

1178

LISTS

FIELD BOOK

No. 385



Books 1206

Induct 1206

MICROFILMED

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- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
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**THE FREDERICK POST CO.**  
 ENGINEERING and DRAFTING SUPPLIES  
 IRVING PARK STATION  
 CHICAGO, ILL.



X Sec Catalina Blvd.	Orchard To Voltaire.	1
" " " "	" " " " PTLoma	40
" " " "	" at Voltaire	49
" " Exchange Pl.	Ivenhoe Ave East.	52
" " Catalina PL.	East of Catalina	58
" Derigible Site	Camp Keanny-	59
" " Polk.	35 to Cherokee	62

Berrice Drive <sup>West line Wells to</sup> ~~East line~~ CATALINA Blvd <sup>34</sup> ~~36~~



X Section, Catalina Blvd.  
From N. Orchard St to S.W. Yoltaine St.

12.92 176.83 ✓ 168.91 <sup>511 NW 80' Bank Cont. - Catalina</sup>

T.D. 13.09 189.41 ✓ 0.51 176.32 ✓

T.P. 9.74 199.14 ✓ 0.01 189.40 ✓

North East Return Orchard St 4 Bars

P.C. = 20' ECL. Catalina 3.89 195.75

60 Plopped J.L.M. & Stark 4.00 95.14  
4.16 94.98  
4.45 94.69

E.C. = 20' N.N.L. Orchard 4.72 94.84

N.W. Return Orchard St

P.C. = 20' N.N.L. Catalina 2.55 96.59

2.80 96.34

3.14 96.00

3.42 95.74

E.C. = 20' N.N.L. Orchard 3.71 95.43

100' N.N.L. Orchard = PVC

N cb. 5.18 93.96

E cb. 6.09 93.05

120' N

E cb. 6.52 94.64

W cb. 5.55 93.59

140' N

W cb. 6.08 93.06

E cb. 7.04 94.10

160' N

INK = HATCH  
JUNE 1962

± Santa

± Coronado

± Del Mar

195.93 P.K.

380.25

379.91

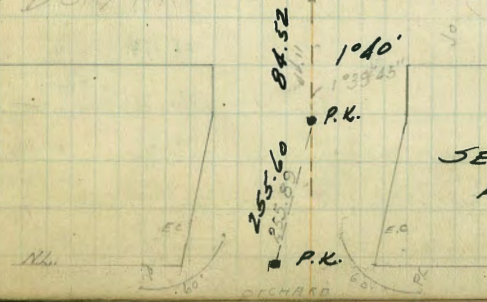
84.52

255.60

P.K.

P.K.

SEE T.P. No. 26  
PAGE 29





199.14 /

E. cb 7.65 191.49  
 W. cb 6.70 94.44

180' N

W. cb 7.47 91.67  
 E. cb 8.40 90.74

200' N = End Vertical Curve

E. cb 9.22 89.94  
 W. cb 8.31 90.83

255.89' N =  $\Delta 41^{\circ}39'15''$

W. cb 10.62 88.54  
 E. cb 11.43 87.71

Del Mar Rye  
 280.4' = P.C. South East Return 4 Parts

T.P. 2.56 189.11 12.59 186.55 ✓

P.C. d 2.56 186.55

1 d 3.29 85.84

2 d 3.92 185.19

3 d 4.30 84.81

E.C. = 20' x 20' Calabona 4.30 84.81

S.W. Return Del Mar 4 Parts

P.C. d 1.69 87.44

1 d 2.35 86.76

2 d 2.82 86.49

3 d 2.79 86.34

E.C. = 20' x 20' Calabona 2.41 86.70

N.W. Return Del Mar

P.C. = 20' x 20' Calabona 3.38 85.73

INK = HATCH  
 JUNE 1962

NIAGARA

NARRAGANSETT

N4

Del Monte

$\Delta = 32^{\circ}28'29''$   
 $R = 200'$   
 $T = 58.25$   
 $L = 113.36$   
 $D_1 = 8.5944$

292.28

P.K.

P.K.

P.K.

P.K.

P.K.

P.K.

P.K.

385.40

213.51

383.29

End of existing cb on East  
 Elev. = 157.47

$\Delta = 40^{\circ}$   
 $R = 250'$   
 $T = 90.99$   
 $L = 174.53$   
 $D_1 = 6.8755$

P.R.C.

P.I.

P.S.

34.17 Ave



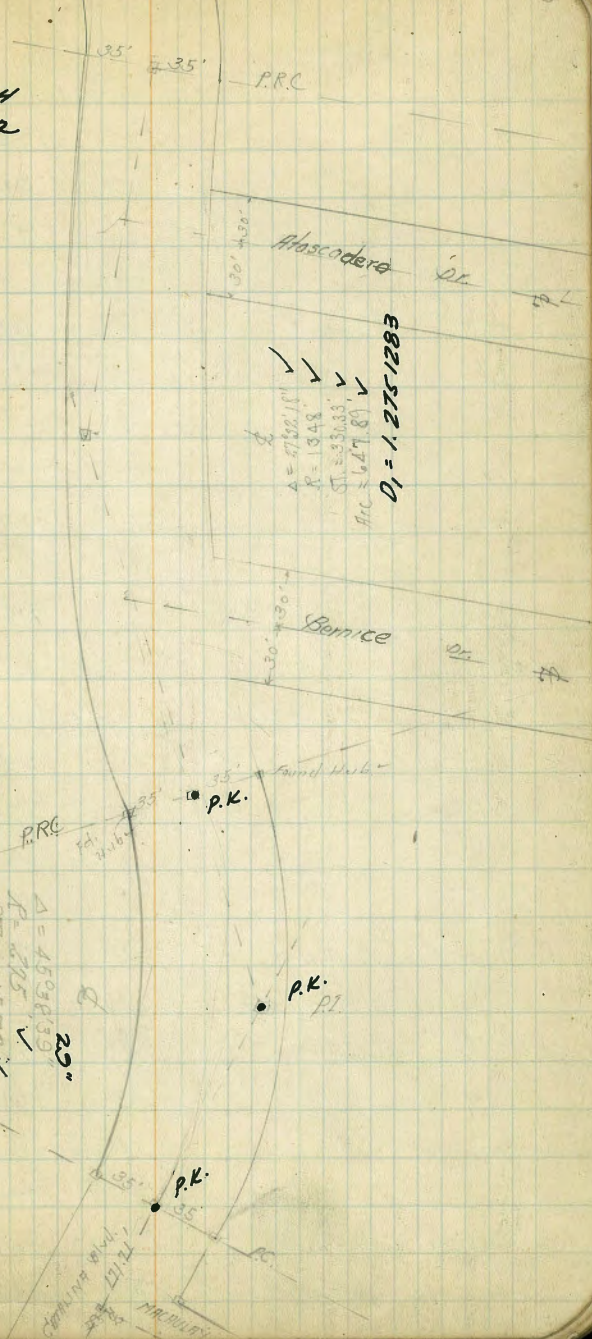
189.11

E cb	3.76	85.35
W cb	4.25	84.86
E cb	4.81	84.30
W cb	5.34	83.77
E.C. = 20' N.N.L. Del Mar		
N.E. Return Del Mar 4 Parts		
E cb	4.83	84.78
W cb	5.06	84.05
E cb	5.28	83.83
W cb	5.80	83.31
E cb	6.33	82.78
E.C. = 20' N.N.L. Del Mar		
40' N.N.L. Del Mar		
E cb	7.11	82.00
W cb	6.13	87.98
60' N		
E cb	7.05	84.06
W cb	8.13	80.98
77' N to 109' N cb on East Washed out		
77' N		
E cb	9.03	80.08
W cb	7.90	81.41
100' N		
W cb	9.12	79.99
109' N		
E cb	10.78	78.33
120' N		
E cb	11.37	77.74
W cb	10.28	78.83

INK = HATCH  
JUNE 1962

$\Delta = 15038.139$   
 $R = 205$   
 $ST = 14572$   
 $L = 219.06$   
 $D_1 = 6.2505$

$\Delta = 4122.11$   
 $R = 1948$   
 $ST = 33033$   
 $MC = 647.8$   
 $D_1 = 1.2751283$









177.86 ✓

PC<sup>cb</sup> = 20' E.E.L. Catalina 5.87 171.99

+ 15 6.67 71.19

+ 30 7.33 70.53

+ 34<sup>cb</sup> = beginning of washed out cb. 7.46 70.40

From above PC + 34 to line + 23.7 cb is washed out

E.C. + 37 = end washed out cb. 8.40 69.46

NW Return at Coronado 4 parts

PC<sup>cb</sup> = 20' W.W. Catalina 3.17 74.69

1 cb. 5.03 77.83

60 cb. 6.09 71.77

1 cb. 6.74 71.14

E.C. = 60' W.W. Coronado 7.24 70.64

100' N N.W. Coronado Ave

W cb. 9.56 68.30

E cb. 10.59 67.77

120' N

E cb. 11.11 66.75

W cb. 10.10 67.76

140' N

W cb. 10.49 67.37

E cb. 11.50 66.36

160' N

E cb. 11.83 66.03

W cb. 10.88 66.98

200' N

W cb. 11.44 66.44

E cb. 12.38 65.48

177.86 ✓

5

T.P. 2.88 16.770 13.04 164.82 ✓

280' N.W.W. Coronado = PC. SW + SE Returns at Guiz <sup>Santa</sup>

SW Return

PC = 20' S.S.L. Santa Cruz 2.16 165.54

1 2.36 65.34

1 2.11 65.59

1 1.26 66.44

EC = 20' W.W. Catalina 0.14 67.56

S.E. Return

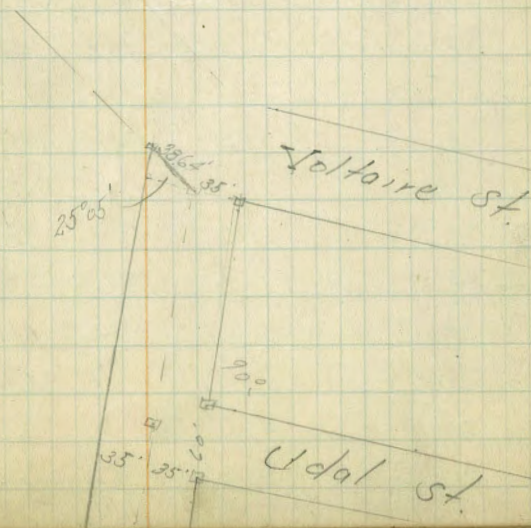
PC = 20' S.S.L. Santa Cruz 3.22 64.48

1 3.44 64.46

1 3.34 64.36

1 2.55 65.15

EC = 20' E.E.L. Catalina 1.37 66.33





16770 ✓

N.E. Return at Santa Cruz

PC = 20' E.E.L. Catalina	3.19	164.51
	4.33	63.37
	5.11	64.59
	5.75	61.95

EC = 20' N.N.L. Santa Cruz

N.W. Return at Santa Cruz

PC = 20' N.W.L. Catalina	2.11	65.59
	2.28	65.44

Check on BM <sup>60</sup> <sub>4 parts</sub>

3.80 63.70

4.07 63.63

4.71 64.99

EC = 20' N.N.L. Santa Cruz

5.24 64.46

<sup>70' wide</sup>  
N. Section CATALINA Blvd. for Tardage

BM N.W. of Santa Cruz + Catalina

FROM N.E. SANTA CRUZ TO S.L. VOLTAIRE ST. <sup>14' ch.</sup> <sub>10.5' 408</sub>

N 0.8 63.78

Ch. Ground 1.6 64.98

1/4 1.8 64.78

C 2.3 64.48

1/4 2.4 64.18

Ch. Ground 2.6 61.98

E 3.0 64.58

50' N N.L. Santa Cruz

164.58 ✓

E 3.4 161.18

Ch. Ground 3.3 61.78

Top Ch. 4.23 60.35

1/4 3.1 61.18

C 3.35 61.08

1/4 3.5 61.08

Gutter 3.6 60.98

Ch. 3.26 61.34

N 3.0 61.58

100' N

N 4.3 60.78

Ch. Ground 4.1 60.18

Top Ch. 4.85 59.73

1/4 4.3 60.48

C 4.3 60.48

1/4 4.3 60.48

Ch. Ground 4.3 60.78

Top Ch. 5.88 58.70

E 4.2 60.38

155.87' N = PC. 2 stations

E 5.2 59.38

Ch. Ground 5.2 59.38

Top Ch. 6.50 58.08

1/4 5.2 59.38

C 5.3 59.48

1/4 5.2 59.38



164.58 ✓

Cb. Ground	5.1	59.48
Cb	5.52	59.06
N	5.1	59.48

212.55' N = Middle of Curve

N	5.0	59.58
Top Cb.	5.62	59.96
Gutter	5.8	59.78

'14	5.8	59.78
-----	-----	-------

C	5.9	59.68
---	-----	-------

'12	5.8	59.78
-----	-----	-------

Gutter	5.9	59.68
--------	-----	-------

Top Cb.	6.64	59.94
---------	------	-------

E	6.0	58.58
---	-----	-------

269.23' N = PRC

E	6.4	58.18
---	-----	-------

Cb. Ground	6.3	59.78
------------	-----	-------

Top Cb.	6.83	59.75
---------	------	-------

'14	6.3	58.78
-----	-----	-------

C	6.1	58.48
---	-----	-------

'12	5.9	59.68
-----	-----	-------

Gutter	6.1	59.48
--------	-----	-------

Top Cb.	5.79	58.79
---------	------	-------

N	5.2	59.38
---	-----	-------

323.69' N = Section Rt. Angle to Catalina on SL Del Norte

N	5.3	59.78
---	-----	-------

Cb. Ground	5.6	58.98
------------	-----	-------

164.58 ✓

7

Top Cb.	5.95	58.63
---------	------	-------

'14	6.0	58.58
-----	-----	-------

E	6.1	58.48
---	-----	-------

'12	6.5	58.08
-----	-----	-------

Cb. Ground	6.7	57.88
------------	-----	-------

Top Cb.	6.85	57.73
---------	------	-------

405.62' N = Section of Rt. Angle to Catalina on SL Del Norte

E	6.7	57.88
---	-----	-------

Cb.	7.11 for end existing	57.47
-----	-----------------------	-------

Gutter	7.2	57.38
--------	-----	-------

'14	6.3	58.78
-----	-----	-------

E	5.9	58.68
---	-----	-------

'12	5.6	59.98
-----	-----	-------

Cb. Ground	5.3	59.78
------------	-----	-------

N	5.2	59.38
---	-----	-------

443.76 = EC = 0 + 00

N	5.7	58.88
---	-----	-------

Top Cb.	6.38	58.70
---------	------	-------

Gutter	6.6	57.98
--------	-----	-------

'14	6.3	58.78
-----	-----	-------

E	6.3	58.78
---	-----	-------

'12	6.9	57.68
-----	-----	-------

+2	7.4	57.18
----	-----	-------

Cb. Ground	7.4	57.18
------------	-----	-------

E	6.9	57.68
---	-----	-------



16458 ✓

LEVELS on Returns of Del Monte  
 (North)  
 South west return

P.C. = 16' N.W. Catalina 2.91 161.67

3.84 60.74

4.71 59.87

5.39 59.19

E.C. = N.W. Del Monte 5.87 58.71

(South)  
 N.W. RETURN

P.C. = 16' N.W. Catalina 3.35 61.43

4.32 60.46

5.22 59.36

5.57 59.01

E.C. = S.W. Del Monte 5.96 57.64

T.P. 4.40 162.47 ✓ 6.51 158.07 ✓

4 + 13.75 = E.C. Page 7 = 0 + 0.0  
 50' N of E.C.

E 4.7 57.77

cb. 3.7 56.77

1/4 5.3 56.97

1/4 4.8 57.67

1/4 4.5 57.97

Gutter 4.2 57.27

top cb. 4.35 58.17

W 3.8 58.67

100' N of E.C.

