

1183

UNIVERSITY  
OF CALIFORNIA

---

FIELD BOOK

No. 385 F

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1183

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*ENGINEERING and DRAFTING SUPPLIES*

IRVING PARK STATION

CHICAGO, ILL.

	Page
Sewer levels Russell St	1
" Udall	2
" Whittier	4
" Voltaire	5
" Easement in West Cliff Pl. w.	7
X Sec Lincoln St - Bdry E	18
" " Culvert	19
Sewer levels Dell Mar Ave	8
" Blk 1 Rosecrans Park	9
X Sec (Anna) Polk, Chamouna-Euclid	10
" 51st - Orange to University	24
Sewer Blk 5, Loma Alta No 1	36+67
" levels Venice - Orchard to Alley	37
" " Renault - Verona to La Paloma	38
" " McCauley - Capistrano to Tustin	39
" " Plum - Lowell to SW	40
X Sec Evergreen - Zola to Yonge	41
" " Tennyson to Sterne	43
" Mar Ave - Ex. Pl. to P.L.	47
" College Ave - Prospect to 350' N	57
" Landis St - Euclid to alley	62
" High St - Torrey Rd to College	64
" Alley Blk 6 South Challas	68
" " " 20 L.W. Kimball's	72

16133  
error

Lower levels of Rainfall 57  
 Rainfall to Plum

1000  
 211.2

5700	1188	17.11	5.23	
	W/nd all Rainfall = 00	4.1	13.0	
TP	1272	19.43	0.30	16.81
+50		4.3	17.9	
		6.2	23.0	
+50		1.5	27.7	
TP	1278	41.76	0.25	48.98
		8.9	32.9	
+60 & Locust		2.6	39.2	
TP	1286	54.25	0.17	41.50
		10.4	43.8	
+50		4.6	49.6	
TP	1288	66.90	0.14	54.03
		9.8	57.1	
+50		4.6	62.3	
TP	1271	79.11	0.50	66.40
+50		9.6	69.5	
+75		0.8	78.3	
TP	1276	91.33	0.54	78.57
+50		5.9	85.4	
+25		2.5	88.8	
+50		2.2	89.1	
+75		6.0	85.3	
+50		11.2	80.1	
+90		6.3	85.0	
+50		2.7	88.6	
TP	1322	104.80	0.57	90.76

Rainfall  
 Rainfall

100.00

6430 & Evergreen	7.3	96.7
TP	1319	117.10
6465	9.0	108.1
7400	2.2	113.3
TP	1298	129.61
+25	11.8	117.8
+50	6.8	122.8
+75	2.3	127.3
TP	1328	142.19
+50	8.3	133.9
+25	2.2	139.8
TP	1268	152.63
+50	6.2	147.8
+75	3.2	151.2
TP	1328	167.21
+50	12.2	151.8
+50	8.2	159.0
10400 & Willow	7.0	160.2
check to sugar willow & Rainfall	6.0	161.11
+50	6.4	160.8
11	5.2	162.0
+50	3.2	164.0
12	1.2	165.8
TP	887	175.27
+50	7.2	167.8
13400	4.6	170.7
+70 & PLUM	3.0	172.3

161.33  
 div error

EODAL		Sewer Levels		Plum to Pavers		16324	
SWOP 126	194.77	1871.6	193.1	8+50	✓ 5.8	157.4	
E Plum 200	67	193.1	193.1	T.P. 041	151.11	12.5	150.70 ✓
+25	5.5	195.3	195.3	9		3.2	147.9
+50	5.7	194.1	194.1	+40		9.8	141.3
1	4.5	195.0	195.0	+50		13.1	138.0
+50	2.6	195.2	195.2	T.P. 042	138.70	12.83	138.78 ✓
✓	5.5	194.3	194.3	10+00		9.1	129.6
+50	7.2	192.4	192.4	T.P. 044	126.91	12.23	126.97 ✓
3	8.6	191.2	191.2	+50		6.7	120.2
+30	8.6	191.4	191.4	+75		13.3	113.6
285	13.3	186.5	186.5	T.P. 011	114.01	13.01	113.90 ✓
+70 Fullout	13.7	186.1	186.1	11+10		9.2	104.8
J	12.2	185.6	185.6	T.P. 019	101.78	12.42	101.59 ✓
+05	12.9	186.9	186.9	+35		6.3	95.5
+50	12.0	187.8	187.8	T.P. 064	89.32	13.10	88.68 ✓
✓	12.7	187.1	187.1	+60		3.3	86.0
T.P. 063	12.7	187.23	187.23	+85		13.3	76.0
+50	2.7	185.0	185.0	T.P. 021	76.30	13.23	76.09 ✓
6	5.0	182.7	182.7	12+10		10.4	65.9
+50	6.9	180.8	180.8	T.P. 191	65.29	12.92	63.38 ✓
7	9.8	177.9	177.9	+25		10.7	54.6
+25	12.7	175.0	175.0	T.P. 011	52.92	12.46	52.83 ✓
+50 & Overground	12.9	174.8	174.8	+50		6.1	46.8
T.P. 109	12.67	172.99	172.99	T.P. 005	40.14	12.85	40.09 ✓
8+00	9.8	166.3	166.3	+75		2.3	37.8
T.P. 002	12.56	163.22	163.22	13+00		7.7	32.4
				T.P. 098	28.76	12.96	27.18 ✓

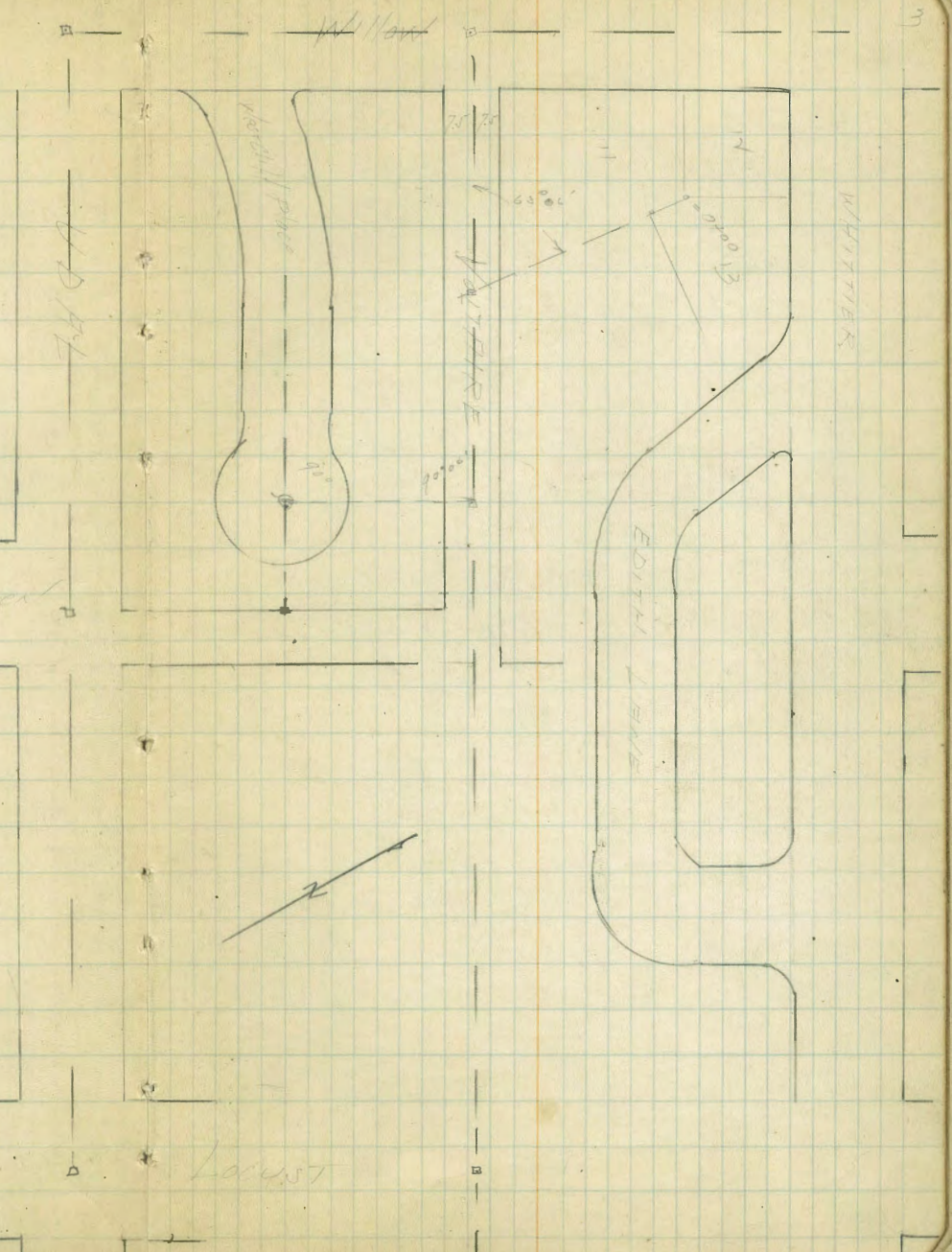
Sewer Levels & UDAAL

2816

13+50	2.0	25.8
+700 S. Alp. ...	4.9	23.3
14+00	7.0	19.2
T.P. 2.8v	12.2v	15.50
14+15 S. W. ...	5.0	13.1
14+20	12.0	12.31

Sewer Levels & Willow / UDAAL to Whittier

18716	0.5	187.92
18610	2.0	186.0
184.0	4.0	184.0
179.9	8.1	179.9
175.6	12.4	175.6
175.16	12.8	175.16
171.3	15.1	171.3
169.2	16.2	169.2
167.97	17.6	167.97
167.3	18.1	167.3
166.6	18.8	166.6
166.3	19.1	166.3
165.9	19.5	165.9
165.4	10.2	165.4
165.0	10.4	165.0



Sewer Levels  
 @ Whittier Willow to Evergreen ✓

175.43

2 Willow - 0100	10.4	165.0
2+35 = El Willow	11.8	163.6
+70	13.1	162.3
T.P. 1.71	163.88	132.6
1+00	2.4	161.5
+50	3.7	160.2
4	6.1	157.8
+50	8.9	155.0
3	12.8	151.1
T.P. 4.21	153.42	130.0
+35	2.3	158.9
3+70 @ Evergreen	5.7	147.5

Use old notes from here to Rosecrans

± 6' ELEVATIONS between Lots 10-11  
 & 14-15  
 Sewer Levels ✓

156.86

2+00 = 5' at edge of Lot 10-11-14	3.2	153.7
0+28	8.5	148.4
T.P. 0.51	144.03	131.4
0+58	15.5	128.7
T.P. 0.27	131.39	131.02
0+81	13.7	117.7
0+83	16.9	119.5
0+89	18.4	113.0
0+97.5 = Junction with 3' distance	10.1	121.3

5/17/07  
 off Rosecrans

Source Levels  
 P Voltages without to Roscrans ✓

121.71 ✓

0.89	168.86	167.97	#465 <sup>with/out</sup> voltages
0.7	168.0		
0.35	2.0	166.9	
4.55	4.5	164.4	
4.75	9.8	159.1	
1+20	13.5	155.4	
T.P. 0.95	156.86	155.91	
T.P. 0.51	144.03	143.7	
1+50	11.4	133.0	
T.P. 0.37	131.39	131.0	
1+64	5.0	126.4	
1+69	9.5	121.9	
4.74	10.8	120.6	
4.74	8.2	123.2	
4.79	6.5	124.9	
1+96.5 = Junction of 1st & 2nd	10.1	121.3	
T.P. 0.25	121.71	118.66	
2+25	9.8	111.9	
4.55	10.8	110.9	
4.75	9.0	112.7	
4.91 <sup>near road lots 5-6</sup>	8.30	113.71	
3+00	8.2	113.5	
4.25	10.8	110.9	
4.35	9.0	112.7	
4.50	4.8	111.9	
4.65	9.7	112.0	

3+78	wedge having strip	5.2	115.9
3+91	" "	6.7	115.0
4.96	" "	6.7	114.8
4+05	= 51 EMP ground	10.7	110.8
T.P. 1.71	111.88	11.5	110.17
4+25		8.0	103.9
4.75		11.0	100.9
5+15		16.5	95.5
T.P. 0.42	100.75	11.55	100.33
5+45		11.6	89.1
4.83		9.8	90.9
6+04.5	wedge having strip	8.6	92.1
4.33	" "	12.5	88.2
4.65	" "	12.4	87.3
4.51		7.5	93.2
7+00		10.1	90.6
T.P. 0.30	87.88	13.7	87.55
7+40	4th line out	3.1	84.8
7+75		9.9	78.0
T.P. 0.65	75.67	12.86	75.0
8+00		2.2	73.4
4+25		10.6	65.1
7+0 - 0.95	65.57	12.15	63.54
4.55		3.5	61.0
4.55		8.5	56.0
T.P. 0.58	52.27	12.78	51.69



527 Sewer Level  
± Voltage ✓

8+75		2.5	49.8
9+00		11.6	40.7
TP 0.88	42.9	12.6	39.31 ✓
+2		6.4	33.8
+50		8.8	31.4
+75		10.6	29.6
10+00		13.4	27.0
TP 0.56	27.93	13.4	27.07 ✓
+50		6.8	21.1
+75		4.6	18.3
+75 w/ Rosecrans		12.4	15.5
TP 2.50	18.25	13.08	14.85 ✓
check BM Rosecrans Adal		5.94	12.31 ✓
			1307.3 Jerron

10+75  
2+91  
7+84

Southern Levels

6 segments between lots 5 & 6

South to Westchill of a thumb west

10.53	123.94	11.24	142.29	Sub
10.5		113.4		
+10 South		15.5	108.4	
+25		16.5	107.4	
+40		8.2	115.5	
+55		1.1	122.8	
T.P. 12.51	136.44	0.31	123.63	✓
+70		6.7	129.7	
T.P. 12.75	148.36	0.86	135.58	✓
+90		11.7	136.7	
1.42 East of Westchill Pass		1.0	147.4	
T.P. 13.11	161.17	0.30	148.06	✓
+150		10.7	150.3	
+75		6.7	154.5	
		3.0	159.2	
F.P. 13.20	173.75	0.62	160.55	✓
+200		11.9	161.8	
+253 = distance lot 9 & 8		5.5	165.2	
willow tree hub & distance		5.78	167.77	167.97

120

Senior Levels

Del MAR Five ✓

Catalina Blvd to Chatsworth 4

WBSP	12.56	176.47	163.91	South Coast Catalina
TP	11.85	187.14 ✓	118	175.79 ✓
4 Catalina - 0000			2.7	184.4
+50			2.9	184.2
1			2.8	184.3
+50			2.5	184.6
✓			2.4	184.7
+50			1.8	185.3
3			0.8	186.3
TP	10.80	197.06 ✓	0.88	186.76
+50			9.2	187.9
✓			6.3	190.8
+50			3.1	194.0
TP	13.11	209.41 ✓	1.06	196.00 ✓
5			11.4	197.7
+50			6.7	202.4
6			2.8	206.3
TP	10.18	218.77 ✓	0.52	208.19 ✓
+50			9.4	209.4
7			7.4	211.4
+50			6.2	212.6
8			5.4	213.4
+50			5.0	213.8
9			4.9	213.9
+50			5.4	213.4

218.77

10+00. L = Wagon parking 5.30 213.47  
out Chatsworth Blvd

Sewer Levels  $\pm$  11/10/1  
 BIK 1 Rosecrans Park ✓

WBP	130'	262.8	0.57	250.7	catchment corridor
T.P.	5-97	268.58	0.57	262.67	
00-30 & Verona St			5.8	262.8	
0100-172	" "		4.6	264.8	
+50			5.4	263.2	
1			6.7	261.9	
+50			8.0	260.6	
2			9.6	259.0	
+50			11.1	257.5	
3			12.0	256.6	
+50			12.9	255.7	
T.P.	6-21	262.16	12.86	255.7	
4			7.4	251.8	
+50			8.7	253.5	
5			10.2	252.0	
+50			11.6	250.6	
+95			12.2	250.0	
6 - St Paloma			14.5	247.7	
+30 & "			14.6	247.6	
T.P.	11-40	272.95	0.58	246.58	

Sewer Levels  $\pm$  11/10/1  
 BIK 2 Rosecrans Park ✓

				272.95	
St Paloma 200		3.2	269.8	1/2	Paloma not connected
0+0		5.3	267.2		
+20		7.0	266.0		
+30 - St Paloma		5.1	267.9		
+40		1.1	271.9		
T.P.	12-60	285.26	0.32	272.46	
+80		12.0	273.3		
1+30		11.7	273.6		
+50		10.6	274.7		
2+30		9.4	275.9		
+80		8.3	277.0		
3+30		7.1	278.2		
+80		5.2	279.9		
4+30		4.1	281.2		
T.P.	6-60	290.98	0.58	284.38	
5+50		7.7	283.3		
5+30		5.8	285.2		
+80		2.5	288.5		
6+20		1.9	289.1		
+30 - St Verona		5.2	285.8		
+40		7.2	283.8		
+60 & "		5.1	285.9		
T.P.	9-86	278.69	13.15	277.83	
T.P.	13-1	267.27	12.73	265.96	
200		256.13	13.20	254.07	
check to B.M.		5.95	259.18	250.7	

