1185

ZIZIC

FIELD BOOK

No. 385

INDEX

3/15/15. Moore

Cross Section of Woolman to Imperial

47+45 60 wide 10 cts

Woolman 47+45

Switchito	40+00	1+00 N		1+85.6
	N.L. Woolman = 0+00			
W			4.4	
CL			3.3	
1/4			3.8	
C			2.9	
1/4			2.8	
CL			1.5	
E			1.0	
	0+00 N			
E			1.0	
CL			1.6	
+4			2.4	
1/4			2.7	
C			2.9	
1/4			3.4	
+5			3.6	
CL			2.6	
W			2.8	
	0+50 N			
W			4.0	
CL			3.1	
1/4			2.8	
+5			4.9	
C			4.9	
1/4			5.4	

1+24.5.8

+5	3.8
CL	3.3
E	2.9
0+75	
E	4.5
CL	5.7
+3	7.0
1/4	6.8
C	7.4
+6	7.4
+8	6.3
1/4	6.3
CL	6.7
W	7.0
1+00	
W	8.7
CL	8.4
1/4	8.4
+4	8.0
+5	8.7
C	8.5
1/4	8.5
+8	8.6
CL	7.7
E	7.1

		1+75.8			
	1+75				
E			8.5		
cb			9.2		
+2	1		10.5		
1/4			9.9		
C			10.1		
+5			10.3		
+7			8.8		
1/4			8.5		
cb			8.5		
W			9.7		
T.P.	3+7.	114.19	1166	110.92	
	1+50				
W			5.2		
cb			5.2		
1/4			4.3		
C			3.8		
1/4			3.6		
+6			4.5		
cb			2.9		
E			2.4		
	2+00				
E			4.5		
cb			5.3		
1/4			6.4		
C			6.7		

114.19 47+45

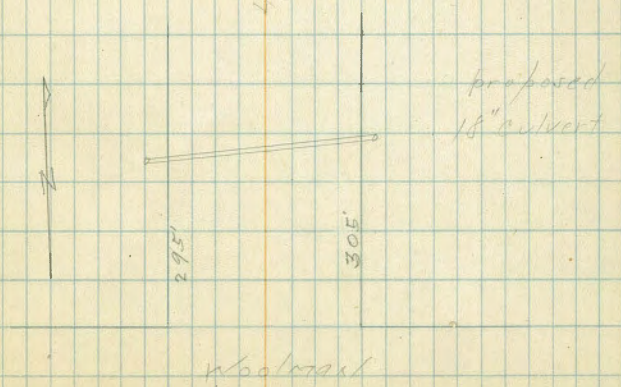
1/4	7.7
cb	8.4
W	8.7
2+50	
W	8.1
cb	6.9
+8	6.7
1/4	7.5
C	7.7
1/4	7.6
cb	6.9
E	6.6

Culvert Levels #1 Culvert

S'E of E 47+50 = 00 7.6

E of " 8.2

S'W of W " 10.9



	3+00		
W			10.1
CB			9.7
1/4			8.9
C			8.3
1/4			7.8
CB			7.7
E			7.7
	3+50		
E			6.9
CB			7.3
1/4			7.7
C			7.9
1/4			8.2
CB			8.2
W			8.2
	4+00		
W			7.5
CB			7.5
1/4			7.5
C			7.2
1/4			7.0
CB			6.2
E			5.7
	4+50		
E			5.0

CB		5.1
1/4		6.0
C		6.3
1/4		6.7
CB		7.0
W		7.2
	5+00	
W		7.0
CB		6.7
1/4		6.1
C		5.4
1/4		5.6
CB		5.2
E		4.8
	5+50	
E		4.9
CB		5.0
1/4		5.3
C		5.7
1/4		5.7
CB		6.0
W		6.1

6+05.8 = 8.2 Frankford West - Sec A

W		4.3
CB		4.2
114		4.4

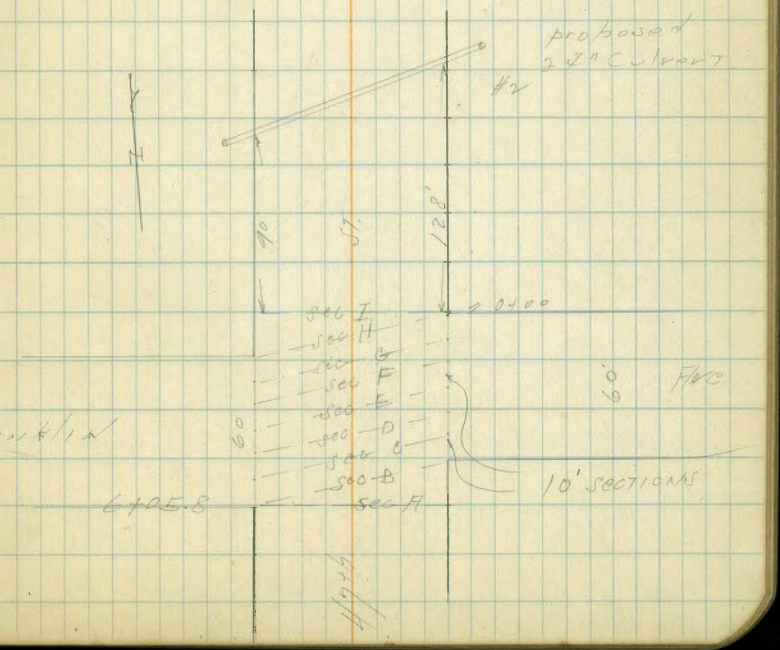
11/4/19

C		5.0
1/4		4.7
cb		3.8
E		3.6
	6+11 = St Franklin EAST = Sec B	
E		3.5
cb		4.1
1/4		4.6
C		5.0
1/4		4.6
cb		4.1
W		4.2
	St cb = Sec C	
W		4.2
cb		3.9
1/4		4.2
C		4.8
1/4		4.8
cb		4.2
E		3.6
	St 1/4 = Sec D	
E		4.1
cb		4.5
1/4		4.5
C		4.7
1/4		4.6

11/4/19

45-45

cb	4.8
W	5.1
	E = Sec E
W	4.9
cb	4.7
1/4	4.7
C	4.4
1/4	4.3
cb	4.1
E	4.0



1/4/19

Sec F = N 4

E	3.8
C6	4.2
1/4	4.3
C	4.4
1/4	4.4
C6	4.7
W	5.1

Sec G = N C6

N	3.4
C6	3.1
1/4	2.8
+2	2.8
+4	4.5
C	4.5
1/4	4.3
C6	3.5
E	2.9

Sec H = NE angle

E	3.0
C6	3.0
+2	3.9
1/4	4.4
C	4.5
+5	4.8
+8	3.4

1/4/19

1/4	3.3
C6	3.3
W	3.3

Sec I = 0+00 NL FRONTING to EAST

N	3.2
C6	3.2
1/4	3.4
+2	3.6
+4	4.7
C	4.6
1/4	4.4
+8	4.1
C6	3.0
E	3.0
T.P. 6.30	116.16 4.23 109.96
0+30	
E	5.6
C6	6.4
1/4	6.5
C	6.7
+5	6.9
1/4	4.7
C6	5.2
W	6.2
0+50	~~11~~
W	9.1

11626

CL	8.4
1/4	7.0
C	7.0
1/4	6.8
CL	6.4
E	5.9
0+75	
E	6.6
CL	7.1
1/4	7.2
C	7.3
1/4	8.3
CL	10.6
W	11.4
+5	11.5
1+00	
-5	10.5
W	10.5
CL	10.9
1/4	10.6
+5	7.3
C	7.6
1/4	7.6
CL	7.6
E	7.5

Levels for Culvert #2

0+00 = SURFACE	9.4
0+15	8.1
0+25	7.7
0+45	7.9
0+48	10.0
0+77	11.0
1+30	
-5	9.2
E	8.8
CL	8.4
1/4	7.2
C	7.7
1/4	9.3
CL	8.9
W	7.8
+5	7.4
1+50	
W	6.8
CL	7.9
1/4	7.9
C	7.8
1/4	7.4
CL	7.8
E	7.7
+5	8.2

116.26

2+00

E 6.1
cb 6.4
1/4 6.8
C 6.9
1/4 7.2
cb 6.7
W 5.7

2+50

W 6.6
cb 7.0
1/4 6.5
C 5.9
1/4 5.9
cb 5.5
E 5.6

3+00

E 4.6
cb 5.1
1/4 5.0
C 5.1
1/4 5.1
cb 4.9
W 4.8

3+50

W 3.9

116.26 4745 7

cb 3.9
1/4 4.0
C 4.2
1/4 4.0
cb 4.1
E 4.0

4+00

E 3.5
cb 4.0
1/4 3.9
C 3.8
1/4 3.6
cb 3.5
W 3.6

4+50

W 3.5
cb 3.8
1/4 3.7
C 3.7
1/4 3.5
cb 3.8
E 3.6

5+00

E 3.0
cb 3.7
1/4 3.5

11626

C 3.7
1/4 4.4
ob 4.3
W 4.0

5+50

W 5.2
ob 5.5
1/4 4.4
C 3.6
1/4 3.6
+5 2.6
+7 2.4
ob 2.3
E 2.7

6+00 = 5L 1 interval = 6' wide 10' ob

E 2.5
ob 3.1
1/4 3.7
C 3.6
1/4 4.2
ob 4.2
W 5.1

5 ob

W 4.8
ob 4.4
1/4 4.2

11626

47+4

8

E 3.7
1/4 3.8
ob 3.7
E 3.3

22' N of 5L interval = 5 edge 18' wide paving

E 5 edge of paving 3.20
C " " " 4.3 1119
W " " " 5.33

11626

11503
9 5 4
1 3.6 2
5 0 7
116.5 5 = 116.5 6 0.0
5 0 0

11 5 4
11 1.9
3.5

3/15/27 Cross Section of 80' wide
Moore Narragansett = 20' curbs
10' 1/4's
Ebens to Santa Barbara

SW Leading Corbak	191	7238	7047	Point Ebens	
W/ Ebens = 60' wide in curbs 9' 1/4's					
S			11.0	61.4	
cb			12.0	60.4	
1/4			12.3	60.1	
C			12.4	60.0	
1/4			12.8	59.6	
cb			12.2	60.2	
N			12.7	59.7	
W curb					
N			12.2	60.2	
cb			11.6	60.8	
1/4			12.4	60.0	
C			11.8	60.6	
1/4			11.7	60.7	
cb			11.4	61.0	
S			11.2	61.2	
W 1/4					
S			11.2	61.2	
cb			11.2	61.2	
1/4			11.1	61.3	
C			11.7	60.7	
1/4			12.0	60.4	
cb			11.4	61.0	
N			11.8	60.6	

Plotted by Tolman 3/19/27

℄

1	11.7	60.7
cb	11.6	60.8
1/4	11.4	61.0
C	11.4	61.0
1/4	11.5	60.7
cb	10.9	61.5
S	10.6	61.8
E 1/4		
S	9.9	61.5
cb	9.9	61.5
1/4	11.0	61.4
C	10.7	61.7
1/4	10.5	61.9
cb	11.4	61.0
N	10.8	61.6
E curb		
N	9.1	63.3
1+10	8.8	63.6
cb	10.7	61.7
1/4	9.4	63.0
C	9.6	62.8
1/4	10.2	62.2
cb	9.4	63.0
S	9.1	63.3

7238

7v4

ELEBERS=00

√	8.0	64.4	✓
c6	8.9	63.5	✓
+v	7.7	64.7	✓
1/4	7.8	64.6	✓
c	8.7	63.7	✓
1/4	8.5	63.9	✓
c6	10.5	61.9	✓
+7	9.1	63.3	✓
+9	6.8	65.4	✓
√	7.3	65.1	✓
0+25			
√	3.4	69.0	✓
+17	3.0	69.4	✓
+1v	7.1	65.3	✓
c6	9.4	63.0	✓
+v	9.0	63.4	✓
+3	6.v	66.v	✓
1/4	5.4	67.0	✓
+5	5.8	66.6	✓
+7	6.8	65.6	✓
c	5.5	66.9	✓
+3	4.3	68.1	✓
1/4	4.4	68.0	✓
+4	4.6	67.8	✓
+5	7.6	64.8	✓

7238 Narragansett 10

7v4

c6	7.4	65.0	✓
+5	7.6	64.8	✓
+8	5.6	66.8	✓
+11	4.8	67.6	✓
5	5v	67.4	✓
0+50			
5	3.0	69.4	✓
+10	2.6	69.8	✓
+12	5.8	66.6	✓
c6	6.0	66.4	✓
+5	5.8	66.6	✓
1/4	0.9	71.5	✓
+7	0.8	71.6	✓
+8	3.0	69.4	
C	4.0	68.4	✓
+3	3.8	68.6	✓
+4	2.0	70.4	✓
1/4	2.v	70.v	✓
c6	2.1	70.3	✓
+v	2.3	70.1	✓
+3	5.7	66.7	✓
+8	4.7	67.7	✓
T.D 1129	E 3 13	0 52	71.84
+12	10.1	73.0	✓
N	10.v	7v.9	✓

8313

	0+75		83 1/		
N		6.4	76.7	/	
+9		7.4	75.7	/	
+10		9.9	73.2	/	
+15		10.5	72.6	/	
+17		13.0	70.1	/	
cb		9.4	73.7	/	
1/4		9.3	73.8	/	
+7		9.1	74.0	/	
+9		11.5	71.6	/	
C		11.5	71.6	/	
+N		7.9	75.2	/	
1/4		7.9	75.2	/	
+7		7.9	75.2	/	
+3		13.9	69.2	/	
cb		14.2	68.9	/	
+3		14.2	68.9	/	
+11		10.6	72.5	/	
S		11.2	71.9	/	
+5	1+03	11.2	71.9	/	
-5		10.5	72.6	/	
S		10.9	72.2	/	
cb		11.3	71.8	/	
1/4		9.7	73.4	/	
+7		4.8	78.3	/	
+8		5.2	77.9	/	

83.13 Narragansett 11

C	5.2	74.9	/
+7	5.5	77.6	/
1/4	5.6	77.5	/
cb	5.7	77.4	/
+5	5.3	77.8	/
+6	6.0	77.1	/
+8	6.4	76.7	/
+9	5.1	78.0	/
+14	5.0	78.1	/
+13	3.6	79.5	/
N	1.7	81.4	/
1+06			
N	1.1	82.0	/
+7	3.3	79.8	/
+8	4.5	78.6	/
+11	4.6	78.5	/
+14	6.0	77.1	/
+14	5.3	77.8	/
+15	4.6	78.5	/
cb	4.5	78.6	/
1/4	4.6	78.5	/
C	4.4	78.7	/
+8	4.5	78.6	/
1/4	7.9	75.2	/
cb	10.5	72.6	/
+5	7.9	75.2	/

8313

			83½		
c+7		3.9	79.2	✓	
S		4.7	78.4	✓	
	1+25				
S		2.0	81.1	✓	
+15		2.2	80.9	✓	
+16		8.1	75.0	✓	
c6		8.2	74.9	✓	
+3		6.6	76.5	✓	
+5		2.5	80.6	✓	
1/4		2.3	80.8	✓	
C		2.4	80.7	✓	
1/4		2.6	80.5	✓	
c6		2.3	80.8	✓	
+13		2.8	80.3	✓	
T.P.	10.94	9391	0.16	8297	
N			8.5	85.4	
	1+50			93⁹	
N			4.2	89.7	✓
+4			5.7	88.2	✓
+6			10.0	83.9	✓
c6			9.9	84.0	✓
1/4			10.7	83.2	✓
C			10.5	83.4	✓
1/4			10.1	83.9	✓
c6			10.4	83.5	✓
+1			13.9	80.0	✓

9391 Narragansett 12

c6	+5	13.9	80.0
	+7	10.2	83.7
	S	10.6	83.3
	1+77		
	S	7.5	86.4
	+14	6.9	87.0
	4/5	10.8	83.1
	+17	10.4	83.5
	+19	6.9	87.0
	c6	6.9	87.0
	1/4	6.6	87.3
	C	6.3	87.6
	1+79		
	S	5.0	88.9
	+14	6.6	87.3
	+15	10.6	83.3
	+17	10.2	83.7
	+18	6.9	87.0
	c6	6.7	87.2
	1/4	6.3	87.6
	C	6.0	87.9
	1/4	5.6	88.3
	c6	5.5	88.4
	+15	5.5	88.1
	+17	0.0	93.9
	T.P. 10.74	10391	0.74 93.17

