

1189

GROSS SECTIONS

EAST

FIELD BOOK

No. 385

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5th and G sts.

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No. 385 App 50 7/18/20 HA.

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No. Jim Appy 50 7/18/20 HA.

LEVELS on Walks + Drives on S. & E. of 397b

476	74.28	70.02	Sta 4+30 Page 25 Top con. 10/18
chk. on N.H. Sta. 2+00	5.8	64.5	✓
		74.3	
107' E. E. L. 397b = L. Con. Dr. on N on line			
Top of Dr.	7.19	67.2	
1+34 = L. Con. Walk on N	6.16	68.1	2' Back
1+39 = L. Garage on S 3' Back Con. Floor. With Con. Apron			
5+3' on Con. Apron = toe	7.33	67.0	
5+4' on Garage Floor	7.24	67.1	
	con. R = 4.81	69.5	
2+39 = L. Dr. on N 1' Back	4.10	70.2	
6+55 = L. Con. Dr. on N 3' Back			07' Back
2+90 = L. Con. Walk on N	3.78	70.5	4' Wide

Walker
3-12-27

X Section TEAK st 60' wide 10' cbs
10' 4's.
From 37th to 40th st 88.94

S.E. top Hydt
Woolman + 37th 12.56 76.03 63.47

T.P. 12.93 88.94 0.02 76.01

E.L. 37th st.

N 9.6 79.34

N top of cb 9.80 79.14

1/4 10.1 78.84

2/4 9.0 79.94

3/4 8.8 80.14

Gut 8.9 80.04

Stop of cb 8.35 80.59

S 7.9 81.04

3' E

S 3.7 85.24

cb. 4.4 84.54

+7 4.5 84.44

+9 7.2 81.74

1/4 7.2 81.74

2/4 8.2 80.74

+2 5.2 80.74

+4 4.8 84.14

1/4 4.8 84.14

cb. 5.4 83.54

N 5.9 83.04

30' E

N 5.0 83.94

88.94

cb 4.3 84.64

1/4 4.1 84.84

2/4 3.7 85.24

3/4 4.0 84.94

cb. 3.6 85.34

S 3.0 85.94

50' E

S 2.5 86.44

cb. 2.7 86.24

1/4 3.1 85.84

2/4 3.2 85.74

3/4 3.6 85.34

cb 4.0 84.94

N 4.4 84.54

100' E

N 2.5 86.44

cb. 1.8 87.14

1/4 1.4 87.54

2/4 1.1 87.84

3/4 0.9 88.14

cb 0.8 88.64

S +0.1 88.84

T.P. 578 94.60 0.12 88.82

150' E

S 4.1 90.50

cb. 4.3 90.30

94.60

$\frac{1}{2}$	4.8	89.80
$\frac{1}{4}$	5.4	89.20
$\frac{1}{4}$	5.6	89.00
cb	6.1	88.50
N	4.6	88.00

200'E

N	7.4	87.20
cb	5.9	88.70
$\frac{1}{4}$	5.4	89.20
$\frac{1}{4}$	5.0	89.60
$\frac{1}{4}$	4.9	89.70
cb	4.6	90.00
S	4.5	90.10

230'E

S	4.9	89.70
cb	5.0	89.60
$\frac{1}{4}$	5.7	88.90
$\frac{1}{4}$	6.7	87.90
$\frac{1}{2}$	8.1	86.50
cb	9.4	85.20
N	11.4	83.20
+5	12.5	82.10

260'E

-10	18.0	76.60
N	16.5	78.10
cb	15.3	79.30

94.60

$\frac{1}{4}$	14.2	80.40
$\frac{1}{4}$	11.9	82.70
$\frac{1}{4}$	10.1	84.50
cb	8.7	85.90
S	8.0	86.60

300'E

T.P. 591	9061	9.90	84.70
S		6.3	84.31
cb		7.9	82.71
$\frac{1}{4}$		10.1	80.51
$\frac{1}{4}$		11.6	79.01
$\frac{1}{4}$		12.8	77.81
cb		13.1	76.51
N		14.4	76.21
+10		15.3	75.31

315'E

-10	15.5	75.11
N	15.7	74.91
cb	15.3	75.31
$\frac{1}{4}$	13.8	76.81
$\frac{1}{4}$	12.7	77.91
$\frac{1}{4}$	10.6	80.01
cb	8.2	82.41
S	6.0	84.61

342'E

S	8.9	82.21
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9061

cd	9.9	80.71
$\frac{1}{4}$	10.1	80.57
$\frac{1}{2}$	11.7	78.91
$\frac{3}{4}$	14.6	76.01
cb	14.9	75.71
N	15.0	75.61
+10	15.3	75.31

360'E

-10	14.0	75.81
N	14.3	76.31
cb	14.2	76.41
$\frac{1}{4}$	14.0	76.61
$\frac{1}{2}$	13.3	77.31
$\frac{3}{4}$	12.2	78.41
cb	11.1	79.51
S	9.7	80.91

400'E

S	10.7	79.91
cb	12.2	78.41
$\frac{1}{4}$	13.0	77.61
$\frac{1}{2}$	13.0	77.61
$\frac{3}{4}$	12.8	77.81
cb	12.6	78.01
N	12.7	77.91
+10	12.5	78.11

450'E

9061

3

-10	8.3	82.31
N	9.0	81.61
cd	9.0	81.61
$\frac{1}{4}$	9.2	81.41
$\frac{1}{2}$	9.3	81.31
$\frac{3}{4}$	10.1	80.51
cb	10.5	80.11
S	9.5	81.11

475'E

S	8.2	82.41
cb	8.1	82.51
$\frac{1}{4}$	7.4	83.21
$\frac{1}{2}$	6.6	84.01
$\frac{3}{4}$	6.9	83.90
cb	7.2	83.41
N	6.4	84.21

500'E

N	4.4	86.21
cd	5.1	85.51
$\frac{1}{4}$	5.0	85.61
+8	1.6	86.01
$\frac{1}{2}$	3.8	86.81
$\frac{3}{4}$	3.8	86.81
cb	4.3	86.31
S	4.7	85.91

532'E

Note: if any fill is necessary on South
of West should be located

9061

S	14	89.21
cb	11	89.57
$\frac{1}{4}$	17	88.91
$\frac{1}{2}$	18	88.81
+2	27	87.91
$\frac{1}{4}$	31	86.91
cb	29	87.71
N	26	88.01

575' E

N	21	88.51
+2	30	87.61
cb	33	87.31
$\frac{1}{4}$	33	87.31
$\frac{1}{2}$	39	86.71
+4	11	89.51
$\frac{1}{4}$	14	89.21
+8	13	89.31
cb	0.5	90.11
S	0.7	89.90

580' E

S	0.8	89.81
cb	0.9	89.71
+1	2.0	88.61
$\frac{1}{4}$	1.9	88.71
+8	1.3	89.31
$\frac{1}{2}$	2.9	87.71

9061

$\frac{1}{4}$	3.5	87.11
cb	3.5	87.11
N	3.0	87.61

583' E

N	3.5	87.11
cb	3.5	87.11
$\frac{1}{4}$	3.7	86.91
$\frac{1}{2}$	3.5	87.11
+4	1.6	89.01
$\frac{1}{4}$	1.6	89.01
cb	2.0	88.61
+8	2.3	88.31
+9	0.7	89.91
S	0.7	89.91

597' E

S	0.1	90.51
+2	2.0	88.61
cb	2.2	88.41
$\frac{1}{4}$	3.1	87.51
+7	3.3	87.31
+9	4.3	86.31
$\frac{1}{2}$	4.3	86.31
$\frac{1}{4}$	4.1	86.51
cb	4.3	86.31
N	3.3	87.31

600' E = 116.38 ± 0.07

70.61

92.98

92.98

5

N 4.3 86.31
 N top of cb 4.45 86.16
 Gut 4.9 85.71
 $\frac{1}{2}$ 4.4 86.21
 $\frac{1}{4}$ 4.5 86.11
 $\frac{1}{4}$ 3.8 86.81
 Gut 3.8 86.81
 S top of cb 3.52 87.09
 S 3.3 87.31

chk. on BM. SE top Hyd't 6.95 83.66
 TP 7.32 92.98 6.95 83.66

Note: from ca. 38th to ca. 40th T&E st. runs 6.88 to 6.3

EL 38th

S 4.1 88.88
 top of cb 4.43 88.55
 Gut 4.8 88.18
 $\frac{1}{2}$ 4.6 87.38
 $\frac{1}{4}$ 4.5 88.48
 $\frac{1}{2}$ 5.1 87.88
 top cb 4.87 88.11
 N 4.5 88.48

5' E

N 3.6 89.38
 cb 4.2 88.78
 $\frac{1}{4}$ 4.5 88.48
 $\frac{1}{2}$ 4.8 88.18

Woolman
+30th st.odd cbs
(10' 4.5'
maximum)

$\frac{1}{2}$ 4.8 88.18
 cb 4.8 88.18
 S 4.5 88.48
 17' E
 S 5.6 87.38
 cb 5.5 87.48
 $\frac{1}{4}$ 5.2 87.78
 $\frac{1}{2}$ 4.9 88.08
 $\frac{1}{4}$ 4.6 88.38
 cb 4.5 88.48
 N 4.0 88.98

50' E

N 6.0 86.98
 cb 5.9 87.08
 $\frac{1}{4}$ 6.3 86.68
 $\frac{1}{2}$ 6.4 86.58
 $\frac{1}{4}$ 6.7 86.28
 cb 7.0 85.98
 S 7.2 85.78

100' E

S 11.2 81.78
 S 11.0 81.98
 S 10.0 82.98
 cb 9.5 83.48
 $\frac{1}{4}$ 9.4 83.58
 $\frac{1}{2}$ 9.2 83.78

92.98

1/4	9.0	83.98
cb	8.6	84.38
N	8.1	84.88

Note: if any fill is necessary at approx. sta. 1+45 on N ^E located _{Maybe}

150' E

N	8.9	84.08
cb	9.9	83.08
1/4	10.7	82.28
1/2	10.9	82.08
3/4	11.1	81.88
cb	11.4	81.58
S	11.2	81.78
+5	11.4	81.58
1+68 = 2. Com. Walk on S on line 5' wide		81.86

185' E

-5	10.0	82.98
S	10.0	82.98
cb	9.9	83.08
1/4	9.4	83.58
1/2	9.2	83.78
3/4	8.9	84.08
cb	9.2	83.78
N	8.2	84.78

235' E

N	4.2	88.78
cb	4.8	88.18
1/4	4.7	88.78

92.98

1/2	4.6	88.38
1/4	4.0	88.98
+5	3.5	89.48
cb	3.7	89.28
S	3.6	89.38

259' E

S	3.0	89.98
cb	3.0	89.98
1/4	3.0	89.98
1/2	3.5	89.48
3/4	3.6	89.38
cb	3.4	89.58
N	3.5	89.48

280' E

N	4.0	88.98
cb	4.0	88.98
1/2	4.2	88.78
1/4	4.1	88.88
+7	3.7	89.28
1/4	2.9	90.08
cb	2.6	90.38
S	3.0	89.98

305' E

S	5.2	87.78
cb	5.0	87.98
1/4	5.4	87.58

92.98

94.31

2	6.0	86.98
$\frac{1}{4}$	6.2	86.78
cb	6.0	86.98
+4	5.7	87.28
N	3.9	89.08

319'E

N	6.9	86.08
cb	7.3	85.68
$\frac{1}{4}$	6.9	86.08
2	6.8	86.18
$\frac{1}{4}$	7.0	85.98
cb	8.1	84.88
S	8.3	84.68
+5	8.3	84.68
TP	7.97	94.31
	6.64	86.34

337'E

-10	12.6	81.71
S	12.4	81.91
cb	11.6	82.71
$\frac{1}{4}$	9.9	84.41
2	8.8	85.51
$\frac{1}{4}$	8.5	85.81
cb	9.0	85.31
N	8.6	85.71

360'E

N	6.4	87.91
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94.31

7

cb	7.8	86.51
$\frac{1}{4}$	8.0	86.31
2	7.8	86.51
+8	7.8	86.51
$\frac{1}{4}$	8.2	86.11
cb	10.7	83.61
S	11.8	82.51
+10	12.7	81.61

395'E

-10	9.4	84.91
S	8.0	86.31
cb	6.7	87.61
+7	5.6	88.71
$\frac{1}{4}$	5.6	88.71
2	5.2	88.11
$\frac{1}{4}$	5.1	89.21
+3	4.9	89.41
cb	3.0	91.31
N	2.2	92.11

410'E

N	1.1	93.21
cb	1.3	93.01
$\frac{1}{4}$	4.1	90.21
2	4.2	90.11
$\frac{1}{4}$	4.5	89.81
cb	5.1	89.21

9300
9431

S	23	88.01
	431'E	
S	55	88.81
cb	43	90.01
$\frac{1}{4}$	39	90.41
$\frac{1}{2}$	38	90.51
$\frac{1}{4}$	37	90.61
+8	24	91.91
cb	09	93.41
N	08	93.51

450'

N	30	91.31
cb	31	91.21
+5	51	89.21
$\frac{1}{4}$	56	88.71
$\frac{1}{2}$	52	89.11
$\frac{1}{4}$	52	89.11
cb	53	89.01
S	64	87.91

487'E

S	11.5	82.81
cb	11.0	83.31
$\frac{1}{4}$	10.2	84.11
$\frac{1}{2}$	10.4	83.91
$\frac{1}{4}$	10.0	84.31
cb	78	84.51

9431

90.88

8

N	96	84.71	
	520'E		
N	132	81.11	
cb	143	80.01	
$\frac{1}{4}$	144	79.91	
$\frac{1}{2}$	146	79.71	
$\frac{1}{4}$	146	79.71	
cb	16.2	78.11	
S	16.3	78.01	
+10	16.5	77.81	
TD 740	70.88	12.83	81.48

550'E

-10	15.9	74.98
S	15.4	75.48
cb	14.6	76.28
$\frac{1}{4}$	12.4	78.48
$\frac{1}{2}$	11.9	78.98
$\frac{1}{4}$	11.4	79.48
cb	11.4	79.48
+9	10.6	80.28
N	9.7	81.18

600'E = 14.3941

N	80	82.88
cb	93	81.58
$\frac{1}{4}$	10.4	80.48
$\frac{1}{2}$	10.9	79.98

90.88

z	10.3	80.58
+5	11.9	78.98
cb	13.4	77.48
S	14.5	76.38
+5	15.2	75.68
	+3	
S	13.9	76.98
cb	12.5	78.38
z	11.2	79.68
z	10.9	80.08
z	10.5	80.38
cb	9.4	81.48
N	8.2	82.68
	Ncb	
N	9.3	82.58
cb	9.5	81.38
z	10.4	80.48
z	10.8	80.08
z	11.7	79.18
cb	12.8	78.08
S	13.5	77.38
	Nz	
S	14.5	76.38
cb	13.6	77.28
z	12.4	78.48
z	11.5	79.38

90.88

9

z	10.4	80.48
cb	9.4	81.48
N	8.6	82.28
	d	
N	8.2	82.68
cb	7.2	81.68
z	10.0	80.88
z	11.0	79.88
z	12.0	78.88
cb	13.2	77.68
S	14.5	76.38
	z	
S	14.1	76.78
cb	13.8	78.28
z	11.7	79.18
z	10.7	80.18
z	9.8	81.08
cb	9.0	81.88
N	8.1	82.78
	Ncb	
N	7.7	83.18
cb	9.1	81.78
z	9.7	81.18
z	10.3	80.58
z	10.9	79.98
z	12.1	78.78