Cross Section of (Anna) St  
Chamounie to Euclid

60' wide  
65' chs  
675' 1/2  
UNIL APP  
116 1/2 ST

357.65

3/4/27

Moore  
Prater  
Flood  
Asbury

12

NUMBER	142	357.65	351.23
	EL Chamounie = 0100		
S top cem curb	3.3	349.42	
N " " "	3.30	349.35	
	142.5 = w/1 alloy curb sidewalk in to w/1 alloy		
	alloy sidewalks should be constructed		
S	3.6	49.0	
cb top cem cb	3.8	48.84	
gut	5.1	47.5	
1/4	4.4	48.2	
c	3.8	48.8	
1/4	5.1	47.5	
gut	4.7	47.9	
cb top cem cb	3.8	48.84	
N	5.0	48.6	
	1470		
N	5.3	47.3	
cb	5.3	47.3	
1/4	5.5	47.1	
c	5.5	47.1	
1/4	5.7	46.9	
cb	5.2	47.4	
S	5.1	47.5	
	2420		
S	6.2	46.4	
cb	5.6	47.0	
1/4	6.0	46.6	

**PLOTTED**  
3/4/27  
Larry

c	5.2	347.4
1/4	5.5	47.1
cb	5.5	47.1
N	5.7	46.9
	2470 = w/1 of 46 1/2 ST = 60' wide 12 curbs	
N	5.3	47.3
cb	5.3	47.3
1/4	5.5	47.1
c	5.5	47.1
1/4	5.6	47.0
cb	5.8	46.8
S	5.7	46.9
	w/1 cb	
S	5.6	47.0
cb	6.0	46.6
1/4	5.5	47.1
c	5.2	47.4
1/4	5.1	47.5
cb	5.3	47.3
N	5.2	47.4
	w/1 1/4	
N	5.2	47.4
cb	5.2	47.4
1/4	5.2	47.4
c	5.2	47.4
1/4	5.2	47.4

35265

cb	5.7	346.9
S	6.0	46.6
Center		
S	5.8	46.8
cb	5.5	47.1
1/4	5.2	47.3
c	5.1	47.5
1/4	5.0	47.6
cb	5.0	47.6
N	5.1	47.5
E 1/4		
N	5.0	47.6
cb	4.9	47.7
1/4	4.9	47.7
c	5.0	47.6
1/4	5.2	47.4
cb	5.5	47.1
S	5.7	46.9
E cb		
S	5.7	46.9
cb	5.4	47.2
1/4	5.1	47.5
c	4.8	47.8
1/4	4.7	47.9
cb	5.0	47.6
N top corner cb	4.48	48.17

35265

FINNA

11

FL 4644 = 0400		
N	4.6	48.0
cb	4.7	47.9
1/4	4.6	48.0
c	4.7	47.9
1/4	5.0	47.6
cb	5.4	47.2
S	5.2	47.4
0+50		
S	4.9	47.8
cb	4.6	48.0
1/4	4.3	48.3
c	4.0	48.6
1/4	3.9	48.7
cb	4.3	48.3
N	3.8	48.8
1+00		
N	2.6	50.0
cb	3.4	49.2
1/4	3.2	49.4
c	3.2	49.4
1/4	3.3	49.3
cb	3.5	49.1
S	3.7	48.9
1+50		
S	3.0	49.6

352.65

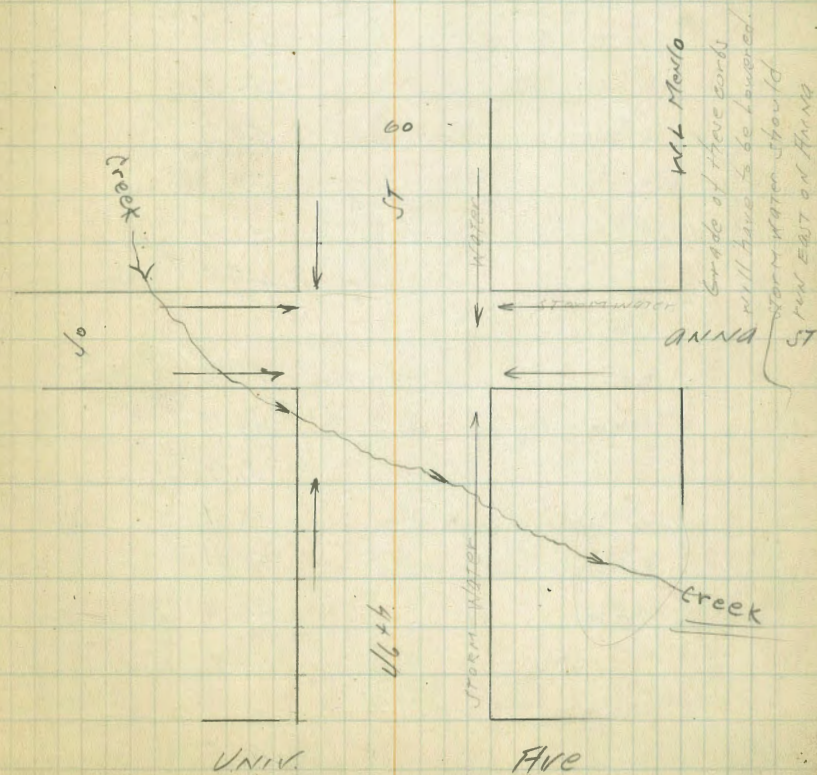
cb	3.0	349.6
1/4	2.5	50.1
c	2.3	50.3
1/4	2.4	50.2
cb	2.5	50.1
N	1.8	50.8
2400		0
N	0.8	51.8
cb	1.4	51.2
1/4	1.4	51.2
c	1.4	51.2
1/4	1.4	51.2
cb	1.8	50.8
S	1.5	51.1
2435		
S	1.2	51.4
cb	1.6	51.0
1/4	1.4	51.2
c	1.3	51.3
1/4	1.4	51.2
cb	1.5	51.1
N	0.9	51.7
T.P.	222	353.61
2470 = WL Menlo = 12' curbs, 60' wide		351.39 ✓
N	2.6	51.0
cb	3.7	49.9

353.61

Anna

12

1/4	2.9	350.7
c	2.7	50.9
1/4	2.9	50.7
cb	3.0	50.6
S	2.5	51.1



353.61

Web

S		2.5	351.1
cb		3.5	50.1
1/4		3.3	50.3
C		3.0	50.6
1/4		3.3	50.3
cb		3.6	50.0
N	top com cb	3.20	50.41
	w 1/4		
N		3.8	49.8
cb		3.6	50.0
1/4		3.4	50.2
C		3.3	50.3
1/4		3.4	50.2
cb		3.7	49.9
S		3.7	49.9

Center

S		3.8	49.8
cb		3.9	49.7
1/4		3.7	49.9
C		3.5	50.1
1/4		3.5	50.1
cb		3.6	50.0
N		3.7	49.9

E 1/4

N		4.1	49.5
---	--	-----	------

353.61

Flora

13

cb		3.9	349.7
1/4		3.8	49.8
C		3.7	49.9
1/4		3.8	49.8
cb		4.0	49.6
S		4.1	49.5
	E cb		
S		4.0	49.6
cb		4.3	49.3
1/4		4.1	49.5
C		4.0	49.6
1/4		4.2	49.4
cb		4.4	49.2
N	top com cb	4.05	49.56
N	top ydpo	4.4	49.2
	E L Mentla = 0+00		
N		4.6	49.0
cb		4.7	49.9
1/4		4.5	49.1
C		4.3	49.3
1/4		4.6	49.2
cb		4.7	48.9
S		4.2	49.4
	0+50		
S		5.6	48.0
cb		6.1	47.5



353.61

1/4	5.9	347.7
e	5.7	47.9
1/4	5.7	47.9
cb	5.9	47.7
n	5.5	48.1
1+00		
n	6.8	46.8
cb	7.2	46.2
1/4	7.1	46.5
e	7.0	46.6
1/4	7.3	46.3
cb	6.7	46.9
S	6.5	47.1
1+50		
S	7.0	46.6
cb	8.5	45.1
1/4	8.4	45.2
e	8.6	45.0
1/4	8.3	45.3
cb	8.7	44.9
n	8.6	45.0
2+00		
n	10.1	43.5
cb	10.4	43.2
1/4	10.2	43.4
e	10.0	43.6

353.61

Flora

1/4	10.3	343.3
cb	10.3	43.3
S	8.4	45.2
2+35		
S	10.1	43.5
1/4	10.3	43.3
cb	11.9	41.7
1/4	11.5	42.1
e	11.2	42.4
1/4	11.4	42.2
cb	11.6	42.0
n	11.7	41.9
2+70 = WL	4/7+3 ST	60 m de 15' curbs
n	12.8	40.8
cb	12.7	40.9
1/4	12.3	41.3
e	12.5	41.1
1/4	13.2	40.4
cb	13.0	40.6
S	12.6	41.0
T.P. 690	347.30 ✓	13.2 ✓ 340.37 ✓
W/cb		
S	7.7	39.6
cb	7.5	39.8
1/4	7.0	40.3
e	6.3	41.0

347.30

1/4	6.3	341.0
cb	6.7	40.6
N to beam ab w 1/4	6.32	40.98
1/4	6.4	40.9
cb	6.6	40.7
1/4	6.7	40.6
c	6.4	40.9
1/4	6.7	40.6
cb	7.3	40.0
S	7.6	39.7
Center		
S	7.7	39.6
cb	7.6	39.7
1/4	7.2	40.1
c	6.6	40.7
1/4	6.7	40.6
cb	6.7	40.6
1/4	6.4	40.9
E 1/4		
1/4	6.5	40.8
cb	6.6	40.7
1/4	6.9	40.4
e	6.9	40.4
1/4	7.3	40.0
cb	7.7	39.6
S	7.9	39.4

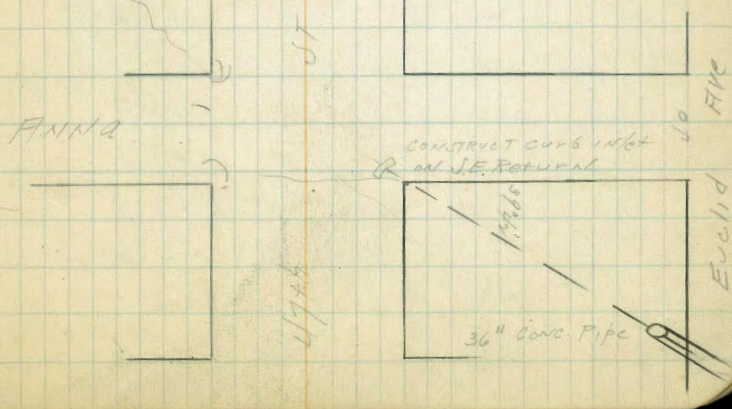
347.30

Anna

15

E cb

S	9.3	338.0
cb	8.2	39.1
1/4	7.3	40.0
c	6.9	40.4
1/4	6.6	40.7
cb	6.6	40.7
N	6.26	41.04
FL 47+4 ST = 0+00		
N	6.7	40.6
cb	6.7	40.6
1/4	6.7	40.6
c	6.6	40.7
1/4	7.4	39.9
cb	9.0	38.3
S	10.1	37.2
+5	10.5	36.8
Culvert Levels		
SE Cor Anna 47+6 = 00	10.1	37.2
0+20	10.3	37.0



347.30

0425

-5	9.8	337.5
S	9.6	37.7
cb	8.9	38.4
1/4	7.6	39.7
C	6.6	40.7
1/4	6.7	40.6
cb	6.6	40.7
N	6.0	41.3

0450

N	5.5	41.8
cb	6.2	41.1
1/4	6.2	41.1
C	6.0	41.3
1/4	6.2	41.1
cb	7.1	40.2
S	7.4	39.9

1400

S	6.5	40.8
t3	6.3	41.0
t4	5.1	42.2
cb	4.6	42.7
1/4	3.8	43.5
C	5.2	43.1
1/4	4.1	43.2
cb	4.2	43.1
N	3.7	43.6

347.30

FINN

16

1450

N	1.5	345.8
cb	2.1	45.2
1/4	2.0	45.3
C	1.9	45.4
1/4	2.0	45.3
cb	2.8	44.5
S	4.5	47.8

2400

S	2.5	44.5
cb	0.7	46.6
1/4	0.1	47.2
C	0.2	47.1
1/4	0.5	46.8
cb	0.8	46.5
N	0.1	47.2

TP	5.62	354.87	✓	005	347.25	✓
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2435

N	4.3	48.6
cb	4.9	48.0
1/4	4.8	48.1
C	4.6	48.3
1/4	4.6	48.3
cb	5.2	47.7
S	6.9	46.0

352.87

2+68

S	4.5	348.4
cb	4.1	48.8
1/4	5.8	47.1
c	6.0	46.9
1/4	5.8	47.1
cb	5.0	47.9
N	3.5	49.5

2+70 = WL Euclid Ave

N	7.1	45.8
cb top com curb	7.27	45.55
1/4	8.1	44.8
c	8.1	44.8
1/4	8.7	44.7
ab " " "	7.86	45.01
S	7.6	45.3
sheet to 357. 351.30	1.48	351.39✓

17

Walker  
9-26-27

X. Section Lincoln St 14' cb 80' side  
From E.L. Boundary St. East  
13 1/2 S.

Note: Cb line Stations on north

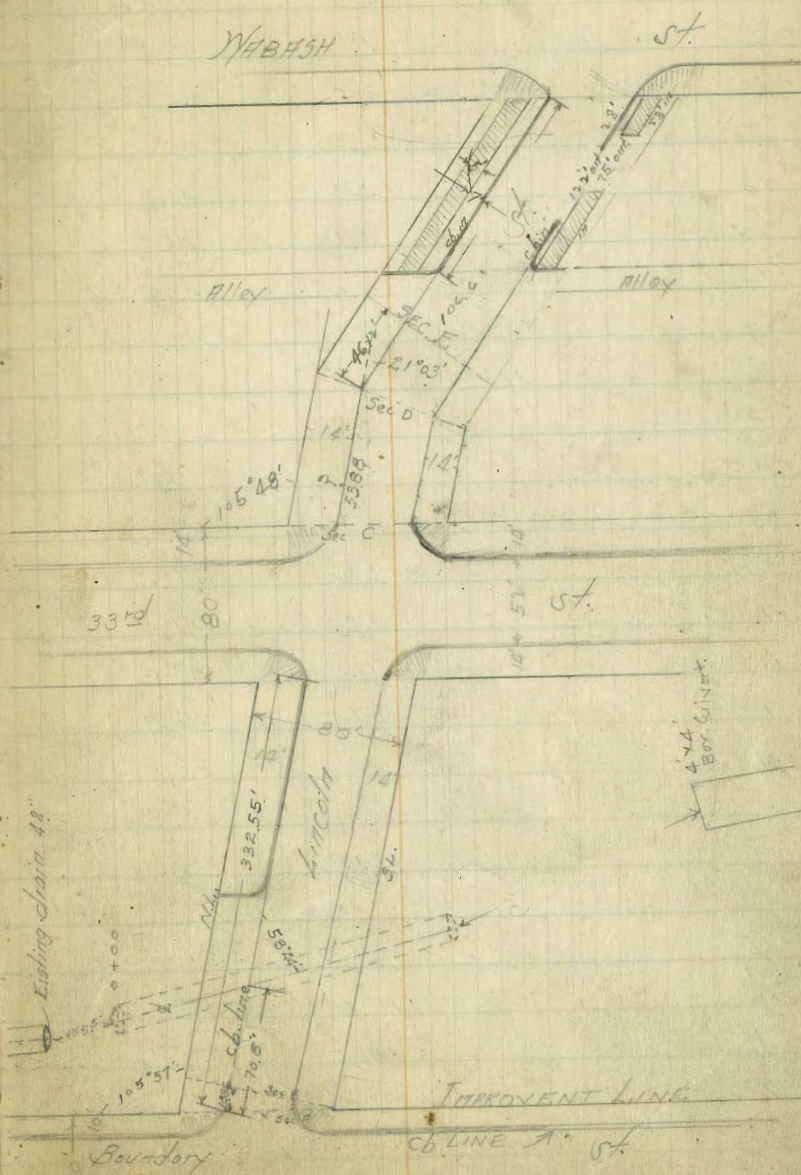
N.V. SF				
Univ. of Bdry.	1.42	337.86		333.44
T.P.	7.19	346.37	0.68	337.18
Sec A. Parallel with E.L. Bdry.				
N		4.8		41.6
N top cb		5.01		41.36
Gut		5.8		40.6
1/4		4.9		41.5
1/2		5.2		41.2
3/4		4.4		42.0
Gut		5.9		40.5
S top cb		5.38		40.99
S		5.1		41.3

Sec B = 18.86 E

S.	5.1	41.3
+5	3.8	42.6
cb	4.6	41.8
1/4	4.4	42.0
1/2	4.2	42.2
3/4	3.8	42.6
cb	2.7	43.7
N	2.8	43.6
+10	7.7	38.7

33' E OF E.L. Boundary St.