		103.91		103.9				103.91		Mornagan 5-7 T	13
N			9.9	94.0						103.9	
	2+00							2+50			
N			5.9	98.0	✓			N	+1.0	104.9	✓
+3			6.8	97.1	✓			+8	-5.1	98.8	✓
+5			12.4	91.5	✓			cb	4.6	99.3	
cb			12.3	91.6				1/4	4.6	99.3	
1/4			12.6	91.3				C	5.2	98.7	
C			12.8	91.1				1/4	5.4	98.5	
1/4			13.5	90.4				cb	6.1	97.8	
cb			13.7	90.2				+2	9.0	94.9	
+1			13.7	90.2				+5	5.8	98.1	
+2			18.2	85.7				S	4.7	99.2	✓
+5			18.2	85.7					2+75		
+6			13.4	90.5				S	1.4	102.5	
S			12.3	91.6				+13	2.2	101.7	
	2+25							+15	4.6	99.3	
S			8.4	95.5	✓			cb	2.3	101.6	✓
+15			10.3	93.6	✓			1/4	1.8	102.1	
+17			12.0	91.9				C	2.0	101.9	
cb			9.7	94.2				1/4	2.0	101.9	
1/4			9.4	94.5				cb	0.6	103.3	
C			9.0	94.9				+15	1.9	102.0	
1/4			9.2	94.7	✓			T.P	12.77	116.12	0.56	103.35
cb			8.6	95.3				N	9.8	107.1	
+11			9.1	94.8					3+00		
N			1.8	102.1				N	3.6	112.5	
								+4	3.9	112.2	

11612

+6			10.2	105.9
cb			9.2	106.9
1/4			10.5	105.6
c			10.1	106.0
1/4			10.2	105.9
cb			10.7	105.4
+4			14.7	101.4
+6			10.7	105.4
S			10.6	105.5
	3+25			
S			6.2	109.9
+14			7.2	108.9
+16			12.7	103.4
+18			7.3	108.8
cb			7.3	108.8
1/4			6.3	109.8
c			6.5	109.6
1/4			7.0	109.1
cb			5.4	110.7
+10			5.0	111.1
+15			7.4	108.7
+16			0.5	115.6
N			0.0	116.1
T.P.	116.1	12.7.46	0.27	1.15.85
	3+50			
N			7.2	120.1

12.7.46 Narragansett

+3		8.1	119.4
+5		13.6	113.9
cb		12.6	114.9
1/4		13.6	113.9
+2		15.8	111.7
+7		14.0	113.5
c		14.0	113.5
1/4		14.1	113.4
+3		22.1	105.4
cb		14.7	112.8
S		14.4	113.1
	3+75		
S		10.4	117.1
cb		8.9	118.6
+2		15.0	112.5
+7		8.9	118.6
1/4		8.9	118.6
+5		10.4	117.1
c		8.8	118.7
1/4		8.3	119.2
cb		8.6	118.9
+16		8.2	119.3
N		4.7	122.8
	4+00		
N		2.0	125.5
+5		4.4	123.1

127.46

cb			4.2	1x3.3
1/4			3.7	1x3.8
C			4.4	1x3.1
+6			4.8	1x2.7
1/4			7.7	119.8
+3			4.8	1x2.7
cb			4.8	1x2.7
S			6.3	1x1.2
	4+25			
S			4.0	1x3.5
cb			2.9	1x4.6
1/4			2.4	1x5.1
+1			5.0	1x2.5
+7			5.0	1x2.5
C			2.0	1x5.5
1/4			1.4	1x6.1
cb			1.5	1x6.0
+3			3.8	1x3.7
+5			3.8	1x3.7
+6			1.9	125.6
N			0.2	1x7.3
T.P.	1x83	139.90	0.39	1x7.07
	4+50			
N			9.8	130.1
cb			12.5	127.4
+2			14.0	1x5.9

139.90 Narragansett 15

cb +4		11.0	128.9
1/4		11.6	128.3
C		11.9	1x8.0
+2		13.8	126.1
1/4		15.3	124.6
+2		12.5	127.4
cb		12.9	127.0
S		14.4	1x5.5
+5		14.8	125.1
	4+75		
-S		13.1	126.8
S		12.5	1x7.4
cb		10.7	129.2
+8		10.0	129.9
1/4		12.8	127.1
C		9.4	130.5
1/4		8.8	131.1
+6		8.3	131.6
+7		9.7	130.2
cb		9.8	130.1
+7		9.3	130.6
+8		7.8	132.1
N		7.0	132.9
	5+00		
N		4.5	135.4
+13		5.4	134.5

+14		6.9	133.0
+17		8.2	131.7
+18		5.9	134.0
c6		6.3	133.6
1/4		6.9	133.0
+5		7.5	132.4
+6		9.2	130.7
1/2		9.2	130.7
+3		9.7	130.2
+4		8.0	131.9
c6		8.7	131.2
S		11.3	128.6
+5		11.9	128.0
	S+25		
-5		9.0	130.9
S		8.3	131.6
c6		6.0	133.9
+7		5.5	134.4
1/2		8.0	131.9
+4		7.5	132.4
C		4.6	135.3
1/4		3.7	136.2
c6		3.7	136.2
+1		4.9	135.0
+7		4.6	135.3
+8		2.8	137.1

N		1.7	138.2
TP	13.11	15.28	1.83	138.17
	S+50		
N		10.0	141.3
+13		11.6	139.7
+14		11.2	137.1
c6		14.3	137.0
+1		12.9	138.2
1/4		12.9	138.2
C		13.6	137.7
+5		14.2	137.1
+9		17.6	133.7
1/4		17.7	133.6
+1		17.5	133.8
+3		14.8	136.5
c6		15.1	136.2
S		17.0	134.3
+5		17.8	133.5
	S+75		
-5		16.5	134.8
S		15.5	135.8
c6		13.1	138.2
1/4		12.3	139.0
+1		15.3	136.0
+4		15.2	136.1
+7		12.1	139.2

C		11.0	140.3
1/4		11.5	139.8
c6		10.4	140.9
+4		10.6	140.7
+3		13.1	138.2
+9		13.0	138.3
+10		8.5	142.8
N		7.3	144.0
	6 + 00 = WL Froude = 60' wide 12' curbs 9' 1/2 S		
N		6.0	145.3
+8		6.8	144.5
+9		11.0	140.3
c6		11.5	139.8
+1		11.5	139.8
+4		7.9	143.4
1/4		8.8	142.5
+8		8.8	142.5
+9		17.1	139.2
C		12.8	138.5
+5		12.8	138.5
+6		10.5	140.8
1/2		10.2	141.1
c6		11.5	139.8
S		13.9	137.4
+5		14.9	136.4

W cur 6		
-5	13.9	137.4
S	13.0	138.3
c6	10.4	140.9
1/4	9.3	142.0
+5	9.0	142.3
+6	11.6	139.7
C	11.6	139.7
+1	7.8	143.5
1/4	7.6	143.7
+7	6.9	144.4
+8	10.3	141.0
c6	10.3	141.0
+5	10.4	140.9
+7	5.9	145.4
N	4.8	146.5
W 1/4		
N	3.8	147.5
+13	4.7	146.6
+15	9.3	142.0
c6	9.8	141.5
+4	9.8	141.5
+5	6.1	145.2
1/4	6.6	144.7
+7	6.9	144.4
+8	9.8	141.5

15128

C		11.3	140.0
+7		10.5	140.8
+8		8.0	143.3
1/4		8.0	143.3
c6		9.5	141.8
S		12.3	139.0
+5		13.3	138.0
	Center		
-5		12.5	138.8
S		11.6	139.7
c6		8.3	143.0
1/4		7.1	144.2
+2		7.1	144.2
+3		9.6	141.7
C		9.9	141.4
+1		9.9	141.4
+3		6.1	145.2
1/4		6.0	145.3
+5		5.2	146.1
+6		7.5	143.8
c6		8.4	142.9
+6		8.3	143.0
+8		4.1	147.2
N		3.0	148.3
	E 1/4		
N		2.3	149.0

15128 Narragansett 18

+12	3.4	147.9
+13	6.3	145.0
c6	7.1	144.2
+1	4.1	147.2
1/4	5.4	145.9
+8	5.6	145.7
+9	8.5	142.8
C	8.5	142.8
+7	9.8	141.5
+8	6.4	144.9
1/4	6.4	144.9
c6	7.6	143.7
S	10.9	140.4
+5	11.9	139.4
	E c6	
-5	11.1	140.2
S	10.2	141.1
c6	6.8	144.5
+8	5.9	145.4
1/4	8.4	142.9
+8	8.0	143.3
C	5.1	146.2
1/4	4.4	146.9
c6	3.6	147.7
+1	6.0	145.3
+5	5.7	145.6

15128

cb +6			2.6	148.7
N			1.6	149.7
	EL Froude = 0.100			
N			0.5	150.8
+13			1.7	149.6
+14			3.4	147.9
+16			3.4	147.9
+18			2.7	148.6
cb			2.7	148.6
1/4			3.2	148.1
C			4.0	147.3
+1			6.6	144.7
+6			7.3	144.0
+7			5.0	146.3
1/4			4.8	146.5
cb			6.1	145.2
S			9.6	141.7
+5			10.6	140.7
	0+25			
-5			7.7	143.6
S			6.6	144.7
cb			4.3	147.0
1/4			3.3	148.0
T.P.	1054	161.67	0.15	151.13
+5			13.4	148.3
+6			16.4	145.3

161.67 Narragansett 19

C		15.6	146.1
+1		12.7	149.0
1/4		12.0	149.7
+9		11.4	150.3
cb		13.0	148.7
+3		12.7	149.0
+6		10.2	151.5
N		9.2	152.5
	0+50		
N		7.3	154.4
+N		8.8	152.9
cb		11.5	150.2
+1		10.1	151.6
1/4		10.3	151.4
+8		11.5	150.2
C		13.5	148.2
+6		13.7	148.0
+7		12.2	149.5
1/4		12.0	149.7
cb		13.2	148.5
S		15.0	146.7
+5		15.5	146.2
	0+75		
-5		13.8	147.9
S		13.3	148.4
cb		11.5	150.2

16167

1/4		10.7	N 1.0
+5		10.8	N 0.9
C		12.2	N 9.5
+5		10.9	N 0.8
1/4		8.6	N 3.1
cb		10.1	N 1.6
+2		8.2	N 3.5
N		5.7	N 6.0
	1+00		
N		4.0	N 7.7
cb		6.2	N 5.5
1/4		7.5	N 4.2
C		8.6	N 3.1
1/4		8.9	N 2.8
cb		10.3	N 1.4
S		11.7	N 0.0
+5		11.9	N 9.8
	1+25		
-S		9.6	N 2.1
S		9.7	N 2.0
cb		8.5	N 3.2
1/4		7.4	N 4.3
C		6.9	N 4.8
1/4		6.8	N 4.9
cb		5.2	N 6.5
N		2.6	N 9.1

16167 Narragansett 70

	1+50		
N		1.7	160.0
cb		3.3	N 8.4
1/4		4.5	N 7.2
C		5.2	N 6.5
1/4		5.2	N 6.5
cb		6.1	N 5.6
S		6.3	N 5.4
+5		6.3	N 5.4
	1+75		
-S		3.1	N 8.6
S		3.1	N 8.6
cb		3.0	N 8.7
1/4		3.0	N 8.7
C		2.7	N 9.0
1/4		2.5	N 9.2
cb		2.0	N 9.7
N		0.0	161.7
T.P.	12.83	173.93	0.57 161.10
	2+00		
N		10.8	163.1
cb		11.5	162.4
1/4		12.2	161.7
+2		13.0	160.9
C		13.0	160.9
+1		12.0	161.9

173.93

1/4		12.4	161.5
a6		12.2	161.7
S		11.4	162.5
+5		10.4	163.5
	2+25		
S		5.9	168.0
c6		7.3	166.6
1/4		7.9	166.0
C		9.0	164.9
+6		9.4	164.5
+7		11.3	162.6
1/4		11.3	162.6
+4		11.2	162.7
+5		9.1	164.8
c6		8.8	165.1
N		8.1	165.8
	2+50		
N		4.5	169.4
c6		5.9	168.0
+5		7.0	166.9
1/4		6.2	167.7
C		4.3	169.6
1/4		3.3	170.6
c6		3.2	170.7
+4		3.2	170.7
+5		2.0	171.9

173.93 Narragansett 21

S	1.7	172.2
T.P. 12:90 - 18.57	12.6	172.67
2+75		
S	10.5	175.1
c6	10.8	174.8
1/4	11.3	174.3
C	11.8	173.8
+6	11.7	173.9
+7	14.2	171.4
1/4	14.2	171.4
+6	14.3	171.3
c6	11.8	173.8
N	13.2	172.4
3+00		
N	8.2	177.4
c6	7.8	177.8
7.8	8.1	177.5
+9	10.6	175.0
1/4	10.7	174.9
+4	10.6	175.0
+3	8.0	177.6
C	7.8	177.8
1/4	7.7	177.9
c6	7.3	178.3
S	6.3	179.3

		185.57		
	3+25			
S			2.8	182.8
+15			3.2	182.4
+16			4.2	181.4
cb			3.8	181.8
1/4			4.1	181.5
C			4.3	181.3
+2			4.2	181.4
+3			6.3	179.3
1/4			6.2	179.4
+1			4.7	180.9
cb			4.3	181.3
N			4.9	180.7
	3+50			
N			1.4	184.2
cb			0.6	185.0
1/4			1.0	184.6
C			0.7	184.9
1/4			0.7	184.9
cb			0.6	185.0
T.P.	13.2	198.49	0.20	185.37
S			12.6	185.9
	3+75			
S			9.0	189.5
+13			9.7	188.8
+14			10.8	187.7

		198.49	Narragansett	
cb			10.3	188.2
1/4			10.4	188.1
C			10.6	187.9
+6			11.6	186.9
+7			10.5	188.0
1/4			10.5	188.0
cb			10.7	187.8
			11.3	187.2
	4+00			
N			8.4	189.1
cb			7.8	190.7
1/4			7.7	190.8
C			9.0	189.5
1/4			8.0	190.5
cb			6.7	191.8
S			6.0	192.5
	4+25			
S			2.9	195.6
cb			3.7	194.8
+9			4.6	193.9
1/4			6.5	192.0
+3			4.3	194.2
C			4.5	194.1
1/4			4.8	193.7
cb			5.2	193.1
N			6.9	191.6

		1984.9		
	4+50			
N			4.9	193.6
cb			3.5	195.0
1/4			3.0	195.5
C			2.4	196.1
1/4			2.4	196.1
cb			2.0	196.5
S			0.9	197.6
T.P.	9.65	206.66	1.48	197.01
	5+00			
S			7.1	199.6
cb			7.5	199.2
1/4			8.0	198.7
C			8.3	198.4
1/4			8.5	198.2
cb			8.8	197.9
N			9.9	196.8
	5+50			
N			7.2	199.5
cb			6.7	200.0
1/4			6.5	200.2
C			6.4	200.3
1/4			6.1	200.6
cb			5.8	200.9
S			5.2	201.5

206.66 Narragansett 23

6+00 = W/L Circuit bounds 12' curbs 9' 1/2 on West

S	3.2	203.5	
cb	4.0	202.7	14' curbs on East.
1/4	4.2	202.5	
C	4.5	202.2	
1/4	4.6	202.1	
cb	4.8	201.9	
N	5.2	201.5	
	W/ curb		
N	5.0	201.7	
cb	4.4	202.3	
1/4	4.3	202.4	
C	4.1	202.6	
1/4	3.9	202.8	
cb	3.6	203.1	
S	2.9	203.8	
	W 1/2		
S	3.3	203.4	
cb	3.6	203.1	
1/4	3.9	202.8	
C	4.1	202.6	
1/4	4.1	202.6	
cb	4.2	202.5	
N	4.3	202.4	
	Center		
N	3.9	202.8	