90.88

90.9

90.88

90.9

10

S		13.3	77.6	77.6	$\frac{1}{4}$	82	82.7
	E.L. 39 [±] 50 [±] 0 [±]				cb	77	83.2
S		13.0	77.9		+5	73	83.6
cb		11.9	79.0		N	58	85.1
$\frac{1}{4}$		10.7	80.2				
L		10.1	80.8		N	23	88.6
$\frac{1}{4}$		9.8	81.1		cb	40	86.9
cb		9.0	81.9		$\frac{1}{4}$	49	86.0
N		8.0	82.9		L	53	85.6
	0507 7'E				$\frac{1}{4}$	55	85.4
N		7.6	82.3		cb	66	84.3
cb		9.0	81.9		+6	89	82.0
$\frac{1}{4}$		9.6	81.3		S	87	82.2
L		10.0	80.9		+10	92	81.7
$\frac{1}{4}$		10.0	80.9				
cb		11.4	79.5		-5	51	85.8
+3		12.7	78.2		S	51	85.8
S		13.3	77.6		+5	49	86.0
+5		13.5	77.4		cb	28	88.1
	40'E				$\frac{1}{4}$	25	88.4
-5		12.2	78.7		L	23	88.3
S		11.9	79.0		+5	21	88.8
cb		10.4	80.5		$\frac{1}{4}$	10	89.9
+7		9.0	81.9		cb	0.4	90.5
$\frac{1}{4}$		8.7	82.2		+7	+0.7	91.6
L		8.4	82.5		N	+3.1	94.0

80'E

112'E

90.58

103.5

TP	13.93	103.50	041	90.47
		129' E		
N			71	96.4
cb			90	95.5
$\frac{1}{4}$			105	93.0
+5			132	90.3
$\frac{1}{2}$			134	90.1
$\frac{1}{4}$			132	90.3
+4			135	90.2
+5			129	90.6
cb			133	90.2
S			168	87.7
+10			174	86.1
		155' E		
-10			158	87.7
S			148	88.7
+5			136	89.9
cb			117	91.8
+4			111	92.4
$\frac{1}{4}$			112	92.3
$\frac{1}{2}$			113	92.2
+5			110	92.5
$\frac{1}{2}$			83	95.2
cb			75	96.0
+7			60	97.5
N			45	99.0

103.50

103.5

1775

11

N		28	100.70
+5		51	98.4
cb		59	97.6
$\frac{1}{4}$		70	96.5
+5		93	94.2
$\frac{1}{2}$		98	93.7
$\frac{1}{4}$		97	93.8
cb		99	94.6
+5		110	92.5
S		132	90.3
+10		149	88.6
		181' E	
-10		151	88.4
S		129	90.6
+4		118	91.7
cb		95	94.0
$\frac{1}{4}$		93	94.2
$\frac{1}{2}$		92	94.3
+5		86	94.9
$\frac{1}{4}$		65	97.0
cb		50	98.5
+8		37	99.8
N		26	100.9
		195' E	
N		20	101.5
+6		18	98.7

103.50

103.5

cb	35	98.0
$\frac{1}{2}$	5.9	97.6
+7	8.5	95.0
$\frac{1}{2}$	8.5	95.0
$\frac{1}{2}$	8.8	94.7
cb	9.1	94.4
+8	12.1	91.4
S	12.4	91.1
+10	14.6	88.9

222'E

-10	14.9	88.6
S	13.3	90.2
cb	9.5	94.0
$\frac{1}{2}$	8.7	94.8
$\frac{1}{2}$	8.4	95.1
+4	7.9	95.6
$\frac{1}{2}$	5.0	98.5
cb	3.5	100.0
+7	2.3	101.2
N	0.9	102.6

240'E

N	0.3	103.2
+6	3.3	100.2
cb	4.3	99.2
$\frac{1}{2}$	6.0	97.5
+2	6.3	97.2

103.50

103.5

+6	5.0	95.5
$\frac{1}{2}$	8.5	95.0
$\frac{1}{2}$	8.8	94.7
cb	9.5	94.0
S	13.3	90.2
+10	15.2	88.3

257'E

-10	14.4	89.1
S	12.6	90.9
cb	9.2	94.3
$\frac{1}{2}$	8.6	94.9
$\frac{1}{2}$	8.3	95.2
+3	7.9	95.6
$\frac{1}{2}$	5.2	98.3
+6	4.0	99.5
cb	3.7	99.8
N	2.5	101.0

270'E

N	2.6	100.9
cb	4.5	99.0
$\frac{1}{4}$	5.9	97.6
$\frac{1}{2}$	7.9	95.4
$\frac{1}{2}$	8.5	95.0
cb	9.0	94.5
S	12.9	90.6
+10	14.0	89.5

103.50

103.5

103.50

13

274'E

-10	14.5	89.0
S	12.3	91.2
cb	9.0	94.5
$\frac{1}{4}$	8.5	95.0
2	7.9	95.6
$\frac{1}{4}$	5.2	98.3
cb	3.6	99.9
N	2.3	101.2

300'E

N	2.1	101.4
cb	3.6	99.9
$\frac{1}{4}$	4.8	98.7
+3	5.0	98.5
2	8.1	95.4
$\frac{1}{4}$	8.5	95.0
cb	8.9	94.6
+5	9.5	94.0
S	12.5	91.0
+10	14.3	89.2

320'E

-10	14.7	88.8
-3	13.2	90.3
S	12.2	91.3
+6	9.9	93.6
cb	9.7	93.8

 $\frac{1}{2}$

2

+7

 $\frac{1}{4}$

cb

N

N

+8

cb

 $\frac{1}{4}$

+3

+7

2

 $\frac{1}{4}$

cb

+5

S

+10

T.P.

715

-10

S

+7

cb

 $\frac{1}{4}$ 94.3

7.5	94.0
9.3	95.2
6.2	97.3
5.6	97.9
4.4	99.1
2.5	101.0

360'E

6.8	96.7
9.3	94.2
9.7	93.8
10.9	92.6
11.3	92.2
13.0	90.5
13.2	90.3
13.2	90.3
13.3	90.2
13.5	90.0
16.2	87.3
17.2	86.3

98.89 12.36

91.14

400'E

14.9	83.4
14.8	83.5
11.1	87.2
10.4	87.9
9.9	88.4

9829

98.3

d	9.7	88.6
$\frac{1}{4}$	7.3	91.0
cb	6.3	92.0
+8	4.9	93.4
N	3.8	94.5

450'E

N	2.9	95.4
cb	4.6	93.7
$\frac{1}{4}$	6.0	92.3
d	8.5	89.8
+5	9.3	89.0
$\frac{1}{4}$	9.5	88.8
cb	9.8	88.5
+7	10.5	87.8
S	12.2	86.1
+10	14.2	84.1

480'E

-10	13.4	84.9
-5	12.8	85.5
S	11.7	86.5
+3	10.2	88.1
cb	9.8	88.5
$\frac{1}{4}$	9.5	88.8
d	8.1	89.9
$\frac{1}{4}$	6.8	91.5
cb	5.5	92.8

9829

98.3

14

N	4.4	93.9
500'E		
N	5.7	92.6
cb	7.2	91.1
$\frac{1}{4}$	8.3	90.0
d	9.4	88.9
$\frac{1}{4}$	10.4	87.9
cb	10.6	87.7
+8	10.8	87.5
S	12.1	86.2
+10	14.0	84.3

525'E

-10	15.2	83.1
S	14.3	84.0
+7	13.2	85.1
+5	12.4	85.9
cb	12.4	85.9
$\frac{1}{4}$	12.1	86.2
+9	11.7	86.6
d	11.1	87.2
+3	10.4	87.9
$\frac{1}{4}$	9.7	88.6
cb	9.0	89.3
N	8.1	90.2

TP 440

89.96	12.73	85.56
555'E		

89.96

96.0

87.38

15

N	30	87.0
cb	4.0	86.0
$\frac{1}{2}$	4.4	85.6
$\frac{1}{4}$	5.0	85.0
$\frac{1}{4}$	5.1	84.9
cb	5.4	84.6
S	6.1	83.9

600' E

S	7.7	82.3
7.5	6.8	83.2
cb	6.6	83.4
$\frac{1}{4}$	6.5	83.5
$\frac{1}{4}$	6.7	83.3
$\frac{1}{4}$	6.5	83.5
$\frac{1}{4}$	6.5	83.5

N

649.75 E

N	8.3	81.7
cb	8.8	81.2
$\frac{1}{2}$	9.0	81.0
$\frac{1}{4}$	8.6	81.4
$\frac{1}{4}$	8.9	81.1
cb	9.1	80.9
4.4	8.5	81.5
S	8.9	81.1
T.P.	6.27	87.38
	8.85	81.1

on Mon. N.W. Cor.

TICK + 40th

T.P. on ^{8M.} 1917 back Woolman + 40th 5.34

8214
 8218 = 8M.
 0.04

Marker
3-14-27

X Section 5' st 60' wide
From EL 37th to N.L. 38th
" EL 38th " N.L. 40th 50' wide

10' cbs
10' 1/2 S

88.30

94.0

16

10 cbs
7 1/2 1/2 S
Elev. S stop cb

7.71 88.30 80.59

Page 1

EL

N	3.8	84.5
N top of cb	4.21	84.1
Gut	4.7	83.6
1/4	4.7	83.6
1/2	4.7	83.6
3/4	5.2	83.1
Gut	5.4	82.9
S stop cb	5.07	83.23
S	4.9	83.4

24' E

S	3.7	84.6
cb	3.6	84.7
1/4	3.5	84.8
1/2	3.5	84.8
3/4	3.1	85.2
cb	2.3	86.0
N	1.6	86.7

45' E

N	1.0	87.3
cb	1.5	86.8
1/4	1.7	86.6
1/2	1.8	86.5
3/4	1.8	86.5

cb
S

2.3 86.0
2.8 85.5

100' E

S	1.4	86.9
cb	1.1	87.2
1/4	1.0	87.3
1/2	1.0	87.3
3/4	1.1	87.2
cb	0.6	87.7
N	0.0	88.3

TP 648

94.00 0.78 87.52

150' E

N	5.0	89.0
cb	5.3	88.7
1/4	5.7	88.3
1/2	5.8	88.2
3/4	5.8	88.2
cb	5.4	88.6
S	5.2	88.8

200' E

S	4.3	89.7
cb	4.2	89.8
1/4	4.2	89.8
1/2	4.5	89.5
3/4	4.1	89.9
cb	4.0	90.0

94.00

N 3.6 90.4

250' E

N 3.2 90.8

cb 3.5 90.5

 $\frac{1}{4}$ 4.0 90.0

d 4.4 89.6

 $\frac{1}{4}$ 4.3 89.7

cb 3.7 90.3

S 4.0 90.0

268' E

S 4.2 89.8

cb 4.7 89.3

 $\frac{1}{4}$ 5.2 88.8

d 5.0 89.0

 $\frac{1}{4}$ 4.3 89.7

cb 3.4 90.6

N 2.5 91.5

285' E

N 3.6 90.4

cb 4.3 89.7

 $\frac{1}{4}$ 4.9 89.1

d 5.4 88.6

 $\frac{1}{4}$ 5.6 88.4

cb 5.6 88.4

S 5.7 88.3

300' E

94.00

17

S 5.8 88.2

cb 5.8 88.2

 $\frac{1}{4}$ 5.9 88.1

d 5.4 88.6

 $\frac{1}{4}$ 5.0 89.0

cb 4.7 89.3

N 4.0 90.0

345' E

N 3.8 90.2

d 4.5 89.5

 $\frac{1}{4}$ 4.8 89.2

d 5.2 88.8

 $\frac{1}{4}$ 5.3 88.7

cb 5.6 88.4

S 5.5 88.5

358' E

S 4.7 89.3

cb 4.7 89.3

 $\frac{1}{4}$ 4.5 89.5

d 4.5 89.5

 $\frac{1}{4}$ 4.0 90.0

cb 3.3 90.7

N 3.1 90.9

400' E

N 2.4 91.6

cb 2.7 91.3

94.00

1/4	32	90.8
2	30	91.0
1/2	29	91.1
cb	34	90.6
S	39	90.1

450'E

S	28	91.2
cb	32	90.8
1/4	31	90.9
2	28	91.2
1/2	28	91.2
cb	27	91.3
N	23	91.7

483'E

N	41	89.9
cb	33	90.7
1/4	31	90.9
2	34	90.6
1/2	30	91.0
cb	21	91.9
S	18	92.2

505'E

S	15	92.5
cb	17	92.3
+5	28	91.2
1/4	31	90.9

94.00

18

2	37	90.3
1/4	45	89.5
cb	47	89.3
N	51	88.9

540'E

N	42	89.8
cb	46	89.4
1/4	45	89.5
2	40	90.0
1/2	28	91.2
+8	19	92.1
cb	09	93.1
S	10	93.0

575'E

S	15	92.5
+8	16	92.4
cb	25	91.5
1/4	37	90.3
2	39	90.1
1/2	38	90.2
cb	37	90.3
N	34	90.6

598'E

N	32	90.8
cb	37	90.3
1/4	37	90.3

94.00

97.0

96.96

97.0

19

2		3.6	90.4	
$\frac{1}{4}$		3.4	90.6	
+7		3.2	90.8	
cb		2.3	91.7	
+5		1.5	92.5	
S		1.2	92.8	
	600' E = N.L. 38th			
S		2.8	91.2	
S top of cb.		2.86	91.14	
Gut		3.3	90.7	
$\frac{1}{2}$		3.5	90.5	
2		3.6	90.4	
$\frac{1}{4}$		3.7	90.3	
Gut		4.2	89.8	
N top cb.		3.91	90.1	
N		3.6	90.4	
I.P.	489	96.96	1.93	92.07
		E.L. 38th	50' st	10' cbs
				7 1/2 1/4
N		3.5	93.5	
N top cb		3.81	93.2	
Gut		4.1	92.9	
$\frac{1}{2}$		3.7	93.3	
2		3.7	93.3	
$\frac{1}{4}$		3.8	93.2	
Gut		3.8	93.2	
S top of cb		3.41	93.6	

S		2.9	94.1
	2'E		
S		2.3	94.7
cb		2.8	94.2
+2		3.6	93.4
$\frac{1}{4}$		3.6	93.4
2		3.6	93.4
$\frac{1}{2}$		3.8	93.2
+5		3.8	93.2
cb		3.3	93.7
N		3.3	93.7
	50'E		
N		2.2	94.8
cb		2.9	94.1
+2		3.3	93.7
$\frac{1}{4}$		3.4	93.6
2		3.0	94.0
$\frac{1}{2}$		3.3	93.7
cb		3.7	93.3
+2		3.1	93.9
S		2.7	94.3
	100'E		
S		3.8	93.2
+8		4.3	92.7
cb		4.8	92.2
$\frac{1}{4}$		4.6	92.4

9696

97.0

d	46	92.4
$\frac{1}{4}$	49	92.1
cb	48	92.2
N	49	92.1
+2	67	90.3
+10	77	89.3

150'E

-15	122	84.8
N	78	89.2
+3	66	90.4
cb	66	90.4
$\frac{1}{4}$	67	90.3
d	64	90.6
$\frac{1}{4}$	66	90.4
cb	68	90.2
-2	57	91.3
S	53	91.7

200'E

S	83	88.7
cb	93	87.7
$\frac{1}{4}$	92	87.8
d	89	88.1
$\frac{1}{4}$	91	87.9
cb	89	88.1
N	93	87.7
+10	146	82.4

9696

97.0

80

87.7

250'E

-10	151	81.9
N	121	84.9
cb	110	86.0
$\frac{1}{4}$	111	85.9
d	108	86.2
$\frac{1}{4}$	111	85.9
cb	110	86.0
S	104	86.6

300'E

S	113	85.7
cb	120	85.0
$\frac{1}{4}$	121	84.9
d	120	85.0
$\frac{1}{4}$	125	84.5
cb	122	84.8
N	125	84.5
+10	171	79.9
T.P. 334	8773 12.57	8439

305'E

-5	33	84.4
N	31	84.6
cb	31	84.6
$\frac{1}{4}$	31	84.6
d	28	84.9
$\frac{1}{4}$	29	84.8