-10	6.6	39.8
N	4.1	42.3



cb	4.4	42.0
$\frac{1}{4}$	4.3	42.1
2	4.1	42.3
$\frac{1}{4}$	3.9	42.5
+8	6.3	40.1
cb	4.7	41.7
+4	4.7	41.7
+8	3.0	43.4
S	3.1	43.3
	44'E	
S	3.3	43.1
+5	3.6	42.8
cb	8.7	37.7
+9	5.1	41.3
$\frac{1}{4}$	5.4	41.0
6	9.2	37.2
$\frac{1}{4}$	9.7	36.7
cb	9.7	36.7
N	10.7	35.7
+10	11.4	35.0
	56'E	
-15	15.3	31.1
N	16.3	30.1
cb	16.5	29.9
$\frac{1}{4}$	17.0	29.4
2	15.4	31.0

$\frac{1}{2}$	10.3	36.1
cb	12.8	33.6
S	8.6	37.8
+5	8.0 ✓	38.4
T.P. 2.76	336.83	12.30
	74'E	334.07
-10	6.5	30.3
S	7.5	29.3
cb	8.5	28.3
$\frac{1}{2}$	8.1	28.7
2	7.7	29.1
$\frac{1}{4}$	7.3	29.5
cb	7.0	29.8
N	7.1	29.7
+15	7.6	29.2

## LEVELS For Robert

-155.5 = Floor line of Existing Drain	6.17	330.71
-30	7.1	29.7
-25	5.1	31.7
0+00	5.1	31.7
+40	7.0	29.8
+76	8.3	28.5
+86	7.8	27.0
+96	8.4	26.4
1+05	6.9	29.9
+25	8.6	28.2

1441 = End		9.7	27.1
T.P.	135	329.10	9.08
109.5' S.E. of End on Rim of H.H.		5.75	323.35
163' S.E. " " = Hand line 4' to Box Culvert		<sup>39</sup> 5.40	320.70
T.P.	12.61	340.49	13.5

94' E of E.L. Boley on N. cb line

-10		9.0	31.4
N		11.0	29.4
cb		12.2	28.2
$\frac{1}{2}$		12.6	27.8
$\frac{1}{4}$		12.6	27.8
$\frac{1}{4}$		12.9	27.5
cb		13.2	27.2
S		13.5	26.8
+15		13.7	26.7

101' E

-15		13.4	27.0
S		12.7	28.7
cb		12.0	28.4
$\frac{1}{2}$		12.5	28.9
$\frac{1}{4}$		12.4	28.0
$\frac{1}{4}$		11.6	28.8
cb		8.2	32.2
N		6.9	33.5
+10		8.5	31.9

118' E

-1.0		6.6	33.8
N		6.9	33.5
cb		4.6	35.8
+6		5.5	34.9
$\frac{1}{4}$		9.0	31.4
$\frac{1}{2}$		9.3	31.1
$\frac{1}{2}$		7.2	33.2
cb		8.8	31.6
S		11.5	29.9
+15		12.8	27.6

131' E

-15		12.7	27.7
S		6.6	31.8
cb		3.8	36.6
+7		4.6	35.8
$\frac{1}{4}$		2.0	38.4
$\frac{1}{2}$		5.8	34.6
$\frac{1}{2}$		6.0	34.4
+8		4.3	36.1
cb		3.5	37.9
+4		5.0	35.4
N		5.4	35.0
+5		5.5	34.9

139

-5		4.7	35.7
N		4.7	35.9

34049  
39

+7	5.0	35.4
cb	3.8	36.6
$\frac{1}{4}$	3.5	36.9
$\frac{1}{2}$	2.3	38.1
$\frac{1}{4}$	0.6	39.8
+6	2.6	37.8
cb	2.2	38.2
S	9.1	31.0
+7	13.0	27.4
+15	13.0	27.4

163' E

-15	13.1	27.3
S	10.0	30.4
cb	3.4	37.0
$\frac{1}{2}$	2.8	37.6
$\frac{1}{4}$	2.6	37.8
$\frac{1}{4}$	4.0	36.4
cb	3.8	36.6
N	3.5	36.9

20'  
East line of alley North  
No. 2nd. 1870-11

↑  
187' E = beginning of East cb on N

N top cb	3.04	37.35
$\frac{1}{4}$	3.5	36.9
$\frac{1}{2}$	3.4	37.0
$\frac{1}{4}$	3.8	36.6
cb	3.6	36.8
+8	4.6	35.8

34049  
39

21

S	6.9	33.5
+10	9.1	31.0
209' E		
-10	8.6	31.8
S	4.4	36.0
+2	3.6	36.8
cb	4.1	35.3
$\frac{1}{4}$	3.5	36.9
$\frac{1}{2}$	3.2	37.2
$\frac{1}{4}$	3.1	37.3

N top cb	2.88	37.51
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250' E

N " "	2.65	37.74
$\frac{1}{4}$	2.9	37.5
$\frac{1}{2}$	3.1	37.3
$\frac{1}{4}$	3.4	37.0
+10	4.2	36.2
cb	3.5	36.9
S	3.6	36.8
+10	8.5	31.9

300' E

-10	6.4	34.0
S	4.5	35.9
cb	3.6	36.8
$\frac{1}{4}$	3.3	37.1
$\frac{1}{2}$	2.7	37.7



340.49  
.39

$\frac{1}{2}$	2.6	37.8
N top cb	2.49	37.90
of EL. Boundary 332.55' E = N.L. 33rd st.		
N top cb	2.34	38.05
N Gut on Paving	3.00	37.39
$\frac{1}{4}$ " "	2.73	37.76
$\frac{1}{2}$ " "	2.63	37.76
$\frac{1}{4}$ " "	3.05	37.34
Gut. " "	3.80	36.59
S top cb	3.31	37.05
T.P.	10.42	347.57 <sup>47</sup>
	3.34	337.15 <sup>05</sup>

Sec C

S top cb	8.10	39.37
S top cb	8.37	39.10
Gut on Paving	8.85	38.62
$\frac{1}{2}$ " "	8.21	39.26
$\frac{1}{2}$ " "	7.86	39.61
$\frac{1}{4}$ " "	7.80	39.67
Gut " "	8.05	39.42
N top cb	7.37	40.10
N	7.0	40.5

Sec D

N	6.0	41.5
$\frac{1}{2}$	6.0	41.5
$\frac{1}{4}$	7.4	40.1
$\frac{1}{2}$	7.3	40.1

347.57  
.47

32

$\frac{1}{4}$	8.1	39.4
cb	8.2	39.3
$\frac{1}{2}$	7.9	39.6
S	6.7	40.8
Sec E		
S	7.4	40.1
cb	8.1	39.4
$\frac{1}{2}$	7.6	39.9
$\frac{1}{2}$	6.7	40.8
$\frac{1}{4}$	6.6	40.9
cb	6.6	40.9
N	5.5	42.0

50' East of Sec E

N	4.7	42.8
cb	5.9	41.6
$\frac{1}{2}$	5.9	41.6
$\frac{1}{2}$	5.7	41.8
$\frac{1}{2}$	6.9	40.6
cb	7.5	40.0
S	7.0	40.5

106.40' East of Sec. E = East line of Alley  
Section Parallel with Alley

S top cb at Prop.	5.80	41.67
top cb on cb line	5.94	41.53
Gut	6.6	40.9
$\frac{1}{4}$	6.2	41.3
$\frac{1}{2}$	5.7	41.8

327.57  
.47

23

$\frac{1}{4}$	5.5	42.0
Gut on top of Grate	6.21	41.26
top of cb	5.32	42.15
N top of cb at Prop. line	5.23	42.24

194' East of Sec. E = End of Krist. cb on S. From St. Hwy

N top cb	4.37	43.10
Gut.	4.8	42.7
$\frac{1}{4}$	4.6	42.9
$\frac{1}{2}$	4.5	43.0
$\frac{1}{4}$	5.2	42.3
Gut	5.7	41.8

S top cb	5.47	42.00
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on N cb line  
304.66 East of Sec. E = N.W. Hoback Section Parallel  
N.W. Hoback

S top cb	3.86	43.61
Gut on Parity	4.41	43.06
$\frac{1}{4}$ " "	3.82	43.65
$\frac{1}{2}$ " "	3.61	43.86
$\frac{1}{4}$ " "	3.70	43.77
N Gut " "	4.21	43.26
N top cb	3.35	44.12

Y.P. 1.09. 335.25<sup>65</sup> 12.91 334.66<sup>56</sup>

chk on BM. UNIV + MISC 13.50 322.15<sup>15</sup>  
322.15 - BM.  
0.00

Walker  
3

X. Section 51st St. 60' wide 9' 7" to N.L. Polk.  
From S.W. Orange Ave to N.L. Univ. {50' wide 10' 4" to N.L. Univ. 7.5' 4"}

342.94

21

BY N.E.				
ORANGE + Alabama	12.48	320.46		307.98
T.P.	12.91	333.35	2.02	320.44
T.P.	9.71	342.94	0.12	333.23
S.L. Orange = 0 + 0.0				
E		2.0		340.9
cb		4.2		338.7
1/4		7.0		335.9
+5		8.0		334.9
2		8.5		334.4
1/4		9.2		333.7
+5		9.8		333.1
N		12.3		330.6
+10		14.9		328.0
50' S				
-10		10.0		332.9
N		9.5		333.4
+7		6.8		336.1
cb		6.8		336.1
1/4		6.3		336.6
2		6.4		336.6
+5		5.9		337.0
1/4		4.4		338.5
+5		2.3		340.6
cb		1.9		341.0
E		0.3		342.6

	100' S	
E	0.4	342.5
cb	1.6	341.3
+3	2.0	340.9
1/4	4.2	338.7
+3	5.1	337.8
2	5.7	337.2
1/4	5.4	337.6
cb	6.2	336.7
N	7.7	335.2
+10	9.5	333.2
150' S		
-10	11.9	331.0
N	10.4	332.5
cb	9.5	333.4
1/4	8.3	334.6
2	8.1	334.8
+6	8.8	334.1
1/4	8.1	334.8
+4	6.4	336.5
cb	5.5	337.4
E	4.3	338.6
200' S		
E	9.0	333.9
cb	9.9	333.0
1/4	11.5	331.4

322.94

2	11.5	331 4
$\frac{1}{4}$	11.9	331 0
cb	12.7	330 2
N	13.5	329 4
+10	14.4	328 5

250'S

-5	16.0	326 9
N	16.0	326 9
cb	15.2	327 7
$\frac{1}{4}$	14.2	328 7
2	13.8	329 1
$\frac{1}{2}$	13.5	329 4
cb	12.7	330 2
E	12.3	330 6

T.P.	0.08	329.96	13.06	329.88
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300'S

E	1.7	327 3
cb	2.4	326 6
$\frac{1}{2}$	2.8	326 2
2	3.0	327 0
$\frac{1}{4}$	3.6	326 4
cb	3.8	326 2
N	4.8	325 2
-5	4.9	325 1

350'S

N	5.6	324 4
---	-----	-------

329.96

cb	5.3	324 7
$\frac{1}{4}$	5.2	324 8
2	4.6	325 4
$\frac{1}{4}$	4.5	325 5
cb	3.9	326 1
E	3.5	326 5

400'S

E	4.9	325 1
cb	5.3	324 7
$\frac{1}{4}$	5.6	324 4
2	5.6	324 4
$\frac{1}{2}$	6.2	323 8
cb	6.1	323 9
N	6.4	323 6

450'S

N	7.6	322 4
cb	7.1	322 6
$\frac{1}{4}$	7.2	322 8
$\frac{1}{2}$	6.9	323 1
$\frac{1}{2}$	7.0	323 0
cb	6.6	323 4
E	6.5	323 5

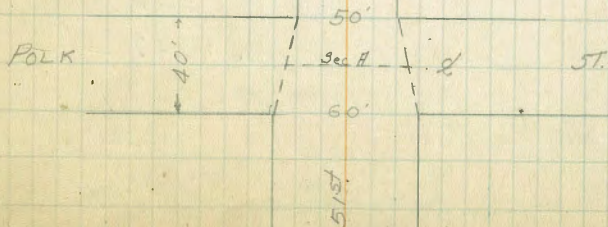
500'S

E	8.6	321 4
cb	8.6	321 4
$\frac{1}{2}$	8.6	321 4

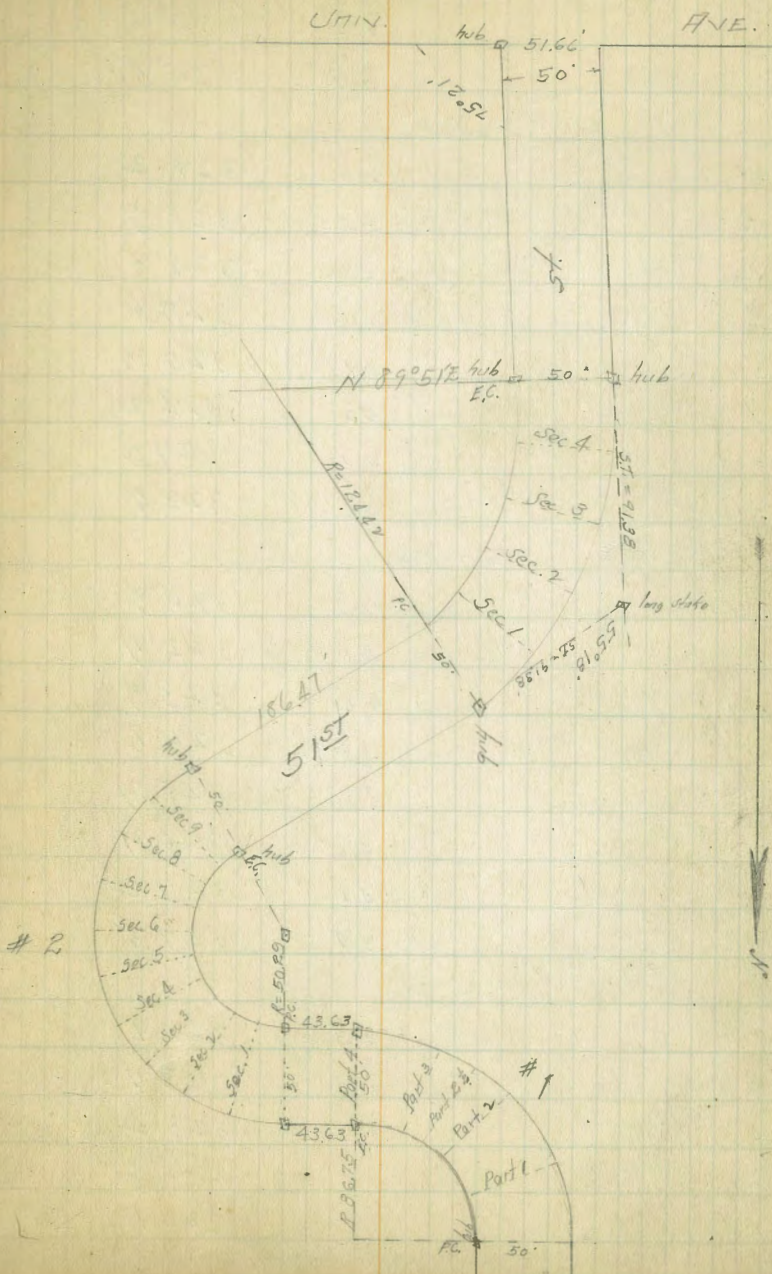
25

2	8.4	321 6
$\frac{1}{2}$	8.5	321 5
cb	8.5	321 5
N	8.3	321 7
540' S		
N	7.1	322 6
cb	8.0	322 0
$\frac{1}{4}$	8.9	321 1
2	9.1	320 9
$\frac{1}{4}$	9.3	320 7
cb	9.4	320 6
E	9.5	320 5
577' S = N.L. Polk <sup>5' cbs,</sup> 7.5' 4.5		
E	10.2	319 8
cb	9.7	320 3
$\frac{1}{2}$	9.4	320 6
2	8.6	321 4
$\frac{1}{4}$	8.1	321 9
cb	7.4	322 6
N	6.6	323 4
Sec A = 4' Polk		
N	6.0	324 0
cb	7.1	322 9
$\frac{1}{2}$	7.8	322 2
2	8.2	321 8
$\frac{1}{4}$	8.5	321 5

cb	9.0	321 0
E	9.7	320 3
5 L. Polk { Note: From S.L. Polk to N.L. Union } 10' cbs 7.5' 4.5		
E	9.8	320 2
cb	9.2	320 8
$\frac{1}{4}$	8.8	321 2
2	8.2	321 8
$\frac{1}{4}$	7.4	322 6
cb	6.5	323 5
N	5.6	324 4
50' S		
N	3.8	326 2
cb	4.5	325 5
$\frac{1}{2}$	5.6	324 4
2	6.2	323 8
$\frac{1}{2}$	7.0	323 0
cb	7.5	322 5
E	8.4	321 6
+5	8.8	321 2