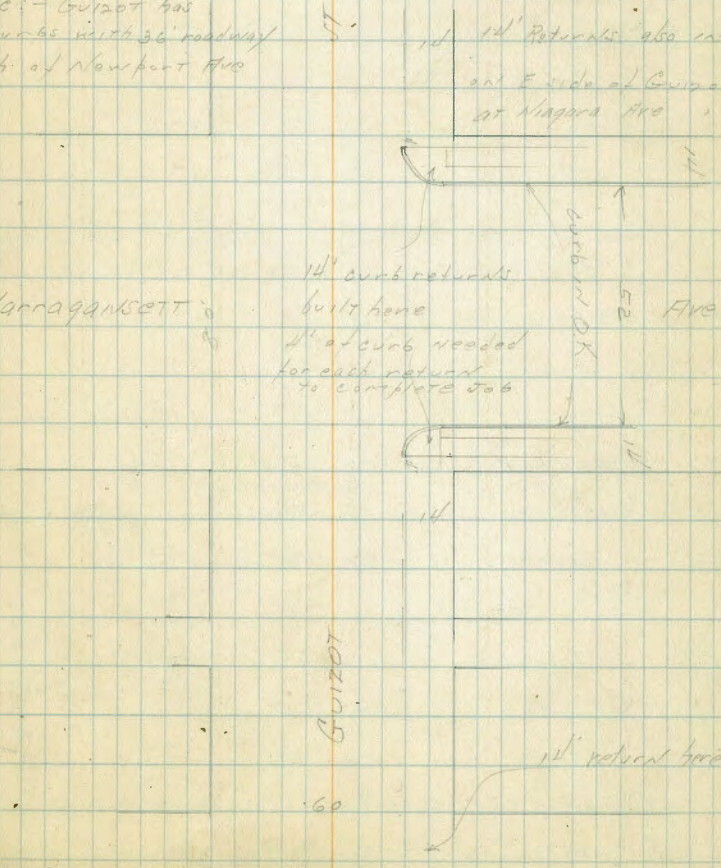
206.66

cb		4.1	202.6
1/4		4.1	202.6
c		3.9	202.8
1/4		3.9	202.8
cb		3.7	203.0
S		3.4	203.3
	E 1/4		
S		3.0	203.7
cb		3.6	203.1
		3.7	203.0
		3.7	203.0
		4.0	202.7
cb		4.0	202.7
N		4.0	202.7
	E curb		
N		3.3	203.4
cb		3.9	202.8
1/4		3.6	203.1
c		3.3	203.4
1/4		3.4	203.3
cb		3.5	203.2
S		2.3	204.4
	E. Guizot		
S		2.0	204.7
cb	top semi curb	2.55	204.11
1/4		3.0	203.7

206.66 Narragansett 24

C		2.7	204.0
1/4		3.2	203.5
cb	Top semi curb	2.64	203.94
N		2.8	203.9
T.P.	130 218.94	0.82	217.84
check to BP	Del Monte Guizot	1.21	217.73 218.03 0.30 error

Note:- Guizot has 72' curbs with 36' roadway North of Newport Ave



Walker 4-14-27

X. Section 20' Alley. Blk. 17 Univ. Hts
Bet. Hamilton + Arizona
From N.L. MADISON to S.L. ADAMS AVE

S.E. B.P. Madison & Hamilton	1.96	380.95		378.99
N.L. MADISON = South End of Fence on E 0.2 in Alley				
E top cb			5.70	375.25
Gut			6.0	375.0
℄			6.6	374.4
Gut			6.8	374.2
W top cb			6.54	374.41
17' N N.L. MADISON				
W			5.1	375.9
℄			5.3	375.7
E			4.8	376.2
From 30' N = Con. Walk Parallel with Alley on E 1.8 0.4' in Alley 2.5' Wide				
56' N = N end of Above fence on E 0.5 in Alley				
E + 0.4 = top con Walk			3.92	377.03
℄			4.8	376.2
W			4.9	376.1
65' N = ℄ Garage on W 9' Back Con. Floor			5.50	375.45
		R= 3.54		377.36
86' N = N end Con. Walk on E 2.5 Wide 0.6' in Alley				
91' N = ℄ Garage on E 2' Back Con. Floor			3.40	377.6
100' N				
W			4.3	376.7
℄			4.2	376.8
E			3.8	377.2
116' N = ℄ Garage on W 2.5' Back Con. Floor			4.13	376.87
128' N = ℄ " on E 5' Back dirt Floor			4.0	377.0
132' N = ℄ " " W 7.3' " con. Floor			4.37	376.63

Plotted by Tolman 4/28/27

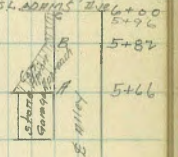
380.95

146' N = ℄ Garage on E 1.5' Back con. Floor With con. Apron Approach		
-1.5' = Garage Floor	3.30	377.65
E + 0.5 = toe of con. Apron	3.37	377.58
℄	3.9	377.1
W	4.2	376.8
176' N = ℄ Garage on W 2.4' Back Con. Floor With con. Apron Approach		
-2.2 = Garage Floor	3.99	376.96
-1' = toe of Apron	4.17	376.78
W	4.2	376.8
℄	3.7	377.3
E	3.5	377.5
216' N = ℄ Garage on W 2' Back con. Floor With con. Apron Approach		
E	3.5	377.5
℄	3.6	377.4
W	3.9	377.1
+0.5' = toe of Apron	3.68	377.07
+2' = Garage Floor	3.71	377.24
Garage Floor =	2.77	378.18 Garage 2' Back
242' N = ℄ Garage on E Con. Floor. Con Apron =	2.98	377.97 Con. Apron 1' in Alley
T.P. 6.89	380.58	3.26 377.69
250' N		
W	6.9	377.7
℄	6.8	377.8
E	6.6	378.0
308' N = ℄ Garage on E. 1.4' Back dirt Floor		
-1.4 on Garage	5.5	379.1
E	5.5	379.1

℄	6.1	378.5
W	6.4	378.2
371'N = ℄ Garage on E 1' Back dirt Floor		
W	5.8	378.8
℄	5.7	379.4
E	4.9	379.7
+1 = Garage	4.9	379.7
380'N = ℄ Garage on E 1' Back dirt Floor	4.9	379.7
400'N		
E	4.8	379.8
℄	5.0	379.6
W	5.4	379.2
{345'N = ℄ sheds on E 1.6' in Alley 27' Wide}		
457'N = ℄ Garage on W 3' Back dirt Floor		
-3' = Garage	5.3	379.3
W	5.3	379.3
℄	4.8	379.8
E	4.6	380.0
507'N = ℄ Garage on W 3' Back con. Floor with		
E	4.2	380.4
℄	4.3	380.3
W = toe of con. Apron	4.63	380.0
+3 = Garage Floor	4.48	380.1
5750		
W	4.0	380.6
℄	3.8	380.8

384.58

E	3.6	381.0
566'N = N edge of Garage on West Wall (con. Floor) North Entrance to Alley Con. Apron Approach		
E	3.7	380.9
℄	4.3	380.3
W = A on top con Apron	4.47	380.2
587'N		
W = B on top con Apron	4.50	380.1
℄	5.0	379.6
+7	5.1	379.5
E	4.5	380.1
596'N		
E	5.9	378.7
+4	6.8	377.8
℄	6.8	377.8
+1	6.2	378.4
W = C top of Walk see sketch	6.14	378.5
600'N = S.L. ADAMS		
W on top of Walk	7.21	377.37
" " " " C6.	7.67	376.91
W Gut on Paving	7.82	376.76
℄ " "	7.76	376.82
E " " "	7.22	377.36
E top C6	6.86	377.72
{590'N = ℄ M.H. on Rim	5.77}	378.81
T.P. 1.64 3793.3	6.89	377.69
Chk. on S.E. Bld. Madison + Hamilton	0.34	375.79 ✓



Walker 6-20-24

X. Section 20' Alley Blk 184 Univ. Hts

From Sh. Lincoln to N. Richmond

(℄ stations)

S.W. S.P. Henchicks & Richmond	3.30	301.78		298.48
T.P.	6.27	306.55	150	300.28

S. L. Lincoln Section Parallel with Lincoln

W top ob	3.96
Gut on Paving	4.10
℄ " "	4.33
Gut " "	4.01
E. top ob	3.66

38' South Section Rt. Angles to Alley

E	6.6
℄	6.2
W	6.3

63' S

-V	8.9
W	8.9
℄	9.0
E.	8.6
+V	8.6

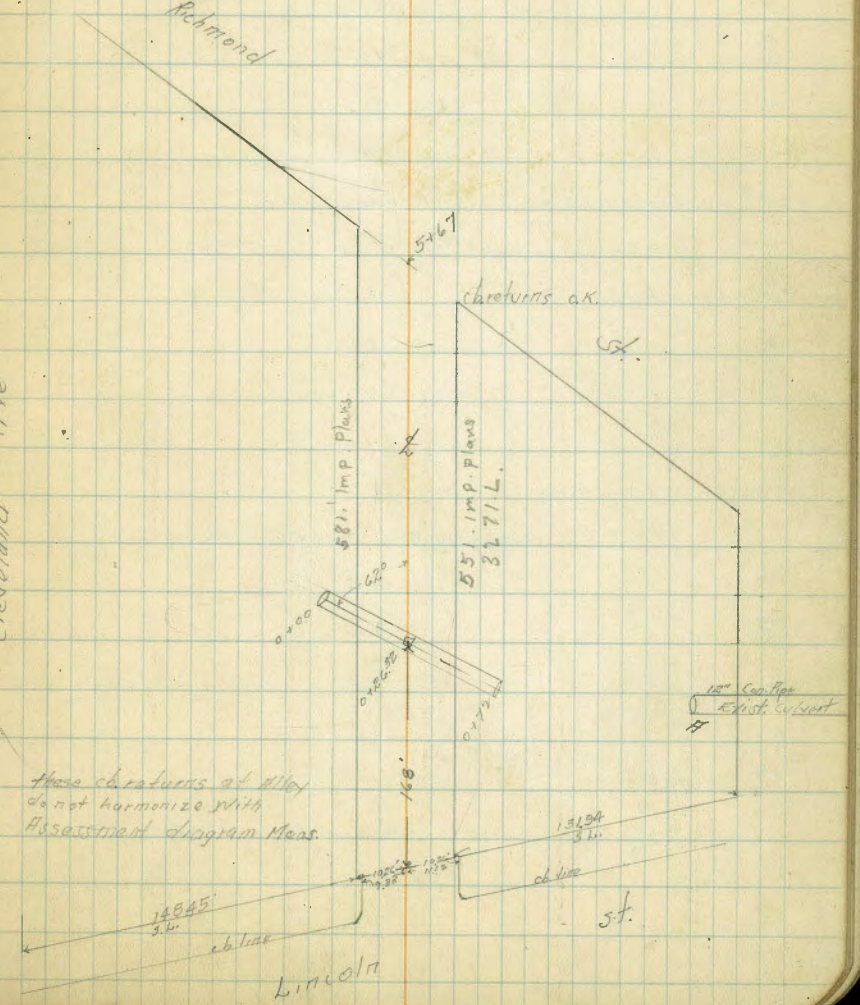
103' S

-1 = Fence	10.9
E	10.9
℄	10.7
W	10.8
+5	10.4

143' S = ℄ Garages on E. and West = 0.4 in Alley dirt Floor

East = 2' Back Brick Floor

Note: if Grade is raised at station 143' South of S.L. Lincoln a culvert should be located as these Garages at this station are on line of natural drainage — Walter



30655

W + 0.4 = Garage		11.6
C		10.8
E		10.5
+ 7 = Garage Floor		10.37
	150'S	
E		5.8
C		7.3
W		8.7
+5		10.0
		All Con. Floors on W
155'S = C Garage on E. = N End of 4 Garages on W		
T.P.	3.20 30185	7.90 29865
- 7 = Garage Con. Floor		3.76
W		3.7
C		2.7
E		1.0
+7 = Garage dirt Floor		0.7
	178'S = C Garage on E 6' Back dirt Floor	
- 6		1.4
E		1.6
C		3.3
W		4.1
+7 = Garage Floor		3.99 4.15
195'S = South End of 4 Garages on W Con. Floors 6' Back		
196'S = N " " 3 " " " " " " "		
- 6 = Garage Floor		4.66
W		4.6

30185

38

C	3.9
E	2.0
205'S.	
E	3.7
C	4.3
W	4.7
223'S = S End 3 Garages on W Con. Floors 5.5' Back	
-5.5 = Garage Floor	4.67
W	5.1
C	5.6
E	4.7
244'S	
E	4.7
C	6.1
W	6.2
+5	6.4
234'S = Point where 6" Gas Main Emerges	
-5	8.1
W	7.5
+6 on top of Gas Main	6.95
C	6.7
E	5.4
257'S	
-5	5.8
E	6.1
C	5.5

+4 on Top Gas Main	6.41
W	12.0
+20	18.7
266'S = Point Where Gas Main Submerges	
-15	12.3
-10	13.2
W	9.6
+6 = top of Main	5.92
℄	5.1
E	5.9
+5	5.9
Levels for Culvert see Sketch Page 27	
0+00	8.8
+05	8.5
+10	5.3
+26.32 on stub in ℄ Alley	4.86
+45	16.2
+72 = End	19.3
Exist Floor line ℄ E see Sketch	23.2
277'S	
-10	6.6
E	5.2
℄	4.6
+4	4.5
W	8.2
+4	10.4

+10	9.5
280'S	
-10	7.9
-3	9.0
W	7.5
+6	4.2
℄	4.5
E	5.1
+4	5.0
+10	8.0
295'S	
-5	4.5
E	4.0
℄	3.5
W	3.4
+5	3.5
308'S = ℄ Garage on E dirt Floor	
W	2.3
℄	2.5
E	3.3
+4 = Garage	3.3
T.P 6.07	305.67 2.20 299.65
325'S = ℄ Garage on E Wood Floor 0.2 Back	
-0.2 = Garage Floor	4.47
E	5.6
℄	5.7

W 5.7
Floor = 4.92
325'S = ℄ Garage on Con Floor, With Con Apron 5.74 Con Apron ℓ in Alley
5.09
353'S = N end triple Garages on E on line dirt Floor
355'S = ℄ Garage 45' Back on N Con Floor 5.2
376'S = S end triple Garages on E dirt Floor
W 5.2
℄ 5.2
E 5.3
401'S = N end 2 Garages on E 5.0 dirt Floors
405'S = ℄ Garage on W
E 4.9
℄ 5.2
W 5.1
+2' = Garage 5.1
441'S = S end of 4 Garages on E 4.9 dirt Floors
446'S = ℄ Garages on E and W Con Floor
-5' = Garage Floor 5.4
W 5.4
℄ 5.4
E = Garage Floor 4.89
503'S = N end dble. Garage on E dirt Floor
E = Garage 5.5
℄ 5.7
W 5.7
513'S = S end Above Garages on E
W 6.2

℄ 6.0
E = Garage 5.8
528'S = N end Dble. Garages on E 5.7 dirt Floors
548'S = S " " " " " " "
E 6.0
℄ 6.1
W 6.1
567'S = N.L. Richmond at ℄ Alley Note: this section Parallel with N.L.
W top cb 5.84
W Gut. on Pav. 5.91
℄ " " 6.35
E Gut. " " 6.07
E top cb 5.90
T.P 5.01 30454 6.14 29953
cbk. on B.M. Hendricks & Richmond 6.05 x98.49
x98.49 = B.M.
0.01

Notes 4-20-27

X. Section 20' Alley. Pueblo Lot 1122 Blk 476
Bet. Bush & Sutter St.
From E.L. Goldfinch to W.L. (GOLDFINCH PL.)

V.S. B.P.
Sutter & Goldfinch 5.95 ℄ 267.94 256.99

E.L. Goldfinch

S top ℄	4.78	258.16
S Gutter on Bring	4.90	258.04
℄ " "	5.00	257.94
N Gut "	4.75	258.19

Plotted JAB

No ℄ of Prop. on N steps West edge of walk

15' E = ℄ Con steps on N 5.3' Wide

N top Ref. Wall = 3'E of ℄ "	2.72	260.22
N top steps	3.42	259.52
N Gut	4.9	258.0
℄	4.2	258.7
+6	4.2	258.7
S	2.3	260.6

45' E = ℄ Garage on South 1.2' Back Dirt floor

-1.2	3.2	259.7
S	3.2	259.7
+1	3.8	259.1
℄	4.1	258.8
N	3.8	259.1
N top Ret. Wall	3.23	259.71

57' E = ℄ Garage (Dirt floor) on S 5.5' Back 2.6 260.3

63' E = End of Con Ret. Wall on E. (5) in line

N top Wall	3.5 ℄	259.40
N Gut	4.1	258.8
℄	4.2	258.7

267.94

3.1

+5	4.1	258.8
S	2.8	260.1

93' E = ℄ Garage on N Con. Floor With Con. Apron

S	3.0	259.9
+4	4.4	258.5
℄	4.4	258.5
N	4.3	258.6
+5 = toe Apron	3.92	259.02

South Garages has Con. Apron Approach

103' E = West end Dble. Garages on N +5

-1.7 = Garage Floor on Con.	4.30	258.64
N	4.4	258.5
℄	4.4	258.5
S	4.1	258.8
+1 = toe of Apron	4.02	258.92
+5 = Garage Floor	3.41	259.53

