3" dia 40.9

1+50 = " " " " " 7' 10 St 6" dia 37.2

T.P. 2.07 213.44 1226 241.37

1+58.5 = P.C. on N

-5 3.7 39.7

S 4.8 38.6

cb 7.4 36.0

z 7.1 36.9

z 4.8 38.6

z 4.6 38.8

cb 3.9 39.5

N 3.7 39.7

1+78

N 4.5 36.9

cb 6.1 37.3

z 6.1 37.3

z 6.1 37.3

+5 8.5 34.9

z 9.1 33.3

z 7.4 34.0

cb 8.7 34.7

S 7.8 35.6

+5 7.8 35.6

1+87

-10 9.8 33.6

S 10.6 32.8

cb 10.2 33.2

z 7.8 34.0

z 8.0 35.4

z 7.5 35.9

cb 7.3 36.1

N 7.2 36.2

1+97.39 = Section II

N 7.2 36.2

cb 7.0 36.4

z 7.4 36.0

z 8.4 35.0

+1 11.8 32.6

+5 14.6 28.8

z 12.8 30.6

+2 10.9 32.5

S 12.0 31.4

+10 10.7 33.1

Section I = Parallel with E.L. 9th St.

-10 11.4 32.0

S 11.00 31.8

+6 11.1 32.3

+7 12.7 30.7

cb 12.9 30.5

+4 12.6 30.6

+5 10.2 33.2

$\frac{1}{4}$	10.2	33 2
$\frac{1}{2}$	7.9	35 5
$\frac{3}{4}$	7.0	36 4
db.	7.0	36 4
N	7.2	36.2

T.P. 00 El. Hub Bge 24

1.94

241.50

241.50

0.00 = coincident

Marker
8.3.27

X Section Oneida Pl. 40' wide
From S.W. 9th to N.W. Robinson Ave

Page 17
Nail in tree

1294 274.X3 261.29
5' South of A see sketch page 16. = 2' Euc. tree on line 7" dia
12' " " = 2' Euc. tree 16" dia on line
Sec B = 0+00

X	12.3	61.9
cb	11.5	62.7
1/4	10.0	64.2
2	8.5	65.7
1/2	7.5	66.7
cb	6.5	67.7
E	5.7	69.0
+ 0.5		
E	4.05	74.7
cb	0.7	73.5
1/2	2.0	72.2
2	3.2	71.0
1/4	4.3	69.9
cb	5.3	68.9
X	6.2	68.0
+ 10	5.7	68.5
+ 0.24		
- 10	4.6	69.6
X	3.2	71.0
cb	3.0	71.2
1/4	2.4	71.8

Plotted 8/11-27
CBH.

274.73

2	1.3	72.9
TR 11.32	285.35	0.20 274.03
1/4	11.1	74.3
cb	8.9	76.5
E	6.8	78.6
0+49 = end of ble. Garage on E. Con. Floor with Con. E from 0.3' Back		
- 0.3' on Garage Floor	4.60	80.75
E+X = toe of apron	4.99	80.36
cb	5.5	79.9
1/2	6.1	79.3
2	6.5	78.9
1/4	6.6	78.8
cb	6.6	78.8
X	6.9	78.5
0+55 = E Garage on W 0.4' in st		
6.53	6.30	78.82
0+62 = E Con. Walk on W 0.4' in st 4.5' wide tie from 4.93		
4.73	4.59	79.05
0+66 = South end of ble Garage on E. Floor 13' Back		
4.73	4.73	80.42
0+77 = E Garage on E. Con. Floor 13' Back		
4.73	4.73	80.76
1+02 = E Con. Walk on W 4.5' wide 0.4' in st		
X+04 = top Walk	5.86	80.62
cb	5.8	79.4
1/4	5.4	80.0
2	4.9	80.5
1/2	4.7	80.7
cb	4.7	80.9
E	4.1	81.3

		R=4.0	8.14
1+25' = 2	Garage on E. 1' Back dirt Floor		
1+76' = "	" " " " 6' Back Con Floor With Con Apron		
- 0.3' =	Top Con. Apron	3.75	81.60
cb		4.1	81.3
1/2		4.2	81.2
1/2		4.4	81.0
1/4		4.7	80.7
cb		4.9	80.5
W		5.1	80.3
		4.93	80.22
1+91' = 2	Con Walk on W. 4' Wide on line		
<i>This party would like this tree as it is the only one left in California</i>			
2+10' = 2	Acacia tree on W. 1' Back	R=4.9	80.5
W		4.9	80.5
cb		4.6	80.8
1/4		4.4	81.0
1/2		4.3	81.1
1/2		4.2	81.2
cb		4.2	81.2
E		3.9	81.5
T.P.	5.51	285.95	491
	2+32.94 = 2		280.44
			on Con Walk
E		4.6	81.3
cb		4.7	81.2
1/4		4.7	81.2
1/2		5.0	80.9
1/4		4.7	80.7
cb		5.4	80.5

W		5.6	80.3
	2+52.94 = 2		284. Cherokee Lane = 0+00
W		5.5	80.4
cb		5.3	80.6
1/2		5.2	80.7
1/2		5.0	80.9
1/4		4.9	81.0
cb		5.0	80.9
E		4.8	81.1
			Con. 2' Wide
0+53 =	Next of Walk on East Parallel with outside Pl. 0.1 Back		
E =	top of Walk	5.44	80.51
cb		5.8	80.1
1/2		5.8	80.1
1/2		5.9	80.0
1/4		6.1	79.8
cb		6.2	79.7
W			79.9
		R=6.0	79.88
		R=6.07	
0+60 = 2	Con. Dr. Walk on W. 7' Wide 0.3 Back		
0+80 =	5 end Con Walk on E. of Back Parallel with outside Place		
W		7.1	78.8
cb		6.9	79.0
1/2		6.7	79.2
1/2		6.5	79.4
1/4		6.4	79.5
cb		6.3	79.6
E =	top Walk	6.99	79.96

S. 27
Marker

X. Section Cherokee LANE 40' wide
From W.L. 10th St. 100' W. to E.L. Oneida Pl.

28830²
28810

84

CE BP	6.09	288.30 ¹⁰ ?	288.91
Robinson + 10th			
		W.L. 10th	
S		5.9	82.2
S top cb		6.13	81.97
S Gutter on Porch		6.43	81.67
" 1/2 "		6.15	81.95
" 1/4 "		6.04	82.06
N 1/2 "		6.22	81.88
" Gut "		6.39	81.71
N top cb		6.20	81.90
N		5.9	82.2
		12' X W.L. 10th	
N		4.9	83.2
cb		5.1	83.0
1/4		5.3	82.8
1/2		5.3	82.8
1/4		5.3	82.8
cb		5.5	82.6
S		5.6	82.5
		50' W	
S		6.7	81.9
cb		6.7	81.9
1/2		6.0	82.1
1/4		5.8	82.3
1/4		5.8	82.3

Plotted by
C.B.H.

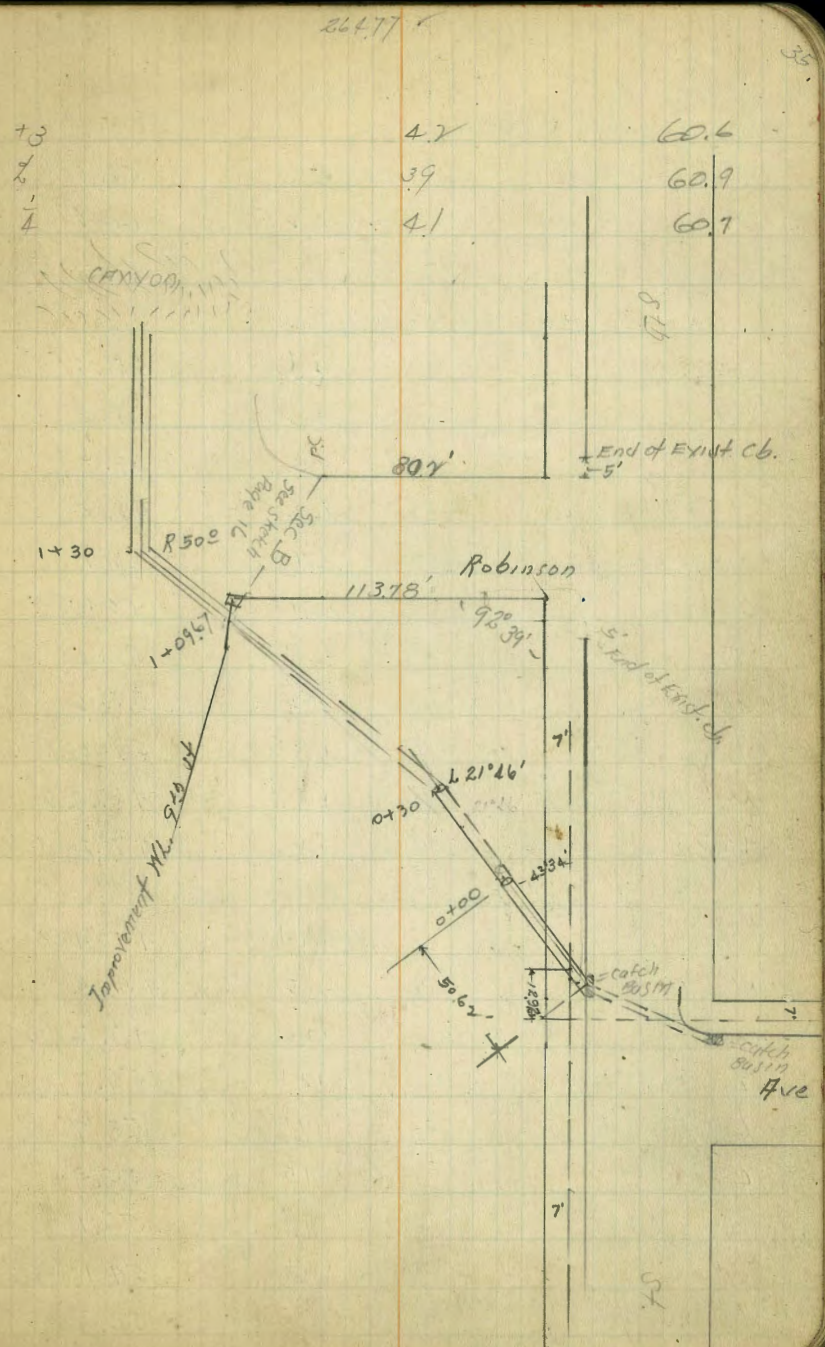
Ncb	5.8	82.3
N	5.5	82.6
		6' High
		71' W = 2 Board Fence on North 51' in length 03' in St.
		R = 6.6
		0+91 = 2 Dble Garage on South 03' Back dirt Floors
		81.5
		1400 = E.L. Oneida Pl.
N	6.7	81.4
cb	7.0	81.1
1/2	6.9	81.2
1/4	6.7	81.4
1/4	6.7	81.4
cb	6.7	81.4
S	6.9	81.2

