

1196

FIELD BOOK

385

Dunn's 6371 Imperial.

MICROFILMED
DEC 22 1964

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Survey of SAMACHA ROAD IN EX-MISSON RANCHO

5 TANGENTS

Walker
4-27

N 35° 06' E

25+80.50 = Intersection of L. of Samacha Road with Bdry. Line

N 35° 06' E

25+74.30 = PL 10° 02' 30"

Approx.
200'

N 45° 04' E

17+22 = PL 4° 19' 30"

Approx.
75'

N 49° 28' E

13+68 = PI R 4° 50'

Approx.
75'

N 44° 36' E

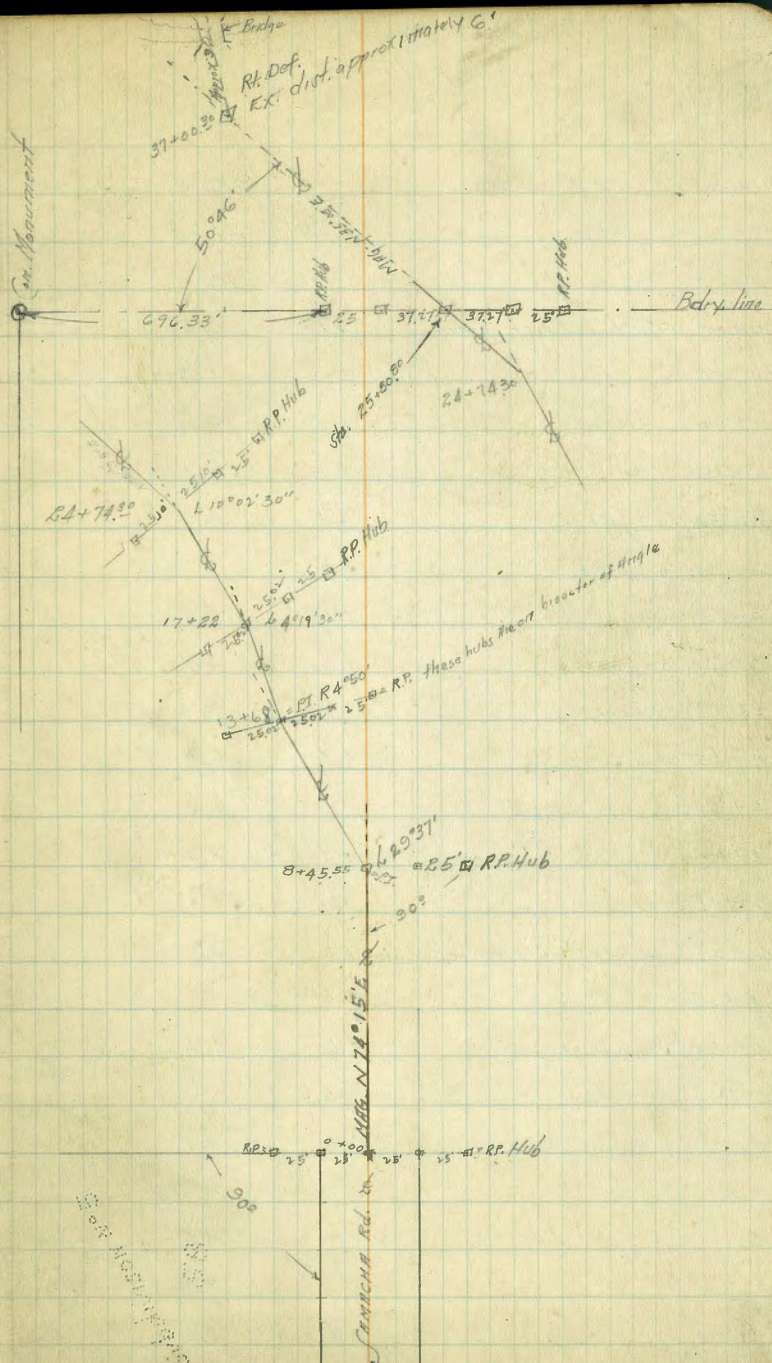
8+45.55 = PI L 29° 37'

Approx.
100'

Mrs. Beatty

N 74° 15' E

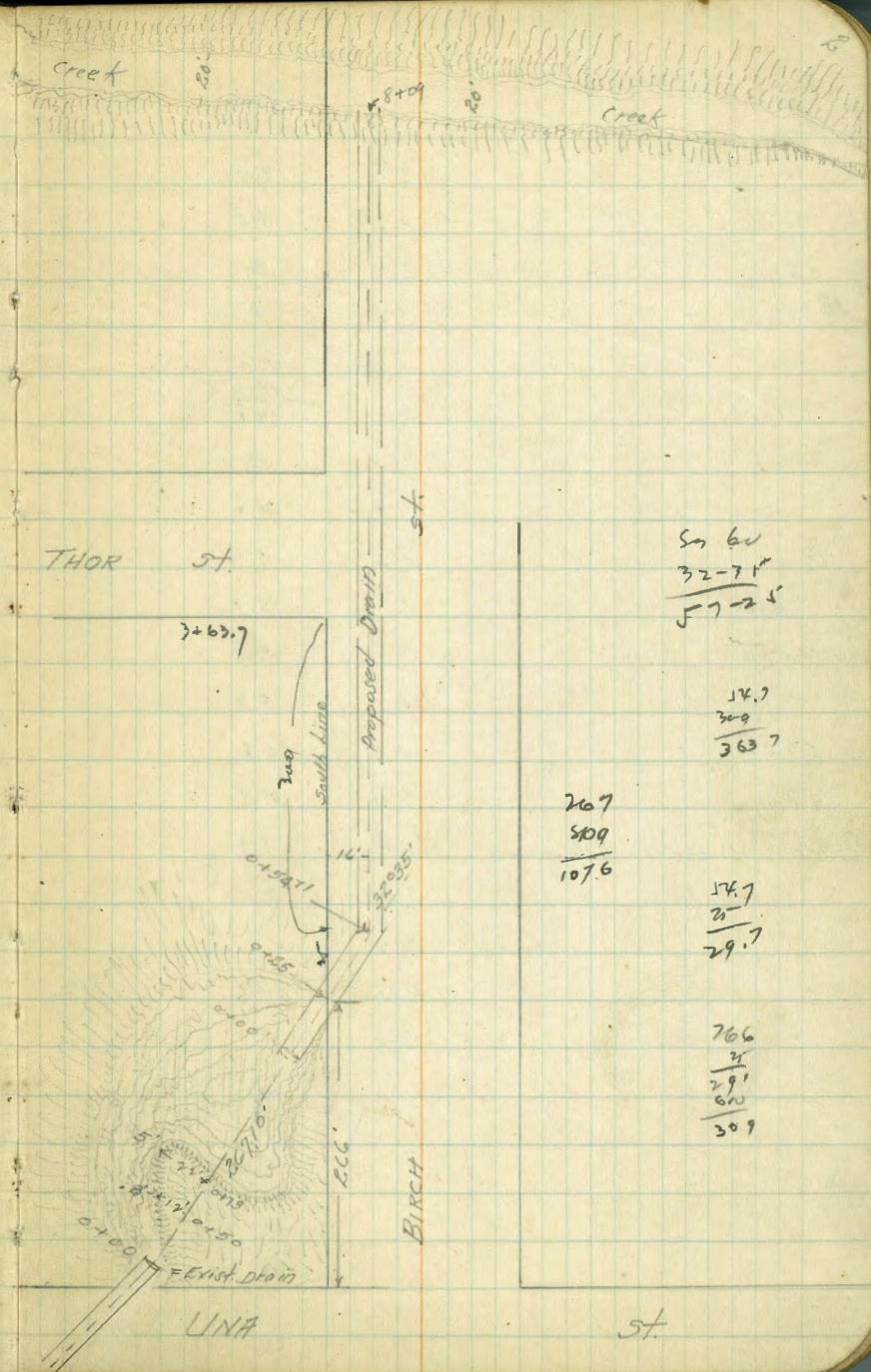
0+00



Walker
2-18-77

Proposed Drain on Birch St
West of Una St.

NY Spk				
Main + Una	8.46	22.91		14.45
T.P.	2.36	20.93	2.34	20.57
T.P.	2.20	12.67	10.46	10.47
0+00 = Flowline Exist Drain		9.18		<u>12.7</u> 3.5
+20		8.3		4.4
+26		6.8		5.9
+50		6.3		6.4
12' South of 0+50		6.3		6.4
20' South of 0+50		8.3		4.4
0+73		7.5		5.2
22' South of 0+73		7.2		5.5
27' " " 0+73		8.7		4.0
0+83		7.2		5.3
0+88		9.1		3.6
1+17		10.4		2.3
2+15		9.9		2.8
2+67.10 = 0+00 of Proposed drain		9.5		3.2
0+25		8.6		4.1
0+54.71 = Δ L 32935		8.6		4.1
T.P.	5.33	9.99	8.67	4.00
1+00		4.6		<u>2.3</u> 4.7
+50		2.7		4.6
2+00		4.5		4.5
+50		5.3		4.0
3+00		5.8		3.5



57.7
32.7
57.25

57.7
30.9
363.7

267
509
107.6

57.7
29.7
29.7

766
29.7
60
309

Burb St. Drain

				<u>9.3</u>
3+06			5.9	3.4
4+16			4.9	7.4
7-50			4.7	4.6
2+00			4.3	5.0
+50			5.2	4.1
T.P.	455	100.2	3.86	5.47
				<u>10.0</u>
5+00			5.2	4.8
+40			4.8	5.2
7-50			5.4	4.6
6+00			4.6	5.4
+50			4.9	5.1
7+00			5.1	4.9
+50			4.7	5.3
8+00			4.4	5.6
8+09			7.9	2.1
100' South of 8+09 in the stream			8.9	1.1
T.P.	436	8.90	5.18	4.54
T.P.	11.32	17.30	2.92	5.98
T.P.	3.58	16.53	4.85	12.85
T.P.	4.80	17.79	3.54	12.99
chk. by B.M. Mansfield			3.30	14.29
				14.25 - RM
				0.04

No. 111
 193-192 UH
 1000
 Sorbyell

15'
 X. Section Alley Bet. Center St and Park Blvd.
 From N.W. Robinson to S.W. Univ. Ave
 193-192 UH

284.74

NE BR
 Robinson + West 2.85 296.90 294.05

-3'

E 11.7
 S 11.7
 W 11.6

N.W. Robinson = 0+00 Note No. 6 Return on E.W. Alley

W top 6 10.69
 W Gut. on Ground 11.6
 S 12.1
 E 13.0
 +5 12.6
 T.D. 0.16 284.74 13.62 284.78

17' N N.W. Robinson

-10 11.0
 E 9.4
 S 7.3
 W 3.0
 +5 = Base of Wf. House 17

12' N

-5.5 = " " " 2.2
 W 3.3
 S 6.8
 +5 10.6
 E 11.5
 +25 14.1

70' N = 1/2 Pickett Fence on W 13' in Alley 17' Wide

-25 13.0
 E 7.7
 S 5.4
 W 3.3
 +5 1.8

94' N

-5 3.0
 W 4.0
 S 6.2
 +3 6.7
 E 8.6
 +25 12.5

115' N

-25 14.4
 E 11.2
 S 10.3
 W 8.4
 +5 6.8

124' N

-10 8.6
 W 11.5
 S 12.2
 E 13.0
 +25 13.7

174' N

289.74

-10	9.1
E	7.2
L	9.2
W	10.9
+15	10.0

196' N

-15	8.4
-9	8.3
W	10.6
L	10.5
E	10.3
+15	5.0

246' N

-25	6.8
-14	10.0
E	8.1
L	7.3
W	6.6
+10	5.6

296' N

-5	+1.0
W	-0.7
L	4.5
E	7.1
+15	7.5

TP	13.01	291.14	6.61	7813
----	-------	--------	------	------

291.14

5

346' N

-15	11.1
-10	9.4
E	7.6
L	6.4
W	7.3
+4	1.0

Flow liner = 8.51

353' N = sand 15" Coa. G. heart 15' E.E.L. Alley.

356' N

-10	1.7
W	1.9
L	4.1
E	2.0
+5	2.7
+10	5.0

391' N = 2' M.H.

-15	2.5			
E	1.3			
TP	7.60	297.90	0.84	290.30
L	= Rim of M.H.	6.56		
L	on ground	7.3		
W		6.6		
+5		5.7		

416' N

-5	5.6
W	4.1

29790

♀	6.8
E	7.4
+13.5 = Fence	10.5
456' N = ♀ House on E South Entrance 30' wide	
-15 = House	9.7
E	7.7
♀	5.9
W	5.4
+10	4.6
567' N	
-5	5.0
W	5.2
♀	5.3
E	6.6
+5	7.5
+13.5 = Fence	10.1
TP 1381	300.77
10.34	287.56
522' N = ♀ Clear out Box. For 18" Con. Culvert 3' E of line	
Floor Line =	14.65
Rim of Box =	11.82
542' N	
-20	13.4
-5	11.7
E	10.4
♀	8.5
W	8.0

30077

6

+5	7.5
TP 1439	306.71
8.45	292.32
568' N	
-5	8.5
W	7.0
♀	10.6
E	15.3
+10	16.4
+15	18.5
+25	18.8
592' N	
E-25	17.3
E-5	15.6
E	14.0
♀	9.1
W	3.6
+2	1.5
+1	1.3
602' N	
-7	1.3
-2	1.0
W	3.6
♀	8.9
E	13.0
+25	15.0
622' N	

306.71

-35			13.5	
-10			11.9	
E			5.4	
L			1.4	
+3			+0.1	
W			-0.4	
+5			-0.4	
T.P.	9.28	312.54	3.45	303.26
	637.6	N		

W			6.2	
L			8.4	
E			12.3	
+15			16.7	
+25			17.3	

647.1 N

-15			13.5	
-5			11.3	
E			8.2	
+7			5.9	
L			5.9	
W			5.8	

653.9' = S.L. Univ. Ave

Note:
No. of Returns on E or W
Side Walk extends to Prop. Lines

W top Par 104			5.12	
L " "			5.29	
E " "			5.04	

Chk. on NW & M. Univ. Center st. 8.55

303.95
303.88
007.17 Error

Make
the top
level
of
the
wall

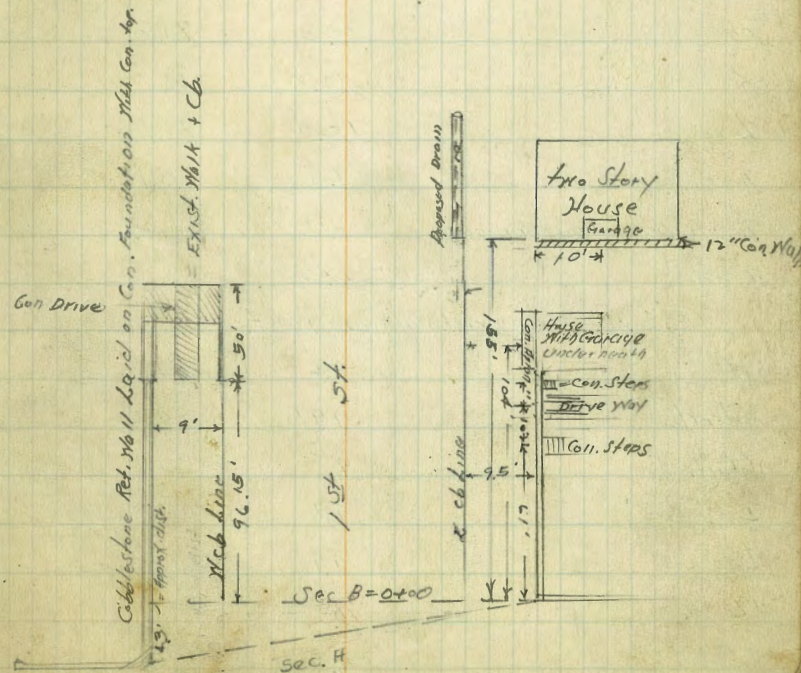
X. Section 1st St. 50' wide 10' cbs, 75' 75
From N.L. Harbor Dr. North

2193

Estimate Book # 15
Page 47

-3	N.Y. B.P.				
-10	Monticito + Bathman 8.31	295.85		287.54	
E	T.P.	296	291.93	6.88	288.97
			Section A		
+3	E			4.1	87.8
W	E top cb			4.42	87.5
+5	" Gut			4.6	87.3
T.P.	+3			5.1	86.8
	$\frac{1}{4}$			4.9	87.0
W	$\frac{1}{2}$			4.6	87.3
$\frac{1}{2}$	$\frac{1}{4}$			4.5	87.4
E	cb			4.6	87.3
+15	W			4.3	87.6
125					
					Sec B = 0+00
	W at Wall			4.2	87.7
-13	cb			4.6	87.3
-5	$\frac{1}{2}$			4.5	87.4
E	$\frac{1}{2}$			4.6	87.3
+2	$\frac{1}{4}$			4.9	87.0
$\frac{1}{2}$	+4			5.2	86.7
W	Gut			4.7	87.4
	E top cb.			4.42	87.57
W	E at Con Wall			4.2	87.7
$\frac{1}{2}$	"				50' N
E	E at Wall			5.9	86.0
ch	cb.			6.5	85.4

+2		7.0		84.4
$\frac{1}{4}$		6.9		85.3
$\frac{1}{2}$		6.1		85.8
$\frac{1}{2}$		6.3		85.6
cb		6.3		85.6
W at Wall = Base		5.4		86.5
Top of 1st Step =		5.71		84.8
61' N = 2 Con Steps on E. Ord. =		6.4		85.5
71' N = " " Dr. on E		6.52		85.41
82' N = " " Steps on E top of		6.87		85.06
96.5' N = Beginning Con. Side Walk + Curb on West				
W		7.1		84.8
W top cb		7.42		84.51



Gut	7.6	84.3
+3	8.2	83.7
$\frac{1}{2}$	7.8	84.1
$\frac{1}{4}$	7.6	84.3
$\frac{1}{4}$	7.9	84.0
cb	8.0	83.9
E at N end Con. Ret Wall	7.4	84.5
104' N = E Garage on E. Con. Floor with Con. Apron		
E	8.34	83.59
+5 = toe of Con Apron	8.23	83.70
1+41 = E Con Dr on W		
E	10.3	81.6
cb	10.3	81.6
$\frac{1}{2}$	10.2	81.7
$\frac{1}{4}$	10.0	81.9
$\frac{1}{4}$	9.8	82.1
cb on Drive Way Approach	10.19	81.74
W	9.42	82.51
140.4' N = End Exist Walk on West		
W	9.6	82.3
W top cb	9.91	82.02
W Gut.	9.8	82.1
$\frac{1}{4}$	9.7	82.2
$\frac{1}{4}$	9.9	82.0
+L	10.3	81.6
+5	11.3	80.6

$\frac{1}{4}$	12.7	79.2
+1	10.5	81.4
cb	11.5	80.4
+4	10.6	81.5
E	10.6	81.5
155' N		
-10' = E Garage see sketch	10.69	81.24
E on top of Wall "	10.50	81.43
+1	13.3	78.6
+3	11.4	80.5
+8	11.3	80.6
cb	14.0	77.9
+4	14.6	77.3
+6	11.0	80.9
$\frac{1}{4}$	10.9	81.0
$\frac{1}{4}$	9.8	82.1
$\frac{1}{4}$	9.5	82.4
cb	9.5	82.4
W	9.5	82.4
Levels For Drain 0+00 = 155' N Drain 1' W of Ecb Line		
0+00	14.9	77.0
+7	11.3	80.6
+25	12.0	79.9
+40	18.0	73.9
+55	19.0	62.9
+65	33.4	58.2

TP. 676 86.29 26.0
 ch. on 819. Monticello + Richman 87.6

891.93

281.53

281.53 = 81.7

0.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

10.00

Curb levels on Robinson Place

E/E
Aug 26-27
Vermont
Flood
Bichet
Kiernan.

1.19 275.29

291.05 B.P. NE Herbert
and Robinson;

Note: Stations on P.C.

0+00 = S.L. Robinson: E Curb	4.08	291.16
0+50 E Curb	4.28	290.96
1+00 " "	4.49	290.75
1+320' " " P.C.	4.53	290.61
1+7360' " " P.T.	4.86	290.38
2+020' " " = 1/4 of 29' Radius Curve	5.08	290.16
2+3054' " " = 1/2 " " " "	5.20	290.04
0+00 = S.W. Robinson W. Curb	4.22	290.82
0+50 W. Curb	4.58	290.66
1+00 " "	4.72	290.52
1+320' " " opposite East P.C.	4.82	290.42
1+80 " "	4.90	290.34
1+90 " " P.C.	4.95	290.29
2+180' " " 1/4 of 29' Radius curve	5.14	290.10
2+4699' " " 2+3054' East curb:	5.20	290.04
#	1.19	291.05 Initial B.M.