	85' S	
-5	8.0	322 0
E	7.5	322 5
cb	6.1	323 9
$\frac{1}{2}$	5.0	325 0
$\frac{1}{2}$	4.5	325 5
$\frac{1}{2}$	3.8	326 2
cb	2.9	327 1
N	2.2	327 8
115' S = PC.		
N	0.4	329 6
cb	1.0	329 0
$\frac{1}{2}$	1.5	328 5
$\frac{1}{2}$	2.3	327 7
$\frac{1}{2}$	3.3	326 7
cb	4.3	325 7
E	5.9	324 1
+10	7.4	322 6
T.P.	8.44	331.44
	0.96	329.00
CURVE #1 Part 1		
-10	8.3	323 1
E	5.8	325 6
cb	4.2	327 2
$\frac{1}{2}$	3.3	328 1
$\frac{1}{2}$	2.5	328 9
$\frac{1}{2}$	1.7	329 7



cb	1.4	3300
N	0.9	3305
Part 2		
N	2.2	3292
cb	2.5	3289
$\frac{1}{2}$	2.9	3285
$\frac{1}{2}$	3.6	3278
$\frac{1}{2}$	4.1	3273
cb	5.2	3262
E	7.1	3243
+10	8.6	3228
PART 2 $\frac{1}{2}$		
-10	10.7	3207
E	9.0	3224
cb	7.5	3239
$\frac{1}{2}$	6.8	3246
$\frac{1}{2}$	6.0	3254
$\frac{1}{2}$	5.0	3264
cb	4.2	3272
N	3.9	3275
Part 3		
N	7.3	3241
cb	7.7	3237
$\frac{1}{2}$	8.2	3232
$\frac{1}{2}$	8.8	3226
$\frac{1}{2}$	9.3	3221

cb	10.0	3214
E	11.1	3203
+10	✓12.9	3185
T.P. 013	318.65 12.72	31872
PART 4 = E.C.		
-10	4.3	3145
E	4.1	3147
cb	1.2	3146
$\frac{1}{2}$	4.1	3147
$\frac{1}{2}$	4.0	3148
$\frac{1}{2}$	4.1	3147
cb	4.3	3145
N	4.3	3145
P.C. Curve #2		
N	10.5	3083
cb	10.1	3087
$\frac{1}{2}$	10.0	3088
$\frac{1}{2}$	9.7	3091
$\frac{1}{2}$	9.9	3089
cb	9.5	3093
E	8.8	3100
Sec. 1		
E	9.0	3098
cb	9.8	3090
$\frac{1}{2}$	10.6	3082
$\frac{1}{2}$	11.8	3070

$\frac{1}{4}$	11.7	307 1
cb	12.0	306 8
N	12.0	306 8
+10	12.0	306 8

## Sec. 2

-10	13.2	305 6
N	13.4	304 4
cb	12.8	306 0
$\frac{1}{4}$	12.1	306 7
L	11.1	307 7
$\frac{1}{4}$	10.1	308 7
cb	9.2	309 6
E	8.3	310 5

## Sec. 3

E	8.8	310 0
cb	9.7	309 1
$\frac{1}{4}$	10.2	308 6
L	10.9	307 9
$\frac{1}{4}$	11.8	307 0
cb	12.8	306 0
N	13.4	305 4
+10	14.2	304 6

## Sec. 4

-10	7.1	304 6
N	6.2	305 5

cb	4.9	306 8
$\frac{1}{4}$	3.9	307 8
L	3.3	308 4
$\frac{1}{4}$	3.0	308 7
cb	2.7	309 0
E	2.1	309 6

## Sec. 5

E	2.9	309 8
cb	3.3	308 4
$\frac{1}{4}$	3.5	308 2
L	4.1	307 6
$\frac{1}{4}$	4.8	306 9
cb	5.7	306 0
N	6.8	304 9
+10	7.7	304 0

## Sec. 6

-10	6.5	303 2
N	7.1	304 3
cb	6.2	305 5
$\frac{1}{4}$	5.5	306 2
L	5.1	306 6
$\frac{1}{4}$	4.7	307 0
cb	4.4	307 3
E	4.1	307 6

## Sec. 7

E	6.4	305 3
---	-----	-------



cb	6.3	305 4
$\frac{1}{2}$	6.5	305 2
d	6.8	304 9
$\frac{1}{2}$	7.1	304 6
cb	7.5	304 2
N	8.2	303 5
+10	9.5	302 2

Sec 8

-15	9.9	301 8
-8	12.4	299 3
N	9.7	302 0
cb	9.0	302 7
$\frac{1}{2}$	8.9	302 8
d	8.7	303 0
$\frac{1}{2}$	8.6	303 1
cb	8.3	303 4
E	7.8	303 9

Sec. 9

E	7.9	303 8
cb	8.7	303 0
$\frac{1}{2}$	9.3	302 4
d	10.2	301 5
$\frac{1}{2}$	9.9	301 8
cb	10.5	301 2
N	13.0	298 7
+5	11.5	300 2

+10	10.6	301.1
-----	------	-------

E.C. Curve #2

-10	10.1	301 6
N	12.1	299 6
+3	13.5	298 2
cb	11.3	300 4
$\frac{1}{2}$	10.9	300 8
$\frac{1}{2}$	9.7	302 0
$\frac{1}{2}$	9.0	302 7
cb	8.2	303 5
E	7.2	304 5

17' South of E.C.

E	7.1	304 6
cb	8.5	303 2
$\frac{1}{2}$	9.3	302 4
d	10.3	301 4
$\frac{1}{2}$	12.4	299 3
cb	13.0	298 7
N	13.0	298 7
+10	11.3	300 4

31'S

-10	11.8	299 7
N	15.7	296 0
cb	13.7	298 0
$\frac{1}{2}$	13.3	298 4
d	11.0	300 7

31169

$\frac{1}{2}$	9.3	302 4
cb	8.3	303 4
E	6.1	305 6
45' South		
E	4.8	306 9
cb	7.3	304 4
$\frac{1}{4}$	9.6	302 1
$\frac{1}{2}$	11.5	300 2
$\frac{3}{4}$	13.6	298 1
cb	12.8	296 9
+5	16.4	295 3
N	14.4	297 3
+10	11.7	300 0
60' S		
-10	11.9	299 8
N	14.6	297 1
+2	16.8	294 9
cb	15.6	296 1
$\frac{1}{2}$	14.8	296 9
$\frac{3}{4}$	11.2	300 5
$\frac{1}{4}$	9.1	302 6
cb	6.8	304 9
E	4.4	307 3
100' S		
E	5.6	306 1
cb	8.6	303 1

31169

31

$\frac{1}{2}$	11.1	300 6
$\frac{1}{4}$	13.2	298 5
$\frac{1}{4}$	15.3	296 4
cb	16.9	294 8
+9	17.8	293 9
N	19.0	292 7
+10	15.2	296 5
130' S		
-10	15.5	296 2
N	18.9	292 8
+2	19.9	291 8
cb	19.3	292 4
$\frac{1}{2}$	16.8	294 9
$\frac{1}{4}$	14.6	297 1
$\frac{1}{2}$	11.5	300 2
cb	9.3	302 4
E	7.2	304 5
144' S		
E	7.7	304 0
cb	11.4	300 3
$\frac{1}{4}$	13.3	298 4
$\frac{1}{2}$	17.0	294 7
$\frac{1}{4}$	18.0	293 7
+4	22.0	291 7
cb	21.8	289 9
+6	21.0	290 7

N		19.4	292 3
+10		16.5	295 2
T.P.	158	300.55	12.72 298.97
		164'S	
-10		4.0	296 5
N		7.8	292 7
cb		10.3	290 2
+5		11.1	289 4
+6		9.9	290 6
$\frac{1}{2}$		9.3	291 2
$\frac{1}{4}$		7.3	293 2
$\frac{1}{4}$		4.8	295 7
cb		3.3	297 2
E		+0.2	300 7
	186.47 South = PC Curve #3		
E		2.1	298 4
cb		5.0	295 5
$\frac{1}{2}$		7.4	293 1
$\frac{1}{4}$		9.4	290 9
$\frac{1}{4}$		10.7	289 6
cb		11.5	289 0
+2		11.5	289 0
N		8.9	291 6
+10		5.8	294 7
	Sec 1		
-20		16.3	284 2

-15		14.0	286 5
N		13.1	287 4
cb		13.6	286 9
$\frac{1}{2}$		13.3	287 2
$\frac{1}{4}$		12.5	288 0
$\frac{1}{4}$		11.7	288 8
cb		10.1	290 4
E		8.2	292 3
+10		6.9	293 6
	Sec 2		
-15		13.3	287 2
E		14.1	286 4
cb		14.4	286 1
$\frac{1}{4}$		14.6	285 9
$\frac{1}{4}$		14.7	285 8
$\frac{1}{4}$		15.0	285 5
cb		15.0	285 5
N		15.7	284 8
+10		15.7	284 8
+20		16.8	283 7
T.P. 142	289.98	12.99	287.56
	Sec 3		
-20		6.4	283 6
-15		7.6	282 4
-10		6.5	283 5
N		6.3	283 7

cb	6.3	283 7
$\frac{1}{2}$	6.6	283 4
$\frac{2}{2}$	6.0	284 0
$\frac{2}{2}$	5.0	285 0
cb	5.2	284 8
E	5.0	285 0
+ 20	5.1	284 9

Sec 4

- 20	5.9	284 1
E	6.3	283 7
cb	6.6	283 4
$\frac{1}{2}$	6.6	283 4
$\frac{2}{2}$	6.7	283 3
$\frac{1}{2}$	6.6	283 4
cb	7.0	283 0
H	6.7	283 3
+ 15	7.7	282 3
+ 20	9.3	280 7

E.C. Curve # 3 E.L. Stations

- 20	7.3	282 7
- 12	7.3	282 7
- 10	9.0	281 0
- 3	7.6	282 4
H	7.4	282 6
cb	7.4	282 6
$\frac{1}{2}$	7.1	282 8

$\frac{2}{2}$	7.1	282 8
$\frac{1}{2}$	6.7	283 3
cb	6.6	283 4
E	6.3	283 7
+ 20	6.2	283 8

50' South of E.C.

- 20	6.2	283 6
E	6.6	283 4
cb	7.1	282 9
$\frac{1}{2}$	7.2	282 8
$\frac{2}{2}$	7.0	283 0
$\frac{1}{2}$	7.1	282 9
cb	7.5	282 5
H	7.5	282 5
+ 3	7.7	282 3
+ 8	10.3	279 7
+ 15	8.5	281 5
+ 20	7.8	282 2

100' S

- 20	7.8	282 8
- 13	10.8	279 2
- 8	7.8	282 2
H	7.9	282 1
cb	7.5	282 5
$\frac{1}{2}$	7.3	282 7
$\frac{2}{2}$	7.2	282 8

1/4	7.0	283 0
cb	6.6	283 4
E <sub>0</sub>	6.6	283 4
+20	6.2	283 8
150' S		
-20	6.2	283 8
E <sub>0</sub>	6.6	283 4
cb	6.8	283 2
1/4	7.0	283 0
1/2	7.0	283 0
1/4	7.1	282 9
cb	7.9	282 1
W	7.9	282 1
+6	8.4	281 6
+9	10.0	281 0
+16	10.1	279 9
+20	8.1	281 9
176' S Section Parallel with Univ. Ave		
-20	10.4	279 6
-10 = 48" Cor. Pipe	10.84	279 14
-5 = "E" " " "	11.07	278 91
W	7.8	282 2
cb	6.1	283 9
1/4	6.1	283 9
1/2	7.0	283 0
1/4	7.2	282 8

cb	6.4	283 6
E	6.0	284 0
+20	6.0	284 0
180' S		
-20	4.3	285 7
E	4.5	285 7
cb	4.9	285 1
1/2	5.2	284 8
1/4	4.9	285 1
1/2	5.4	284 6
cb	5.4	284 6
W	6.2	283 8
+20	6.4	283 6
TP 873	278.54	0.17
200' S Section Parallel with Univ.		
W	4.0	294 5
cb	2.6	295 9
1/4	2.0	296 5
1/2	2.0	296 5
1/4	1.7	296 8
cb	1.5	297 0
E <sub>0</sub>	0.6	297 5
202' S South = N. Univ. Section Parallel with Univ.		
E	0.7	297 8
E-top cb	1.22	297 32
E Gut on Parking	1.92	296 62

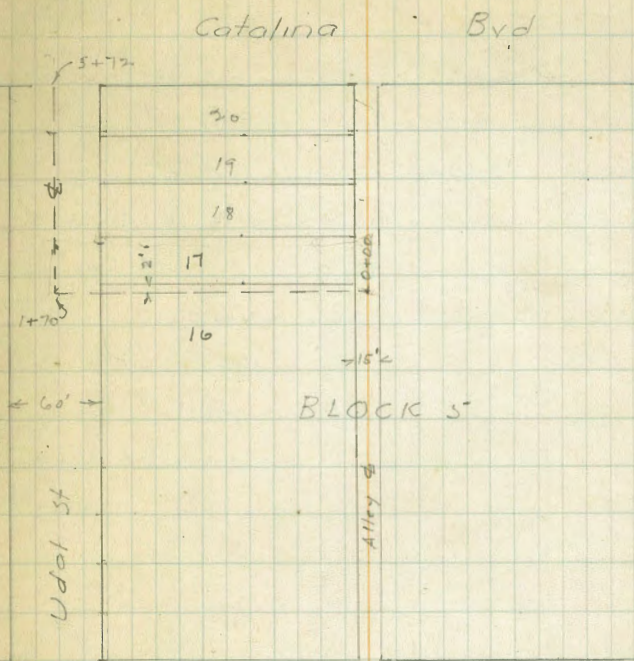
1/2 on paving	185	296.59
1/2 " "	200	296.54
1/4 " "	229	296.25
W Gut " "	276	295.78
W top cb	226	296.28
X	19	296.16
T.P. 1.62	287.92	1224 286.30
chk. on BM N.E. cor Cement Pkwy ss. d.	7.49	2804.3
		28039 - BM
		0.04

Tolman  
6/21/07

7/1/07 checked  
& plotted  
on Pt Loma  
Census sheet  
renewed

Proposed Sewer Line Change  
Block 5, Loma Alta No. 1.

	7.13	79.55		77.42	BM. Spk in Pole SE. cor Voltaire & San Clemente
	11.31	89.13	17.3	77.82	
	12.82	92.52	9.43	79.70	
0+00			12.8	79.7	± Alley
0+06			12.1	80.4	
0+07.5			10.8	81.7	Prop. line
0+50			5.3	81.2	
TP	11.17	101.87	1.82	90.70	
1+00			9.2	92.7	
1+52.6			0.9	101.0	break
1+70			0.1	101.2	± Udal
TP	0.36	102.18	0.05	101.82	
2+12			3.2	99.0	Break
2+37			7.1	95.1	"
TP	2.00	93.37	10.81	91.37	
2+83			4.5	88.9	"
3+10			9.1	84.3	"
TP	0.92	83.60	10.75	82.62	
3+50			5.8	79.8	
3+72			6.6	77.0	



San Clemente St

For Additional Notes See Page 67

Tolman  
6/21/17

Sewer levels on Venice St  
fr. E Orchard St to E Alley to S.W.

37

	2.45	254.76	↓	252.31	SM NW Orch + St Bar
	0.11	242.05	↓	12.82	241.94
	1.13	230.38	↓	12.80	229.25
0+00				13.0	217.4
0+40				13.0	SW Pt. Orch.
TP	3.82	222.58	↓	11.62	218.76
0+90				5.3	211.3
1+40				5.5	211.1
1+90				5.7	210.9

E Alley



Tolson  
6-11-27

Sewer levels on Renauld St  
from  $\pm$  Verona to  $\pm$  La Paloma

38

				En Verona & Catalina
	10.44	260.61	✓	250.17
	12.65	272.60	0.66 ✓	259.95 ✓
	10.96	283.44	0.12 ✓	272.48 ✓
$\pm$ Renauld & Verona $\pm 0-30$			4.8 ✓	278.6 ✓
N.W. PL $\pm 0+00$			4.9 ✓	278.5 ✓
1+00			8.2 ✓	275.2 ✓
2+00			11.3 ✓	272.1 ✓
TP	0.81	271.40	✓	12.85 ✓ 270.59 ✓
3+00			2.3 ✓	269.1 ✓
4+00			5.8 ✓	265.6 ✓
5+00			8.6 ✓	262.8 ✓
6+00-PL			4.5 ✓	259.9 ✓
$\pm$ La Paloma $\pm 30$			11.2 ✓	260.2 ✓

7/4/27.  
Checked & Plotted  
Profile. West #19.  
Point Lower.  
Newcomb.

Tolman  
6/24/27

Prelim. Sewer Levels on Macaulay St  
fr.  $\pm$  of Capistrano towards Tustin St.