Walker
p. 4-27

N. Section Robinson Ave 50' Wide
Front. El. 8th St 817' E

	183	275.98	Line 8th	274.95
N-5 = top of exist. cb			10.0	66.0
N = " " Paving			10.51	65.48
cb " " " "			10.72	65.26
1/4 " " "			10.92	65.06
1/2 " " "			11.15	64.93
3/4 " " "			11.25	64.73
cb " " "			11.44	64.54
S " " "			11.63	64.35
+5 = top of exist. cb			11.64	64.94
El. 8th				
S			11.1	64.9
cb			14.2	61.8
1/2			12.9	63.1
1/4			13.0	63.0
+5			12.9	63.1
1/2			11.5	64.5
cb			11.3	64.7
N			11.1	64.9
T.P.	116	264.77	12.37	263.61
15' E.				
-15			8.4	56.4
N			9.9	54.9
cb			7.4	57.4
1/4			3.1	61.7

Plotted 8/11/27
CBH



264.77

35

cb	46	60.2
+1	60	58.8
+2	42	60.6
S	0.1	64.7
30' E. E.L. 8 ^{1/2}		
S	2.6	62.2
+9	62	58.6
cb	7.5	57.3
+1	63	58.5
$\frac{1}{4}$	67	58.1
$\frac{1}{2}$	67	58.1
+4	68	58.0
$\frac{1}{4}$	92	55.6
cb	13.5	51.3
N	18.1	46.7
+25	17.6	47.2
48' E		
-25	19.4	45.4
N	21.5	43.3
cb	17.6	47.2
$\frac{1}{2}$	14.1	50.7
$\frac{1}{4}$	9.1	55.7
$\frac{1}{4}$	9.5	55.3
cb	9.7	55.1
+2	10.7	54.1
+6	8.5	56.3

S	3.5	61.3
T.P. 339 258.0V 10.14 259.63		
60' E		
S	+3.3	61.3
+1	+3.0	61.0
+2	-1.8	56.2
+6	8.0	50.0
+9	8.2	49.6
cb	5.3	52.7
$\frac{1}{4}$	4.6	53.4
$\frac{1}{2}$	4.3	53.7
$\frac{1}{4}$	8.9	49.1
cb	11.0	47.0
N	14.2	43.5
+5	15.7	42.3
+20	14.7	43.3
81.2' E = P.C. on South		
-20	17.4	40.6
N	16.8	41.2
cb	14.4	43.6
$\frac{1}{4}$	10.5	47.5
$\frac{1}{2}$	6.8	51.2
$\frac{1}{4}$	6.8	51.2
cb	7.5	50.5
+2	7.5	50.5
+4	10.5	47.5

+8	10.5	47.5
U	6.3	51.7

For Section B See Sketch Page 16 ^{Notes} P. 22

LEVELS for DRAIN see sketch Page 35

0+00 = Flow Line Exit Pipe	0.00	258.02
0+1'	4.9'	53.1
+2	6.9	51.1
0+30 = Δ 1.81° 26'	11.34	46.68
T.P. 3.08	249.76	11.34
		246.68
0+70	8.4	41.3
1+30 = Δ R50°	11.4	38.3
1+60	12.2	37.6
1+90	10.8	39.0
2+15	9.9	39.8
2+42	10.4	39.3
+55	15.6	34.2
2+70	19.6	30.2
chk. on EC. ksb Page 24	8.27	241.49

241.50 = Elev. Hub
0.01' in Error

Section of Portion of 10th St.
Between Univ. and Essex St.

SX 87
Univ. & 10th St. 2.16 284.18 282.02

Sec. A = 53.5' South Side Univ.

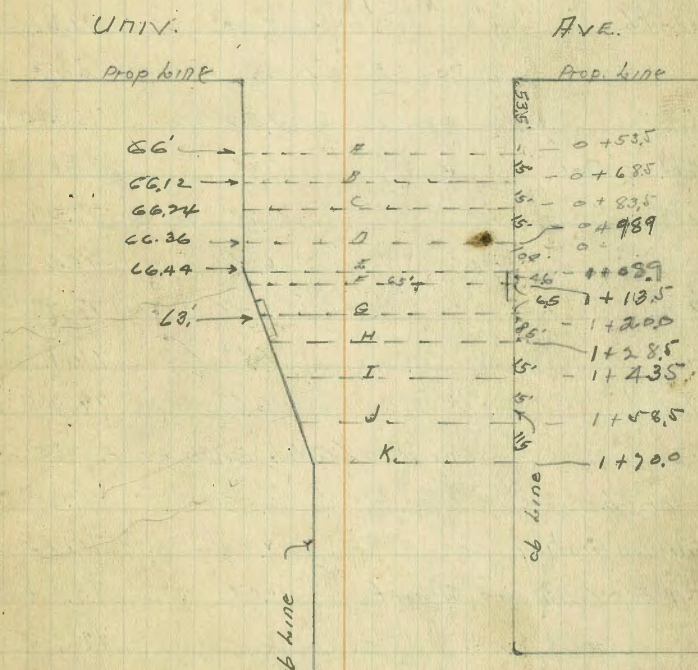
N top cb	4.78	79.40
" Gut on Pav	5.65	78.53
" 1/2 " "	4.55	79.63
1/2 " "	4.06	80.12
E 1/2 " "	4.10	80.02
E Gut "	4.69	79.49
E top cb	3.88	80.30

Sec B

E " "	4.59	79.59
" Gut on Pav	5.40	78.78
" 1/2 " "	4.72	79.46
1/2 " "	4.70	79.48
N 1/2 " "	5.16	79.02
N Gut " "	6.35	77.83

Sec C

N top cb	6.29	77.89
N Gut on Pav	7.05	77.03
" 1/2 " "	5.99	78.19
1/2 " "	5.45	78.73
E 1/2 " "	5.47	78.71
T.P.	3.23	284.41
E Gut on Pav	6.40	78.01
E top cb	5.58	78.83



ESSEX ST.

57

10th

Sec. D

X top cb.	6.86	78.15
" Gut	7.06	77.35
" $\frac{1}{2}$ on Pav.	6.42	77.99
" " "	6.35	78.06
X $\frac{1}{2}$ " "	6.88	77.53
X Gut " "	8.11	76.30
X top cb.	7.30	77.11

Sec E = Δ on West cb line

X " "	7.82	76.59
X Gut on Pav.	8.74	75.67
X $\frac{1}{2}$ " "	7.35	77.06
" " "	6.74	77.67
E $\frac{1}{2}$ " "	6.71	77.70
E Gut " "	7.48	76.93
E top cb.	6.46	77.95

Sec F = $\frac{1}{2}$ Catch Basin on E = 65'

E top cb.	6.53	77.88
" Gut on Grating	7.73	76.68
" on Floor line of Culvert	11.07	73.34
E $\frac{1}{2}$ on Pav.	6.86	77.55
" on " "	6.86	77.55
X $\frac{1}{2}$ " "	7.48	76.93
X Gut " "	8.90	75.51
X top cb.	7.91	76.50

Width sec G = 43'

Sec. G = $\frac{1}{2}$ Catch Basin on X1

X top cb.	7.91	76.50
X Gut on Grating	8.93	75.48
X Floor line of Culvert upper Culvert	15.01	69.40
X $\frac{1}{2}$ on Pav.	7.56	71.00
" " "	6.94	76.85
E $\frac{1}{2}$ " "	6.93	77.47
E Gut " "	7.49	77.48
E top cb.	4.53	76.92
		77.88

Section H = 40' width

E Gut. (also equals top cb.) (= $\frac{1}{2}$ Drive way)	7.27	77.14
E $\frac{1}{2}$ on Pav.	6.76	77.65
" " "	6.83	77.58
X $\frac{1}{2}$ " "	7.50	76.91
X Gut " "	8.85	75.56
X top cb.	7.82	76.59

Section I = 55' width

X top cb.	7.41	77.00
X Gut on Pav.	8.08	76.33
" $\frac{1}{2}$ " "	7.06	77.35
" " "	6.51	77.90
E $\frac{1}{2}$ " "	6.47	77.94
E Gut	6.82	77.59

No. of section in Alley

Section J

E Gut on Pav.	6.34	77.87
" $\frac{1}{2}$ on " "	6.17	78.24

L on Pav	6.16	78.25
N 2" "	6.56	77.85
N Gutter on Pav.	7.59	76.91
N Top cb.	6.96	77.45

Δ in cb = section K = 46.86 width

N Top cb.	6.57	77.84
N Gutter on Pav.	7.07	77.34
" 2" "	6.24	78.17
L " "	5.90	78.51
E 2" "	6.00	78.41
E Gut " "	6.40	78.01
E Top cb.	5.70	78.71

Chk on S.E. B.P. Robinson 10th 2.38 282.03

$$\frac{282.01}{.07} = 814$$

TP	3.25	242.28	11.51	289.03
L			6.1	36.2
7			11.5	30.8
cb			11.6	30.7
E			11.7	31.1
+15			9.6	32.7

55.30 South of Section 2 = Section ③

-15			10.9	31.4
E			12.1	30.2
cb			12.1	30.2
7			12.8	29.5
L			7.2	35.1
+3			4.3	38.0
7			4.4	37.9 ⁺
+5			4.9	37.4
cb			0.0	42.3
+2			+3.8	46.1
Y			+6.4	48.7

Sec 4

Y			+6.0	48.3
+7			+4.0	46.3
cb			+2.0	44.3
+5			5.2	37.1
7			4.8	37.5 ⁺
+6			4.3	38.0
L			6.2	36.1

+7			11.2	31.1
7			12.4	29.9
cb			12.1	30.2
E			12.1	30.2
+15			10.9	31.4

Sec 5

-15			10.7	31.6
E			12.1	30.2
cb			12.1	30.2
7			12.5	29.8
+4			12.1	30.1
+5			8.2	33.1
L			5.9	36.4
+2			4.4	37.9 ⁺
7			4.8	37.5 ⁺
+7			5.1	37.2
cb			+1.0	43.3
Y			+4.2	46.5