10-8-27
Miller //

PL 1781

W. line 1780

PL 1780

PL 1784

chained

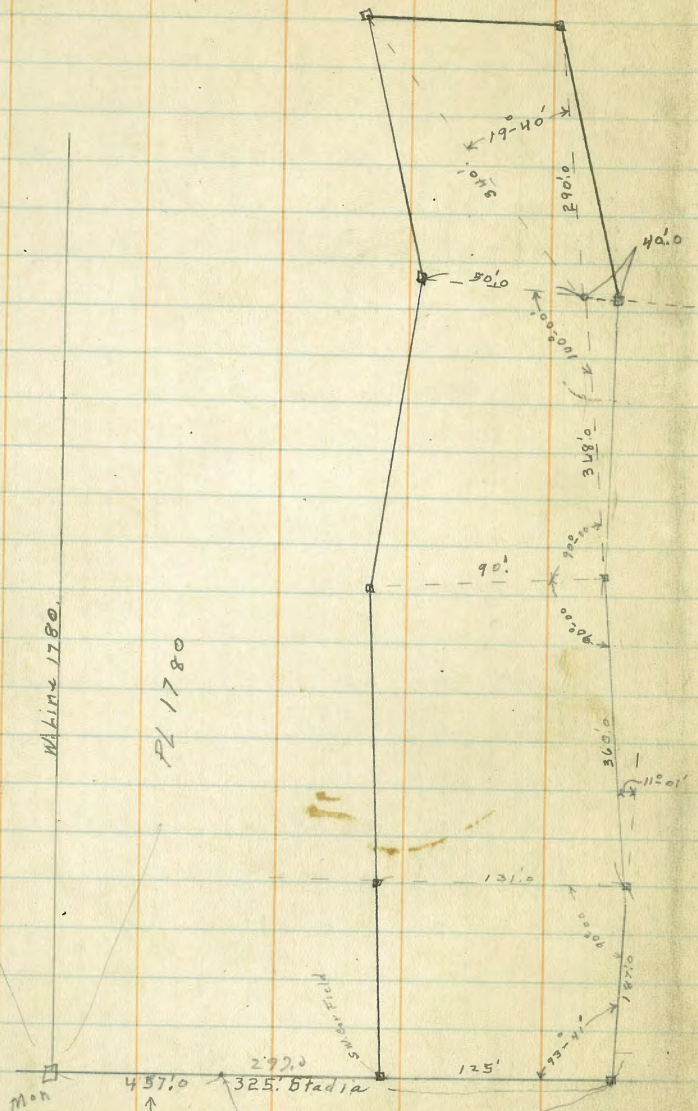
BRASS ROD
17500 METERS

APPROXIMATE

PL. 1785

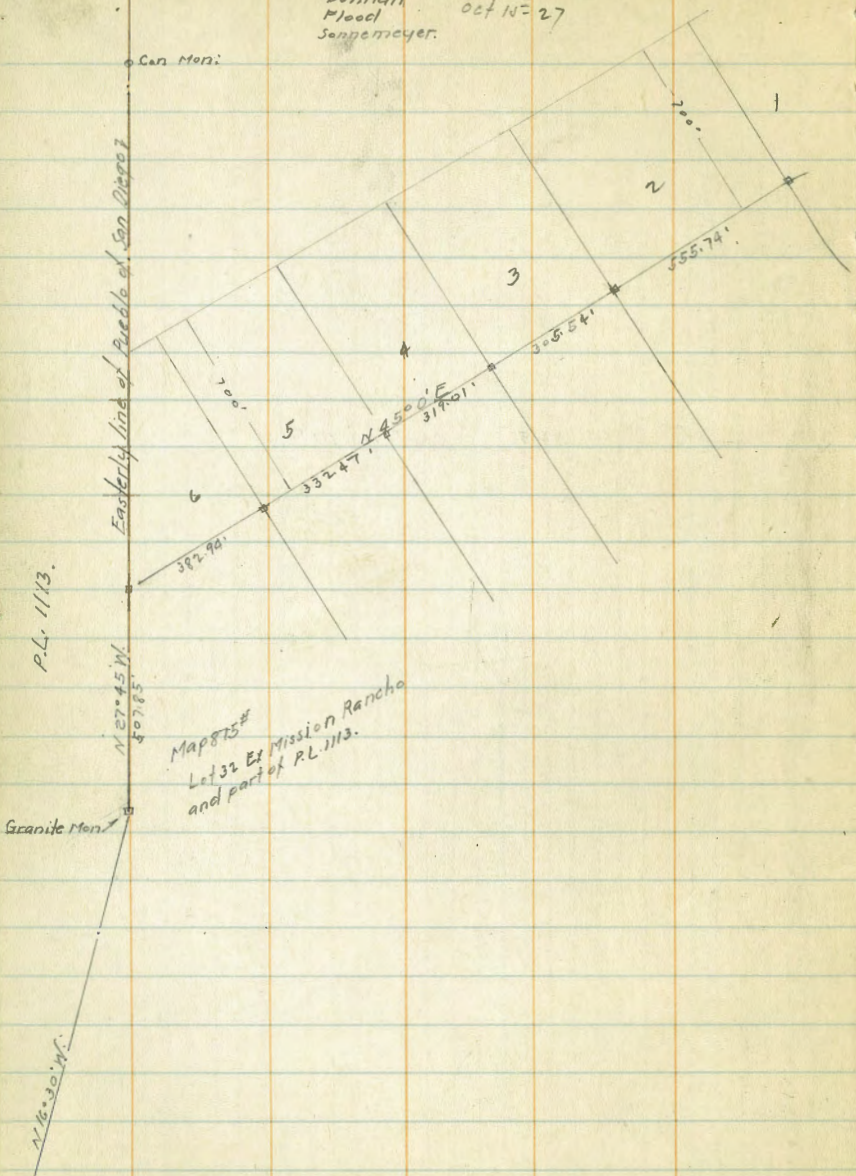
325 Vert L 17200

S. line PL-1780



Survey of a portion of Zschocetts Sub for water Line

Dennan
Mlood
Sennemeyer. Oct N=27



Levels and slopes on N.L. of Golden Gate Drive

+	π	-	Elev
5.91	353.88	353.9	0.P. 347.97 S.C. Cleveland Co. Golden Gate
N.L.		4.90	
0+00 = E.L. of 395' Radius curve: 0+200' on Hub		346.98	
12' North of 0+00 = top of fill	5.1	348.8	
0+24 ²² N.L.	5.2	348.7	
5' North of 0+24 ²² = top of fill	5.4	348.7	
0+48 ⁶⁹			
4' South = Top of bank	5.5	348.4	
N.L.	8.9	345.0	
13' N.	21.7	332.2	
26' N.	31.7	322.2	
39' N.	41.0	312.9	
52' N.	49.6	304.3	
65' N.	59.4	294.5	
78' N.	68.7	285.2	
91' N.	77.0	276.7	
104' N.	85.7	268.2	
117' N.	92.7	261.2	
130' N.	98.6	255.3	
143' N.	106.8	247.1	
156' N.	113.7	240.2	
169' N.	112.0	241.9	
there is a little wash that would go out 50' beyond 169'			
0+72 ⁹⁶		353.5	
5' South of N.L.	5.4	348.5 ✓	
N.L. = Top of fill.	6.1	347.6 ✓	
This slope out = the same 0+48 ⁶⁹			

+	π	-	Elev.
	353.88		
	0+77 ²⁸	353.9	
N.L.		4.9	349.0 ✓
7' N of N.L. = Top of fill		4.6	349.3 ✓
	1+21 ⁶⁰		
N.L.		5.8	348.1 ✓
5' North of N.L. = Top of fill		5.7	348.4 ✓
	1+45 ⁹² = End of curve		
	1+46 ⁹³ = BC 82' Radius: curve divided into 3 = parts.		
N.L. = Top of fill		5.4	348.5 ✓
4' South of N.L.		5.3	348.6 ✓
6 " " "		5.9	348.0 ✓
	1+63 ⁸²		
N.L.		8.7	345.4 ✓
9' S of N.L.		6.4	349.5 ✓
13' N of N.L.		21.9	304.0 ✓
26 " " "		29.8	304.1 ✓
39 " " "		39.8	314.1 ✓
52 " " "		50.3	303.1 ✓
65 " " "		60.2	293.7 ✓
78 " " "		68.8	285.1 ✓
91 " " "		76.6	277.5 ✓
104 " " "		87.7	266.4 ✓
117 " " "		94.1	259.8 ✓
130 " " "		108.8	245.1 ✓
143 " " "		115.8	238.1 ✓
156 " " "		134.0	219.5 ✓
			1/ Bottom of canyon:

35388

3539

c/c.

14

169 N 128.0 3459 ✓

182 N. 127.0 3469 ✓

178027

N.U. 6.5 3474 ✓

20' N of N.U. = Top of slope 8.5 3484 ✓

1798" = P.R.C.

N.U. 6.9 3490 ✓

15' N of N.U. = Top of fill 6.3 3496 ✓

End of curb N.W. Cor Cleveland and Golden Gate: 6.84 3481 ✓

Note at 1779 a clump of 2 small eucalyptus from 4" to 6" diameter = 3' South of N.U.

at 0+31 = 1" eucalyptus 15' S of N.U.

at 0+40 = Fan Palm 2' S of N.U. (Tree 18" diameter)

5.91 347.97 = initial B.M.

Curb Levels on Mansfield-Adams to 10-25-27
 School St. + School St. Mansfield to Hawley Blvd Miller

Mansfield

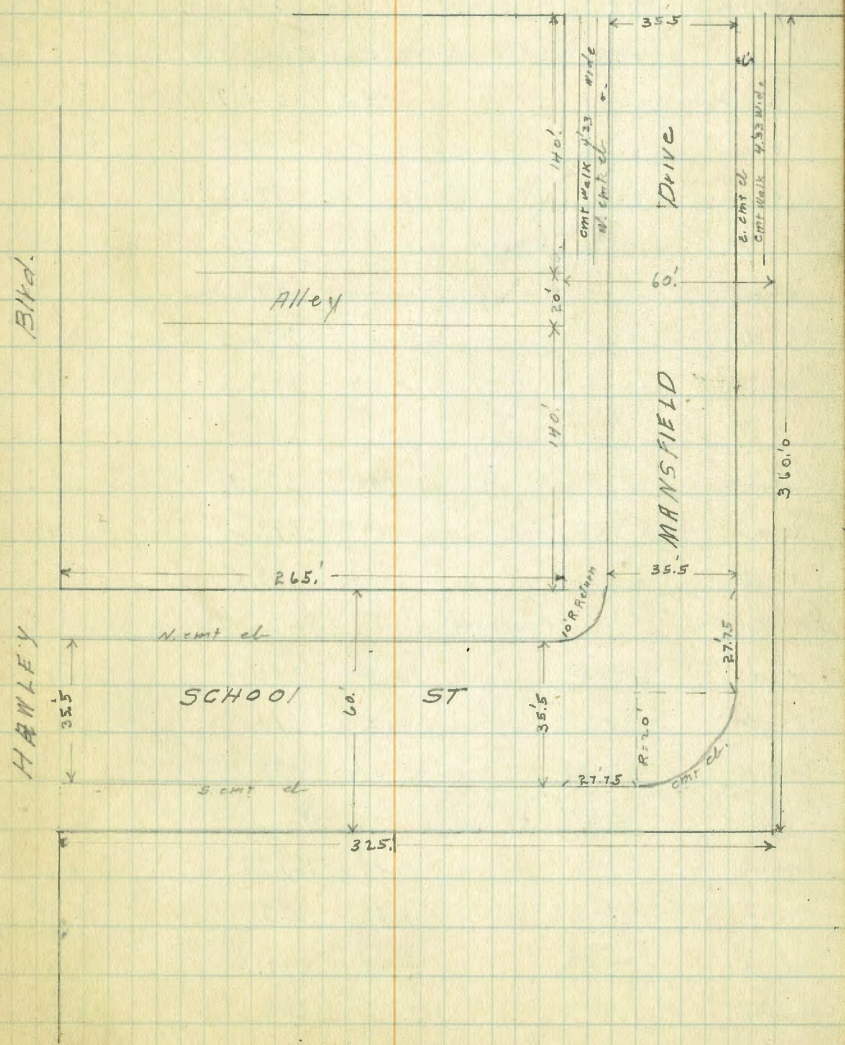
S.E. Adams +
 Mansfield
398.6

B.M. 5.83 398.41 392.78

30' Stone Adams Ave

Adams Ave

Walk	5.73	392.9
E. cl	5.95	392.7
W. cl	5.89	392.7
Walk	5.73	392.9
40's		
Walk	5.87	392.7
W. cl	5.91	392.7
E. cl	5.85	392.7
Walk	5.70	392.9
80's		
Walk	5.55	393.1
E. cl	5.84	392.7
W. cl	5.96	392.6
Walk	5.70	392.9
104's		
Walk covered with dirt		
W. cl	6.24	392.4
E. cl	6.17	392.4
Walk	6.15	392.4
125's		
Walk	6.06	392.5
E. cl	5.87	392.7
W. cl	6.41	392.2



398.41

398.6

140' S = N Line Alley on West

W. cl	6.58	392.0
E. cl	6.25	392.3
walk	6.17	392.4

165' S = End of ch. S. of Alley on W.

walk	5.85	392.7
E. cl	5.87	392.7
W. cl	6.10	392.5

188' S

W. cl	6.26	392.3
E. cl	6.02	392.6
walk	5.97	392.6

200' S

walk	5.81	392.8
E. cl	5.95	392.6
W. cl	6.06	392.5

220' S

W. cl	5.97	392.6
E. cl	5.83	392.7
walk	5.64	392.7

240' S

walk	5.49	293.1
E. cl	5.54	293.1
W. cl	5.43	293.2
walk	5.40	293.2

398.61

Mansfield School Sts.

398.6

16

270' S.

walk	4.79	393.8
W. cl	4.91	393.7
E. cl	5.04	393.6
walk	4.82	393.8

300' S. = N. Line of School St

walk	4.34	394.3
E. cl	4.58	394.0
W. cl	4.57	394.0
walk	4.37	394.2

275 S. of N. Line School St on E. cl Line = Beginning 20' R Curve

E. cl	4.49	394.1
walk	4.41	394.2

School St

275 E. of W. Line of Mansfield on S. = End of 20' R Curve

S. cl	4.79	393.8
walk	4.58	394.0

00 = W. Line Mansfield

W. cl	4.81	393.8
S. cl	5.00	393.6
N. cl	5.03	393.6
walk	4.60	394.0

20' W

walk	4.64	393.9
N. cl	4.92	393.7
S. cl	5.13	393.5
walk	4.93	393.7

398.61

397.5

T.P.	3.94	397.52	5.03	393.58
	45' N of Mansfield			
walk		3.98		393.5
s. cl		4.12		393.4
N. cl		3.84		393.7
walk		3.57		393.9
	65' W			
walk		3.80		393.7
N. cl		3.96		393.5
s. cl		4.26		393.2
walk		4.04		393.5
	100' W			
walk		4.18		393.3
s. cl		4.40		393.1
N. cl		4.15		393.3
walk		4.02		393.5
	140' W			
walk		4.17		393.3
N. cl		4.42		393.1
s. cl		4.59		392.9
walk		4.51		393.0
	170' W			
walk		4.66		392.8
s. cl		4.79		392.7
N. cl		4.71		392.8
walk		4.54		393.0

397.52

Mansfield + School Sts.

397.5

17

					200' W		
walk					4.68		392.8
N. cl					4.87		392.6
s. cl					4.91		392.6
walk					4.74		392.7
						240' W	
walk					5.02		392.5
s. cl					5.16		392.3
N. cl					5.18		392.3
walk					5.07		392.4
						265' W = E. Line Hawley Blvd	
walk					5.01		392.5
N. cl					5.24		392.2
s. cl					5.23		392.3
walk					5.16		392.3
T.P.	3.05	395.53	5.04				392.48
ch on BM S.W Adams + 34 th Sts			6.24				389.29 = 389.25

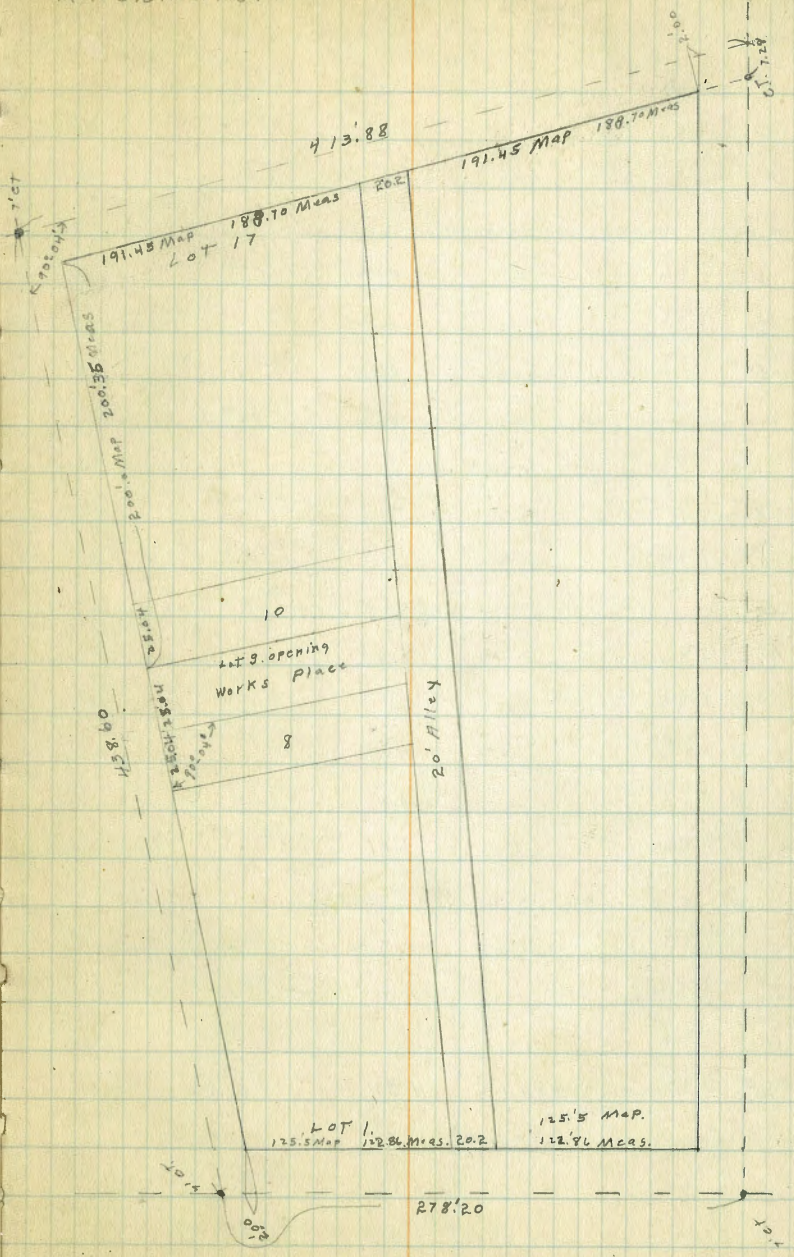
See Alley BIK J. U.H. Sub
 & Work S. Place = Lot 9 BIKJ.

10-25-27
 miles

B.M. S.E. Adams + 30th 389.0 W

18

B.M.	3.24	394.19	390.95	SE. Boundary + Adams
	00 = $\frac{1}{2}$ Alley + W. Line Boundary Stations on $\frac{1}{2}$ Alley			
S		4.5	389.7	✓
E		4.4	389.8	✓
N		4.5	389.7	✓
	3.25 W			
N		4.2	390	✓
E		4.2	390	✓
C+T		4.5	389.7	✓ N.E. Car House 3' in Alley
	34' W			
S		4.4	389.8	✓
S+3.0		4.4	389.8	✓ N.W. Car House 3' 0" in Alley
E		4.6	389.6	✓
N		4.0	390.2	✓ center walk on line
	55' W			
N		4.3	389.9	✓ on line S.W. Car House
E		4.3	389.9	✓
S		4.6	389.6	✓
	27' W			
S		4.4	389.8	✓
E		4.1	390.1	✓
N		4.2	390.0	✓
	93' W. Garage on S. dirt floor on line			
N		4.4	389.8	✓
E		4.0	390.2	✓
S		4.0	390.2	✓



394.19

S	110' W	4.5	389.7	✓
E		4.0	390.2	✓
N		4.5	389.7	
	165' W			
N		4.2	390.0	✓
E		4.0	390.2	✓
S		4.9	389.3	✓
+S		5.0	389.2	
	2+05 W			
-S		4.8	389.4	✓
S		4.1	390.1	✓
E		4.0	390.2	✓
N		4.8	389.4	✓ Top Curb E. line Works Place
	231' N			
N		4.7	389.5	✓ W. line Works Place
E		4.4	389.8	✓
S		4.0	390.2	✓
	261' S. & Double Garage on S. end floor on line			
S		3.7	390.5	✓
E		4.7	389.5	✓
N		4.7	389.5	
T.P.	4.27 394.15	4.31	389.84	✓
	300' W			
N		4.6	389.6	✓
E		4.4	389.8	✓
S		5.0	389.2	✓

394.15

Alley BIK J. Univ. Hts.