121' E = End of Above Dble Garages

-6 = Garage Floo	3.31	259.63
-5' = toe of Apron	4.06	258.88
S	4.2	258.7
℄	4.5	258.4
N	4.5	258.4
+1.7 = Garage Floor	4.30	258.6
133' E = ℄ Con. Walk (3' Wide) on S	3.95	258.99
137' E = " " " " N (2' Wide)	5.20	257.74
152' E = West edge Con Ret. Wall on N 0.3' in Alley		
-1	7.2	255.7

1+52

43' N=top Wall	5.20	257.7
℄	5.1	257.8
S	5.1	257.8
	toe Apron 5.11	257.83 Con Apron on line
161' E = ℄ Garage on S Con Floor	4.42	258.52 Garage 5' Back
196' E = ℄ " " N on line "	6.00	256.9
201' E = Wend Dble. " S Con. Floor with Con. Apron.		
-2' = Garage Floor	5.57	257.37
S = toe of Apron	5.87	257.12
℄	6.0	256.9
N	6.0	256.9
	Garage Floor 5.60	257.34
218' E = E end Dble. Garage on S	toe Apron 5.90	257.04
267' E = ℄ Dble Garage on S Dirt Floor 2' Back		
-1'	11.3	251.6
N = top Ret. Wall Begins at Station 1+52	6.35	256.59
℄	6.0	256.9
S	6.5	256.4
+2	6.5	256.4
304' E = ℄ Catch Basin on N 10" Corrugated Iron Pipe out let 1.5' S of N.L.		
on top Grade	6.70	256.7
" Flow line	9.31	253.63
	top Wall 6.39	256.55
303' E = E end Con. Ret Wall on N		
309' E = ℄ Garage on S con. Floor		
S = Garage Floor	5.87	257.09
℄	6.1	256.8
N	6.4	256.5

343' E = ℄ Garage on N 45' Back dirt Floor

767.94

(343 E)

-45 = Garage Floor	6.8	256.1
N	6.5	256.4
℄	6.1	256.8
S	6.5	256.4
397' E = West end Dble. Garage on N 5' Back dirt Floor		
399' E = " " " " " S with Con Floor & Con Apron		
-5' = Garage Floor	5.48	257.46
S = toe of Apron	6.14	256.80
℄	6.1	256.8
N	6.3	256.6
+5' = Garage	6.4	256.5
410' E = E end Dble Garage on N	6.3	256.6
416' E = " " " " S		
S = toe of Apron	5.90	257.04
+5	5.31	257.63
431' E = ℄ Con. Walk on S 0.3' Back		
N	5.8	257.1
℄	5.9	257.0
S	5.8	257.1
+0.3 = Walk	5.74	257.20
480' E = W L. EAGLE St		
S top cb	5.26	257.68
Gut on Par.	5.54	257.40
℄ " "	5.89	257.05
Gut " "	5.70	257.24
N top cb	5.45	257.49

Plotted 8-8

Walker 1-30-27

X. Section 15' Alley Blk 28 Normal Hts.

Bet 34th & Felton And Bet Adams & Jefferson

S.E. B.P. Adam & Boundary	3.26	394.22 ✓		390.96	
T.P.	3.27	392.34 ✓	5.15	389.07 ✓	N.E. B.P. Adams & Mountain View
T.P.	3.79	389.92 ✓	6.21	386.13 ✓	
T.P.	6.64	393.22 ✓	3.34	386.58 ✓	
T.P.	5.06	393.38 ✓	4.90	388.32 ✓	N.W. B.P. Adams & Felton
T.P.	7.24	397.24 ✓	3.38	390.00 ✓	N.E. B.P. Jefferson & Felton

Note; 6' North of South Line ~~Jefferson~~ Collier st. = End of exist. cb.

E top cb		6.56	390.68
W top cb		6.79	390.45

S.L. ~~Jefferson~~ Collier = 0+00

W		6.5	390.7
℄		6.3	390.9
E		6.3	390.9

30' South S.L. Jefferson

E		4.1	393.1
℄		4.4	392.8
W		3.9	393.3

Apron is Level

64'S = ℄ Dble. Garage on W 18' Wide Con. Floor Con. Apron

-1.3' = Garage Floor		3.09	394.15
-7' = toe of Apron		3.41	393.76
W		4.0	393.7
℄		4.3	392.9
E		4.0	393.7

173'S = ℄ Garages on E & W dirt Floors

-1.3' = Garage		4.7	392.5
E		4.6	392.6
℄		4.6	392.6
W		4.3	392.9
+6.5 = Garage		3.9	393.3

138'S = N end Board Fence on W 0.9' in Alley

186'S = S " " " " " 0.8' " "

188'S = ℄ Garage on E. Dirt Floor

W		4.5	392.7
℄		4.6	392.6
E		4.8	392.4
+5 = Garage		5.1	392.1

191'S = ℄ Garage on W 10' Wide 0.8' in Alley St. Entrance

196'S = N end Board Fence on W 0.8' in Alley

241'S = S " " " " " 1.3' " "

E		5.1	392.1
℄		4.8	392.4
+6" = Fence		4.8	392.4

259'S = ℄ Shed on West 36' Wide 1.5' in Alley

285'S = ℄ Garage on W Entrance on E+W Alley 1.5' in N+S Alley

W+1.5 = Garage		4.8	392.4
℄		4.9	392.3
E		4.8	392.4

301'S = N.L. of E+W Alley

E		5.2	392.0
℄		5.3	391.9
W		5.2	392.0

Walker 4-21-21

397.24 = HI, From Page 33

E + W Alley 15' Wide Blk of Normal Hts.

T.P.	459	396.78	5.05	391.73
Note: End of Exist. Paving Mod cb is 2' W of E.L. Felton St.				
S. top cb			7.02	389.76
S Gut on Paving			7.12	389.66
℄ " "			7.37	389.41
N " " "			7.24	389.54
N top cb			7.22	389.56

Plotted JBB

E.L. Felton = 0+00

N	6.9	389.9
℄	7.1	389.7
+4	6.9	389.9
S	6.2	390.6

4'E = ℄ Con. Ret. Wall on N 0.4' in Alley

S	5.1	391.7
+4	6.4	390.4
℄	6.6	390.2
+7.1 = Base of Wall	6.2	390.6
+7.1' on top of "	4.87	391.91

20'E

N	5.0	391.8
+3	5.7	391.1
℄	5.8	391.0
+3	5.4	391.4
S	4.8	392.0

50'E

S	4.5	392.3

396.78

84

+4	5.0	391.8
℄	5.1	391.7
N	4.8	392.0

72' S = N end Board Fence on S of 4' in Alley

100'E

N	5.2	391.6
℄	4.8	392.0
+7.2 = Fence	4.7	392.1

129'E = E end Board Fence on S of 2' in Alley = ℄ Garage on N Con. Floor

5+0.2' = Fence	4.7	392.1
℄	4.8	392.0
N	4.9	391.9
+6.5 = Garage	4.70	392.1
136'E = ℄ Garage on S (dirt Floor 1.7' Back)	4.7	392.1
141.5'E = ℄ M.H. 4's of ℄ Alley	4.85	391.93 on Rim
146'E = ℄ Garage on S con. Floor with Con. Apron		
N	4.8	392.0
℄	4.9	391.9
S	4.8	392.0
+1 = toe of Con. Apron	4.66	392.14
+1.7 = Garage Floor	4.59	392.19

200'E

S	5.0	391.8
℄	5.0	391.8
N	5.1	391.7

39698

35

250' E

N		5.3	391.5
d		4.9	391.9
S		4.3	392.5

281' E = N.Y.C. 34th St. = Westedge of Paving

S top of Paving		5.89	390.89
d " "		6.15	390.63
N " "		6.01	390.77

278.5' E = N End of Exist. c.b. {c.b. does not extend to N line by 1.5'}

N top cb		6.09	~~390.69~~
S " "		6.01	390.77
T.P.	5.33	395.19	389.86 ✓
Chk. on B.M. S.W. Adams+30th		5.94	389.25 ✓

Walker 4-21-27

X. Section 47th St. 60' Wide 12' cbs 9' ⅄s
From N.L. E.L. Cajon to
TALMADGE PARK

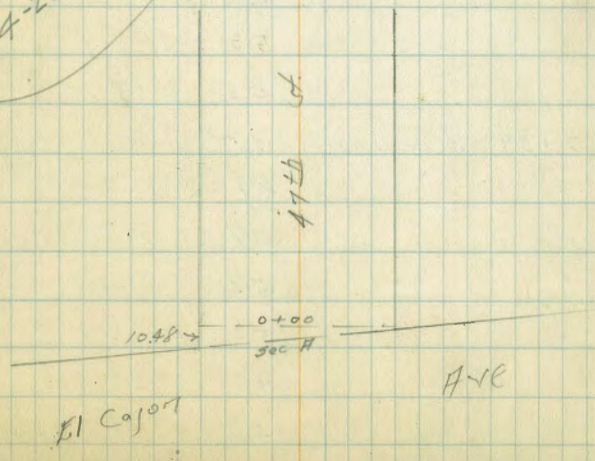
S.W. B.P.				
E. Cajon + 47th	6.08	353.28	347.20	
		Sec 4		
E.		5.9	347.4	
E. top cb		6.05	347.23	
" Gut. on Paving		6.50	346.78	
¼ " "		6.19	347.09	
℄ " "		5.99	347.29	
¼ " "		6.09	347.19	
Gut " "		6.28	347.00	
W top cb		5.68	347.70	
W		5.6	347.7	
	0+00			
W		5.6	347.7	
cb		5.6	347.7	
¼		5.6	347.7	
℄		5.7	347.6	
¼		6.0	347.3	
cb		6.2	347.1	
E.		5.9	347.4	
0+42 = M.H. 5' W of ℄		5.15	348.13	on Rim
	0+50			
E.		5.4	347.9	
cb		5.5	347.8	
¼		5.0	348.3	
℄		5.1	348.2	

353.28

36.

¼		5.4	347.9
cb		5.4	347.9
W		5.0	348.3
	1+00		
W		5.1	348.2
cb		5.3	348.0
¼		4.7	348.6
℄		4.5	348.8
¼		4.6	348.7
cb		5.1	348.2
E.		5.0	348.3

Plotted 4-22-27 LBH



1+60 = ℄ Con. Walk on W

E	5.2	348.1
cb	5.4	347.9
¼	4.7	348.6
℄	4.3	349.0
¼	4.6	348.7
cb	4.9	348.4
W	4.9	348.4
+1' = top Walk	4.8 W	348.46

1+99 = ℄ Con. Walk on W

-0.5' = top Walk	4.40	348.98
℄ W	4.4	348.9
cb	4.5	348.8
¼	4.2	349.1
℄	4.3	349.0
¼	4.9	348.4
cb	5.1	348.2
E	5.3	348.0
+5	5.5	347.8

2+39 = ℄ Con. Walk on W

-5	5.9	347.4
E	5.7	347.6
cb	5.4	347.9
¼	5.0	348.3
℄	4.6	348.7
¼	4.7	348.6

cb	4.7	348.6
W	4.1	349.2
+1.4 = top Walk	4.0 W	349.26

2+74 = ℄ Con. Walk on W

-1 = top Walk	3.96	349.42
W	4.2	349.1
cb	4.7	348.6
¼	4.8	348.5
℄	4.7	348.6
¼	5.0	348.3
cb	5.7	347.6
E	6.1	347.2
+5	6.1	347.2

8+00.97 W = S.L. MEHDE 40' Wide

E	5.4	347.9
cb	5.4	347.9
¼	5.0	348.3
℄	4.7	348.6
¼	4.8	348.5
cb	4.6	348.7
W	4.0	349.3
T.P. 0.97 W	34.946 4.74	348.54

℄ MEHDE

W	0.9	348.6
cb	1.0	348.5
¼	1.1	348.4

34946

Lo		0.9	348.6
¼		1.1	348.4
cb		1.3	348.2
E.		1.3	348.2
+5		1.5	348.0

Note: From N.L. MEADE 10.685 10.43

N.L. MEADE = 0+00 to telmadge Bch

-5		1.4	348.1
E.		1.4	348.1
cb		1.5	348.0
¼		1.4	348.1
Lo		1.1	348.4
¼		1.2	348.3
cb		1.4	348.1
W		0.8	348.7

50' N

W		1.5	348.0
cb		1.8	347.7
¼		1.8	347.7
Lo		1.6	347.9
¼		2.3	347.2
cb		2.4	347.1
E.		2.8	346.7
+5		3.0	346.5

1+00

-5		3.8	345.7
E.		3.8	345.7

34946

38

cb	42	345.3
½	39	345.6
Lo	37	346.3
¼	34	346.1
cb	31	346.4
W	27	346.8

1+50

W	41	345.4
cb	44	345.1
¼	48	344.7
Lo	46	344.9
¼	49	344.6
cb	50	344.5
E.	48	344.7
+5	48	344.7

1+94 = L. Peppertree on Lo 6' in St. 1'dia.

-5	53	344.2
E.	53	344.2
+6. = tree	56	343.9
cb	59	343.6
¼	58	343.7
Lo	53	344.2
¼	53	344.2
cb	53	344.2
W	47	344.8

2+16 = L. Peppertree on E. 6' in St. 1'd.a.

	349.46		
W		5.0	344.5
cb		5.3	344.2
¼		5.6	343.9
℄		5.6	343.9
¼		6.1	343.4
cb		6.3	343.2
+4 = tree		5.9	343.6
E		6.1	343.4
2.5 wide on line			
2+24 = ℄ Con. Walk on E		5.86	343.66
	2+50		
T.P.	6.63 349.51	6.58	342.88
E		6.6	342.9
cb		6.8	342.7
¼		6.6	342.9
℄		6.2	343.3
¼		6.0	343.5
W cb		6.2	343.3
W		5.8	343.7
	3+00		
-6		8.6	340.9
W		8.6	340.9
cb		7.9	341.6
+7		7.6	341.9
¼		6.7	342.8
℄		6.8	342.7
¼		7.1	342.4

	349.51		59
cb		7.2	342.3
E		7.1	342.4
3+28 = ℄ Pepper tree on W		4' in ct.	3' dia
E		6.7	342.8
cb		7.2	342.3
¼		7.1	342.4
℄		6.7	342.8
¼		6.4	343.1
+6		8.3	341.2
cb		8.6	340.9
+6 at tree		9.1	340.4
W		9.8	339.7
+10		10.1	339.4
	3+50		
-10		11.7	337.8
W		10.7	338.8
cb		8.9	340.6
¼		6.9	342.6
℄		6.6	342.9
¼		7.0	342.5
cb		7.0	342.5
E		6.1	343.4
3+97 = ℄ Dr. Way on E		4' Back Asphalt Pav.	
-4 = Dr. Way		4.39	345.12
E		4.6	344.9
cb		5.6	343.9

℄		6.1	343.4
℄		6.3	343.2
¼		6.6	342.9
cb		7.1	342.4
W		7.7	341.8
+5		8.2	341.3
	4+50		
-5		6.1	343.4
W		5.8	343.7
cb		5.3	344.2
¼		4.9	344.6
℄		4.6	344.9
¼		4.6	344.9
cb		4.4	345.1
E		3.7	345.8
	5+00		
E		3.9	346.2
cb		3.6	345.9
¼		3.7	345.8
℄		3.5	346.0
¼		3.9	345.6
cb		4.1	345.1
W		4.6	344.9
	5+50		
W		5.6	343.9
cb		5.5	344.0

349.51

¼		4.7	344.8
℄		4.2	345.3
¼		4.9	344.6
cb		5.0	344.5
+2		5.0	344.5
+3		4.4	345.1
E		4.4	345.1
	6+00		
E		4.9	344.6
+2		5.2	344.3
+8		9.0	340.5
cb		9.3	340.2
¼		9.4	340.1
℄		9.2	340.3
¼		9.0	340.5
+8		9.6	339.9
cb		9.0	340.5
W		7.9	341.6
	6+02' = N.L. City Boundary		
W		9.7	339.8
top cb		9.99	339.52
¼		9.7	339.8
℄		9.5	340.0
¼		9.5	340.0
top cb		9.58	339.93
E		9.4	340.1

