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This index app 80 7/17/30 H.H.

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This index App 80 7/17/30 M.H. M.

Index

Page 67 to 76 X-Section 9/16 Block 77 Park Villas

Walker  
A-27

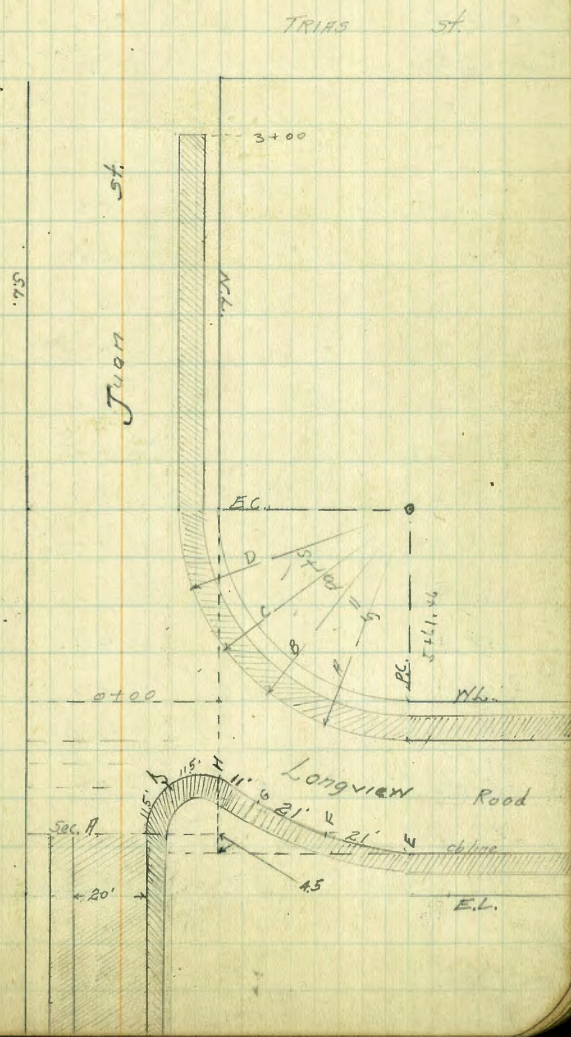
X. SECTION JUAN St. 50' wide 10' cbs  
From LONGVIEW Rd. To TAYLOR St.  
7.5'  $\frac{1}{4}$  S

N.E. B.P.				
Sunset + M.H. Perry	1.09	262.11		261.02
T.P.	0.31	249.36	13.06	249.05
T.P.	0.19	236.89	12.66	236.70
T.P.	2.99	226.91	12.97	223.92
P.C. on top of cb.		0.27		226.64
H " " "		2.41		224.50
B " " "		4.59		222.32
C " " "		6.82		220.09
D " " "		8.97		217.94
E.C. " " "		11.12		215.79
E " " "		+ 0.66		227.57
F " " "		0.99		225.92
G " " "		2.56		224.35
H " " "		3.60		223.31
J " " "		3.77		223.14

PLOTTED

Section H = 4.5' West of E. cb. line Longview Rd.

N top of cb	3.30	223.61
" Gutter on paving	3.67	223.24
d " "	3.56	223.35
S " "	3.36	223.85
S top of cb	3.11	223.80
S.L.	4.8	224.11
L Longview Rd.		
- 10	7.1	219.8
- 5	4.8	222.1