W 4.3 58.17

cb. Ground 5.1 57.37

162:47 ✓

W	4.8	157.67
C	5.2	57.27
1/4	5.4	57.07
+2	5.8	56.67
cb	5.9	56.57
+2	5.9	56.57
+3	5.5	56.97
E	5.3	57.17
	150' N of E.C.	
E	5.3	57.17
+9	5.8	56.67
+10	6.2	56.27
cb	6.2	56.27
+6	6.3	56.17
1/4	5.7	56.77
1/4	5.4	57.07
1/4	5.1	57.37
Gutter	5.2	57.27
top cb.	4.67	57.80
W	3.9	58.57
	200' N of E.C.	
W	4.2	58.27
top cb.	4.87	57.65
Gutter	5.4	57.07
1/4	5.4	57.07
1/4	5.7	56.77



162.47 ✓

1/4	5.9	56.57
+ 4	5.9	56.57
+ 5	6.6	55.87
cb	6.7	55.77
+ 2	6.7	55.77
+ 3	6.4	56.07
E	5.6	56.87
25286' N of E.C. = S.L. NARRAGANSETT S.L.		
E	5.8	56.67
+ 6	5.5	56.97
+ 7	7.0	55.47
cb	6.9	55.57
1/4	6.1	56.37
E	5.7	56.77
1/4	5.3	57.17
cb. Ground	4.9	57.57
W	4.3	58.17
E NARRAGANSETT Pt. Angles to Calalina		
W	4.5	57.97
cb	5.0	57.47
1/4	5.0	57.47
E	5.9	56.57
1/4	6.2	56.27
cb	7.2	55.27
+ 5	7.3	55.17
cb + 10	6.3	56.17
E	6.3	56.17

162.47 ✓

9

N.E.L. NARRAGANSETT = 0 + 00 Pt. Angles to Calalina

E	6.3	56.17
+ 10	6.7	55.77
+ 11	7.7	54.77
cb	7.8	54.67
+ 4	6.6	55.87
1/4	6.5	55.97
E	6.2	56.27
1/4	5.8	56.67
cb. Ground	5.7	56.77
W	4.5	57.97

Levels on South West + N.W. Returns of Narragansett  
South West Return 4 Parts

PC = 26' S.S.L. Narragansett	4.92	57.55
	4.87	57.60
	4.37	58.10
	3.07	59.40
EC = 25' N.W. Calalina	1.67	60.80

N.W. Return 4 Parts

PC = 25' N.W. Calalina	2.81	59.63
	4.06	58.41
	4.82	57.65
	5.29	57.18
EC = 26' N.W. Narragansett	5.71	56.76
50' N N.L. NARRAGANSETT		
W	5.9	56.57



162.47 ✓

top cb.	6.55	55.94
Gutter	6.9	55.57
1/2	7.1	55.37
2	7.1	55.37
1/4	7.5	54.97
+2.	7.6	54.87
cb.	9.1	53.37
+3	7.6	54.87
E	7.6	54.87
100' N		
E	8.7	53.77
+10	9.6	54.87
+11	11.3	51.17
cb.	10.8	51.67
1/4	8.8	53.67
2	8.5	53.97
1/4	8.3	54.17
Gutter	8.1	54.37
top cb.	7.85	54.67
N	7.4	55.07
150' N		
W	9.2	53.47
top cb.	9.17	53.30
Gutter	9.6	54.87
1/2	9.7	54.77
2	9.9	54.57

162.47

10

1/4	10.3	54.17
+7	11.1	51.37
cb.	12.8	49.67
+4	11.4	51.07
E	10.4	54.07
200' N		
E	12.2	50.27
+7	13.7	49.77
+8	13.6	48.87
cb.	14.0	48.47
+3	12.4	50.07
1/4	11.6	50.87
2	11.5	50.97
1/4	11.4	51.07
Gutter	11.1	51.37
top cb.	10.48	51.99
N	10.5	51.97
250' N		
T.P. 228.	152.50 ✓	1225
W	1.9	50.60
top cb.	1.85	50.85
Gutter	2.8	49.70
1/4	2.6	49.90
2	2.9	49.60
1/4	3.0	49.50
+2	5.5	47.00



152.50 ✓

cb.	7.8	144.70
+6	6.8	45.70
+7	3.1	49.40
E	3.2	49.30
+5	4.8	47.70
+10	3.2	49.30

225' N

-10	4.2	48.30
-3	5.5	47.00
E	4.3	48.40
+2	8.9	43.60
cb.	7.6	44.90
+5	7.6	44.90
+6	4.1	48.40
1/4	3.7	48.80
∅	3.6	48.90
1/4	3.3	49.40
Gutter	3.3	49.40
Top cb.	2.49	50.01
W	2.40	50.10

303.29 = S.L. NIAGARA

W	2.8	149.7
cb. Ground	4.1	48.40
1/4	4.6	47.90
∅	4.7	47.80
1/4	5.0	47.50

152.50 ✓

+5	5.2	147.30
+6	9.3	43.40
cb.	9.8	44.70
+4	11.2	41.30
+9	10.3	42.40
+10	5.3	47.40
E	5.7	46.80
+5	6.0	46.50

343.29 = <sup>North</sup> 40' North S.L. NIAGARA Pt. Angles to Catarina

-10	8.8	43.70
-4	10.8	41.70
E	7.8	44.70
+3	7.8	44.70
+4	12.5	40.00
cb.	11.3	41.40
+2	7.6	44.90
1/4	6.6	45.90
∅	6.3	46.20
1/4	6.8	45.70
cb.	5.8	46.70
W	4.1	48.40

353.29 = 80' N S.L. Niagara = 0+00

W	7.1	45.40
cb.	9.1	43.40
1/4	8.8	43.70
∅	8.5	44.00

Error → ~~45.40~~



152.50 ✓

1/4	8.9	143.60
cb.	9.6	144.90
+3	14.1	38.40
+10	13.6	38.9
E	11.1	41.40
+5	10.8	41.70

## Levels on South West Return at Niagara

P.C. = 29' W.W. Cololima	+ 0.25	54.75
	1.60	50.90
	2.85	49.65
	3.06	49.44
E.C. = 22' S.S. Niagara	2.60	49.90

T.P. 0.45 150.45 ✓ 2.50 150.00 = + Niagara

60' North

-10	12.0	38.45
E	14.0	36.45
+3	11.8	38.65
cb.	12.9	37.55
+1	14.0	36.45
+6	13.3	37.15
+9	10.8	39.65
1/4	10.1	40.35
E	10.1	40.35
1/4	10.2	40.75
cb.	11.0	39.45
1/4	9.4	41.05

150.45 ✓

12

T.P. 1.62

139.57 / 12.50

137.95

110' N

1/4	2.0	137.57
cb.	2.3	37.47
1/4	2.2	37.37
1/4	2.3	37.77
1/4	2.6	36.97
+7	3.3	36.47
cb.	4.3	35.77
+8	3.8	35.77
E	3.4	36.17
+5	3.3	36.77

143.25 North N.L. Niagara = S.L. Macaulay

-5	4.5	35.07
E	4.5	35.07
cb.	5.6	33.97
+3	6.5	33.07
+5	5.3	34.47
1/4	4.3	35.77
E	3.8	35.77
1/4	3.7	35.87
cb.	5.4	36.17
1/4	3.4	36.17

South of Macaulay

1/4	3.7	35.87
cb.	3.8	35.77

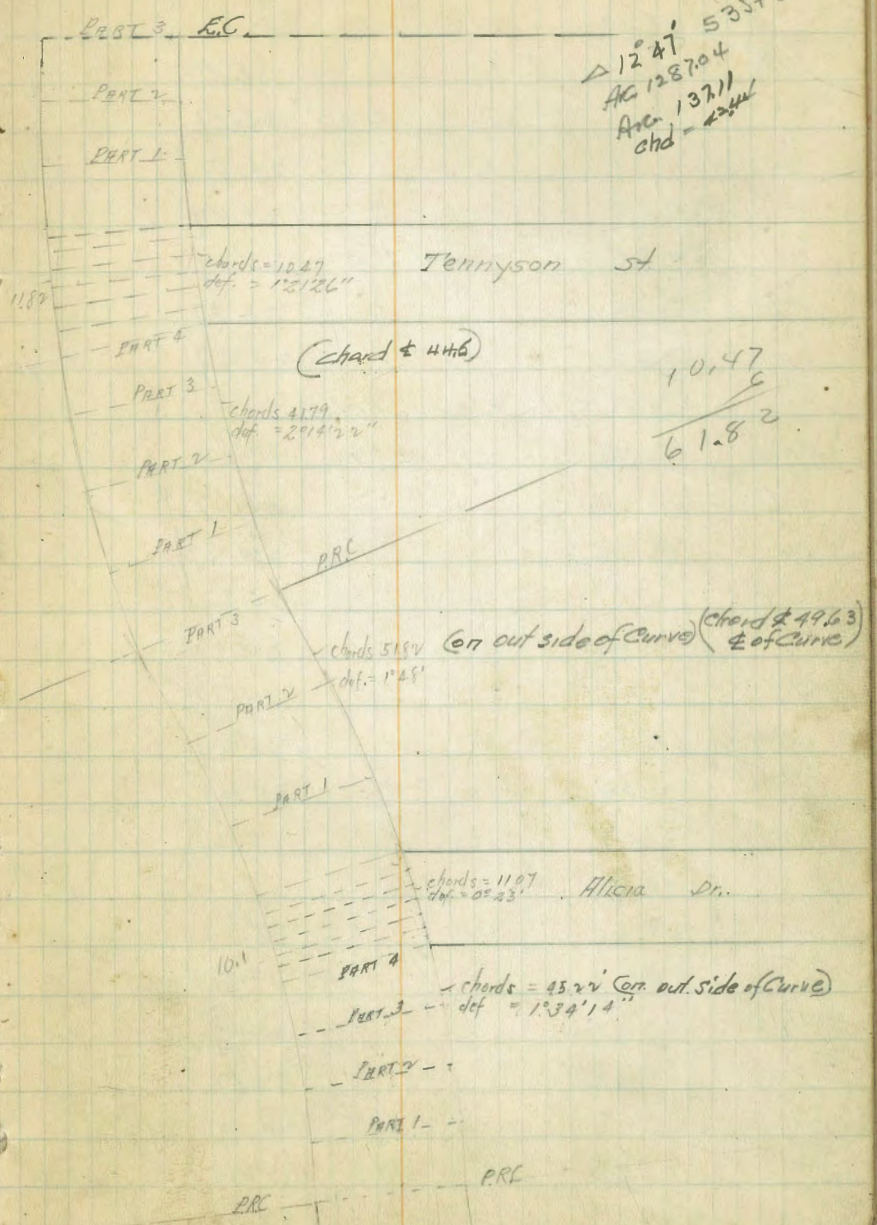
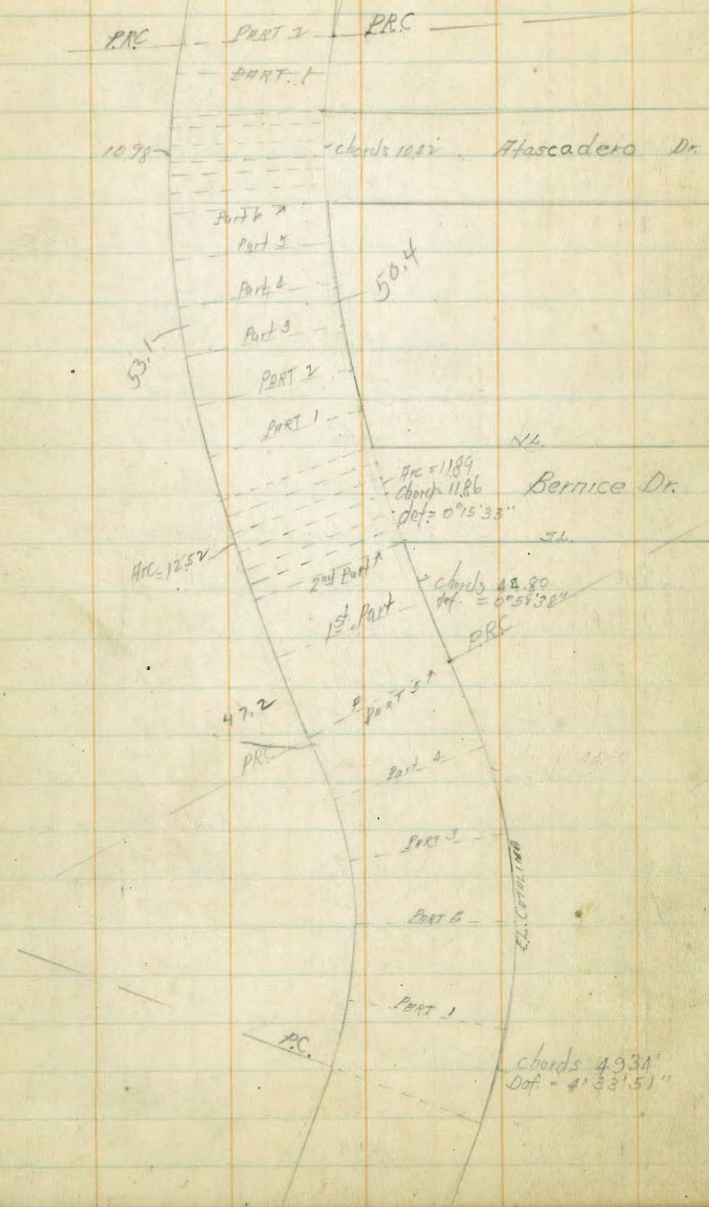
Sections  
of  
10' cb.  
10' 1/2



10.524  
2.5  
6

$\Delta 12^\circ 47'$  535+35  
Arc 1287.04  
Area 137.11  
chd - 234.4

10.47  
6  
61.82





139.57 ✓

W	4.0	135.57
E	4.4	35.17
1/4	4.7	34.87
+4	5.1	34.47
+7	6.5	33.07
cb	5.6	33.97
E	4.7	34.87
South 1/4 Macaulay		
E	4.9	34.67
cb	5.9	33.67
+2	6.9	34.67
+4	5.7	33.87
W	5.7	34.47
E	4.7	34.87
1/4	4.3	35.27
cb	4.5	35.27
N	5.8	35.77
E Macaulay		
N	4.1	35.47
cb	4.7	34.87
1/4	4.7	34.87
E	5.0	34.57
1/4	5.5	34.07
+4	5.6	33.97
+9	7.1	34.47

139.57 ✓

14

cb	5.9	133.67
E	5.1	34.47
N 1/4 Macaulay		
E	5.4	34.17
cb	6.2	33.37
+2	7.3	37.77
+6	6.0	33.57
1/4	5.5	34.07
E	5.1	34.47
1/4	5.0	34.57
cb	5.1	34.47
N	3.7	35.87
N cb Macaulay		
N	3.0	36.57
+10	5.4	34.17
cb	5.4	34.17
1/4	5.1	34.47
E	5.4	34.17
1/4	5.8	33.77
+5	6.1	33.47
+8	7.3	37.77
cb	6.4	33.17
E	5.8	33.77
N 1/4 Macaulay = 0+00		
E	5.9	33.67
+11	6.6	37.97



cb.	6.6	137.97
+1	7.7	31.87
+6	6.5	33.07
1/4	6.0	33.57
1/2	5.7	33.87
1/4	5.4	34.17
1/2	5.6	33.97
W	2.7	36.87

50' N N.L. Macaulay

W	0.7	38.87
+12	4.9	34.67
cb.	7.0	37.57
1/4	6.6	37.97
1/2	6.5	33.07
1/4	6.8	37.77
+4	7.0	37.57
+5	8.4	31.17
cb.	8.4	31.17
E	7.4	37.17

100' N

E	8.7	30.87
+7	9.2	30.37
+9	10.5	29.07
cb.	8.3	31.27
1/4	7.3	34.27
1/2	7.5	37.07

W	7.7	131.87
cb.	8.3	31.27
+2	6.3	33.27
W	3.7	35.87

14.21' N = P.C. 5 PARTS See sketch Page 13

W	7.5	37.07
+11	8.2	31.37
+12	9.9	29.67
cb.	9.9	29.67
1/4	9.1	30.47
1/2	8.7	30.87
1/4	8.5	31.07
+5	8.6	30.97
+7	12.5	27.07
+9	12.5	27.07
cb.	10.0	29.57
E	8.2	31.37

1st PART.

E	9.0	30.57
+13	11.0	28.57
cb.	14.1	25.47
+3	14.1	25.47
+4	11.3	28.27
W	9.8	29.77
1/2	10.2	29.37
1/4	10.4	29.17



+8	10.8	148.77
cb	11.7	147.87
+3	11.7	147.87
+4	10.5	149.07
W	10.1	149.47

2<sup>nd</sup> Part

W	11.9	147.67
+6	11.7	147.87
+7	13.1	146.47
cb	14.9	144.67
+2	12.6	146.97
W	12.2	147.37
♀	11.9	147.67
+8	11.6	147.97
W	13.1	146.47
+8	15.9	143.67
cb	13.6	145.97
E	10.6	148.97
T.P.	0.50	127.41
	12.66	126.91

3<sup>rd</sup> Part

E	0.5	146.91
+6	0.9	146.51
cb	3.3	144.11
+J	1.6	145.81
W	1.2	146.41
♀	1.4	146.01

W	1.9	145.51
cb	2.6	144.81
+4	2.5	144.91
+5	1.2	146.41
W	1.1	146.31

4<sup>th</sup> Part

W	3.4	144.01
cb	3.8	143.61
W	3.8	143.61
♀	3.5	143.91
W	3.6	143.81
cb	3.9	143.51
E	2.3	145.11

5<sup>th</sup> PART = PRC. South of Bernice

1/3 Parts to S.L. of  
Bernice from  
P.R.C. See sketch

E	4.1	143.31
cb	4.5	144.91
W	4.5	144.91
♀	4.5	144.91
W	4.6	144.81
cb	4.6	144.81
W	4.6	144.81

PART 1

W	5.3	144.11
cb	5.1	144.31
W	5.2	144.41
♀	5.1	144.31



1/4	5.1	71.31
cb.	5.2	71.41
E	4.9	71.51
E	5.7	71.71
cb.	5.6	71.81
1/4	5.6	71.81
2	5.7	71.71
1/4	5.8	71.61
cb.	5.7	71.71
1/4	5.6	71.81

20th PART = S.L. Bernice Dr. H. Angles to Catalina

CBS = 1189  
1/4 = 1189

South cb. Bernice Dr. H. Angles to Catalina

1/4	5.6	71.81
cb.	5.9	71.51
1/4	5.8	71.61
2	5.8	71.61
1/4	5.8	71.61
cb.	5.7	71.71
E	5.8	71.61

South 1/4

E	5.9	71.51
cb.	5.9	71.51
1/4	5.9	71.51
2	6.0	71.41
1/4	5.9	71.51
cb.	5.9	71.51
1/4	5.7	71.71

E. Bernice Dr. H. Angles to Catalina

1/4	6.2	71.41
cb.	6.3	71.11
1/4	6.2	71.41
2	6.2	71.41
1/4	6.1	71.31
2	6.2	71.41
E	6.1	71.31

N 1/4

E.	6.2	71.71
cb.	6.3	71.11
1/4	6.2	71.41
2	6.4	71.01
1/4	6.3	71.11
cb.	6.3	71.11
1/4	6.3	71.11

N cb.