349.51 = A
092 =
348.59 = TP
4.44
35323
.01
347.22
347.20
0.02

Hawk St 6-16-27

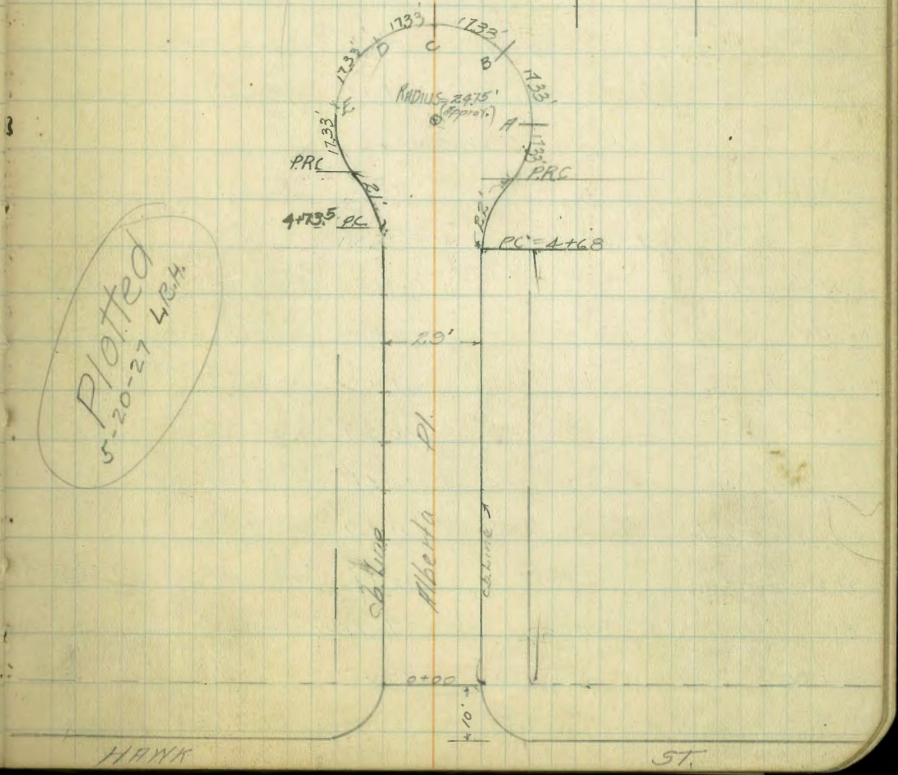
CURB LEVELS ON ALBERTA PL.
FROM HAWK ST. WEST

B.M. SE top hyd. Douglas & Hawk	4.97	270.94		266.02
10' N N cb line HAWK = 0+00				
N top cb			5.22	265.72
S " "			5.16	265.78
50' N				
S " "			4.73	266.21
N " "			4.56	266.38
100' N				
N " "			4.00	266.94
S " "			4.03	266.91
150' N				
S " "			3.56	267.38
N " "			3.32	267.62
T.P.	7.16	270.47	2.63	268.31
2+00				
N top cb			6.67	268.80
S " "			7.03	268.44
2+40				
S " "			6.07	269.40
N " "			5.99	269.48
2+60				
N " "			5.62	269.85
S " "			5.61	269.86
2+80				
S " "			5.34	270.18

270.47

41

N top cb	5.57	269.90
3+00		
N top cb	5.73	269.74
S " "	5.43	270.04
3+20		
S " "	5.79	269.68
N " "	6.23	269.24
3+40		
N " "	6.91	268.56
S " "	6.39	269.08



PLOTTED 5-20-27 L.C.H.

		276.47		
	3+60			
S top cb			7.28	268.19
N " "			7.89	267.58
	3+80			
N " "			8.91	266.56
S " "			8.31	267.16
	4+00			
S " "			9.34	266.13
N " "			9.90	265.57
	4+34			
N " "			11.87	263.60
S " "			11.17	264.30
T.P.	8.09	270.78	12.78	265.69
	4+73 = P.C. on South			
S top cb			8.81	261.97
	4+68 = P.C. on N			
N top cb			8.75	262.03
N P.R.C.			9.50	261.28
A on top cb			9.92	260.86
B " " "			10.29	260.49
C " " "			10.45	260.33
C on top Grate			11.49	259.29
D on top cb			10.18	260.60
E " " "			9.90	260.88
S.P.R.C. " "			9.63	261.15
T.P.	5.09	270.85	5.02	265.76

270.85

4

Dunbar Harris

T.P. = Chk. on B.M. S.E. top Hyd. St. 487 265.98

265.97

0.04 in Error.

Walker 5-1627

LEVELS ON Improvements ON FRANKLIN Ave From 30th to 28th St.

N.Y. B.P. Woolman + 30th	1.19	89.27		88.08	
				89.2	
S.L. at Bottom of Wall on Ground	0+00 = Wh. 30th = East end Con. Wall on South (Top is 1.4' Higher)		4.9	84.3	
S top Cb.			5.16	84.0	84.06
N " "			5.16	84.0	84.06
T.P.	6.08	93.13	7.17	87.95	Franklin + 30th SW. top Hydt.
				93.1	
0+17 = ℄ Con. steps on South			7.53	85.6	
0+56 = Wedge Con. Wall on South.	Rod taken on Ground top is 1.4' Higher		6.0	87.1	
1+49 = ℄ Con. Steps on South 4' Wide on line					
on dirt at steps			7.4	90.7	
on top of 1st Step			1.83	91.3	
			top step = 4.95	88.1	
2+38 = ℄ Con. steps on N 1' Back			dirt = 5.5	87.6	
3+12 = ℄ Con. Walk on N 0.50' Back			4.26	86.9	3' Wide
3+49 = " " " " " "			4.27	86.7	" "
4+89 = " " " " 1' "			4.70	86.4	" "
T.P.	6.00	98.48	0.65	97.98	Franklin + 29th SW top Hydt.
				98.5	
0+00 = Wh. 29th St. = East end of Con. Ret. Wall on South (top of Wall is 4.3' Higher)					
Ground at Wall			8.1	90.4	
0+50 = ℄ Con. Steps on South 1' in St.				Wall is 0.5' in St.	
Rod on Ground at step			7.0	91.5	
" " step			6.09	92.4	
1+00 = ℄ Con. Walk on N 1' back			8.87	89.6	
1+26 = ℄ " Steps on South 1' in St.					
Ground =			5.0	93.5	
top of step =			4.39	94.1	
1+33 = ℄ Con. Walk on N 4' Back			8.38	90.1	2.5 Wide

98.48

98.5

1+49 = West end con. Wall on South 0.5 in St. (top Wall is 3.5' Higher)			
Ground at Wall =	4.4	94.1	
1+65 = ℄ Con. Walk on N 3.5 Back	7.71	90.8	3.5' Wide
1+98 = " " " " " on line	6.69	91.8	2' "
2+61 = " " " " " 0.7 Back (top is 2.2' Higher)	5.00	93.5	4' "
2+75 = East end Con. Ret. Wall	5.2	93.3	on Ground
3+24 = ℄ Con. Steps on South 0.5' in St.			6' Wide
Ground =	2.6	95.9	
top Step =	1.97	96.5	
3+28 = ℄ Con. Steps on N 0.5' back			8' Wide
Ground =	5.6	92.9	
top steps	4.98	93.5	
3+62 = West end Con. Wall on N 0.5' in St. (top is 2.1' Higher)			
Ground =	6.5	92.0	
4+25 = ℄ Con. Walk on N 1' Back	8.29	90.2	3' Wide
4+75 = ℄ " " " N 1.5' in St.	10.45	88.0	3' "
T.P. 44	9.26	10.21	88.27
El. 28th			92.7
S top Cb.	7.29	85.4	85.39
N " "	8.57	84.1	84.11
Sht. on NE. BP Woolman + 28th	1.56	91.12	
		91.05 = Ck.	
		0.07 - Error	

Walker Ishelle Kanouse 9-14-71

X. Section Chamoune Ave 60' Wide

From S.L. Thorn to N.L. Quince

12.'c65 9.'75

N.W. BP Myrtle + Chaumouse	2.63	338.57		335.81
TP	1.97	334.33	5.56	332.96
	S.L. Thorn = 0+00			
W			1.9	332.4
W top cb			1.97	332.36
" Gutter			2.1	332.2
" ¼		Reduced	2.5	331.8
cb			2.3	332.0
E ¼	Plotted by W.M.M.		2.5	331.8
" Gut			2.9	331.4
" top cb			2.44	331.89
E			2.3	332.0
	0+50			
E			3.1	331.2
cb			3.1	331.2
¼			2.9	331.4
℄			3.0	331.3
¼			3.1	331.2
cb			2.9	331.4
W			2.6	331.7
	1+00			
W			3.5	330.8
cb			3.8	330.5
¼			4.1	330.2
℄			4.1	330.2

¼		3.7	330.6
cb		3.9	330.4
E		3.8	330.5
	1+50		
E		4.8	329.5
cb		4.4	329.9
¼		4.1	330.2
℄		4.5	329.8
¼		4.7	329.6
cb		4.8	329.5
W		4.7	329.6
1+38 = ℄ Con Dr. on West	0.5' Back	4.64	329.69 ✓ Ribbon Drive
1+79 = ℄ Con Walk on West	0.4' Back.	4.90	329.43 ✓ Rbl.
	2+00		
W		5.5	328.8
cb		5.4	328.9
¼		5.6	328.7
℄		5.6	328.7
¼		5.7	328.6
cb		5.7	328.6
E		5.6	328.7
2+24 = ℄ Con. Dr. on W	0.5' Back.	5.49	328.84 ✓ Solid Drive
	2+50		
E		6.5	327.8
cb		6.7	328.1
¼		6.3	328.0

℄		6.3	328.0
¼		6.4	327.9
cb		6.3	328.0
W		6.0	328.3
	3+00		
W		6.6	327.7
cb		7.0	327.3
¼		7.2	327.1
℄		6.9	327.4
¼		7.1	327.2
cb		7.2	327.1
E		7.2	327.1
	3+50		
E		7.8	326.5
cb		7.7	326.6
¼		7.7	326.6
℄		7.9	326.4
¼		8.0	326.3
cb		7.9	326.4
W		8.0	326.3
	4+00		
W		8.8	325.5
cb		8.8	325.5
¼		8.7	325.6
℄		8.6	325.7
¼		8.6	325.7

plotted & reduced by W.M.McC.

cb		8.5	325.8
E		8.4	325.9
	4+50		
E		9.2	325.1
cb		9.5	324.8
¼		9.5	324.8
℄		9.8	324.5
¼		9.8	324.5
cb		9.8	324.5
W		9.7	324.6
4+67 = ℄ Con Walk on East	on Line	9.71	324.62
4+91 = " " Drive " "	on Line	10.16	324.17
	5+00		
W		10.8	323.5
cb		10.8	323.5
¼		11.0	323.3
℄		10.7	323.6
¼		10.8	323.5
cb		10.8	323.5
E		10.6	323.7
	5+50		
E		12.1	322.2
cb		12.1	322.2
¼		12.1	322.2
℄		12.3	322.0
¼		12.1	322.2

Ribbon Drive

cb.		12.1	322.2
W		12.1	322.2

6+00 = Nb. Redwood 60' Wide 10' cbs. 10' cbs.

W		13.5	320.8
cb		13.4	320.9
¼		13.4	320.9
℄		13.4	320.9
¼		13.3	321.0
cb		13.4	320.9
E		13.5	320.8
T.P.	2.32 323.66	12.99	321.34

N cb

E.		31	320.6
cb.		29	320.8
¼		28	320.9
℄		29	320.8
¼		28	320.9
cb		37	320.5
W		30	320.7

N ¼

W		36	320.1
cb.		31	320.6
¼		31	320.6
℄		33	320.4
¼		37	320.5
cb		37	320.5

E		34	320.3

E

E		36	320.1
cb		35	320.2
¼		35	320.2
℄		35	320.2
¼		36	320.1
cb		35	320.2
W		35	320.2

S ¼

W		41	319.6
cb		40	319.7
¼		37	320.0
℄		38	319.9
¼		37	320.0
cb		38	319.9
E		39	319.8

S cb.

E.		42	319.5
cb.		41	31.96
¼		40	319.7
℄		41	3196
¼		40	3197
cb.		42	319.5
W		41	3196

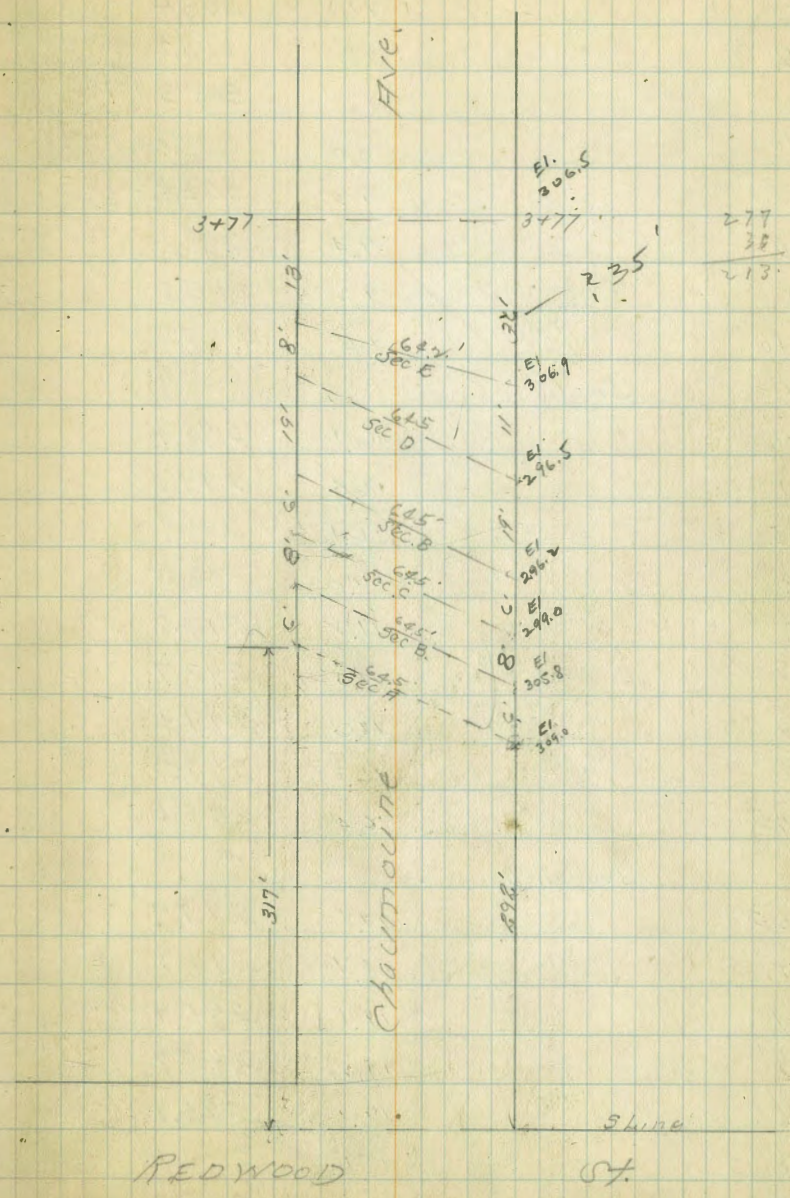
S Line Redwood on W = 0+00

W	4.6	319.1
cb.	4.5	319.2
¼	4.3	319.4
℄	4.5	319.2
¼	4.3	319.4
cb	4.5	319.2
E	4.4	319.3
22' South = North end Con. Wall on East 0.1 Back.		
E at Base of Wall	4.8	318.9
cb.	4.7	319.0
¼	4.9	318.8
℄	4.9	318.8
¼	4.9	318.8
cb	5.1	318.6
W	5.3	318.4
0+50		
W	6.1	317.6
cb	6.0	317.7
¼	5.8	317.9
℄	5.7	318.0
¼	5.7	318.0
cb.	5.6	318.1
E at Wall	5.6	318.1
1+00		
E " "	6.9	316.8
cb.	7.1	316.6

¼	7.1	3166
cb.	7.7	3165
¼	7.5	3162
cb.	7.6	3161
W	8.0	3157
+5	8.2	3155
1+46 = South end Con Wall on East of Back.		
-5	10.0	3137
W	9.7	3140
cb.	9.0	3147
¼	8.7	3150
℄	8.7	3150
¼	8.6	3151
cb.	8.5	3152
E	8.3	3154
2+00		
E	9.7	3140
cb.	9.8	3139
¼	10.2	3135
℄	10.3	3134
¼	10.7	3130
cb.	10.9	3128
W	11.1	3126
+5	11.3	3124
2+50		
-5	13.3	3104

3+366

W			13.1	310.6
cb.			12.4	311.3
℄			12.1	311.6
℄			11.8	311.9
℄			11.3	312.4
cb.			10.9	312.8
E.			10.8	312.9
	2+99			
E			12.1	311.6
cb			12.4	311.3
℄			12.6	311.1
TP	4.08	314.99	12.75	310.91
℄			4.5	310.5
℄			4.8	310.2
cb			5.2	309.8
W			6.0	309.0
	Sec A			
W			6.0	309.0
cb.			5.8	309.2
℄			5.1	309.9
℄			5.0	310.0
℄			4.6	310.4
cb.			4.4	310.6
E			4.4	310.6
	Sec B.			
TP			9.6	305.4