226.91

JAIN ST

S	4.3	22.6
cb	4.0	22.9
$\frac{1}{4}$	4.3	22.9
L on Rim Mt.	4.25	22.66
$\frac{1}{4}$	4.3	22.6
cb	4.3	22.6
E on Ground	4.7	22.7
	N $\frac{1}{4}$	
E	5.0	21.9
cb	5.2	21.7
$\frac{1}{4}$	5.0	21.9
L	5.1	21.8
$\frac{1}{4}$	5.3	21.6
cb	5.0	21.9
S	5.5	21.4
+6	6.1	20.8
+14	9.2	17.7
	Ncb	
-14	9.4	17.5
-7	6.9	20.0
S	6.4	20.5
cb	5.9	21.0
$\frac{1}{4}$	6.0	20.9
L	6.0	20.9
$\frac{1}{4}$	5.5	21.4
cb	5.6	21.3

slightly west  
of L

226.91

2

N	4.7	22.0
	W.L. Longview 0+00	
N	6.0	20.9
cb	6.2	20.7
$\frac{1}{4}$	6.7	20.2
L	6.9	20.0
$\frac{1}{4}$	7.0	19.9
cb	7.2	19.9
S	6.4	20.5
-14	10.9	16.0
	50' W.W.L. = E.C.	
-10	14.8	12.1
-6	14.7	12.7
S	11.0	15.9
cb	11.1	15.8
+2	12.6	14.3
$\frac{1}{4}$	12.1	14.8
L	12.0	14.9
$\frac{1}{4}$	12.0	14.9
N Gut	12.1	14.8
N Top cb	11.7	15.7.9
+8	11.0	15.9
N	10.1	16.8
T.P. 041	214.31 13.01	213.90
	100' W.W.L.	
N	4.3	10.0

214.31

+2	4.9	9.4
N top cb	5.20	9.11
Gut.	6.4	7.9
$\frac{1}{4}$	6.3	8.0
$\frac{1}{2}$	6.0	8.3
$\frac{1}{4}$	6.1	8.2
cb	6.0	8.3
+2	5.1	9.2
S	5.0	9.3
+8	7.4	4.9
+15	10.1	4.2

150' West

-10	15.1	99.7
-5	14.7	99.6
S	11.9	2.4
+8	11.7	2.6
cb	12.6	1.7
$\frac{1}{2}$	12.1	2.2
$\frac{1}{4}$	12.2	2.1
$\frac{1}{4}$	12.5	1.8
Gut	12.6	1.7
N top cb	11.77	2.54
N	11.5	2.8
TP	11.74	401.57
N	5.3	97.5
N top cb	5.74	97.15

1.30  
200' W

202.87 JAIN ST

3

Gut	6.8	96.0
$\frac{1}{2}$	6.7	96.6
$\frac{1}{4}$	6.0	96.8
$\frac{1}{4}$	6.3	96.5
cb	6.1	96.7
S	5.7	97.1
+2	5.8	97.0
+8	8.0	94.8
	250' W	
-5	9.9	93.0
S	9.3	93.6
cb	9.6	93.3
$\frac{1}{4}$	10.1	92.8
$\frac{1}{2}$	9.9	93.0
$\frac{1}{4}$	9.6	93.3
N Gut	9.5	93.4
N top cb	9.24	93.63
N	9.7	93.6
	300' W = End of Exist. cb on N	
N	12.2	90.6
N top cb	12.24	90.63
TP	9.34	192.97
	12.24	190.63
N Gut	2.8	90.1
$\frac{1}{2}$	2.2	90.7
$\frac{1}{4}$	2.1	90.8
$\frac{1}{4}$	2.1	90.8

192.97

cb	23	90.6
S	24	90.5
+5	24	90.5

315' = E.L. Trias st = 0+00

S	29	90.0
cb	29	90.0
$\frac{1}{2}$	26	90.3
$\frac{1}{2}$	26	90.3
$\frac{1}{4}$	26	90.3
cb	34	89.5
N	35	89.4

0+25

-10	7.6	85.3
N	7.1	85.8
+4	7.0	85.9
cb	4.3	88.6
+5	3.4	89.5
$\frac{1}{2}$	3.5	89.4
+3	2.7	90.2
$\frac{1}{2}$ on Rim of M.H.	3.33	89.64
$\frac{1}{2}$	3.5	89.4
cb	3.5	89.4
S	3.1	89.2

0+50 = W.L. Trias

-5	5.9	87.0
S	4.8	88.1

192.97

TOWN ST.