87.73

87.7

cb	28	84.9
S	21	85.6
317'E = ⁴⁶ on steps on South to House 192 on line		85.8
326'E = ⁴⁶ " " " N to House	278	84.9
351'E = ⁴⁶ on Dr. on S 15' wide as East		
-0.5 = top Dr.	179	85.9
S	17	85.8
cb	38	84.4
$\frac{1}{4}$	36	84.1
$\frac{1}{4}$	36	84.1
$\frac{1}{4}$	39	83.8
cb	39	83.8
N	41	83.6
+5	41	83.6
	354'E	
-10	60	81.7
N	50	82.7
+5	41	83.6
cb	40	83.7
$\frac{1}{4}$	39	83.8
$\frac{1}{4}$	36	84.1
$\frac{1}{4}$	36	84.1
cb	32	84.5
S	21	85.6
	400'E	
S	34	84.3

87.73

87.7

cb	47	83.0
$\frac{1}{4}$	49	82.8
$\frac{1}{4}$	46	83.1
$\frac{1}{4}$	51	82.6
cb	49	83.8
+7	50	82.7
N	60	81.7
+10	52	79.5
	408' N	
-5	55	82.2
N	55	82.2
cb	51	82.6
$\frac{1}{4}$	52	82.5
$\frac{1}{4}$	50	82.7
$\frac{1}{4}$	51	82.6
+6	49	82.8
cb	45	83.2
S	37	84.0
	445'E	
S	51	82.6
cb	63	81.4
$\frac{1}{4}$	63	81.4
$\frac{1}{4}$	62	81.5
$\frac{1}{4}$	65	81.2
cb	62	81.5
N	60	81.7

87.73

87.776.9

+5 60 81.7

450'E

-10 96 78.1

N 65 81.2

cb 63 81.4

 $\frac{1}{2}$ 66 81.1 $\frac{1}{4}$ 64 81.3 $\frac{1}{4}$ 68 80.9

cb 57 82.0

S 50 82.7

190'E

S 52 82.5

+5 76 80.1

cb 87 79.0

 $\frac{1}{4}$ 94 78.3 $\frac{1}{4}$ 92 78.5 $\frac{1}{2}$ 98 77.9

cb 93 78.4

+1 83 79.4

N 90 78.7

+10 11.4 76.3

T.P. 2.00 76.89 12.14 74.89

550'E

-10 65 70.4

N 39 73.0

cb 36 73.3

76.89

76.9

22

+2 42 72.7

 $\frac{1}{4}$ 38 73.1 $\frac{1}{2}$ 36 73.3 $\frac{1}{4}$ 34 73.5

cb 29 74.0

+8 20 74.9

S 14 75.5

592'E

S 63 70.6

cb 65 70.4

 $\frac{1}{4}$ 70 69.9 $\frac{1}{4}$ 65 70.4 $\frac{1}{4}$ 69 70.0

cb 67 70.2

N 68 70.1

+10 80 68.9

600'E = 16.394 ^{10' chs} 10' 45

-5 74 69.5

N 70 69.9

cb 72 69.7

 $\frac{1}{4}$ 71 69.8 $\frac{1}{4}$ 69 70.0 $\frac{1}{2}$ 72 69.7

cb 72 69.7

S 69 70.0

Ncb

7689

76.9

S	73	69.6
cb	76	69.3
i	76	69.3
L	74	69.5
i	74	69.5
cb	77	69.2
N	77	69.2
	$\frac{1}{2}$	
N	81	68.8
cb	80	68.9
i	80	68.9
L	79	69.0
i	80	68.9
cb	81	68.8
S	84	68.5
	$\frac{1}{2}$	
S	84	68.5
cb	83	68.6
i	82	68.7
L	82	68.7
i	83	68.6
cb	85	68.4
N	84	68.5
	$\frac{1}{2}$	
N	87	68.2
cb	87	68.2

7689

76.9

23

~~72.4~~

i	87	68.2
L	87	68.2
i	88	68.1
cb	87	68.2
S	87	68.2
	E.Cb	
S	90	67.9
cb	89	68.0
i	89	68.0
L	88	68.1
i	89	68.0
cb	88	68.1
N	88	68.1
	El. 3954 = 0+00	
N	89	68.0
cb	90	67.9
i	90	67.9
L	91	67.8
i	91	67.8
cb	91	67.8
S	91	67.8
	TP 217	76.37
		649
		70.80
	$\frac{1}{2}$	
S	51	67.3
cb	50	67.4
i	49	67.6

7237

72.4

d	47	67.7
i	46	67.8
cb	47	67.8
N	48	67.6

60'E

N	52	67.2
cb	53	67.1
i	52	67.2
d	53	67.1
i	56	66.8
cb	62	66.2
S	70	65.4

100'E

S	63	65.1
cb	62	66.2
i	60	66.4
d	57	66.7
i	55	66.9
cb	59	66.5
N	57	66.7

150'E

N	47	67.7
+3	54	67.0
cb	55	66.9
i	55	66.9
d	57	66.7

7237

72.4

24

i	40	66.4
cb	57	66.7
S	61	66.3

200'E

S	53	67.1
cb	51	67.3
i	48	67.6
d	45	67.9
i	48	67.6
cb	46	67.8
N	39	68.5

250'E

N	31	69.3
cb	33	69.1
i	38	68.6
d	36	68.8
i	39	68.5
cb	41	68.3
S	40	68.4

300'E

S	30	69.4
cb	32	69.2
i	32	69.2
d	29	69.5
i	30	69.4
cb	27	69.7

72.37

72.4

N 21 70.3

350' E

N 25 69.9

cb 29 69.5

 $\frac{1}{2}$ 30 69.4 $\frac{1}{4}$ 31 69.3 $\frac{1}{2}$ 34 69.0

cb 34 69.0

S 36 68.8

+5 34 69.0

355' E

-5 47 67.7

S 37 68.7

cb 34 69.0

 $\frac{1}{4}$ 33 69.1 $\frac{1}{2}$ 31 69.3

7 31 69.3

cb 30 69.4

N 25 69.9

400' E

N 29 69.5

cb 32 69.2

 $\frac{1}{4}$ 33 69.1 $\frac{1}{2}$ 33 69.1 $\frac{1}{4}$ 34 69.0

cb 36 68.8

72.37

72.473.7

S 42 68.2

+5 53 67.1

430' E - d Co. Halk on N 35' wide 2.35 70.1

450' E

-5 42 68.2

S 36 68.8

+5 29 69.5

cb 30 69.4

 $\frac{1}{2}$ 28 69.6 $\frac{1}{4}$ 26 69.8 $\frac{1}{2}$ 26 69.8

cb 25 69.9

N 23 70.1

T.P. 439 75.71 1.05 71.32

500' E

N 36 72.1

cb 46 71.1

 $\frac{1}{4}$ 48 70.9 $\frac{1}{2}$ 47 71.0 $\frac{1}{4}$ 51 70.6

cb 51 70.6

S 48 70.9

+5 48 70.9

550' E

S 43 71.4

cb 40 71.7

35

75.71

75.7

$\frac{1}{4}$	4.0	71.7
$\frac{1}{2}$	37	72.0
$\frac{3}{4}$	38	71.9
+7	39	71.8
cb	34	72.3
N	27	73.0
600'E		
N	27	73.0
+8	29	72.8
cb	34	72.3
+2	39	71.8
$\frac{1}{4}$	4.0	71.7
$\frac{1}{2}$	42	71.5
$\frac{3}{4}$	44	71.3
cb	4.5	71.2
S	5.7	70.0
+5	6.2	69.5
651'E = N.L. 40 th		
-5	8.4	62.3
V	7.9	67.8
cb	7.4	68.3
$\frac{1}{4}$	7.2	68.5
$\frac{1}{2}$	6.9	68.8
$\frac{3}{4}$	6.9	68.8
+5	6.8	68.9
cb	6.2	69.5

75.71

75.7

N	5.8	69.9
10'		
N	6.8	68.9
cb	7.2	68.5
+2	7.7	68.0
$\frac{1}{4}$	7.9	67.8
$\frac{1}{2}$	7.7	68.0
$\frac{3}{4}$	8.0	67.5
cb	8.3	67.4
S	9.2	66.5
+5	9.7	66.0

on Nch. S. side of Intersection for future Reford 12.26

63.15

T.P. 850

84.07

044

75.27

chk. on Plan. TEXAS + 40th Page 15

296

81.11

 $\frac{81.11}{100} = .8111$

Walker
3-15-21

X. Section T' st. 60' wide 10' cbs
From E.L. 37th to N.L. 38th 10' cbs
" " 38th to N.L. 40th 7.5' cbs

85.30

85.3

67

Page 16

			Elev. Stop of cb	cb		
	2.07	85.30	82.23	S	11.3	74.0
		E.L. 37 th ct.			11.0	74.3
					45' E	
N ₂	12.8	72.5		S	9.0	76.3
N	13.20	72.1		cb	8.7	76.6
Gut	13.7	71.6		i	8.9	76.4
i	13.7	71.6		cb	9.4	75.9
cb	13.9	71.4		i	10.1	75.2
i	13.7	71.6		cb	10.4	74.9
Gut.	14.4	70.9		N	10.7	74.6
Stop cb.	14.12	71.2			68' E	76.0
S	14.2	71.1		N	9.3	76.0
	4' E			+2	8.4	76.9
S	13.1	72.2		cb	8.1	77.2
cb	12.8	72.5		i	7.5	77.8
i	12.8	72.5		cb	7.4	77.9
cb	12.7	72.6		i	6.9	78.4
i	13.4	71.9		cb	6.3	79.0
cb	13.4	71.9		S	6.2	79.1
N	12.3	73.0			54' E	
	25' E			C	4.9	80.4
N	11.7	73.6		cb	5.4	79.9
cb	12.0	73.3		i	5.8	79.5
i	11.0	74.3		cb	5.7	79.6
cb	10.1	75.2		i	4.9	80.4
i	10.6	74.7		cb	5.5	79.8

85.30

85.3

+7	4.4	78.9
N ⁵	7.6	77.7
100' E		
N	6.7	78.6
cb	5.7	79.6
$\frac{1}{4}$	5.1	80.2
$\frac{1}{2}$	4.9	80.4
$\frac{3}{4}$	4.8	80.5
cb	4.3	81.0
S	4.0	81.3

140' E = E Con. Walk on South on line

S top of walk	1.60	83.7
S	1.7	83.6
cb	2.0	83.3
$\frac{1}{4}$	2.4	82.9
$\frac{1}{2}$	2.7	82.6
$\frac{3}{4}$	3.1	82.2
cb	3.0	82.3
N	3.0	82.3

166' E

N	2.9	82.4
cb	2.5	82.8
$\frac{1}{4}$	1.7	83.6
$\frac{1}{2}$	1.6	83.7
$\frac{3}{4}$	1.3	84.0
cb	1.1	84.2

85.30

85.393.1

S	1.1	84.2
185' E		
S	0.7	84.6
cb	0.6	84.7
$\frac{1}{4}$	0.9	84.4
$\frac{1}{2}$	0.9	84.4
$\frac{3}{4}$	0.8	84.5
+L	1.0	84.3
cb	0.8	84.5
N	1.6	83.7

200' E

N	1.3	84.0	
cb	0.7	84.6	
$\frac{1}{4}$	0.6	84.7	
$\frac{1}{2}$	0.4	84.9	
$\frac{3}{4}$	0.8	84.5	
cb	0.4	84.9	
S	0.3	85.0	
TP 810	93.07	0.33	84.97

250' E

S	6.7	86.5
cb	6.9	86.2
$\frac{1}{4}$	7.2	85.9
$\frac{1}{2}$	7.1	86.0
$\frac{3}{4}$	7.2	85.9
d	7.4	85.9

93.07

93.1

N	7.6	85.5
	277' E	
N	5.5	87.6
cb	5.6	87.5
i	5.9	87.2
d	6.1	87.0
i	6.0	87.1
cb	6.0	87.1
S	5.9	87.2
300' E = 2 con. walk on N 35' wide 54' in st.		
S	5.6	87.5
cb	5.6	87.5
i	5.5	87.6
d	5.1	88.0
i	5.1	88.0
cb	5.0	88.1
+ 46 = top of walk	4.9	88.1
N	4.9	88.2
	335' E	
N	4.7	88.4
cb	4.9	88.2
i	4.7	88.4
d	4.6	88.5
i	4.6	88.5
cb	5.2	87.9
S	5.3	87.8

93.07

93.1

59

	350' E	
i	4.8	88.3
cb	4.5	88.6
i	4.3	88.8
d	3.7	89.4
i	4.4	88.7
cb	4.9	89.2
N	5.0	88.1
	400' E	
N	5.2	87.9
cb	5.2	87.9
i	5.0	88.1
d	4.7	88.4
i	4.8	88.3
cb	4.7	88.4
S	4.7	88.4
	450' E	
S	4.1	89.0
cb	4.5	88.6
i	4.7	88.5
d	4.4	88.7
i	4.0	89.1
cb	4.1	89.0
N	4.0	89.1
466' E = d olive tree on S 10.5' in st. 6" dia.		
481' " " " " " " 10' " " 10' "		

93.07

93.1

500' E - to olive tree on S 10' in st 12" dia.

N	27	90.4
cb	33	89.8
$\frac{1}{4}$	35	89.6
d	35	89.6
$\frac{1}{4}$	35	89.6
cb	29	90.2
S	29	90.2

L 530' E

S	22	90.9
cb	25	90.6
$\frac{1}{4}$	28	90.3
d	31	90.0
$\frac{1}{4}$	27	90.4
cb	21	91.0
N	13	91.8

540' E

N	12	91.9
cb	19	91.2
$\frac{1}{4}$	22	90.9
d	22	90.9
$\frac{1}{4}$	21	91.0
cb	19	91.2
S	19	91.2

594' E

S	15	91.6
---	----	------

93.07

93.1

30

cb	15	91.6
$\frac{1}{4}$	17	91.5
d	14	91.7
$\frac{1}{4}$	12	91.9
cb	11	92.0
N	05	92.6

597' E

N	01	93.0
cb	03	92.8
+2	09	92.2
$\frac{1}{4}$	12	91.9
d	14	91.7
$\frac{1}{4}$	17	91.5
cb	15	91.6
S	13	91.8

600' E

S	10	92.1
Stop cb	096	92.1
Gut	14	91.7
$\frac{1}{4}$	15	91.6
d	11	92.0
$\frac{1}{4}$	11	92.0
Gut	06	92.5
N top of cb	0.00	93.1
N	+0.2	93.3

TP 307

96.14 0.00

93.07

96.14

96.1

10 cbs. 7.5' S from EL 3144000 E.L. 3844 = 0+00

N	2.5	93.6
N top of cb	2.96	93.1
Gut	3.4	92.7
$\frac{1}{4}$	3.3	92.8
$\frac{1}{2}$	3.5	92.6
$\frac{3}{4}$	3.9	92.2
Gut	4.3	91.8
S top of cb	4.05	92.1
S	3.7	92.4
5' E		
S	3.4	92.7
cb	3.2	92.9
+d	4.1	92.0
$\frac{1}{4}$	3.9	92.2
$\frac{1}{2}$	3.4	92.7
$\frac{3}{4}$	3.5	92.6
cb	3.2	93.1
N	1.9	94.2
50' E		
N	1.8	94.3
cb	2.1	94.0
$\frac{1}{4}$	2.5	93.6
$\frac{1}{2}$	2.8	93.3
$\frac{3}{4}$	2.8	93.3
cb	2.9	93.2

96.14

96.1

31

S	2.8	93.3
83' E = 2' Con Walk on N 4' House	0.95	95.19
100' E		
S	2.2	93.9
cb	2.1	94.0
$\frac{1}{4}$	2.1	94.0
$\frac{1}{2}$	2.0	94.1
$\frac{3}{4}$	2.1	94.0
cb	1.9	93.2
N	1.0	95.1
132' E = 2' Con Dr on N 4' Back	0.92	95.2
146' E = 2' Con Dr on N 4' Back	0.92	95.2
150' E		
N	1.2	94.9
cb	1.5	94.6
$\frac{1}{4}$	1.5	94.4
$\frac{1}{2}$	1.5	94.6
$\frac{3}{4}$	1.7	94.4
cb	1.8	94.3
S	1.7	94.4
177' E = 2' Con Walk on S	1.46	94.48
191' E = " " " " " 35' Back	1.37	94.77
200' E		
S	1.9	94.2
cb	2.0	94.1
$\frac{1}{4}$	2.2	93.9