1/4	6.4	71.01
cb.	6.5	70.91
1/4	6.5	70.91
2	6.4	71.01
1/4	6.4	71.01
cb.	6.4	71.01
E	6.1	71.31

N.L. Bernice Dr. H. Angles to Catalina

E	6.2	71.41
---	-----	-------



cb	6.4	171.01
1/4	6.5	70.91
E	6.5	70.91
1/4	6.6	70.81
cb	6.5	70.91
W	6.5	70.71

## PART 1

W	7.2	70.71
cb	7.2	70.71
1/4	7.2	70.71
E	7.2	70.71
1/4	7.1	70.31
cb	6.9	70.51
E	6.7	70.71

## PART 2

E	7.3	70.11
cb	7.5	19.91
1/4	7.7	19.71
E	7.8	19.61
1/4	7.9	19.51
cb	7.9	19.51
W	7.9	19.51

T.P. 275 12189 827 11914

## PART 3

W	3.2	118.69
cb	3.1	18.79

on PI Hub Bot  
Barrie  
+ Alascadero Dr.

1/4	30	118.89
E	29	18.99
1/4	28	19.09
cb	27	19.19
E	22	19.69

## PART 4

E	31	18.79
cb	33	18.59
1/4	33	18.59
E	32	18.69
1/4	36	18.79
cb	40	17.89
+3	32	18.69
W	28	19.09

## PART 5

W	26	19.49
+6	37	18.19
+7	48	17.09
cb	47	17.19
+4	46	17.49
+5	38	18.09
1/4	38	18.09
E	32	18.69
1/4	35	18.39
cb	40	17.89
E	31	18.79



PART 6 = St. Mascadero Dr.

E	3.3	118.59
+9	3.6	18.49
cb	4.7	17.19
1/4	3.9	17.99
£	3.7	18.19
1/4	3.8	18.09
+4	4.0	17.89
+6	5.5	16.39
cb	5.5	16.39
+9	4.9	16.99
N	3.6	18.49
South cb		
N	3.8	18.09
+12	5.1	16.79
+13	7.0	14.89
cb	5.4	16.49
+6	4.3	17.59
1/4	4.3	17.59
£	3.8	18.09
1/4	4.0	17.89
+5	4.1	17.79
cb	5.2	16.69
+2	4.2	17.69
E	3.6	18.49

South N

E	3.4	118.49
+10	4.0	17.89
+11	5.4	16.49
cb	5.4	16.49
+4	4.3	17.59
1/4	4.3	17.59
£	4.0	17.89
1/4	4.3	17.59
+5	4.4	17.49
+8	5.5	16.39
+9	6.8	15.09
cb	6.8	15.09
+1	6.8	15.09
+2	4.6	17.49
+11	4.4	17.49
N	3.4	18.49
St. Mascadero Dr. Rt. Angles to Catalina		
N	4.9	16.99
+11	4.8	17.09
+12	8.4	13.49
cb	8.4	13.49
+1	5.8	16.09
+5	4.8	17.09
1/4	4.6	17.49
£	4.3	17.59
1/4	4.3	17.59



+5	4.6	117.49
+7	5.8	16.09
cb.	5.8	16.09
+3	4.0	17.89
E	3.4	18.49
N W		
E	3.5	18.39
+10	4.4	17.49
+12	6.1	15.79
cb.	6.1	15.79
+4	6.1	15.79
+6	4.6	17.49
W	4.4	17.49
d	4.6	17.49
W	4.8	17.09
+5	4.8	17.09
+9	6.7	15.19
cb.	8.3	13.59
+3	8.3	13.59
+4	4.8	17.09
W	4.9	16.99
N cb.		
W	4.7	17.19
+12	5.1	16.79
+13	8.8	13.09
cb.	8.8	13.09

+2	8.8	113.09
+3	5.1	16.49
W	5.2	16.69
d	5.0	16.89
W	4.7	17.19
+7	4.9	16.99
+8	6.5	15.39
cb.	6.5	15.39
+4	4.5	17.39
E.	4.0	17.89
N. H. Atascadero at St. Angles to Catalina		
E	4.1	17.79
+11	4.9	16.99
+12	6.7	15.19
cb.	6.7	15.19
+1	6.6	15.49
+2	5.6	16.49
W	5.0	16.89
d	5.1	16.79
W	5.4	16.39
+5	5.6	16.49
+6	8.9	12.99
cb.	8.9	12.99
+1	5.3	16.59
+8	5.5	16.39
W	3.9	17.99



121.89 ✓

## PART 1

N	3.7	118.19
+4	7.3	14.59
+11	7.0	14.89
+12	10.0	11.89
cb	10.0	11.89
+5	10.0	11.89
+6	7.6	14.49
1/4	7.1	14.79
2	6.6	15.49
1/4	6.5	15.39
+8	7.4	14.49
+9	8.4	13.49
cb	8.4	13.49
+2	8.4	13.49
+3	6.1	15.79
E	5.5	16.39

## PART 2 = PRC bet. Ascadero + Alicia

E	7.4	14.49
+11	8.1	13.79
+12	10.9	10.99
cb	10.9	10.99
+8	9.2	14.69
1/4	8.6	13.49
2	8.8	13.09
1/4	9.2	14.69

121.89 ✓

21

+4	9.4	114.49
+5	10.8	11.09
cb	10.8	11.09
+1	9.2	14.69
+10	9.1	14.79
N	7.4	14.49
T.P. 0.86	111.35 ✓	11.40
		110.49 ✓

## PART 1

N	+0.9	14.75
+2	0.3	11.05
+11	0.0	11.35
+12	2.9	8.45
cb	0.5	10.85
N	+0.2	11.55
2	+0.6	11.95
1/4	+0.5	11.85
+7	0.0	11.35
+8	1.8	9.55
cb	1.8	9.55
+6	1.8	9.55
+7	+0.3	11.65
E	+0.6	11.95

## PART 2

E	0.8	10.55
+10	0.9	10.45
+11	2.7	8.65



cb	2.7	108.65
+3	2.7	8.65
+4	1.2	10.15
W	1.2	10.15
L	1.2	10.15
1/4	1.3	10.05
+8	1.5	9.85
cb	3.0	8.35
+2.9	5.2	6.15
+3	2.1	9.45
N	1.1	10.45

## PART 3

N	3.0	8.35
+12	3.3	8.05
+13	6.8	4.55
L	6.8	4.55
+1	3.8	7.55
1/4	3.0	8.35
L	2.7	8.65
W	2.7	8.65
+4	2.6	8.75
+5	4.4	6.95
cb	4.3	7.05
+3	4.3	7.05
+4	2.4	8.95
L	2.0	9.35

## PART 4 = SL. Alicia Dr.

E	4.0	107.35
+6	4.0	7.35
+7	5.0	6.35
cb	5.7	5.65
+6	5.5	5.85
1/4	4.2	7.15
L	3.9	7.45
1/4	4.4	6.95
+6	4.6	6.75
cb	7.3	4.05
+5	7.3	4.05
+6	4.9	6.45
N	4.9	6.45

## South cb. Alicia Dr.

N	4.9	6.45
+11	5.3	6.05
+12	8.4	7.95
cb	7.5	3.85
+4	4.9	6.45
1/4	4.6	6.75
L	4.6	6.75
+5	2.7	6.65
+6	6.4	4.95
1/4	6.2	5.15
cb	6.0	5.35



+9	4.4	07.0
E	4.4	106.95
	South 1/4	
E	4.6	6.75
cb.	4.9	6.5
+7	4.9	6.5
1/2	6.8	4.6
+7	6.7	4.7
E	5.0	6.4
1/2	5.1	6.3
+6	4.8	6.6
+8	9.2	2.2
cb.	9.2	2.2
+3	8.4	3.0
+4	6.2	4.2
N	5.0	6.35
	E. Alicia Rt. Huelmo de Calatana	
N	5.7	5.65
+12	5.9	5.5
+13	9.0	2.4
cb.	9.0	2.4
+2	6.7	4.7
1/2	5.5	5.9
E	5.4	105.95
+8	5.4	6.0
1/2	7.4	4.0

+5	7.4	4.0
+6	5.5	5.9
cb.	5.3	6.1
E	5.2	106.15
	N 1/4	
E	5.1	6.75
cb.	5.6	5.8
+3	5.3	6.1
+4	7.7	3.7
1/2	7.8	3.5
+3	7.5	3.6
+1	5.9	5.5
E	6.0	5.4
1/4	5.8	5.6
+1	6.0	5.4
cb.	9.2	2.2
+5	9.2	2.2
+6	6.2	5.2
N	6.2	5.15
	N cb.	
N	6.0	5.35
+11	6.7	4.7
+12	9.5	1.9
cb.	9.5	1.9
+2	7.4	4.0
1/4	6.1	5.3



L	6.2	5.2
+3	6.2	6.2
+4	8.2	3.2
$\frac{1}{4}$	8.3	3.1
+1	6.3	5.1
cb	5.9	5.5
E	5.7	105.65

N. to Alicia St. Angles to Catalina

E	6.1	5.75
cb	6.2	5.2
+5	6.2	5.2
+6	8.9	2.5
$\frac{1}{4}$	8.9	2.5
+2	8.9	2.5
+3	6.5	4.9
L	6.5	4.85
$\frac{1}{4}$	6.4	5.0
cb	7.6	3.8
+1	7.6	3.8
+2	10.8	0.6
+4	6.7	4.7
W	6.6	4.75

PART 1

W	8.6	7.75
+12	8.8	2.6
+13	12.9	98.5

cb	10.8	0.6
$\frac{1}{4}$	9.0	2.4
L	8.6	102.75
+7	8.7	2.7
$\frac{1}{4}$	12.9	98.5
+4	12.9	98.5
+6	8.6	2.8
cb	8.6	2.8
E	8.1	103.75

PART 1 + 35

E	9.6	1.75
cb	10.0	1.4
W	10.0	1.4
+2	16.6	94.8
L	16.6	94.75
+3	16.6	94.8
+5	10.4	01.0
W	10.4	01.0
+6	12.3	99.1
cb	15.7	95.7
+4	10.3	01.1
W	10.2	01.15

PART 2

W	10.6	100.75
cb	10.9	00.5
+2	10.9	00.5



+3	18.00	93.4
1/4	18.0	93.4
+4	18.0	93.4
+5	11.1	90.3
L	11.1	100.25
1/4	10.7	90.7
cb	10.7	90.7
E	10.5	100.85

PART 3 = P.R.C. South of Tennessee St.

T.P	0.39	99.32 ✓	12.42	98.93 ✓
E		0.7	98.64	
cb		0.9	98.4	
1/4		0.9	98.4	
L		0.9	98.42	
+8		1.2	98.1	
1/4		7.5	91.8	
cb ✓		7.6	91.7	
+2		7.6	91.7	
+3		1.4	97.9	
N		1.3	98.04	

PART 1

N	2.8	96.54
+6	3.1	96.2
+8	8.6	90.7
cb	8.6	90.7
+6	8.6	90.7

+7	3.9	95.4
1/2	3.3	96.0
L	2.8	96.52
1/4	2.8	96.5
cb	2.7	96.6
E	2.2	97.14

PART 2

E	4.5	94.84
cb	4.8	94.5
1/4	4.7	94.6
L	4.9	94.42 c
+9	4.9	94.4
1/4	10.0	89.3
+10	10.0	89.3
cb	5.3	94.0
N	5.4	93.94

PART 3

N	7.7	91.64
+1	11.0	88.3
+11	11.0	88.3
+12	8.2	91.1
cb	7.7	91.6
1/4	7.4	91.9
L	6.6	92.72
1/4	6.4	92.9
cb	6.6	92.7



99.32 ✓

E	6.3	93.04
PART 3 + 20		
E	7.0	94.34
cb	7.5	91.8
1/4	7.3	92.0
2	7.3	92.02
1/4	7.9	91.4
cb	8.1	91.2
+8	8.9	90.4
+9	11.4	87.9
W	11.4	87.94
+1	11.4	87.9
+6	8.0	91.3

PART 4 = S.L. TENNYSON St.

-5	9.0	90.3
-4	12.1	87.2
W	12.1	87.44
+12	11.3	88.0
cb.	9.4	89.9
1/4	8.7	90.6
2.	8.4	90.92
1/4	8.7	90.6
cb.	8.6	90.7
E	7.4	91.94

TP	1.68	91.67 ✓	9.33	89.99 ✓
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South Ch

on stump

91.67 ✓

86

E	0.5	91.17
cb	1.4	90.3
+6	1.6	90.1
1/4	1.2	90.5
2	1.3	90.37
1/4	1.8	89.9
+8	2.5	89.2
+9	5.0	86.7
cb	5.0	86.7
+9	5.0	86.7
+10	4.4	87.3
W	3.5	88.17
+5	2.2	89.5
South 1/4		
-5	3.0	88.7
W	4.2	87.47
+7	5.0	86.7
+8	5.5	86.2
cb	5.5	86.2
+1	5.5	86.2
+2	2.9	88.8
1/4	2.3	88.4
2	1.9	89.77
1/4	1.8	89.9
cb.	1.9	89.8
E	0.9	90.77



## L Tennyson St. Angles to Catalina

E	1.9	89.77
cb	2.4	89.3
1/4	2.7	89.0
L	2.6	89.1
1/4	2.9	88.77
+9	3.2	88.5
+10	6.0	85.7
cb	6.0	85.7
+7	6.0	85.7
+8	3.8	87.9
N	3.2	88.47
	N 1/2	
N	3.5	88.17
+5	5.9	85.8
cb	5.9	85.8
+2	5.9	85.8
+3	3.5	88.2
1/4	3.1	88.6
L	2.8	88.67
1/4	3.0	88.7
cb	2.7	89.0
E	2.3	89.37
	N cb	
E	2.7	88.97
cb	3.5	88.2

1/4	3.5	88.2
L	3.4	88.27
1/4	3.8	87.9
+7	4.1	87.6
+8	6.3	85.4
cb	6.3	85.4
+8	6.3	85.4
+9	5.5	86.2
+12	5.5	86.2
N	4.0	87.67

## N.G. TENNYSON

-5	4.4	87.3
N	5.1	85.87
+8	5.4	86.3
+9	6.6	85.1
cb	6.6	85.1
+3	6.6	85.1
+4	4.4	87.3
1/4	4.2	86.5
L	3.8	87.27
1/4	4.2	87.5
cb	3.7	88.0
E	3.1	88.57

## PART 1

-3	1.0	90.7
E	4.1	87.57



9167 ✓

+3	5.7	86.0
cb.	5.7	86.0
1/4	5.7	86.0
2	5.9	85.77
1/4	6.4	85.3
cb.	6.8	84.9
+11	7.7	84.0
W	8.1	83.57
+5	6.7	85.0

PART 2

W	8.2	83.47
+12	10.3	81.4
+13	12.0	79.7
cb.	12.0	79.7
+2	12.0	79.7
+4	8.8	82.9
1/4	8.8	82.4
2	7.9	83.77
1/4	8.1	83.6
cb.	7.9	83.8
+10	7.5	84.2
E	5.5	86.17
+3	2.7	89.0

PART 3 = E.C. = 0+00

-3	3.9	87.8
E	6.6	85.07

9167 ✓

28

+3	7.6	84.1
+10	8.1	83.6
+11	9.8	81.9
cb.	9.8	81.9
1/4	9.9	81.8
2	9.6	82.07
1/4	10.2	81.5
+2	12.9	78.8
cb.	12.9	78.8
+2	10.9	80.8
W	9.6	84.07

16' N EC

W	9.8	81.87
cb.	10.3	81.4
+3	10.6	81.1
+4	13.2	78.5
1/4	10.2	78.5
+2	12.7	79.0
+3	10.7	81.0
2	10.2	81.47
1/4	10.3	81.4
cb.	11.1	80.6
+2	11.1	80.6
+3	3.5	86.2
E	4.1	87.57

50' N



E	6.0	85.67
cb.	7.0	84.7
+2	7.0	84.7
+3	11.6	80.1
14	11.9	79.8
2	11.9	79.77
+4	12.2	79.5
4	15.9	75.8
+3	15.9	75.8
+4	11.5	80.2
cb.	11.5	80.2
W	11.2	80.47
	100' N	
W	11.7	79.97
cb.	12.9	78.8
+5	13.3	78.4
+6	18.1	73.6
+8	18.1	73.6
+9	16.0	75.7
4	16.0	75.7
+2	14.3	77.4
2	14.0	77.67
14	14.3	77.4
+5	14.0	77.7
+6	9.9	81.8
cb.	9.9	81.8

E	83	83.37
	125' N	
E	10.3	81.4
cb.	11.5	80.2
+2	11.7	80.0
+3	15.6	76.1
1/2	15.5	76.2
2	15.2	76.47
+3	15.2	76.5
4	17.2	74.5
+2	21.2	70.5
+4	21.2	70.5
+5	17.1	74.6
cb.	14.5	77.2
W	13.3	78.37
	142.37 North of E.C. = South line Udal st.	
W-5	19.8	71.9
W	18.7	74.97
+5	17.2	74.5
cb.	15.8	75.9
+6	18.2	73.5
+11	21.7	70.0
14	21.7	70.0
+3	18.3	73.4
+5	16.6	75.1
2	15.9	75.77



1/4		16.8	74.9
+2		16.8	74.9
+8		12.5	79.2
cb.		12.5	79.2
E		11.1	80.57
T.P.	0.08	79.01	12.74
		78.93	
	Sub. +5		
E		+ 1.0	80.01
cb.		2.0	77.0
1/4		4.2	74.8
2		3.6	75.41
+6		4.0	75.0
+8		6.5	72.5
1/4		8.2	70.8
+4		8.2	70.8
+6		5.0	74.0
cb.		4.0	75.0
+6		4.4	74.6
+7		8.5	70.5
N		8.2	70.81
+10.		8.0	71.0
	South cb.		
-10		8.0	71.0
N		8.4	70.61
+10		8.2	70.8
+12		4.6	74.4

cb.		4.6	74.4
+5		6.2	72.8
+6		7.6	71.4
1/4		8.1	70.9
+1		6.4	72.6
+5		4.2	74.8
2		3.9	75.11
1/4		4.5	74.5
cb.		2.7	76.3
E		0.5	78.51
	South 1/4 ~		
E		1.5	77.51
cb.		4.1	74.9
1/4		4.8	74.2
2		4.5	74.5
1/4		4.9	74.1
+2		8.5	70.5
cb.		8.5	70.5
N		8.8	70.41
+2		8.2	70.8
+5		5.7	73.3
	E Udal st.		
-5		6.2	72.8
-2		6.2	72.8
N		9.2	69.81
+11		9.2	69.8



79.01 ✓

+12	72	71.8
cb	72	71.8
1/4	57	73.3
2	50	74.01
1/4	54	73.6
cb	3.8	75.2
E	1.8	77.41
	N 1/4	
E	2.7	76.31
cb	3.2	75.8
1/4	6.0	73.0
2	5.6	73.41
1/4	6.2	72.8
cb	8.5	70.5
W	8.5	70.51
+2	7.1	71.9
	N cb.	
W	8.1	70.91
+1	9.8	69.2
cb	9.7	69.3
+6	7.4	71.6
W	6.4	72.6
2	6.1	73.71
1/4	6.1	72.9
cb	5.0	74.0
E	2.9	76.11

79.01 ✓

31

N.W. Udalst.