15' South Sec 5

Y			+1.4	43.7
+7			0.0	42.3
cb			1.9	40.4
+3			5.6	36.7
7			5.3	37.0 ⁺
+7			4.5	37.8
L			6.1	36.2

+3	7.1	35.2
+5	12.9	29.4
$\frac{1}{4}$	12.9	29.4
cb.	13.3	29.0
E	12.8	29.5
+15	11.2	31.1

22' South of Section ⑤

-15	11.2	31.1
E	13.3	29.0
cb	12.6	29.7
$\frac{1}{2}$	9.7	32.6
X	6.4	35.9
+3	4.9	37.4
$\frac{1}{2}$	5.3	37.0+
+8	5.6	36.7
cb	1.5	40.8
X	+1.8	44.1

49.51 South = Section ⑥

X	1.8	40.5
+2	1.9	40.4
+5	6.2	36.1
cb	6.3	36.0 X
+5	6.5	35.8
$\frac{1}{2}$	7.1	35.2
+4	7.3	35.0
$\frac{1}{2}$	9.1	33.2

$\frac{1}{2}$	11.1	31.2
cb	12.8	29.5
E	13.6	28.7
+15	13.1	29.2
+20	12.0	30.3

Sec ⑦

-20	15.1	27.2
E	13.9	28.4
cb	13.4	28.9
$\frac{1}{2}$	11.5	30.8
$\frac{1}{2}$	9.9	32.4
+6	7.5	34.8
$\frac{1}{2}$	7.3	35.0
+5	6.7	35.6+
cb	6.4	35.9
+5	6.3	36.0
+8	1.9	40.4
X	1.8	40.5

Sec 8

X	1.8	40.5
+2	1.9	40.4
+5	6.3	36.0
cb	6.4	35.9+
$\frac{1}{2}$	6.8	35.5
+5	7.5	34.8
cb	10.1	32.2

1/4	12.1	30.2
cb.	13.5	28.8
E	14.1	28.2
+20	15.1	27.2

25' South Sec. 8

-20	15.7	26.6
E	15.8	26.5
cb.	14.8	27.5
+7	12.9	29.4
1/4	12.8	29.5
1/2	11.9	30.4
1/4	2.0	35.3
cb.	7.3	35.0
+6	1.4	40.9
N	1.0	41.3

60' South Sec. 8

N	1.7	40.6
+6	8.2	34.1
cb.	8.0	34.3
1/4	8.1	34.2
1/2	14.7	27.6
1/4	18.3	24.0
cb.	17.3	25.0
E	14.7	25.6
+15	14.8	27.5

82.11' South = Section 9

TP 376	2342.3	11.81	23047
-15'	8.9		27.3
E	10.1		24.1
cb.	10.5		23.7
1/4	0.6		23.6
+8	12.0		22.2
1/2	11.2		23.0
1/4	1.2		33.0
cb.	1.6		32.6
+4	1.1		35.3
N	+5.2		39.4

Sec. 10

N	+7.2		41.4
+7	+4.6		38.8
cb.	+1.6		35.8
+2	+0.6		34.8
1/2	3.0		31.2
1/4	2.9		31.3
+7	2.7		31.5
1/2	8.8		25.4
1/4	12.4		22.8
cb.	10.8		23.4
E	10.1		24.1
+15	8.7		25.5

Sec 11

-15'	8.6		25.6
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E	89	25.3
cb	11.0	23.2
$\frac{1}{4}$	12.8	21.4
+3	12.2	22.0
+5	6.5	27.7
2	4.1	30.1
+5	3.1	31.1
$\frac{1}{2}$	4.3	29.9
+7	4.6	29.6
+8	0.3	33.9
cb	0.3	33.9
+3	+ 3.4	37.6
Y	+ 6.2	40.4

34' South of Sec 11

Y	+ 4.0	38.2
cb	+ 0.4	34.6
+2	6.8	27.4
$\frac{1}{2}$	4.1	28.1
2	4.9	29.3
$\frac{1}{2}$	8.3	25.9
cb	11.0	23.2
+3	12.0	22.2
+5	14.6	19.6
E	14.5	19.7
+2	12.0	22.2
+15	9.3	24.9

9th St. Section 46

57.22' South - Section 12

-15	9.9	24.3
6	13.1	21.1
E	13.2	21.0
+5	13.6	20.6
cb	15.2	19.0
+4	11.7	22.5
$\frac{1}{4}$	9.8	24.4
2	8.5	25.7
+6	6.1	28.1
$\frac{1}{2}$	6.6	27.6
cb	8.0	26.2
+3	8.0	26.2
+5	1.9	32.3
Y	1.3	32.9

Sec (13)

Y	1.3	32.9
+4	2.2	32.0
+6	8.1	26.1
cb	8.1	26.1
$\frac{1}{4}$	7.0	27.2
+3	7.0	27.2
2	9.1	25.1
$\frac{1}{2}$	10.8	23.4
+6	14.8	19.4
cb	15.1	19.1

+2	13.2	21.0
E	14.0	20.2
+5	13.9	20.3
+8	11.0	23.2
+15	8.4	25.8

sec (14)

-15'	9.5	24.7
-8	11.5	22.7
-7	14.4	19.8
E	14.4	19.8
cb	14.0	20.2
+2	15.3	18.9
+8	14.2	20.0
$\frac{1}{2}$	12.1	22.1
$\frac{1}{2}$	9.9	24.3
+7	7.0	27.0
$\frac{1}{2}$	7.3	26.9
cb	8.2	26.0
+4	8.1	26.1
+6	2.3	31.9
W	1.3	32.9

25' South Sec 14

W	4.3	29.9
-5	5.4	28.8
+6	9.3	24.9
cb	9.5	24.7

$\frac{1}{2}$	9.0	25.2
+6	9.1	25.1
$\frac{1}{2}$	10.4	23.8
$\frac{1}{2}$	12.6	21.6
+1	15.0	19.2
cb	15.6	18.6
+5	14.5	19.7
E	13.8	20.4
+15	9.4	24.8

50' South Section 14

-15	9.2	25.0
E	13.3	20.9
+5	15.7	18.8
cb	15.9	18.3
$\frac{1}{2}$	13.6	20.6
$\frac{1}{2}$	11.8	22.4
$\frac{1}{2}$	10.4	23.8
cb	10.9	23.3
+1	9.6	24.6
+5	8.8	25.4
+7	7.8	26.4
W	7.3	26.9

76.08' South = Section (15)

W	10.6	23.6
cb	10.8	23.4
+3	11.0	21.2

23423

2	11.8	22.4
+5	11.7	22.5
2	11.8	22.4
2	14.7	19.5
cb.	15.8	18.4
E	15.1	19.1
+10	12.8	21.4

T.P. 5.35 227.51 1207 722.16
 { Note: if Any Fall is Made on (227.51) in this section closed
 (at least should be 100 ft) = N.W. Penn. Area only birds taken

-10	12	21.3
E	8.2	19.3
cb	9.0	18.5
2	8.4	19.1
2	7.1	20.4
2	5.7	21.8
+4	5.8	21.7
+6	4.5	23.0
cb.	4.5	23.0
11	3.8	23.7
Section 17		
11	1.2	26.3
+7	3.0	24.5
cb.	5.1	22.4
+11	4.4	21.1
2	6.0	21.5
+9	6.1	21.4

227.51

9th Sta. X Section 46

2	7.6	19.9
2	8.7	18.8
+5	9.4	18.1
cb.	8.9	18.6
E	8.2	19.3
+10	6.2	21.3

17' South of Section 17

-10	5.2	22.3
E	7.0	20.5
cb.	8.5	19.0
2	9.6	17.9
2	8.5	18.0
+7	6.4	21.1
2	6.3	21.2
cb.	6.9	20.6
+3	2.4	25.1
11	+2.4	27.9

Section 18

11	+0.2	27.7
+5	1.5	26.0
+8	7.9	19.6
cb.	7.9	19.6
2	6.6	20.9
+7	9.8	17.7
+8	13.0	14.5
2	1.2	15.2

+4	9.7	17.8
$\frac{1}{2}$	9.6	17.9
cb	8.9	18.6
E	7.8	19.7
+10	6.1	21.4

section 19 - S.L. Penn. H're

-10	8.5	19.0
E	10.0	17.5
cb.	10.0	17.5
$\frac{1}{2}$	10.1	17.4
+7	10.0	17.5
+8	12.0	15.5
$\frac{1}{2}$	13.5	14.0
+1	10.2	17.3
$\frac{1}{2}$	6.8	20.7
cb	7.8	19.7
+2	8.0	18.5
+5	1.7	25.8
W	+0.2	27.7

Section A

W	1.5	26.0		
TP	2.95	27.87	7.59	21.99
W+5	1.5	21.3		
+6	4.1	18.7		
cb.	4.1	18.7		
$\frac{1}{2}$	2.8	20.0		

+3	4.2	18.6
+4	7.3	15.5
$\frac{1}{2}$	8.2	14.6
+1	5.6	17.2
$\frac{1}{2}$	5.7	17.1
cb.	5.8	17.0
E	5.1	17.7
+10	3.1	19.7

35' South Section A

-10	4.7	18.1
E	6.8	16.0
cb.	7.0	15.8
$\frac{1}{2}$	6.7	16.1
+5	6.9	15.9
$\frac{1}{2}$	8.6	14.2
+4	7.6	15.2
+5	4.6	18.2
$\frac{1}{2}$	4.6	18.2
cb.	5.8	17.0
+3	5.3	17.5
+5	3.0	19.8
W	0.1	22.7

50' South Section A

W	1.2	21.6
+6	2.9	20.3
+8	6.8	16.0

22277

cb	6.8	16.0
4	5.4	17.4
2	4.6	18.2
+2	8.5	14.3
4	8.5	14.3
cb	7.7	15.1
E	8.0	14.8
+10	3.6	19.2

69' South

-10	12	21.6
-8	1.9	20.9
E	7.9	15.0
cb	8.3	14.6
+5	9.0	13.9
4	8.0	14.0
2	6.2	16.6
2	6.3	16.6
cb	7.6	15.2
+1	7.2	15.6
+3	3.6	19.2
W	2.5	20.3