E	9.6	305.4
cb.	9.8	305.2
¼	9.7	305.3
℄	10.0	305.0
¼	9.2	305.8
cb	9.4	305.6
W	9.2	305.8
+10	9.5	305.5
Section C		
-25	16.1	298.9
W	16.0	299.0
cb.	16.1	298.9
¼	17.0	298.0
℄	17.2	297.8
¼	17.3	297.7
cb	17.6	297.4
E	16.3	298.7
+25	16.4	298.6
Section B.		
-25	19.1	295.9
E.	18.7	296.3
cb	19.1	295.9
¼	19.2	295.8
℄	19.1	295.9
¼	18.9	296.1
cb	19.2	295.8

W	18.8	296.2
+25	18.7	296.3
Section D		
-25	18.3	296.7
W	18.5	296.5
cb	18.4	296.6
¼	18.5	296.5
℄	18.6	296.4
¼	18.6	296.4
cb	18.7	296.3
E	18.9	296.1
+25	18.7	296.3
Section E		
-5	7.9	307.1
E	12.3	302.7
+8	7.4	307.6
cb	7.7	307.3
¼	7.8	307.2
℄	7.1	307.9
¼	7.7	307.3
cb	7.6	307.4
W	8.1	306.9
+10	8.7	306.3
3+77		
W	8.5	306.5
cb.	8.3	306.7

℄		8.1	306.9
℄		7.8	307.2
℄		7.6	307.4
cb		8.0	307.0
+6		9.0	306.0
E		7.1	307.9
	3+85		
E		7.5	307.5
cb		7.9	307.1
℄		8.1	306.9
℄		8.4	306.6
℄		8.5	306.5
cb		8.5	306.5
W		8.7	306.3
	4+40		
W		10.6	304.6
cb		11.3	303.7
℄		11.0	304.0
℄		11.1	303.9
℄		11.1	303.9
cb		11.2	303.8
E		11.3	303.7
+5		10.3	304.7
	4+50		
-5		12.1	302.9
E		11.9	303.1

cb.		11.5	303.5
℄		11.3	303.7
℄		11.4	303.6
℄		11.5	303.5
cb		11.6	303.4
W		12.0	303.0
+5		12.2	302.8
	5+00		
+5		14.5	300.5
W		14.2	300.8
cb.		13.7	301.3
℄		13.5	301.5
℄		13.3	301.7
℄		13.1	301.9
cb.		13.2	301.8
E		13.3	301.7
+5		13.3	301.7
	5+50		
-5		14.2	298.8
E		16.2	299.8
cb		14.6	300.4
℄		14.7	300.3
℄		14.9	300.1
℄		15.1	299.9
cb		15.6	299.4
W		15.4	299.1
+5		16.1	298.9

Plotted & Reduced by W. M. McC.

31499-T
0371-
31478=TP
1324+
37802=T
0370-
37762=TP
1204
33966
384
33584
33589=BM.
005 in Error

20' wide X See Alley Blk. 226 U.H. 9-30-27 Miller

Bet Univ. Ave. & Essex - Vermont to Richmond

B.M.	5.11	294.84		289.73	S.W. Univ Ave & Vermont
		00' E. line Vermont			
N			5.06	289.78	Pavmt
E			5.42	289.42	"
S			5.11	289.73	"
T.P.	6.13	295.69	5.28	289.56	
	0+60' E Garage on N. dirt floor			Garage on S dirt 2' Back	
S			5.6	290.1	
E			5.7	290.0	
N			5.7	290.0	
	90' E Garage on N. dirt floor			2.0 in Alley	
N			5.8	289.9	
E			5.5	290.2	
S			5.7	290.0	
	125' E Public Garage on N cmt floor 8' Back				
S			5.6	290.1	
E			5.5	290.2	
N			5.0	290.7	
+8			4.4	291.3	floor
	165' E Garage on N 1.3 in Alley dirt floor				
N			5.2	290.5	
E			5.3	290.4	
S			5.2	290.5	✓

295.69

(51)

205' E garage on S. dirt floor 0.2 in Alley

S	4.7	291.0
E	4.8	290.9
N	4.5	291.2
250' E		
N	4.3	291.4
E	4.3	291.4
S	4.2	291.5
300' E		
S	3.4	292.3
E	3.6	292.1
N	3.4	292.3
333' E garage on S. dirt floor 0.3 in Alley		
N	3.2	292.5
E	3.2	292.5
S	3.2	292.5
364' E & 3 Garages on S. cmt floors 0.7 in Alley		
S	2.6	293.1 floor
E	2.7	293.0
N	2.7	293.0
383' E Garage on N dirt floor 0.8 Back Garage on S dirt floor 0.3 in Alley		
N	2.1	293.6
E	2.6	293.1
S	2.4	293.3

295.69

394'E garage on N. dirt floor 0.8 Back

S		2.4	293.3
C		2.5	293.2
N		2.1	293.6
T.P.	7.43 301.00	2.12	293.57

446'E garage on N cmt floor 0.4 Back

N		6.8	294.2
C		7.4	293.6
S		7.1	293.9

garage on S dirt floor 1.0 Back
439'E double garage on N " " 0.3 Back

S		6.9	294.1
C		6.9	294.1
N		6.5	294.5

470'E

N		6.0	295.0
C		6.2	294.8
S		6.2	294.8

garage on N wood floor 4.6 Back
489'E Rear cmt apron approach to garages 0.7 in Alley apron 2' wide

S		5.6	295.4 Ridge apron
C		5.9	295.1
N		5.7	295.3

520'E. = E. end cmt apron on S. 0.8 in Alley

N		5.6	295.4
C		5.6	295.4
S		5.3	295.7 cmt apron

297.15 BM. S.W. Richmond & Univ gone to checks 0.01 low

301.00

538'E garage on S dirt floor 2.0 Back

S		5.4	295.6
C		5.3	295.7
N		5.4	295.6

580'E

N		4.6	296.4
C		4.7	296.3
S		4.9	296.1

601.5 E=W. Line Richmond

S		4.54	296.46 cmt el Return
C		4.6	296.4
N		4.52	296.48 cmt el Return

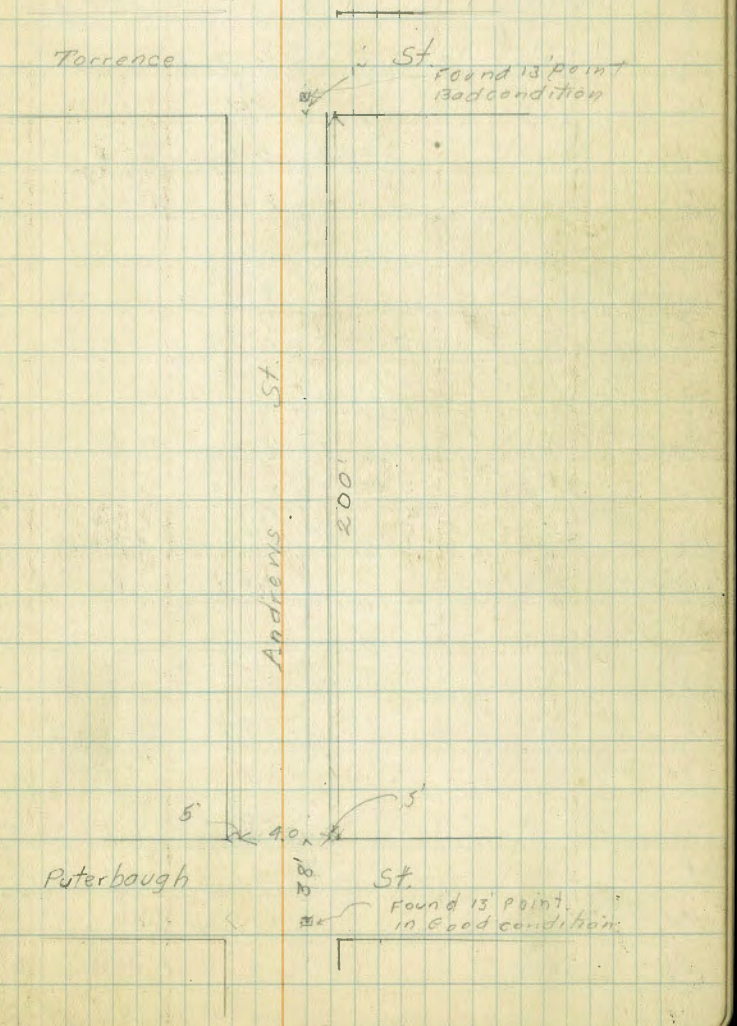
Bliss
Isabell
Morgan
12/19-7

X Section of Andrews St. Middletown
Addition from the East line of Peterbaugh to the West line of Torrence

Pierce St	T	X	-	Elev
B.M. S.W.B.P. Kettner & Andrews	13.00	75.78		62.78
T.P.	12.04	87.80	0.02	75.76
T.P.	12.33	99.91	0.22	87.58
T.P.	12.72	112.50	0.13	99.78
T.P.	12.99	125.34	0.15	112.35
T.P.	13.03	137.99	0.38	129.96
B.M. Spike in Pole S.W. Andrews & Torrence			10.02	127.97
T.P.	12.79	150.63	0.15	137.84
T.P.	12.98	163.39	0.22	150.41
Set B.M. Nail & Tack in Walk	North Side of		3.59	159.85
T.P.	12.98	176.30	0.07	163.32
T.P.	12.89	189.18	0.01	176.29
T.P.	12.81	201.79	0.20	188.98
Set B.M. 13' Point Peterbaugh & Andrews			0.28	201.51
T.P.	6.22	207.73	0.28	201.51
		0+00 = E. Line of Peterbaugh		
S.			0.3	207.4
cb			1.7	206.0
+6			3.9	203.8
1/4			7.4	200.3
℄			13.8	193.9
1/4			20.7	187.0
cb			28.	179.7
N			51.7	176.0
N+20			43.5	164.2

53

129.90 Spike



	+	↑ 207.73	−	E 10.1
		05' East of the East Line of Peterboro		
N-20			44.2	163.5
N			32.4	175.3
cb			29.9	178.3
1/4			21.6	186.1
℄			15.2	192.5
1/4			10.8	196.9
+6			7.1	200.6
cb			3.2	204.5
S			1.6	206.1
		15' East		
S			7.5	200.2
cb			9.7	198.0
1/4			13.9	193.8
℄			18.0	189.7
1/4			23.8	183.9
cb			30.8	176.9
N			33.1	174.6
N+30			96.7	161.0
		34' East		
N-30			49.0	158.7
N			37.0	170.7
cb			34.4	173.3
1/4			30.0	177.7
℄			26.1	181.6
1/4			21.5	186.2
cb			18.3	189.4
S			16.4	191.3

T.P. 2.11	197.81	12.03	195.70
		53' East	
S		9.3	188.5
cb		12.1	185.7
1/4		16.6	181.2
℄		22.0	175.8
1/4		26.0	171.8
cb		30.4	167.4
N		32.5	165.3
+20		38.6	159.2
+30		41.5	156.3
		61' East	
N-30		38.5	159.3
-20		36.0	161.8
N		30.6	167.2
cb		29.0	168.8
1/4		24.5	173.3
℄		21.0	176.8
1/4		16.5	181.3
cb		11.9	185.9
S		10.0	187.8
		79' East	
S		6.3	191.5
cb		8.3	189.5
1/4		13.6	184.2
℄		17.5	180.3

	+	↑ 197.61	−	Elev 177.8
1/4			20.0	177.8
cb			23.0	174.8
N			24.1	173.7
N+20			29.5	168.3
		95' East		
N-20			24.0	173.8
N			20.5	177.3
cb			19.4	178.4
1/4			17.0	180.8
℄			14.4	183.4
1/4			9.0	188.4
℄			6.9	191.9
cb			4.8	193.0
S			3.1	194.7
		100' East		
S			1.1	196.7
cb			3.6	194.2
℄			6.0	191.8
1/4			8.4	189.4
℄			13.2	184.6
1/4			15.7	182.1
cb			18.1	179.7
N			19.2	178.6
N+20			22.5	175.3
		113' East		
N-20			19.5	178.3

	+	↑ 197.86	−	Elev
N			16.2	181.6
cb			15.5	182.3
1/4			12.5	185.3
℄			10.2	187.6
1/4			6.0	191.8
T.P.	12.70	10.46	0.05	197.76
cb			12.7	198.3
S			9.9	201.1
		125' East		
S			7.2	203.8
cb			9.3	201.7
1/4			13.8	197.2
℄			18.8	192.2
1/4			22.5	188.5
cb			24.8	186.2
N			25.7	185.3
N+20			30.2	177.8
		138' East		
N-20			25.8	185.2
N			23.2	187.8
cb			22.7	188.3
1/4			20.0	191.0
℄			16.2	194.8
1/4			10.5	200.5
cb			6.5	204.5
S			4.1	206.9

	+	π	−	Elev.
		210.96		
T.P	9.04	216.90	3.10	207.36
		159 East		
S			9.6	211.8
cb			7.0	209.4
1/4			12.3	204.1
℄			17.2	199.2
1/4			20.5	195.9
℄cb			23.2	193.2
N			29.2	192.2
N+20			28.0	188.4
		183 E =		
N-30			30.2	186.2
N-20			27.0	189.4
N			21.0	195.4
cb			20.2	196.2
1/4			18.0	198.4
℄			14.8	201.6
1/4			10.0	206.4
cb			4.7	211.7
S			2.5	213.9
		200 E. = W'ly L Torrence.		
S			1.3	215.1
cb			4.3	212.1
1/4			8.5	207.9
℄			12.1	204.3
1/4			15.6	200.8

cb			19.6	196.8
N			21.2	195.2
N+20			28.7	187.7
N+30			32.5	183.9
T.P.	0.39	205.13	11.66	209.74
T.P.	0.03	192.4	12.95	192.18
T.P.	0.08	179.22	13.07	179.14
T.P.	0.18	166.69	12.71	166.51
T.P.	0.70	154.60	12.79	153.90
T.P.	0.89	142.91	12.58	142.02
Top. Re for in B.E Harwood & Andrews			15.91	127.50
B.M. on Pole			15.05	2.75 Roof 127.86

Not Sought
Check this Bench
by 1.54 Pole
Mosthaven Sunk.

McHugh Flood Runner 9/11/28

X section Puterbaugh St

S.Ely Line Of Andrews to N.Wly. Line Wellborn St.

street 50' wide 10'cbs 2.5'quarters

0+00 = N.L. Wellborn

B.M. on 13' Hub Puterbaugh & Andrews 201.51

T P	12.59	214.10		201.51
3+05 = S.L. Andrews		This station is (5.6 N. of S. Line of Andrews on W (6.7 " " " " " " E Not on St Line		
WL			13.2	200.9
cb		See Page 63 for New Notes F.B.M.	11.5	202.6
¼			10.3	203.8
℄			9.2	204.9
¼			8.7	205.4
cb			8.1	206.0
EL			8.5	205.6
2+75				
EL		O.K.	0.2	213.9
cb			1.3	212.8
¼			2.0	212.1
℄			3.0	211.1
¼			3.9	210.2
cb			5.2	208.9
WL			7.0	207.1
T.P.	12.26	226.28	0.08	214.02
2+50				
WL			15.2	211.1
cb		O.K.	13.0	213.3
¼			11.6	214.7
℄			10.4	215.9

Andrews street has been closed 5' on each side, making Puterbaugh 305' long see page 53 this book.