E	40	75.01
cb	6.1	72.9
2	6.9	72.1
2	6.7	72.31
4	6.9	72.1
+8	7.3	71.7
+9	10.1	68.9
cb	10.1	68.9
W	9.2	69.81
	40' N	
W	9.6	69.41
cb	11.3	67.7
2	11.3	67.7
+1	11.3	67.7
+3	8.9	70.1
2	8.7	70.31
1/4	9.3	69.7
cb	9.4	69.6
E	8.3	70.71
	60' N	
E	10.5	68.51
cb	10.3	68.7
1/4	10.1	68.9
2	9.6	69.41
1/4	9.9	69.1



7901

+2		9.9	69.1
+3		11.8	67.2
cb.		11.8	67.2
N		11.5	67.51
	100' N		
N		12.7	66.31
cb.		12.7	66.3
1/4		12.7	66.3
+3		12.7	66.3
+4		11.2	67.8
1/4		11.2	67.81
1/4		11.2	67.8
cb.		11.6	67.4
E		11.7	67.31
T.P.	258	68.58 ✓	13.01 66.00 -
		150' N	
E		2.5	66.08
cb.		2.5	66.1
1/4		2.4	66.2
1/4		2.3	66.28
1/4		2.2	66.4
+2		2.2	66.4
+3		3.7	64.9
cb.		3.5	65.1
N		3.9	64.68
	200' N		

6858 ✓

32

N		5.4	63.18
cb.		5.5	63.1
+2		5.5	63.1
+3		3.6	65.0
N		3.9	64.7
1/4		3.9	64.68
1/4		4.0	64.6
cb.		3.8	64.8
E		3.8	64.78
	240' N		
E		4.7	63.88
cb.		4.8	63.8
1/4		5.1	63.5
1/4		5.3	63.28
1/4		5.1	63.5
cb.		5.0	63.6
+2		7.4	61.2
N		6.9	61.68
	280' N = S.W. Voltaire st. on East		
N		8.0	60.58
+10		8.8	59.5
+12 = 4' Culvert		10.45 = flow line 30" culvert	58.13
cb.		10.5	58.1
+5		10.5	58.1
+6		5.8	62.8
1/4		6.0	62.6



d	6.1	62.48
1/4	6.2	62.4
cb.	6.0	62.6
E	5.5	63.08

## Section AB

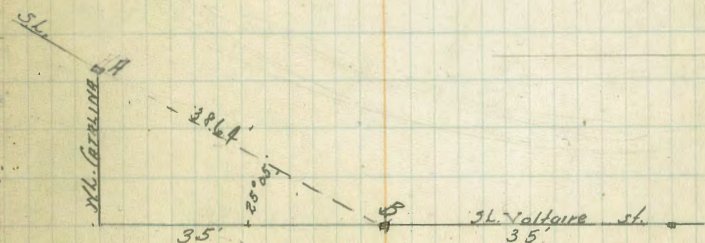
B	6.2	67.38
1/4	6.4	62.2
cb.	6.3	62.3
H.	6.4	67.18

## Section on south edge of paving = St. Voltaire St.

W	7.95	61.73
cb.	7.92	61.16
1/4	7.92	61.26
d	7.26	61.32
1/4	7.12	61.46
cb.	6.96	61.62
E	6.85	61.73
T.P.	12.95	79.32

2.81 66.37  
 0.23 79.09  
 79.00 = 84.11 X Mon.  
 0.09 = 11.00 X Voltaire St.

Catalina Blvd.



CATALINA



X. Section Bernice Dr. 60' wide  
 From N.W. Wells St. to E.L. CATHARINA Blvd.

168.68 ✓

34  
 1-27

B.M. 5. N.W. C.P.  
 CATHARINA + N. WELLS 11.17 161.17

T.P.	8.81	168.68	1.30	159.87
		N.W. Wells St.		
S			0.6	168.08
cb.			0.9	167.78
1/4			1.0	167.68
2			0.9	167.78
1/4			1.2	167.48
cb.			0.8	167.88
N			+ 0.2	168.78

25' West

N			2.2	66.48
cb.			3.3	65.38
1/4			3.5	65.18
2			3.2	65.48
1/4			3.5	65.18
cb.			4.3	64.38
S			2.9	65.78

50' West

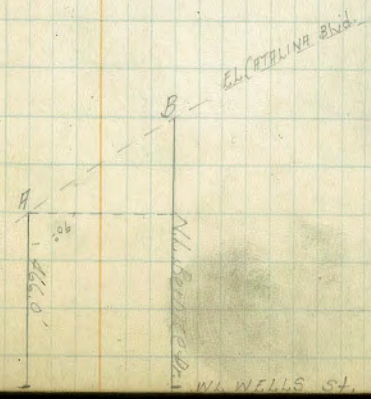
S			6.9	61.78
cb.			7.6	61.08
1/4			7.1	61.58
2			6.7	61.98
1/4			6.7	61.98
cb.			7.2	61.48
N			5.9	64.78

Plotted  
 1-26-27  
 J.L.M.

		100' West		
N			13.0	155.68
cb.			14.0	54.68
1/4			13.8	54.88
2			13.7	54.98
1/4			14.1	54.58
cb.			14.7	53.98
S			14.0	54.68
T.P.	0.04	156.03 ✓	12.69	155.99 ✓

12.5' West

S			4.6	51.43
cb.			5.0	51.03
1/4			4.3	51.73
2			4.2	51.83
1/4			4.3	51.73
cb.			4.6	51.43
N			3.8	54.43





156.03

175' West

N	8.0	147.83
cb	9.5	46.53
1/2	9.3	46.73
1/4	9.2	46.83
1/8	9.8	46.43
cb	10.4	45.63
+2	11.6	44.43
+5	9.5	46.53
5	9.8	46.73

200' N

5	11.9	44.13
+6	11.8	44.23
+7	13.3	42.73
cb	12.9	43.13
1/4	12.0	44.03
1/2	11.5	44.53
1/4	11.5	44.53
cb	11.7	44.33
N	10.7	45.33

T.P. 0.37 143.68 12.74 144.31 ✓

250' West

N	2.7	140.98
+6	3.1	40.58
cb	4.2	39.48
1/4	3.7	39.98

143.68

135

1/2	5.4	140.48
1/4	4.1	39.58
cb	4.5	39.18
+2	5.3	38.38
+5	3.9	39.78
5	3.8	39.88

300' West

5	8.3	35.38
+5	8.5	35.18
+8	10.0	33.68
cb	9.4	34.48
1/4	8.7	34.98
1/2	8.3	35.38
1/4	8.5	35.18
cb	8.8	34.88
+4	8.2	35.48
N	7.8	35.88

350' West

N	12.9	30.78
+7	15.0	30.68
cb	13.5	30.18
1/2	13.3	30.38
1/4	13.1	30.58
1/4	13.5	30.18
+7	13.5	30.18
+8	14.5	149.18



143.68

cb		14.8	178.88
+L		14.8	178.88
+5		13.7	49.98
S		13.3	30.38
T.P.	0.00	<del>131.69</del>	<del>130.69</del>

400' West

S		4.7	75.99
cb		5.3	75.39
1/4		5.3	75.39
1/2		5.2	75.49
1/4		5.4	75.79
cb		5.3	75.39
N		4.7	75.99

450' West

N		7.8	77.89
cb		7.6	73.09
1/4		8.0	77.69
1/2		8.1	77.59
1/4		8.3	77.39
cb		8.4	77.49
S		8.5	77.19

466' West

S		9.0	71.69
cb		9.1	71.59
1/4		8.9	71.79
1/2		9.5	77.19

130.69

36

1/4		8.5	127.19
cb		8.4	77.79
N		8.5	77.19

Section B.A. See sketch

N		9.5	71.19
cb		9.4	71.79
1/4		9.4	71.79
1/2		9.3	71.39
1/4		9.2	71.49
cb		9.0	71.69
S		9.0	71.69

T.P. on L.I. Map PAGE 18.

11.55

119.14 ✓



Cross Section of Warren  
 Moore at Industrial Ave. West of Linnet Drive

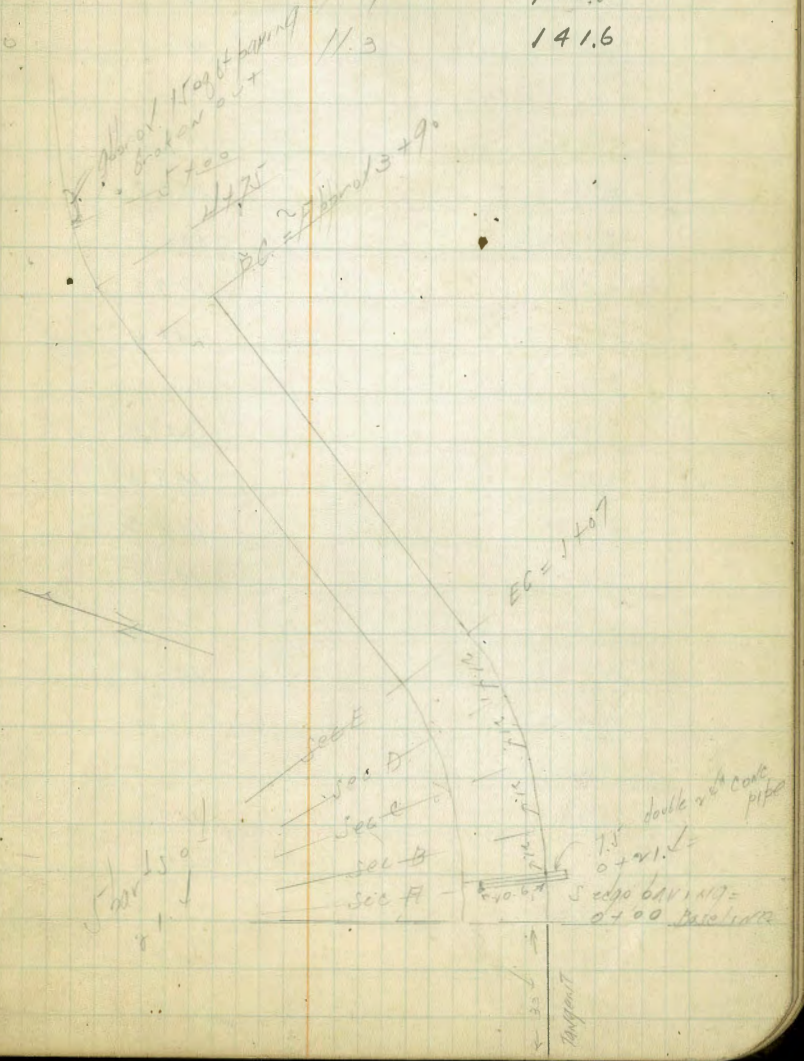
157.80

37

Plotted 2/27/44

Station	113	180.87	179.70	HAINS Edges
TP	115	170.12	1190	168.97
TP	010	160.00	1027	159.85
TP	311	153.88	102	149.77
00-30				
S edge paving	= baseline	4.2		148.7
H&A	"	5.2		147.7
S +30		7.0		145.9
S +35		13.2		139.7
PB = 00				
S edge		3.9		149.0
+20.5 Nedge		5.3		147.6
+23		5.3		147.6
+25		12.3		140.6
+40		12.4		140.5
Sec F				
S edge paving		3.8		149.1
+20 Nedge paving		5.2		147.7
+21		12.5		140.4
+40		12.0		140.9
Sec D				
S edge paving		3.8		149.1
+15 Nedge paving		4.5		148.9
+16		12.1		140.8
+40		12.0		140.9

Sec C		
S edge paving	3.6	149.3
+11 Nedge "	4.1	148.8
+12	9.1	143.8
+22	12.1	140.8
+40	11.3	141.6





2+50 - break in paving full width

S edge paving	3.6	149.3
+10 No "	4.0	148.9
+11	10.0	142.9
+22	12.0	140.9
+40	11.0	141.9

Sec D

S	3.8	149.1
+5	4.1	148.8
+16	13.0	139.9
+30	13.0	139.9
+40	11.3	148.6

Sec E = EC = 540 1407

S	3.5	149.4
+2	4.1	148.0
+5	8.7	144.2
+15	12.4	140.5
+30	12.8	140.1
+40	10.9	142.0

1+75

S	3.6	149.3
+12	11.7	141.2
+40	10.8	142.1

1+50

S	3.9	149.0
+2	4.3	148.6

+13	11.7	141.2
+40	10.7	142.2
1+75		
S	4.0	148.9
+13	10.3	142.6
+40	10.2	142.7

2+00

S	4.0	148.9
+5	4.3	148.6
+14	10.7	142.2
+40	10.3	142.6

2+15

S edge of paving	4.0	148.9
+7 No " "	4.0	148.9
+8	8.0	144.9
+15	10.3	142.6
+40	9.2	143.7

2+30

S edge paving	3.8	149.1
+9 No edge "	3.8	149.1
+10	8.6	144.3
+40	8.9	144.0

2+60 paving full width

S edge paving	3.6	149.3
+8 " "	3.6	149.3
+9	8.7	144.2
+40	8.4	144.5



15.2.88

2+25

N edge paving	3.5	1494.
+4	3.9	1490
+9	8.0	1489
+8	8.6	1483
+24	8.4	1485

3+00 = edge of 1st washout

N edge paving	3.3	1496
+10	4.8	1481
+11	8.4	1447
+22	8.5	1444

T.P. 975 159.6.7 ✓ 296 149.9.7 ✓

4+25 = beginning of 2nd washout

N edge paving - baseline	5.2	154.5
+5	5.2	154.5
+7	14.6	145.1
+12	15.6	144.1
+30	13.2	146.5

5+00

N edge paving	4.1	155.6
+1	9.3	150.9
+6	13.8	145.9
+30	12.8	146.9

5+25

N edge paving	3.0	
---------------	-----	--

15.9.67

39

N edge	11.0	1487
+10	13.6	146.1
+30	13.2	1465

5+37

N edge paving	2.5	1577.2
+4	9.8	1499
+11	13.5	1462
+30	13.4	1463

5+60

N edge paving	1.6	1581
+1	1.5	158.2
+15	11.2	1485
+30	13.2	1465

5+75

N edge paving	1.0	158.7
+11	1.5	158.2
+18	10.4	1493
+23	11.3	1484
+30	12.9	146.8



70' st  
9' Cbs  
18' at  
Xsection of Catalina from Orchard Ave to Point Loma Ave