96.14

96.1

d	22	93.9
i	24	93.7
cb	25	93.6
N	19	94.2
209' E = d Con. Dn. on N on line	227	93.87
222' E = d "Walk on" 3' back	256	93.58
235' E = d " " " S1' "	297	93.17

250' E

N	3.7	92.4
cb	1.2	91.9
i	4.0	92.1
d	4.0	92.1
i	4.1	92.0
cb	3.8	92.3
S	3.8	92.3
276' E = d Con. Walk on N 25' back	442	91.72

300' E

S	62	89.9
cb	62	89.9
i	62	89.9
d	60	90.1
i	60	90.1
cb	59	90.2
N	46	91.3
324' E = d Con. Walk on S		
N	52	90.9

96.14

96.1

32

+4	57	90.4
cb	68	89.3
i	72	88.9
d	70	89.1
i	72	88.9
cb	73	88.8
S	70	89.1
S on top of Walk	673	89.31

355' E

S	85	87.6
cb	88	87.3
i	89	87.2
d	86	87.5
i	88	87.3
cb	86	87.5
N	89	87.2

400' E

N	10.5	85.6
+8	11.2	84.9
cb	12.3	83.8
i	11.4	84.7
d	10.8	85.3
i	11.2	84.9
cb	11.4	84.7
S	11.6	84.5
TP 0.35	8363	12.86
		83.58

8363

83.6

446'E

S	2.6	81.0
cb	2.6	81.0
$\frac{1}{4}$	2.9	80.7
$\frac{1}{2}$	2.6	81.0
$\frac{3}{4}$	2.6	81.0
cb	3.7	79.9
+5	2.6	81.0
+8	0.6	83.0
N	0.6	83.0

500'E

N	4.8	78.8
+3	4.8	78.8
+6	7.2	76.4
+8	7.1	76.5
cb	7.8	75.8
$\frac{1}{4}$	7.0	76.6
$\frac{1}{2}$	6.9	76.7
$\frac{3}{4}$	7.4	76.2
cb	7.2	76.4
S	7.8	75.8

550'E

S	11.0	72.6
cb	10.9	72.7
$\frac{1}{4}$	11.3	72.3
$\frac{1}{2}$	11.0	72.6

8363

83.6

33

724

$\frac{1}{4}$	10.8	72.8
cb	11.1	72.5
+2	10.3	73.3
+7	9.4	74.2
N	9.1	74.5

595'E

N	12.0	71.6
cb	15.8	69.8
$\frac{1}{4}$	13.3	70.3
$\frac{1}{2}$	13.4	70.2
$\frac{3}{4}$	15.7	69.9
cb	13.7	69.9
S	12.8	70.8

600'E = N.L. 39th

S	13.8	69.8
cb	13.9	69.5
$\frac{1}{4}$	14.2	69.4
$\frac{1}{2}$	13.7	69.9
$\frac{3}{4}$	13.4	69.7
cb	14.0	69.6
N	13.4	70.0

T.P. 1.55

7237 13.09

70.52

Ncb

N	3.0	69.4
cb	2.9	69.5
$\frac{1}{4}$	2.5	69.9

72.39

72.41

8		28	69.6
$\frac{1}{4}$		31	69.3
cb		37	68.7
S		39	68.5
	N $\frac{1}{4}$		
S		27	69.7
cb		33	69.1
$\frac{1}{4}$		35	68.9
$\frac{1}{2}$		31	69.3
$\frac{1}{2}$		29	69.5
cb		30	69.4
N		31	69.3
	L		
N		29	69.5
cb		34	69.0
$\frac{1}{4}$		34	69.0
L on Rim M.H.		340	69.0
$\frac{1}{4}$		33	69.1
cb		31	69.3
S		29	69.5
	E $\frac{1}{4}$		
S		31	69.3
cb		35	68.9
$\frac{1}{4}$		36	68.8
$\frac{1}{2}$		37	68.7
$\frac{1}{2}$		37	68.7

72.39

72.4

34

cb		35	68.9
N		31	69.3
	E cb		
N		35	68.9
cb		40	68.4
$\frac{1}{4}$		42	68.2
$\frac{1}{2}$		40	68.4
$\frac{1}{2}$		42	68.2
cb		37	68.7
S		34	69.0
	Eh. 39 th = 0400		
S		42	68.2
cb		45	67.9
$\frac{1}{4}$		47	67.7
$\frac{1}{2}$		41	68.3
$\frac{1}{4}$		41	68.3
cb		42	68.2
N		40	68.4
	40'E		
N-5		6.9	65.5
N		6.8	65.6
cb		5.9	66.5
$\frac{1}{2}$		6.1	66.3
$\frac{1}{2}$		5.6	66.8
$\frac{1}{2}$		5.8	66.6
cb		6.0	66.4

72.39

72.4

+7		6.1	66.3
S		4.9	67.5
	65'E		
S		4.4	68.0
+2		6.6	65.8
cb		6.6	65.8
$\frac{1}{4}$		6.4	66.0
2		6.3	66.1
$\frac{1}{4}$		6.6	65.8
cb		6.6	65.8
+4		6.8	65.6
N		8.7	63.7
+10		9.1	63.3
	100'E		
-10		9.8	62.6
N		9.2	62.2
76		7.3	65.1
cb		6.9	65.5
$\frac{1}{2}$		6.6	65.8
2		6.8	65.6
$\frac{1}{4}$		7.5	64.9
cb		7.1	65.3
+7		7.3	65.1
S		5.3	67.1
	150'E		
S		7.1	65.3

72.39

64.9

35

+5		8.8	63.6
cb		8.6	63.8
$\frac{1}{4}$		8.3	64.1
2		8.3	64.1
$\frac{1}{4}$		8.4	64.0
cb		8.0	64.4
+8		8.1	64.3
N		10.1	62.3
+10		10.0	62.4
T.P. 7.37	64.95	9.81	62.58
	200'E		
-10		3.1	61.8
N		2.7	62.2
+2		2.1	62.8
cb		2.0	62.9
$\frac{1}{4}$		2.5	62.4
2		2.2	62.7
$\frac{1}{4}$		2.4	62.5
cb		2.4	62.5
+5		2.4	62.3
S		0.6	64.3
	235'E		
S		0.5	64.4
+5		3.0	61.9
cb		3.6	61.3
2		3.4	61.5

64.95

64.9

cb	7.3	57.6
+1	7.5	57.4
$\frac{1}{4}$	8.5	56.4
+2	7.7	57.2
$\frac{1}{2}$	7.2	57.7
$\frac{1}{2}$	7.5	57.4
cb	8.3	56.6
S	8.5	56.4
+5	8.8	56.1

425'E

-5	9.5	55.4
S	8.7	56.2
cb	8.0	56.9
$\frac{1}{4}$	7.9	57.0
$\frac{1}{2}$	7.8	57.1
+5	8.1	56.8
+6	7.1	55.8
$\frac{1}{4}$	7.1	55.8
+2	7.5	57.4
cb	6.7	58.2
+6	5.5	59.4
N	1.4	63.5

450'E

N	4.2	60.7
+5	6.6	58.3
cb	7.6	57.3

64.95

64.9

37

+3	7.8	57.1
$\frac{1}{4}$	9.7	55.2
+3	8.7	56.2
$\frac{1}{2}$	8.5	56.4
$\frac{1}{2}$	8.8	56.1
cb	9.4	55.5
S	10.0	54.9
+5	10.1	54.8

500'E

-5	11.4	53.5
S	11.5	53.4
cb	11.4	53.5
$\frac{1}{4}$	11.1	53.8
$\frac{1}{2}$	10.8	54.1
+5	10.8	54.1
$\frac{1}{4}$	11.9	53.0
+3	10.4	54.5
cb	10.3	54.6
+5	9.7	55.2
N	6.4	58.1

535'E

N	7.3	57.6
+5	10.1	54.8
cb	10.6	54.3
+6	11.2	53.7
$\frac{1}{2}$	12.3	52.6

64.95

64.9

cb	7.3	57.6
+1	7.5	57.4
$\frac{1}{4}$	8.5	56.4
+2	7.7	57.2
$\frac{1}{2}$	7.2	57.7
$\frac{1}{2}$	7.5	57.4
cb	8.3	56.6
S	8.5	56.4
+5	8.8	56.1

425'E

-5	9.5	55.4
S	8.7	56.2
cb	8.0	56.9
$\frac{1}{4}$	7.9	57.0
$\frac{1}{2}$	7.8	57.1
+5	8.1	56.8
+6	7.1	55.8
$\frac{1}{4}$	7.1	55.8
+2	7.5	57.4
cb	6.7	58.2
+6	5.5	59.4
N	1.4	63.5

450'E

N	4.2	60.7
+5	6.6	58.3
cb	7.6	57.3

64.95

64.9

37

+3	7.8	57.1
$\frac{1}{4}$	9.7	55.2
+3	8.7	56.2
$\frac{1}{2}$	8.5	56.4
$\frac{1}{2}$	8.8	56.1
cb	9.4	55.5
S	10.0	54.9
+5	10.1	54.8

500'E

-5	11.4	53.5
S	11.5	53.4
cb	11.4	53.5
$\frac{1}{4}$	11.1	53.8
$\frac{1}{2}$	10.8	54.1
+5	10.8	54.1
$\frac{1}{4}$	11.9	53.0
+3	10.4	54.5
cb	10.3	54.6
+5	9.7	55.2
N	6.4	58.1

535'E

N	7.3	57.6
+5	10.1	54.8
cb	10.6	54.3
+6	11.2	53.7
$\frac{1}{2}$	12.3	52.6

64.95

64.9

64.95

64.9

38

63.5

+3	11.8	53.1
2	11.9	53.0
$\frac{1}{4}$	11.7	53.2
6	12.1	52.8
5	12.1	52.8
+5	11.6	53.3

541'E

-5	11.8	53.1
5	12.4	52.5
6	12.2	52.7
$\frac{1}{4}$	12.0	52.9
2	12.1	52.8
+6	12.4	52.5
$\frac{1}{2}$	10.6	54.3
6	8.5	56.4
N	7.1	57.8

550'E

N	7.8	59.1
6	9.6	55.3
+5	10.6	54.3
$\frac{1}{4}$	12.5	52.4
+6	12.5	52.4
2	12.2	52.7
$\frac{1}{2}$	11.7	53.2
6	12.6	52.3
5	12.6	52.3

+5	12.6	52.3
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5+75-

-5	12.6	52.3
5	12.6	52.3
6	12.2	52.7
$\frac{1}{4}$	12.0	52.9
6	12.5	52.4
$\frac{1}{4}$	12.4	52.5
6	11.7	53.2
+5	11.1	53.8
N	8.3	56.6

T.P. 1123

63.54

12.64

52.31

600'E

N	9.4	54.1
+5	11.1	52.4
6	11.3	52.2
$\frac{1}{2}$	11.5	52.0
+5	12.5	51.0
6	12.5	51.0
+2	11.5	52.0
$\frac{1}{4}$	11.2	52.1
6	12.3	51.2
5	12.3	51.2
+5	12.3	51.2

652.19 E = 112.404

-5

13.1

60.4

6354

63.5

39

S	131	50.4
cb	129	50.6
$\frac{1}{4}$	129	50.6
$\frac{1}{4}$	125	51.0
$\frac{1}{4}$	121	51.4
cb	120	51.5
N	113	52.2

10'E

N	112	52.3
cb	122	51.3
$\frac{1}{4}$	123	51.2
$\frac{1}{4}$	127	50.8
$\frac{1}{4}$	131	50.4
cb	135	50.0
S	135	50.0
+5	135	50.0

chk. on Rock Page 26

+ 0.01

63.55

63.45 = E/cv. of Rock

0.10

Walker
3-16-27

X. Section TRINS st. 50' wide
From Moore st to La Jolla Blvd.

3884

40

BM. Moore st.
approx. 200' E
of RT. NE Viaduct

4.74 32.67 27.73
T.P. 12.92 3884 675 25.92

X.L. Moore -5'

-5 14.7 24.1
S 15.2 23.6
cb 15.0 23.8
1/2 14.5 24.3
1/2 14.2 24.6
1/4 14.0 24.8
cb 14.0 24.8
N 13.0 25.8

X.L. Moore 10' cbs
7.5' 25

N 13.0 25.8
cb 14.0 24.9
1/4 14.0 24.8
1/2 13.9 24.9
1/4 14.4 24.4
cb 15.2 23.6
S 14.8 24.0
+5 14.6 24.2

Xcb

-5 14.3 24.5
S 14.1 24.7
cb 14.6 24.2
1/4 14.0 24.8

Plotted in profile by Tolman
5-11-27

1/2	14.0	24.8
1/2	13.8	25.0
cb	13.5	25.3
N	13.5	25.3
N 1/2		
N	13.0	25.8
cb	13.0	25.5
1/2	13.5	25.3
1/2	13.7	25.1
1/4	14.1	24.7
cb	14.0	24.8
S	13.9	24.7
+5	13.9	24.9
1/2		
5	13.8	25.0
S	13.8	25.0
cb	13.6	25.2
1/4	13.9	24.9
2 on Man.	13.66	25.1
1/4	13.4	25.4
cb	13.0	25.8
N	12.8	26.0
N 1/2		
N	12.8	26.0
cb	13.2	25.6
1/4	13.2	25.6

d	133	25.5
$\frac{1}{4}$	134	25.4
cb	138	25.0
s	139	24.9
+5	139	24.9
s	127	26.1
+7	123	26.5
+8	132	25.4
cb	134	25.4
$\frac{1}{4}$	132	25.6
d	120	25.8
$\frac{1}{4}$	128	26.0
cb	129	25.9
N	123	26.5

Elev. Moore = 0400

N	11.5	27.3
cb	12.4	26.4
$\frac{1}{4}$	125	25.3
d	127	26.1
$\frac{1}{4}$	130	25.8
+5	13.1	25.7
+6	12.0	26.8
cb	11.9	26.9
s	120	26.8

27.97

3'E = d Can Platform to Grocery store 10.87 on N 5' wide road on line
Elev. of floor inside of store is same

50'E

s	83	30.5
cb	85	30.3
+5	87	30.1
$\frac{1}{4}$	94	29.4
d	94	29.4
$\frac{1}{4}$	95	28.3
d	94	29.4
+5	87	30.1
N	81	30.7

100'E

N	60	32.8
cb	64	32.4
$\frac{1}{4}$	66	32.2
d	65	32.3
$\frac{1}{4}$	65	32.3
+2	57	33.1
cb	57	33.1
s	61	34.7

137'E = d Can Dr on N 4' Bast

s	42	34.6
cb	42	34.6
+5	41	34.7
$\frac{1}{4}$	46	34.2
d	45	34.3
$\frac{1}{4}$	45	34.3

3884

cb	47	34.1
N	44	34.4
+1 = top Dr.	436	34.48

170'E

N	33	35.5
cb	29	35.9
$\frac{1}{2}$	32	35.6
$\frac{1}{4}$	31	35.7
$\frac{1}{4}$	35	35.3
cb	28	36.0
+2	27	36.6
S	20	36.8

200'E

S	15	37.3
+4	12	37.6
cb	06	38.4
+3	10	37.8
$\frac{1}{4}$	19	36.9
$\frac{1}{2}$	16	37.2
$\frac{1}{2}$	16	37.2
cb	17	37.1
+3	11	37.7
N	09	37.9