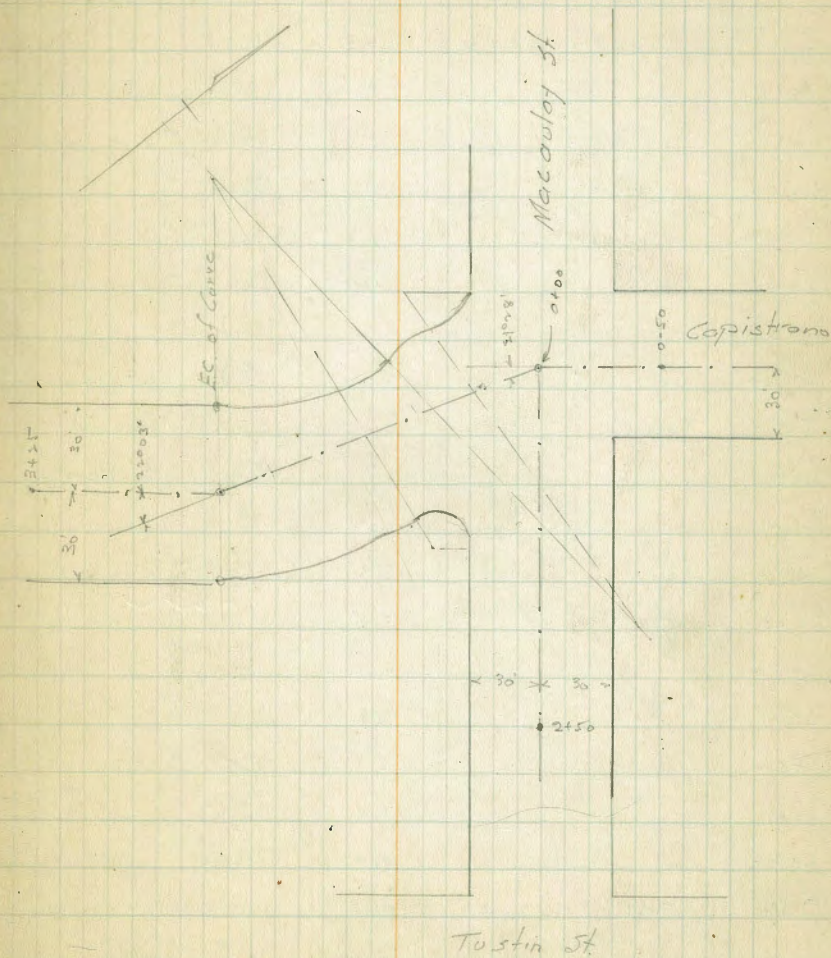
				BM. N.E. Chats & Arlington
	0.48	133.71 ✓		133.23
	6.85	131.03 ✓	9.53	124.19 ✓
	10.36	140.21 ✓	1.18	129.85 ✓
0+00			7.9	✓ 132.3 ✓
0+50			4.2	✓ 136.0 ✓
1+00			0.6	✓ 139.6 ✓
TP	10.28	149.91 ✓	0.58	139.63 ✓
1+50			6.9	✓ 143.0 ✓
2+00			4.3	✓ 145.6 ✓
2+50			1.5 ?	✓ 148.0 ✓

7/2/27  
Plotted on  
Point Level  
P. 8 x 12  
Newcomb

Sewer levels on Macaulay St fr. 50' N.E.  
of N.E. line of Capistrano to a point on  $\pm$  of  
Capistrano St to S.W.

				TP
	12.45	142.30 ✓		129.85
0+50			13.3	129.0 ✓
0+00			10.0	✓ 132.3 ✓
0+20			8.6	✓ 133.7 ✓
0+25			5.6	✓ 136.7 ✓
0+50			5.3	✓ 137.0 ✓
1+00			3.4	✓ 138.9 ✓
TP	7.23	146.80 ✓	2.73	✓ 139.57 ✓
1+50			5.9	✓ 140.9 ✓
1+61.48			5.9	✓ 140.9 ✓
2+00			5.8	✓ 141.0 ✓
2+50			6.4	✓ 140.4 ✓
3+00			9.2	✓ 137.6 ✓
3+25			11.2	✓ 136.6 ✓

7/2/27  
Plotted on  
Point Level  
P. 8 x 12  
Newcomb



Tolman  
4/15/17

Prelim. Sewer Levels on Plum St  
from Lowell st. to the S.W.

			99.29	BM Plum & Macaulay
1.20	100.40		88.14	± Lowell & Plum
5.68	93.82	12.35	83.9	S.W. Prop line
		9.9	86.3	
0+00		7.5	92.4	
+50		1.4	93.19	
TP	12.75	105.94	98.1	
1+00			100.7	
+50			103.3	N.E. Keats St.
2+00			105.72	
T.P.	13.01	118.79	106.9	± Keats
(2+35			108.6	
(30' rt			111.0	S.W. Keats
(2+70			113.3	
(30' rt			112.1	
(3+00			115.4	
(30' rt			115.5	
(3+50			117.0	
(30' rt			118.6	
(4+00			118.69	
TP	5.31	123.90	118.7	
(30' rt			118.8	N.E. Jarvis
(4+70			119.8	
(30' rt			118.0	± Jarvis
(5+05			119.7	
(30' rt				

Tolman  
Checked  
Point Range  
Plotted  
Open shot  
Newcomb

(5+40	123.90	5.7	118.2	S.W. Jarvis
(30' rt		4.9	119.1	
(6+00		6.1	117.8	
(30' rt		4.7	119.2	
(6+50		7.0	116.9	
(30' rt		7.0	116.9	
(6+75		9.4	114.5	
(30' rt		10.8	113.1	

7/2/17  
Same  
Newcomb

Tolman  
9-14-25

70' Street  
18' Curbs  
85 Grts

Xsection Evergreen St - Zola to Yonge

	1.23	136.59	135.36	svr BP Willow & Yonge
TP	6.16	132.57	10.18	126.41

= 0+00 = 5 L Zola St

EL Top Cb		10.74		121.83
& Top Paving		10.31		122.26
W.L. Top Cb		9.60		122.97

= 0+03 =

W.L.		4.6		128.0
cb		6.5		126.1
1/4		7.8		124.8
1/4		9.5		123.1
1/4		9.8		122.8
cb		10.4		122.2
E.L.		10.0		122.6

= 0+16 =

EL		10.1		122.5
cb		9.0		123.6
1/4		8.2		124.4
1/4		6.8		125.8
1/4		6.4		126.2
cb		5.8		126.8

W.L.	4.3	128.3
------	-----	-------

= 0+50 =

W.L.	4.2	128.4
cb	5.7	126.9
1/4	6.4	126.2
1/4	7.6	125.0
1/4	8.4	124.2
cb	9.1	123.5
EL	10.8	121.1

= 0+70 =

EL	11.2	121.4
cb	9.5	123.1
1/4	8.6	124.0
1/4	7.9	124.7
1/4	7.0	125.6
cb	6.1	126.5
W.L.	4.1	128.5

= 1+00 =

W.L.	5.1	127.5
cb	7.2	125.4
1/4	8.2	124.4
1/4	9.1	123.5
1/4	10.1	122.5

Reduced to plotted on Old Profile  
 by L.B.H. 9-19-27

cb	132.57	11.3	121.5
EL		13.1	119.5

= 1 + 35 =

EL		15.9	116.7
cb		14.3	118.3
1/4		13.6	119.0
E		12.3	120.3
1/4		11.3	121.3
cb		10.4	122.2
NL		8.5	124.1

TP	1.43	121.15	12.85	119.72
----	------	--------	-------	--------

= 1 + 56 =

NL		2.6	118.6
cb		4.2	117.0
1/4		5.1	116.1
E		6.6	114.6
1/4		7.3	113.9
cb		8.0	113.2
EL		9.3	111.9

= 1 + 75 =

EL		16.2	105.0
cb		14.3	106.9

1/4		13.7	107.5
E		12.6	108.6
1/4		11.7	109.5
cb		11.0	110.2
NL		9.3	111.9

TP	2.29	111.41	12.03	109.12
----	------	--------	-------	--------

= 2 + 0.0 = NL Yonge St

NL		4.6	106.8
cb		7.3	104.1
1/4		9.1	102.3
E		10.4	101.0
1/4		11.5	99.9
cb		12.3	99.1
EL		15.7	95.7

filled on old  
profile

Tolson  
7-14-27

70' St.  
18' cbs  
89' ats

43

Xsection Evergreen St - Tennyson to Sterne

9.60 203.50<sup>✓</sup> 193.90  
2.06 193.89<sup>✓</sup> 12.67 190.83<sup>✓</sup>

= N.L. Tennyson =

N.L.	2.3	190.6
cb	6.5	186.4
1/2	6.9	186.0
3/4	6.9	186.0
2	8.3	184.6
cb	10.2	182.7
EL	12.9	180.0
+10	14.5	178.4

Reduced and  
plotted by W.M. McG.

North Ck

-10	15.0	177.9
EL	12.9	180.0
cb	10.3	182.6
1/2	8.5	184.4
3/4	7.7	185.2
1/4	6.7	186.2
cb	6.4	186.5
N.L.	5.3	187.6

N Quarter

N.L.	50	187.6
cb	62	186.7
1/2	64	186.5
3/4	70	185.9
2	82	184.7
cb	98	183.1
EL	127	180.2
+10	146	178.3

2 Tennyson

-10	13.8	179.1
EL	12.8	180.1
cb	9.5	183.4
1/4	8.2	184.7
3/4	7.4	185.5
1/2	6.3	186.6
cb	6.0	186.9
N.L.	5.0	187.9

= 2 + 03 =

N.L.	3.0	189.9
cb	5.0	187.9
1/4	6.4	186.5
3/4	7.5	185.4

192.89

1/4	8.6	184.3
cb	10.0	182.9
EL	12.5	180.4

## S. Quarter

-10	14.3	178.6
EL	12.6	180.3
cb	9.6	183.3
1/4	8.7	184.2
±	7.5	185.4
1/4	6.2	186.7
cb	4.9	188.0
W.L	3.0	189.9

## S. Cb

W.L	2.6	190.3
cb	4.5	188.4
1/4	5.9	187.2
±	7.2	185.7
1/4	8.6	184.3
cb	10.1	182.8
EL	12.8	180.1
+10	14.4	178.5

Evergreen

44

## S.L. Tenneyson

-10	15.2	177.7
EL	13.8	179.1
cb	10.6	182.3
1/4	8.8	184.1
±	7.8	185.1
1/4	6.5	186.4
cb	5.2	187.7
W.L	3.3	189.6

## S.L. + 50

W.L	3.6	189.3
cb	6.1	186.8
1/4	7.5	185.4
±	8.8	184.1
1/4	10.5	182.4
cb	12.3	180.6
EL	15.4	177.5
+10	17.6	175.3

TP 2.49 187.55 7.83

185.06

## S.L. + 100

-10	16.5	171.1
EL	14.0	173.6
cb	10.3	177.3

187.55

1/4	8.3	179.3
1/2	6.9	180.7
3/4	5.0	182.6
cb	2.4	184.2
NL	0.8	186.8

SL + 150

NL	5.2	182.4
cb	8.2	179.4
1/4	9.6	178.0
1/2	11.6	176.0
3/4	13.6	174.0
cb	14.5	173.1
EL	17.5	170.1
+10	20.1	167.5

TP	9.64	184.41	12.78	174.77
----	------	--------	-------	--------

NL sterna St

-10	21.0	163.4
EL	19.7	164.7
cb	14.9	169.5
1/4	13.2	171.2
1/2	12.0	172.4
3/4	10.2	174.2
cb	8.5	175.9
NL	5.8	178.6

Evergreen

45

TP	1.22	179.29	6.54	177.84
----	------	--------	------	--------

N cb

NL	1.2	177.9
cb	3.1	175.2
1/4	5.4	173.7
1/2	6.7	172.4
3/4	8.5	170.6
cb	10.3	168.8
EL	14.0	165.1

N 1/4

EL	15.1	164.0
cb	10.9	168.2
1/4	6.5	170.6
1/2	7.0	172.1
3/4	5.6	173.5
cb	4.2	174.9
NL	1.7	177.4

1/2 sterna

NL	2.3	176.8
cb	5.0	174.1
1/4	6.3	172.8
1/2	7.9	171.2
3/4	9.3	169.8



179.09  
+90.09

cb 11.1 168.0  
EL 15.3 163.8

S. 1/4

EL 16.8 162.3  
cb 12.2 166.9  
1/4 10.3 168.8  
♀ 8.6 170.5  
1/4 6.8 172.3  
cb 5.4 173.7  
WL 2.8 176.3

S. cb

WL 2.9 176.2  
cb 5.3 173.8  
1/4 7.2 171.9  
♀ 9.3 169.8  
1/4 11.2 167.9  
cb 13.3 165.8  
EL 19.1 160.0

S. PL

EL 20.5 158.6  
cb 14.4 164.7  
1/4 12.4 166.7  
♀ 10.7 168.4

1/4 8.5 170.6  
cb 6.3 172.8  
1/4 3.5 175.6

12.69 168.76 ✓ 3.0 ✓ 170.07 ✓  
3.3 ✓ 185.44 ✓

Reduced and plotted by W.M.M.C.

X-Section MAR H.V.S.  
from Exchange Pl. to Reblo line

33618

47

BP Paper (Exchange)  
see Field Book 1105  
Page 62

5' c.l.s.  
7.5' r.s.

0.13 245.96 245.83  
T.P. 0.43 233.76 12.63 233.33

Sec. A = Parallel with Exchange

X = top of Drive 13.4 220.4

+3 = top " 12.64 221.12

5.25 = Gutter on Pav. 12.99 220.8

1/2 on Pav. 12.07 221.7

1/2 " " 11.38 222.38

1/2 " " 10.98 222.8

E. Gut " 10.74 223.1

E top of 10.34 223.5

E 9.83 224.0

0+00

E on Ground at Wall 9.05 224.7

1/2 9.1 224.1

1/2 10.5 223.3

1/2 10.9 222.9

1/2 11.2 222.6

cb. 11.4 222.4

X 11.5 222.3

T.P. 12.11 236.18 9.69 224.07

0+24

X 10.3 225.9

cb. 10.5 225.7

1/2 10.3 225.9

10.0 226.2

9.3 226.9

cb. 8.6 227.6

E on Ground at Wall 8.3 227.9

0+44

E at Wall 8.7 230.5

cb. 6.1 230.1

1/2 6.4 229.8

1/2 7.8 228.9

1/2 7.5 228.7

cb. 7.6 228.6

X 7.9 228.3

0+80 = 2 Garage on W. Con. Floor 2' Back = 2' Acacia Tree on East 2' in St. 10" dia.

-2' = Floor 2.97 233.3

X 3.2 233.0

cb. 3.0 233.2

1/2 2.9 233.3

1/2 2.5 233.7

1/2 2.2 234.0

cb. 1.9 234.3

+3 = at tree 1.9 234.3

E at Wall 1.9 234.3

0+84 = 2 Con. Walk on E. 5' in St. 5' wide 1.67 234.6

T.P. 12.88 249.01 0.01 236.17

0+90 = 2 Acacia tree on East 2' in St. 10" dia.