Ele Aug 31st 1927  
Dannan  
Flood  
Richard  
Kierman

+ π - Ele  
206.74

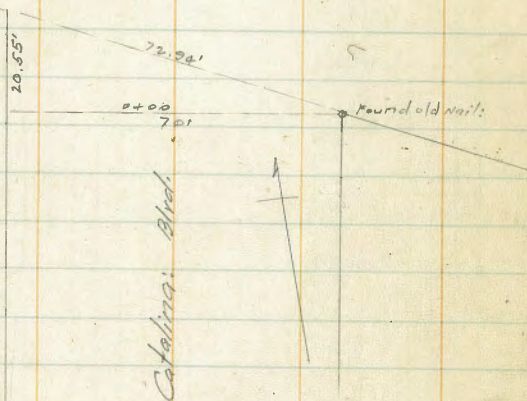
40

0+00 See sketch

#	9.23	173.14		162.91	B.P.M.W. Cor Santa Cruz and Catalina:	E.U.
#	11.71	184.57	0.28	172.86	On curb:	+2
#	12.36	196.35	0.58	183.99	" "	cb
o				187.31	Top Hyd. S.E. Cor Del Mar and Catalina:	+4
#	10.39	206.74		0.00	196.35 Nail	1/2
o			8.82	197.92	Nail Pole S.W. Cor of Orchard and Catalina:	±
			9.53			1/2

end Curb S.W. Orchard and Catalina

Orchard Ave



Diagonal along S.W. Orchard Ave = 72.94 See sketch

W.L.	9.9	196.8
cb	10.0	196.7
1/2	10.1	196.6
±	10.1	196.6
1/2	10.2	196.5
cb	10.5	196.2
EL.	10.8	196.5

	19.4	196.5
	7.0	199.7
	6.7	200.0
	6.0	200.7
	10.0	196.7
	9.7	197.0
	9.6	197.1
	9.1	197.5
	9.4	197.3

0+50

	5.9	200.8
	6.2	200.5
	6.2	200.5
	6.3	200.4
	6.9	199.8
	5.3	201.4
	5.8	200.9
	6.2	200.5

0+70

	6.0	200.7
	5.6	201.1
	5.2	201.5
	5.0	201.7
	5.1	201.6
	9.9	201.8
	4.0	202.7



	+	π 206.74	-	E/e
cb			3.6	203.1
W.L.			4.1	202.6
	1400			
W.L.			3.0	203.7
cb			3.4	203.3
+10			3.4	203.3
1/2			2.8	201.9
±			4.8	201.9
1/4			5.2	201.5
cb			5.6	201.1
E.U.			5.9	200.8
	1+50			
E.L.			6.5	200.2
cb			6.1	200.6
1/2			5.6	201.1
±			5.4	201.3
1/4			5.6	201.1
+1			4.2	202.5
cb			4.2	202.5
W.L.			3.8	202.9
	2400			
W.L.			5.1	201.6
cb			6.2	200.2
+6			6.9	199.8
1/2			6.2	200.5
±			6.2	200.5

	+	π 206.74	-	E/e
+8			6.6	200.1
1/4			7.4	199.3
cb			8.1	198.6
E.L.			7.9	198.8
+10			8.8	197.9
At 2+07 Wood Box Culvert 8'x8"				F.L. 7.75 intake } F.L. 8.25 outlet }
26' long: from 1/4 to 1/4				
		2+50		
E.L.-10			6.9	199.8
E.U.			7.2	199.2
cb			7.0	199.7
1/2			6.9	199.8
±			6.1	200.6
+9			5.7	201.0
1/4			6.7	200.0
+2			5.4	201.3
cb			5.4	201.3
W.L.			5.0	201.7
		3+00		
W.L.			3.7	203.0
cb			4.2	202.5
+9			4.4	202.3
+11			5.9	200.8
1/4			5.3	201.4
±			5.4	201.3
1/2			6.5	200.2



	+	π 206.74	-	E/6
cb			7.0	199.2
E.L.			8.0	198.7
E.L.+10			9.0	197.7
3+12 <sup>60</sup> = N.L. Pescadero Ave 83.37 diagonal 20.82 cbs 10.41 dts; 80'st 20' cbs 10' dts				
E.L.-10			8.9	197.8 198.78
E.L.			7.96	on old Blk Cor Hub. N.E Catalina and Pescadero 199.2
cb.			7.0	199.2
+10			6.8	199.9
1/2			5.8	200.9
±			5.2	201.5
+9			5.1	201.6
1/2			5.9	200.8
+1			4.1	202.6
cb			4.0	202.7
W.L.			3.0	203.2
N. Curb of Pescadero:				
W.L.			3.4	203.3
cb			3.9	202.8
+10			3.8	202.9
+11			5.0	201.2
1/2			5.7	201.0
+3			5.0	201.7
±			5.2	201.5
1/2			5.8	200.9
cb			7.3	199.4
E.L.			7.9	198.8
E.L.+10			8.9	197.8

	+	π 206.74	-	E/6
N 1/4 Pescadero:				
E.L.-10			9.2	197.5
E.L.			8.0	198.7
cb.			7.4	199.3
±			7.2	199.5
1/2			5.8	200.9
±			5.2	201.5
+10			5.0	201.7
1/2			5.6	201.1
+2			4.1	202.6
cb			3.8	202.9
W.L.			3.3	203.4
± Pescadero				
W.L.			3.1	203.6
cb			3.9	202.8
+10			3.8	202.9
1/2			5.6	201.1
+3			4.9	201.8
±			5.1	201.6
1/2			5.8	200.9
cb			7.4	199.3
E.L.			7.9	198.8
E.L.+10			8.9	197.5
S 1/4 Pescadero				
E.L.-10			9.3	197.4
E.L.			8.2	198.5



+	$\pi$ 206.74	-	E/e
cb		7.5	199.2
1/2		5.9	200.8
+6		5.2	201.5
<del>5</del>		5.0	201.7
+11		4.8	201.9
1/2		5.6	201.1
+2		4.1	202.6
cb		4.1	202.6
W.L.		3.4	203.3

Scarb Pascadero:

W.L.		3.3	203.4
cb		3.9	202.8
+10		4.7	202.0
1/2		5.5	201.2
+3		4.8	201.9
<del>5</del>		4.9	201.8
+10		5.1	201.6
1/2		6.0	200.7
cb		7.5	199.2
E.L.		8.4	198.3
E.L.+10		9.5	197.2

# 732 207.47 8.59 198.15 S.E. Cor. Hub. Catalina and Pascadero,

at 100 S.L. Pascadero AIC:

E.L.-10		10.8	196.7
E.L.		9.3	198.2
cb		7.6	199.9

+	$\pi$ 207.47	-	E/e
1/2		6.8	200.7
+6		5.9	201.6
<del>5</del>		5.8	201.7
+10		5.4	202.1
1/2		6.1	201.4
+2		5.1	202.4
cb		4.8	202.7
W.L.		4.4	203.1

0+50

W.L.		3.5	204.0
cb		4.1	203.4
+7		4.6	202.9
1/2		5.7	201.8
+3		4.9	202.6
<del>5</del>		5.5	202.0
1/2		6.1	201.1
cb		6.8	200.7
EL		6.9	200.6
+10		8.2	199.3

1+00

E.L.-10		7.0	200.5
E.L.		6.6	200.9
cb		6.4	201.1
1/2		5.7	201.8
<del>5</del>		5.1	202.4
+10		4.4	203.1



+       $\pi$       -      Elev  
 207.47

1/4      5.3      202.2  
 +3      4.2      203.3  
 cb.      5.7      203.8  
 W.L.      2.9      204.6

1+50

W.L.      2.7      204.8  
 cb.      2.8      204.7  
 +11      3.3      204.2  
 1/4      4.9      202.6  
 +3      4.0      203.5  
 E.      4.5      203.0  
 1/4      4.9      202.6  
 cb.      5.6      204.9  
 E.L.      6.0      201.5  
 +10      6.8      200.7

0+00 = 1+70.28 = End of Curve N.E. Return  
 Chatsworth and Catalina Blvds.

E.L. -10      6.6      200.9  
 E.L.      6.0      201.5  
 cb.      5.3      202.2  
 1/4      4.9      202.6  
 E.      4.3      203.2  
 +7      3.8      203.7  
 +11      4.9      202.6  
 1/4      4.2      203.3

+       $\pi$       -      Elev  
 207.47

+2      2.9      204.6  
 cb.      2.6      204.9  
 W.L.      2.0      205.5

0+50

W.L.      1.4      206.1  
 cb.      1.9      205.6  
 +11      2.4      205.1  
 1/4      4.3      203.2  
 +9      3.5      204.0  
 E.      3.9      203.6  
 1/4      4.7      202.8  
 cb.      5.5      202.0  
 E.L.      6.3      201.2  
 E.L. +10      7.1      200.4

1+00

E.L.      5.8      201.7  
 cb.      5.3      202.2  
 1/4      4.6      202.9  
 E.      3.6      203.9  
 +10      3.1      204.4  
 1/4      3.7      203.8  
 +2      2.2      205.3  
 cb.      1.6      205.9  
 W.L.      0.6      206.9  
 # 1.112      211.53      5.06      202.41 Nail header board.

1+2+0 = Northwesterly line pavement



+

π  
211.53

-

E/e

W.V		4.9	206.6
cb		5.7	205.8
+11		6.0	205.5
1/2		7.2	204.3
+5		6.9	204.6
±		7.4	204.1
1/4		8.4	203.1
cb		8.9	202.6
E.L. Edge Pavement		9.19	202.34
E.L. 1+61° = ± Pavement		8.84	202.69
1+88° = Southernly edge pavement			
E.L. on Pavement		8.05	202.98
cb	" "	8.14	203.39
+12	" "	7.71	203.82
1/2		7.6	203.9
±		6.8	204.7
+9		6.2	205.3
1/4		6.6	204.9
+1		5.5	206.0
cb		4.7	206.8
W.V		3.9	207.6
	2450		
W.V		2.8	208.7
cb		3.8	207.7
1/2		5.9	205.6
+3		5.5	206.0

0.298  
0.234  
.64

+

π  
211.53

-

E/e

45

+11 = Edge Pavement		6.26	205.27
±	" "	6.34	205.19
1/4	" "	6.97	204.56
1/2	" "	7.27	204.26
cb Ground		8.1	203.4
E.L.		7.3	204.2
	3400		
E.L.		5.9	205.6
cb		6.3	205.2
1/4		6.2	205.3
+2 Edge Pavement		6.06	205.47
±	" "	5.59	205.94
+9	" "	5.24	206.31
1/2		5.1	206.4
cb		3.8	207.7
W.V		2.4	209.1
	3450		
W.V		1.7	210.3
+6		1.8	209.7
cb		2.8	208.7
1/4		3.6	207.9
+3 edge pavement		3.65	207.88
±	" "	3.74	207.79
+10	" "	4.07	207.46
1/2		4.4	207.3
+3		4.7	206.8



	T	Σ	-	
		211.53		
+6			4.0	207.5
cb			4.3	207.2
E.C.			4.0	207.5
#	12.00	221.92	1.61	20992 Nail header
		4400		
E.C.			11.9	210.0
cb			11.7	210.2
+9			11.5	210.4
+10			12.6	209.3
1/2			11.8	210.1
+3 Edge pavement			11.59	210.33
±	"		11.39	210.53
+10 " "			11.42	210.50
1/2			11.05	210.4
cb			10.6	211.3
+5			6.3	215.6
W.C.			5.4	216.5
		4450		
W.C.			1.0	220.9
+6			1.7	220.2
cb			6.5	215.4
+9			7.2	214.7
+10			8.4	213.5
1/2			8.3	213.6
+3 Edge Pavement			8.20	213.7
±	"		8.10	213.8
+10 " "			8.25	213.67

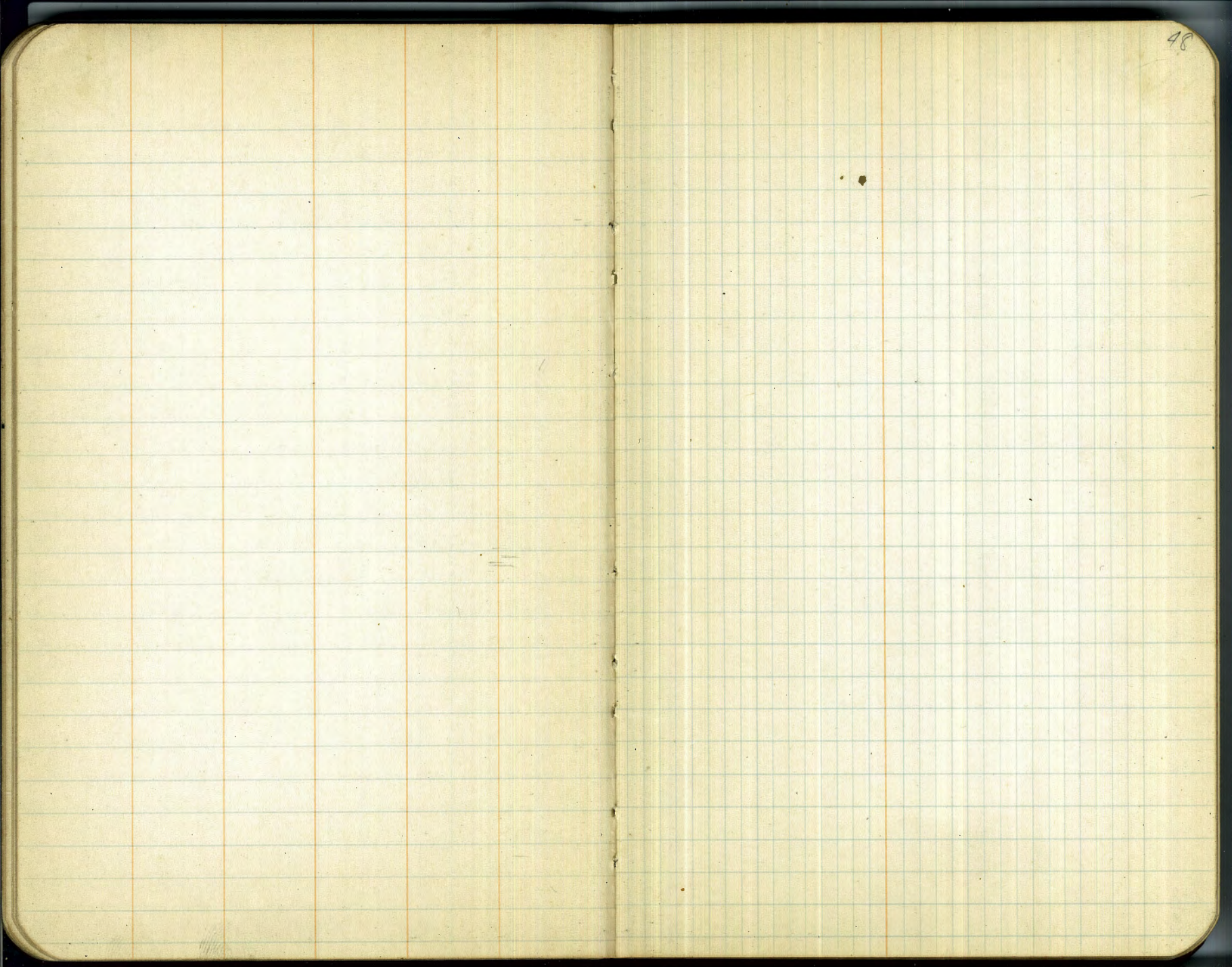
	T	Σ	-	E10	46
		221.92			
1/2			8.7	213.2	
+			9.2	212.7	
+5			8.5	213.6	
cb			8.2	213.7	
E.C.			8.4	213.5	
499362 = Intersection of the Northwesterly production of the Northeastly line of Point Loma Ave with the Westerly line of Catalina Blvd. = end of work 2857L.					
E.C.			4.9	217.0	
cb			4.6	217.3	
+8			4.5	217.4	
+10			5.7	216.2	
1/2			5.2	216.7	
+3 Edge pavement			4.86	217.0	
±	"		4.63	217.3	
+10 " "			4.68	217.2	
1/2			4.8	217.1	
+2			4.9	217.1	
+3			3.8	218.1	
+11			3.3	218.6	
cb			2.4	219.5	
+4			+1.1	223.0	
W.C.			+1.4	223.3	
{ 49936 see description - see above; { 521991 = N.E. Cor Point Loma and Catalina Blvd } Diagonal = End work.					
W.C.			+2.4	224.3	



+  
π  
221.92

			-		
+6			+1.0	222.9	
c6			2.6	219.3	
+6			3.3	218.6	
+7			4.2	217.5	
1/2			4.4	217.5	
+3	Edge pavement		4.27	217.6	
E	"	"	4.02	217.9	
+10	"	"	4.08	217.8	
1/2			4.2	217.7	
+3			4.6	217.3	
+7			3.9	218.5	
c6			3.15	218.4	
E.V.			3.7	218.7	
#	12.74	224.66	0.00	221.92	naill
#	11.51	225.06	1.11	223.50	Flan.
#	7.59	252.61	2.04	245.02	Naill
			2.83	250.18 = 250.17 B.P	
				W. Catalina and Varona.	