4

cb	4.7	88.2
$\frac{1}{2}$	4.7	88.2
$\frac{1}{2}$	4.9	88.0
$\frac{1}{2}$	9.9	83.0
cb	13.7	79.2
N	18.0	74.9
+4	18.0	74.9
+8	14.9	78.0
+25	17.1	75.8

0+77

-25	23.5	69.4
-7	20.7	72.2
-5	19.1	73.8
N	19.1	73.8
cb	13.3	79.6
$\frac{1}{2}$	10.7	82.2
$\frac{1}{2}$	5.3	87.6
$\frac{1}{2}$	5.3	87.6
cb	5.2	87.7
S	5.3	87.6
+2	6.6	86.3
+5	6.6	86.3

1+08

-5	7.5	85.4
-2	6.8	86.1
S	5.5	87.4

192.97

cb	55	87.4
$\frac{1}{4}$	56	87.3
2	55	87.4
$\frac{1}{2}$	10.3	82.6
cb	12.8	80.1
N	14.5	78.4
+25	22.2	70.7
1450		
-25	14.4	78.5
N	11.7	81.2
cb	10.7	80.2
$\frac{1}{4}$	9.6	83.3
+4	6.0	86.9
2	6.0	87.0
$\frac{1}{4}$	6.2	86.7
cb	4.2	86.7
5	6.3	86.6
+2	7.5	85.4
+5	7.5	85.4
1480		
5	6.2	86.7
+3	6.9	86.0
cb	4.8	86.1
$\frac{1}{2}$	4.3	86.6
cb	6.3	86.6
+1	5.9	87.0

192.97

John St.

5

$\frac{1}{2}$	6.8	86.1
cb	7.3	85.6
N	7.8	85.1
+10	8.4	84.5
2+00		
N	5.4	87.5
cb	5.3	87.6
$\frac{1}{4}$	5.0	87.9
+5	4.8	88.1
2	7.1	85.9
$\frac{1}{4}$	7.1	85.9
cb	7.4	85.5
+5	7.5	85.4
5	5.2	87.7
T.P. 390	197.14	4.71
188.76		
2+50		
5	5.7	86.5
+2	6.2	86.0
+3	8.2	84.0
cb	7.5	84.7
$\frac{1}{4}$	7.5	84.7
+5	7.8	84.4
2	6.7	85.5
+2	3.2	89.0
$\frac{1}{4}$	2.9	89.3
cb	2.6	89.6

187.76  
 187.76  
 187.76  
 187.76  
 187.76



19216

N		3.4	88.8
	3+00		
N		4.0	88.2
cb		3.1	89.1
$\frac{1}{4}$		2.8	89.4
+5		2.8	89.4
d		5.4	86.8
+1		5.4	83.8
+3		7.7	82.5
$\frac{1}{4}$		9.5	82.7
cb		9.5	82.7
+8		9.9	82.3
S		8.2	84.0
	3+50 = K.L. Ampudia		
S		10.6	81.6
+4		11.6	80.6
cb		11.3	80.9
$\frac{1}{4}$		11.3	80.9
+5		11.3	80.9
d		10.1	82.1
+3		5.6	86.6
$\frac{1}{4}$		5.7	87.0
cb		5.7	87.0
N		5.7	87.0
	Kcb		
N		5.1	87.1

10' cbs  
7.5'  $\frac{1}{4}$  S

19216 JUN 54

6

cb		53	86.9
$\frac{1}{4}$		54	86.8
+4		57	86.5
cb		86	83.6
+1		10.6	81.6
+3		11.8	80.4
$\frac{1}{4}$		11.6	80.6
cb		11.7	80.5
+9		12.1	80.1
S		11.0	81.2
S		11.2	81.0
+1		12.4	79.8
cb		11.9	80.2
$\frac{1}{4}$		11.9	80.2
+3		12.1	80.1
+6		11.3	80.9
cb		9.7	83.0
+4		5.8	86.4
$\frac{1}{4}$		5.6	86.6
cb		5.3	86.9
+9		5.0	86.2
N		4.4	87.8
N		4.0	88.2
+4		4.9	87.3