	+	T. 226.28	−	
¼			9.0	217.3
cb			7.1	219.2
EL			5.0	221.3
2+25				
EL			1.8	224.5
cb			3.9	222.4
¼		O.K.	6.0	220.3
℄			7.6	218.7
¼			9.0	217.3
cb			10.2	216.1
WL			12.1	214.2
T.P.	9.94	235.56	0.66	225.62
2+00				
WL			18.9	216.7
cb			16.0	219.6
¼			15.0	220.6
℄			12.2	223.4
¼			10.2	225.4
cb			8.8	226.8
EL			7.1	228.5

1+74 = start of Concrete retaining wall on East 7' High. Situated on East Line

	+	℄ 235.56	−	
EL			4.6	231.0
cb			6.2	229.4
¼			8.1	227.5
℄			10.9	224.7
¼			11.9	223.7
cb			12.0	223.6
+7			13.2	222.4
WL			14.7	220.9
+13			19.5	216.1
1+42 = ℄ cement walk 3' wide & as back leading to				
stucco residence 8' Back (on west)				
WL-0.5 Top of walk			12.60	223.0
WL			12.7	222.9
cb			12.0	223.6
¼			9.2	226.4
℄			7.6	228.0
¼			4.9	230.7
cb			3.9	231.7
EL Wall 4.0' High Here			1.4	234.2
1+09 = ℄ cement walk 11' wide & 6.5' Back				
Leading to same stucco Residence on west.				
WL-6.5 on walk			12.83	
1+00 = End of concrete retaining				
Wall on East				
EL			4.1	231.5

	+	℄ 235.56	−	
cb			6.0	229.6
¼			6.9	228.7
℄			7.7	227.9
¼			9.5	226.1
cb			12.4	223.2
WL			16.0	219.6
T.P	1.01	223.72	12.85	222.71
0+97				
WL			13.5	210.4
+9			11.2	212.5
cb			4.0	219.7
¼			2.5	221.2
℄	0.5			224.2
¼	2.5			226.2
cb	5.2			228.9
EL	7.2			230.9
0+90 = ℄ Wood House 1' Back 12' Wide				
0+70				
EL			1.9	221.8
cb			7.0	216.7
¼			9.8	213.9
+2			12.7	211.0
℄			14.2	209.5
¼			14.9	208.8
cb			15.4	208.3

	+	℄ 223.72	−	
WL			15.7	208.0
0+58				
WL-10			31.3	192.4
WL			31.3	192.4
+6			24.7	199.0
cb			22.3	201.4
¼			18.2	205.5
+5			17.9	205.8
℄			14.3	209.4
+5			14.1	209.6
¼			11.0	212.7
cb			5.4	218.3
EL			1.4	222.3
0+45				
EL			8.3	215.4
cb			11.2	212.5
¼			13.4	210.3
+4			14.9	208.8
℄			18.4	205.3
¼			19.0	204.7
cb			28.7	195.0
WL			34.9	188.8
+10			38.5	185.2
0+25				
WL-10			40.0	183.7

	+	℄ 223.72	−	
WL			39.8	183.9
+4			38.5	185.2
cb			33.6	190.1
+1			29.6	194.1
¼			28.1	195.6
℄			27.7	196.0
¼			23.7	200.0
cb			21.6	202.1
EL			17.8	205.9
0+00 = WL Wellborn St				
EL			31.3	192.4
cb			30.1	193.6
¼			32.0	191.7
℄			34.7	189.0
¼			37.8	185.9
cb			40.3	183.4
+5			40.3	183.4
WL			42.9	180.8
+10			46.3	177.4
T.P.	1.95	224.66	1.01	222.71
T.P.	0.57	212.71	12.52	212.14
T.P.			11.23	201.48

201.51
201.48
.03

McHugh Flood Rawlins 1/11/28

X section Alley Mission Hills No. 3

				+	T	−
B M	Trias x Ft Stockton N.E. BP.				272.38	
	0+00 = W.L. with ERBy 267.06					
T.P.	657	27363	267.06			
6+49.31	on paving = El Trias					
S cb			4.83	68.8		
Gut			4.85	68.7		
℄			5.06	68.5		
Gut			4.79	68.8		
N cb			4.70	68.9		
T. P.	4.06	272.38	5.31	268.32		
5+90	= ℄ double garage on South 16' wide					
NL			4.2	68.2		
℄			4.1	68.3		
SL			4.0	68.4		
+1.6	Edge of Apron		3.74	68.6		
5+63	= ℄ double garage on South Apron 15' wide					
	= ℄ cement driveway on North 9.5' "					
SL-2	Edge of Apron		4.20	68.2		
SL			4.2	68.2		
℄			4.4	68.0		
NL			4.4	68.0		
NL+1.5	on concrete		4.33	68.1		
5+09	= ℄ double garage on south Apron 15' wide					
NL			5.0	67.4		
℄			5.0	67.4		
SL			5.0	67.4		
+2	Edge of Apron		4.86	67.5		
4+60 = ℄ double garage on South Apron 18' wide						
S.L.	Edge of Apron		5.30	67.1		
℄			5.1	67.3		
NL			5.3	67.1		
4+40 = ℄ garage on North Apron 9.6' wide						
NL-2	Edge of Apron		5.31	67.1		
4+07 = ℄ garage on south 10' wide						
NL			5.7	66.7		
℄			5.5	66.9		
SL			5.6	66.8		
+3.5	concrete floor		5.48	66.9		
3+90 = ℄ garage on North Floor 9' wide						
SL			5.4	67.0		
+3			5.5	66.9		
℄			5.6	66.8		
NL			5.8	66.6		
+2	concrete Floor		5.55	66.8		
T.P.	4.70	271.08	6.00	266.38		
3+79 = ℄ garage on North 8' wide						
NL-3	on concrete Floor		4.44	66.6		
3+62 = ℄ double garage on South Apron 23' wide						
NL			46	66.5		
℄			46	66.5		

2711

	+	⊼	−	
SL	on Concrete Apron	4.87		66,2
3+40	= ℄ garage on North Floor 7' wide			
NL+3	Edge of Floor		4.92	66,7
3+07	= ℄ garage on south Door 7.8 wide			
SL-3	concrete floor		5.24	65,9
SL			5.2	65,9
℄			5.0	66,1
NL			5.0	66,1
2+64	= ℄ garage on North Apron 16.4 wide			
NL-2	on Edge of Apron		5.16	65,9
NL			5.3	65,8
℄			5.1	66,0
SL			5.2	65,9
2+07	= ℄ garage on south Apron 7' wide			
	= ℄ " " North Door wide			
SL-3	Edge of Apron		5.69	65,4
SL			5.6	65,5
℄			5.4	65,7
NL			5.4	65,7
+5	concrete floor		4.89	66,2
1+62	= ℄ garage on North Apron 9.6 wide			
	= ℄ double garage on South doors 16' wide			
NL-3	Edge of Apron		6.06	65,0
NL			6.2	64,9
℄			6.0	65,1

	+	⊼	−	
SL			6.2	64,9
+1	concrete floor		6.17	64,9
T.P.	340	267.84	6.64	264.44
1+08 = ℄ garage on south Door 10' wide				
SL-2.5	concrete floor		3.22	64,6
SL			3.5	64,3
℄			4.0	63,8
NL			4.9	62,9
0+78 = End of concrete retaining wall on North Line				
Top of wall			4.82	63,0
0+60				
NL. Top of wall			5.09	62,7
N.L. Ground			5.3	62,5
℄			4.8	63,0
SL.			4.5	63,3
0+10				
SL			5.0	62,8
℄			6.6	61,2
NL ground			5.9	61,9
NL Top of wall			5.73	62,1
0+00 = WL Witherby on paving				
N. Top of Cb			6.47	~~61,3~~
Gut			6.53	~~61,3~~
℄			7.89	60,0
Gut			7.16	60,6

⊼ 267.55 / 259.40 2 62.11 5.04

⊼ 267.55 / 259.40

⊼ 267.55 / 260.81 6.74 checks S.Cb within 01

259.46 / 259.40

67.8

	+	↑	−	
Top of Cb			7.14	60.7
T.P.	7.59	268.24	7.19	260.65
T.P.	8.31	270.95	5.60	262.64
T.P.			3.91	267.04

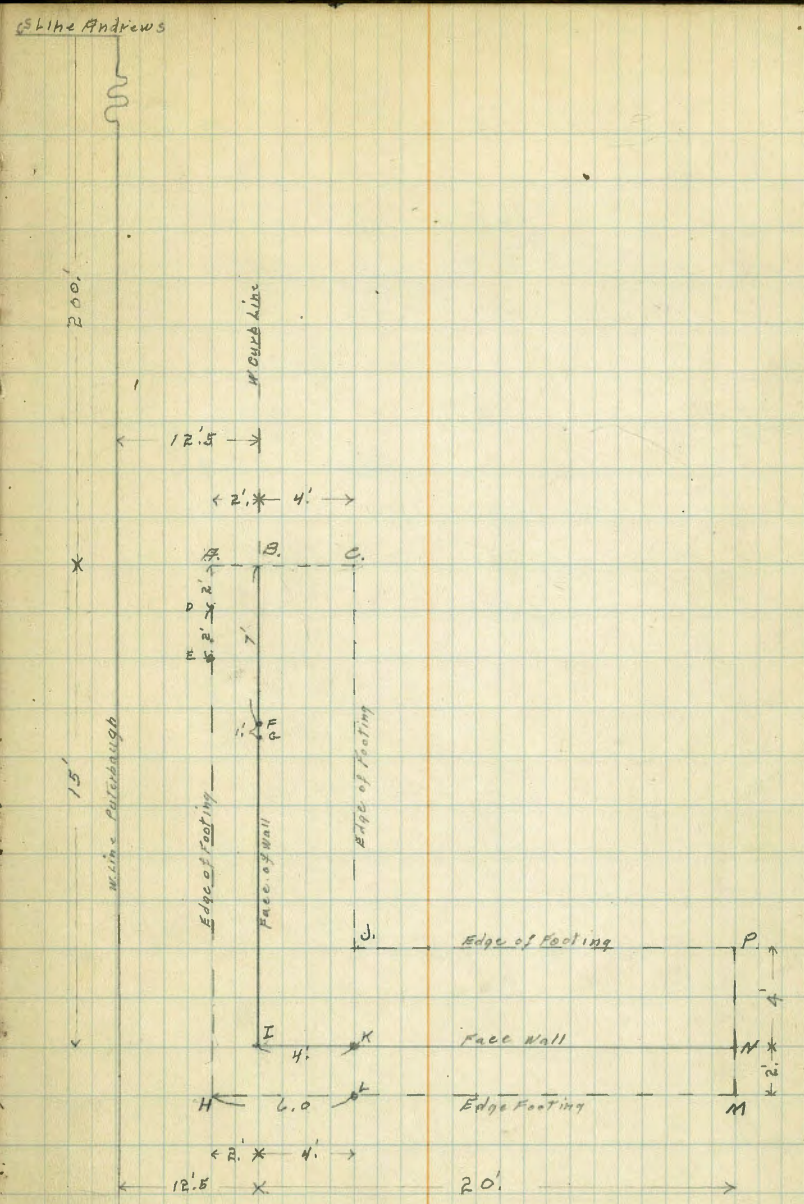
BM = 267.06
267.04
0.02

Levels for Retaining Wall
Puterbaugh Bet. Andrews + Wellborn
Ref. X. See Puterbaugh. Page 57.

3-6-28
Miller

13' Hub Andrews
+ Puterbaugh

B.M.	12.28	213.79		201.51
	300' N. of Wellborn = S. Line Andrews			
W			11.6	
el			10.3	
1/4			9.5	
C			8.5	
3/4			7.6	
el			6.7	
E.			6.4	
	Sta 2+75 N Page 57 OK			
T.P.	12.91	225.89	0.81	212.98
	Sta 2+50 O.K.			
T.P.	3.82.	X 228.48	1.23	224.66
A			7.2	221.3
B			6.5	222.0
C			4.9	223.6
2'S. of A=D			7.7	220.8
2'S. of D=E			17.0	211.5
7'S. of B=F			9.7	218.8
7'S of F=G			17.0	211.5
H			20.0	208.5
I			18.0	210.5
J.			10.6	217.9
4'E. of I=K			13.4	215.1
6'E of H=L			14.5	214.0
M			10.0	218.5
N			9.0	219.5



X 228.48

P = 7.2 221.3

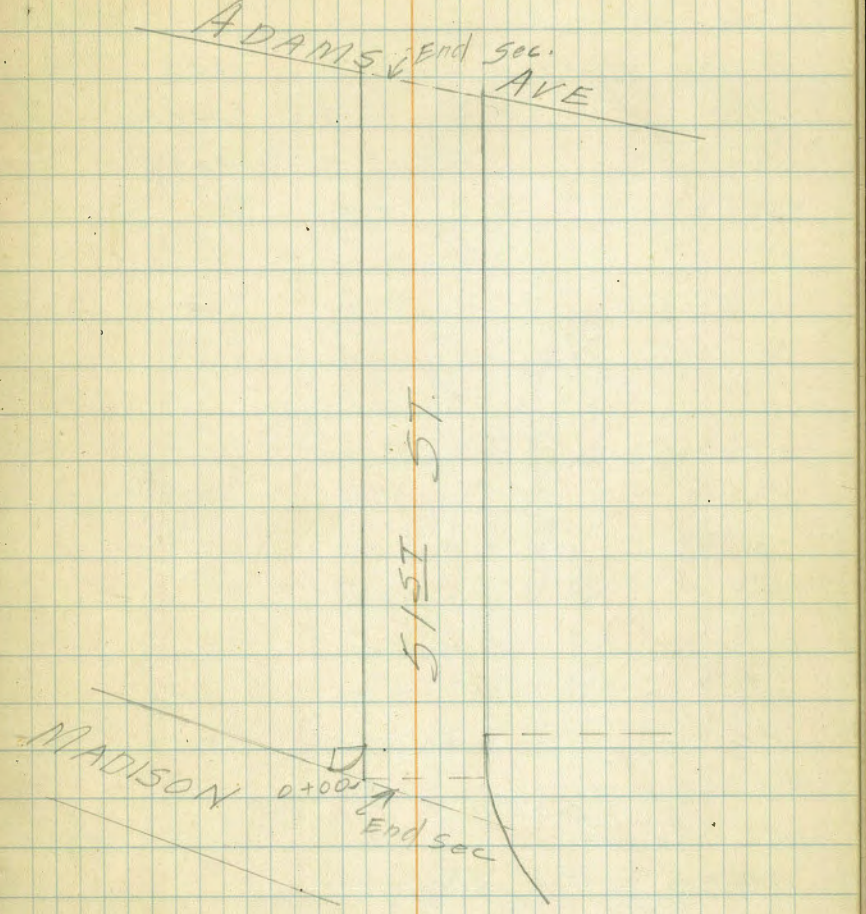
3-20-24 Miller

Levels for Water Pipe on Guy St. 10' S.W. of

B.M.	12.42	151.91		139.49	Northerly Cor Wellborn & Linwood
N. Line Wellborn/~~Linwood~~ St.			3.6	148.3	
0+10			2.6	149.3	
0+18			2.9	149.0	
0+24			3.7	148.2	
0+38			0.3	151.6	
T.P.	12.90	164.74	0.07	151.84	
0+40			12.8	151.9	
0+45			10.1	154.6	
0+52			6.7	158.0	
T.P.	11.86	175.59	1.01	163.73	
0+64			10.3	165.4	
0+64			4.1	169.6	
0+71			5.6	170.1	
T.P.	9.53	82.08	3.04	172.55	
0+78			5.6	176.5	
1400=200' S. of Andrews			3.7	178.4	

X Sec. 51st St - Madison to Adams

64



X Section 51st From Madison to Adams.

60' street 40' Roadway 10' cbs.