70.5' section Catalina Blvd at Voltaire St:  
 14' C&G  
 10 1/2' G&S:

30p 1st 27

Dennan  
 Flood-  
 Bichel:

66.18

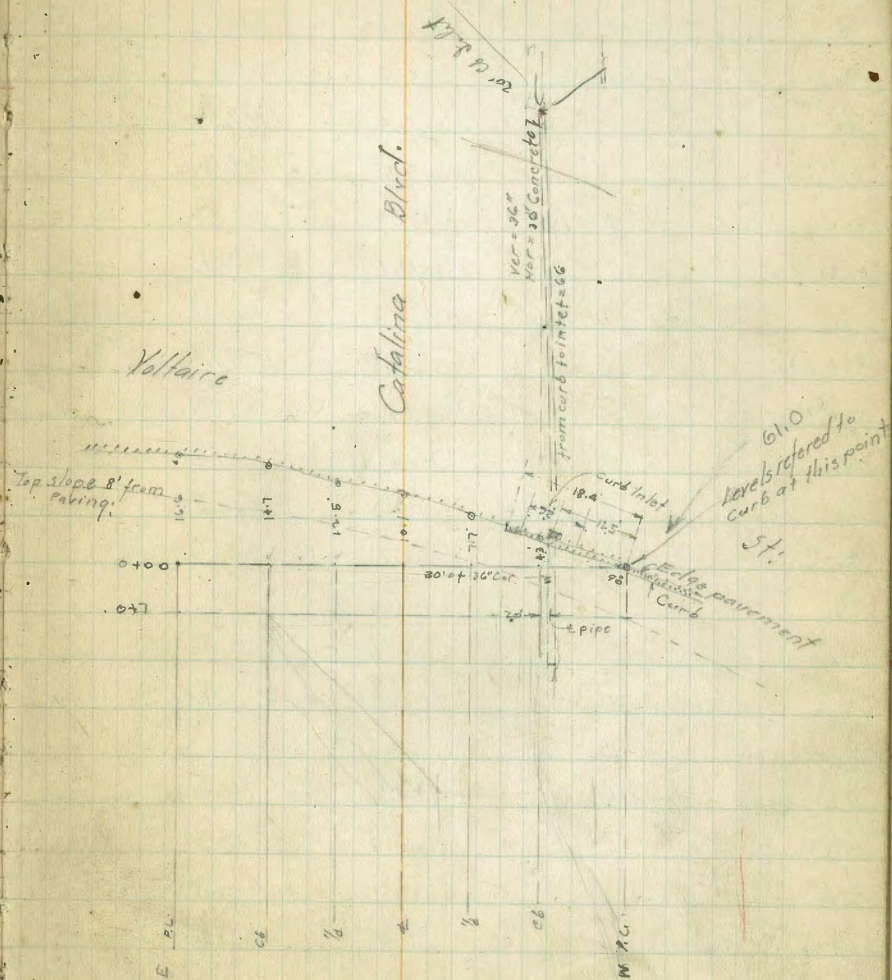
0+00 on curb	5.18	61.00	Corb. Sec sketch.
0+00 Cutter	6.16	60.62	
End of existing curb	5.10	61.08	
Top of grating Culvert	6.22	59.96	
Flow line at curb inlet	11.47	54.74	
Outlet Cor Pipe	13.06	53.12	
Intake Concrete Pipe	8.70	57.48	
N. Edge Paving & Catalina	5.80	60.38	
" " " E.L. " "	5.32	60.86	

Ground elevations on sidewalk adjacent to paving.

N.L.	5.3	60.9
cb	5.3	60.9
1/4	5.9	61.3
1/2	5.0	61.2
3/4	5.0	61.2
cb	5.0	61.2
E.L.	4.8	61.4

Ground elevations 8' from paving: Top slope sec sketch

E.L.	5.0	61.2
cb	5.0	61.2
1/4	5.1	61.1
1/2	4.9	61.3
3/4	4.7	61.5
cb	5.4	60.8
N.L.	5.4	61.5





	$\pi$	-	E16
0+00 = Right angles to Catalina			
W.L. on sidewalk	5.3		60.9
cb	6.5		60.7
1/4	9.2		61.5
E " in edge:	4.9		61.3
1/4	5.4		60.7
cb	9.0		56.6
E.L.	9.8		56.4
E.L. + 15'	11.1		55.1
0+7			
E.L. - 15'	11.8		54.4
E.L.	12.0		54.2
cb	12.7		54.0
1/4	9.6		56.6
E	8.1		58.1
1/4	7.0		59.2
cb	8.0		58.2
W.L. on sidewalk	5.3		60.9
0+17			
W.L. - 15' on sidewalk	4.7		61.5
W.L.	10.9		55.3
cb	22.1		44.1
1/2	16.8		49.4
+3	16.8		49.4
+4	12.0		54.2
E	12.1		54.1

	$\pi$	-	E16
1/4		12.7	53.5
cb		12.7	53.5
E.L.		12.9	53.3
E.L. + 15'		12.6	53.6
0+20			
E.L. - 15'		13.0	53.2
E.L.		13.3	52.9
cb		12.6	53.6
1/2		12.7	53.5
E		12.3	53.9
+7		12.5	53.7
+8		12.1	48.1
1/4		18.1	48.1
cb		24.0	42.2
+7		21.9	44.3
W.L.		17.0	49.2
W.L. + 7		17.0	49.2
W.L. + 15' on old slope		7.7	57.5
0+22			
W.L. - 15'		14.4	51.8
W.L. - 8		14.3	51.9
W.L. BoHom Wash		24.7	41.5
cb "		23.0	43.2
+2		23.0	43.2
+3		17.1	49.1
1/4		15.2	51.0



+      π      -      E/e

±		14.2	52.0
1/2		14.3	51.9
cb		14.6	51.6
E.L.		14.3	51.9
E.L + 15		13.8	52.4
	0+50		
E.L. - 15		14.0	52.2
E.L.		14.5	51.7
cb		15.0	51.2
1/2		14.8	51.4
±		14.5	51.7
1/2		14.3	51.9
+2		14.7	51.5
+6		17.2	49.0
cb		20.1	46.1
+7		24.0	42.2
W.L.	Bottom wash	24.9	41.3
+2	" "	24.9	41.3
+6		14.5	51.7
+15		14.8	51.4



Oliver St. Cross Sections

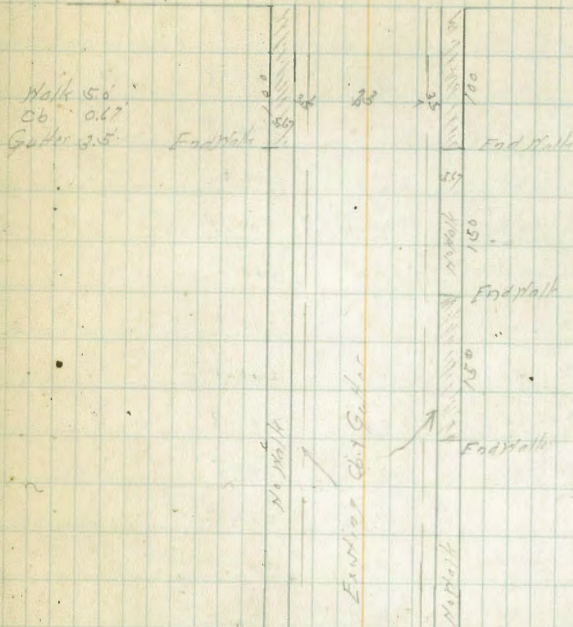
Exchange Place to Washoe Ave. 50 N. do  
Cb 7594

BM	0.00	222.87	222.87
TP	0.65	210.71	1278 210.09
TP	6.93	207.54	1013 200.61
S.E. Exchange Place			
H		81	199.4
Cb Existing		252	200.0
Gutter		804	199.5
+3.5 Edge Gutter		776	199.8
1/4 on Parapet		738	200.2
1/2 " "		693	200.8
3/4 " "		622	201.3
+4 Edge Gutter		594	201.6
Gutter		585	201.6
Cb		556	202.0
F		45	203.0
S.E. of S.E. of Exchange			
F		41	203.4
Cb		542	202.12
Gutter		583	201.71
+3.5 Edge		575	201.8
1/4		59	201.6
1/2		62	201.3
3/4		71	200.7
+4 Edge		745	200.4
Gutter		719	199.9

To Hyd of Exchange  
+ Seledad

Exchange

Place



Washoe Ave. East

50  
120-20  
100-100  
100-100  
100-100  
100-100



207.54

Cb	708	200.4
N	90	200.5
	50.5	
N	68	200.7
Cb	666	200.9
Gutter	737	200.2
+3.5 Edge	710	200.4
1/4	67	200.8
2	61	201.1
1/4	59	201.6
1/4 - Edge	565	201.9
Gutter	525	201.8
Cb	535	202.2
F	44	203.1
	75.5	
F	45	203.0
Cb	581	202.3
Gutter	577	201.8
+3.5 Edge	560	201.9
1/4	55	202.0
2	59	201.1
1/4	64	201.1
1/4 - Edge	672	200.8
Gutter	704	200.5
Cb	634	201.2
N	66	200.9

207.54

	100.5	
N	66	200.9
Cb	607	201.4
Gutter	681	200.7
+3.5 Edge	654	201.0
1/4	63	201.2
2	58	201.7
1/4	55	202.0
1/4 - Edge	558	202.0
Gutter	568	201.8
Cb	503	202.5
F	41	203.7
	125	
F	31	204.4
Cb	488	202.7
Gutter	557	202.8
+3.5 Edge	542	202.1
1/4	53	202.2
2	55	202.0
1/4	59	201.6
1/4 - Edge	628	201.3
Gutter	663	200.9
Cb	586	201.8
N	69	200.6
	150.5	
N	56	202.0



207.51

Cb	5.62	201.9
Gutter	636	201.6
+3.5-Edge	616	201.3
1/4	555	202.0
1/2	571	202.4
1/4	558	202.3
7.4-Edge	535	202.8
Gutter	545	202.1
Cb	468	202.9
F	25	205.0

175'S

F	21	204.9
Cb	442	203.1
Gutter	522	202.3
+3.5-Edge	499	202.6
1/4	50	202.5
1/2	50	202.5
1/4	51	201.9
1.4-Edge	593	201.6
Gutter	615	201.3
Cb	593	202.1
H	59	201.6

200'S

H	69	200.6
Cb	521	202.3
Gutter	600	201.5

207.52

+3.5-Edge	578	201.7
1/4	53	202.2
1/2	48	202.7
1/4	17	202.8
7.4-Edge	486	202.9
Gutter	504	202.5
Cb	461	203.3
F	1.9	205.6

225'S

F	1.9	205.6
Cb	465	203.4
Gutter	478	202.8
+3.5-Edge	465	202.9
1/4	46	202.9
1/2	46	202.9
1/4	53	202.2
7.4-Edge	549	202.1
Gutter	500	201.7
Cb	503	202.5
H	64	201.1

250'S

H	60	201.5
Cb	483	202.7
Gutter	566	201.7
+3.5-Edge	538	202.2
1/4	49	202.5



807.54

1/8	43	203.2
1/4	43	203.2
1/4 - Edge	441	203.1
Gutter	463	202.9
cb	386	203.9
F	3.5	204.0

275.5

F	32	204.3
cb	363	203.9
Gutter	448	203.4
13.5 - Edge	430	203.2
1/4	42	203.3
1/8	43	203.2
1/4	48	202.7
1/4 - Edge	509	202.8
Gutter	536	202.8
cb	467	202.9
H	49	202.6

300.0

H	51	202.4
cb	449	203.0
Gutter	516	202.4
13.5 - Edge	493	202.6
1/4	45	203.0
1/8	41	203.4
1/4	40	203.5

807.54

1/4 - Edge	401	203.5
Gutter	428	203.3
cb	346	204.9
F	34	204.1

325.0

F	15	206.0
cb	374	203.8
Gutter	446	203.6
13.5 - Edge	436	203.4
1/4	42	203.3
1/8	43	203.2
1/4	49	202.6
1/4 - Edge	519	202.4
Gutter	542	202.1
cb	482	202.7
H	50	202.5

350.0

H	54	202.1
cb	509	202.8
Gutter	574	201.8
13.5 - Edge	550	202.0
1/4	50	202.5
1/8	46	202.9
1/4	45	203.0
1/4 - Edge	466	202.9
Gutter	483	202.7



207.54

cb		4.07	203.5
F		1.3	206.2
	275.5		
F		2.1	205.4
cb		4.96	202.6
Gutter		5.93	201.7
+3.5-Edge		5.61	201.7
1/4		5.5	202.0
1/2		5.5	202.0
1/4		6.0	201.5
+4-Edge		6.40	201.1
Gutter		6.68	200.9
cb		5.96	201.8
H		5.8	201.7
	400.5		
H		7.8	199.7
cb		7.00	200.5
Gutter		7.70	199.8
+3.5-Edge		7.42	200.1
1/4		7.2	200.3
1/2		6.7	200.8
1/4		6.6	200.9
+4-Edge		6.62	200.9
Gutter		6.84	200.7
cb		5.99	201.6
I		3.2	204.3

207.54

		4.7	202.8	
cb		7.90	199.6	
Gutter		8.62	198.9	
+3.5-Edge		8.44	199.1	
1/4		8.3	199.2	
1/2		8.4	199.1	
1/4		8.9	198.6	
+4-Edge		9.33	198.2	
Gutter		9.55	199.0	
cb		8.95	198.6	
H		9.3	198.2	
TP	1.75	199.86	9.83	197.71
	450.5			
H		3.8	195.7	
cb		2.86	198.4	
Gutter		3.46	196.0	
+3.5-Edge		3.18	196.3	
1/4		2.8	196.7	
1/2		2.4	197.1	
1/4		3.1	197.4	
+4-Edge		3.21	197.3	
Gutter		2.65	197.0	
cb		1.75	198.7	
F		0.0	199.5	
	475.5			

56



199.46

F	10	198.5
Cb	363	195.8
Gutter	436	195.1
435-Edge	419	195.3
1/4	42	195.3
1/2	41	195.1
1/4	49	194.6
74-Edge	515	194.3
Gutter	536	194.1
Cb	477	194.7
H	55	194.0

500'S

H	71	192.4
Cb	676	192.7
Gutter	737	192.1
435-Edge	706	192.4
1/4	68	192.7
1/2	62	193.3
1/4	60	193.5
74-Edge	612	193.3
Gutter	631	193.1
Cb	559	193.9
F	30	196.5

527'S

F	46	194.9
Cb	760	191.9

57

199.46

Gutter	834	191.1
435	816	191.3
1/4	79	191.6
1/2	82	191.3
1/4	87	191.8
74-Edge	923	190.2
Gutter	948	190.0
Cb - pc. of Return	884	190.6
H	86	190.9
TP	696	
End Cb on F 550'S	838	191.1

192.50  
 192.50  
 527'S on F



Catalina Place  
Top Curb Levels East of Catalina Blvd.

6.18

BM	11.45	143.44	131.99
		FL Catalina Blvd. 77' Bet Curb	
N Top Cb		10.88	132.56
Gutter on Pavng		11.44	132.02
1/4		11.61	31.83
1/2		11.78	31.66
3/4		11.98	31.46
Gutter		12.17	31.27
S Top Cb		11.60	31.84
		20' E of FL = EC on N	61.80' Curb
S Top Cb		10.18	33.26
Gutter on Pavng		10.85	32.59
1/4		10.63	32.81
1/2		10.41	33.03
3/4		10.21	33.16
Gutter		10.13	33.31
N Top Cb		9.58	33.86
		28' E on N	
		35' E on S = EC on N	60' Bet Curb
N Top Cb		9.16	34.28
Gutter on Pavng		9.71	33.73
1/4		9.70	33.74
1/2		9.70	33.74
3/4		9.62	33.75
Gutter		9.80	33.64
S Top Cb		9.13	34.31

ct. line  
E.S.  
Catalina +  
Catalina Place

143.44  
25' E of EC on N

S Top Cb		7.66	35.98
N " "		7.46	36.02
		50' E of EC on N	
N Top Cb		5.67	37.27
S " "		5.69	37.25
		75' E	
S Top Cb		3.97	39.47
N " "		3.97	39.47
		100' E	
N Top Cb		2.29	41.15
S " "		2.29	41.16
		125' E	
S Top Cb		0.58	42.86
N " "		0.58	42.86



Proposed Dirigible Site  
Camp Kearny

STADIA

9/14/08  
Stoops  
OSBORN  
Calagatoun  
Pedice

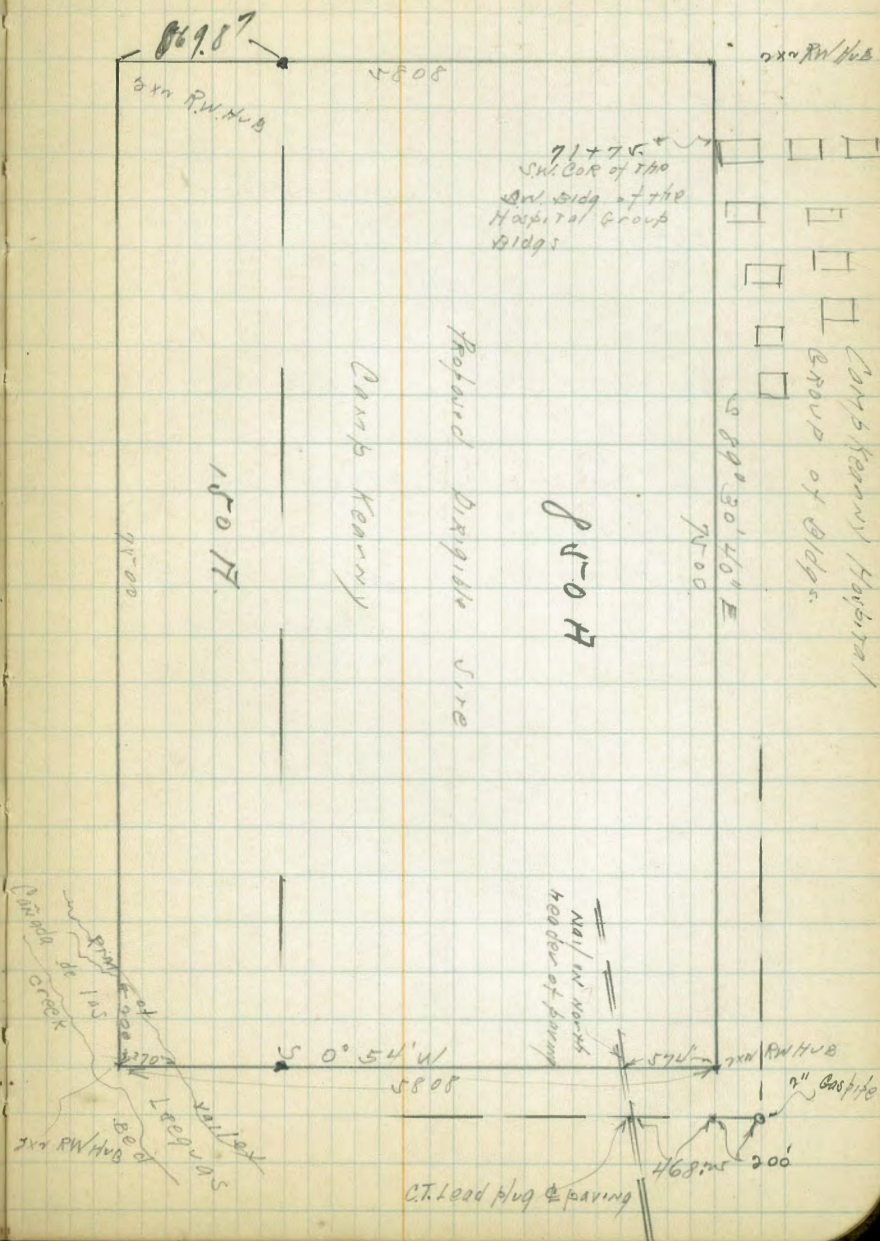
NE COR SITE = 00

WHT 470	POT	Lat	
" 2501	"	"	
" 2888	"	"	
" 3454	"	"	
" 4220	"	"	
" 4920	"	"	
" 5668	"	"	
" 6775	"	"	
" 7175	nail in underpinning post of Hospital Bldg		
" 7500	NW COR. SITE 2x2 RW HUB		
0700	"	"	" - Heavy BRUSH