19

	3+25			
	425' W			
S	Garage on N. end floor 2' Back	4.5	389.7	✓
E	" " " " " " " "	4.6	389.6	✓
N	" " " " " " " "	4.4	389.8	✓
	3+55			
	453' W			
N	E. end 3 Garages on N. end apron on line	4.3	389.9	✓
E		4.7	389.5	✓
S		4.6	389.6	✓
	3+45			
	4.83 W. end above garages end apron on line			
S		4.9	389.3	✓
E		4.5	389.9	✓
N		4.2	390.0	✓
	4+25			
	525' W			
N		4.6	388.6	✓
E		4.0	390.2	✓
+9		4.0	390.2	
S		5.0	389.2	✓
+5		5.0	389.2	
	4+36			
	5.35 W			
-5		5.0	389.2	
S		5.2	389.0	✓
	5+0.3 N.E. cor garage	4.6	389.6	✓ 0.3 in Alley
E		4.5	389.7	✓
N		4.3	389.9	✓

4.51 394.15
5.51

Alley BIK J. V. H.

25' wide Sec Works Place

10-26-27
mills

20

S		4.9	389.3
+1.2 N.E. Cor Garage		4.9	389.3
C		5.0	389.2
N		5.0	389.2
	549' W of Mc95 = E. Line 30th st		
N		5.5	388.7
C		5.5	388.7
S	+1.8	5.2	389.0
	4' W. of E. Line - E edge Walk		
S		5.6	388.6
C		5.7	388.5
N		5.8	388.4
T.P.	5.53 393.77	5.91	388.24
CHK on BM S.E. 30th & Adams		4.72	389.05 = 389.04

T.P. Page 19.	4.54	394.42	387.88
	00 = S. Line Works Ave		
E		7.56	386.86 / amt cl return
+0.7 = gutter		7.75	385.67 / amt
C		7.21	31.7
W Line		7.70	386.72
+0.5		7.50	388.22 / amt cl, return
	12' S.		
-0.5		6.3	388.1 / amt cl
W		6.5	387.9
C		6.1	388.3
+1.2		6.5	387.9
E		6.0	388.4 / amt cl
	55' S		
C		5.5	388.9 / amt cl
C		5.5	388.9
W		6.0	388.4
+0.5		6.0	388.4 / amt cl
	95' S		
-0.5		5.5	388.9 / amt cl
W		4.7	389.7
+1.2		5.4	389.0
C		5.0	389.4 / amt cl
	156' S. on E. = N. Line Alley		
E		5.0	387.4 / amt cl
C		4.6	389.1
W		4.9	389.5
W + 0.5		5.25	389.7 / amt cl

Levels for Sewer Connection
Between Fire Alarm Central Station &
Existing Comfort Station in Balboa Park

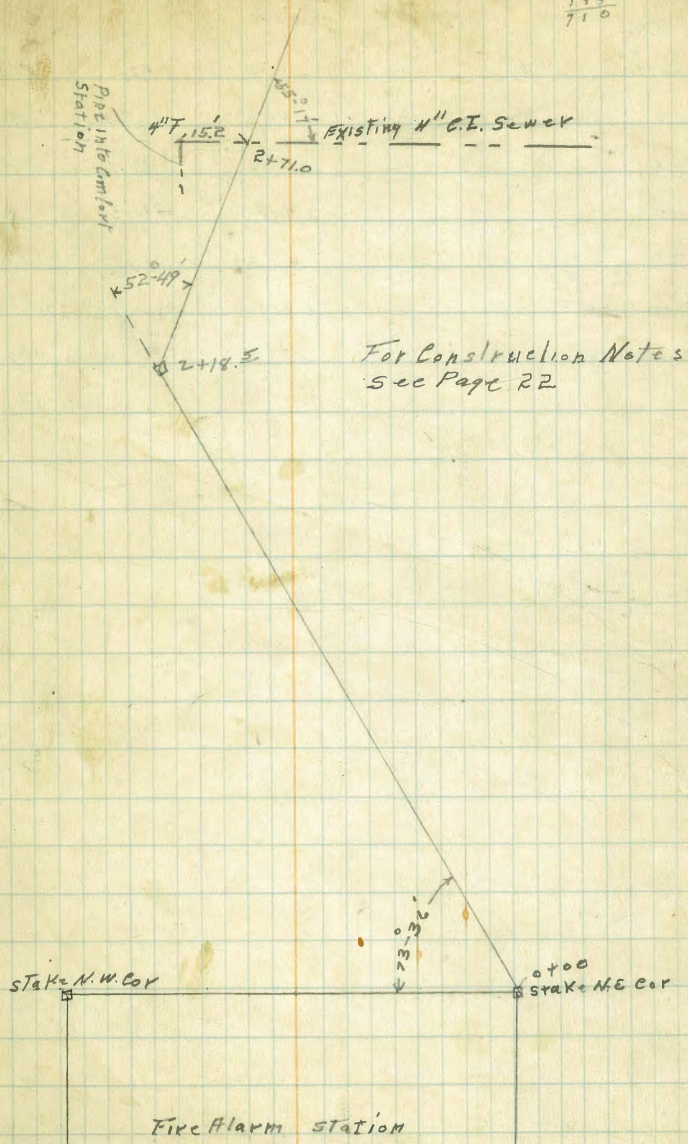
10-27-27
mill

165.17
400

335
165
548
185
710

21

B.M.	9.27	169.25		159.98	SW 8 th St & Cedar
T.P.	12.47	181.16	0.56	168.69	
T.P.	10.04	190.74	0.46	180.70	
T.P.	6.10	191.03	5.81	184.93	
0+00 Stake	N.E. Cor Fire Alarm Station	2.90		188.13	Top Stake
0+00	" " " " " "	3.2		187.8	ground
0+50		2.8		188.2	
1+00		4.0		187.0	
T.P.	3.86	190.16	4.73	186.30	
1+42		4.5		185.7	Top Cobble T Wall
1+43		5.6		184.6	S. edge Road
1+55		4.7		185.5	E. Road
1+67		5.0		185.2	N. Edge Road
1+70		4.1		186.1	
1+83		4.4		185.8	
2+00		10.0		180.2	
2+18.5	$\Delta 52^{\circ} 49' RT$	11.1		179.1	
T.P.	0.27	177.96	12.49	177.67	
2+52		2.6		175.4	
2+47	Bottom of Cobble Gutter	6.1		171.9	
2+71.0		6.2		171.8	ground
2+71.0	connection with 4" sewer	8.60		169.36	Flowline



For Construction Notes
See Page 22

Robt W Snyder, Architect says the stake at the
NE Cor of Bldg is Eler 9.45
Basement Floor 3.86
First Floor 14.48
G.R.H. 10-28-27

10-29-29
Miller

25

Sewer Construction Bet
Central Fire Alarm Station & Existing 11"

B.M. Sewer 11" Balboa Park
2.80 190.93 188.13 Top Stake

ME. Cor Pitt 000 Alarm Station		3.10	187.83	180.00	+ 7.83
+ 50		2.47	188.46	179.23	+ 9.23
1 + 00		3.48	187.25	178.46	+ 8.79
1 + 40		4.63	186.30	177.84	+ 8.46
1 + 80		4.52	186.41	177.22	+ 9.19
TR 2.66	188.12	5.47	185.44		
R + 18 ⁵⁰ Δ 52-49 Rt		8.12	180.00	174.63	+ 3.37
2 + 71 = Connection Ex 4" Sewer				169.36	

McHugh
Flood
Rutledge
12/6/27

X section Notes of Alley
+ Block 10 Teralia

B.M. 4.13 374.00 369.87 ^{N.W. Orange} #37th

0+00 = S.L. Orange

Paving
0+00

E. curb 4.73

E.L. 4.86

C.L. 5.10

W.L. 4.65

W. curb 4.34

0+05

W.L. 4.0

☐ 4.5

EL 4.5

0+35

E.L. 4.13

☐ 4.4

W.L. 4.4

0+65

W.L. 4.3

☐ 4.4

E.L. 4.8

0+92

EL 5.0

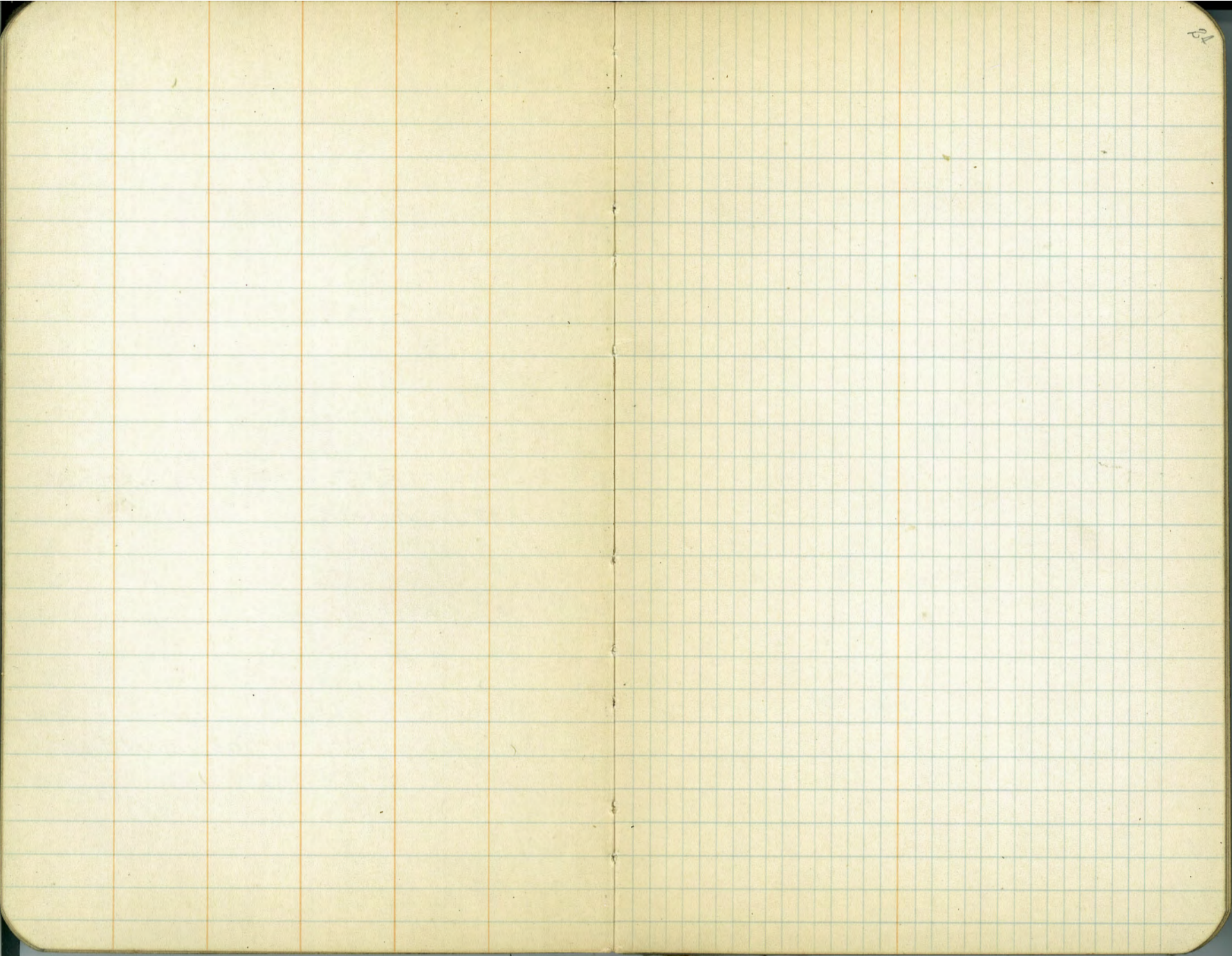
☐ 5.0

W.L. 4.9

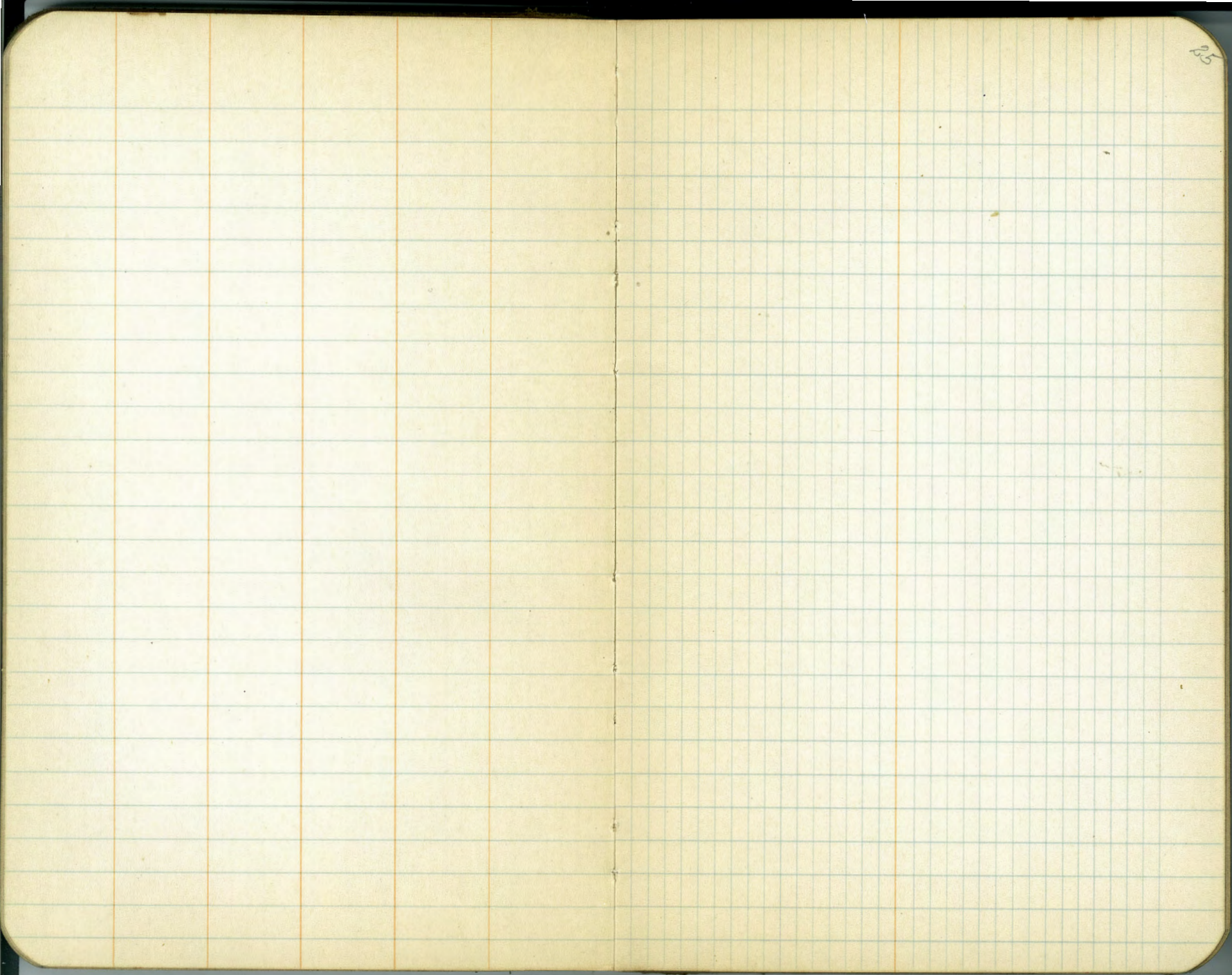
= ☐ Garage on East. Approx 8' long 1.6' in Alley
Garage is 0.4' back

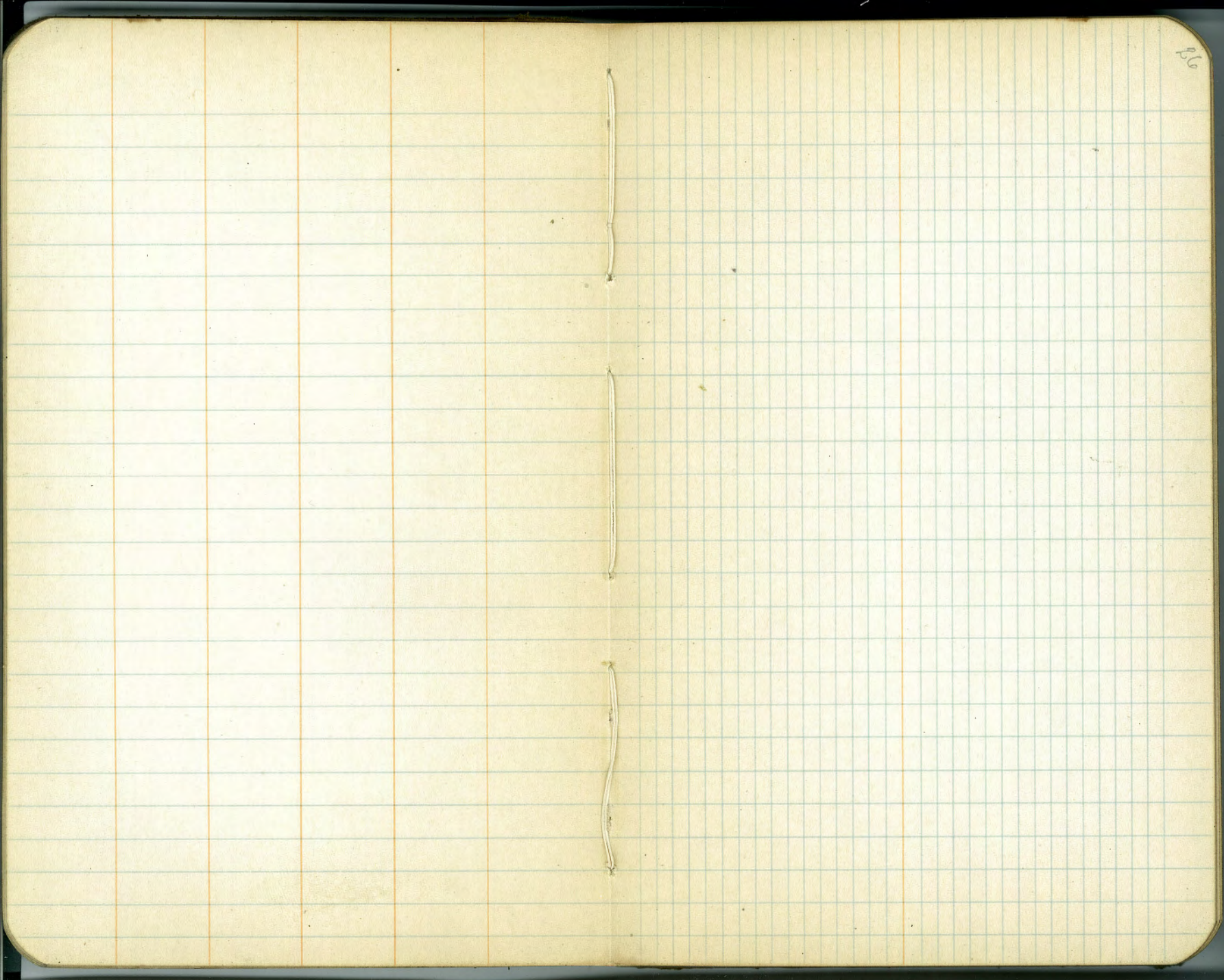
= ☐ House on West 1' Back

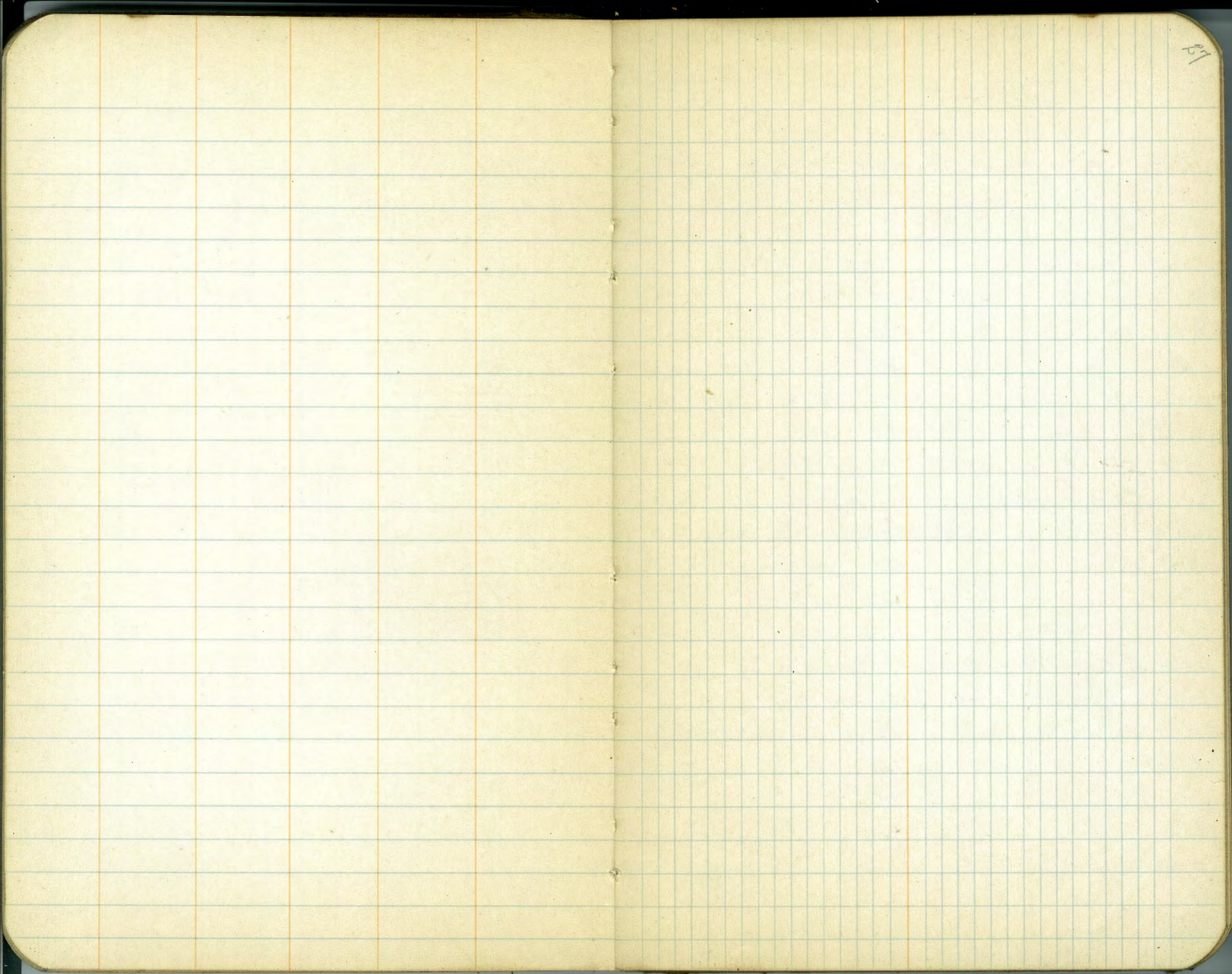
= ☐ Garage on west on line Board floor



21







13

McHugh
12/24/27

28

X section Alley Block 1
St Louis Heights
+ - ELEV BM N.E.R.P.
 THORN & GRADAR
 323.49