19216

cb	53	86.9
$\frac{1}{4}$	55	86.7
+5	60	86.2
$\frac{1}{2}$	86	83.6
+2	120	80.2
$\frac{1}{4}$	121	80.1
cb	122	80.0
+9	125	79.7
S	11.6	80.6
	$\frac{1}{2}$	
S	11.3	80.8
+1	12.9	79.3
cb	12.5	79.7
$\frac{1}{4}$	12.4	79.8
+4	12.5	79.7
$\frac{1}{2}$	10.6	81.6
+4	5.9	86.3
$\frac{1}{2}$	5.4	86.8
cb	5.3	86.9
+8	4.8	87.4
N	3.8	88.4
	$\frac{1}{2}$ cb	
N	3.7	88.5
+1	4.5	87.7
cb	5.1	87.0
+3	5.2	87.0

19216

JAN ST.

7

+4	7.4	84.8
+7	8.0	84.2
$\frac{1}{4}$	5.6	86.6
+3	5.8	86.4
$\frac{1}{2}$	9.4	82.8
+1	12.4	79.8
$\frac{1}{2}$	12.7	79.5
cb	12.8	79.3
+9	13.2	78.0
S	12.7	79.5
	N.L. Ampudia = 0400	
S	13.1	79.1
+1	13.7	78.5
cb	13.3	78.9
$\frac{1}{2}$	13.2	79.0
+4	13.5	78.7
+6	12.5	79.7
cb	10.7	81.5
+5	5.7	86.5
$\frac{1}{4}$	5.7	86.9
cb	5.0	86.2
N	2.4	88.0
	0430	
N	3.1	89.1
cb	4.0	88.2
$\frac{1}{2}$	4.4	87.8

192.16

+3	11.2	81.0
2	13.3	78.9
+4	15.4	76.8
$\frac{1}{2}$	15.1	77.1
cb	15.1	77.1
S	15.8	76.4

0+40

S	16.2	76.0
cb	15.9	76.3
$\frac{1}{4}$	15.7	76.5
2	15.1	77.1
$\frac{1}{4}$	13.9	78.3
+1	4.0	88.2
cb	3.9	88.3
N	3.0	89.2

0+50

N	3.1	89.1
cb	4.0	88.2
$\frac{1}{4}$	4.3	87.9
+1	10.7	81.5
2	15.5	76.7
+2	16.2	76.0
$\frac{1}{2}$	16.5	75.7
cb	16.5	75.7
S	16.3	75.9

0+60

192.16

JAUN ST.

8

9

S	17.5	74.7
cb	17.0	75.2
$\frac{1}{4}$	16.8	75.4
+5	16.7	75.5
2	14.3	77.9
+3	11.4	80.8
+4	4.9	87.3
$\frac{1}{2}$	4.8	87.4
cb	4.3	87.9
N	2.7	89.5

0+70

N	3.5	88.7
cb	4.6	87.6
$\frac{1}{4}$	5.3	86.8
+1	8.2	84.0
+6	12.0	80.2
2	15.0	77.2
+2	17.3	74.9
$\frac{1}{4}$	17.9	74.3
cb	17.6	74.6
S	17.8	74.4