BM	5.85	394.58	386.73	SW 70' tie Madison & Alter
End Sec.				
21½'W (on diag)		EC NW ret.	7.9	389.7
14.18'W		"	4.8	387.8
W.L.			5.3	387.3
cb			5.5	
¼			5.6	
℄			5.7	386.9
¼			6.2	
+5			6.5	
+7			7.2	
cb			7.4	
+5			8.4	
+7			8.5	
+8			8.0	
+9			7.2	
E.L.			7.2	385.4
9'E on diag		Int. with NE ret.	7.4	
11.5'E		"	7.1	
.0+00 = N.L. Madison				
5'E		Int. with NE ret	6.5	
2'E			6.6	
E.L.			6.9	385.7
+4			6.8	
+6			7.7	
+9			7.7	
cb			7.4	

Plotted 7-2-28 G.B. Keough

end	0+00	392.58	
E cb	+2	6.8	
	+8	6.3	
	¼	6.2	
	+7	5.7	
	℄	5.6	387.0
	¼	5.6	
	+4	5.7	
	cb	5.5	
	+7	5.2	
	W.L.	5.2	387.4
0+21½	= EC NW ret.		
W.L.		4.4	387.2
	+3	5.7	
	cb	5.3	
	+5	5.5	
	¼	5.5	
	+5	5.6	
	+9	5.4	
	℄	5.5	387.1
	¼	6.2	
	+5	6.7	
	+6	7.4	
	+7	7.3	
	cb	6.5	
	+6	6.5	
E.L.		6.2	386.4

0+21 18	392.58		
1' E Int with N.E ret.		6.2	
0+34 54 = Ec N.E. ret			
E.L.		5.9	386.7
+1		6.2	
cb		6.3	
+1		6.4	
+2		7.2	
+4		7.0	
+7		6.3	
¼		6.0	
+8		5.5	
℄		5.3	387.3
¼		5.5	
+5		5.5	
cb		5.2	
+7		4.8	
w.L.		4.2	388.4
0+70			
w.L.		4.3	388.3
+2		4.9	
cb		4.9	
+2		5.1	
¼		5.3	
+7		5.3	
℄		5.4	387.2

0+70	392.58		
E ¼		6.0	
+8		6.5	
cb		6.3	
E.C.		5.7	386.9
1+00			
E.C.		5.5	387.1
+1		5.9	
+9		5.9	
cb		6.0	
+2		6.2	
¼		5.9	
℄		5.2	387.4
+3		5.3	
¼		5.2	
cb		4.9	
+5		4.7	
w.L.		4.4	388.2
1+34 48			
w.L.		4.4	388.2
+4		4.8	
cb		4.8	
+5		5.1	
¼		5.0	
℄		5.1	387.5
+3		5.3	

1+34.48	392.58		
E'A		5.6	
+7		5.9	
cb		5.7	
+1		5.6	
E.L		5.6	387.0
M.H. on ℄ at 1+37		5.01	
1+55.18			
E.L.		5.6	387.0
cb		5.4	
+4		5.6	
¼		5.5	
℄		5.0	387.6
+4		4.9	
+8		5.0	
¼		5.4	
+2		5.0	
cb		4.9	
w.L.		4.5	388.1
2+00			
w.L.		4.6	388.0
+1		4.8	
cb		4.8	
+3		5.2	
+7		5.0	
¼		5.0	
+8		4.8	

2+00	392.58		
℄		4.8	387.8
¼		5.4	
+6		5.5	
+8		5.7	
cb		5.2	
E.L.		5.4	387.2
2+50			
E.L		5.4	387.2
+8		5.1	
cb.		5.3	
+2		5.4	
¼		5.0	
+8		4.5	
℄		4.5	388.1
¼		4.8	
+4		5.0	
+6		5.1	
49		4.7	
cb		4.6	
+9		4.3	
w.L.		4.1	388.5

3+00		394.58		
w.L.			3.9	388.7
+2			4.2	
+9			4.4	
cb			4.7	
+5			4.8	
1/4			4.7	
+8			4.4	
℄			4.5	388.1
1/4			4.8	
+6			5.1	
cb			4.8	
E.L.			5.0	387.6
T.P	6.15	394.35 ✓	4.38	388.20
3+50				
E.L.			6.6	387.8
cb			6.4	
+3			7.0	
+5			6.6	
1/4			6.5	
℄			6.0	388.4
+3			5.9	
1/4			6.3	
+8			6.7	
cb			6.0	
w.L.			6.1	388.3

4+00	394.35	
w.L.	5.6	388.8
+9	5.6	
cb	5.5	
+5	6.2	
1/4	5.8	
+5	5.7	
℄	5.8	388.6
+5	5.9	
1/4	6.3	
+8	6.7	
cb	6.4	
E.L.	6.2	388.2
4+50		
E.L.	6.0	388.4
cb	5.9	
+3	6.3	
+5	6.5	
1/4	5.9	
℄	5.3	389.1
+7	5.3	
1/4	5.5	
+7	5.9	
cb	5.2	
w.L.	5.0	389.4
Walk at 4+68 2.5'E 2.5' wide	6.06	388.4 ✓

5+00	394.35		
w.L.		4.8	389.6
+2		4.6	
+9		4.6	
cb		4.7	
+2		5.2	
+5		5.3	
1/4		5.2	
℄		5.1	389.3
+2		5.0	
1/4		5.6	
+8		6.2	
cb		5.7	
E.L.		5.9	388.5
5+07.08			
E.L.		5.8	388.6
+9		5.6	
cb		5.7	
+2		6.2	
1/4		5.6	
+8		5.0	
℄		5.0	389.4
1/4		5.2	
+7		5.3	
cb		4.7	
+1		4.6	
w.L.		4.7	389.7

5+27.78	394.35		
w.L		4.8	389.6
cb		4.6	
+2		5.3	
+5		5.4	
1/4		5.2	
+6		5.1	
℄		5.2	389.2
+5		5.3	
1/4		5.7	
+8		6.1	
cb		5.6	
E.L.		5.5	388.9
5+60			
E.L.		5.4	389.0
+8		5.3	
cb		5.5	
+2		5.9	
1/4		5.4	
+8		4.9	
℄		4.9	389.5
+3		4.8	
1/4		5.0	
+5		5.2	
cb		4.6	
w.L.		4.6	389.8

6+00	394.35		
w.L.		4.3	390.1
+9		4.2	
c b		4.4	
+3		5.1	
¼		4.9	
℄		4.7	389.7
+6		4.7	
¼		5.0	
+8		5.2	
c b		5.0	
+1		4.9	
E.L		5.0	389.4
Drive at 5+82 on E.L 7' wide		5.34	389.03 ✓
Walk at 6+02 on E.L 3' wide		4.74	389.61 ✓
6+35			
E.L		5.3	389.1
+3		5.0	
c b		5.1	
+2		5.5	
+4		5.3	
¼		5.0	
℄		4.4	390.0
¼		4.6	
+7		4.9	
c b		4.2	

6+35	394.35		
w c b + 5		4.1	
w.L.		4.4	390.0
6+56 99 = S.L. Adams on East.			
w.L.		4.2	390.2
+4		4.0	
c b		4.1	
+4		4.4	
¼		4.3	
℄		4.6	389.8
+4		4.7	
¼		5.0	
+8		5.2	
c b		4.8	
+7		4.8	
E.L		5.1	389.3
End Sec. on S.L. Adams			
E.L		5.1	389.3
+3		4.8	
c b		4.8	
+2		5.1	
¼		4.9	
℄		4.5	389.9
¼		4.0	
c b		4.0	
w.L.		4.1	390.3

		394.35		
T.P.	4.00	393.87	4.48	389.87
B.M. Beginning			7.13	386.74

Profile for Sewer between 37th & Jewell Drive North of T. St.

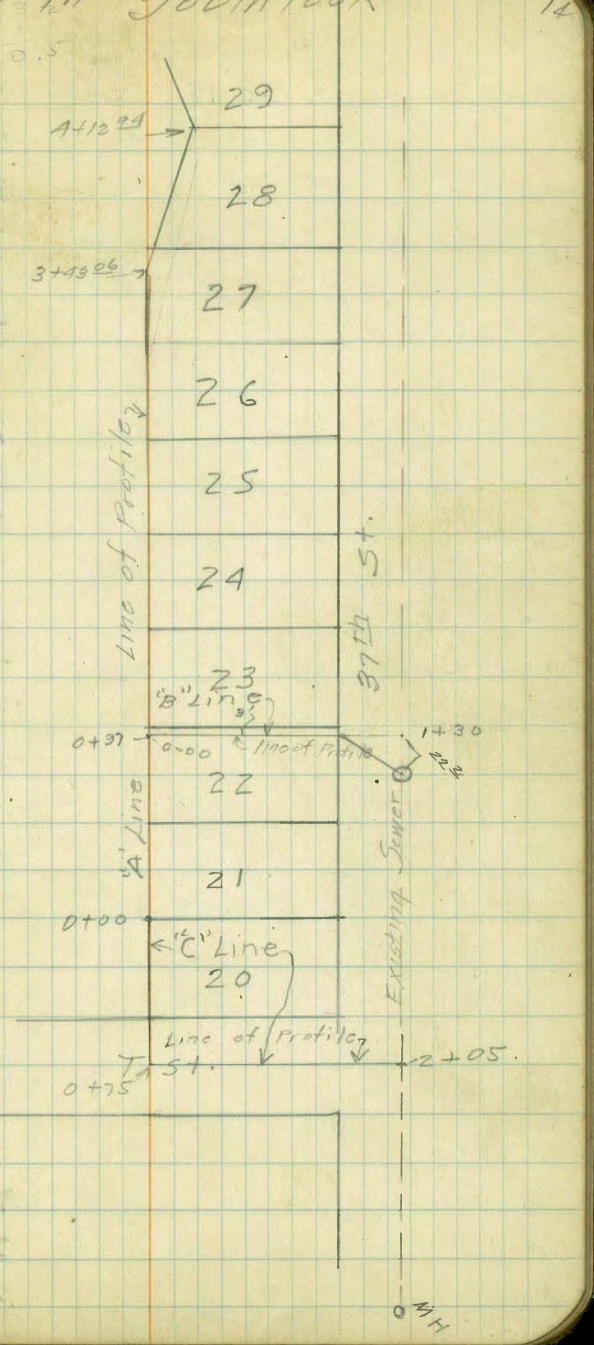
"A" Line

				63.47
B.M	13.10	76.57		63.48
T.P	12.75	89.13	0.19	76.38
T.P.	1.78	81.54	9.37	79.76
0+00			10.1	71.4
0+17			9.2	72.3
0+40			8.2	73.3
0+56			7.9	73.6
+0+60			7.3	74.2
0+97			7.7	73.8
1+30			7.5	74.0
1+46			7.0	74.5
1+63			6.8	74.7
1+97			6.8	74.7
2+04			6.4	75.1
2+14			6.5	75.0
2+33			6.1	75.4
2+42			5.8	75.7
2+50			5.8	75.7
T.P.	5.27	80.17	6.64	74.90
2+80			8.3	76.9
3+00			2.9	77.3
3+15			2.3	77.9
3+43.06 = L			1.4	78.8
3+60			1.1	79.1
3+70			0.7	79.5
3+71			+0.1	80.3

Wohlman e 37th Top F. Hyd S.E.

Sewer in Southlook

74



Sewer in Southlook

"A" Line

3+85	80.17	+0.5	80.7
4+00		+1.0	81.2
4+12.22		+1.8	82.0

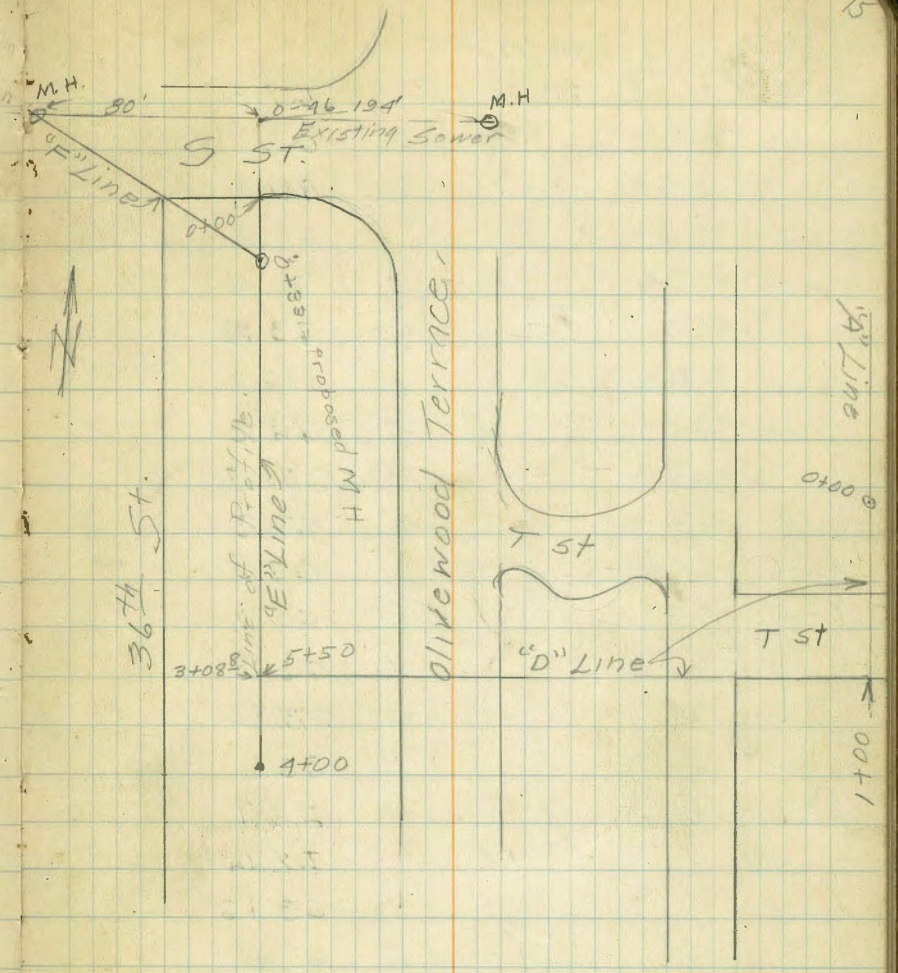
Line from back line to MH on N.L. Lot 22. "B" Line.

0+09 = 0+97		6.3	73.9
0+25		6.1	74.1
0+59		5.9	74.3
0+55		5.5	74.7
0+75		4.9	75.3
0+97		3.8	76.4
1+00 = ℄		3.0	77.2
1+12.5 = cb line		3.47	76.70
1+13		4.1	76.1
1+23.5		3.9	76.3
1+37.4	North of T St. on 37th = M.H.	2.25	77.22
Flow line at M.H.		9.53	70.64
T.P. 6.30	74.53	11.94	68.23

Line from N.L. Lot 20. to ℄ T St on ℄ T St to ℄ 37th

"C" Line

0+16		4.1	70.4
0+45		5.0	69.5
0+48		5.9	68.6
0+54		6.4	68.1
0+60 cb		6.48	68.05
0+60		7.1	67.4



"C" Line — Sewer in South Look

74.53

0+75 = ℄ T st		6.7	67.8
1+25		5.3	69.2
1+75		4.1	70.4
1+89		4.1	70.4
2+05 = ℄ 37th on 37th		3.1	71.4
F.L. of MH South of T st.		10.40	64.13

"D" Line

0+90		7.9	66.6
0+90 cb		7.43	67.05
0+97		7.3	67.2
1+00 = S ℄ T st.		7.0	67.5
1+50		8.6	65.9
2+00		10.6	63.9
2+10 cb		10.79	63.74
2+10		11.4	63.1
2+25 = ℄ Jewell		10.8	63.7
2+40		11.9	62.6
2+40 cb		11.37	63.16
2+50 = W.L. Jewell		11.5	63.0
T.P.	0.40	11.40	63.13
3+00	63.53	4.3	59.2
3+10		5.9	57.6
3+50		9.0	54.5
4+00		13.3	50.2
T.P.	0.11	12.52	51.01
	51.12		

"D" Line

51.12

4+30	3.9	47.2
4+50	4.5	46.6
4+60 cb	4.91	46.21
4+60	5.7	45.4
4+75 = ℄ Olivewood	5.2	45.9
4+90	6.7	44.4
4+90 cb	5.93	45.19
4+98	6.1	45.0
5+00	7.1	44.0
5+05	10.0	41.1
5+25	12.4	38.7
5+50 = 3408 ℄	13.5	37.6

Sewer in Southbrook

"E" Line

51.12

4+00			+1.8	52.9
3+75			1.8	49.3
3+50			7.4	43.7
3+25			10.8	40.3
3+08	8		13.5	37.6
3+00			13.8	37.3
2+75			13.6	37.5
2+50			12.7	38.4
2+25			10.9	40.2
2+00			7.9	43.2
1+75			5.8	45.3
1+50			3.1	48.0
1+40			1.8	49.3
1+25			1.5	49.6
1+00			2.8	48.3
T.P.	4.12	52.50	2.74	48.38
0+75			4.9	47.6
0+50			5.4	47.1
0+33	✓		5.6	46.9
0+28			5.0	47.5
0+23			4.3	48.2
0+02			1.9	50.6
0+00			2.1	50.4
0-5			1.6	50.9
0-10	eb		1.63	50.87

"E" line

52.50

0-10		2.4	50.1
0-21		1.6	50.9
0-46 = Sewer Man on S st.		1.6	50.9
T.P. X		0.33	52.17
T.P. 2.14	42.66	11.98	40.52
M.H. W of 36th (F.L.)		8.94	33.72
T.P. X 12.66	64.83		
M.H. E of Olivewood (F.L.)		8.98	55.85
T.P. 0.48	53.93	11.38	53.45
T.P. 9.67	57.05	6.55	47.38
T.P. 10.07	65.96	1.16	55.89
BM Beginning		2.51	63.45

Sewer in Southbrook

"F" Line.

TP x	0.97	53.14	52.17
0+00 = 0+33		6.4	46.7
0+20		6.1	47.0
0+45		6.3	46.8
0+50		7.2	45.9
0+64 = Sub S st.		8.64	44.50
0+64		9.3	43.8
0+90		11.2	41.9
1+10 = M.H.		15.1	38.0

Levels along Dead End

115' South from M.H. #3 Southlook Sewer. 0+00. & M.H. #3

H.I. 60.01

	Rod	
0+00	5.5	54.5
0+25	6.2	53.8
0+50	3.4	56.6
0+70	1.7	58.3
1+00	1.8	58.2
1+15 D.E.	2.1	57.9

IMPROVED TABLES

AND

INFORMATION