B.M.	7.41	330.90		323.49
T.P.	4.31	334.48	0.73	330.17

334.5

0+00 = S.L. UPAS
16' Alley

0+00	PARING			
E C6	"	4.80		329.7
E Pavement	"	4.80		329.7
♀	"	5.05		329.5
W Pavement	"	4.93		329.6
W C6	"	4.84		329.7
0+24.5	♀ ManHole	4.94		329.6

0+90				
WL-9.5		6.02		328.5
WL		6.1		328.4
♀		6.2		328.3

♀+7.8	Edge of Apron	5.77		328.8
E.L.		5.70		328.8
1+00	Beginning of shed 0.2 in alley			
1+35	End of same shed 0.2 in alley			

on East

1+57				
E 1+1		7.4		327.1
♀		7.1		327.4
WL		7.0		327.5

1+69				
T.P.	3.50	330.78	7.26	327.22
WL-5.3 on concrete		2.74		328.1

330.8

= ♀ Double Garage on West, concrete floors.
4.5' Back 20' wide. ♀ Garage on East 4.1' Back
Apron 0.2 in Alley

= ♀ dirt floor Garage on East 1.0 in Alley

= ♀ concrete floor Garage on west 5.3' Back

330.8

	+	\bar{x} 330.78	-	
WL-5			3.5	327.3
WL			3.8	327.0
¢			4.0	326.8
EL.			3.8	327.0
2+50				
EL			4.9	325.9
¢			5.5	325.3
+3			5.3	325.5
WL.			4.3	326.5
3+00				
WL			4.6	326.2
+5			6.0	324.8
¢			6.1	324.7
EL			5.9	324.9
3+25	¢ manhole		6.04	324.8
3+50				
EL			6.2	324.6
¢			6.6	324.2
WL			5.7	325.1
4+00				
WL			6.4	324.4
¢			6.9	323.9
EL			7.1	323.7
T.P.	4.84	328.76	6.86	323.92
4+08	EL. on Apron		4.45	324.4

concrete floor Garage on East Edge of
 = ¢ Apron on line. Garage door 8.3' Back

328.8

	+	X	-
		328.76	
4+50			
EL		5.3	323.5
¢		5.3	323.5
WL		3.4	325.4
4+78			
EL-0.6	on edge of Apron	4.43	324.4
4+97.6			
EL-0.6'		4.42	324.4
5+05			
WL	on concrete	4.10	324.7
WL	on ground	4.40	324.4
¢		4.5	324.3
EL		4.4	324.4
5+33			
EL.		4.5	324.3
¢		4.2	324.6
WL	on ground	4.0	324.8
WL	on walk	3.65	325.2
5+57			
WL		4.9	323.9
¢		5.0	323.8
EL		5.6	323.2
EL+2	on concrete	5.64	323.2
5+93			

{ = start of concrete Apron of double Garage on East
 Apron 0.6' Back
 = End of concrete Apron of double Garage on East

{ = ¢ of Concrete floor garage on West built in
 two story Stucco dwelling. Building is on line

= ¢ of concrete walk on W.L.

= ¢ concrete floor garage on East Built in rear
 end of dwelling facing on Thorn st. 2' Back

328.8

	+	Σ	-	
EL		328.76	5.4	323.4
ℓ			5.6	323.2
WL			5.5	323.3
T.P.	6.07	327.38	7.45	321.31
6500 ²⁰	= N.L. THORN ST.			
W cb			5.61	321.8
PAVING			5.75	321.7
ℓ			5.86	321.6
PAVING			5.69	321.7
F cb			5.51	321.9
T.P.			3.85	323.53

BM3 23.49

.04 ERROR

327.4

Cross Section of Golden Gate Drive 40' wide
 Cleveland east to alley.

Moore
 12/20/87

SEDP 641 35438 34797 Cleveland Golden Gate

Sec A at WL Cleveland

N top curb	6.33	348.05
N gutter top	6.25	347.53
1/4	6.59	347.79
C	6.22	347.94
1/4	6.67	347.76
S gutter	6.77	347.61
S top curb	6.70	348.18

Sec B 18.8' ±

S top paving	6.1	348.3
1/4	6.4	348.0
C	6.6	347.8
1/4	6.9	347.5
N curb	6.8	347.6
+5	6.9	347.5

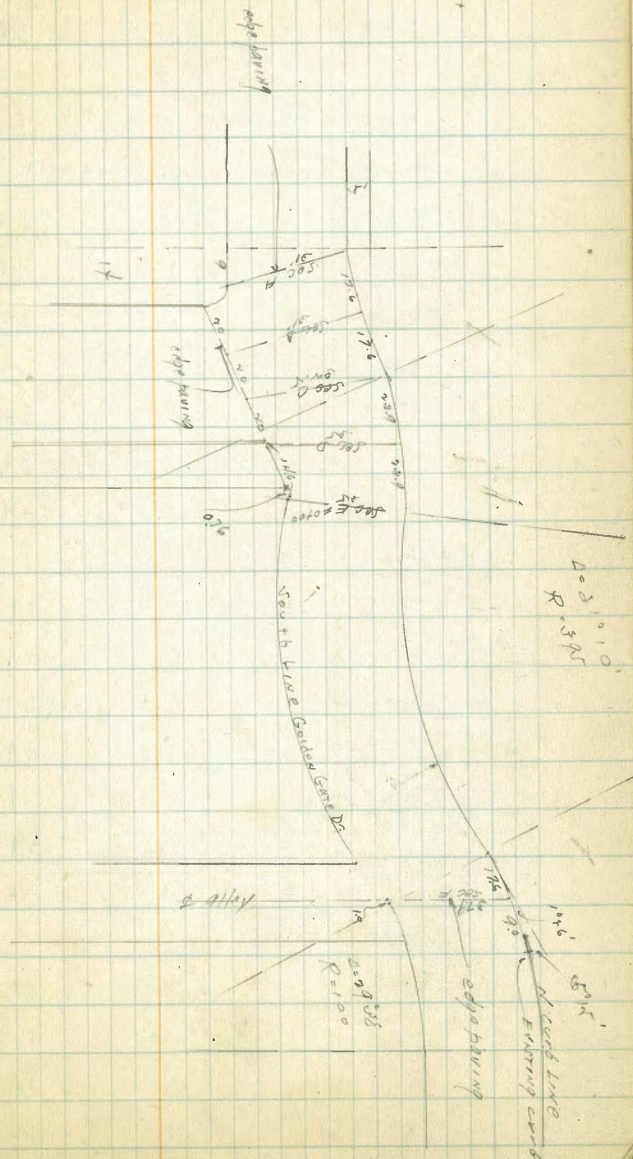
Sec C 18.8' ±

-5	7.2	347.2
N curb	7.1	347.3
1/4	7.1	347.3
C	6.8	347.6
1/4	6.8	347.6
S edge paving	6.2	348.2

Sec D 21.95' ±

S top curb	6.44	347.96	348.0
S gutter	6.8	347.6	

El Cleveland



1/4	7.0	347.4
c	7.3	347.1
1/4	7.7	347.2
Nob	7.3	347.1
45	7.7	346.7

Sec E = PC = 0400 station 19.25'

N	6.4	348.0
cb	5.7	348.7
1/4	6.9	347.5
c	6.8	347.6
1/4	6.6	347.8
cb	6.2	348.1
S	6.1	348.3

0245.9

S	4.5	348.9
cb	5.8	348.6
1/4	6.1	348.3
c	6.1	348.3
1/4	6.0	348.4
cb	5.6	348.8
N	5.5	348.9

0272.54

N	7.1	346.5
cb	6.0	348.4
1/4	5.5	348.9
c	5.4	349.0

1/4	5.2	349.1
cb	5.0	349.4
S	5.0	349.4

1+16.80

S	5.2	349.2
cb	5.5	349.1
1/4	5.5	348.9
c	5.6	348.8
1/4	5.6	348.8
cb	5.5	348.9
N	7.1	347.1

1+37.76

N	5.6	348.8
cb	5.8	348.6
1/4	5.4	349.0
c	5.4	349.0
1/4	5.1	349.3
cb	5.2	349.2
S	4.9	349.5

1+48.9 = approx. w/ alley

-v	5.15	349.23
S	5.1	349.3
cb	4.9	349.5
1/4	5.1	349.3
c	5.5	348.9
1/4	5.4	349.0
cb	5.7	348.7
N	5.6	348.8

w/ 1/2 alley

10030 = PRL

N	V. 4	349.0
cb	V. 8	348.6
1/4	V. 7	348.7
c	V. 7	348.7
1/4	V. 5	348.9
cb	V. 6	348.8
S Top paving	V. 5	348.9
SW edge of paving with alley	V. 4	349.0

Sec F = edge of paving approx & alley

S	V. 5	348.9
cb	V. 7	348.7
1/4	V. 5	348.9
c	V. 5	348.9
1/4	V. 6	348.8
cb	V. 8	348.6
N	V. 3	349.1

9' EAST of Last Sec F =

Top of existing curb north line	V. 46	348.92
---------------------------------	-------	--------

Bliss
 13 de 11
 X Section of James Place Loma Portal
 Merpan From Rosecrans to Chatsworth

B.M. SWBP					
Station Rosecrans	6.62	48.57		41.95	56.57
T.P.	7.30	55.68	0.19	48.38	51.05
T.P.	6.18	57.31	9.55	51.13	56.95

Sec A
 Elevation on Paving on Rosecrans

Top cb at PT of curb return N Side	8.31	49.0
Gutter at PT of cb " " "	9.32	
Paving at " " " "	9.00	
Prop Produced East to Paving	8.15	
cb " " " "	7.90	49.4
1/4 " " " "	7.65	
1/4 " " " "	7.43	
1/4 " " " "	7.19	
cb " " " "	6.99	50.3
S Prop " " " "	6.69	
Paving at PT of curb return on South	5.77	
Gutter " " " " "	6.26	
Top cb " " " " "	5.28	52.0
Catch Basin 3's of Prop on South	6.78	

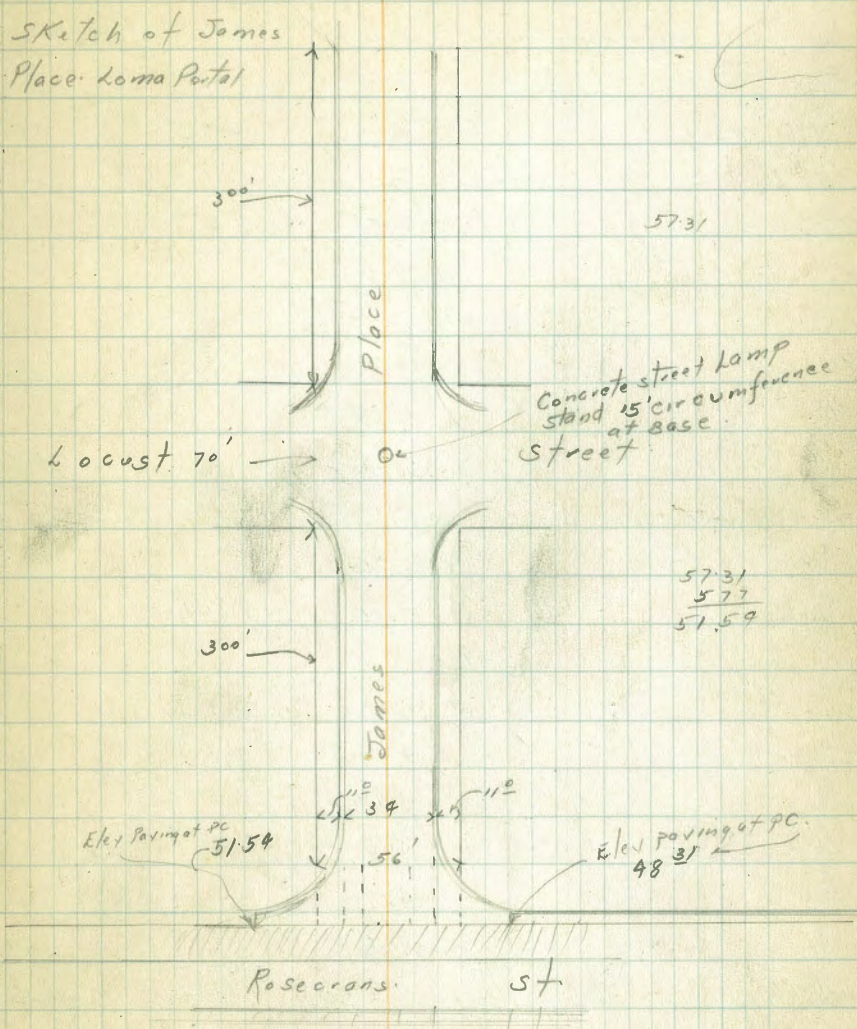
etc = Whine of Rosecrans

Prop + 1/2 Top cb on Return	5.62	51.7 5
1/2 in gutter	6.65	
+5	6.31	
cb	6.22	51.1 5
1/4	6.4	
1/4	6.8	
1/4	7.2	

56
 22
 34

35

Sketch of James Place Loma Portal



T
5731

cb	7.8	49.5 N
+6 edge of concrete Gutter	8.23	
+9.5	8.56	
+9.6 Topcb	7.59	49.7
	0+28 P.C.	
Topcb	6.57	50.7 N
Gutter	7.23	
+2.5	7.01	
1/4	6.5	
1/2	5.8	
1/4	5.4	
+6 edge of Gutter	5.63	
Gutter	5.95	
Topcb	5.15	52.1 S
	0+50	
S Top Cb	4.20	53.1 S
Gutter	4.82	
+2.5	4.60	
1/4	4.5	
1/2	4.9	
1/4	5.6	
+6	6.03	
Gutter	6.26	
N Topcb	5.59	51.7 N
	100' West	
N Topcb	3.28	54.0 N

T
5731

36

Gutter	3.93	
+2.5	3.70	
1/4	3.2	
1/2	2.7	
+3	2.5	
1/4	2.4	
+6	2.59	
Gutter	2.83	
S Topcb	2.18	55.1
	150' West	
S Topcb	0.06	57.2
Gutter	0.72	
+2.5	0.45	
1/4	0.2	
1/2	0.5	
1/4	1.0	
+6	1.42	
Gutter	1.62	
N Topcb	0.97	56.3
T.P.	11.83	69.13
		0.01
		57.30
	200' West	
N Topcb	10.46	58.7
Gutter	11.12	
+2.5	10.90	
1/4	10.4	
1/2	9.8	

X
69.13

69.13

76.57 67

300' West E Line of Locust

+3	9.5	
1/4	9.8	
+6	10.17	
Gutter	10.94	
Topcb	9.78	59.3
250' West		
S Topcb	7.77	61.3
Gutter	8.92	
+2.5	8.14	
1/4	7.7	
2	7.6	
1/4	8.2	
+6	8.57	
Gutter	8.82	
N Topcb	8.17	60.9
277' West PC		
N Topcb	6.93	62.2
Gutter	7.58	
+2.5	7.39	
1/4	7.0	
2	6.7	
1/4	6.7	
+6	6.92	
Gutter	7.04	
Topcb	6.68	62.4

S+2.7 Topcb	5.95	63.1
S+2.8	6.61	
S+5.7	6.90	
cb	6.5	62.6
+5	6.1	
1/4	6.1	
2	6.1	
1/4	6.1	
+4	6.2	
cb	6.5	62.6
+5 edge gutter	6.92	
+8	7.15	
+8 Topcb	6.50	62.6
E cb		
N	6.4	
cb	5.8	63.3
1/4	5.6	
2	5.6	
1/4	5.6	
cb	6.0	63.1
+5	6.2	
S	6.0	
E 1/4		
S	5.8	
+3	6.0	

X
69.13

+6	6.0	
cb	5.8	63.3
1/4	5.5	
1/2	5.4	
1/4	5.5	
cb	5.6	63.5
N	5.9	

1/2

N	5.6	
cb	5.4	63.7
1/4	5.2	
1/2	5.3	
1/4	5.3	
cb	5.5	63.6
S	5.7	

W 1/4

S	5.5	
cb	5.2	63.9
1/4	5.1	
1/2	5.1	
1/4	5.2	
cb	5.3	63.8
N	5.6	

W. cb.

N	5.5	
cb	5.2	63.9

X
69.13

38

1/4	5.1	
1/2	5.0	
1/4	5.0	
cb	5.0	64.1
S	5.2	

W. line of Locust

S + 3. Top cb 4.63 64.5

Gutter 5.27

+6 5.05

cb 5.0

1/4 4.9

1/2 4.8

1/4 5.0

cb 5.2 63.9

+ 5 edge of gutter 5.50

Gutter 5.76

Top cb 5.12 64.0

25' West of the W line of Locust
PC

N 4.80

Gutter 5.34

+ 2.5 5.20

cb 1/4 4.8 64.3

1/2 4.5

1/4 4.7

+6 4.8

Gutter 5.06

69.13

69.13

39

S.TopCb. 4.90 64.7

50' West

¢ 3.5

1/4 3.9

S.Topcb 4.24 64.9

+6 4.36

Gutter 4.88

Gutter 4.58

+2.5 4.65

N.Topcb 2.98 65.1

1/4 4.5

200' West

¢ 4.4

N.Topcb 3.65 65.4

1/4 4.6

Gutter 4.35

+6 5.03

+2.5 4.06

Gutter 5.23

+4 3.6

N.TopCb 4.56 64.5

1/4 3.5

100'

¢ 3.2

N.TopCb 4.20 64.9

1/4 3.4

Gutter 4.86

+2 3.3

+2.5 4.65

+6 3.64

1/4 4.2

Gutter 3.92

¢ 3.8

S.Topcb 3.25 65.8

1/4 4.1

250'