72' South

W	2.6	20.3
+6	3.7	19.2
+8	5.7	17.1
+9	7.7	15.1

22287

9th St. N. Section 50

cb	7.7	15.1
4	6.5	16.3
2	6.6	16.2
+5	8.3	14.5
4	8.5	14.3
+4	8.9	14.0
cb	7.4	15.4
E	4.5	18.3
+5	3.2	19.6

100' South Sec A

-10	1.1	21.8
E	4.4	18.4
cb	7.0	15.9
2	8.9	14.0
+5	10.0	12.9
2	8.4	14.4
+4	7.6	15.2
4	7.7	15.1
cb	8.5	14.3
+1	5.7	19.1
W	3.9	19.0

135' South ✓

W	6.1	16.8
+6	6.4	16.5
cb	9.4	13.4
2	8.8	14.0

+5	8.5	14.4
2	9.6	13.2
+3	10.9	12.0
+5	9.8	13.0
$\frac{1}{4}$	9.5	13.3
cb	7.9	15.0
E	5.2	17.6
+10	2.7	20.1

150' South

-10	3.7	19.1
E	5.2	17.6
cb	8.0	14.8
$\frac{1}{4}$	9.9	13.0
+6	10.6	12.2
+8	11.2	11.6
2	10.0	12.9
+7	8.9	14.0
$\frac{1}{4}$	9.0	13.9
cb	7.9	13.0
+4	9.7	13.1
+5	7.5	15.3
W	6.1	16.8

165/6 South = Section (B)

W	8.0	14.9
-12	8.0	14.9
+3	9.6	13.2

cb	9.8	13.0
$\frac{1}{4}$	9.5	13.3
2	10.6	12.2
+8	12.0	10.8
+5	10.6	12.2
$\frac{1}{4}$	10.2	12.6
cb	8.8	14.0
E	7.5	15.3
+10	5.8	17.0

Sec C

-10	8.1	14.8
E	8.6	14.2
cb	9.1	13.8
$\frac{1}{4}$	10.4	12.5
+5	11.5	11.3
2	10.7	12.1
$\frac{1}{4}$	9.6	13.2
+3	9.2	13.6
cb	9.8	13.0
+7	9.8	13.0
+8	8.0	14.8
W	8.0	14.8

(D) Note: if fill is made on E. of this section, current should be located

Sec E

W	8.0	14.8
+2	8.0	14.8
+3	9.8	13.0

222.87

cb.		99	13.0
+7		93	13.5
4		99	13.0
d		106	12.3
+3		13.6	09.2
+8		12.8	10.0
4		10.6	10.2
cb		10.0	12.9
E		96	13.2
+10		9.0	13.8
TP	424	218.71	840

on 4" Iron Pipe
on Section C
on East

29' South Section D

		840	21447
-10		2.8	15.9
E		4.2	14.5
cb		34	13.3
1/2		4	12.3
+2		10.1	08.6
+6		10.3	08.4
+7		7.1	11.6
d		7.0	11.7
+8		6.7	12.0
1/2		6.1	12.6
cb.		6.4	12.5
+6		6.4	12.3
+7		4.5	14.2
W		4.2	14.5

218.71

9th S. X Section 57

54' South of Section D

W	4.9	13.8
+5	6.4	12.3
d	6.7	12.0
+7	6.4	12.3
1/2	6.7	12.0
+5	7.8	10.9
+6	10.8	07.9
+9	10.9	07.8
d	7.6	11.1
1/2	6.8	11.9
cb	6.2	12.5
E	5.3	13.4

67.33' South = Section E

E	6.1	12.6
cb	7.0	11.7
1/2	7.8	10.9
d	8.0	10.7
+2	8.4	10.3
+3	10.8	07.9
+7	10.9	07.8
+8	7.5	11.2
1/2	7.5	11.2
cb	7.3	11.4
+3	6.8	11.9
+2	4.9	13.8

W	2.5	16.2
Section F		
W	1.0	17.7
+7	4.0	14.7
+9	6.9	11.8
cb	7.4	11.3
+9	7.6	11.1
$\frac{1}{2}$	8.6	10.1
+3	10.8	07.9
+8	10.6	08.1
L	8.2	10.5
$\frac{1}{2}$	8.1	10.6
cb	7.3	11.4
E	6.1	12.6
Section G		
E	6.1	12.6
cb	7.2	11.5
$\frac{1}{2}$	8.2	10.5
L	8.2	10.5
+2	10.4	08.3
+9	10.7	08.0
$\frac{1}{4}$	7.0	11.7
cb	7.5	11.2
+2	4.0	14.7
W	1.3	17.4

15' South Section G

W	1.3	17.4
+7	4.1	14.6
cb	6.4	12.3
+1	7.7	11.0
$\frac{1}{2}$	7.2	11.5
+1	10.6	08.1
L	11.2	07.5
+2	9.1	09.6
$\frac{1}{2}$	8.8	09.9
cb	8.2	10.5
E	6.7	12.0
	for location see sketch	
	30' South Sec G. = 2' of Front of Garage on West	Gar. Floor
E	7.7	11.0
cb	9.2	09.5
+5	9.3	09.4
+6	11.7	07.0
$\frac{1}{4}$	12.0	06.7
+2	11.6	07.1
+3	9.3	09.4
L	7.9	10.8
+2	6.7	12.0
$\frac{1}{4}$	7.3	11.4
cb	7.7	11.0
+3 = on Garage Floor	7.35	211.36
	50' South Sec G	
W	1.3	17.4

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+7	5.7	13.0
+8	8.3	10.4
cb.	8.3	10.4
$\frac{1}{4}$	7.5	11.2
+9	7.2	11.5
$\frac{1}{2}$	7.7	10.8
$\frac{3}{4}$	9.3	09.4
cb.	10.0	08.7
+1	12.5	06.2
+6	12.3	06.4
E	9.4	09.3
+5	9.0	09.7

73.87 South = Section H

-10	6.5	12.2
E	10.3	08.4
+2	11.1	07.6
+3	13.0	05.7
+7	12.9	05.8
+8	10.4	08.3
cb.	10.3	08.4
$\frac{1}{4}$	10.0	08.7
$\frac{1}{2}$	9.6	09.1
+5	8.5	10.5
$\frac{3}{4}$	7.8	10.9
cb.	8.3	10.4
+9	8.4	10.3

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9th St X Section 54

14	6.6	12.1
SEC I		
14	6.6	12.1
+1	8.4	10.3
cb.	8.1	10.6
$\frac{1}{2}$	8.0	10.7
$\frac{3}{4}$	10.1	08.6
$\frac{1}{4}$	10.7	08.0
+7	11.1	07.6
cb.	13.6	05.1
+5	12.5	06.2
+7	11.7	07.0
+8	6.4	12.3
E	5.9	12.8

Section J

E	9.2	09.5
+7	4.2	04.5
6	14.2	04.5
+2	11.9	06.8
+3	11.5	07.2
$\frac{1}{4}$	11.3	07.4
$\frac{1}{2}$	9.9	08.8
+5	8.3	10.4
$\frac{3}{4}$	7.8	10.9
cb.	8.4	10.3
+9	8.4	10.3

218.71

34		6.6	12.1
	35' South of Sec J		
34		5.2	13.5
+3		6.6	12.1
+5		9.6	09.1
cb		9.6	09.1
z		8.6	10.1
+5		8.7	10.0
z		10.1	08.6
z		11.4	07.3
+9		12.3	06.4
cb		14.6	04.1
+6		14.3	04.4
+7		11.7	07.0
E		10.4	08.3
+5		9.4	09.3
T.P.	354 213.59	8.66	210.85
	60' South J		
-5		3.7	09.9
E		5.4	07.5
+5		7.2	06.4
+6		9.7	03.9
cb		9.8	03.8
+4		9.6	04.0
+3		7.6	06.0
z		7.5	06.1

213.59

9th X. Section

55

z		6.1	07.5
z		4.0	09.6
cb		4.1	08.8
+5		5.3	08.3
+7		1.0	12.6
34		1.0	12.6
	100' South J		
34		0.5	13.1
+5		4.4	09.2
+6		5.8	07.8
cb		6.1	07.5
z		5.6	08.0
z		8.3	05.3
+5		8.3	05.3
z		10.5	03.1
+6		9.9	03.7
+7		7.4	06.2
cb		6.7	06.6
z		5.5	08.1
+5		4.8	08.8
	119.82' South = Sec K		
-5		6.6	06.0
E		7.0	06.6
cb		8.0	05.6
z		8.8	05.2
+5		8.6	15.0

213.59

+6	11.3	02.3
8	11.4	02.2
+5	10.3	03.3
+6	9.1	04.5
+7	6.1	07.5
$\frac{1}{4}$	6.3	07.3
cb	6.2	07.4
+2	5.2	08.4
+7	2.0	11.6
11	1.1	12.6

Sec (L)

11	0.0	13.6
cb	7.9	10.7
+3	6.2	07.4
$\frac{1}{4}$	6.4	07.2
+6	6.9	06.7
+7	11.5	02.1
$\frac{1}{2}$	11.6	02.0
+6	11.1	02.5
+7	8.8	04.8
$\frac{1}{2}$	8.8	04.8
cb	8.4	05.2
E	7.0	06.6
+5'	6.6	07.0

Sec (M)

-5'	6.6	07.0
-----	-----	------

213.59

9th N. X. Section 56

E	7.0	06.6
cb	8.3	05.3
$\frac{1}{4}$	9.1	04.5
+5	9.0	04.6
+6	11.0	02.6
$\frac{1}{2}$	11.8	01.8
+4	11.7	01.9
+5	7.3	05.3
$\frac{1}{4}$	6.6	07.0
+7	6.3	07.3
cb	3.4	10.2
11	1.1	12.5

30' South of Section 17

11	1.5	12.1
cb	3.6	10.0
+2	6.8	06.8
$\frac{1}{2}$	6.7	06.9
+5	6.2	07.4
$\frac{1}{2}$	8.2	05.4
+3	9.2	04.4
+4	12.2	01.4
$\frac{1}{4}$	14.4	01.2
11	9.7	03.9
cb	9.9	03.7
+10	6.9	06.7

60' South of 17

21359

-10	69	06.7
E	10.6	03.0
+2	12.2	01.4
cb	13.3	00.3
+2	10.5	03.1
$\frac{1}{2}$	9.3	04.3
$\frac{1}{2}$	7.6	06.0
+3	6.6	07.0
$\frac{1}{2}$	6.9	06.7
+5	6.9	06.7
cb	3.9	09.7
W	0.8	12.8