TP 13.10 51.74 220 38.64

250'E

N 108 40.9

5174

12

cb	11.0	40.7
$\frac{1}{2}$	10.9	40.8
$\frac{1}{4}$	10.7	41.0
$\frac{1}{2}$	10.5	41.2
+5	10.9	40.8
cb	10.3	41.2
S	10.7	41.0

300'E - H.L. Jefferson 10' cbs 7.575

S	7.2	44.5
cb	6.9	44.8
+2	7.5	44.4
$\frac{1}{4}$	7.1	44.6
$\frac{1}{2}$	7.3	44.4
$\frac{1}{2}$	7.6	44.1
cb	7.8	43.9
N	8.1	43.6

N'cb

N	7.5	44.2
cb	7.0	44.7
$\frac{1}{2}$	6.9	44.8
$\frac{1}{4}$	6.6	45.1
$\frac{1}{2}$	6.5	45.2
+5	6.7	45.0
cb	6.4	45.3
S	6.3	45.2

N $\frac{1}{2}$

S	53	46.4
cb	57	46.0
+3	64	45.9
$\frac{1}{4}$	60	45.7
$\frac{1}{2}$	61	45.6
$\frac{1}{4}$	64	45.3
cb	64	45.3
N	70	44.7
$\frac{1}{2}$		
N	69	44.8
cb	60	45.7
$\frac{1}{4}$	57	46.0
$\frac{1}{2}$	54	46.3
$\frac{1}{4}$	53	46.4
+5	56	46.1
cb	54	46.3
S	49	46.8
$E \frac{1}{4}$		
S	47	47.0
cb	50	46.7
+2	55	46.2
$\frac{1}{4}$	50	46.7
$\frac{1}{2}$	50	46.7
$\frac{1}{4}$	52	46.1
cb	57	46.0
N	63	45.4

E. cb

N	48	46.9
cb	49	46.8
$\frac{1}{4}$	47	47.0
$\frac{1}{2}$	45	47.4
$\frac{1}{4}$	44	47.3
+5	50	46.7
cb	46	47.1
S	42	47.5
$E. L. Jefferson = 0+00$		
S	40	47.7
cb	39	47.8
+2	45	47.4
$\frac{1}{4}$	40	47.7
$\frac{1}{2}$	41	47.6
$\frac{1}{4}$	40	47.7
+5	45	47.2
cb	40	47.7
N	42	47.5
$52' E = 2$ Dble. Garage on N. con. Floor 16' wide on line		
N = Garage Floor	190	49.8
cb	17	50.0
$\frac{1}{4}$	14	50.3
$\frac{1}{2}$	12	50.5
$\frac{1}{4}$	10	50.7
cb	16	50.1

+1		0.5	51.2
S		0.2	51.5
T.P.	6.73	51.45	1.02
			50.72
70' N = \angle Pepper tree on N 10' inst 16" dia.			
87' " " " " " " " " " " " " 6' "			
100' " " " " " " " " " " " " 8' "			

Approx 96.9' E on S = Section at Rt. Angles to Trias

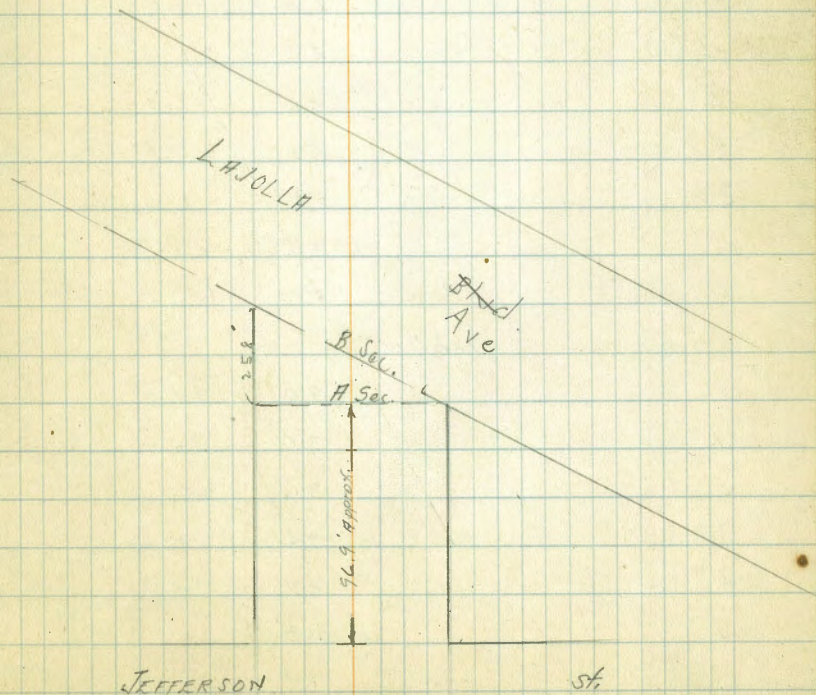
S	2.7	54.8
+8	3.2	54.3
cb	4.1	53.4
+2	4.8	52.7
$\frac{1}{4}$	4.5	53.0
$\frac{1}{4}$	5.0	52.5
$\frac{1}{4}$	5.2	52.3
cb	5.3	52.2
N	5.5	52.0

96.9' on E Section Parallel With La Jolla Blvd

N	4.4	53.1
N top of cb	4.62	52.83
Gut. on Parking	4.81	52.64
$\frac{1}{4}$ " "	4.85	53.10
$\frac{1}{4}$ " "	3.98	53.47
$\frac{1}{4}$ " "	3.77	53.68
Gut " "	3.78	53.67
S top of cb	3.36	54.09
S	2.7	54.8

T.P. 042	44.92	12.95	49.50
T.P. 106	33.00	12.98	31.94

This H.F. Used on Page 45



Walker
3-16-27

X. Section Moore St. 60' wide
From N.L. Trias St. to Sh. Ampudia

10' cbs
7.5' 45

3300

45

3300 = N.L. From Page 44

N.L. Trias

W	7.5	25.5
cb	7.8	25.2
$\frac{1}{2}$	7.2	25.8
$\frac{1}{4}$	6.9	26.1
$\frac{1}{4}$	7.0	26.0
cb	6.5	26.5
E	5.6	27.4

50' N

E	4.0	29.0
cb	4.3	28.7
$\frac{1}{2}$	5.0	28.0
$\frac{1}{4}$	5.2	27.8
$\frac{1}{4}$	5.4	27.6
cb	5.3	27.7
W	5.1	27.9

100' N

W	3.0	30.0
cb	3.0	30.0
$\frac{1}{2}$	3.6	29.4
$\frac{1}{4}$	3.4	29.6
$\frac{1}{4}$	2.9	30.1
cb	2.3	30.7
E	2.1	30.9

135' N

Plotted by Tolman 5/18/27

E	1.5	31.5
cb	1.9	31.1
$\frac{1}{2}$	2.4	30.6
$\frac{1}{4}$	2.7	30.3
$\frac{1}{4}$	2.7	30.3
cb	2.4	30.6
W	2.4	30.6

170' N

W	3.2	29.8
cb	2.8	30.2
$\frac{1}{2}$	2.8	30.2
$\frac{1}{4}$	2.6	30.5
$\frac{1}{4}$	2.6	30.4
cb	2.1	30.9
E	1.8	31.2

200' N

E	2.0	31.0
cb	2.6	30.4
$\frac{1}{2}$	2.8	30.2
$\frac{1}{4}$	2.9	30.1
$\frac{1}{4}$	3.3	29.7
cb	3.2	29.8
W	3.3	29.7

250' N

W	4.2	28.8
cb	3.6	29.4

$\frac{1}{4}$		39	29.1
$\frac{1}{2}$		38	29.2
$\frac{3}{4}$		37	29.3
cb		33	29.7
E		28	30.2

300' N = SL.

E		28	29.2
E top of cb		404	28.96
Gut		45	28.5
$\frac{1}{2}$		45	28.5
$\frac{1}{4}$		46	28.4
$\frac{1}{2}$		49	28.1
Gut		50	28.0
N top of cb		500	28.00
N		48	28.2
T.P.	3.40	31.06	5.34
chk on	BM. Wood 400' E. of Bridge	3.38	27.68

$$\begin{array}{r} 27.73 = \text{EM} \\ - 1.005 \\ \hline \end{array}$$

Walker
3-16-27

X. Section 29th St. 60' wide 10' cbs
From Broadway to C St. 10' $\frac{1}{4}$ S.

195.75

47

S.E. BP
Broadway 1.30' 0.67 195.75 195.08

N cb Line Bdwy.

E	13.0	182.8
cb	12.8	183.0
$\frac{1}{4}$	12.5	183.3
$\frac{1}{2}$	12.3	183.5
$\frac{3}{4}$	12.1	183.7
cb	11.8	184.0
N	11.4	184.4
+ 12		
N	10.9	184.9
cb	11.2	184.6
$\frac{1}{4}$	11.3	184.5
$\frac{1}{2}$	11.4	184.4
$\frac{3}{4}$	11.6	184.2
cb	11.4	184.4
E	11.6	184.2

N.H. Bdwy. = 0+00

E	10.0	185.8 ✓
cb	9.8	185.0
$\frac{1}{4}$	11.2	184.6
$\frac{1}{2}$	11.2	184.6 ✓
$\frac{3}{4}$	11.3	184.5
cb	10.6	185.2
N	10.2	185.6 ✓

6' N of N.H. Bdwy.

N	6.5	189.3 ✓
+6	7.5	187.3
+8	9.4	186.4
cb	11.0	184.8
$\frac{1}{4}$	10.8	185.0
$\frac{1}{2}$	10.9	184.9 ✓
+3	10.8	185.0
+5	9.5	186.3
$\frac{1}{4}$	6.5	189.3
+1	6.0	189.8
cb	5.2	190.2
E	5.6	190.2 ✓

11' N

E	5.4	190.4 ✓
+9	5.4	190.4
cb	6.4	189.4
$\frac{1}{4}$	6.0	189.8
+2	6.0	189.8
+4	9.8	186.0
$\frac{1}{2}$	10.4	185.4 ✓
$\frac{3}{4}$	10.6	185.2
cb	10.2	185.6
+3	8.3	187.5
+5	5.2	190.6
N	4.5	191.2 ✓

44' N

W	3.4	192.4	✓
+8	6.1	189.7	
cb	6.8	189.0	
$\frac{1}{4}$	7.7	188.1	
L	7.5	188.3	✓
+5	7.5	188.3	
+7	6.6	189.2	
$\frac{1}{4}$	5.3	190.5	
+3	5.3	190.5	
+4	6.1	189.7	
+8	6.0	189.8	
+9	5.4	190.4	
cb	4.7	191.1	
E	4.9	191.9	✓
49' N = S. edge Oble. Garage on W. dirt floor, on line			
E	4.9	190.9	✓
cb	4.9	190.9	
$\frac{1}{4}$	5.3	190.5	
+3	7.0	188.8	
L	7.4	188.4	✓
$\frac{1}{4}$	7.1	188.7	
cb	6.6	189.2	
W = dirt floor of Garage	4.9	190.9	✓
67' N = N. edge Oble. Garage on W. on line dirt floor			
W = Garage Floor	4.7	191.1	✓

cb	5.7	190.1	
$\frac{1}{4}$	6.0	189.8	
L	6.3	189.5	✓
+5	6.2	189.6	
$\frac{1}{4}$	4.6	191.2	
cb	4.5	191.3	
E	4.9	190.9	✓
69' E			
E	4.9	190.9	✓
cb	4.5	191.3	
$\frac{1}{4}$	4.6	191.2	
+5	6.1	189.7	
L	6.0	189.8	✓
$\frac{1}{4}$	5.8	190.0	
cb	5.4	190.4	
+5	4.5	191.3	
W	3.6	192.2	✓
Rod on Ground, steps = 2.8 top of 12' = 1.48			
71' N = L. of steps to house on W. 5.4' Back		193.0	193.0
		194.2	194.27
100' N = L. of steps to house on W. 12' Back with N. Entrance			
-12 on top of steps	1.45	194.30	
-12 Ground Bottom of steps	2.1	193.7	✓
W	2.7	193.1	✓
+6	3.7	192.1	
cb	4.0	191.8	
$\frac{1}{4}$	4.3	191.5	
L	4.7	191.1	✓

z	4.7	191.1	
cb	4.8	191.0	
E	5.3	190.5 ✓	
110' N			
E	5.6	190.2 ✓	
cb	5.4	190.4	
z	4.6	191.2	
z	4.1	191.7 ✓	
z	3.8	192.0	
+5	3.3	192.5	
cb	3.1	192.7	
W	2.8	193.0 ✓	
134' N = ^{to house} end of Cor. Walk on W. 4' wide	2.35	0.5' back of line 193.40	
150' N = Garage on E dirt Floor on line			
W	3.0	192.8 ✓	
cb	3.5	192.3	
z	4.4	191.2	
z	5.3	190.5 ✓	
z	6.2	189.6	
cb			
+5	8.0	187.8	
E on Garage dirt Floor	8.1	187.7 ✓	
175' N = S end of House on E 4.5' Back Cor. Foundation			
- 4.5 = top of Foundation Also Elev. of Ground	10.10	185.65	
E	10.0	185.6 ✓	
+4	8.7	187.1	

cb	8.4	187.4	
+4	8.2	187.6	
+6	7.5	188.3	
z	7.2	188.6	
z	6.3	189.5 ✓	
z	5.7	190.1	
+6	4.5	191.3	
cb	4.2	191.6	
W	3.2	192.6 ✓	
+1 on Ground	2.8	193.0	
+1 on top of ^{1st} steps to House on W	1.85	193.90	194.00
212' N = L. of Steps to Houses on W + N			
-5.2' = Ground at steps	4.2	191.6	
-5.2' = top of ^{1st} step	3.37		192.58
W	4.5	191.3 ✓	
cb	6.1	189.7	
z	7.6	188.2	
z	8.5	187.3 ✓	
z	9.6	186.2	
+7	10.9	184.9	
cb	10.9	184.9	
E	10.9	184.9 ✓	
E ⁺¹ on top of 1st step	9.97	185.78	185.78
815' N = N end of House on E	10.2		185.6
221' N			
-10	15.3	180.5	

19575

-2	196	181.2
E	129	182.9 ✓
cb	129	182.9
+5	11.3	184.5
$\frac{1}{2}$	10.3	185.5
$\frac{1}{4}$	9.5	186.3 ✓
$\frac{1}{2}$	8.2	187.6
cb	7.1	188.7
W	5.1	190.7 ✓

224'N

W	5.5	190.3 ✓
cb	7.4	188.4
$\frac{1}{2}$	8.6	187.2
$\frac{1}{4}$	9.7	186.1 ✓
$\frac{1}{2}$	10.3	185.5
+5	11.5	184.3
cb	13.3	182.5
E	15.0	180.8 ✓
+10	16.3	179.5
T.P.	6.02	189.64
	12.13	183.22

250'N

-10	139	175.7
E	11.5	178.1 ✓
cb	10.3	179.3
+5	8.0	181.6
$\frac{1}{4}$	7.4	182.2

18964

50

$\frac{1}{2}$	6.2	183.4 ✓
+7	4.5	185.1
$\frac{1}{4}$	3.9	185.7
+5	2.7	186.9
W	0.8	189.8 ✓

275'N

W	1.4	188.2 ✓
+8	3.0	186.6
cb	3.0	186.6
+5	5.1	184.5
$\frac{1}{4}$	5.3	184.3
+5	8.7	180.9
$\frac{1}{2}$	8.8	180.8 ✓
+5	10.2	179.4
$\frac{1}{4}$	10.6	179.0
+5	11.1	178.5
cb	13.1	176.5
+5	14.5	175.1
E	15.3	174.3 ✓
+10	17.5	172.1

290'N

-10	18.3	171.3
E	15.8	173.8 ✓
+5	14.2	175.4
cb	13.7	175.9
+5	11.7	177.9

$\frac{1}{2}$	114	178.2
+5	121	177.5
$\frac{1}{2}$	108	178.8 ✓
+5	101	179.5
$\frac{1}{4}$	84	181.2
+4	56	184.0
cb	55	184.1
w	50	184.6 ✓