+6 4.28

S.Topcb 3.11 66.0

Gutter 4.50

Gutter 4.02

S.Topcb 3.86 65.2

+2.5 3.38

150' West

1/4 3.1

S.TopCb 4.54 65.6

¢ 3.0

Gutter 4.20

1/4 3.2

+2.5 4.00

+6 3.82

1/4 3.8

Gutter 4.22

69.13

Topcb		3.48	65.6
T.P.	10.79	76.65	3.27 65.86
		2.75	West P.C.
N Topcb		10.86	65.8
Gutter		11.58	
+2.5		11.24	
1/4		10.7	
1/2		10.3	
1/4		10.3	
+6		10.38	
Gutter		11.90	
Topcb		10.37	66.3
		300'	West E Line of Evergreen
S 7.3 Topcb	on Par.ing	10.10	66.5
Gutter		10.61	
Cb		10.21	66.4
1/4		10.00	
1/2		10.06	
1/4		10.27	
Cb		10.64	66.0
+8 Gutter		11.20	
Topcb		10.55	66.1
		W. line of Evergreen = 00	
N 7.3 Topcb	on Par.ing	9.27	67.4
Gutter		10.00	
Cb		9.43	67.2

76.65

10

1/4	9.23	
1/2	9.14	
1/4	9.20	
Cb	9.33	67.3
+8 Gutter	9.60	
+8 Topcb	9.00	67.6
	25'	West of the W. Line of Evergreen P.C.
S Topcb	8.67	68.0
Gutter	9.30	
+2.5	9.00	
1/4	8.8	
1/2	8.6	
1/4	8.6	
+6	9.00	
Gutter	9.27	
N Topcb	8.64	68.0
	50'	West
N Topcb	7.94	68.7
Gutter	8.59	
+2.5	8.34	
1/4	8.1	
1/2	8.0	
1/4	8.2	
+6	8.22	
Gutter	8.96	
S Topcb	7.82	68.8

76.65

100' West

S Top cb	6.20	70.4
Gutter	6.86	
+2.5	6.66	
1/4	6.6	
¢	6.5	
1/4	6.7	
+6	7.00	
Gutter	7.26	
N Top cb	6.62	70.0

150' West

N Top cb	5.25	71.4
Gutter	5.88	
+2.5	5.62	
1/4	5.2	
¢	5.0	
1/4	5.0	
+6	5.03	
Gutter	5.25	
S Top cb	4.60	72.0

175' West PC on North

S Top cb	5.79	72.8
Gutter	4.43	
+2.5	4.22	
1/4	4.2	
¢	4.2	
1/4	4.5	

76.65

41

+6	4.99	
Gutter	5.22	
N Top cb	9.57	72.1
185' West P.C. on South		
N Line +10 Top cb	4.94	72.2
Gutter	5.10	
cb	5.02	71.6
+1.5	4.92	
1/4	4.2	
¢	3.9	
1/4	3.9	
+6	3.94	
Gutter	4.12	
S Top cb	3.96	73.1

200' West

S Line +8 Top cb	2.93	73.7
Gutter	3.88	
cb	3.63	73.0
+4	3.3	
1/4	3.4	
¢	3.4	
1/4	3.8	
N cb	4.2	72.4
+8 Gutter	4.96	
N Top cb	4.20	72.4

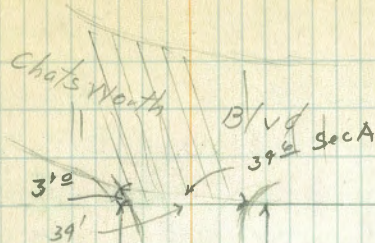
*
7.6.65

Sec A: 203' on South = 200' on North

on paving

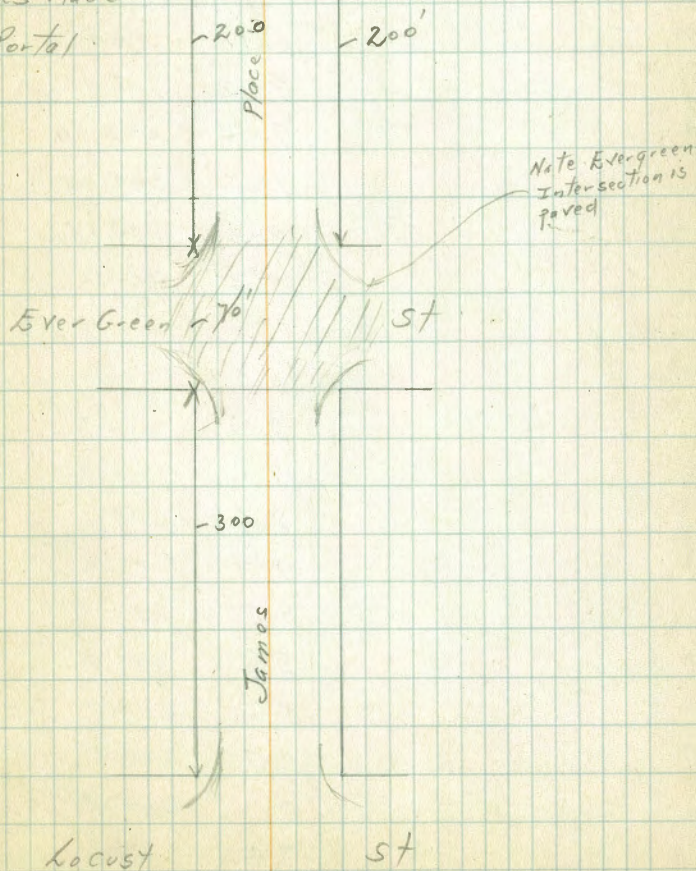
* N. line to Topch	9.21	72.4		
Gutter	9.98			
cb	9.28	72.4		
1/4	3.85			
1/4	3.97			
1/4	3.38			
cb	3.50			
+5 Gutter	3.77			
+5 Topch	2.82	73.8		
T.P.	1.11	66.55	112.1	65.94
T.P.	0.53	53.99	13.09	53.96
T.P.	1.62	96.53	9.08	94.91
B.M.S.W.B.P.				
Lythons Reservoir	9.62	91.91		

42



Sketch of
James Place

Loma Portal



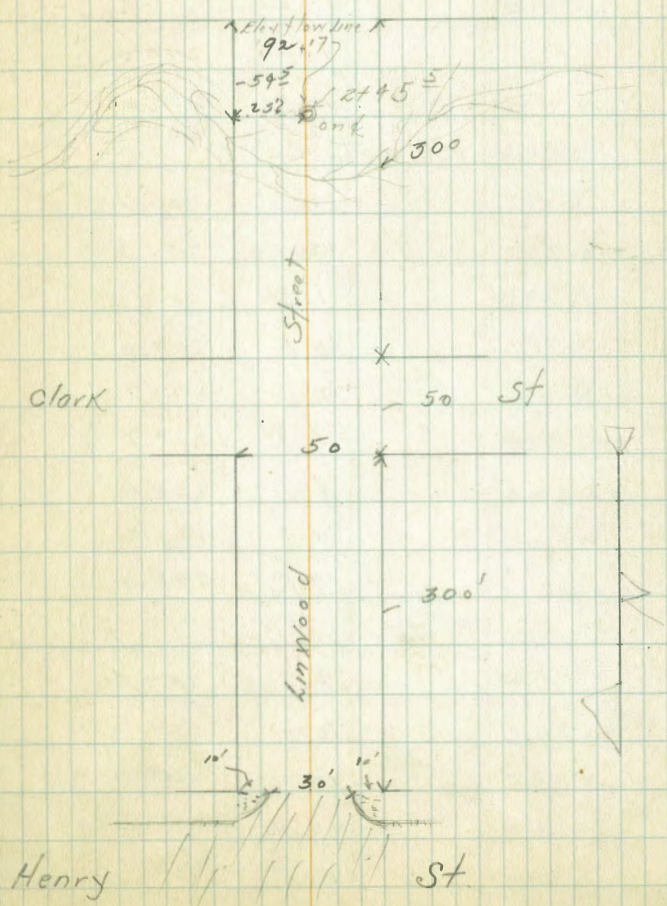
Bliss Isbell Morgan
 1/16-8 of Mission Hills Blvd
 X Sections of Linwood St. Middletown Addition from the S. line of Henry to the N. line

	8.56	227.46	218.90
B.M. NE 8th Alameda place & Henry	8.56	227.46	218.90
T.P.	0.13	219.52	13.07 214.39
E	on Paring	7.8	206.9
Top cb		8.00	206.5
Gutter		8.69	205.83
1/4		8.57	205.95
1/4		8.62	205.90
1/4		9.04	205.50
Gutter		9.88	204.64
W Top cb		9.33	205.19
W		9.3	205.2
W	10.1	204.4	
+8	9.2	205.3	
cb	9.2	205.3	
+3	9.4	205.1	
1/4	9.3	205.2	
1/4	8.8	205.7	
1/4	8.6	205.9	
+6	8.6	205.9	
cb	8.9	206.1	
+2	8.1	206.4	
E	7.9	206.6	

0+00 = S line of Henry

06' S of the S line of Henry

Sketch of Lindwood St. Middletown Addition showing width of st. and location of Man Hole North of Mission Hills Blvd



214.52

25' South

E	8.5	206.0
cb	9.0	205.5
1/4	9.0	205.5
1/2	9.1	205.4
3/4	9.7	204.8
cb	10.2	204.3
cb	10.1	204.4
W	10.9	203.6
W+10	12.4	202.1
W-10	13.6	200.9
W on WALK	12.20	201.3
cb	11.0	203.5
1/4	10.5	204.0
1/2	10.8	203.7
3/4	9.8	204.7
cb	9.9	204.6
+2	9.5	205.0
E	9.1	205.4

75' South

E	9.9	204.6
+9	10.0	204.5
cb	10.3	204.2
+1/4	10.4	204.1
E 1/2	10.4	204.1
+2	10.4	204.1

214.52

1st on Walk
Rod 4 913

44

1/4	11.2	203.3
+3	11.5	203.0
cb	11.5	203.0
W	12.6	201.9
W+2	12.3	202.2
W+10	17.1	200.4
T.P.	2.20	204.80
	11.92	202.60

100' South

W-10	5.4	199.4
W	9.1	200.7
cb	3.0	201.8
1/4	2.6	202.2
+6	1.9	202.9
1/2	1.9	202.9
3/4	1.9	202.9
+3	2.1	202.7
cb	1.6	203.2
E	0.8	204.0

102' South Walk on West

Walk on line ctr 4.13 200.67

125' South

E	17	203.1
cb	2.4	202.4
1/4	2.7	202.1
1/2	3.3	201.5
3/4	4.0	200.8

T
204.80

cb		4.6	200.2
+4		5.0	199.8
W		5.2	199.6
	135' South Walk on West		
Walk on line ctr		5.79	199.01
	150' South		
W-10		8.6	196.2
W		7.0	197.8
cb		5.9	198.9
1/4		5.2	199.6
cb		4.6	200.2
1/4		4.1	200.7
cb		3.5	201.5
E		3.2	201.6
	155' South Auto Drive Way on East		
1.0 Back ctr		5.93	201.37
	175' South		
E		5.1	199.7
cb		5.5	199.3
1/4		6.0	198.8
+3		6.7	198.1
cb		7.0	197.8
1/4		7.4	197.4
cb		8.1	196.7
+3		8.4	196.4
W		9.4	195.4

T
209.80

45

W+10		11.3	193.5
	200' South		
W-10		13.3	191.5
W		10.9	193.9
cb		10.3	194.5
1/4		9.7	195.1
cb		9.3	195.5
1/4		9.1	195.7
+3		8.7	196.1
+6		7.9	196.9
cb		7.9	196.9
E		7.5	197.3
	225' South		
E		11.3	193.5
cb		11.8	193.0
1/4		12.1	192.7
cb		12.3	192.5
1/4		12.8	192.0
cb		12.8	192.0
W		13.9	190.9
W+10		15.5	189.3
T.P.	1.53	194.17	12.16
			192.64
	256' South		
W-10		7.9	186.8
W		6.8	187.4
+5		5.7	188.5

T
194.17

cb	51	189.1
1/4	4.6	189.6
1/4	4.6	189.6
1/4	4.5	189.6
cb	4.3	189.9
+9	4.2	190.0
+8	5.4	188.8
E	5.5	188.7
E+10	5.4	188.8

269 South

E-10	12.0	182.2
E	11.6	182.6
+7	11.5	182.7
cb	10.3	183.9
1/4	8.1	186.1
1/4	7.8	186.4
1/4	7.5	186.7
cb	7.9	186.3
W	9.1	185.1
W+6	10.5	183.7
W+10	10.7	183.5
T.P.	0.03	181.55
12.65	181.52	

284 South

W-10	1.8	179.8
W	1.5	180.1
cb	1.6	180.0

181.55

284 South

16

1/4	1.2	180.4
1/4	2.1	179.5
1/4	2.2	179.4
cb	2.9	178.7
E	2.5	179.1
E+10	3.6	178.0

300 South N. line of Clark

E	9.4	172.2
cb	8.7	172.9
1/4	8.8	172.8
1/4	8.5	173.1
1/4	8.2	173.4
cb	8.0	173.6
W	8.1	173.5

Ncb

W	10.9	170.7
cb	10.9	170.7
1/4	11.4	170.2
1/4	11.7	169.9
1/4	11.9	169.7
cb	11.9	169.7
E	12.9	169.2

B.M. Pole NW

T.P.	0.20	168.67	13.08	168.47
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N 1/4

E	1.9	166.8
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16867

cb	1.8	166.9
1/4	1.6	167.1
2	1.5	167.2
1/4	1.4	167.3
cb	1.3	167.4
W	0.9	167.8
	2 Clark	
N	38	164.9
cb	40	164.7
1/4	3.9	164.8
2	3.5	165.2
1/4	3.8	164.9
cb	3.8	164.9
E	4.0	164.7
	S 1/4	
E	6.3	162.4
cb	5.6	163.1
1/4	5.6	163.1
2	5.6	163.1
1/4	5.9	162.8
cb	6.5	162.2
W	6.4	162.3
	s cb	
W	8.1	160.6
cb	7.9	160.8
1/4	7.9	160.8

16867

47

2	7.9	160.8
1/4	7.8	160.9
cb	8.2	160.5
E	8.8	159.9
	S. Line of Clark	
E	12.7	156.0
cb	11.7	157.0
1/4	11.3	157.4
2	11.1	157.6
1/4	10.9	157.8
cb	11.1	157.6
W	11.1	157.6
	T.P. 0.89	156.65 12.91
		155.76
		25' South of the S. Line of Clark
W-10	7.6	149.1
W	7.1	149.6
cb	7.1	149.6
1/4	7.4	149.3
2	8.0	148.7
1/4	8.5	148.2
cb	8.7	148.0
E	8.6	148.1
	E+10	8.5
		148.2
		90' South
E-10	10.2	144.5
E	11.7	145.0

156.65

cb		12.4	144.3
1/4		12.9	143.8
1/2		13.2	143.5
1/4		12.7	144.0
cb		12.7	144.0
W		13.2	143.5
W+10		13.4	143.3
T.P.	0.11	144.10	12.66 143.99
50' South			
W-10		2.4	141.7
W		2.9	141.2
cb		3.2	140.9
1/4		3.3	140.8
1/2		3.2	140.9
1/4		3.1	141.0
cb		2.8	141.3
E		2.8	141.3
E+10		3.9	141.7
75' South			
E-10		11.5	132.6
E		11.1	133.0
cb		11.4	132.7
1/4		11.0	133.1
1/2		10.6	133.5
1/4		10.2	133.9
cb		10.0	134.1

194.10

48

W		9.8	134.3
W+10		10.0	134.1
T.P.	0.22	131.55	12.77 131.33
100' South			
W		9.0	122.6
cb		4.1	127.5
1/4		4.1	127.5
1/2		4.1	127.5
1/4		4.0	127.6
cb		4.0	127.6
E		3.6	128.8
E+10		3.8	127.8
120' South			
E-10		8.7	122.9
E		8.7	122.9
cb		8.3	123.3
1/4		8.1	123.5
1/2		8.1	123.5
1/4		8.4	123.2
cb		8.6	123.0
W		8.3	123.3
125' South			
W		9.3	122.3
cb		9.5	122.1
1/4		9.1	122.5
1/2		9.6	122.0

T
131.55

1/4		10.0	121.6
cb		10.1	121.5
E		10.4	121.2
E+10		10.0	121.6
T.P.	0.62	119.49	12.68 118.87

150' South

E-10		5.6	113.9
E		6.5	113.0
cb		7.3	112.2
1/4		7.4	112.1
1/2		7.4	112.1
1/4		6.5	113.0
cb		6.3	113.2
W		5.1	114.4

175' South

W		12.0	107.5
cb		13.0	106.5
1/4		13.3	106.2
1/2		13.2	106.3
1/4		12.8	106.7
cb		12.5	107.0
E		12.6	106.9
E+10		12.6	106.9
T.P.	0.97	107.96	12.50 106.99

193' South

E		3.4	104.6
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T
107.96

49

cb		4.6	103.4
1/4		4.6	103.4
1/2		5.2	102.8
1/4		5.7	102.3
cb		4.9	103.1
W		4.5	103.5

210' South

W		8.6	99.4
cb		10.1	97.9
1/4		9.6	98.4
1/2		8.8	99.2
1/4		8.0	100.0
cb		7.0	101.0
E		5.4	102.6

225' South

E		7.8	100.2
cb		8.3	99.7
1/4		9.5	98.5
1/2		9.7	98.3
1/4		11.8	96.2
1/2		12.0	96.0
1/4		12.7	95.3
cb		12.9	95.1
W		12.8	95.2
W+10		13.0	95.0

107.96

230' South

W-10	13.5	94.5
W	13.4	94.6
cb	13.0	95.0
1/4	12.2	95.8
1/2	12.2	95.8
1/4	12.5	95.5
1/2	9.7	98.3
cb	9.2	98.8
E	8.0	100.0

232' South

E	8.0	100.0
cb	9.5	98.5
+4	12.0	96.0
1/4	12.3	95.7
1/2	10.7	97.3
1/4	10.9	97.1
cb	10.7	97.3
W	11.3	96.7
+10	12.3	95.7
+15	13.8	94.2

250' South

W-20	10.6	97.4
W-10	10.0	98.0
W	9.1	98.9
cb	8.3	99.7
1/4	7.2	100.8
E	7.0	101.0

T
107.96107.96
15.79
092.17

50

1/2	6.5	101.5
cb	7.7	100.3
+1	7.7	100.3
+2	10.6	97.4
+8	10.8	97.2
E	9.7	98.3
E+10	7.7	100.3

266' South

E-25	8.4	98.6
E	9.6	98.4
1/2	5.1	102.9
+5	1.9	106.1
cb	1.2	106.8
1/4	0.9	107.1
1/2	1.9	107.6

T.P. 10.82 118.50 0.28 107.68

2+45⁵ Mt. dx 1/4
Redon/lowline
15.795

1/4	13.6	104.9
cb	15.2	103.3
W	17.3	101.2
W+25	20.1	98.4

275' South

W-25	17.7	100.8
W	15.0	103.5
cb	12.5	106.0
1/4	9.2	109.3
1/2	7.3	111.2

X
118.50

1/4	6.8	111.7
cb	8.0	110.5
18	9.3	109.2
E	13.7	104.8
E+7	14.1	104.4
E+8	19.2	99.3
E+25	19.0	99.5
280' South		
E-25	12.2	106.3
E-1	10.0	108.5
E	7.0	111.5
cb	6.3	112.2
1/4	5.6	112.9
♀	6.4	112.1
1/4	8.3	110.2
cb	10.6	107.9
W	13.0	105.5
W+25	16.6	101.9
300' South		
W-25	7.9	110.6
W	4.3	114.2
cb	2.1	116.4
1/4	0.9	117.6
♀	0.2	118.3
T.P.	11.96	130.96
1/4	10.6	119.9