95' South of M

W	0.1	13.5
cb	3.2	10.4
+4	5.2	08.4
+5	7.1	06.5
$\frac{1}{2}$	7.0	06.6
+8	7.2	06.4
$\frac{1}{2}$	8.5	05.1
+2	9.8	03.8
$\frac{1}{4}$	10.5	03.1
+2	11.1	02.5
+3	14.5	01.1
cb	13.3	200.3
+5	13.8	99.8

21359

9th St. X. Section

57

+7	9.9	03.7
E	9.3	04.3
+10	7.5	06.1

115' South of M

-10	7.7	06.9
E	9.6	04.0
cb	11.2	02.4
+3	13.7	99.9
+9	13.6	200.0
$\frac{1}{2}$	11.7	01.9
+3	10.7	02.9
$\frac{1}{2}$	8.4	05.2
+2	7.2	06.4
$\frac{1}{2}$	7.1	06.5
+7	7.1	06.5
cb	4.4	09.2
+5	2.2	11.4
W	1.1	12.5

134.0' South = H.L. BROOKES

W	4.6	09.0
+8	5.7	07.9
cb	6.5	07.1
$\frac{1}{2}$	7.0	06.6
$\frac{1}{2}$	7.2	06.3
$\frac{1}{2}$	11.2	02.4
+11	13.9	99.7

21359

9th & N. Section

58

+7		14.2	99.4
cb		12.2	01.4
+5		11.9	01.7
+7		10.5	03.2
L		10.4	03.2
+10		9.0	04.6

Find & North of N.W. ^{Brookline}
 (Prof on 2" Iron Pipe for Future Use

6.90	70669	}		
T.P.	11.33	224.10	0.82	21271
TP	12.38	236.11	0.37	21373
TP	13.04	249.10	0.05	23606
TP	12.81	261.79	0.12	24898
T.P.	11.86	273.04	0.61	261.18
TP	6.48	277.0	1.82	271.22

cht. on B.M. N.Y. Robinson & St. ^{St.}
 275 274.95
 274.95 - 819

(Interpolated)

Sec 110.72' South Sec A.

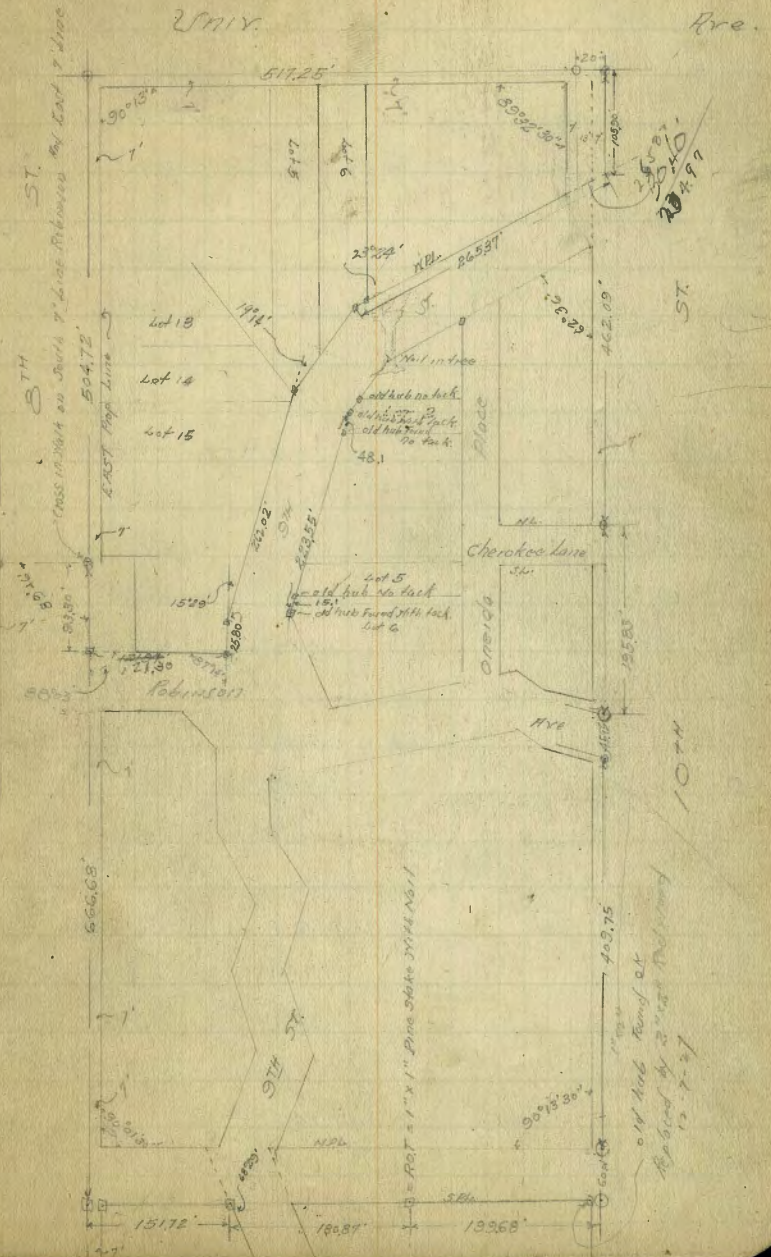
W	18.4
+6	16.5
cb	14.0
1/4	14.8
+5	14.8
L	14.1
+5	12.9
1/4	13.4
cb	15.6
W	18.1
+10	21.3

Walter
C. ...
12-7-27

SURVEY LA CANYON VILLAGE TRACT
As Per Sketch Page 57

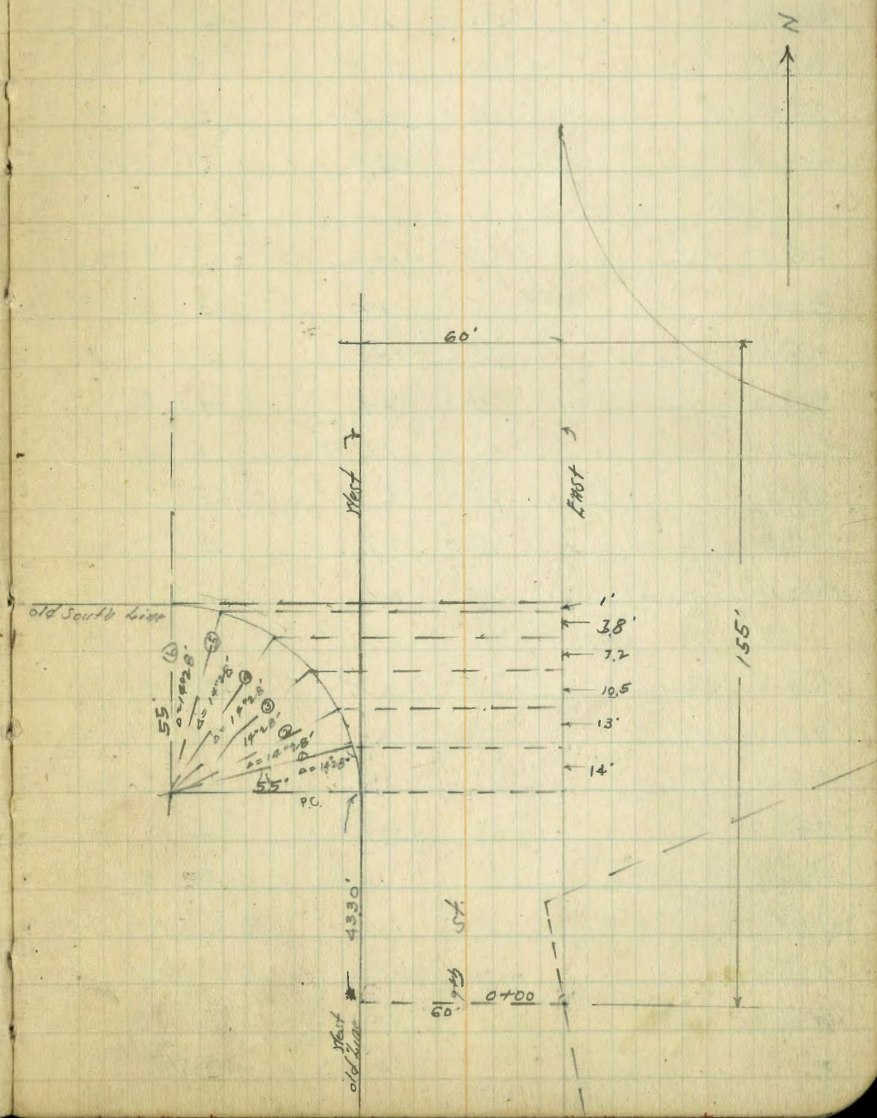
97.14
15.29
71.45

Robinson Ave



SAIKER
RUPH...
1.18.28 X. Section 9th St. And Robinson
Intersection as per sketch

Robinson 8th	0.20	275.15		279.95
TP	1.20	263.64	1271	762.44
T.P.	0.60	251.54	1270	250.94
0+00				
Y		3.4		48.1
+5		6.4		45.1
+10		9.7		41.8
+12		12.7		38.8
+26		12.7		39.3
+41		21.0		30.5
+55		20.6		30.9
+60 = E		20.5		31.0
E+10		19.5		32.0
0+17				
E-15		20.0		31.5
E		21.0		30.5
+5		20.1		31.4
+23		16.3		35.2
+33		11.3		40.2
+48		11.4		40.1
+55		3.3		48.2
+60 = Y		+17		53.2
0+43.3 = PC @ 00 Y.				
Y		10.7		51.7
+5		22		48.3



+1	5.5	46.0
+12	10.2	41.3
+25	10.1	41.4
+50	12.6	38.9
+55	14.7	36.8
+60 = E	16.1	35.4
E+10	18.0	33.5
	o+57.4	
-5	18.7	37.8
E	13.2	38.3
+5	12.8	38.7
+35	9.7	41.8
+52	9.6	41.9
+55	6.5	45.0
+60 = M	2.7	48.8
M+25 = on Curve	0.6	50.9
	o+70.3	
M-8' = on Curve	+3.2	54.7
M	5.0	45.5
+5	8.5	43.0
+20	9.7	41.8
+32	11.0	40.5
+45	10.4	38.1
+55	13.7	37.8
+60 = E	14.2	37.3
E+10	14.5	37.0

	o+80.8	
E-10'	15.6	35.9
E	15.0	36.5
+5'	14.3	37.2
+30	12.3	39.2
+40	P.8	42.7
+60 = M	8.3	43.2
M+03	7.4	44.1
" +08	2.5	49.0
" +09	+25	54.0
" +11.5	+38	55.3
" +16.5 = on Curve	+57	57.2
	o+88	
M-27' = on Curve	+8.0	59.5
M-22'	+67	58.2
-15'	+40	55.5
-14'	2.5	49.0
-9'	6.6	44.9
M	7.2	44.3
+17	7.7	43.8
+25	11.6	39.9
+40	14.4	37.1
+55	14.7	36.8
+60 = E	15.2	36.3
E+10	15.1	36.4
	o+91.8	