South 551	POT	Lat	
" 9575	"	"	"
" 1709	"	"	"
" 2717	"	"	Light "
" 3390	"	"	"
" 3976	"	"	"
" 4541	"	"	Heavy "
" 5619	"	"	"
" 5808	SW COR SITE = 2x2 RW HUB	"	"

NE COR SITE = 0700

South 574 nail in N header of Camp Kearny paving





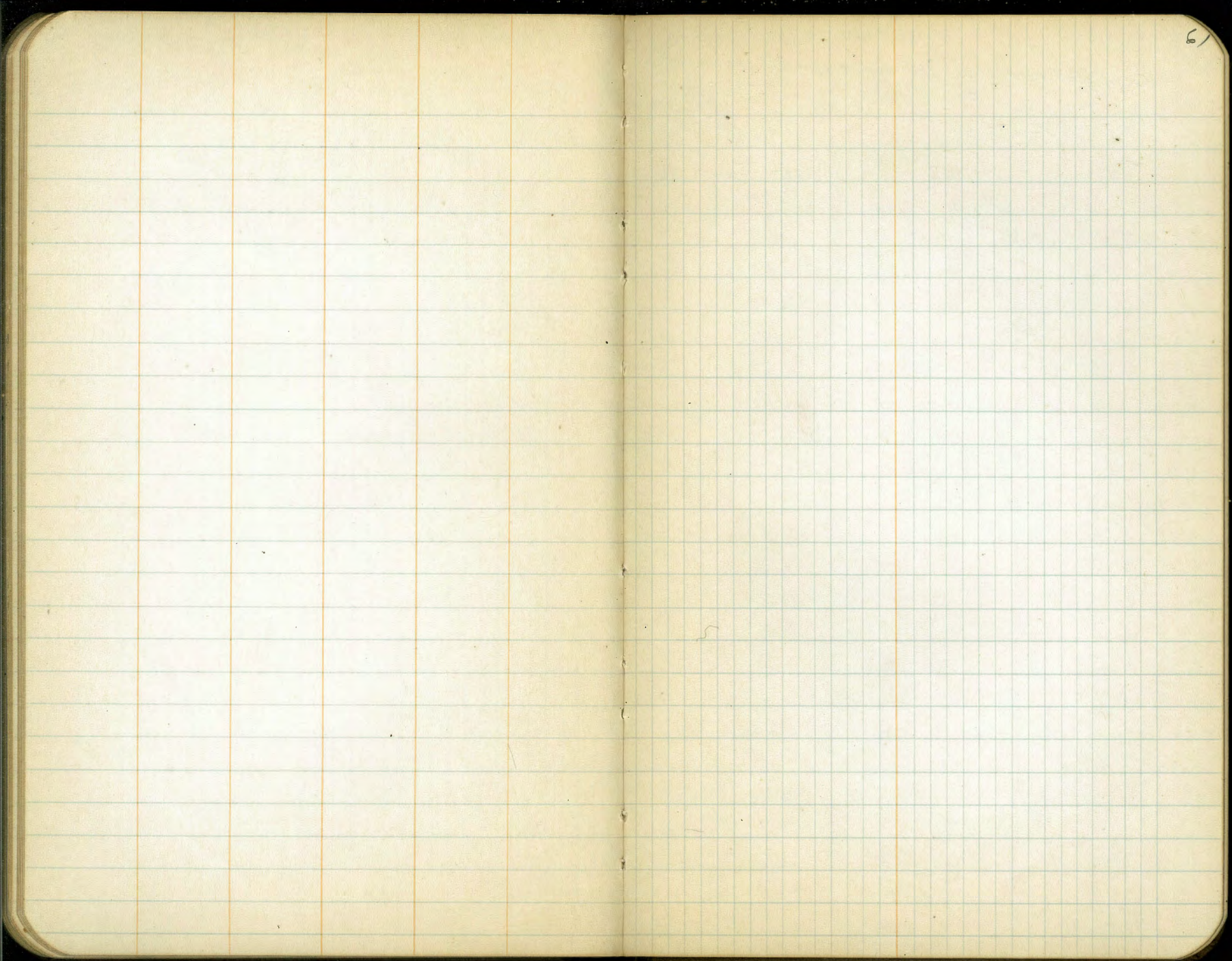
Proposed Dirigible Site

South	1009	P.O.T.	Lat
"	1829	"	"
"	2577	"	"
"	3443	"	"
"	4458	"	Heavy BRUSH
"	4860	"	"
"	5127	"	"
"	5439	"	"
"	5800	= SE COR Site = near RW HUB	

Angle turned from S.E. COR to  
<sup>intersection</sup> West line of Site.

No STADIA taken on South line  
 South line Heavy BRUSH





10



Cross Section of Polk 35<sup>th</sup> to Cherokee 37<sup>th</sup> to Chamounie

374.17

62

40' st.  
6 1/2' Sidewalks  
6 3/4' = 1/4

374.17

0.67 377.72 377.05 B.P. N.W. Cor. Wilson  
3.74 374.17 7.29 370.43 \*Orange

F.L. 35<sup>th</sup> Existing Paving

s cb. Top Corn.

gut.

1/4

1/4

1/4

gut

N. cb

o+00 see sketch

N. cb

gut

1/4

1/4

1/4

gut

s cb.

o+50

s cb.

gut

1/4

1/4

1/4

3.62 370.55  
3.99 370.18  
3.68 70.49  
3.55 70.62  
3.55 70.62  
3.67 70.50  
3.15 371.02  
3.15 371.02  
3.67 70.50  
3.5 70.7  
3.4 70.8  
3.7 70.5  
4.1 70.1  
3.72 370.45  
3.85 370.32  
4.5 69.7  
3.9 70.3  
3.5 70.7  
3.6 70.6

Reduced  
9-27-28  
Run

gut.

N. cb

1+00

N. cb

gut

1/4

1/4

1/4

gut

s cb.

1+25 = break in curb on North for Alley

s cb

gut

1/4

1/4

1/4

gut

N. cb

1+29 = break for Alley on South.

Top Ch.

1+48 Bk for Alley on North

Top Ch.

1+54 = Alley on South.

N. cb

gut

3.8

3.29

3.55

3.9

4.0

3.6

3.7

4.2

3.92

3.96

4.6

4.0

3.6

3.6

3.7

3.53

3.97

3.61

3.61

4.0

370.4

70.88

70.62

70.3

70.2

70.6

70.5

70.0

370.25

370.21

69.6

70.2

70.6

70.6

70.5

370.64

370.20

70.56

70.56

370.2



374.17

¼	4.1	370.1
e	4.0	370.2
¼	4.3	69.9
gut	4.5	69.7
scb	4.05	70.12
2+00		
scb	4.25	69.92
gut	4.7	69.5
¼	4.4	69.8
e	4.2	370.0
¼	4.1	70.1
gut	4.0	70.2
n. cb	3.73	370.44
2+50		
n. cb.	3.82	370.35
gut	4.5	369.7
¼	4.3	69.9
e	4.1	70.1
¼	4.5	69.7
gut	4.8	69.4
scb	4.39	369.78
2+94 = W.L. Wilson on paving		
scb	4.56	69.61
gut	5.06	69.11
¼	4.65	69.52
¼	4.32	369.85

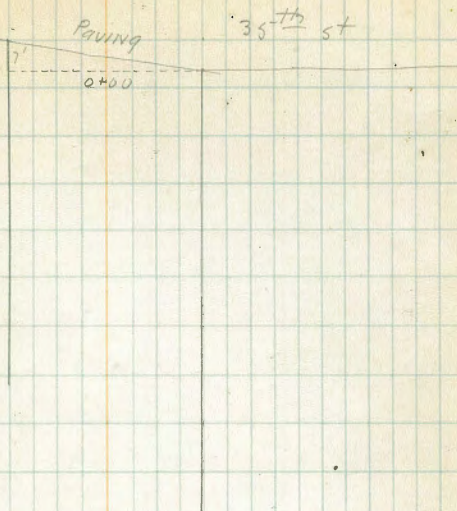
374.17

¼	4.21	369.96
gut	4.27	69.90
n. cb	3.88	70.29
0+00 = E.L. of Wilson, on paving = 1+01		
scb	4.29	69.28
gut	5.33	68.84
¼	5.05	69.12
e	4.00	69.37
¼	4.85	69.32
gut	4.98	69.19
n. cb	4.44	69.73
0+50		
n. cb	4.60	69.57
gut	5.4	68.8
¼	5.4	68.8
e	5.1	69.1
¼	5.3	68.9
gut	5.2	68.4
scb	5.00	69.17
1+00		
scb	5.19	68.98
gut	5.7	68.5
¼	5.7	68.5
e	5.3	68.9
¼	5.5	68.7
gut	5.6	68.6

63



n. cb	4.68	69.49
1+40		
n. cb	4.25	369.32
gut	5.2	
$\frac{1}{4}$	5.2	
e	5.1	
$\frac{1}{4}$	5.6	
gut	5.7	
s. cb	5.37	68.80
1+60		
s. cb	5.41	68.76
gut	5.7	
$\frac{1}{4}$	5.5	
e	5.2	
$\frac{1}{4}$	5.2	
gut	5.3	
n. cb.	5.02	69.15
2+00		
n. cb	5.06	69.11
gut	5.6	
$\frac{1}{4}$	5.5	
e	5.5	
$\frac{1}{4}$	5.8	
gut	5.8	
s. cb	5.43	68.74





374.17

2+50

scb.	5.56	368.61
gut	6.0	
$\frac{1}{4}$	5.8	
d	5.4	
$\frac{1}{4}$	5.6	
gut	5.7	
n cb	5.15	369.02

3+00 = W.L. 36<sup>th</sup> st on paving

n cb	5.42	368.75
gut	5.25	68.32
$\frac{1}{4}$	5.66	
e	5.70	68.47
$\frac{1}{4}$	5.90	
gut	6.22	67.95
scb.	5.73	368.44
T.P.	5.24	368.93

0.38 369.31

0+00 = E.L. 36<sup>th</sup> st on paving

scb	1.39	67.92
gut	2.17	67.14
$\frac{1}{4}$	1.90	
d	1.57	67.74
$\frac{1}{4}$	1.48	
gut	1.63	67.68
n cb	0.93	68.48

369.31

65

0+50

n cb.	1.67	67.64
gut	2.6	
$\frac{1}{4}$	2.2	
e	1.9	
$\frac{1}{4}$	2.4	
gut	2.8	
scb	2.06	67.25

+ 1+00

scb	2.68	66.63
gut	3.3	
$\frac{1}{4}$	2.9	
e	2.5	
$\frac{1}{4}$	2.9	
gut	2.9	
n cb.	2.13	67.18

+ 1+40

n cb	2.73	66.58
gut	3.2	
$\frac{1}{4}$	3.1	
e	3.0	
$\frac{1}{4}$	3.2	
gut	3.5	
scb	3.24	66.07

+ 1+62

scb	3.50	65.81
-----	------	-------



369.31

gut	4.1	
$\frac{1}{4}$	3.5	
ε	3.2	
$\frac{1}{4}$	3.6	
gut	3.7	
n.c.b	2.98	66.33
2+00		
n.c.b	3.55	65.76
gut	4.3	
$\frac{1}{4}$	4.3	
ε	3.9	
$\frac{1}{4}$	4.3	
gut	4.4	
s.c.b.	3.89	65.42
2+50		
s.c.b.	4.49	64.82
gut	5.1	
$\frac{1}{4}$	4.9	
d	4.6	
$\frac{1}{4}$	4.9	
gut	4.9	
n.c.b	4.22	65.09
3+00 = W.L. CHEROKEE paving.		
n.c.b	4.89	64.42
gut	3.50	63.81
$\frac{1}{4}$	3.26	

369.31

66

ε	5.30	64.01
$\frac{1}{4}$	5.43	
gut	5.77	63.54
s.c.b	5.23	64.08
E.L. Cherokee on paving		
s.c.b.	5.62	63.69
gut	6.07	63.24
gut	5.75	63.56
n.c.b	5.14	64.17
T.P. 283	362.67	9.47
W.L. 37 <sup>th</sup> ON PAVING		359.84
n.c.b	2.40	60.27
gut	2.87	59.80
gut	3.20	59.47
s.c.b.	2.46	60.21
0+00 = E.L. 37 <sup>th</sup> ON PAVING		
s.c.b	3.00	59.67
gut	3.64	59.03
$\frac{1}{4}$	3.28	
ε	3.25	59.42
$\frac{1}{4}$	3.27	
gut	3.49	59.18
n.c.b	3.04	59.63
0+50		
n.c.b	3.33	59.34
gut	4.0	



362.67

¼	3.7	
e	3.3	
¼	3.8	
gut	4.2	
scb	3.35	59.32

1+00

scb	3.70	58.97
gut	4.3	
¼	3.9	
e	3.6	
¼	3.9	
gut	4.1	
n.cb.	3.50	59.17

1+40

n.cb	3.88	58.79
gut	4.5	
¼	4.1	
e	3.8	
¼	4.0	
gut	4.3	
scb	3.99	58.68

1+60

scb	4.16	58.51
gut	4.4	
¼	4.3	
e	4.2	

362.67

67

¼	4.3	
gut	4.5	
n.cb	3.96	58.71

2+00

n.cb	4.08	58.59
gut	4.7	
¼	4.5	
e	4.5	
¼	4.9	
gut	5.1	
scb	4.54	58.13

2+50

scb	4.70	57.97
gut	5.5	
¼	5.0	
e	4.6	
¼	4.8	
gut	5.0	
n.cb	4.36	58.31

3+00 = W.L. 38<sup>th</sup>

on paving

n.cb	4.48	58.19 ✓
gut	5.12	57.55
¼	4.89	
e	4.86	57.81
¼	5.14	
gut	5.39	57.28



s cb.	4.93	357.74	✓
0+00 = E.L. 38 <sup>th</sup> st. on paving			
s cb.	4.97	57.70	
gut	5.65	57.02	
$\frac{1}{4}$	5.28		
ε	5.15	57.57	
$\frac{1}{4}$	5.06		
gut	5.14	57.53	9
n cb.	5.47	58.20	0
0+50			
n cb.	4.28	58.39	
gut	5.0		
$\frac{1}{4}$	4.8		
ε	4.6		
$\frac{1}{4}$	5.0		
gut	5.3		
s cb.	4.67	58.00	
1+00			
s cb.	4.46	58.21	
gut	4.9		
$\frac{1}{4}$	4.7		
ε	4.3		
$\frac{1}{4}$	4.6		
gut	4.8		
n cb.	3.94	358.73	
1+40			

n cb.	3.79	358.88	
gut	4.8		
$\frac{1}{4}$	4.2		
ε	4.1		
$\frac{1}{4}$	4.4		
gut	4.8		
s cb.	4.17	58.50	
1+61			
s cb.	4.00	58.67	
gut	4.7		
$\frac{1}{4}$	4.2		
ε	4.0		
$\frac{1}{4}$	4.2		
gut	4.5		
n cb.	3.56	59.11	
2+00			
n cb.	3.42	59.25	
gut	4.2		
$\frac{1}{4}$	4.0		
ε	3.7		
$\frac{1}{4}$	4.3		
gut	4.6		
s cb.	3.80	58.87	
2+50			
s cb.	3.52	359.15	
gut	4.1		