X
130.96

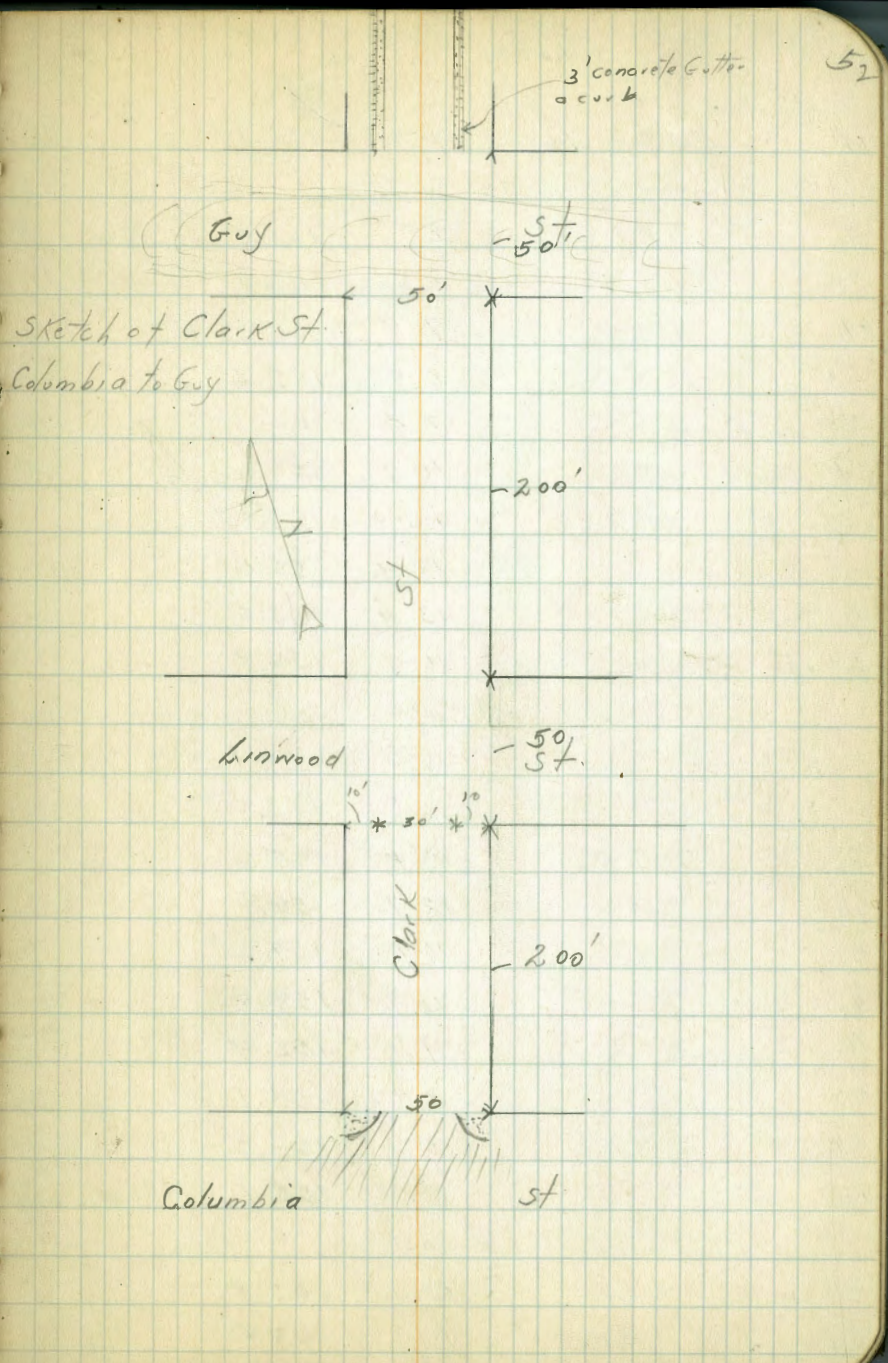
51

cb	9.7	120.8
E	9.3	121.2
E+10	9.7	120.8
E+20	9.5	121.0
T.P.	12.69	142.97
T.P.	12.97	155.94
T.P.	12.84	168.78
T.P.	3.64	172.40
B.M. SPIRE in Pole N.Y. CL. X.	0.76	171.64

Bliss
Isbell
Morgan
11/1/28

X Sections of Clark St Middletown Addition
from the East Line of Columbia to the E Line
of Guy

	+	π	-	Elev
B.M. SPIKE in Pole NW Clark & Isbell	0.76	172.90		171.64
T.P.	0.69	160.79	12.30	160.10
		etc = E Line of Columbia		
N on Paving		7.8		153.0
N.cb		8.88		151.91
Gutter 1/4		9.58		151.21
1/4		9.52		151.27
1/4		9.60		151.19
1/4		9.89		150.90
Gutter		10.28		150.51
S Top cb		9.83		150.96
S		9.5		151.3
S+10		8.9		151.9
		04' East of the E Line of Columbia		
S-15		8.1		152.7
S-11		7.9		152.9
S		5.1		155.7
cb		4.4		156.4
1/4		4.0		156.8
+5		3.3		157.5
1/4		3.0		157.8
+5		2.4		158.4
1/4		1.5		159.3
cb		0.9		159.9
N		1.2		159.6



160.79

TP	11.57	169.96	2.90	157.89
		08' East		
N			8.7	160.8
+2			8.5	161.0
cb			7.9	161.6
+5			6.9	162.6
1/4			7.4	162.1
¢			10.9	158.6
1/4			12.9	157.1
cb			12.9	156.6
S			13.9	155.6
S+15			16.7	152.8
		17' East		
S-15			16.9	153.1
S-9			16.1	153.4
S			13.9	155.6
cb			12.7	156.8
1/4			11.9	157.6
¢			10.7	158.8
1/4			7.1	162.4
+5			5.9	164.1
cb			5.7	163.2
N			6.9	162.6
		25' East		
N			6.0	163.5
cb			6.1	163.4

169.96

53

1/4		7.1	162.4
+3		8.9	160.6
¢		10.4	159.1
1/4		11.6	157.9
cb		12.2	157.3
+4		12.2	157.3
S		13.9	155.6
S+7		16.1	153.4
S+15		16.3	153.2
		35' East	
S-15		16.7	152.8
S-9		16.9	153.1
S		13.8	155.7
cb		11.6	157.9
1/4		10.7	158.8
¢		9.5	160.0
+5		8.6	160.9
1/4		8.0	161.5
cb		6.2	163.3
N		4.7	164.8
		50' East	
N		2.3	167.2
cb		3.9	165.6
1/4		6.6	162.9
¢		8.1	161.4
1/4		9.5	160.0

169.96

cb	10.7	158.8
S.	13.3	156.2
S+2.	14.3	155.2
S+2v	16.9	152.6
	75' East	
S-25	21.2	148.3
S-17	17.3	152.2
S.	12.8	156.7
cb.	9.0	160.5
1/4	7.6	161.9
¢	5.0	164.5
1/4	4.0	165.5
cb	2.7	166.8
+5	1.4	168.1
N.	0.7	168.8
T.P.	6.88	172.09
	9.25	165.21
	100' East	
N	2.1	170.0
cb	3.1	169.0
1/4	5.1	167.0
¢	6.5	165.6
1/4	9.2	162.9
cb	11.5	160.6
S.	16.0	156.1
S+25	24.2	147.9

172.09
125' East

54

S-25	24.3	147.8
S	15.8	156.3
cb.	11.9	160.2
1/4	9.9	162.2
¢	7.8	164.3
1/4	9.8	167.3
cb	2.9	169.7
N.	0.8	171.3
T.P.	3.55	175.00
	0.64	171.95
	150' East	
N	2.3	172.7
+8	3.3	171.7
cb	4.4	170.6
1/4	7.2	167.8
¢	9.6	165.4
1/4	14.6	160.4
S	18.3	156.7
S+25	26.4	148.6
	175' East	
S-23	26.3	148.7
S	18.1	156.9
cb	14.1	160.9
1/4	11.5	163.5
¢	9.3	165.7
1/4	7.1	167.9
cb	4.9	170.1

X
175.00

N 1.6 173.4

200' East W Line of Linwood

This section taken in the X section of Linwood.

0+00 = E line of Linwood taken in the X section of Linwood

25' East of the E line of Linwood

N 9.2 170.8

cb 6.8 168.2

1/4 9.1 165.9

ϕ 11.5 163.5

+5 12.5 162.5

1/4 13.8 161.2

cb 16.8 158.2

S 20.6 154.4

S+25 29.0 146.0

S+35 31.2 143.8

50' East

S-35 32.5 142.5

S 25.1 149.9

cb 21.0 154.0

1/4 17.1 157.9

ϕ 14.1 160.9

1/4 10.9 164.1

cb 8.6 166.4

N 6.0 169.0

65' East

N 8.2 166.8

X
175.00

55

cb 10.7 164.3

1/4 12.7 162.3

TP 5.05 167.10 12.95 162.05

ϕ 7.5 159.6

1/4 9.7 156.4

cb 12.4 154.7

S 15.8 151.3

S+35 29.0 143.1

25' East

S-35 25.5 141.6

S-25 23.8 143.3

S 17.0 150.1

cb 13.2 153.9

1/4 10.5 156.6

ϕ 8.2 158.9

1/4 6.1 161.0

cb 3.4 163.7

N 1.5 165.6

100' North

N 4.6 162.5

cb 7.3 159.8

1/4 9.0 158.1

ϕ 11.3 155.8

1/4 13.7 153.4

cb 15.3 151.8

S 19.3 147.8

π
16710

1 S+13	23.0	144.1
S+25	25.0	142.1
	112' East	
S-25	25.1	142.0
S	20.6	146.5
1 cb	18.0	149.1
1/4	14.9	152.2
⊕	12.3	154.8
1/4	10.1	157.0
+ cb	8.4	158.7
1 N	6.6	160.5
	125'	
S N	8.0	159.1
S cb	10.2	156.9
S 1/4	12.7	154.4
⊕	15.4	151.7
1/4	17.5	149.6
cb	18.2	148.9
S	21.0	146.1
S-25	26.1	141.0
	132' East	
S-35	28.2	138.9
S	21.1	146.0
1 cb	19.0	148.1
1/4	17.3	149.8
⊕	15.8	151.3

π
16710

56

1/4	13.9	153.2
cb	11.7	155.4
N	8.8	158.3
TP 0.38	156.11	11.37
	150' East	
N	0.3	155.8
cb	3.5	152.6
1/4	5.7	150.4
⊕	7.4	148.7
1/4	9.6	146.5
cb	11.5	144.6
S	14.2	141.9
S+10	16.6	139.5
S+20	18.7	137.4
S+35	22.6	133.5
	167' East	
S-35	25.2	130.9
S-10	15.2	140.9
S	19.8	136.3
cb	16.9	139.2
1/4	13.7	142.4
⊕	11.5	144.6
1/4	9.1	147.0
cb	6.7	149.4
N	3.7	152.4

15611

175' East

N	5.8	150.3
cb	8.5	147.6
1/4	10.6	145.5
1/2	12.9	143.2
3/4	14.6	141.5
cb	18.2	137.9
S	19.8	136.3
S+10	18.0	138.1
S+35	25.6	130.5

180' E

S-35	27.8	128.3
S-10	27.2	128.9
S	24.1	132.0
+6	23.8	132.3
+8	18.6	137.5
cb	18.3	137.8
1/4	16.3	139.8
1/2	13.8	142.3
3/4	11.5	144.6
cb	10.0	146.1
N	7.2	148.9

185' East

N	8.5	147.6
cb	11.3	144.8
1/4	13.4	142.7
1/2	14.2	141.9

15611

57

1/4	16.6	139.5
cb	18.4	137.7
+4	19.3	136.8
+5	23.4	132.7
S	24.5	131.6
S+5	25.2	130.9
S+15	16.1	140.0
S+30	18.0	138.1

193' East

S-30	15.6	140.5
S-15	14.1	142.0
S-10	14.2	141.9
S-5	18.0	138.1
S	19.5	136.6
S+6	21.7	134.4
cb	21.8	134.3
+5	21.0	135.1
1/4	19.5	136.6
1/2	18.4	137.7
3/4	17.3	138.8
cb	19.0	142.1
N	10.7	145.4
N+10	8.4	147.7
N+20	5.4	150.7

200' East W Line of Guy

N-20	7.9	148.2
------	-----	-------

50' st
10' cb
7.5 9.5

π
156.11

N-10	10.8	145.3
N	13.9	142.2
+5	15.8	140.3
cb	17.3	138.8
1/4	17.4	138.7
¢	18.0	138.1
1/4	19.0	137.1
cb	19.2	136.9
+8	17.5	138.6
S	15.1	141.0
S+10	10.7	145.4
S+25	11.6	144.5
	Wcb	
S-25	5.4	150.7
S-10	5.5	150.6
S	10.0	146.1
+1	11.3	144.8
+7	11.0	145.1
+8	13.8	142.3
cb	13.9	142.2
+5	14.4	141.7
+6	13.1	143.0
1/4	13.1	143.0
¢	12.2	143.9
1/4	13.2	142.9
cb	15.0	141.1

π
156.11

58

N	16.4	139.7
N+10	13.2	142.9
N+20	10.6	145.5
	W 1/4	
N-25	11.9	144.2
N-10	14.2	141.9
N	19.0	142.1
cb	11.2	144.9
1/4	8.2	147.9
¢	6.6	149.5
+5	6.4	149.7
1/4	8.6	147.5
+3	8.8	147.3
+3.5	11.4	144.7
+7.5	12.1	144.0
cb	6.9	149.2
+2	6.9	149.2
+5	8.3	147.8
+7	5.2	150.9
S	9.5	151.6
S+25	5.3	150.8
	¢	
S-25	4.6	151.5
S	9.1	152.0
+7	4.6	151.5
+8	6.6	149.5

156.11

cb	6.3	149.8
+6	7.9	148.2
+7	4.7	151.4
1/4	4.7	151.4
¢	4.5	151.6
1/2	4.7	151.4
+3	5.5	150.6
cb	7.4	148.7
N	10.0	146.1
N+10	12.6	143.5
N+17	12.4	143.7
N+30	13.8	142.3
	E 1/4	
N-15	7.0	149.1
N	9.9	151.2
cb	3.8	152.3
1/4	3.0	153.1
¢	3.6	152.5
1/4	4.3	151.8
cb	3.9	152.2
S	3.7	152.4
S+10	3.4	152.7
	E cb	
S-10	3.2	152.9
S	3.2	152.9
cb	3.4	152.7

156.11

59

1/4	2.9	153.2		
¢	3.1	153.0		
1/4	2.7	153.4		
+6	1.7	154.4		
cb	1.7	154.4		
N	1.8	154.3		
N+15	2.5	153.6		
	E line of Gully			
N	0.2	155.9		
+3	1.0	155.1		
Top cb	1.71	154.40		
Gutter	2.38	153.73		
+3 edge of concrete gutter	2.32	153.79		
1/4	2.0	154.1		
¢	2.1	154.0		
1/4	2.6	153.5		
+4.5 edge of concrete gutter	3.27	152.84		
Gutter	3.32	152.79		
Top cb	3.11	153.00		
S	2.4	153.7		
TP	12.93	168.54	0.50	155.61
TP	12.79	181.32	0.01	168.53
TP	12.85	199.17	0.00	181.32
TP	12.26	206.36	0.07	199.10
TP	13.08	219.44	0.00	206.36
			0.57	218.87

B.M. NE 8P
 Nome da Terra
 Henry

B.M. 2890
 218.87
 .03

50' wide
10' ebs
7.5' 11.5'
3.0' emt gutter on
Both sides

X See Puterbaugh
Henry to Clark

3-5-28
mills

219.25

8 ps
10.6
9'

60

B.M. 0.35 219.25 218.90

N.W. Henry
& Puterbaugh

W. edge emt. gutter 6.25

00 = S. Line Henry produced from west

E " " " 4.37

W. emt. el. 1.57 217.68

E. emt. el. 5.57 213.68

emt gutter 2.09

130' S

1/4 1.53

on pavmt.

E. emt. el. 7.14 212.11

c 1.25

E. edge. emt gutter 7.94

1/4 1.19

W " " " 7.80

emt. gutter. gutter 1.28

1/4 7.8

E. emt. el. 0.53 218.72

c 7.9

50' S

1/4 8.3

E. emt. el. 3.01 216.24

E. edge emt gutter 8.48

gutter 3.82

W " " " 8.66

1/3 = Edge emt gutter 3.69

W. emt. el. 8.12 211.13

1/4 3.5

150' S

c 3.7

W. emt. el. 9.55 209.7

1/4 4.1

W. edge emt gutter 10.05

E. edge emt gutter 4.45

E " " " 9.87

W " " " 4.70

1/4 9.6

W emt. el. 4.18 215.07

c 9.3

100' S

1/4 9.3

W emt. el. 6.69 212.63

W. edge emt gutter 9.24

gutter 7.23

E. " " " 9.36

1/3 = E. edge emt gutter 6.97

E. emt. el. 8.56 210.69

1/4 6.7

c 6.2

1/4 6.1

219.25

170's

E. emb. ch.	10.45	208.8
E. emb. gutter	11.27	
W. " "	11.15	
" "	11.2	
C	11.3	
" "	11.6	
E. emb. gutter	11.81	
W. " "	11.97	
W. emb. ch.	11.45	207.8
T.P.	0.93	208.16
	12.02	207.23

190's

W. emb. ch.	2.91	205.25
W. " gutter	3.43	
E. " "	3.23	
" "	3.0	
C	2.5	
" "	2.7	
W. edge emb. gutter	2.51	
E. " "	2.64	
E. " ch.	1.85	206.31
+ 1.5	2.6	
+ 2.5 = W. edge walk	1.86	

210's

W. edge emb. walk	4.88	
O.I.W.	5.7	
1.7 W. dirt back of curb	6.3	Back of curb

208.16

Puterbaugh

61

E. emb. ch.	4.92	203.24
E. " gutter	5.72	
W. " "	5.63	
" "	5.5	
C	5.6	
" "	5.9	
E. edge emb. gutter	6.43	
W. " "	6.65	
W. emb. ch.	6.07	202.09

From 210's to 250's E. ch. is undermined and broken away
from emb. gutter. W. edge emb. walk also undermined or to be

230's

m. ch.	9.46	198.7
W. gutter	10.06	
E. edge "	9.81	
" "	9.1	
C	9.0	
" "	9.0	
W. edge gutter	8.98	
E. " "	9.07	
E. emb. ch.	8.43	199.73
dirt under ch.	9.9	
" " W. edge walk	8.9	
W. edge walk	8.25	

208.16
250.5

w. edge ent walk	11.61	
dirt under walk	13.2	
" " cl.	13.2	
E. ent cl.	11.65	196.51
E. edge gutter	12.45	
W " "	12.34	
" "	12.3	
E	12.4	
" "	12.8	
E. edge gutter	13.15	
W " "	13.38	
W. ent cl.	12.83	195.33
T.P.	0.61	195.88
		12.89
		195.27
	265.5	
W. ent. cl.	3.12	192.76
W. edge gutter	3.66	
E " "	3.46	
" "	3.1	
E	2.7	
" "	2.6	
W. edge gutter	2.58	
E. " "	2.69	
E. ent cl.	1.88	194.00
dirt back of cl.	2.6	
" under walk	3.8	
walk	1.84	

walk undermined
1.4 at this point.195.88
290.5

W. edge walk	6.09	
dirt under walk	7.2	walk undermined 0.6 here
dirt back of cl.	6.8	
E. ent cl.	6.12	189.76
E. edge gutter	6.90	
W " "	6.77	
" "	6.8	
E	6.9	
" "	7.3	
E. edge gutter	7.67	
W " "	7.88	
W. ent. cl.	7.33	188.55
	300.3 = N. Line	Clark
W. ent. cl.	9.02	186.86
gutter	9.58	186.3
E. edge gutter	9.37	
" "	8.5	
E	8.0	
" "	8.0	
W. edge gutter	8.41	
gutter	8.52	
E. ent cl.	7.86	188.02

50' wide
10' els
7.5' 1/4s
3.0 cm gutter on
N. 4 S.

Clark St X See
Torrence To Guy
19588

3-5-28
Muller

198.67

63

T.P.	11.90	198.67	9.11	186.77
	00 = W. Line Torrence on S.			
	00 on S + 11.3 W. on N. = End improved St			
S. ent. el			2.45	196.22
gutter			2.99	
W. edge gutter			2.78	
" "			2.5	
C			2.7	
" "			1.9	
S. edge gutter			2.27	
gutter			2.35	
N. ent. el			1.51	197.16
	11.3 W. on N. + S.			
N. el			1.51	197.16
gutter			2.35	
S. side gutter			2.27	
" "			2.0	
C			2.4	
" "			3.0	
N. edge gutter			3.37	
S " "			3.55	
3. ent. el			3.01	195.66
	60' W.			
S. ent. el			5.32	193.35
S. Edge gutter			5.86	
N " "			5.71	

" "	5.4
C	4.7
" "	4.4
S. edge gutter	4.57
N. " "	4.67
N. el	3.90
	65' W.
S. edge walk	4.08
dirt under walk	4.7
" back of el	4.7
N. el	4.12
N. edge ent. gutter	4.91
S " " "	4.80
el + 3' dirt at edge of gutter	5.5
el + 5	4.8
" "	4.6
C	4.9
" "	4.5
N. edge ent. gutter	5.92
S " " "	6.08
S. ent. el	5.53
	100' W.
S. el	7.24
S. edge gutter	7.79
N. " "	7.61
" "	7.3

194.77

Walk undermined
1.0 Here

194.55

193.14

191.43

198.67
100' W. (con)

c	6.6	
"	6.4	
+ 2.5	6.5	
+ 4.5 dirt at edge of gutter	7.1	
s. edge emb gutter	6.51	
N " " "	6.61	
N. emb	5.79	191.88
dirt back of d	6.2	
" at edge of walk	6.2	
s. edge of walk	5.72	
	125' W	
s. edge walk	6.95	
dirt under walk	7.8	
" back of d.	7.8	
N. emb d	7.00	191.67
N. edge gutter	7.80	
s " "	7.70	
dirt at d + 3	8.3	
"	7.7	
c	7.9	
"	8.4	
N. edge gutter	8.80	
s " "	8.96	
s. emb d	8.40	190.27

walk undermined
1.0

walk undermined
2.0

Clark St.