0+76

S	17.7	74.5
cb	18.3	73.9
$\frac{1}{2}$	18.3	73.9
+5	18.3	73.9

L	10.7	81.5
+2	7.9	84.3
+3	6.0	86.2
1/2	5.6	86.6
cb	5.0	87.2
N	3.8	88.4
0+90		
N	5.4	86.8
cb	6.5	85.7
+1	6.7	85.5
+4	12.0	80.2
1/2	15.6	76.6
L	17.3	72.9
1/2	19.2	73.0
cb	19.2	73.0
S	19.4	72.8
17.00		
S	19.8	72.4
cb	19.8	72.4
1/2	20.3	71.9
L	20.3	71.9
1/2	18.8	73.4
+4	16.9	75.2
+5	7.6	84.6
cb	7.4	84.8
N	6.9	85.3

T.P. 0.87	185.04	7.99	184.17
1710			
N		0.9	84.1
cb		1.4	83.6
+6		2.3	82.7
1/2		10.1	74.9
L		13.5	71.5
1/4		13.8	71.2
cb		13.7	71.3
S		13.3	71.7
1433			
S		15.3	69.7
cb		15.5	69.5
1/2		15.5	69.5
L		14.8	60.2
+7		9.0	76.0
1/2		4.7	80.3
cb		3.9	81.1
N		3.0	82.0
1747			
N		4.6	80.4
cb		5.1	79.6
1/2		5.9	79.1
+4		6.5	78.5
cb		11.3	73.7
+4		16.4	78.6

7		16.9	68.1
cb		16.6	68.4
S		16.7	68.3
	1+56		
S		17.6	67.4
cb		17.6	67.4
$\frac{1}{4}$		17.4	67.6
+3		17.4	67.6
$\frac{1}{2}$		14.3	70.7
+3		12.3	72.7
+5		7.0	78.0
$\frac{1}{4}$		7.0	78.0
cb		6.2	78.8
N		6.0	79.0
T.P.	282 179.21	8.65	176.39
	1+66		
N		1.1	78.1
cb		1.4	77.8
$\frac{1}{4}$		1.9	77.3
+5		2.4	76.8
d		9.3	68.9
+5		12.8	66.4
$\frac{1}{4}$		13.0	66.2
cb		12.8	66.4
S		12.9	66.3

1+84

S		14.6	64.7
cb		14.8	64.4
$\frac{1}{4}$		15.2	64.0
+4		14.9	64.3
$\frac{1}{2}$		12.2	67.0
+3		6.2	73.0
$\frac{1}{4}$		5.4	73.8
cb		4.7	74.5
N		4.2	75.0
	2+00		
N		7.7	71.5
d		8.2	71.0
$\frac{1}{4}$		8.5	70.7
+5		8.9	70.3
$\frac{1}{4}$		16.1	63.0
$\frac{1}{4}$		16.5	62.7
cb		16.5	62.7
S		17.0	62.2
	2+87		
S		20.3	58.9
cb		20.0	59.2
$\frac{1}{2}$		20.1	59.1
+5		20.4	58.8
d		14.1	65.1
N		12.2	67.0
$\frac{1}{4}$		12.0	67.2

cb		11.9	67.3
N		11.6	67.6
T.P.	0.30	166.94	12.57
	2135		16664
N		0.8	66.1
cb		1.2	65.7
1/4		0.8	66.1
1/2		1.8	65.1
+2		9.4	57.5
1/4		8.7	58.2
cb		8.7	58.2
S		8.5	58.4
	2148		
S		10.3	56.6
cb		10.3	56.6
1/2		10.4	56.5
+6		10.9	56.0
1/2		7.9	59.0
+2		4.6	62.3
1/4		4.4	62.5
cb		4.4	62.5
N		4.4	62.5
	2170		
N		9.3	57.6
cb		8.8	58.1
1/2		9.2	57.7

+6		9.8	57.1
1/2		11.5	55.4
+4		13.4	53.5
+2		13.0	53.9
1/4		13.0	53.9
cb		13.1	53.8
S		12.3	54.6
	3+00 = E.L. #11 sta		
S		16.5	50.4
cb		16.8	50.1
1/4		16.8	50.1
1/2		16.9	50.0
+1		16.3	50.6
+3		13.3	53.6
1/4		12.8	54.1
cb		13.1	53.8
N		13.8	53.1
T.P.	0.15	154.67	12.42
			154.52
	Ecb		
N		2.9	51.6
cb		1.7	53.0
1/4		2.4	52.3
+1		3.2	51.5
1/2		3.5	49.2
+1		6.8	47.9
1/4		6.0	48.7