25154

E-10		14.8	36.7
E		14.5	37.0
+5		14.7	36.8
+30		13.4	38.1
+45		7.5	44.0
+60 = W		6.9	44.6
W+16		6.6	44.9
+22		+2.2	53.7
+23		+6.1	57.6
+35		+10.6	62.1
+40 = on Curve		+10.8	62.3
T.P.	110	25204	0.60
			25094
		0+92.8	
-54' = on Curve		+11.5	63.5
-49		+11.3	63.3
-40		+10.3	62.3
-29		+7.5	59.5
-22		4.5	47.5
-16		6.6	45.4
W		7.5	44.5
+13		7.6	44.4
+25		12.6	39.4
+36		15.1	36.9
+55		15.5	36.5
+60 = E		15.4	36.6
E+10		15.5	35.5

25204

67

		1+04	
-10	15.1		36.9
E	14.8		37.2
+5	14.8		37.2
+33	14.3		37.7
+55	6.1		45.9
+60 = W	6.1		45.9
W+27	3.8		48.2
+42	+2.3		54.3
+45	+7.5		59.5
+54	+7.5		59.5
		1+08	
-55	0.7		51.8
-25	3.8		48.2
W	5.8		46.2
+3	5.5		46.5
+25	14.8		37.2
+55	15.1		36.9
+60 = E	15.1		36.9
E+10	15.1		36.9
		1+24	
E-10	12.5		39.5
E	14.3		37.7
+5	14.2		37.8
+45	14.5		37.5
+60 = W	7.3		44.7

252.04

$Y+21$	2.4	49.6
$+55$	+1.0	51.0
	1+30	
-55	+0.7	52.7
-38	1.1	50.9
Y	8.6	43.4
+12	13.8	38.2
+55	13.8	38.2
+60 = E	13.3	38.7
E+10	11.3	40.7
	1+44	
E-10	8.2	43.8
E	10.3	41.7
+5	11.3	40.7
+20	14.0	38.0
+45	13.6	38.4
+60 = Y	13.9	38.1
$Y+30$	8.6	43.4
+34	9.0	43.0
+55	5.7	46.3
	1+55	
$Y-55$	7.7	44.3
-40	10.8	41.2
Y	13.3	38.7
+35	13.8	38.2
+45	11.5	40.5

257.04

68

+55	9.6	42.4
+60 = E	8.4	43.6
E+5	7.0	45.0
	1+65	
E	6.4	45.6
+5	7.8	44.2
+29	13.6	38.4
+60 = Y	13.1	38.9
$Y+55$	10.1	41.9
TP 1226	263.68 0.62	251.42
TP 1264	275.60 0.72	267.96
chk. on NY. & M. Robinson + 1.4	0.63	274.97
		274.97 - 0.11
		0.02 1.11 Error

Bliss
Isbell
Morgan
4/6/48

X. Section Polk St from the W Line
of Altadena to the E Line of 5229 St 40' st

π
32355

64

BM spr Pole
N.W. corner
of 5229 St

	+	π 1	-	Elev					
	2.61	330.39		327.78	6.5 cbs 6.75' h/s	6	319.6	316.0	
TP	1.14	327.18	9.35	326.04		7	319.5	315.9	
		0+00 = E. Line of Altadena				8	319.2	315.6	
N		10.6		313.0	316.6	S	8.2	319.0	315.4
cb		10.8		312.8	316.4	S+15	9.3	317.9	314.3
1/4		10.9		312.7	316.3		50' East		
6		11.4		312.2	316.8	S-10	7.3	319.9	316.3
1/4		11.6		312.0	316.6	S	6.9	320.3	316.7
cb		11.9		311.7	316.3	cb	6.7	320.5	316.9
S		12.6		311.0	314.6	1/4	6.3	320.9	317.3
S+5		13.8		309.8	313.4	6	6.3	320.9	317.3
S+15		18.2		305.4	309.0	1/4	6.1	321.13	317.5
		25' East				cb	6.0	321.2	317.6
S-15		12.8		310.8	314.4	N	5.8	321.4	317.8
S-8		10.6		312.0	315.6		75' East		
S		9.7		313.9	317.5	N	3.2	324.0	320.4
cb		9.2		314.4	318.0	cb	3.9	323.8	320.2
1/4		9.0		314.6	318.2	1/4	3.4	323.8	320.2
6		8.4		315.2	318.8	6	3.8	323.4	319.8
1/4		8.5		315.1	318.7	1/4	4.2	323.0	319.4
cb		8.2		315.4	319.0	cb	4.2	323.0	319.4
N		8.0		315.6	319.2	S	4.6	322.63	319.0
		37' East					100' East		
N		7.0		318.6	322.2	S	2.9	324.8	321.2
cb		7.3		318.3	321.9	cb	2.9	324.8	321.2
1/4		7.3		318.3	321.9	1/4	2.9	324.8	321.2

323.55

¢		2.0	321 4	325.2	1/4
1/4		1.7	321 7	325.5	¢
06		1.8	321 7	325.3	1/4
N		1.6	322 0	325.6	06
125' East. W. line of Alley					
N		0.9	322 7	326.3	
06		0.9	322 7	326.3	S
1/4		0.6	323 0	326.6	06
¢		0.8	322 8	326.4	1/4
1/4		1.0	323 6	327.2	¢
06		0.7	322 9	326.5	1/4
S		0.8	322 8	326.4	06

418

327.68

0.05

323.50

N

145' East E. Line of Alley

S		3.5	324 2	327.8	N
06		3.6	324 1	327.7	06
1/4		3.9	323 8	327.4	1/4
+-		4.2	323 5	327.1	¢
¢		4.0	323 7	327.3	45
1/4		4.0	323 7	327.3	1/4
06		4.4	323 3	326.9	+-5
N		4.4	323 3	326.9	06

175' East

N		4.3	323 4	327.0	
06		4.2	323 5	327.1	S
+-		3.8	323 9	327.5	06

327.68

3.7	327.6	324.0
3.6	327.7	324.1
3.6	327.7	324.1
3.2	328.1	324.5
2.9	328.4	324.8

200' East

3.2	328.1	324.5
3.4	327.9	324.3
3.8	327.5	323.9
3.7	327.6	324.0
3.8	327.5	323.9
4.3	327.0	323.4
4.5	326.8	323.2

235' East

5.5	325.8	322.2
5.5	325.8	322.2
4.9	325.4	322.8
5.0	326.3	322.7
4.9	326.4	322.8
4.8	326.5	322.9
4.4	326.9	323.3
4.3	327.0	323.4
4.0	327.3	323.7

258' East

5.3	326.0	322.4
5.3	326.0	322.4

327.68

+4	5.6	322.1	325.7	N
1/4	6.0	321.7	325.3	
+3	6.5	321.2	324.8	N
ϕ	6.3	321.4	325.0	cb
1/4	6.5	321.2	324.8	1/4
+3	6.7	321.0	324.6	ϕ
cb	7.1	320.6	324.2	1/4
N	7.4	320.3	323.9	cb
	270' E. W. line of 51.5'		60.5'	S
			120.6'	
			9.15'	
N	8.1	319.6	323.2	
cb	8.0	319.7	323.3	S
1/4	7.5	320.2	323.8	cb
ϕ	7.4	320.3	323.9	1/4
1/4	7.4	320.3	323.9	ϕ
+3	6.9	320.8	324.4	1/4
cb	6.7	321.0	324.6	cb
S	6.3	321.4	325.0	N
	W cb			
S	7.7	320.0	323.6	N
cb	8.0	319.7	323.3	cb
+4	8.2	319.5	323.1	1/4
1/4	8.6	319.1	322.7	ϕ
ϕ	8.4	319.3	322.9	1/4
1/4	8.4	319.3	322.9	+3
+1	8.5	319.2	322.8	cb
cb	9.0	318.7	322.3	S

327.68

8.1	323.2	319.6
W 1/4		
9.6	321.7	318.1
9.4	321.9	318.3
9.1	322.2	318.6
9.1	322.2	318.6
9.3	322.0	318.4
8.9	322.4	318.8
8.7	322.6	319.0
ϕ		
9.6	321.7	318.1
9.7	321.6	318.0
9.8	321.5	317.9
9.6	321.7	318.1
9.6	321.7	318.1
9.9	321.5	317.9
10.0	321.3	317.7
E 1/4		
10.7	320.6	317.0
10.4	320.9	317.3
10.0	321.3	317.7
10.0	321.3	317.7
10.3	321.0	317.4
10.1	321.2	317.6
10.2	321.1	317.5
10.3	321.0	317.4

327.68 ✓
E. 06

S	10.8	316.9	320.5	
06	10.5	317.2	320.8	N
1/4	10.9	316.8	320.4	06
+2	11.1	316.6	320.2	1/4
±	10.6	317.1	320.8	±
1/4	10.6	317.1	320.7	1/4
06	11.2	316.5	320.1	06
N	11.2	316.5	320.1	S

E Line of 51st Street

N	11.6	316.1	319.7	S
06	11.8	315.9	319.5	06
1/4	11.4	316.3	319.9	1/4
±	11.3	316.4	320.0	±
1/4	11.6	316.1	319.7	+3
06	11.6	316.1	319.7	1/4
S	11.6	316.1	319.7	06

25' East

S	12.6	315.1	318.7		
06	12.6	315.1	318.7		
1/4	12.9	314.8	318.4		
±	12.7	315.0	318.6	N	
1/4	12.6	315.1	318.7	+3	
06	12.6	315.1	318.7	06	
N	12.6	315.1	318.7	1/4	
T.P.	7.00	321.63	13.05	319.63	+4

321.63 ✓

67

62' East

6.3	318.9	315.3
6.8	318.4	314.8
6.7	318.5	314.9
7.0	318.1	314.5
7.4	317.8	314.2
7.6	317.6	314.0
7.5	317.7	314.1