E at Bottom of Wall 12.1 234.9

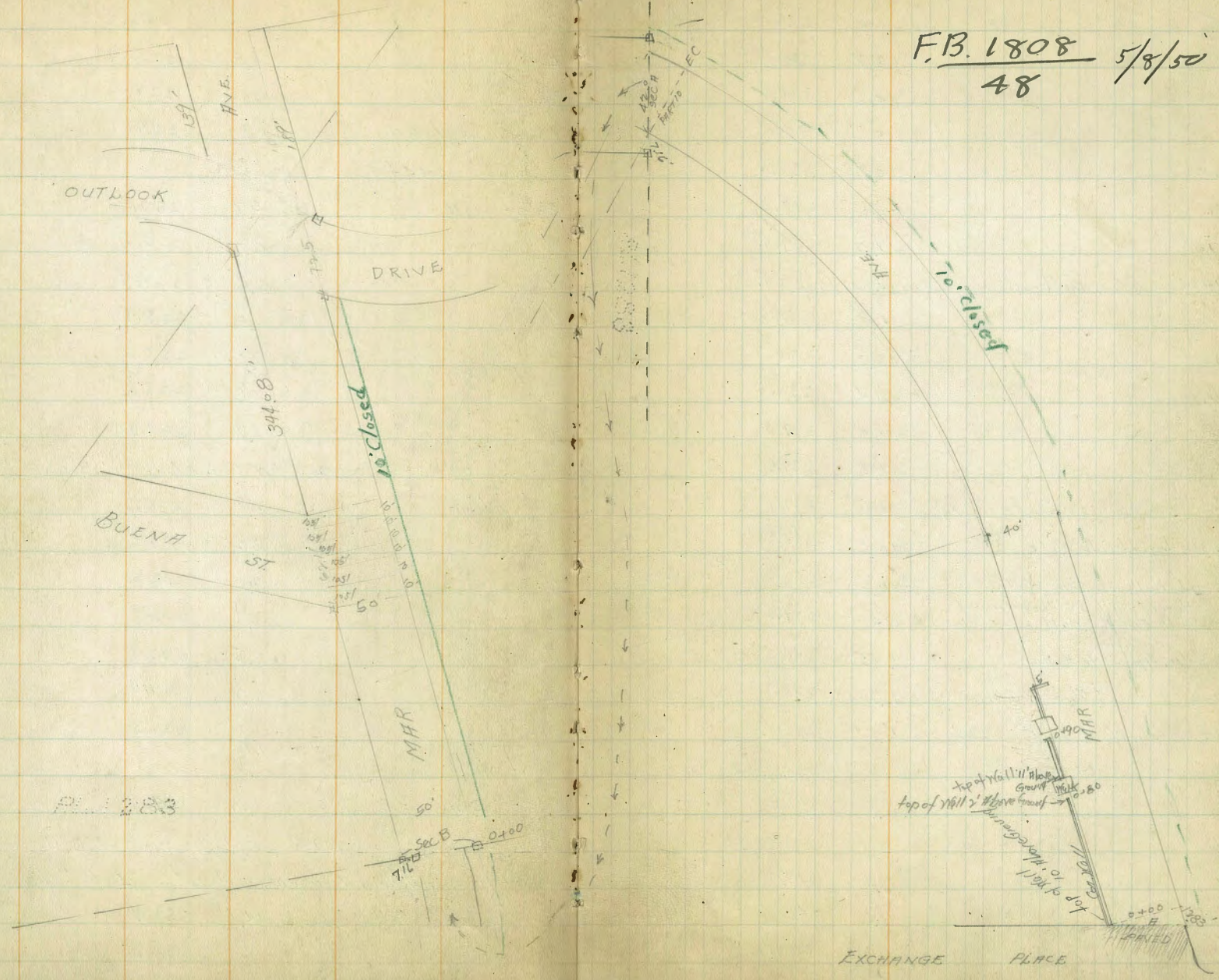
+2 " tree 12.1 234.9

Marker

X. Section MAR Ave. } Cont.  
from Exchange Pl.

48

FB. 1808 5/8/50  
48



FB. 1808

EXCHANGE PLACE



cb.		14.2	244.9	
Y		154	243.7	
+10 = on Back Yard = Terraced		17.2	241.9	
	L+48			
-15 = on Terrace		13.4	245.7	
Y		11.1	248.0	
cb.		8.5	250.6	
$\frac{1}{2}$		5.0	254.1	
$\frac{1}{2}$		5.2	253.9	
$\frac{1}{4}$		5.1	254.0	
cb		0.7	258.4	
E		+0.5	259.6	
TP	12.31	269.89	149	257.58
		L+73.71 = FC. Lt. 38°15'		
E		6.6	263.3	
+3		7.4	262.5	
cb.		10.4	259.5	
$\frac{1}{2}$		12.9	257.0	
$\frac{1}{2}$		13.1	256.8	
$\frac{1}{2}$		13.4	256.5	
cb		18.1	251.8	
Y		20.2	249.7	
+10		21.9	248.0	
+20		25.3	244.6	
	PART 1			
-25		24.8	245.1	

Y		16.5	253.4
cb.		14.0	255.9
$\frac{1}{2}$		10.0	259.9
$\frac{1}{2}$		10.0	259.9
$\frac{1}{2}$		10.1	259.8
+5		9.1	260.8
cb.		6.4	263.5
E		4.9	265.0
	PART 2		
E		0.8	269.1
+3		1.7	268.2
cb		4.4	265.5
+4		7.2	262.7
$\frac{1}{2}$		7.2	262.7
$\frac{1}{2}$		7.4	262.5
$\frac{1}{4}$		7.1	262.8
cb		11.1	258.8
Y		15.7	256.2
+25		21.6	248.3
	PART 3		
-25		6.5	263.4
Y		14.4	258.5
cb.		9.6	260.3
$\frac{1}{2}$		4.9	265.0
$\frac{1}{2}$		5.3	264.6
$\frac{1}{2}$		5.4	264.5

(2) 253.7

269.89

cb.		0.9	269.0
T.P.	11.77	277.05	265.28
+v		4.9	272.2
E		4.8	272.5
PART 4			
E		4.0	273.1
+3		4.7	272.2
cb		7.1	270.0
$\frac{1}{2}$		11.7	265.4
d		11.9	265.2
$\frac{1}{4}$		11.9	265.2
+4		15.9	261.2
cb.		16.5	260.6
W		19.4	257.7
+25		29.5	247.6
PART 5			
-25		31.4	245.7
W		20.5	256.6
cb		18.1	259.0
$\frac{1}{2}$		13.0	264.1
d		12.5	264.6
$\frac{1}{4}$		12.3	264.8
cb.		6.4	270.7
E		4.7	272.4
PART 6			
E		6.1	271.1

277.05

51

+3		7.0	270.1
cb		9.1	268.0
$\frac{1}{2}$		13.5	263.6
d		13.5	263.6
$\frac{1}{4}$		13.7	263.4
cb		18.4	258.7
W		21.2	255.7
+25		32.7	244.4
PART 7			
-25		33.0	244.1
W		23.0	254.1
cb		19.6	257.5
$\frac{1}{4}$		15.3	261.8
d		15.3	261.8
$\frac{1}{2}$		14.3	262.8
cb.		10.6	266.5
E		8.1	269.0
PART 8			
E		8.6	268.5
+v		9.2	267.7
cb		12.1	265.0
$\frac{1}{4}$		16.3	260.8
d		16.3	260.8
$\frac{1}{2}$		16.3	260.8
T.P.	39.2	268.11	264.17
cb		13.5	254.6

W	157	252.4
+25	257	242.4

PART 9

-25	268	241.3
W	159	252.2
cb	125	255.6
$\frac{1}{2}$	89	259.2
$\frac{1}{2}$	88	259.3
$\frac{1}{2}$	84	259.7
cb	40	264.1
E	0.9	267.2

PART 10 = E.C. on EAST

E	3.1	265.0
+2	36	264.5
cb	60	262.0
$\frac{1}{2}$	92	258.9
$\frac{1}{2}$	99	258.2
$\frac{1}{2}$	98	258.3
cb	40	257.0
W	132	254.9
+8	191	248.0

+25	206	241.5
-----	-----	-------

Note: this section will do for Drain  
if needed

Sec # = E.C. on W

Section on Pueblo line  
see sketch

-50	35.8	232.3
-12	22.5	245.6
W	153	252.8

cb	12.1	255.3
$\frac{1}{2}$	10.1	258.0
$\frac{1}{2}$	10.0	258.1
$\frac{1}{2}$	9.2	258.9
cb	67	261.4
+3	67	261.4
E	3.5	264.6

Sec. B = 0+00  $\frac{10.665}{7.5}$  } From Pueblo  
7.5 } to line South

E	0.9	267.2
cb	3.5	264.6
+1	5.6	262.5
$\frac{1}{2}$	8.8	259.3
$\frac{1}{2}$	9.1	259.0
$\frac{1}{2}$	9.5	258.6
cb	11.0	257.1
W	15.5	252.6
+12	22.5	245.6
+35	30.8	237.3
TP 11.64	276.91	284

0+50

-25	30.8	246.1
W	21.8	255.1
cb	16.8	260.1
$\frac{1}{2}$	10.4	260.5
$\frac{1}{2}$	15.8	261.1
$\frac{1}{2}$	11.1	265.8

27691

cb		7.3	267.6	
E		7.0	269.9	
	1400			
E		16	275.3	
cb		4.6	272.3	
$\frac{1}{2}$		6.7	270.2	
+4		7.9	269.0	
$\frac{1}{2}$		10.3	266.4	
$\frac{1}{2}$		11.2	265.7	
+5		11.7	265.5	
cb		12.5	264.4	
W		16.9	260.0	
+25		26.9	250.0	
	1440			
-25		20.7	256.2	
W		12.1	264.8	
cb		7.6	269.3	
+2		6.4	270.5	
$\frac{1}{2}$		6.2	270.7	
$\frac{1}{2}$		5.3	271.6	
+4		1.8	275.1	
TP	1290	288.57	124	275.67
$\frac{1}{2}$			14.1	276.5
cb			9.0	279.6
E			5.8	282.8

1470

28857

53

E		2.3	286.3
cb		5.5	283.1
$\frac{1}{2}$		8.0	280.6
+3		9.1	279.5
$\frac{1}{2}$		13.0	275.6
$\frac{1}{2}$		14.0	274.6
cb		14.5	274.1
W		20.7	268.4
+25		29.2	259.4
	2400		
-25		26.4	262.2
W		16.9	271.7
cb		11.1	277.5
$\frac{1}{2}$		10.8	277.8
$\frac{1}{2}$		9.7	278.9
+4		5.7	282.9
$\frac{1}{2}$		4.6	284.0
cb		2.1	286.5
E		4.0	288.2
TP 774	29537	294	287.63
	2450		
E		3.5	291.9
cb		6.4	289.0
$\frac{1}{2}$		8.8	286.6
+3		9.6	285.8
$\frac{1}{2}$		12.8	282.6



4	13.6	281.8
cb.	14.1	281.3
Y	19.5	275.9
+3.0	22.7	265.7
	3+00	
-3.0	26.6	268.8
Y	16.2	279.2
cb.	11.9	283.5
1/2	11.4	284.0
2	10.3	285.1
+4	7.3	288.1
1/2	6.5	288.9
cb.	4.8	290.6
E	2.8	292.6
	3+50 = N.L. Buena st on E 10' Cb 10' to MAR Ave	
E	4.6	290.8
cb.	6.0	289.7
+15	7.1	288.3
1/2	8.3	287.1
cb.	8.9	286.5
1/2	9.5	285.9
cb.	10.2	285.2
Y	12.7	282.7
+15	17.5	277.9
	N cb.	
-15	17.2	278.2

Y	12.6	282.8
cb.	10.3	285.1
1/2	9.2	286.2
2	8.3	287.1
4	7.7	287.7
cb.	6.8	288.6
E	5.4	290.0
	1/2	
E	5.4	290.0
cb.	5.9	289.5
1/2	7.1	288.3
1/2	8.3	287.1
1/2	9.6	285.8
cb.	10.9	284.5
Y	12.2	283.2
+15	16.1	279.3
	2	
-15	15.8	279.6
Y	12.4	283.0
cb.	10.7	284.7
1/2	9.6	285.8
1/2	8.5	286.9
1/2	7.8	287.6
cb.	7.0	288.4
E	5.6	289.8

E	6.5	288.8
cb	7.6	287.8
$\frac{1}{2}$	8.4	287.0
$\frac{1}{4}$	9.1	286.3
$\frac{1}{4}$	10.0	285.4
cb.	11.0	284.4
Y	12.8	282.6
+15	15.5	279.9

S. cb.

-15	16.0	279.4
Y	13.6	281.8
cb.	11.8	283.6
$\frac{1}{4}$	10.8	284.6
$\frac{1}{4}$	9.8	285.6
$\frac{1}{4}$	9.0	286.4
cb	8.3	287.1
E	7.6	287.8
+10	6.7	288.7

S.L. Buena station East = 0+00

-10	8.5	286.9
E on hub S.W. Cor Buena St	9.24	286.13
cb.	9.7	285.7
$\frac{1}{4}$	10.2	285.2
$\frac{1}{4}$	11.2	284.2
$\frac{1}{4}$	12.3	283.1
cb	13.3	282.1

For future  
check

Y	149	280.5
+15	158	279.6
TP 7.07	307.72	1.72
chk. on B.M. top Hydr. Repit + Buena 0.58		
	0.58	307.18
TP 1.98	291.65	13.11
	0+17	

Grade Book  
110 Page  
23  
307.14  
307.20 = B.M.  
0.06 in Error

307.20 = Above B.M.

289.67

-15 12.5 279.2

Y 14.1 277.6

cb. 13.3 278.4

 $\frac{1}{2}$  12.2 279.5 $\frac{1}{4}$  11.1 280.6 $\frac{1}{4}$  9.9 281.8

cb 9.0 282.7

E 8.4 283.3

+15 8.1 283.6

TP 0.73 279.34 13.02 278.61

0+33

-15 07 278.6

E 07 278.6

cb 10 278.3

 $\frac{1}{4}$  19 277.4 $\frac{1}{4}$  32 276.1 $\frac{1}{4}$  42 275.1

cb 48 274.5

W		54	273.9
+20		60	273.3
	0+48		
-20		76	269.7
W		76	269.7
cb.		89	270.4
$\frac{1}{2}$		80	271.3
$\frac{1}{2}$		80	271.3
$\frac{1}{2}$		77	271.6
cb.		68	272.5
E		63	273.0
+20		47	274.6
T.P.	281 269.26	1289	266.25

0+65

-20		21	267.2
E		26	266.7
cb.		31	266.2
$\frac{1}{2}$		34	265.9
$\frac{1}{2}$		38	265.5
$\frac{1}{2}$		39	265.4
cb.		40	265.3
W		42	265.1
+20		34	265.9

0+97

-25		154	253.9
W		147	254.6

cb.		149	254.4
$\frac{1}{2}$		151	254.2
$\frac{1}{2}$		152	254.1
$\frac{1}{2}$		150	254.3
cb.		151	254.2
E		152	254.1
+25		150	254.3
T.P. 1130	380.42	014	269.12
T.P. 918	289.52	008	280.34
T.P.	328		286.24

SE for  
Eugene  
286.13 on hill  
011

Note: Slope between 0+65 and 0+97 continues approx. the same on West side of St. to 2+20 = Bottom of Canyon and on East the same to Station 1+75 = Bottom of Canyon

X. Section College Ave 80' W 14' C6S  
 From S.W. Prospect to 350' N 13' 1/4 S

College + Prospect 697 194.85 187.88

0+00 = S.W. Aspect

W	47	190.2
cb = top cb	1.82	190.1
Gut	53	189.6
1/4	45	190.7
1/2	38	191.1
3/4	34	191.5
Gut	31	191.8
E top cb	280	192.1
E	27	192.2

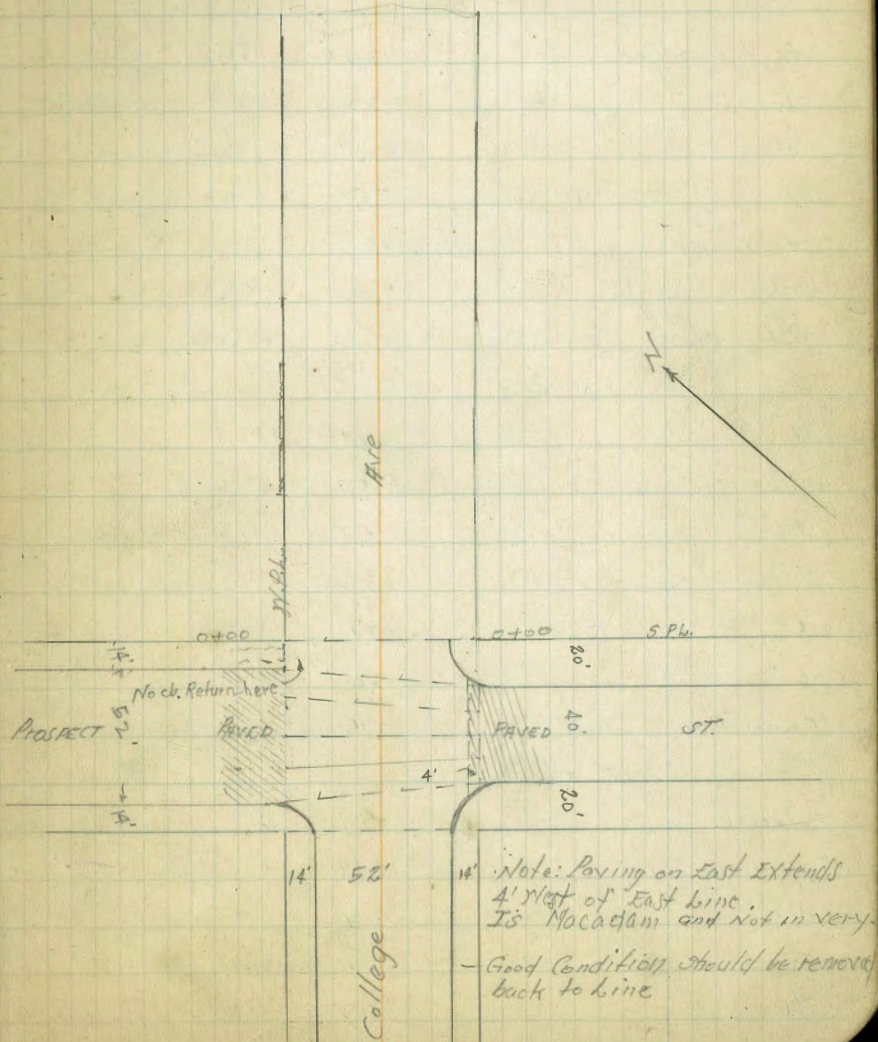
South cb

E on top cb	2.13	192.1
" " Paving	342	191.5
cb	327	191.7
1/4	30	191.9
1/2	33	191.6
3/4	40	190.9
cb on Ground	49	190.8
W Gut on Pav.	569	189.2
W top cb	487	190.0

S 1/4

W on Pav.	576	189.1
cb	48	190.1
1/4	40	190.9

Note: 10" Con. Culvert  
 Constructed by Mr. Helms  
 Prop. owner on W. side of  
 St. Would like for City to  
 connect proposed drainage  
 to 418 S. Also wants st  
 to be improved to station  
 3450 instead of 3400  
 as called for in Petition.  
 SAYS he was out of town when petition was circulated



19485

2	33	191.6
7	26	192.3
cb.	32	191.7
E top Pav.	311	191.8

2

E top of Pav.	327	191.6
cb.	32	191.7
1/4	27	192.2
2	33	191.6
7	42	190.7
cb.	50	189.9
N top Pav.	613	188.8

N 7

N " "	678	188.1
cb.	57	189.2
1/4	47	190.2
2	36	191.3
7	31	191.8
cb.	30	191.9
E on Pav.	374	191.2

N cb.