198.67
150' W

s. emb d	9.56	189.11
s. edge gutter	10.13	
N " " "	9.97	
"	9.7	
c	9.0	
"	8.8	
+ 4.5 dirt at edge of gutter	9.4	
s. edge of gutter	8.94	
" " " "	9.05	
N. emb d	8.24	190.43
dirt back of d	9.2	
dirt at edge of walk	9.2	
s. edge walk	8.18	
	200' W = E. line Peterbaugh	
N. emb d	10.69	187.98
N. edge gutter	11.47	
s " " "	11.39	
" " " dirt	11.7	
"	11.3	
c	11.3	
"	11.9	
N. edge gutter	12.23	
s " "	12.43	
s. emb d	11.92	186.75

68

198.67
E. ch. Line Paterbaugh

S. on ent. ch return.	12.13	186.54
S. gutter	12.69	
ch	12.4	
"	12.0	
c	11.8	
"	11.8	
ch	11.7	
N. on ent. ch return	10.64	188.03
N. " " gutter	11.30	
	E. 14	
N	10.7	187.27
ch	11.4	187.27
"	11.9	
c	12.4	
"	12.3	
ch	12.3	186.37
S	12.6	
	⊕	
S	13.0	
ch	12.8	185.87
"	12.6	
c	12.1	
"	11.7	
ch	11.4	187.27
N.	10.8	

198.67
W. 14

Clark St

65

N	11.3	187.71
ch	11.8	186.87
"	12.0	
c	12.4	
"	12.7	
ch	13.2	185.47
S	13.2	
T.P. 1.12	186.85	12.94
		185.73
	W. ch	
S. on ent. ch return	1.82	185.03
S. " " gutter	2.41	
ch	1.7	185.15
"	1.3	
c	0.8	
"	0.5	
ch	0.5	186.35
N. ent. ch ret	0.02	186.83
N. " gutter	0.56	
	00 = W. Line Paterbaugh	
N. ent. ch	0.33	186.52
N. edge gutter	1.17	
S. " "	1.05	
"	1.3	
c	1.6	
"	2.0	
N. edge gutter	2.24	

186.85

00-W. Line of Puterbaugh (cont)

S. edge gutter	2.45	
S. emb. ch	1.90	184.95
dirt back of ch	3.1	
" at edge of walks	2.3	
N. edge walk	1.83	

10' W.

N. edge walk	3.40	
dirt under walk	4.1	
" back of ch	4.0	
S. emb. ch	3.44	183.41
S. edge gutter	4.00	

N " "

3.77

1/4

3.3

e

2.8

1/4

2.7

S. edge gutter

2.63

N " "

2.75

N. emb. ch

1.96

184.89

20' W.

S. emb. ch

5.03

181.82

dirt under ch

6.5

" " walk

5.5

N. edge "

4.97

From 10' W To. 20' W. ch is undermined as in back

" 20' W. " 40' W. dirt back of ch. shows no wash
and ch. is ok. ch. might be undermined

walk undermined
0.3walk undermined
0.3walk undermined
0.3

186.85

40' W. Brkin curb

N. emb. ch	6.75	180.1
N. edge gutter	7.52	
S " "	7.45	
1/4	7.4	
e	7.6	
1/4	8.2	

N. edge gutter

8.62

S " "

8.81

S. emb. ch

8.25

178.6

T.P. 0.87 174.80 12.92 173.93

75' W.

N. edge walk

1.72

N. emb. ch. G.

2.2

172.6

S. edge gutter OK.

2.35

N " " O.K.

2.18

1/4

2.0

e

1.2

1/4

0.9

S. edge gutter

0.92

N " "

1.00

N. emb. ch

0.25

174.55

84 W. ch. ok. here west

N. emb. ch

1.70

173.1

N. edge gutter

2.50

S " "

2.40

1/4

2.3

5.80
7.70
213.50
6.75

66

174.80
84' W. (E.O.H)

C	2.4	
"	3.2	
N. edge gutter	3.57	
S " "	3.78	
S. emb. cl	2.28	172.52

100' W

S. emb. cl	5.77	169.03
gutter	6.30	
N. edge gutter	6.15	
"	5.8	
C	5.0	
"	4.7	
S. edge gutter	4.92	
N " "	5.00	
N. emb. cl	4.23	170.57

100' W. to 150' W. dirt washed out bet cl + walk on S. side.
out to 1'0 Deep Filled with emb blocks.

150' W.

N. emb. cl	12.26	162.54
gutter	13.03	
S. edge gutter	12.94	
"	12.8	
C	13.0	
"	13.8	
T.P.	0.65	162.78
		12.67
		162.19

162.78

Clark St.

67

N. edge gutter	2.15
S " "	2.32
S. emb. cl	1.78
dirt back of cl	2.8
N. edge walk dirt	2.7
" " "	1.74

161.10

190' W.

Nowash bet cl and walk Here

S. emb. cl	8.11
S. edge gutter	8.64
N " "	8.49
"	8.0
C	7.4
"	7.3
S. edge gutter	7.38
N " "	7.46
N. emb. cl	6.73

154.67

200' W = E. Line

N. emb. cl	8.32
N. edge gutter	9.09
S " "	8.92
"	8.5
C	8.8
"	9.3
N. edge gutter	10.07
S " "	10.22
S. emb. cl	9.71

156.05

154.46

153.07

Levels for Proposed Culvert
1' N. of S. lb. of Clark St. From E. line
of Guy St West

162.78

0+0 E. line Guy St		10.22	emt gutter	
0+4 " " "		9.4	dirt	
0+24		11.2		
T.P.	0.46	150.53	12.71	150.07
0+27		4.7		
0+40		9.9		
0+50		14.8		
0+55 Bottom of wash		15.5		

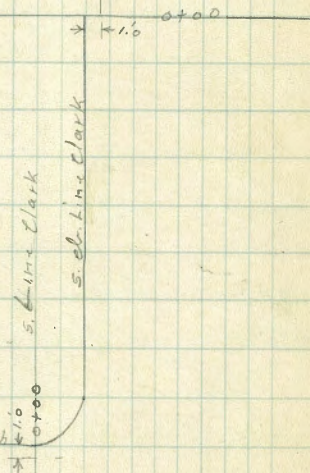
Levels for Proposed Drain

1' E. of wash. of Puterbaugh from S. line
of Clark St. South.

T.P. Page 63	0.29	187.06		186.77
0+0 S. line Clark St		2.5	emt gutter	
0+1 " " "		3.9	dirt fill	
0+10		7.3		
0+18		8.1		
0+30		2.5	on fill	
3' W. of 0+30		9.8		
0+43		2.6	on fill	
8' W. of 0+43		6.1	" "	
15' " " 0+43		13.8	" "	
0+90		13.7	on fill	
T.P.	1.14	175.40	12.80	174.26
1+15		11.6		
1+30		16.0		

E. line Guy St.

Proposed culvert



Alberta Place X Sec
Hawk to W. End.

B.M.	8.35	270.18	261.83	M.W. Bush + Hawk STs
00 - W. Line Hawk STs				
S. cl		4.38		
gutter		4.75		PAVMT
"y		4.47		
e		4.41		
ly		4.52		
gutter		4.79		
N. cl		4.44		

50' W. on N. at 90°

N. cl		3.77		
gutter		4.4		
cl		4.0		
gutter		4.4		
S. cl		3.93		
T.P.	7.86	274.77	3.27	266.91

100' W. on N

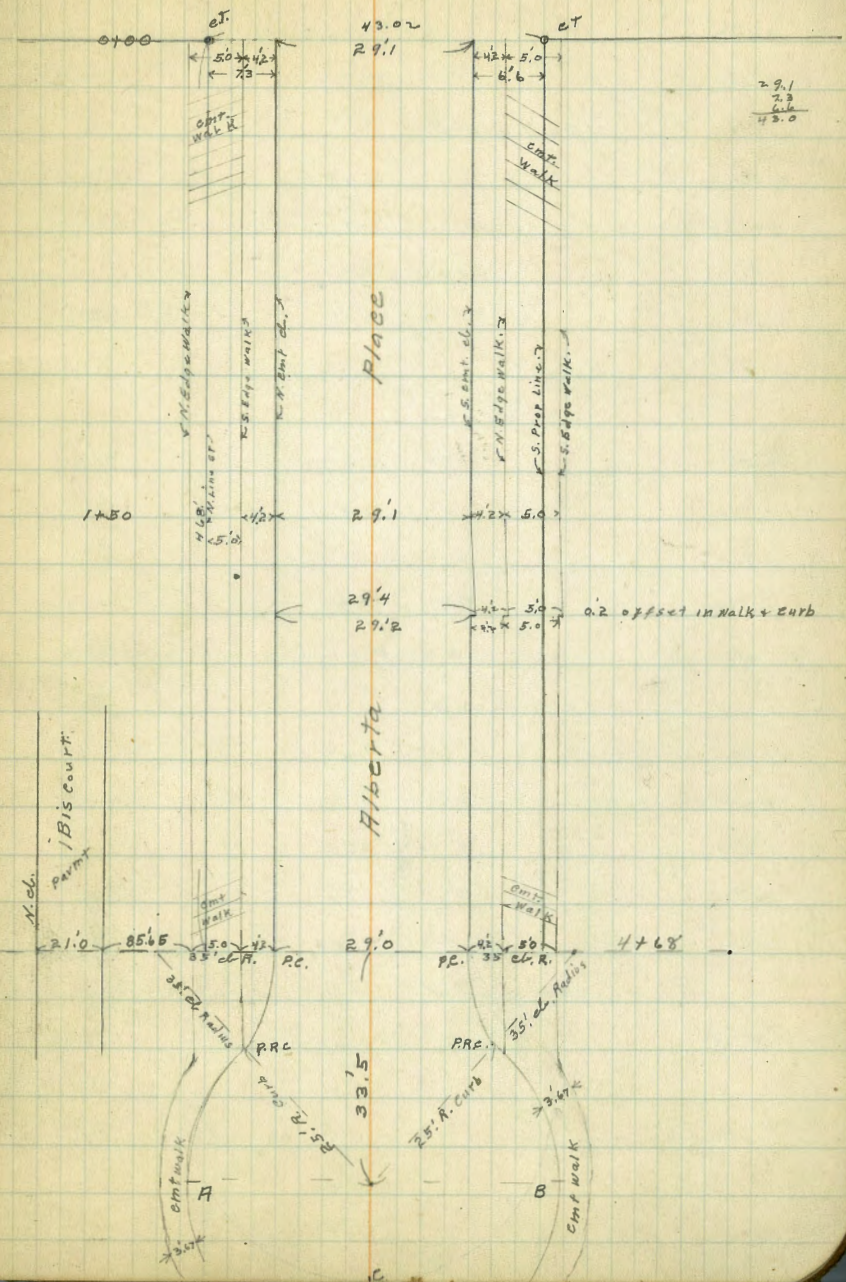
S. cl		7.83		
gutter		8.5		
cl		7.7		
gutter		8.4		
N. cl		7.83		

150' W. on N

N. cl		7.15		
gutter		7.4		
cl		7.0		

Hawk

57 69



274.77

150' W. on N. (con)

gutter	7.6
s. cl.	7.26
194.7 W. on N.	
s. cl.	6.43
gutter	6.9
⊕	6.3
gutter	6.7
N. cl.	6.06
250' W. on N.	
N. cl.	5.08
gutter	5.8
⊕	5.1
gutter	5.8
s. cl.	5.06
275' W. on N.	
s. cl.	4.67
gutter	5.3
⊕	5.0
gutter	5.6
N. cl.	4.84
300' W. on N.	
N. cl.	5.00
gutter	5.8
⊕	5.1
gutter	5.4
s. cl.	4.71

274.77

Alberta Place

.70

325' W. on N.

s. cl.	5.23
gutter	5.9
⊕	5.5
gutter	6.3
N. cl.	5.67
350' W. on N.	
N. cl.	6.69
gutter	7.3
⊕	6.5
gutter	6.8
s. cl.	6.14
375' W. on N.	
s. cl.	7.37
gutter	7.9
⊕	7.7
gutter	8.6
N. cl.	7.93
400' W. on N.	
N. cl.	9.17
gutter	9.9
⊕	8.9
gutter	9.4
s. cl.	8.69
T.P.	1.33 266.77 9.33 265.44

266.77

468' W. on N = P.C. Curb

S. cl	4.52
gutter	5.2
¢	4.7
gutter	5.7
N. cl.	4.72

P.R.C.

N. cl	5.43
gutter	6.2
Radius 25' to cl of Banjo	6.2
gutter	5.9
S. cl.	5.39
at 90° from ¢ at 25' Radius Curb	
S. cl at B	5.73
gutter	6.3
¢ at Radius Pt.	6.2
gutter	6.6
N. cl at A.	5.85

25' W. of Radius Pt. on curb

W. side Banjo at C. on curb	6.45	emt cl
gutter on C.B. grate 1.2 x 1.2	7.50	

12" Cor. Iron Pipe Culvert 43' long

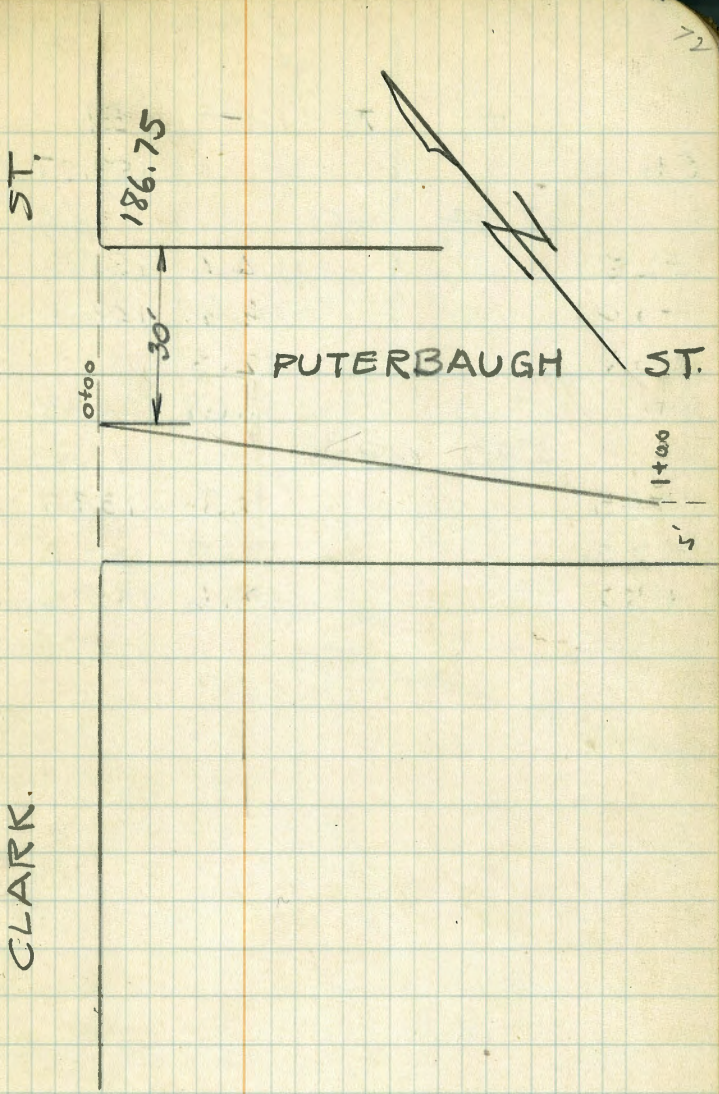
from this C.B. W. on ¢

Alberte Place

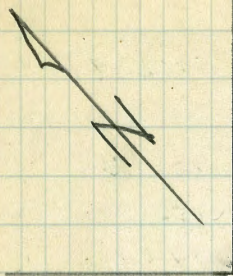
71

Sta.	+	π	-	Elev
SE Cb.	0.80	187.55		186.75
0+00			1.9	185.65
+08			2.7	184.85
+12			6.6	180.95
+16			2.0	185.55
+45			2.6	184.95
+60			7.2	180.35
TP=+77			12.19	175.36
	4.55	179.91		
+90			8.4	176.51
1+00			12.3	167.61

CLARK.

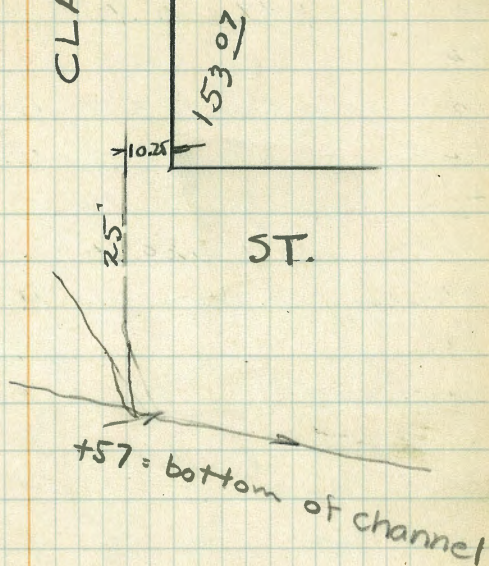


	+	∧	-	El.
Cb				153.07
	2.94	156.01		
+25			4.4	151.6
+29			9.9	146.1
+35			12.5	143.5
TP.			11.68	144.33
	4.87	149.20		
+45			9.5	139.7
+50			12.0	137.2
+57			13.6	135.6



GUY

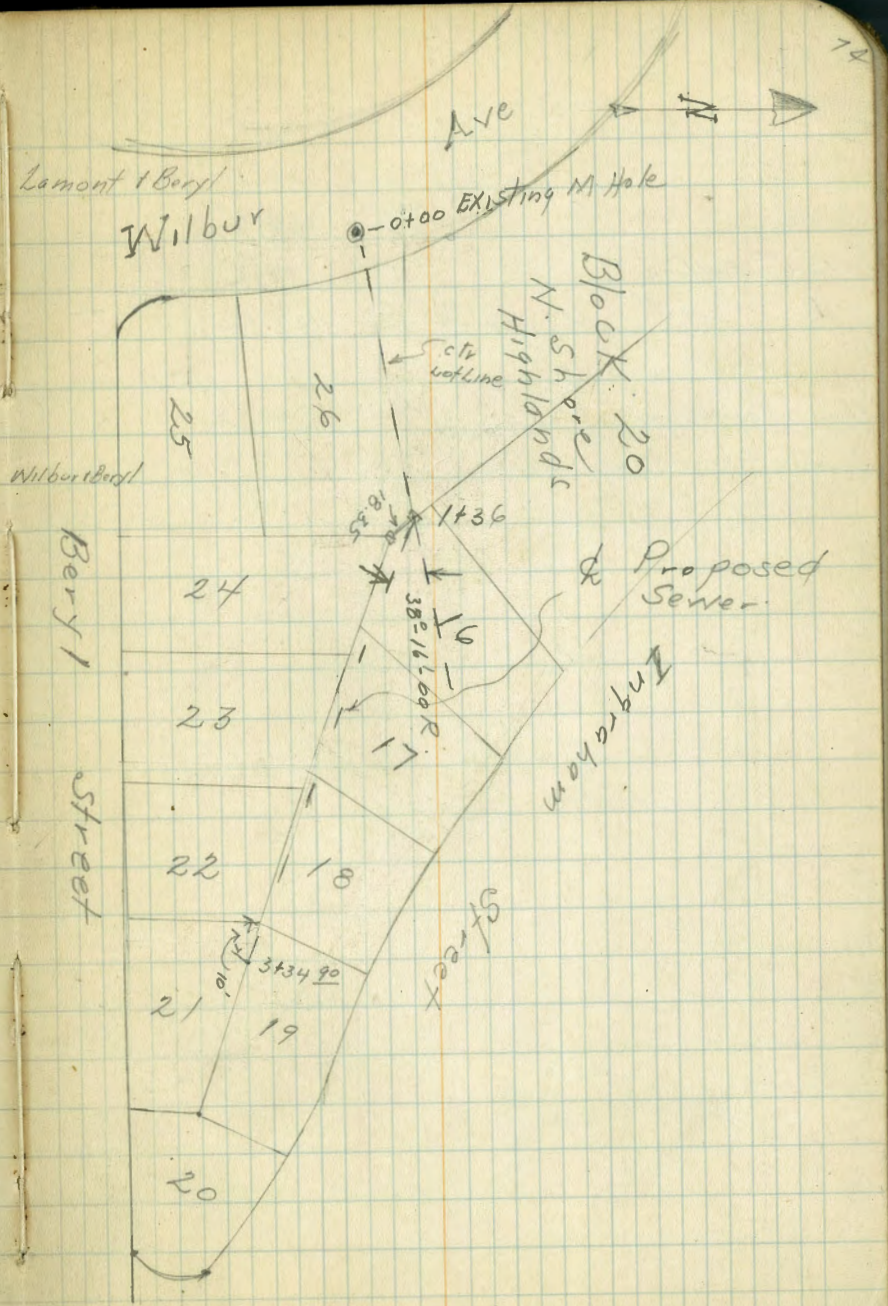
CLARK ST



78

Sewer Preliminary North Shore
Highlands. Block 20

B.M.	H ₁	H ₂	Elev	Notes
B.M.	6.92	169.01	162.09	N.E. 7 th TR
TP	9.47	176.76	172	167.29
TP	4.13	170.48	10.41	166.35
TP	0.38	157.77	13.09	157.39
TP	0.31	144.97	13.11	144.66
TP	0.12	131.99	13.10	131.87
Set B.M.	10.40	129.34	13.05	118.94 S.E. Top of Wilbur Blvd
Flow Line of Existing M.H.	16.44	112.90		
0+00		9.4	119.9	
0+05 ⁵ Gutter		9.66	119.68	
0+05 ⁵⁰ Top cb		8.91	120.43	
0+15 ³⁰ Prop Bottom		8.5	120.8	
0+26 Top		5.7	123.6	
0+35		5.6	123.7	
0+40		4.0	125.3	
0+50		3.7	125.6	
0+75		2.8	126.5	
1+00		1.3	128.0	
TP	9.62	138.58	0.38	128.96
1+36	Δ 38°-16'-00" R		8.0	130.6
1+50			7.5	131.1
+75			6.8	131.8
2+00			6.6	132.0
+25			5.2	133.4
+50			4.8	133.8