75' East

7.4	317.8	314.2
7.0	318.2	314.6
6.8	318.4	314.8
6.6	318.6	315.0
6.9	318.8	315.2
6.4	318.8	315.2
6.1	319.1	315.5
5.7	319.5	315.9

77' East Single Garage on North

±	5.3	319.9	316.3
---	-----	-------	-------

4.5 Back

100' East

5.3	319.9	316.3
5.5	319.7	316.1
5.9	319.3	315.7
6.0	319.2	315.6
6.0	319.2	315.6
6.2	319.0	315.4

π
321.63

1/4	6.6	315.0	318.6	1/4
cb	6.6	315.0	318.6	ϕ
S	6.8	314.8	318.4	1/4
125' East N. Line of Alley				
S	6.6	315.0	318.6	+2
cb	6.4	315.2	318.8	IV
1/4	6.4	315.2	318.8	
ϕ	5.9	315.7	319.3	N
1/4	5.6	315.9	319.3	cb
cb	5.5	316.1	319.7	1/4
+3	5.3	316.3	319.9	ϕ
N	5.0	316.4	320.2	1/4
145' East E. Line of Alley				
N	4.6	317.0	320.6	S
+4	5.0	316.6	320.2	
cb	5.3	316.3	319.9	S
1/4	5.3	316.3	319.9	cb
ϕ	5.4	316.2	319.8	1/4
1/4	6.0	315.6	319.2	ϕ
cb	6.2	315.4	319.0	+5
S	6.4	315.2	318.8	1/4
163 ⁵ Walk on North				
2.5 BACK	3.99	317.64	321.7	N
175' East				
S	6.0	315.0	319.2	N
cb	5.9	315.7	319.3	cb

π
321.63

6.0	319.2	315.6
5.5	319.7	316.1
5.3	319.9	316.3
5.4	319.8	316.2
5.0	320.2	316.6
4.7	320.5	316.9
200' East		
4.8	320.4	316.8
5.3	319.9	316.3
5.4	319.8	316.2
5.5	319.7	316.1
6.0	319.5	315.4
5.9	319.3	315.7
6.1	319.1	315.5
235'		
5.4	319.8	316.2
5.5	319.7	316.1
5.6	320.2	316.0
5.4	319.8	316.2
5.0	320.2	316.6
5.1	320.1	316.5
5.0	320.2	316.6
4.3	320.9	317.3
251' East		
4.7	320.5	316.9
5.3	319.9	316.3

321.63

49	55	316.1	319.7
2	57	315.9	319.5
1/4	58	315.8	319.4
cb	6.0	315.6	319.2
S	6.1	315.5	319.1
270' East			
S	6.5	315.1	318.7
cb	6.9	315.2	318.8
1/4	6.3	315.3	318.9
2	6.0	315.6	319.2
1/4	5.4	316.2	319.8
cb	5.2	316.4	320.0
N	5.2	316.4	320.0
TP	8.55	325.65	4.53 317.10
BM	SPK Pole NW 51 52	1.48	324.17

Levels to check elev of BM at
51st and Orange

BM	+	-	Elev
BM in church step SE Estrella Orange	0.76		349.21
TP	0.21	12.28	336.93
TP	0.75	9.04	328.10
TP	12.65	13.23	315.62
SPK in pole BM NW 51 52 + Orange		0.99	327.78
TP	12.30	0.99	327.78
TP	13.11	0.29	339.84
TP	12.18	0.10	352.85
TP	12.90	0.28	369.75
set B.P. in SW BM Return 52nd + Orange		0.14	377.51
TP	5.25	0.14	377.51
TP	13.09	1.71	381.05
TP	3.52	6.63	387.51
check on starting SW B.M. 51 52		7.78	383.23
TP	0.54	10.33	380.70
TP	0.17	12.91	368.33
check on BM S.E. B.P. 49th + E. Cajon		# 11.54	356.96

69

327.78
316.15
3.63

357.05

Bliss
 2000 11
 Morgan Morse
 11/26
 8M Mon NW
 28' E

X-sections Alleys Block 66 E W N
 Addition Between E & F 28M + 29⁷⁵ Alley
 Elev 20' wide

183.99

70

	13.18	170.54	157.36
TP	13.02	183.99	0.07 170.47
		0 to 0 = slope of E St	
E Top cb		3.58	79.91
Gutter		3.6	79.9
+3		3.6	79.9
+7		3.5	80.0
±		4.1	79.4
+4		4.5	78.9
+7		4.6	78.9
Gutter		5.7	77.8
W Top cb		5.7	77.75
		0.2' South	
W		2.1	81.4
+2		1.8	81.7
+3		3.9	79.6
+8		4.0	79.5
±		3.8	79.7
+2		3.4	80.1
E		3.0	80.5
Top Retaining Wall on Pop on East		1.61	81.88
		13' South	
E Top Retaining Wall		0.93	82.56
E		1.9	81.6
+5		2.4	81.1
+8		2.9	81.1

±	2.5	81.0
+7	2.3	81.2
+8	1.6	81.9
W	1.6	81.9
	20' South end of Retaining Wall on East	
	0.67	82.82
	30' South	
W	1.7	81.8
±	1.5	82.0
+6	1.0	82.5
E	0.4	83.1
	50' South	
E	0.4	83.1
+3	0.9	82.6
±	1.3	82.2
W	1.7	81.8
	75' South	
W	1.2	82.3
±	1.3	82.2
E	1.0	82.5
	100' South	
E	1.5	82.0
±	1.5	82.0
W	1.3	82.2
	120' South	
W	2.1	81.4

183.49

£	2.5	81.0
+6	2.4	81.1
E	2.4	81.1
132' East		
E	3.2	80.3
£	3.5	80.0
+4	3.5	80.0
W	3.1	80.4

140' East

W	3.7	79.8
+7	4.3	79.2
£	4.4	79.1
E	4.6	78.9

146' South Single Garage on East

on Line Dist floor to 5.7 77.8

156' South N. Line of E & W Alley

E	5.9	77.6
£	5.6	77.9
+4	5.0	78.5
W	4.7	78.8

T.P. 0.27 178.55 5.21 178.28

160 South

W	1.3	77.2
+5	1.5	77.0
£	1.8	76.7
+3	1.6	76.9

178.55

E	2.0	76.5
170' South		
E	3.3	75.2
+6	3.5	75.0
£	3.4	75.1
+4	3.4	75.1
W	3.0	75.5
Set 8 M. fdo. Skimo alley		
	2.69	175.86

177' South Single Garage on East

W	4.2	74.3
+7	4.5	74.0
£	4.7	73.8
+7	4.7	73.8
E	4.2	74.3

4.5 Back Dist floor ctr 4.3 74.2

200' South

E	8.7	69.8
£	8.6	69.9
+2	8.3	70.2
W	8.2	70.3

225' South

W	12.4	66.1
£	12.6	65.9
+6	12.9	66.1
E	12.2	66.3

T.P. 1.02 168.04 11.53 167.02

X
168.04

235' South

E	2.1	65.9
+4	3.3	64.7
+7	3.1	64.9
E	3.4	64.6
W	3.0	65.0

258' South

W	6.0	62.0
+7	6.2	61.8
E	6.7	61.3
+7	7.1	60.9
E	6.0	62.0

273' South

E	8.5	59.5
+4	8.9	59.1
E	9.0	59.0
+2	9.0	59.0
+25	8.7	59.3
W	8.8	59.2

300' South

W-10	14.1	53.9
W	12.5	55.5
+4	12.9	55.1
+9	11.3	56.7
E	11.5	56.5
+6	11.3	56.7
E	10.5	57.5

A
168.04

77

320' South

E	11.6	56.8
+6	11.6	56.4
E	12.1	55.9
W	13.4	54.6
W+10	14.9	53.1

TP	11.95	17.975	0.24	167.80
BM			3.90	175.85
				<u>175.85</u>
				0.1

Bliss
Isbell
Morton
1/17/28

B.M. SPK Pole
SW. E. W. Alley

X Section East & West Alley E W Morse

Subdivision Block 66

+	π	-	Elev
8.12	183.98		175.86

0+00 = E Line Nend S Alley

N		6.6	77.4
+3		7.5	76.5
+7		7.3	76.7
⊕		7.9	76.1
+1		7.6	76.4
S		9.2	74.8

25' East

S-10		11.6	72.4
S-5		10.0	74.0
S		9.7	74.3
+7		9.4	74.6
⊕		8.1	75.9
N		7.1	76.9
N. Top concrete Retaining Wall	5.5'		78.47

50' East

N. Top wall		5.06	78.92
N		7.0	77.0
+6		8.0	76.0
⊕		8.3	75.7
S		9.8	74.2
S+10		10.9	73.1

65' East

S-10		10.5	73.5
S		9.0	75.0

18398

£	7.3	76.7
N	6.8	77.2
	75' East	
N Top Wall	9.54	79.44
N	6.0	78.0
£	7.0	77.0
S	8.4	75.6
St 10	10.3	73.7
	83' East Single Garage on North	
on line Dirt floor ctr	5.4	78.6
	95' East Single Garage on North	
on line Dirt floor ctr	5.3	78.7
	100' East	
S-10	8.1	75.9
S	7.1	76.9
£	6.1	77.9
N	5.6	78.4
	105' East Single Garage on North	+3
on Line Dirt floor ctr	5.7	78.3
	112' East	
N	5.2	78.8
£	5.5	78.5
S	6.3	77.7
St 10	7.5	76.5
	190' East	
S	5.6	78.4

121-3-2 N 07077 700
1+31 5.5 N. 07077
18398

74

£	5.2	78.8
N	4.9	79.1
	155' East	
N	4.3	79.7
£	4.6	79.4
S	5.2	78.8
	165' East	
S	4.7	79.3
£	3.9	80.1
N	3.3	80.7
	200' South	
N	3.6	80.4
+6	3.7	80.3
£	4.0	80.0
S	4.0	80.0
	205' East	
S	4.4	79.6
+3	4.4	79.6
£	4.9	79.1
N	5.0	79.0
	209' East Single Garage on North	
6' Back Out floor ctr	5.3	78.7
	220' East	
N	4.9	79.1
+6	5.1	78.9
£	5.9	78.1