E top cb.	388	190.0
" Gut on Pav.	419	190.7
cb.	27	191.2
1/4	32	191.7
2	42	190.7

19485

58

7	52	189.7
cb.	62	188.7
N Gut on Pav.	759	187.3
N top cb.	681	188.1

N.L. College = 0400

N	70	187.9
cb on Ground NO RETURN	63	188.6
7	57	189.2
2	51	189.8
7	42	190.7
Gut on Ground	47	190.2
E top cb.	431	190.6
+5 = toe of lawn	43	190.6
E = " "	28	192.1
+0.08 = Beg. Con Wall on W on line	8.5	186.4
+22 = 2 Acacia tree on W 6" dia. 11' inst.		
E on lawn	28	192.1
+9 " " = toe	41	190.8
cb	40	190.9
1/4	52	189.7
2	60	188.9
7	64	188.5
+9	67	188.2
cb.	76	187.3
N on top of Wall	876	186.1
+1	99	185.0
+5	99	185.0

19485

	Dumosa	R = 8.6	186.3	
0+34 =	2 Palm tree on W	15 inst.		15 inst.
0+48 =	" " " " "	R = 9.9	185.0	
	Con.			
" "	on Wall on line	10.13	184.8	
0+69 =	2 Plumosa Palm on W	15 inst.		
- 5		11.2	183.7	
- 4		11.2	183.7	
W	on top of Con Wall	10.75	184.1	
+ 15	at Palm tree	10.4	184.5	
+ 12	" Acacia tree	9.9	185.0	3" dia
cb		9.9	185.0	
+ 6		8.4	186.5	
$\frac{1}{2}$		8.6	186.3	
$\frac{1}{2}$		7.7	187.2	
$\frac{1}{2}$		7.1	187.8	
cb.		6.8	188.1	
E		4.2	190.7	
0+79 =	2 Acacia tree	9.9	185.0	12 inst.
0+76 =	2 Con. Walk on W	11.18	183.7	5' wide on line
	Rejoining			
1+00 =	South End Cobblestone Wall on W	on line		
T.P.	486	189.19	10.52	184.33
W	on top of Wall	3.93	185.3	
W	at Wall on ground	5.7	183.5	
cb		5.8	183.4	
+ 5		4.0	185.2	
$\frac{1}{2}$		4.5	184.7	
$\frac{1}{2}$		3.8	185.4	

18919

59

$\frac{1}{2}$		2.9	185.3	
cb		2.3	186.9	
E		0.1	189.1	
	1+14 =	2 Con Walk on W		
E		1.4	187.8	
cb		2.4	186.8	
$\frac{1}{2}$		3.6	185.6	
$\frac{1}{2}$		4.4	184.8	
$\frac{1}{2}$		5.2	184.0	
+ 6		5.1	184.1	
cb		7.2	182.0	
+ 9 =	top of Wall	6.97	182.3	
W	on " " = Bottom of Wall	6.91	182.3	
		3.2	186.0	1 inst.
1+50 =	South end of cypress hedge on E			with Cobble stone wall underneath
1+57 =	2 Con. Walk on W on line	5' 11" ft		
W =	top of Walk = Bottom of Wall	7.16	180.0	
+ 5 =	" " "	9.16	180.0	
cb		10.0	179.2	
+ 5		6.9	182.3	
$\frac{1}{2}$		6.7	182.5	
$\frac{1}{2}$		6.2	183.0	
$\frac{1}{2}$		5.5	183.7	
cb		4.5	184.7	
+ 13	at Hedge at Wall	3.6	185.4	
	1+85			
E+1	at hedge at Wall	5.1	184.1	

cb.	5.8	183.4
+6	6.0	183.2
+8	7.3	181.9
$\frac{1}{2}$	7.4	181.8
$\frac{1}{2}$	8.5	180.7
$\frac{1}{2}$	9.1	181.1
+7	9.4	179.8
+11	11.8	177.4
cb.	11.3	177.9
W at Wall	11.6	177.6
2+60 = North end Cobble stone wall <sup>top of Wall</sup>	9.57	179.7
" " Ground at Wall	13.7	175.5
2+66 = $\frac{1}{2}$ Con. Walk on E		
-10	16.4	172.8
W	14.8	174.7
cb.	13.1	176.1
+3	13.6	175.6
$\frac{1}{2}$	11.4	177.8
$\frac{1}{2}$	10.7	178.5
$\frac{1}{2}$	9.7	179.5
+5	8.7	180.5
+7	11.7	177.5
cb.	7.3	181.9
E	6.6	182.6
E on top con step	6.3	182.9
+8.5	5.56	183.6

T.P. 013	187.66	6.66	187.53
2+45 = North end of hedge on E	6.2	176.5	
2+51			
E at Wall on ground	7.0	175.7	
cb.	8.1	174.6	
$\frac{1}{2}$	9.7	173.0	
$\frac{1}{2}$	10.2	172.5	
$\frac{1}{2}$	11.8	170.9	
cb.	13.8	168.9	
W	15.3	167.4	
+15	17.0	165.7	
2+80 = North end Cobble stone Wall on E on hill			
T.P. 2.35	173.11	11.90	170.76
-15	11.1	162.0	
W	9.7	163.4	
cb.	8.2	164.9	
$\frac{1}{2}$	6.6	166.5	
$\frac{1}{2}$	5.7	167.4	
$\frac{1}{2}$	4.5	168.6	
cb.	3.0	170.1	
E	1.9	171.2	
E on Wall	+1.0	174.1	
3+00			
-15	4.5	168.6	
E	5.6	167.5	
cb.	5.9	167.2	

$\frac{1}{2}$	6.7	166.9
$\frac{1}{2}$	7.9	165.2
$\frac{1}{2}$	9.4	163.7
cb.	10.7	162.4
W	11.7	161.4
+15	12.2	160.9
3+12 = 2 Acacia tree	12.0	161.1
3+24 = 2 Palm tree	13.1	160.0
3+31		
-15	16.0	157.1
W	15.0	158.1
cb.	13.6	159.5
$\frac{1}{2}$	12.2	160.9
$\frac{1}{2}$	11.1	162.0
$\frac{1}{2}$	9.8	163.3
cb.	10.5	162.6
E	10.4	162.9
+15	10.4	162.9
3+60 = 2 Euc. tree at Pt. A to st.		
-20	18.0	155.1
-3 at tree 3" dia	16.8	156.3
E	16.8	156.3
cb.	16.9	156.2
+5 at tree 3" dia.	17.1	156.0
$\frac{1}{2}$	16.0	157.1
$\frac{1}{2}$		

13' inst

13' inst

$\frac{1}{2}$	16.1	157.0
+2 at tree 2" dia	16.1	157.0
$\frac{1}{2}$	16.5	156.4
cb.	16.5	156.6
+2 at Acacia 5" dia	16.5	156.6
W	18.0	155.1
+70	19.7	153.4
3+74 on Con. Basin 5' East of Xcb. line		
T.P. 1258	18501 0.68	171.43
T.P. 943	19404 0.20	184.31
T.P. = chf. on B.M.	618	187.86

R = 14.5

3+74 on Con. Basin 5' East of Xcb. line

See note  
on page  
57187.86  
187.86 - 57  
0.07



Tolman

X section of Landis St 63.7 Street  
Euclid to Alley on north 40' roadway

5.18	345.86	340.68	BP NW Euclid Univ.
5.28	346.23	340.55	
6.60	346.55	339.95	
6.37	349.95	343.58	

this should be → 348.95

W. L. Euclid = 0+50

N cb	4.69	437.26
N gut	5.02	438.93
£	5.36	438.59
S gut	5.87	438.08
S cb	5.49	438.46

= 0+50 =

N L	4.5	445
cb	4.5	445
1/4	4.4	446
£	4.5	445
1/4	4.7	443
cb	5.3	437
SL	5.2	437

= 0+50 =

SL	5.9	431
cb	6.0	430
1/4	5.2	438

£	49.95	5.1	439
1/4	50.0	5.4	436
cb		5.5	435
NL		4.9	441

= 0+5 =

NL		5.2	438
cb		5.5	435
1/4		5.7	433
£		5.5	435
1/4		5.5	435
cb		6.5	425
SL		6.4	426

= 1+00 =

SL		6.7	423
cb		6.6	424
1/4		6.1	429
£		6.1	429
1/4		6.2	428
cb		6.2	428
NL		5.8	432

1+24.5 = E. L. Alley

NL		5.9	431
cb		6.4	426
1/4		7.1	41.9

349.95

63

k	50.0	6.7	423
1/4		6.8	422
cb		7.0	420
3L		7.0	420

Cb ret. on W. side Alley

N.cb		7.15	41.0
N.P.L		6.97	41.98

TP		6.78	342.17
----	--	------	--------

"	2.05	344.22	
---	------	--------	--

"		4.48	339.74
---	--	------	--------

"	5.18	344.92	
---	------	--------	--

"		6.01	338.91
---	--	------	--------

"	4.91	348.82	
---	------	--------	--

"		4.13	339.09 - 340.08
---	--	------	-----------------

Marker  
for  
S. Torrey  
9-28-27

X Section HIGH 57.50' wide 14' class  
13.75  
from Sh. Torrey Rd. to N.H. College

12.37

64

J.V. Spk.			
Torrey Exchange	0.95	166.80	165.85
T.P.	0.05	154.08	127.77
T.P.	0.58	141.97	126.9
T.P.	1.36	131.63	117.0
T.P.	6.14	128.37	94.0
S.H. Torrey = 0400			
W top cb.		8.3	120.1
W top cb.		8.38	120.0
W Gut. on par.		8.97	119.5
1/4 " "		8.05	120.3
1/2 " "		7.37	121.1
1/4 " "		6.96	121.0
Gut " "		6.89	121.5
E top cb		6.41	122.0
E		4.8	123.6
0+06			
E		4.1	124.3
+8		3.6	124.8
cb.		5.5	122.9
1/4		6.4	122.0
1/2		7.1	121.3
1/4		9.9	120.5
cb		8.3	120.1
W		10.4	118.0
+10		11.0	119.4

0+25			
-10		11.3	117.1
X		10.3	118.1
cb		9.0	119.4
1/2		7.0	121.4
1/2		5.9	122.5
1/4		5.1	123.3
cb		4.0	124.4
E		3.7	124.7
0+60			
E		4.3	124.1
cb.		5.1	123.3
1/2		5.0	123.4
1/2		6.2	122.2
1/4		6.7	122.2
cb.		8.9	119.5
W		10.8	119.6
+10		11.2	119.2
0+82			
-10		11.1	117.3
W		10.6	117.8
cb.		10.1	118.3
1/4		8.5	119.9
1/2		7.9	120.5
1/2		6.2	122.2
cb.		6.6	121.8

12837

E	4.0	124.0
1400		
E	3.6	124.8
+6	5.6	122.8
cb.	6.4	122.0
$\frac{1}{2}$	7.2	121.2
$\frac{1}{2}$	7.9	120.5
$\frac{1}{2}$	8.7	119.7
cb.	9.4	119.0
W	10.3	118.1
+10	10.9	117.5
1410		
-10	10.7	117.7
W	10.1	118.3
cb.	9.3	119.1
$\frac{1}{2}$	8.4	120.0
$\frac{1}{2}$	7.7	120.7
$\frac{1}{2}$	6.9	121.5
cb	6.2	122.2
E	5.0	123.4
+10	4.3	124.1
1450 = $\frac{1}{2}$ Alley		
-100'	+1.6	130.0
-75'	+0.7	128.6
-50'	-1.6	126.8
-25'	3.0	125.4

12837

65

E	4.0	124.4
cb	4.7	123.7
$\frac{1}{2}$	5.0	123.4
$\frac{1}{2}$	5.3	123.1
$\frac{1}{2}$	6.4	122.0
cb	7.4	121.0
W	8.5	119.9
+25	10.7	117.7
+50	12.3	116.1
+58 = $\frac{1}{2}$ Garage on N.W. Alley	12.7	115.7
+75	13.9	114.5
+100'	14.9	113.5
1400		
-10	8.9	119.5
W	8.3	120.1
cb	7.3	121.1
$\frac{1}{2}$	6.5	121.9
$\frac{1}{2}$	5.6	122.8
$\frac{1}{2}$	5.3	123.1
cb	4.8	123.6
E	3.5	124.9
+10	3.0	125.4
1430		
-10	2.4	126.0
E	2.1	125.7
cb	3.3	124.9

and dirt floor

128.37

z		4.3	124.1	
z		4.8	123.6	
z		5.3	123.1	
cb		6.0	122.4	
W		7.0	121.9	
+10		7.6	120.8	
	2+70			
-10		4.7	122.7	
W		3.5	124.9	
cb		2.7	125.7	
z		1.8	126.6	
z		0.8	127.6	
T.P.	11.17	138.71	0.83	127.54
z		10.3	128.4	
cb		10.0	128.9	
E		10.1	128.6	
+10		9.9	128.8	
	2+80			
-5		8.6	130.1	
E		8.6	130.1	
cb		9.5	129.2	
z		8.9	129.8	
z		9.5	129.2	
z		10.6	128.1	
cb		12.5	126.2	
W		13.2	125.5	

138.71

66

+10		13.1	125.6
	3+10 = N.L. College		
W		12.0	128.9
cb		12.0	128.7
z		9.6	129.1
z		8.9	129.8
z		8.3	130.4
cb		7.5	131.2
E		7.0	131.7

TP	11.78	150.43	0.06	138.65
TP	10.54	160.93	0.04	150.39
TP	11.35	163.32	0.96	151.97
TP	10.08	168.88	4.52	158.80

chk. on B.M. SpK. Exchange + Tariff R. 305

165.83  
 155.85 = BM  
 0.02 = Error

Sewer Levels 2' E. of line Bet Lts 17+18  
 BIK 5. Loma Alta #1

11-1-27  
 Miller

36

For Plat See Page 36.

67

BM	13.13	85.55		72.42	SE. Yellow & San Joaquin Co
T.P.	1.27	86.73	0.09	85.46	
0+00 to 0+00 Page 36			7.0	79.7 = 79.7	
0+10			7.9	78.8	
0+50: $\phi$ Alley $\Delta$ 90° 00' L.			17.5	69.2	2' E. of E. line of lot 18
0+75		✓	11.8	74.9	
T.P.	12.62	93.77	5.58	81.15	
0+95			10.9	82.9 ✓	
1+05			6.5	87.3 ✓	
1+60		✓	1.4	92.4 ✓	
T.P.	11.33	104.95	0.15	93.62	
1+90: N. line Udal			8.5	96.4 ✓	
2+00 to 2+00 Page 36: $\phi$ Udal			7.2	97.7 ✓	
ch Koh Sta 2+12 Page 36			5.9	99.0 = 99.0	

X-Section Alley Bl. G - S.D.L. & T's S. Chollas  
 Detw. National & Newton from 35<sup>th</sup> to 36<sup>th</sup> ✓

STA.	+	H.I.	-	Elev.
				36.33 N.G. should be 36.98
	11.59	48.57 47.92		
T.P.			0.41	48.16 47.51
	6.54	54.70 54.05		
B.M.			3.98	50.72 50.07
T.P.			12.34	41.71
	1.08	43.44 42.79		
0+00				
N.L.			4.60	38.84
⊕			5.18	38.26
S.L.			5.07	38.37
0+15				
S.L.			3.05	40.39
⊕			3.20	40.24
N.L.			2.70	40.74
0+40				
+1.30 North of N.L.			2.70	40.74
N.L.			2.70	40.74
⊕			2.80	40.64
S.L.			3.30	40.14
0+67				
+5.0 South of S.L.			2.40	41.04
S.L.			2.70	40.74
⊕			2.60	40.84
N.L.			2.10	41.34

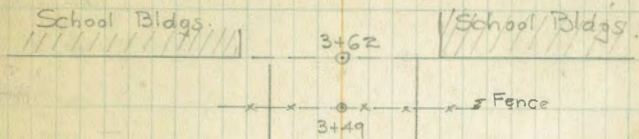
see page 71  
 for CB x sec on 35<sup>th</sup>

Plotted 5/17/28  
 T.G.H.  
 Garage 5/2/28  
 T.G.H.