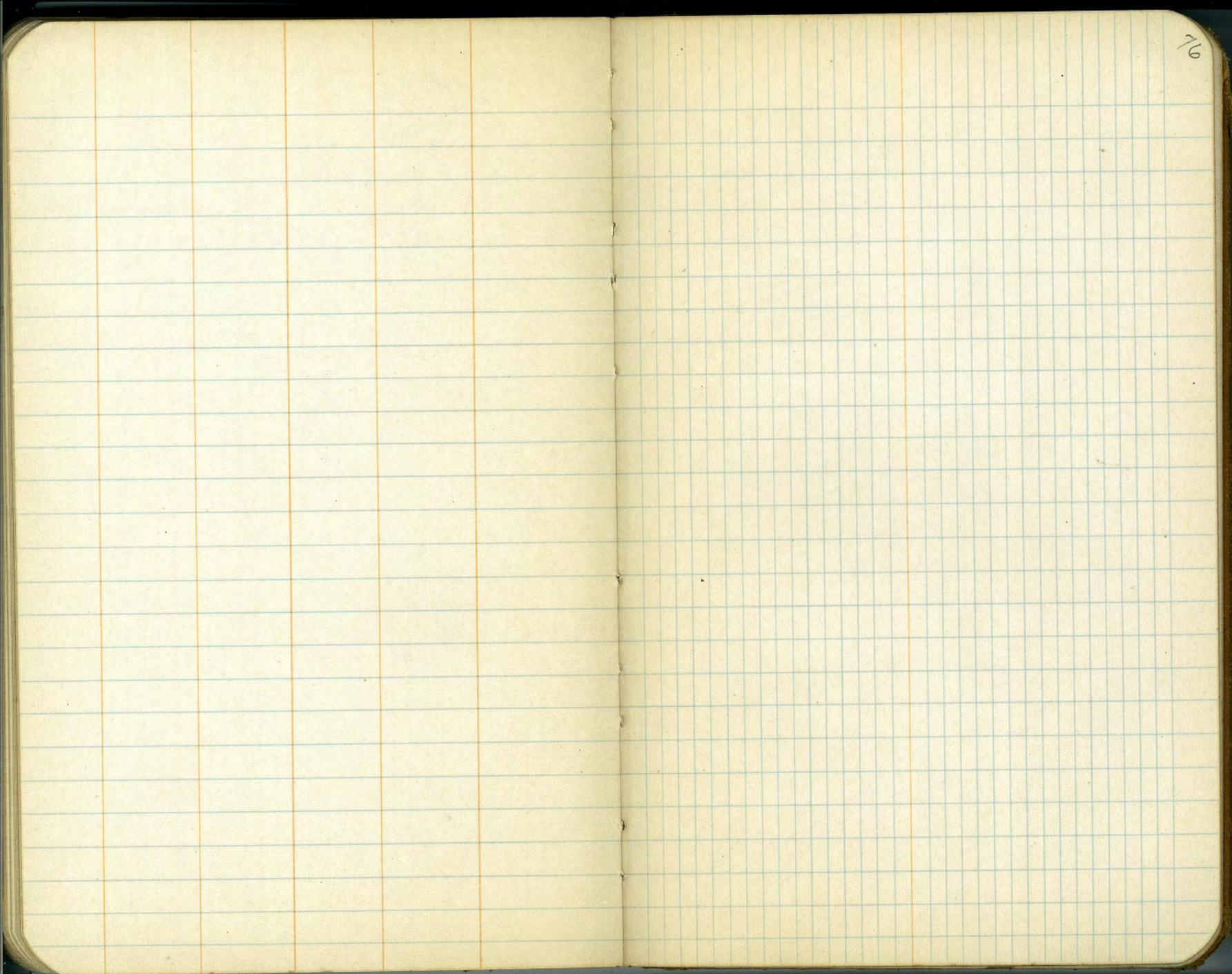
H.I.
138.58

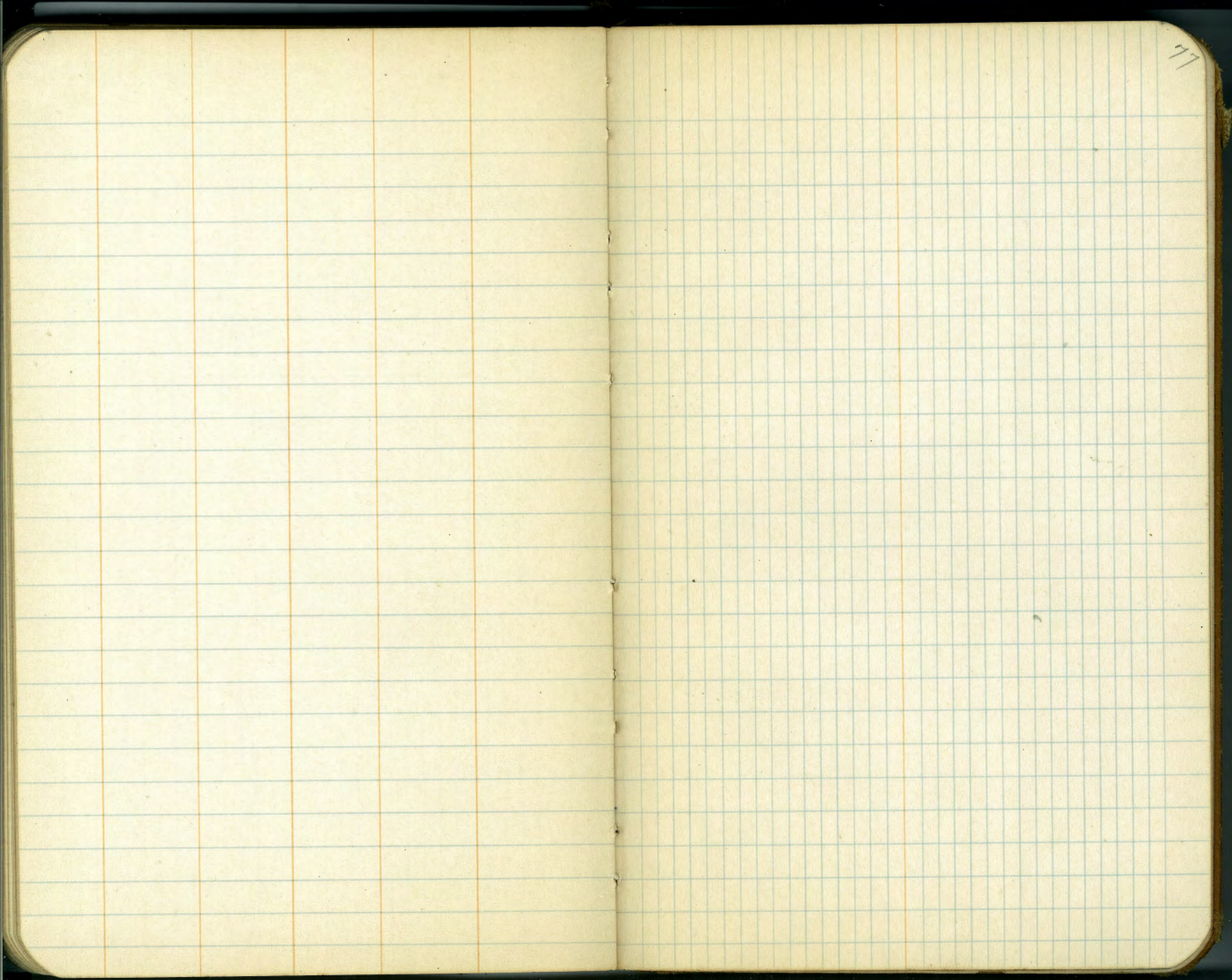
75

+75			4.5	134.1
3+00			4.0	134.6
134 ⁹⁰ End Line			4.5	134.1
T.P.	1.74	129.56	10.76	127.82

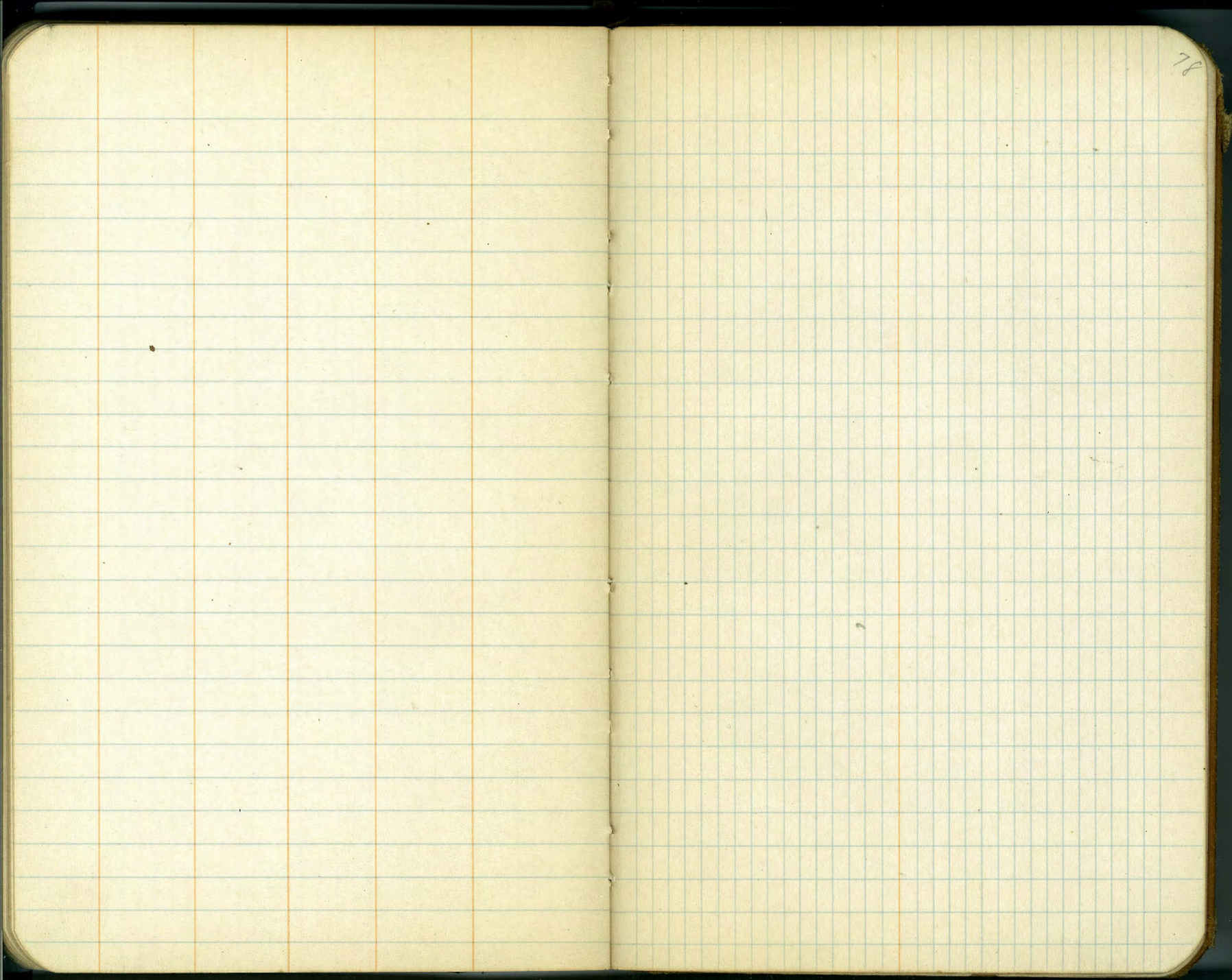
Check out on B.M. 3 miles in Pole
Side Side of Alley S of Berylon
Zagrebam. Set on P.B. Sewer Construction

			12.74	116.82
--	--	--	-------	--------





77

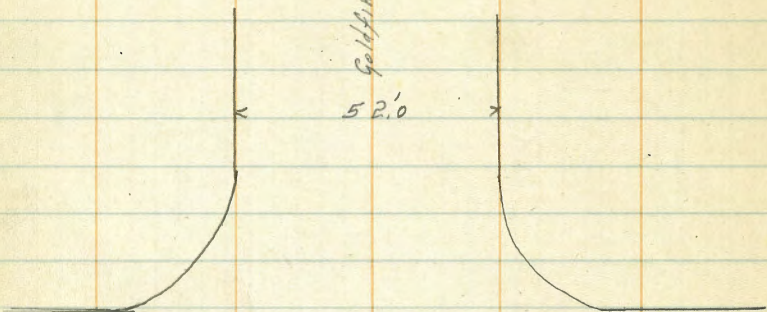


78

Re paving of Intersection of
Goldfinch + Sutter

Goldfinch St

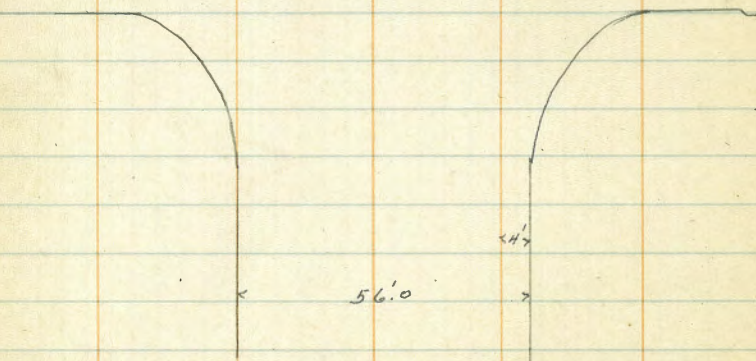
52.0



Sutter

56.0

47



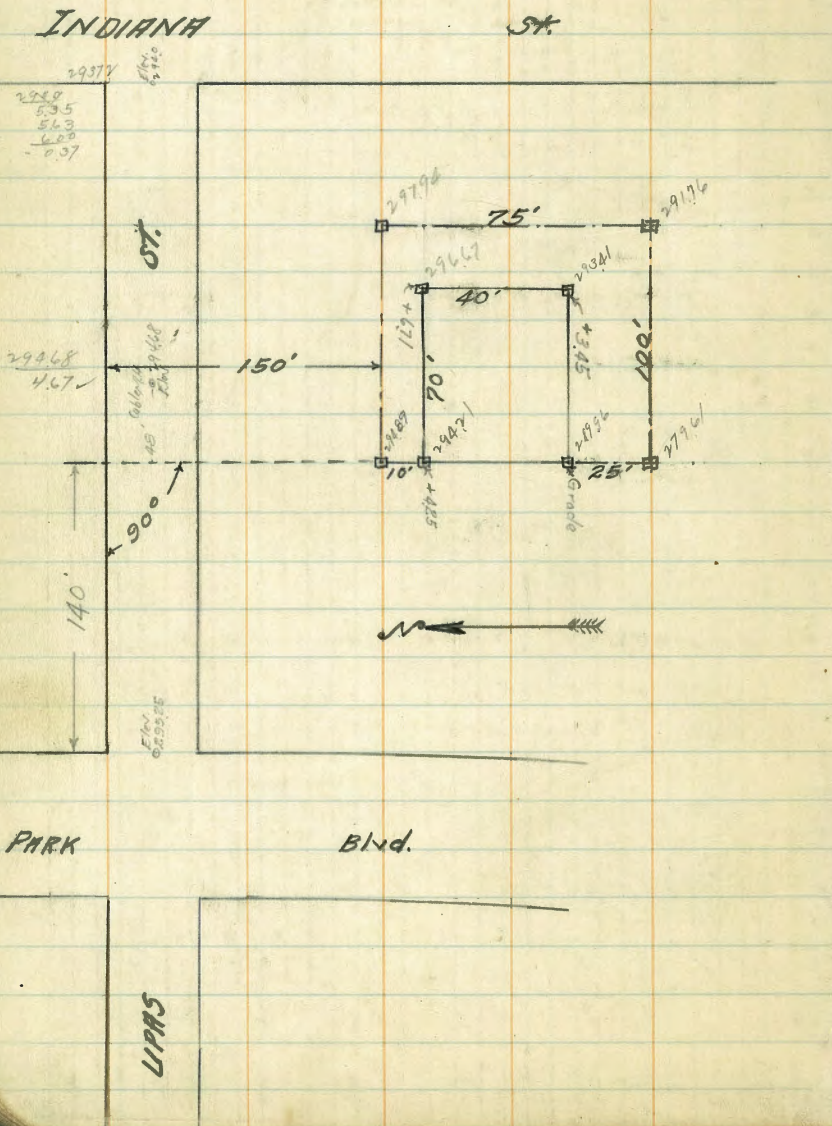
79

BM 254.99 N.E. Goldfinch + Sutter
2.61
259.60

Survey of Fire Alarm Station in Balboa Park

Walker
4-9-27

54.67
295.80
- 5.35
299.35



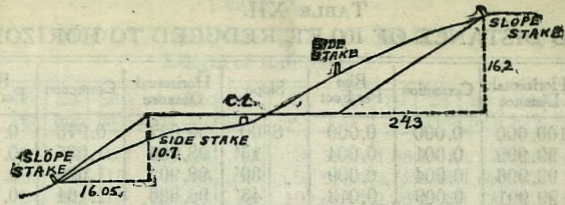
DIRECTIONS FOR USE OF TABLES

TABLE 1
 Distance of slope from top of shoulder
 stake for any width roadway slope 1 1/2 to 1.
 If ground is nearly level the cut or fill side
 stake is located by double entry in
 left column and top row. The number in body
 left column and top row and column distance
 from side stake to slope stake. If ground is not
 level the distance of slope stake from
 stake is nearly level roadway slope 1 1/2 to 1.
 If ground is nearly level the cut or fill side
 stake is located by double entry in
 left column and top row. The number in body
 left column and top row and column distance
 from side stake to slope stake. If ground is not
 level the distance of slope stake from
 stake is nearly level roadway slope 1 1/2 to 1.
 If ground is nearly level the cut or fill side
 stake is located by double entry in
 left column and top row. The number in body
 left column and top row and column distance
 from side stake to slope stake. If ground is not
 level the distance of slope stake from
 stake is nearly level roadway slope 1 1/2 to 1.
 If ground is nearly level the cut or fill side
 stake is located by double entry in
 left column and top row. The number in body
 left column and top row and column distance
 from side stake to slope stake. If ground is not
 level the distance of slope stake from
 stake is nearly level roadway slope 1 1/2 to 1.

IMPROVED TABLES AND INFORMATION

TABLE 2
 To find tangent and External for
 any other degree divide by degree of
 and connection found in column of connection.
 Degree of curve with a given I may be found
 by dividing tangent (or external) opposite I by
 given tangent (or external).
 The distance from a point on the tangent to
 the curve is very nearly the square of the tangent
 length divided by twice the radius.

1291
1291



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.
SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 65	1 80	1 95	2 10	2 25	2 40	2 55	2 70	2 85	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

5+7340 Long
BM 413

29.210
28
267.10
146

1.54
5
770

176.63
59
177.22
62
177.84
62
178.46
77
179.23
77
180.00

127
62
6.5
10.7
167

154
616

3128
2288
806
385
154
1540
1925
385
59290

2 1590
195

290
10650
24743
258080