183.98

+9		5.3	78.7
S		5.3	78.7
	242' East		
S		7.4	76.6
£		7.6	76.4
+7		7.3	76.7
N		7.9	76.1
	250' East. West end of Dwelling		
	Parallel's Alley 2' Back Sill	10.6	73.4
N		9.3	74.7
+2		8.7	75.3
£		8.2	75.8
S		7.9	76.1
	271' East		
S		11.1	72.9
£		10.9	73.1
+3		10.5	73.5
N		11.8	72.2
	275 East. End of Dwelling		
	2' Back Sill	10.7	73.3
	278 E		
N		13.0	71.0
£		12.5	71.5
S		12.2	71.8
TR	1.61	173.45	171.84

173.95

75

	293' East Single Garage on North		
	0-6 Back Dirt floor	ctr 3.0	70.5
	297' East		
S		2.9	70.5
£		2.8	70.6
N		3.0	70.5
	308' East Single Garage on North		
	1.5 Back Dirt floor	ctr 4.1	69.4
N		4.0	69.5
+8		3.8	69.7
£		4.1	69.4
+7		4.2	69.3
S		3.5	70.0
	325 East		
S		4.9	68.5
+5		5.6	67.9
£		5.8	67.7
N		5.3	68.2
	344' East Single Garage on South		
N		6.8	66.7
+8		7.0	66.5
£		7.3	66.2
+4		7.0	66.5
S		6.7	66.8
	4.5 Back Wood floor	ctr 6.2	67.3
	355' East		
S		7.6	65.9

7
173 95

+7	8.2	65.3
E	7.8	65.7
N	8.3	65.2

375' East

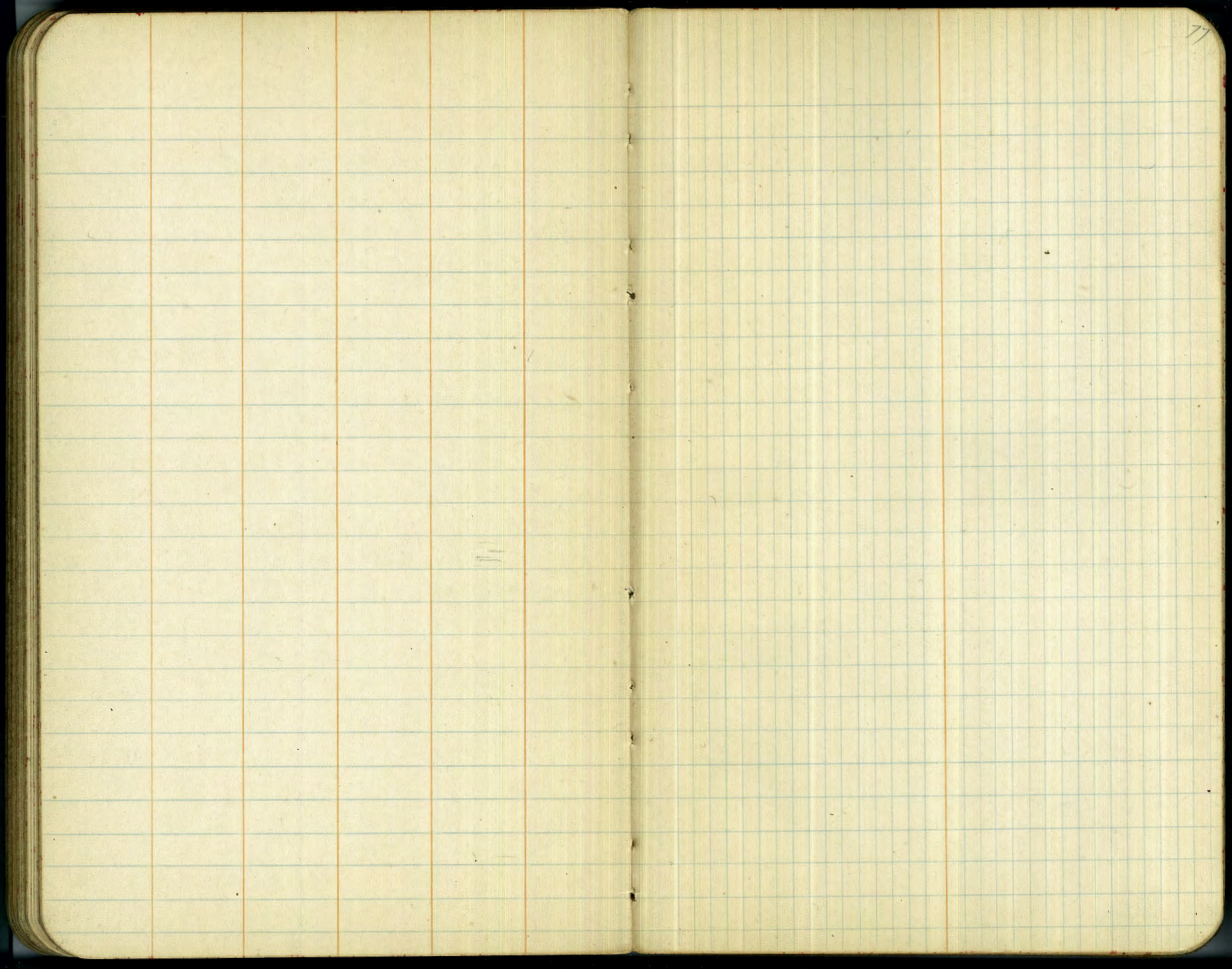
N-10	12.0	61.5
N	10.8	62.7
+7	9.9	63.5
E	10.0	63.5
S	9.7	63.8

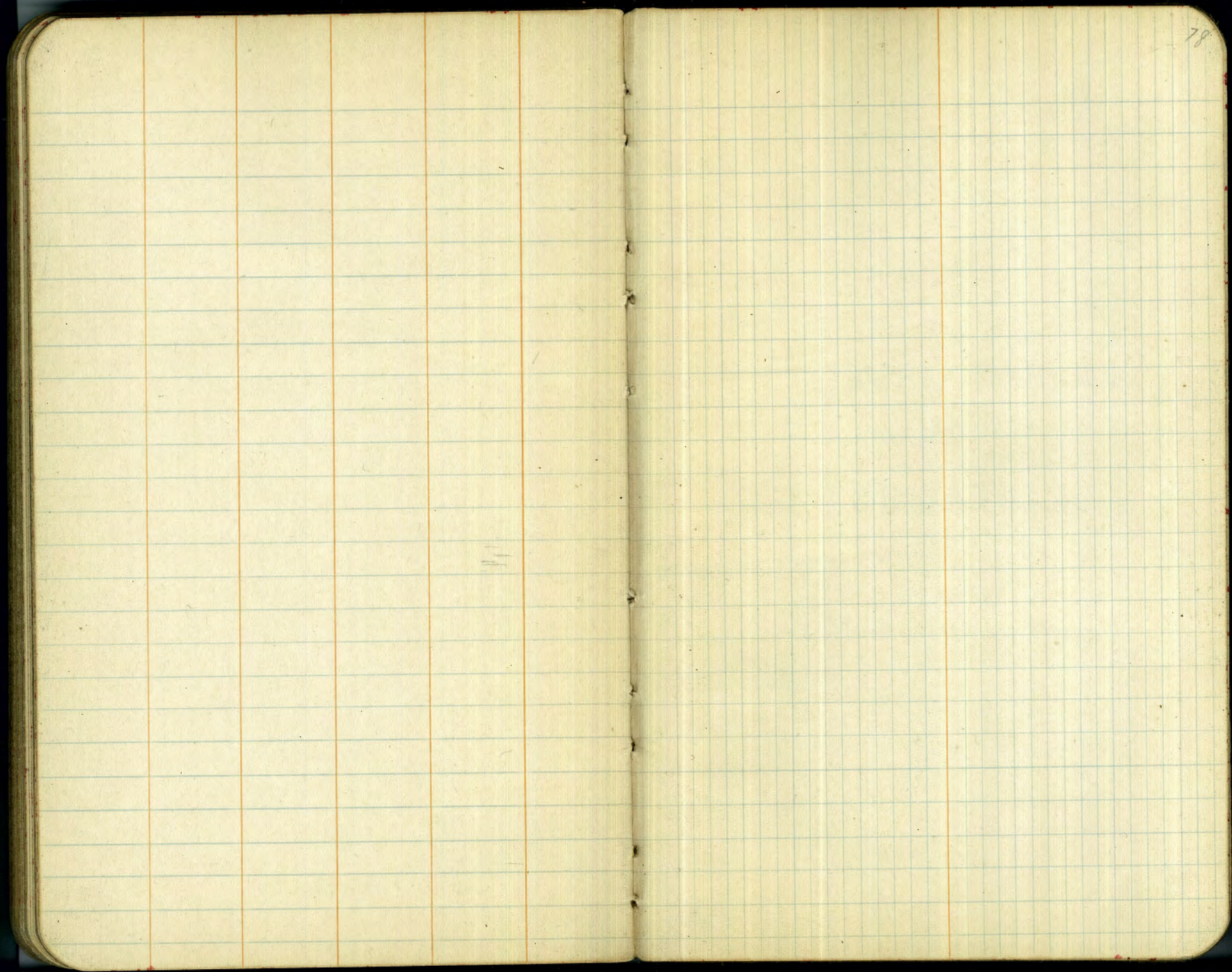
400' East Wline of 29 74

S	12.3	61.2
E	12.8	60.7
N	12.8	60.7
N+10	14.2	59.3

TP	5.84	171.79	7.55	165.90
BNI SEBP 30 21 F			9.80	166.94
				166.94 05 ✓

76





DIRECTIONS FOR USE OF TABLES

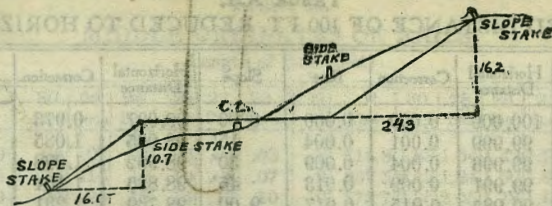
TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width of slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the formula only method in

IMPROVED TABLES AND INFORMATION

TABLE No. 2.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or external), opposite T by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

167
 481
 535
 535
 535
 15.1
 207
 1655
 2235
 481
 535
 535
 535
 15.1
 713.7
 2235
 175.45

59.30

383.45
 59.30
 324.15

325.42
 324.15
 1.27

312
 N-10 12.6
 W 13.5
 E 12.9
 +3 12.8
 +5 12.1
 E 11.3

T.P. 168.00
 0.20
 167.80
 119.5+
 179.75
 390 - B.M.
 175.85 B.M.

95
 40
 03

5