297' N

w	53	184.3 ✓
cb	56	184.0
+0	76	182.0
$\frac{1}{4}$	107	178.9
$\frac{1}{2}$	122	177.4 ✓
$\frac{1}{4}$	132	176.4
cb	140	175.6
E	145	175.1 ✓
+5	146	175.0 ✓

3025' S.W. Cst

E	145	175.1 ✓
E top cb	1465	174.99 ✓
" Gut on Paving	1514	174.52
$\frac{1}{4}$ " "	1471	174.93
$\frac{1}{2}$ " "	1440	175.24 ✓
$\frac{1}{2}$ " "	1428	175.36
Gut " "	1430	175.34

W top cb	1364	176.00 ✓
W	1355	176.1 ✓
TP 862	197.87	0.39
TP 484	199.69	3.02
Chk on B.M. S.E. B.M. + 3055	4.62	195.07
		195.08 = B.M.
		+ 0.01

Walker
3-17-27

X. Section Monroe Ave. 60' wide 10' ch.
10' 48
From a Point 139.10 N.W. 1/4 Monona St. to .53' of st.

384.93

52

				N	7.9	377.0	
	6.70	380.15	382.45		0+38		
TP	3.55	384.93	8.77	381.38	N	7.8	377.1
	139.10' N.W. 1/4 Monona = 0+20 on South			cb	7.8	377.1	
S			7.7	377.2	cb	7.2	377.7
cb			7.5	377.4	cb	7.3	377.6
1/4			7.6	377.3	1/4	7.5	377.4
1/4			7.5	377.4	cb	7.4	377.5
1/4			7.6	377.3	S	7.3	377.6
cb			7.8	377.1		0+75	
N			8.0	376.9	S	7.0	377.9
	0+13			cb	7.0	377.9	
N			8.2	376.7	1/4	7.3	377.6
cb			8.1	376.8	1/4	6.8	378.1
1/4			7.9	377.0	1/4	7.0	377.9
1/4			7.8	377.1	cb	7.3	377.6
1/4			8.0	376.9	N	7.7	377.2
cb			7.5	377.4		1+00	
S			7.3	377.6	N	6.9	378.0
	0+24			cb	6.8	378.1	
S			6.5	378.4	1/4	6.6	378.3
cb			6.6	378.3	1/4	6.3	378.6
1/4			7.8	377.1	1/4	7.1	377.8
1/4			7.4	377.5	cb	6.7	378.2
1/4			7.3	377.6	S	6.8	378.1
cb			7.8	377.1			

139.10' = N.W. 1/4 Monona

S	63	378.6
cb	62	378.7
$\frac{1}{4}$	67	378.2
$\frac{1}{2}$	67	378.7
$\frac{3}{4}$	69	378.0
cb	68	378.1
N	69	378.0

E.L. Moon = 0+00

N	63	378.6
cb	58	379.1
$\frac{1}{4}$	62	378.7
$\frac{1}{2}$	58	379.1
$\frac{3}{4}$	61	378.8
cb	62	378.7
S	62	378.7

50' E

S	58	379.1
cb	58	379.1
$\frac{1}{4}$	60	378.9
$\frac{1}{2}$	53	379.6
$\frac{3}{4}$	55	379.4
cb	59	379.0
N	61	378.8

100' E

N	57	379.2
cb	55	379.4

$\frac{1}{4}$	56	379.3
$\frac{1}{2}$	50	379.9
$\frac{3}{4}$	54	379.5
+	57	379.2
+	47	380.2
cb	47	380.2
S	51	379.8

121' E

S	52	379.7
cb	50	379.9
$\frac{1}{4}$	51	379.8
$\frac{1}{2}$	46	380.3
+	44	380.5
$\frac{3}{4}$	50	379.9
cb	53	379.6
N	54	379.5

135' E = M. Hon. R. Imp. & St.

47P	380.15
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150' E

N	48	380.1
cb	45	380.4
$\frac{1}{4}$	44	380.5
$\frac{1}{2}$	46	380.3
$\frac{3}{4}$	49	380.0
cb	50	379.9
S	49	380.0

200' E

S	47	380.2
cb	42	380.7
+5	46	380.3
$\frac{1}{4}$	46	380.3
$\frac{1}{2}$	38	381.1
$\frac{3}{4}$	41	380.8
cb	40	380.9
N	41	380.8

220'E

N	42	380.7
cb	43	380.6
$\frac{1}{4}$	41	380.8
$\frac{1}{2}$	37	381.2
$\frac{3}{4}$	45	380.4
+5	45	380.4
+7	39	381.0
cb	36	381.3
S	35	381.4

235'E

S	40	380.9
cb	37	381.2
$\frac{1}{4}$	43	380.6
$\frac{1}{2}$	37	381.2
$\frac{3}{4}$	38	381.1
+6	40	380.9
cb	31	381.8

N	32	381.7
	255'E	
N	42	380.7
cb	41	380.8
$\frac{1}{4}$	40	380.9
$\frac{1}{2}$	36	381.3
$\frac{3}{4}$	40	380.9
cb	39	381.1
S	33	381.6

270'E = W.L. 50' + 4' st

S	37	381.2
cb	38	381.1
$\frac{1}{4}$	39	381.0
$\frac{1}{2}$	34	381.5
$\frac{3}{4}$	41	380.8
cb	40	380.9
N	40	380.9

E.L. 50' = 0+00

N	33	381.6
cb	33	381.6
$\frac{1}{4}$	39	381.0
$\frac{1}{2}$	33	381.6
$\frac{3}{4}$	36	381.3
cb	31	381.8
S	30	381.9

50'E

S	24	382.5
cb	27	382.2
$\frac{1}{2}$	29	382.0
$\frac{1}{4}$	24	382.5
$\frac{1}{4}$	20	381.9
cb	27	382.2
N	29	382.0

100' E

N	19	383.0
cb	25	382.4
$\frac{1}{2}$	25	382.4
$\frac{1}{4}$	17	383.2
$\frac{1}{4}$	17	383.2
cb	18	383.1
S	20	382.9

TP	E57	388.93	157	382.36
	135'E = MH. Est.		548	383.45

150' E

S	50	383.9
cb	54	383.5
$\frac{1}{2}$	54	383.5
$\frac{1}{4}$	55	383.4
$\frac{1}{4}$	57	383.2
cb	58	383.1
N	56	383.4

200' E

N	56	383.9
cb	56	383.9
$\frac{1}{2}$	56	383.3
$\frac{1}{4}$	53	383.6
$\frac{1}{4}$	56	383.4
cb	56	383.4
S	54	383.5

215' E

S	52	383.7
cb	48	384.1
$\frac{1}{2}$	53	383.6
$\frac{1}{4}$	50	383.9
$\frac{1}{4}$	55	383.4
cb	55	383.4
N	53	383.6

230' E

N	53	383.6
cb	53	383.6
$\frac{1}{2}$	53	383.6
$\frac{1}{4}$	49	384.0
$\frac{1}{4}$	51	383.8
$\frac{1}{4}$	44	384.5
cb	42	384.7
S	45	384.4

215' E

S	50	383.9
---	----	-------

cb	48	384.1
$\frac{1}{2}$	50	383.9
$\frac{2}{2}$	47	384.2
$\frac{1}{2}$	51	383.8
cb	50	383.9
N	51	383.8

270'E = N. Altadena

N	52	383.7
cb	52	383.7
$\frac{1}{2}$	52	383.7
$\frac{2}{2}$	48	384.1
$\frac{1}{2}$	51	383.8
cb	48	384.1
S	41	384.1

E. Altadena = 2700

S	52	383.7
cb	50	383.9
$\frac{1}{2}$	52	383.7
$\frac{2}{2}$	51	383.8
$\frac{1}{2}$	57	383.2
cb	57	383.2
N	57	383.2

50'E

N	58	383.1
cb	58	383.1
$\frac{1}{2}$	58	383.1

$\frac{2}{2}$	52	383.7
$\frac{1}{2}$	54	383.5
cb	54	383.5
S	54	383.5

100'E

S	53	383.6
cb	53	383.6
$\frac{1}{2}$	53	383.6
$\frac{2}{2}$	51	383.8
$\frac{1}{2}$	54	383.5
cb	54	383.5
N	54	383.5

150'E

N	55	383.4
cb	55	383.4
$\frac{1}{2}$	55	383.4
$\frac{2}{2}$	51	383.8
$\frac{1}{2}$	53	383.6
cb	53	383.6
S	48	384.1

200'E

S	47	384.7
cb	44	384.5
$\frac{1}{2}$	51	383.8
$\frac{2}{2}$	49	384.0
$\frac{1}{2}$	54	383.5

cb		51	383.5
N		51	383.5
	235'E		
N		52	383.7
cb		52	383.7
$\frac{1}{4}$		52	383.7
$\frac{1}{2}$		47	384.2
$\frac{3}{4}$		47	384.2
cb		46	384.3
S		40	384.9
	270'E = N 6.51st ct.		
S		40	384.9
cb		45	384.4
$\frac{1}{4}$		50	383.9
$\frac{1}{2}$		50	383.9
$\frac{3}{4}$		52	383.7
cb		51	383.8
N		51	383.8
	Ncb		
N		50	383.9
cb		52	383.7
$\frac{1}{4}$		55	383.4
$\frac{1}{2}$		48	384.1
$\frac{3}{4}$		48	384.1
cb		46	384.3
S		45	384.4

	N 2		
S		46	384.3
$\frac{1}{4}$		46	384.3
$\frac{1}{2}$		47	384.2
$\frac{3}{4}$		47	384.2
$\frac{1}{4}$		52	383.7
cb		52	383.7
N		53	383.6
	2		
N		50	383.9
cb		50	383.9
$\frac{1}{4}$		49	384.0
$\frac{1}{2}$		45	384.4
$\frac{3}{4}$		44	384.5
cb		42	384.7
S		40	384.9
	E 1/4		
S		45	384.4
$\frac{1}{4}$		47	384.2
$\frac{1}{2}$		46	384.3
$\frac{3}{4}$		47	384.2
$\frac{1}{4}$		49	384.0
cb		49	384.0
N		51	383.8
	Ecb		
N		47	384.2

d		49	384.0
$\frac{1}{2}$		51	383.8
d		47	384.2
$\frac{1}{2}$		47	384.2
cb		47	384.2
S		41	384.8
	EL 51 st Sta = 0+00		
S		43	384.6
cb		45	384.4
$\frac{1}{2}$		46	384.3
d		46	384.3
$\frac{1}{2}$		49	384.0
d		47	384.2
N		49	384.0
T.P.	656 390.66	483	384.10
	50' E		
N		60	384.7
cb		62	384.5
+5		69	383.8
$\frac{1}{2}$		66	384.1
d		60	384.7
$\frac{1}{2}$		62	384.3
cb		61	384.6
S		56	385.1
	100' E		
S		50	385.7

cb		57	385.0
$\frac{1}{2}$		62	384.5
d		59	384.8
$\frac{1}{2}$		63	384.4
+5		67	384.0
cb		60	384.7
N		56	385.1
	135' E = 174' on Rim	564	385.02
	150' E	53	
N		50	385.7
cb		59	384.8
+5		63	384.4
$\frac{1}{2}$		59	384.8
d		53	385.4
$\frac{1}{2}$		58	384.9
cb		53	385.4
S		45	386.2
	200' E		
S		42	386.5
+2		50	385.7
cb		53	385.4
$\frac{1}{2}$		57	385.0
d		50	385.7
$\frac{1}{2}$		56	385.1
+5		61	384.6
cb		54	385.3

39066

+7		51	385.6
N		45	386.2
	235'E		
N		44	386.3
cb		51	385.6
+5		57	385.0
$\frac{1}{4}$		51	385.6
$\frac{1}{2}$		47	386.0
$\frac{1}{4}$		54	385.3
cb		50	385.7
+7		48	385.9
S		38	386.9
	270'E = N. 52nd St.	10' obs. 10' 45.	
S		40	386.7
cb		48	385.9
$\frac{1}{4}$		52	385.5
$\frac{1}{2}$		45	386.2
$\frac{1}{4}$		52	385.5
+5		55	385.2
d		49	385.8
N		47	386.0
TP	578 39224	420	386.6
	Ncb		
N		62	386.0
cb		64	385.8
+5		70	385.2

39224

59

$\frac{1}{4}$		68	385.4
$\frac{1}{2}$		63	385.9
$\frac{1}{4}$		69	385.4
cb		65	385.7
S		63	385.9
	N $\frac{1}{2}$		
S		67	385.5
cb		67	385.5
$\frac{1}{4}$		67	385.5
$\frac{1}{2}$		63	385.9
$\frac{1}{4}$		65	385.7
cb		65	385.7
N		65	385.7
N		63	385.9
cb		63	385.9
$\frac{1}{4}$		64	385.8
$\frac{1}{2}$		61	386.1
$\frac{1}{4}$		64	385.8
cb		64	385.8
S		65	385.7
S		67	385.5
cb		67	385.5
$\frac{1}{4}$		67	385.5
$\frac{1}{2}$		64	385.8

SW pole

Moore + 52nd

39224

$\frac{1}{4}$	66	385.6
cb	66	385.6
N	65	385.7
E cb		
N	65	385.7
cb	66	385.6
$\frac{1}{4}$	67	385.5
$\frac{1}{2}$	65	385.7
$\frac{1}{4}$	67	385.5
cb	68	385.4
S	65	385.7
E.L. 5280 st. = 0+00		
S	62	386.0
cb	63	385.9
$\frac{1}{4}$	66	385.6
$\frac{1}{2}$	63	385.9
$\frac{1}{4}$	67	385.5
cb	63	385.9
N	64	385.8
50' E		
-5	67	385.5
N	63	385.9
cb	62	386.0
$\frac{1}{4}$	63	385.9
$\frac{1}{2}$	61	386.1
$\frac{1}{4}$	62	386.0

39224

60

cb	67	386.1
S	64	385.8
+5	67	385.5
100' E		
-5	72	385.0
S	68	385.4
cb	59	386.3
$\frac{1}{4}$	60	386.2
$\frac{1}{2}$	56	386.6
$\frac{1}{4}$	61	386.1
cb	60	386.2
N	59	386.4
+5	62	386.0
dot. 135' E = 2 MH on Rim	515	387.09
150' E		
-5	53	386.9
N	51	387.1
cb	53	386.9
$\frac{1}{4}$	54	386.8
$\frac{1}{2}$	50	387.2
$\frac{1}{4}$	56	386.6
cb	54	386.8
S	64	385.8
+5	69	385.3
200' E		
-5	55	386.7

392.24

S	5.4	386.8
cb	4.8	387.4
$\frac{1}{2}$	5.0	387.2
$\frac{1}{2}$	4.7	387.5
$\frac{1}{2}$	5.0	387.2
cb	5.0	387.2
N	4.7	387.5
235' E		
N	4.2	388.0
cb	4.4	387.8
+2	4.9	387.3
$\frac{1}{2}$	4.5	387.7
$\frac{1}{2}$	4.2	388.0
$\frac{1}{2}$	4.6	387.6
cb	4.3	387.9
S	4.6	387.6
+5	4.8	387.4
270' E = N.W. DAWSON 10' ^{10' cb} 7.5		
S	3.9	388.3
cb	3.7	388.5
$\frac{1}{2}$	3.9	388.3
$\frac{1}{2}$	3.7	388.5
$\frac{1}{2}$	4.1	388.1
+7	4.3	387.9
cb	4.0	388.2
N	3.9	388.3