10' cbs  
7.5' 1/4s

cb	6.0	48.7
+6	6.2	47.5
S	5.6	49.1
	$E \frac{1}{4}$	
S	6.6	48.1
+2	7.3	47.4
cb	7.0	47.7
$\frac{1}{4}$	7.1	47.6
2	7.6	47.1
+3	4.3	50.4
$\frac{1}{4}$	3.9	50.8
cb	3.8	50.9
N	4.2	50.5
	2	
N	6.0	48.7
cb	5.1	49.3
$\frac{1}{2}$	5.4	49.3
+5	5.7	49.0
2	7.4	47.3
+1	8.6	46.1
$\frac{1}{4}$	8.2	46.5
cb	8.0	46.7
S	8.4	46.3
	$N \frac{1}{4}$	
S	9.4	45.3
cb	9.1	45.6

$\frac{1}{4}$	9.1	45.6
+6	9.0	45.7
2	8.1	46.6
+3	7.0	47.7
$\frac{1}{4}$	6.7	48.0
cb	7.2	47.5
N	7.6	47.1
	Wcb	
N	8.3	45.4
cb	8.3	45.4
$\frac{1}{4}$	8.0	46.7
+5	8.2	46.5
2	9.5	45.2
+1	10.1	44.6
$\frac{1}{4}$	9.9	44.8
cb	9.8	44.9
S	10.6	44.1
	W. Arista = 0+00	
S	11.9	42.8
cb	11.2	43.5
$\frac{1}{4}$	11.2	43.5
cb	11.8	42.9
+1	11.8	42.9
+3	10.1	44.6
$\frac{1}{4}$	9.2	45.5
cb	9.8	44.9

N		10.0	44.7
	0+50		
N		14.2	40.5
cb		13.8	40.9
$\frac{1}{4}$		13.5	41.2
+4		13.5	41.2
$\frac{1}{2}$		14.5	38.2
$\frac{1}{4}$		16.1	38.6
cb		16.2	38.5
S		16.7	38.0
T.P.	0.11	142.28	12.50 12.17
	1+00		
S		8.4	33.9
+1		9.3	33.0
cb		8.7	33.6
$\frac{1}{4}$		8.6	33.7
$\frac{1}{2}$		9.4	32.9
+5		6.1	36.2
$\frac{1}{4}$		5.8	36.3
cb		5.6	36.7
N		6.2	36.1
	1+18		
N		8.2	33.9
cb		7.4	34.7
$\frac{1}{4}$		7.5	34.8
+4		8.4	34.1

$\frac{1}{2}$	10.9	31.4
$\frac{1}{4}$	10.1	32.2
16	10.3	32.0
+8	10.7	31.6
+9	9.4	32.9
S	9.4	32.9
	1+28	
S	10.3	32.0
+1	10.3	32.0
+2	11.3	31.0
cb	11.1	31.2
$\frac{1}{4}$	10.9	31.4
$\frac{1}{2}$	11.4	30.9
+4	11.4	30.9
+5	10.1	32.2
$\frac{1}{4}$	9.4	32.9
cb	9.4	32.9
N	9.4	32.9
	1+37	
N	10.2	32.1
cb	8.5	33.8
$\frac{1}{4}$	8.2	34.1
+2	8.4	33.9
+5	12.1	30.2
$\frac{1}{2}$	12.1	30.2
$\frac{1}{4}$	11.8	30.5