362.67

1/4			3.9	
1/2			3.6	
3/4			3.6	
gut			3.8	
n cb			3.18	359.49
3+00 = W.L. 39 <sup>th</sup> st on paving				
n cb.			2.75	59.92
gut			3.33	59.34
1/4			3.19	
1/2			3.28	59.39
3/4			3.43	
gut			3.67	59.00
s cb.			3.15	59.52
T.P.	1.00	363.29	0.38	362.29
0+00 = E.L. 39 <sup>th</sup> on paving				
s cb			3.74	59.50
gut			4.32	58.97
gut			4.05	59.25
n cb			3.46	59.83
0+50				
n cb			3.54	59.75
s cb			3.98	59.31
1+00				
s cb			4.15	59.14
n cb			3.77	59.52

363.29

69

1+40				
n cb			3.99	59.30
s cb			4.33	58.96
1+60				
s cb			4.42	58.87
n cb			4.02	59.27
2+00				
n cb			4.25	59.04
s cb			4.51	58.78
2+50				
s cb			4.65	58.64
n cb			4.37	58.92
3+00 = W.L. 40 <sup>th</sup> on paving				
n cb			4.50	58.79
gut			5.00	58.29
gut			5.35	57.94
s cb			4.79	58.51
T.P.	2.82	361.27	4.84	358.45
E.L. 40 <sup>th</sup> st. paving				
n cb.			2.83	58.44
gut			3.35	57.92
gut			3.73	57.54
s cb			3.21	58.06
0+50				
s cb			3.42	57.85
n cb			3.06	58.21



1+00		
n cb	3.37	57.90
s cb	3.65	57.62
1+32		
s cb	3.80	57.47
n cb	3.49	57.78
1+60		
n cb	3.46	57.81
s cb	3.86	57.41
2+00		
s cb	4.11	57.16
n cb	3.70	57.57
2+50		
n cb	3.99	57.28
s cb	4.36	56.91
3+00 W.L. Central st. paving		
s cb	4.49	56.78
gut	5.05	56.22
gut	4.75	56.52
n cb	4.19	57.08
0+00 = E.L. Central st paving		
n cb	4.26	57.01
gut	4.60	56.67
gut	5.06	56.21
s cb	4.56	56.71

0+50			
s cb	4.60	56.67	
n cb	4.25	57.02	
1+00			
n cb	4.34	56.93	
s cb	4.63	56.64	
1+40			
s cb	4.73	56.54	
n cb	4.43	56.84	
1+60			
n cb	4.57	56.70	
s cb	4.80	56.47	
2+00			
s cb	4.91	56.36	
n cb	4.65	56.62	
2+50			
n cb	4.68	56.59	
s cb	5.03	56.04	
3+00 = W.L. 41 <sup>st</sup> st. Paving			
s cb	5.23	56.04	
gut	5.79	55.48	
gut	5.32	55.95	
n cb	4.73	56.54	
T.P. + 5.64	362.00	4.91	356.36
0+00 = F.L. 41 <sup>st</sup> st. Paving			
n cb	5.18	56.82	



36200

gut	5.71	56.29
gut	6.03	55.97
s cb	5.47	56.53
0+50		
s cb	5.33	56.67
n cb	5.12	56.88
1+00		
n cb	4.95	57.05
s cb	5.23	56.77
1+40		
s cb	5.02	56.98
n cb	4.80	57.20
1+60		
n cb	4.76	57.24
s cb	5.00	57.00
2+00		
s cb	5.06	56.94
n cb	4.68	57.32
2+50		
n cb	4.50	57.50
s b	5.07	56.93
3+00 = W.L. Marlborough st. paving		
s cb	4.91	57.09
gut	5.24	56.76
gut	4.91	57.09
n cb	4.40	57.60

362.00

71

0+00 = E.L. Marlborough st. paving		
n cb	3.93	58.07
gut	4.53	57.47
gut	4.90	57.10
s cb	4.44	57.56
0+50		
s cb	4.20	57.80
n cb	3.70	58.30
1+00		
n cb	3.51	58.49
s cb	3.88	58.12
1+40		
s cb	3.75	58.25
n cb	3.32	58.68
1+60		
n cb	3.27	58.73
s cb	3.65	58.35
2+00		
s cb	3.32	58.68
n cb	3.04	58.96
2+50		
n cb	2.84	59.16
s cb	3.06	58.94
3+00 = W.L. 42 <sup>nd</sup> st paving		
s cb	2.86	59.14
gut	3.46	58.54



362.00

gut	3.13	58.87
n cb	2.59	59.41
T. P. + 00 = 686 - 2366.52 = 2.34	2.34	359.66
0+00 = E.L. 42 <sup>nd</sup> st paving		
n cb	6.72	59.80
gut	7.37	59.15
gut	7.67	58.85
s cb	7.06	59.46
0+50		
s cb	6.50	60.02
n cb	8.31	60.21
1+00		
n cb	5.80	60.72
s cb	6.05	60.47
1+40		
s cb	5.58	60.94
n cb	5.43	61.09
1+60		
n cb	5.28	61.24
s cb	5.49	61.03
2+00		
s cb	5.04	61.48
n cb	4.86	61.66
2+50		
n cb	4.47	62.05
s cb	4.55	61.97

366.52

72

3+00 = W.L. Van Dyke st. paving		
s cb	3.94	62.58
gut	4.60	61.92
gut	4.54	61.98
n cb	4.05	62.47
0+00 = E.L. Van Dyke st. paving		
n cb	3.99	62.53
gut	4.55	61.97
gut	4.68	61.84
s cb	4.09	62.43
0+50		
s cb	4.41	62.11
n cb	4.51	62.01
1+00		
n cb	4.99	61.55
s cb	4.85	61.67
1+40		
s cb	5.18	61.34
n cb	5.37	61.15
1+60		
n cb	5.60	60.92
s cb	5.30	61.22
2+00		
s cb	5.70	60.82
n cb	6.07	60.45



366.52

2+50		
n cb	6.59	59.93
s cb	6.18	60.34
2+99 W.L. 43 <sup>rd</sup> st paving		
s cb	6.55	59.97
gut	7.20	59.32
gut	7.30	59.22
n cb	6.97	59.55
0+00 = E.L. 43 <sup>rd</sup> st paving		
n cb	7.06	59.46
gut	7.63	58.89
gut	7.65	58.87 ✓
s cb	6.73	59.79
0+50		
s cb	6.82	59.70
n cb	7.09	59.43
1+00		
n cb	7.18	59.34
s cb	6.85	59.67
1+24		
s cb	6.93	59.59
n cb	7.11	59.34
T.P. 0.95 360.65	6.82	359.70
1+45		
n cb	1.34	59.31
s cb	1.16	59.49

360.65

73

2+00		
s cb	1.21	59.44
n cb	1.36	59.29
2+69 = W.L. Fairmount st paving		
n cb	1.40	59.25
gut	1.92	58.73
gut	1.85	58.80 ✓
s cb	1.38	59.27
0+00 = E.L. Fairmount st paving		
s cb	1.43	59.22
gut	2.17	58.48
gut	2.17	58.48
n cb	1.51	59.14
0+50		
n cb	2.36	58.29
s cb	2.33	58.32
1+00		
s cb	3.33	57.32
n cb	3.24	57.41
1+25		
n cb		
s cb	3.72	56.93
	3.84	56.81
1+59		
s cb	4.46	56.19
n cb	4.38	56.27



360.65

2+00		
n cb	5.03	55.62
s cb	5.29	55.36
2+50		
s cb	6.36	54.29
n cb	6.11	54.54
2+75 = W.L. 44 <sup>th</sup> st paving		
n cb	6.39	54.26
gut	6.73	53.92
gut	7.06	53.59
s cb	6.66	53.99
0+00 = E.L. 44 <sup>th</sup> st paving		
s cb	6.89	53.76
gut	7.31	53.34
gut	7.04	53.61
n cb	6.59	54.06
0+50		
n cb	6.66	53.99
s cb	6.99	53.66
1+00		
s cb	7.03	53.62
n cb	6.74	53.91
1+27		
n cb	6.84	53.81
s cb	7.04	53.61
1+49		

360.65

74

s cb	7.01	53.64	
n cb	6.85	53.80	
2+00			
n cb	6.97	53.68	
s cb	7.13	53.52	
2+36			
s cb	7.23	53.42	
n cb	7.02	53.63	
2+73 = W.L. Highland st paving			
n cb	7.01	53.64	
gut	7.61	53.04	
gut	7.78	52.87	
s cb	7.25	53.40	
6+00 = E.L. Highland st paving			
s cb	7.40	53.25	
gut	7.92	52.73	
gut	7.84	52.81	
n cb	7.36	53.29	
T.P. 571	359.02	7.34	353.31
0+50			
n cb	5.59	53.43	
s cb	5.57	53.45	
1+00			
s cb	5.37	53.65	
n cb	5.47	53.55	
<del>7+25</del> 1+25			



359.02

n cb	5.42	53.60
s cb	5.29	53.73
1+47		
s cb	5.15	53.87
n cb	5.35	53.67
2+00		
n cb	5.22	53.75
s cb	4.90	54.12
2+35		
s cb	4.70	54.27
n cb	5.20	53.82
2+71 = W.L. 45 <sup>th</sup> st paving		
n cb	5.00	54.02
gut	5.40	53.62
gut	4.94	54.08
s cb	4.49	54.53
0+00 = E.L. 45 st paving		
s cb	4.92	54.10
gut	5.46	53.56
gut	5.96	53.06
n cb	5.49	53.53
0+50		
n cb	5.18	53.84
s cb	5.26	53.22
1+00		
s cb	6.54	52.48

359.02

75

n cb	6.95	52.07
1+25		
n cb	7.29	51.73
s cb	6.92	52.10
1+47		
s cb	7.25	51.77
n cb	7.59	51.43
2+00		
n cb	8.32	50.70
s cb	8.19	50.83
2+35		
s cb	8.82	50.20
n cb	8.83	50.19
2+70 = W.L. Chamouna st paving.		
n cb	9.35	49.67
gut	9.86	49.16
gut	9.97	49.05
s cb	9.44	49.58
<del>BM</del>	6.44	352.58
		352.56 = B.M.
		N.W. Cor Orange + 45 <sup>th</sup>

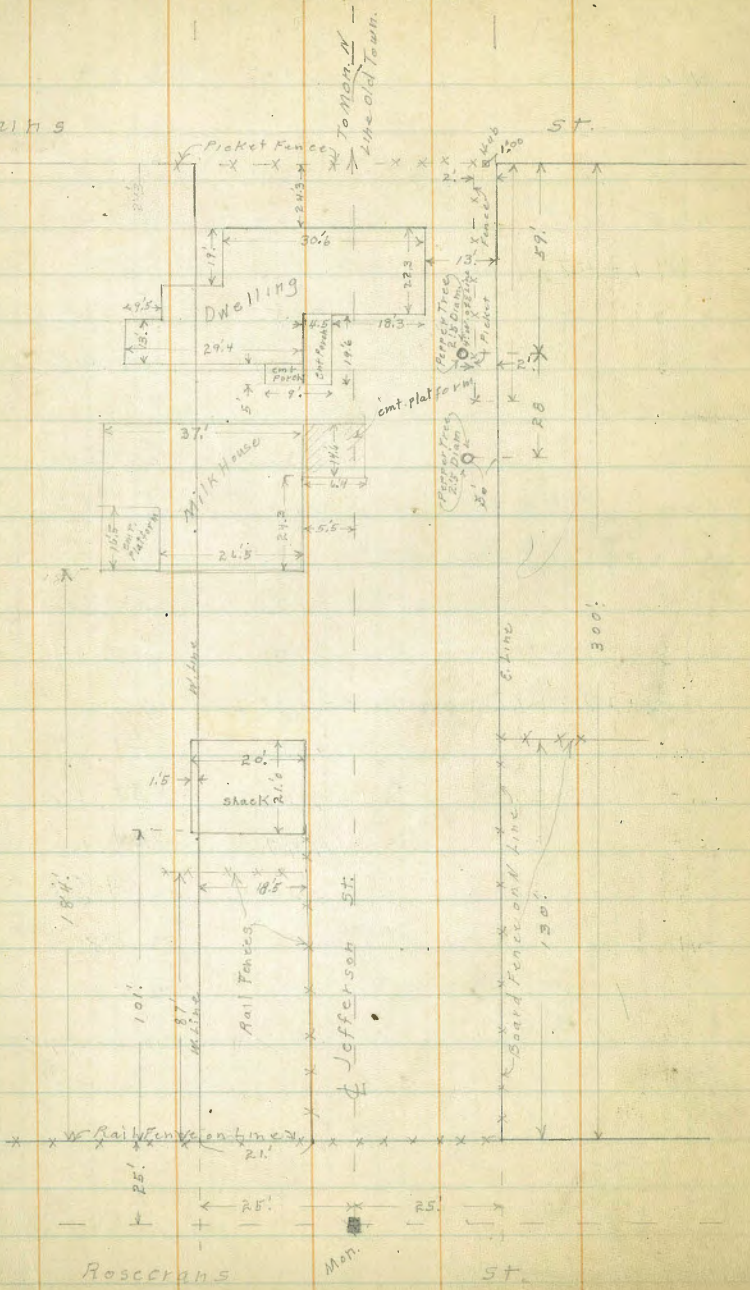


Oct 1929  
M.C.N.

Survey of Bldgs in Jefferson St  
Bet. Rosserans & Gains

Gains

ST.



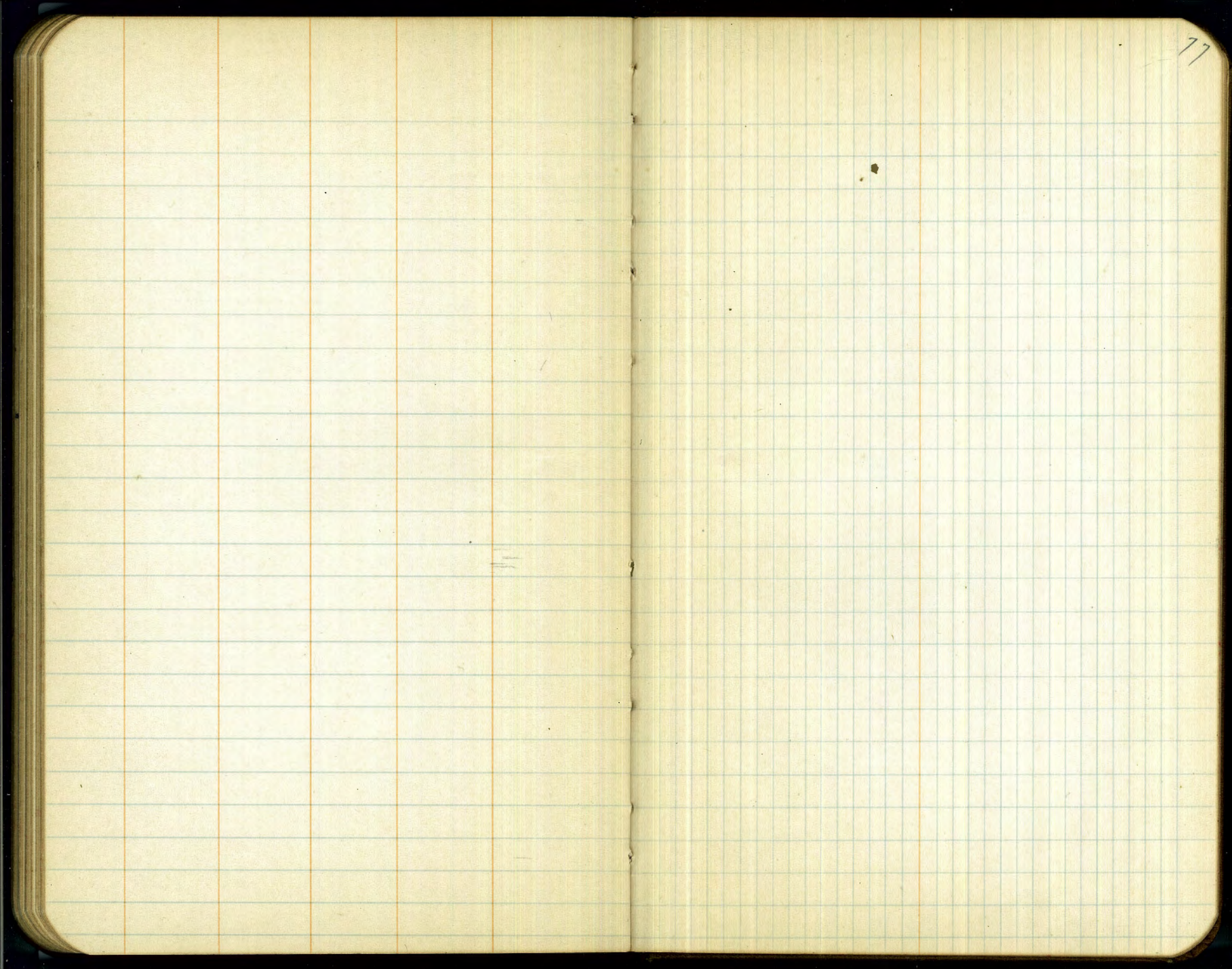
Rosserans

Mon.

ST.

87  
57  
1.5















Recd. 11/17  
0/18M

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder  
stake for any width roadway, slope 1% to 1.  
If ground is nearly level, the run or fall at side  
stake is located by the double entry method in  
left column and top row. The number in body  
of table is run and column gives distance

IMPROVED TABLES  
AND  
INFORMATION

To find Tangent and External for curve of  
any other degree, divide by degree of curve and  
add correction found in column of correction.  
Degree of curve with a given  $L$  may be found  
by dividing tangent (or external), opposite  $L$  by  
given tangent (or external).  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the radius.



Catalina and Varona 250.17