392.24

c1

Ncb		
N	3.8	388.4
cb	3.8	388.4
$\frac{1}{2}$	3.9	388.3
$\frac{1}{2}$	3.7	388.5
$\frac{1}{2}$	3.9	388.3
cb	4.0	388.2
S	3.9	388.3
N $\frac{1}{2}$		
S	3.9	388.3
cb	3.8	388.4
$\frac{1}{2}$	3.8	388.4
$\frac{1}{2}$	3.7	388.5
$\frac{1}{2}$	3.7	388.5
cb	3.9	388.3
N	3.8	388.4
$\frac{1}{2}$		
N	3.3	388.9
cb	3.3	388.9
$\frac{1}{2}$	3.2	389.0
$\frac{1}{2}$	3.1	389.1
$\frac{1}{2}$	3.3	388.9
cb	3.3	388.9
S	3.4	388.8
E $\frac{1}{2}$		
S	3.5	388.7

cb	35	388.7
$\frac{1}{2}$	35	388.7
$\frac{2}{4}$	34	388.8
$\frac{1}{4}$	35	388.7
cb	35	388.7
N	35	388.7

E cb

N	31	389.1
cb	23	388.9
$\frac{1}{4}$	34	388.8
$\frac{2}{4}$	32	389.0
$\frac{1}{4}$	37	388.5
cb	32	389.0
S	31	389.1

E. L. DAYSON = 0+00

S	27	389.5
cb	30	389.2
$\frac{1}{4}$	34	388.8
$\frac{2}{4}$	29	389.3
$\frac{1}{4}$	31	389.1
cb	30	389.2
N	31	389.1

50'E

N	18	390.4
cb	21	390.1
$\frac{1}{4}$	22	390.0

d	19	390.3
$\frac{1}{4}$	25	389.7
cb	23	389.9
S	23	389.9

100'E

S	16	390.6
cb	13	390.9
$\frac{1}{4}$	16	390.6
$\frac{2}{4}$	10	391.2
$\frac{1}{4}$	12	391.0
cb	10	391.2
N	08	391.4

TP 400

395.66

058

391.66

140'E

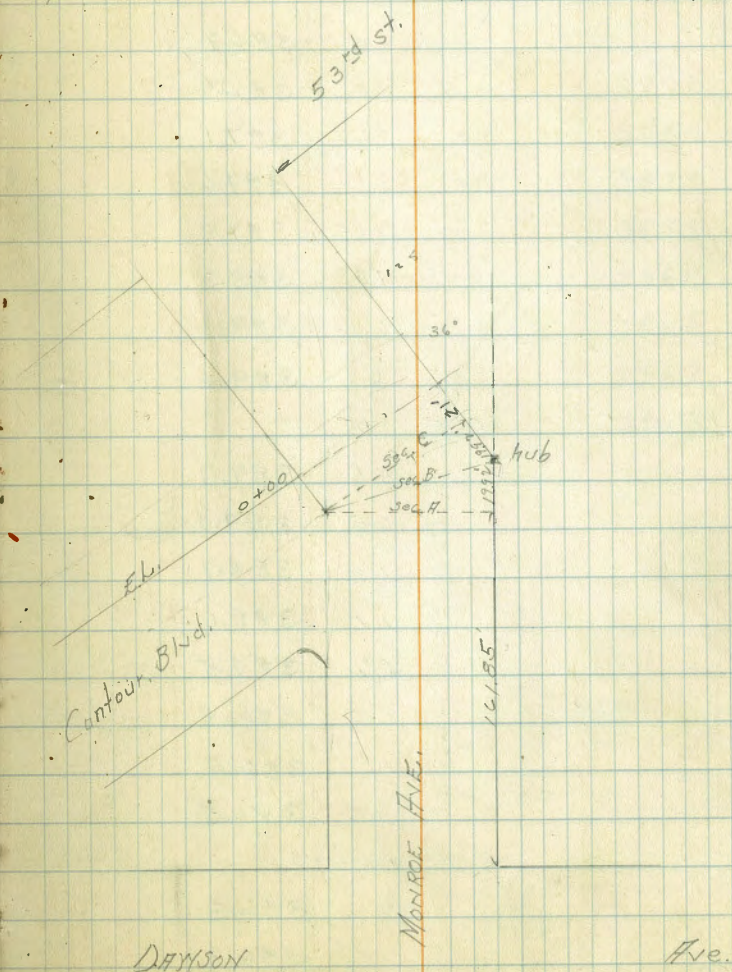
N	33	392.4
cb	34	392.3
$\frac{1}{4}$	35	392.2
$\frac{2}{4}$	36	392.1
$\frac{1}{4}$	37	392.0
cb	38	391.9
S	42	391.5

Sec. #

S	40	391.7
cb	38	391.9
$\frac{1}{4}$	37	392.0
$\frac{2}{4}$	35	392.2

$\frac{1}{4}$		36	392.1
cb		35	392.2
N		36	392.1
	Sec. B		
N		36	392.1
cb		37	392.0
$\frac{1}{4}$		38	391.9
$\frac{1}{2}$		37	392.0
$\frac{1}{4}$		38	391.9
cb		39	391.9
S		40	391.7
	Sec. C		
S		44	391.3
cb		44	391.3
$\frac{1}{4}$		44	391.3
$\frac{1}{2}$		41	391.6
$\frac{1}{4}$		39	391.8
cb		39	391.8
N		36	392.1
Z1-E = E.L. Contour Blvd. = 0+00			
N		45	391.2
cb		44	391.3
$\frac{1}{4}$		44	391.3
$\frac{1}{2}$		45	391.2
$\frac{1}{4}$		47	391.0
cb		48	390.9

S		47	391.0
	50' E of E.L. Contour Blvd.		
S		42	389.5
cb		41	389.3
$\frac{1}{4}$		45	389.2



L	65	389.2
i	65	389.2
cb	64	389.3
N	66	389.1
100' E		
N-5	90	386.7
N	88	386.9
cb	86	387.1
i	81	387.6
L	78	387.9
i	74	388.3
cb	66	389.1
S	61	389.6
115' E		
S	58	389.9
cb	65	389.2
$\frac{1}{4}$	70	388.7
$\frac{1}{2}$	77	388.0
$\frac{1}{4}$	82	387.5
cb	89	386.8
N	91	386.6
+5	92	386.5
125' E = W.L. 53 rd St.		
-5	94	386.3
N	90	386.7
cb	82	387.5

$\frac{1}{2}$	77	388.0
L	69	388.8
$\frac{1}{2}$	63	389.4
cb	60	389.7
S	52	390.5
20' E of W.L. 53 rd St.		
S	67	389.0
cb	73	388.4
i	78	387.9
L	84	387.3
i	88	386.9
cb	92	386.5
N	95	386.2
+10	104	385.3
T.P.	919	386.47

Note: for chk. see page 69

North 10 Pole
Page 59

Kelmer
8-11-27

X. Section 51st St 60' wide
From MADISON to Univ. Ave's

10' cb's
10' 7/8

389.44

65

Nail in pole
Page 64

150'S

297 38724 38707

S.L. MADISON = 0+00

E	13	388.1	X
cb	18	387.6	cb
7	23	387.1	74
L	18	387.6	1/4
2	20	387.4	L
cb	19	387.5	7
X	15	387.9	cb

24	387.0
24	386.8
34	386.0
30	386.4
24	387.0
28	386.6
28	386.6
23	387.1

50'S

200'S

X	15	387.9	E
cb	22	387.2	cb
1/4	23	387.1	1/4
L	18	387.6	L
1/4	20	387.4	1/4
cb	21	387.3	cb
E	17	387.7	X

23	387.1
30	386.4
30	386.4
26	386.8
33	386.1
32	386.2
28	386.6

100'S

250'S

E	20	387.4	X
cb	24	387.0	cb
1/4	25	386.9	1/4
L	22	387.2	L
1/4	27	386.7	1/4
cb	25	386.9	cb
X	18	387.6	E

31	386.3
39	386.1
36	385.8
29	386.5
34	386.0
23	387.1
27	386.7

300'S

E	35	3859
cb	38	3856
$\frac{1}{4}$	39	3855
$\frac{1}{2}$	35	3859
$\frac{3}{4}$	42	3852
cb	38	3856
N	35	3859

350' S

N	40	3854
cb	43	3851
$\frac{1}{4}$	44	3850
$\frac{1}{2}$	37	3857
$\frac{3}{4}$	42	3852
cb	42	3852
E	39	3855

400' S

E	43	3851
cb	47	3847
$\frac{1}{4}$	46	3848
$\frac{1}{2}$	40	3854
$\frac{3}{4}$	49	3845
+5	53	3841
cb	45	3849
N	45	3849

450' S

N	49	3845
---	----	------

cb	50	3844
+3	56	3838
$\frac{1}{4}$	52	3842
$\frac{1}{2}$	45	3849
$\frac{3}{4}$	50	3844
cb	53	3841
E	48	3846

500' S

E	51	3843
cb	51	3843
+2	55	3839
$\frac{1}{4}$	52	3842
$\frac{1}{2}$	47	3847
$\frac{3}{4}$	52	3842
+7	57	3837
cb	52	3842
N	51	3843

550' S

N	54	3840
cb	55	3839
+3	60	3834
$\frac{1}{4}$	55	3839
$\frac{1}{2}$	50	3844
$\frac{3}{4}$	53	3841
+8	59	3835
cb	51	3843

E	50	3844
	600' S	
E	51	3843
cb	51	3843
+2	58	3836
$\frac{1}{4}$	55	3839
$\frac{1}{2}$	53	3841
$\frac{3}{4}$	57	3837
cb	56	3838
N	54	3840

650.53' S on N = N.L. Monroe Ave
 this intersection
 sectioned on Page 57

N	56	383.6
cb	55	3839
$\frac{1}{4}$	57	3837
$\frac{1}{2}$	55	3839
$\frac{3}{4}$	56	3838
cb	52	3842
E	53	3841

S.L. Monroe = 0+00

E	48	3846
cb	46	3848
$\frac{1}{4}$	49	3845
$\frac{1}{2}$	45	3849
$\frac{3}{4}$	50	3844
cb	50	3844
N	45	3839

	50' S	
N	32	3862
cb	39	3855
$\frac{1}{4}$	42	3852
$\frac{1}{2}$	39	3855
$\frac{3}{4}$	43	3851
cb	45	3849
E	40	3850

100' S

E	28	3866
cb	34	3860
$\frac{1}{4}$	34	3860
$\frac{1}{2}$	33	3861
$\frac{3}{4}$	36	3858
cb	33	3861
+8	33	3861
N	26	3868

T.P. 583

392.11 ✓ 316

38628

150' S

N	48	3873
+2	56	3865
cb	57	3864
$\frac{1}{4}$	60	3861
$\frac{1}{2}$	55	3866
$\frac{3}{4}$	59	3863
cb	56	3865

E	52	386 9
200'S		
E	49	387 2
cb	53	386 8
$\frac{1}{4}$	55	386 6
$\frac{1}{2}$	54	386 7
$\frac{3}{4}$	59	386 2
cb	55	386 6
+8	55	386 6
N	47	387 4

250'S

N	49	387 2
cb	52	386 9
$\frac{1}{4}$	56	386 5
$\frac{1}{2}$	50	387 1
$\frac{3}{4}$	54	386 7
cb	50	387 1
E	49	387 3

300'S

E	48	387 3
cb	50	387 1
$\frac{1}{4}$	52	386 9
$\frac{1}{2}$	47	387 4
$\frac{3}{4}$	57	386 4
+7	55	386 6
cb	48	387 3

N	46	387 5
350'S		
N	46	387 5
cb	47	387 4
+3	53	386 8
$\frac{1}{4}$	51	387 0
$\frac{1}{2}$	47	387 4
$\frac{3}{4}$	52	386 9
cb	48	387 3
E	48	387 3

400'S

E	50	387 1
cb	52	386 9
+2	57	386 4
$\frac{1}{4}$	52	386 9
$\frac{1}{2}$	49	387 2
$\frac{3}{4}$	51	387 0
+7	52	386 9
cb	46	387 5
N	44	387 7

450'S

N	45	387 6
cb	46	387 5
+3	52	386 9
$\frac{1}{4}$	51	387 0
$\frac{1}{2}$	48	387 3

1/2	54	3867
+P	59	3862
cb	52	3869
E	52	3869
500' S		
E	56	3865
cb	56	3865
+2	61	3860
1/2	55	3866
1/4	53	3868
1/4	51	3870
1/8	55	3866
cb	47	3874
W	45	3876
550' S		
W	43	3878
cb	46	3875
+L	52	3869
1/4	52	3869
cb	51	3870
1/2	55	3866
+P	62	3859
cb	55	3866
E	57	3864
599.10 S = Section at Rt. Boyles 51st St. = NE Cor		
E	54	3867

cb	55	3866	
1/4	54	3867	
1/4	49	3872	
1/4	49	3872	
cb	42	3879	
W	38	3883	
610.5 S = N.W. El Cajon Section Parallel with El Cajon			
W	38	3883	
cb	42	3879	
1/4	44	3877	
1/2	49	3872	
1/2	53	3868	
cb	54	3867	
E	54	3867	
TP 343	392.62	2.92	38919
TP		9.19	38343
Error of app. Dropped BM used	9.78	393.73	38345
TP 420	394.15	5.29	38795
S.W. El Cajon Section Parallel with El Cajon			
E	66	3875	
E top cb	62.1	38791	
Gut	68	3873	
1/2	64	3877	
1/2	59	3882	
1/2	59	3882	
Gut	62	3879	

ch. or
BM.
Page 57
BM.
El Cajon 50'

387.95
{Note, 51st St. from S.W.
El Cajon to 11th St.
1/2 cb
9' 75'}

W top cb	5.2	388 73
W	5.1	388 7
Section at Rt. Ends to 51st St. from surface		
W	5.4	388 7
W top cb	5.42	388 73
Gut	6.2	387 9
$\frac{1}{4}$	5.9	388 2
$\frac{1}{2}$	5.9	388 2
$\frac{3}{4}$	6.5	387 6
Gut	6.8	387 3
E top cb	6.71	387 94
E	6.5	387 6
50' S		
E	6.2	387 9
E top cb	6.10	388 05
Gut	6.7	387 4
$\frac{1}{4}$	5.7	388 4
$\frac{1}{2}$	5.1	389 0
$\frac{3}{4}$	5.7	388 4
cb	6.1	388 0
W top cb	5.42	388 73
W	5.0	389 1
100' S		
W	5.2	388 9
W top cb	5.36	388 79
Gut	6.1	388 0

$\frac{1}{2}$	5.5	388 6
$\frac{3}{4}$	5.2	388 9
$\frac{1}{4}$	5.7	388 4
Gut	6.5	387 6
E top cb	6.07	388 08
E	6.1	388 0
150' S		
E	5.7	388 4
E top cb	6.02	388 13
Gut	6.5	387 6
$\frac{1}{4}$	5.7	388 4
$\frac{1}{2}$	5.3	388 8
$\frac{3}{4}$	5.6	388 5
Gut	6.0	388 1
W top cb	5.30	388 85
W	5.3	388 8
200' S		
W	5.7	388 4
top cb	5.38	388 77
Gut	6.1	388 0
$\frac{1}{4}$	5.7	388 4
$\frac{1}{2}$	5.2	388 9
$\frac{3}{4}$	5.8	388 3
Gut	6.4	387 7
top cb	5.98	388 17
E	5.8	388 3

394.15

E	62	3879
topcb	599	38816
Gut	66	3875
$\frac{1}{2}$	59	3882
$\frac{1}{4}$	55	3896
$\frac{1}{4}$	58	3883
Gut	60	3881
N topcb	555	38860
N	55	3886
	300'S	
N	55	3886
topcb	592	38833
Gut	64	3877
$\frac{1}{4}$	61	3880
$\frac{1}{4}$	58	3883
$\frac{1}{2}$	62	3879
Gut	65	3876
topcb	602	38813
E	62	3879
	350'S	
E	58	3883
topcb	586	38829
Gut	65	3876
$\frac{1}{4}$	60	3881
$\frac{1}{4}$	57	3884
$\frac{1}{2}$	61	3880