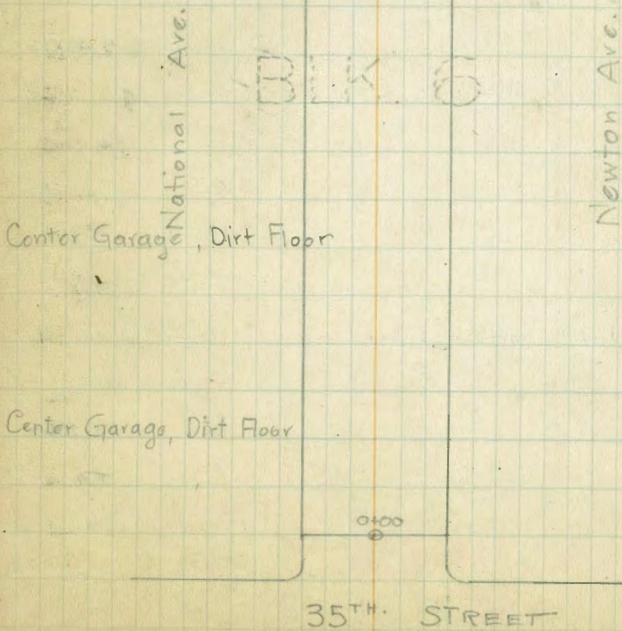
JAEGER }  
 Bailey }  
 Clavey } May 7<sup>th</sup> 1928

CS

B.M. Br. Pl. SE. Cor. 36<sup>th</sup> & National



E.L. 35<sup>th</sup> ST.



43.44

STA.		+	H.I.	-	Elev.
0+85			<del>42.79</del>		
	+1.0	North of N.L.		1.30	42.14
	N.L.			1.60	41.84
	¢			2.00	41.44
	S.L.			2.00	41.44
0+93					
	S.L.			1.80	41.64
	¢			1.60	41.84
	N.L.			1.10	42.34
	+1.0	North of N.L.		0.90	42.54
1+05					
	+1.30	North of N.L.		0.55	42.89
	N.L.			0.75	42.69
	¢			1.10	42.34
	S.L.			1.50	41.94
	T.P.			0.82	42.62
		10.18	52.80		
			52.15		
1+17					
	S.L.			10.50	42.3
	¢			10.10	42.7
	N.L.			9.80	43.0
	Concr. Floor Garage	+1.30		9.30	43.5
1+40					
				8.0	44.8
	N.L.			8.6	44.2
	¢			9.10	43.7
	S.L.			9.70	43.1

Center Garage, Dirt Floor

Center Garage, Dirt Floor

" " Cement Floor

4' north of N.L. Alley & Garage, Dirt Floor



5280

Sta		H.I.	-	Elev.
1+93		<del>52.15</del>		
	S.L.		7.5	45.3
	¢		7.2	45.6
	N.L.		6.6	46.2
2+43	+4.0 North of N.L.		5.10	47.70
	N.L.		5.10	47.7
	¢		5.50	47.3
	S.L.		5.80	47.0
2+61				
	S.L.		5.20	47.6
	¢		4.70	48.1
	N.L.		4.20	48.6
3+05				
	¢		3.40	49.40
	S.L.		3.30	49.50
	+2.5' South of S.L.		3.50	49.30
3+10				
	S.L.		3.10	49.7
	¢		3.20	49.6
	N.L.		3.40	49.4
3+49	+7.0 North of N.L.		2.92	49.88
	N.L.		2.0	50.8
	¢		2.4	50.6
	S.L.		2.4	50.6
3+62				
	¢		2.0	50.8

Center Garage Concrete Floor (on Property Line)

" " Dirt Floor

Center Garage Concrete Floor

" " Dirt Floor

Concrete Apron of Garage  
Garage Floor  
Fence Line



X-Section Alleys - Block 20 - L.W. Kinkalls ✓  
 betw. J. & K - 25th and 26th

STA.	+	H.I.	-	Elev.
	5.22	105.09		<u>93.87</u>
			11.25	93.84
	1.30	95.14		
0+00				
E.L.			0.77	94.3
φ			0.96	94.2
W.L.			0.22	94.9
0+25				
W.L.			3.0	92.1
φ			3.2	91.9
E.L.			3.0	92.1
0+50				
+32	East of E.L.		5.70	
E.L.			4.27	90.9
φ			4.30	90.8
W.L.			4.20	90.9
0+75				
W.L.			5.30	89.8
φ			5.30	89.8
E.L.			5.33	89.8
1+00				
E.L.			6.13	89.0
φ			6.20	88.9
W.L.			6.20	88.9

SE. Cor. 25th & J. Brass Plug

Use this B.M. and change  
 T.P.s & H.I. (Done!)

⑤ N.L. "J" Street

On Concrete

" "

" "

On Cement Walk

Garage, Dirt Floor

On " "

On Cement Walk

" "

Plotted 5/17/28  
 T.G.H.  
 yardage 9-27-28  
 T.G.H.

STA.	+	H.I.	-	Elev.	
1+14		95.14			
W.L.			6.9	88.2	Garage, Dirt Floor (On Prop. Line)
⊕			6.5	88.6	
E.L.			6.72	88.4	On Cement Walk
1+18					
+34			8.05	87.1	Garage, Dirt Floor
E.L.			6.75	88.4	On Cement Walk
⊕			6.60	88.5	
W.L.			7.00	88.1	
1+43					
W.L.			7.60	87.5	Garage, Dirt Floor (On Property Line)
⊕			7.70	87.4	
E.L.			7.40	87.7	On Cement Walk, Termination of Walk
1+50 <sup>35</sup>					N.L. of Alley running E & W
E.L.			8.0	87.1	
⊕			7.85	87.3	
W.L.			7.60	87.5	
1+60 <sup>35</sup>	North Side				⊕ " " E. & W.
W.L.	Garage, Dirt Floor, On Property Line		7.80	87.3	
⊕			8.20	86.9	
E.L.			8.40	86.7	
1+70 <sup>35</sup>	South Side				S.L. " " E. & W.
E.L.	Garage, Dirt Floor, On Property Line		8.80	86.3	
⊕			8.80	86.3	
W.L.			8.40	86.7	

STA.	+	H.L.	-	Elev.
1+9v		95.14		
+3'	West of W.L.		9.10	
W.L.			9.20	85.9
φ			9.40	85.7
E.L.			9.30	85.8
	T.P.		8.16	86.98
	1.57	88.55		

Garage with Dirt Floor

5.26  
 4.96  
 .30

2+17				
E.L.			3.90	84.7
φ			3.80	84.8
W.L.			3.60	85.0
2+50	+12' West of W.L.		3.50	85.1
W.L.			4.20	84.4
φ			5.30	83.3
E.L.			5.00	83.6

Garage Dirt Floor

2+75				
E.L.			5.9	82.7
φ			6.0	82.6
W.L.			5.2	83.4
3+00				
W.L.			5.7	82.9
φ			5.8	82.8
E.L.			7.1	81.5

STA.	+	H.I.	-	Elev.
3+10 <sup>60</sup>		88.55		
E.L.			9.61	79.0
ϕ			10.04	78.5
W.L.			9.86	78.7

N.L. "K" Street  
 Concrete Pavement  
 " " " " " "

Alley between K & J. running E & W

0+00	= 1+60 <sup>35</sup>			86.98
	9.80	96.78		

Intersection of ϕ Alley N&S and ϕ Alley E&W

0+25				
N.L.			10.0	86.8
ϕ			10.6	86.2
S.L.			10.0	86.8

0+41				
S.L.			10.6	86.2
ϕ			10.4	86.4
+7'			8.74	88.1
N.L.			10.10	86.7

Top of M.H. on Drainage

0+75				
N.L.			10.40	86.4
ϕ			10.40	86.4
S.L.			11.60	85.2

STA.	+	H.I.	-	Elev.
1+04		9628		
+0.9	South of S.L.		9.9	
S.L.			9.9	86.9
ϕ			10.0	86.8
N.L.			9.9	86.9
1+19				
N.L.			9.4	87.4
ϕ			9.5	87.3
S.L.			9.8	87.0
+1.30	South of S.L.		9.94	
1+34				
+1.50	South of S.L.		9.18	87.6
S.L.			9.0	87.8
ϕ			8.5	88.3
N.L.			8.3	88.5
1+43				
N.L.			7.5	89.3
ϕ			7.5	89.3
S.L.			9.4	87.4
+1.50	South of S.L.		9.4	
1+54				
+1.50	South of S.L.		8.05	
S.L.			8.0	88.8
ϕ			6.2	90.6
N.L.			6.1	90.7
1+75				
N.L.			4.1	92.7
ϕ			3.5	93.3
S.L.			3.2	93.6

Garage, Dirt Floor

Garage, Cement Floor

" " "

" Cement Floor

" " "

4.36  
368  
 .68  
8.50  
 9.18

4.30  
2.80  
 1.50

1.35  
3.20  
 1.85  
6.20  
 8.05

STA.	+	H.I.	-	Elev.
1+93		9678		
S.L.			2.20	946
ϕ			2.30	945
N.L.			2.60	942
2+03				
N.L.			1.10	957
ϕ			1.30	955
S.L.			0.60	962
+1.60 South of S.L. T.P.			0.50	9628
			0.93	95.85
	12.70	108.55		
2+16				9965
+9.10 North of N.L.			10.9	
N.L.			11.0	976
ϕ			12.5	961
S.L.			12.5	96.1
+1.3 South of S.L.			12.5	
2+52				
S.L.			9.8	988
ϕ			10.0	986
N.L.			7.4	1012
+8.8 North of N.L.			7.3	
2+75				
N.L.			7.3	1013
ϕ			8.4	1002
S.L.			8.1	1005

9765  
18  
 9945  
32  
 9625

Garage, Board Floor (on Property Line)

7.10  
6.30  
 .80

" " "

6.50  
4.80  
 1.60

" Concrete Floor

8.10  
5.40  
 2.70  
10.00  
 7.30

" Board "

ϕ Concrete Run-ways, Beginning of  
 ϕ " Floor



STA.	+	H.I.	-	Elev.
2+99		108.05		
S.L.			6.6	102.0
⊕			6.5	102.1
N.L.			5.0	103.6
+9.5'	North of N.L.		3.1	
3+20			3.1	
+5.20'	North of N.L.		3.2	105.4
N.L.				
⊕			4.8	103.8
S.L.			5.8	102.8
+2.2'	South of S.L.		5.5	
3+50				
S.L.			3.3	105.3
⊕			2.1	106.5
N.L.			1.0	107.6
T.P.	6.67	115.18	0.04	108.51
3+75				
N.L.			4.6	110.6
⊕			6.2	109.0
S.L.			8.8	106.4
4+09 <sup>02</sup>				
S.L.			4.37	110.8
⊕			3.91	111.3
N.L.			1.71	113.5
T.P.			11.86	103.32
	0.16	103.48		
T.P.			12.75	90.73
	3.50	94.23		
			7.41	86.82

Beginning of Concr. Drive Way  
Garage Concr. Floor

" " "

" Dirt "

W.L. 26<sup>TH</sup>. Street

On Concrete

" "

" "

86.86 S.W. Cor 26<sup>TH</sup> & K " Brass Plug

4+09 End of Curb Return.

3+92 Concrete Walk 106.7  
on south

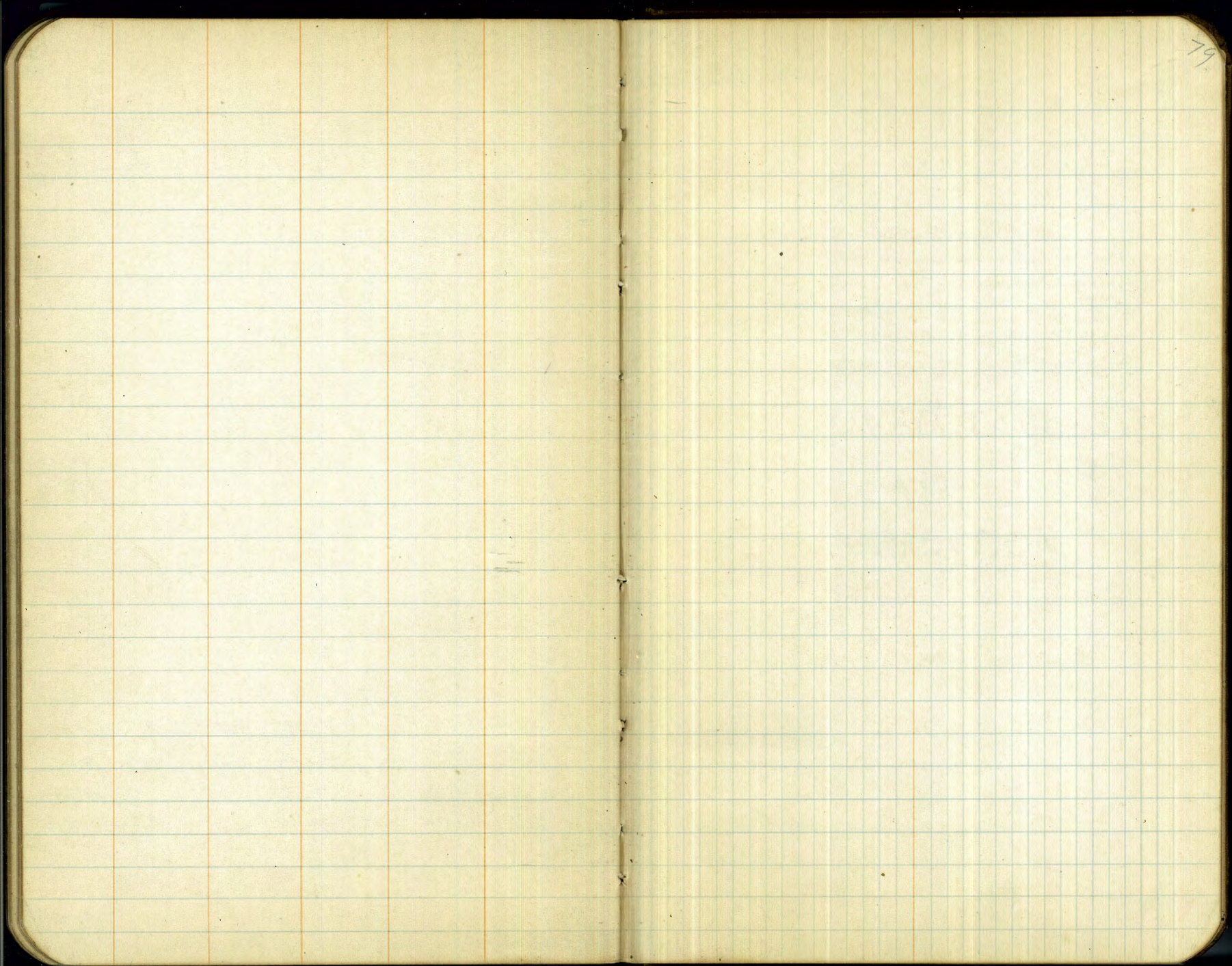
3+59 ✓ ✓ 105.4

3+49 ✓ ✓ 105.0

0.09  
1.12  
1.21

78





6.50  
5.12  

---

1.40

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/2 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column is the distance from side stake to slope stake. If ground is not

**IMPROVED TABLES  
AND  
INFORMATION**

TABLE No. 2.

To find tangent and external for curve of any other degree, divide by degree of curve and add connection found in column of connections. Degree of curve with a given  $L$  may be found by dividing tangent (or external), opposite  $L$  by given tangent (or external). The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

194  
1156  
1350

35  
16  
17  
8.5

185.41  
1.50  
178.87

203.40 = BM. Mor + Exchange = NW Spk. in 206  
115.17 = " Exchange at Prospect - NE Cor. Flush with Walk  
Near Prop. Co. Mor. B.P.

177.07  
12.69  
164.38  
3.24  
167.62

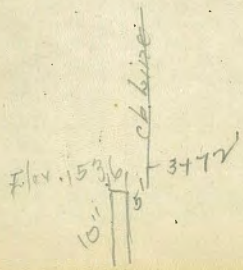
71300	350	225	350
-412.11	62.11	32.08	62.11
306.89	117.11	87	225
-125		32.08	32.08
373.79		300.89	87
189		44.19	756.19
56.5			71300
			43.19

0460 = 25  
785 = 92

19.5 = Rod on Drain  
3472 on Web line

42.79  
6.82  
41.97

52.15  
1.91  
50.24



72.44  
712  
79.55  
1.73  
77.82  
43.1  
84.12  
70.3  
79.70  
12.82  
96.52  
182  
190.70  
11.17  
101.87  
101.82  
36  
102.18  
10.81  
92.37

25  
0.6  
24.9  
16.5  
8.4

340.68  
5.18  
345.86  
5.31  
340.55  
5.28  
345.83  
6.25  
397.95  
6.60  
346.55  
2.97  
343.58  
6.37  
1536.1795

40.52  
40.68  
4.14

12.5  
797

Polonia

397  
1986

1.18  
66  
City Hqts  
S.L.

35  
18  
17

19390  
460  
20350  
1460  
19082  
206  
19289  
753  
18505  
249  
18745  
14.75  
74.77  
7.22  
182.1  
6.54  
177.57  
12  
179.29  
302  
176.27  
124  
168.76  
33  
185.46

300  
20  
20  
1300  
170.1

College  
17311  
5068  
17213

Mr. Helm

17243  
+1238  
18501 = T  
0.20  
18481 = TP  
+9.23  
19404 = T  
6.18  
187.867  
185.43