394.15

Gut	63	3878	
N topcb	583	38832	
N	56	3885	
	400'S		
N	63	3878	
topcb	613	38802	
Gut	65	3876	
$\frac{1}{2}$	64	3877	
$\frac{1}{4}$	61	3880	
$\frac{1}{4}$	64	3876	
Gut	71	3870	
topcb	661	38750	
E	67	3874	
TP 189	38980	624	38791
	425'S		
E	27	387.1	
topcb	266	387.14	
Gut	32	386.6	
$\frac{1}{2}$	27	387.1	
$\frac{1}{4}$	22	387.6	
$\frac{1}{2}$	25	387.3	
topcb	220	387.6	
N	23	387.5	
	450'S		
N	30	386.8	
N topcb	290	386.9	

Gut	35	386.3
$\frac{1}{2}$	33	386.5
$\frac{2}{2}$	29	386.9
$\frac{3}{4}$	34	386.4
Gut	38	386.0
E. top cb	319	386.61
E	36	386.2
475' S		
E	40	385.8
top cb	385	385.95
Gut	46	385.2
$\frac{1}{2}$	41	385.7
$\frac{2}{2}$	36	386.2
$\frac{1}{2}$	41	385.7
Gut	44	385.4
top cb	379	386.01
W	37	386.1
500' S		
W	47	385.1
top cb	472	385.08
Gut	53	384.5
$\frac{1}{2}$	48	385.0
$\frac{2}{2}$	47	385.1
$\frac{1}{4}$	52	384.6
Gut	61	383.7
top cb	507	384.73

E	53	384.6	
525' S			
E	64	383.4	
top cb	686	382.94	
Gut	82	381.6	
$\frac{1}{2}$	72	382.6	
$\frac{2}{2}$	67	383.6	
$\frac{1}{2}$	64	383.4	
Gut	65	383.3	
W top cb	610	383.70	
W	59	383.9	
553.5' S = End of existing cb.			
W	87	381.1	
top cb	855	381.25	
Gut	93	380.5	
$\frac{1}{2}$	84	381.4	
$\frac{2}{2}$	83	381.5	
$\frac{1}{2}$	91	380.7	
Gut	92	380.0	
E. top cb	922	380.56	
E	87	381.1	
TP. 121	381.77	922	380.56
574' S			
E	14	380.4	
$\frac{1}{2}$	34	378.4	
cb	34	378.4	

7	2.8	379 0
8	2.3	379 5
7	3.7	378 1
cb	3.0	378 8
W	2.2	379 4
594.5		
W	3.8	378 0
cb	5.1	376 7
7	4.4	377 4
8	4.6	377 2
7	4.3	377 5
cb	4.9	376 9
+6	5.4	376 4
E	3.6	378 2
609.5		
E	4.9	376 9
+2	7.4	374 4
cb	6.1	375 7
7	5.9	375 9
8	6.0	376 8
7	6.0	376 8
+5	6.4	375 4
cb	10.3	371 5
+2	11.9	369 9
+10	9.8	372 5
W	6.4	375 4

650.5		
W	13.1	368 7
+10	14.5	367 3
cb.	16.4	365 4
+4	18.0	363 8
+5	14.4	367 4
7	14.4	367 4
8	14.2	367 6
7	14.0	367 8
cb	13.4	368 2
+9	13.6	368 2
+10	14.8	367 0
+11	14.8	367 0
E	11.6	370 2
TP. 0.66	349.55	12.52
685.5		
E	6.7	362 8
+8	10.6	358 9
+9	9.2	360 3
cb	8.8	360 7
7	8.5	361 2
8	8.2	361 3
7	8.3	361 2
+3	8.2	361 3
cb.	10.9	358 6
+2	9.2	360 3

N		7.1	3624
			14' obs.
	699.5 = N. to Florence st.	13' 7.5	
N		9.5	3600
cb		10.8	3587
+3		12.3	3572
+1		11.6	3579
$\frac{1}{2}$		11.3	3582
$\frac{1}{2}$		10.6	3589
$\frac{1}{2}$		10.9	3586
cb		11.2	3583
+3		11.5	3580
+5		14.6	3549
+8		12.4	3571
E		10.3	3592
T.P.	2.10	12.99	356.56
	N cb		
E		3.5	3552
+2		4.3	3544
+3		7.0	3517
+7		5.7	3530
+8		3.2	3555
cb		2.9	3558
$\frac{1}{4}$		2.1	3566
$\frac{1}{4}$		2.5	3561
$\frac{1}{4}$		2.9	3558
cb		2.7	3560

Note: Florence X-section was on 80' ST.
 Florence X-section closed.
 20' on N. side closed.
 W.M.B. 1-20-28.

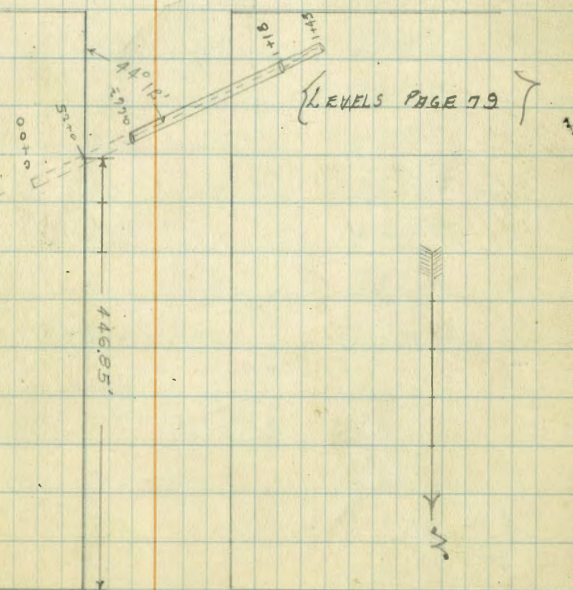
+9		1.7	3570
N		0.3	3584
	N cb + 6'		
N		3.4	3553
cb		3.5	3552
$\frac{1}{2}$		3.5	3552
$\frac{1}{2}$		3.4	3553
$\frac{1}{2}$		3.0	3557
cb		4.0	3547
+5		4.0	3547
+6		7.2	3515
+8		7.4	3513
E		4.9	3538
	N $\frac{1}{2}$		
-5		7.2	3515
E		6.1	3526
+3		7.8	3509
+6		7.5	3512
+8		5.6	3531
cb		5.3	3534
$\frac{1}{4}$		4.7	3540
$\frac{1}{4}$		4.6	3541
$\frac{1}{4}$		4.6	3541
cb		4.9	3538
N		4.3	3544
	N $\frac{1}{2}$ + 5'		

N	5.1	353 6
cb	5.3	353 4
$\frac{1}{2}$	5.0	353 7
$\frac{1}{2}$	5.2	353 5
$\frac{1}{2}$	5.2	353 5
b	6.1	352 6
+5	8.2	350 5
E	9.0	349 7
+5	9.3	349 4
$\frac{1}{2}$		
-5	7.0	351 7
E	6.4	352 3
cb	6.1	352 6
$\frac{1}{2}$	5.8	352 9
$\frac{1}{2}$	5.4	353 3
$\frac{1}{2}$	5.6	353 1
cb	5.6	353 1
N	5.6	353 1
$\frac{1}{2}$		
N	7.0	351 7
cb	7.2	351 5
$\frac{1}{2}$	7.5	351 2
$\frac{1}{2}$	6.9	351 8
$\frac{1}{2}$	6.7	352 0
cb	6.8	351 9
E	7.1	351 6

S cb		
E	8.0	350 7
cb	8.0	350 7
$\frac{1}{2}$	8.1	350 6
$\frac{1}{2}$	8.9	349 9
$\frac{1}{2}$	9.2	349 5
cb	9.3	349 4
N	8.5	350 2
S.L. Florence = 0+00		
N	10.2	348 5
+2	10.0	348 7

Orange

Ave.



Florence

5.4

+3		12.7	3460
+6		12.7	3460
+7		11.3	3474
cb		11.2	3475
$\frac{1}{2}$		11.3	3474
$\frac{1}{2}$		10.9	3478
$\frac{1}{2}$		10.8	3479
cb		10.7	3480
E		11.0	3477
+5		11.2	3475
T.P.	0.95	346.51	18.10 34556
		20'S	
-5		3.7	3428
E		3.7	3428
cb		3.2	3433
$\frac{1}{2}$		2.5	3440
+5		3.2	3433
$\frac{1}{2}$		2.2	3443
$\frac{1}{2}$		2.1	3444
cb		2.3	3442
N		1.6	3449
	45'S		
N		.64	3401
cb		.59	3406
$\frac{1}{2}$.57	3408
+5		.56	3409

$\frac{1}{2}$		7.4	3391
+5		9.5	3370
$\frac{1}{2}$		9.3	3372
cb		7.9	3366
E		10.1	3364
+10		10.4	3361
	80'S		
-10		19.8	3267
E		19.4	3271
cb		18.6	3279
$\frac{1}{2}$		17.8	3287
+3		17.6	3289
$\frac{1}{2}$		13.9	3331
+7		9.8	3367
$\frac{1}{2}$		9.8	3367
cb		10.9	3356
+11		11.0	3355
N		11.8	3347
+5		11.3	3352
T.P.	0.66	334.56	12.61 33370
		135'S	
-5		2.9	3317
N		2.9	3317
cb		3.1	3314
+2		3.6	3310
$\frac{1}{2}$		7.0	3276

334.56

1/4	10.3	324 3
cb	11.6	323 0
E	12.9	321 7
+10	13.4	321 2
155'S		
-10	13.0	321 6
E	10.3	324 3
cb	9.0	325 6
1/4	7.5	327 1
1/2	5.8	324 8
+5	4.6	330 0
1/4	4.4	330 2
cb	4.3	330 3
N	3.9	330 7
175'		
N	4.5	330 1
cb	5.3	329 3
1/4	4.8	329 8
1/2	5.2	329 4
1/4	6.0	328 6
cb	7.3	327 3
E	9.5	325 1
+10	10.7	323 9
200'S		
-10	12.6	322 0
E	11.0	323 6

334.56

77

cb	8.8	325 8
1/4	6.9	327 7
1/2	6.6	328 0
1/4	6.9	327 7
1/2	6.4	328 2
N	5.1	329 5
230'S = 1/2 House on E with Gr. Foundation 19' Back 24' wide		
N	7.5	327 1
1/2	8.6	326 0
1/4	9.0	325 6
1/2	8.9	325 7
1/4	10.7	323 9
+1	11.7	322 9
cb	14.0	320 6
E	15.4	319 2
+10	15.4	319 2
+19 on Ground of Foundation	14.9	319 7
+19 " top of "	11.7	322 9
265'S		
-15	20.1	314 6
E	20.1	314 6
cb	18.5	316 1
1/4	15.9	318 7
1/2	12.2	322 4
+5	11.2	323 4
1/4	11.0	323 6

cb		11.0	323 6
N		10.4	324 2
T.P.	1.51	323.20	12.97

300'S

N		2.9	320 3
cb		3.0	320 2
$\frac{1}{4}$		2.8	320 4
E		3.7	319 5
$\frac{1}{4}$		5.1	318 1
cb		7.3	315 9
E		9.4	313 8
+15		10.0	313 2

350'S

-15		10.4	312 8
E		9.5	313 7
cb		8.8	314 4
$\frac{1}{4}$		8.3	314 9
E		7.9	315 3
$\frac{1}{4}$		7.6	315 6
cb		7.4	315 8
N		7.3	315 9
+10		6.6	316 6

400'S

-10		10.0	313 2
N		10.0	313 2
cb		9.4	313 8

$\frac{1}{4}$		9.2	313 6
E		10.4	312 8
$\frac{1}{4}$		10.6	312 4
cb		11.1	312 1
E		11.6	311 6
+15		11.4	311 8

407'S

-15		11.5	311 7
-5		12.0	311 2
E		12.7	310 5
+5		11.3	311 9
cb		11.2	312 0
$\frac{1}{4}$		11.0	312 2
E		10.5	312 7
$\frac{1}{4}$		9.7	313 5
cb		9.6	313 6
N		10.1	313 1
+10		10.3	312 9

459

-10		13.3	309 9
-6		13.0	310 2
-4		11.3	311 9
N		10.6	312 6
cb		9.5	313 7
$\frac{1}{4}$		9.9	313 3
E		12.5	310 7

1/2	13.3	3099
cb	13.5	3097
E	13.8	3094
+5	11.4	3118
+10	10.5	3127

LEVELS FOR Culvert PAGE 75

0+00	10.5	3127
+15	11.0	3122
+19	13.5	3097
+25 = Intersection E.L. with of culvert	13.5	3097
+66 1/2 = Flow line Exist. 18" con. Pipe	15.27	30798
+78	8.8	3144
+98	9.4	3138
1+18 = Flow line 18" Pipe	16.29	30691
1+43 = End	15.7	3075

461'S

-10	10.5	3127
E	11.1	3121
+3	13.9	3093
cb	13.4	3098
1/4	13.3	3099
1/2	12.9	3103
3/4	9.7	3135
cb	9.5	3137
W	10.6	3126
+6	12.3	3109

+8	13.3	3099
+10	13.3	3099
	500'S	
-15	12.7	3105
-11	13.3	3099

-9	14.8	3084
-5	12.6	3106
W	11.0	3122
+1	7.2	3160
d	6.7	3165
1/2	6.7	3165
1/2	9.3	3139
1/2	8.0	3152
cb	6.8	3164
E	4.7	3185
+10	2.9	3203

525'S

-5	+0.8	3240
E	0.0	3232
cb	2.0	3212
1/4	3.2	3200
1/2	4.9	3183
3/4	4.7	3190
+6	4.2	3190
6	5.2	3178
+7	7.5	3157

N			10.8	312 4
+10			17.1	306 1
+15			15.0	308 2
T.P.	12.08	334.88	0.40	327.80
550'5				
-20			22.7	312 2
-6°			19.6	315 3
N			17.2	317 7
cb			12.5	322 4
$\frac{1}{2}$			12.8	322 1
$\frac{1}{4}$			12.4	322 5
$\frac{1}{4}$			10.4	324 5
cb			7.2	327 7
E			4.3	330 6
580'5				
E			+0.6	335 5
cb			2.1	332 8
+3			2.9	332 0
$\frac{1}{4}$			5.7	329 2
$\frac{1}{2}$			9.0	329 9
$\frac{1}{4}$			9.1	329 8
cb			9.4	329 5
+5			9.6	329 3
N			12.6	322 3
+20			17.2	317 7
T.P.	0.58	328.54	6.92	327.96

APRIL 17 1884
Pole orange 511

3884
1366
2518

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 X to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance

IMPROVED TABLES AND INFORMATION

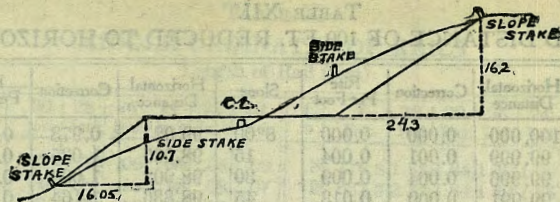
To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of correction. *Note: Cont. in Book 1163 Page 24-35 For Section 600' South St. Florence St. = N.E. Orange St. See Book 1162 Page 36-38*

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

T

CH. on 811	328.54	3.05	325.49
NOV. Orange 511			325.49
			0.04

1470
591
9061



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

9061
836.6 ✓
6.95 ✓

1216
804
1320
1247
275
1522

885 on Mon
581 on Hyd

9829 52 ✓
865 39823
874 38717
627 606

430
136
279 X

8571
524
8027

430
179
251

583.95 - BM SW Mon. EL (1907) +50ft
387.17 - " NW " " " 51ft

TK. 387 + 391
S E 391

430
239
191

430
323
1407
7002
426
47.01

430
296
1434

7428
420
7028

7428
59
6838

7428
58
6838
68.48

191

7889
669 on Spt

7020
70.01

6095
104
599.1
019
160
165
1304
1629

181.77
1492
161.85

106
1240
13.66
23.22 on Mon
7.82
25.18