cb		119	30.4
+5		126	29.7
U		11.1	31.2
	1+65		
S		121	30.2
+2		140	28.3
+5		143	28.0
+6		151	27.2
cb		144	27.7
$\frac{1}{4}$		147	27.6
$\frac{2}{4}$		147	27.6
+1		145	27.8
+5		108	31.5
$\frac{1}{2}$		9.3	33.0
cb		9.6	32.7
N		120	30.3
T.P.	135	130.61	130.2
	2+00		129.26
N		29	27.7
cb		17	28.9
+6		15	29.1
$\frac{1}{2}$		18	28.8
+1		24	28.2
+5		68	23.8
$\frac{1}{4}$		70	23.6
$\frac{1}{4}$		65	24.1

cb		66	24.0
+4		72	23.4
+9		64	24.2
U		53	25.3
	2+87		
S		84	22.2
+1		86	22.0
+2		96	21.0
cb		95	21.1
$\frac{1}{2}$		93	21.3
$\frac{2}{4}$		97	20.9
+3		75	21.1
+6		63	24.3
$\frac{1}{4}$		47	25.9
cb		42	26.4
N		54	25.2
	2+31		
N		62	24.4
cb		68	23.8
$\frac{1}{4}$		76	23.0
+3		88	21.8
+4		101	20.5
$\frac{1}{2}$		100	20.6
$\frac{1}{4}$		96	21.0
cb		98	20.8
+8		10.0	20.6

S	8.2	22.4
L+AV		
S	8.4	22.2
+2	10.9	19.7
cb	11.0	19.6
1/2	10.9	19.7
1/2	11.1	19.5
+5	11.4	19.2
1/4	9.1	21.5
cb	7.4	23.2
N	6.8	23.8
L+Ab		
N	6.1	23.5
cb	6.0	24.6
1/2	6.2	24.4
+1	7.0	23.6
+3	12.5	18.1
1/2	11.7	18.9
1/2	11.4	19.2
cb	11.5	19.1
+7	11.9	18.7
+8	10.9	19.7
S	8.6	22.0
3+00 = E.L. Condo st	10' obs 7.5' obs	
S	17.5	18.1
+3	17.0	13.6

cb	17.1	13.5	
1/2	16.9	13.7	
1/2	17.6	13.0	
+5	16.5	14.1	
1/4	11.7	18.9	
+2	10.5	20.1	
cb	10.0	20.6	
N	9.3	21.3	
E. cb			
T.P. 0.70	121.85	9.46	121.15
N	14	20.4	
cb	21	19.8	
1/4	30	18.8	
+1	7.8	14.0	
+5	9.6	12.2	
1/2	9.5	12.3	
1/4	9.2	12.6	
cb	9.2	12.6	
+7	8.8	13.0	
S	4.7	17.1	
E. 1/4			
S	5.4	16.4	
+3	7.6	14.2	
+4	9.2	14.6	
cb	10.0	11.8	
1/4	9.9	12.0	

2	10.7	11.6
+5	9.7	12.1
$\frac{1}{4}$	3.8	18.0
+1	3.0	18.8
cb	3.4	18.4
N	2.0	19.8

L Conde st

N	2.2	19.6
cb	2.8	19.0
+6	3.3	18.5
$\frac{1}{4}$	4.4	17.4
+1	9.2	12.6
+4	10.9	11.0
2	11.1	10.8
$\frac{1}{4}$	10.9	11.0
cb	10.8	11.0
+7	10.1	11.8
+8	6.8	15.0
S	5.6	16.2

N  $\frac{1}{4}$ 

S	6.0	15.8
+4	7.4	14.4
+3	10.6	11.2
cb	11.6	10.2
$\frac{1}{4}$	11.6	10.2
2	11.6	10.2

+5	10.7	11.1
+6	5.5	16.3
$\frac{1}{4}$	5.0	16.8
cb	3.6	18.2
N	3.3	18.5

Ncb

N	4.3	17.5
cb	6.4	15.4
+5	9.0	12.8
$\frac{1}{4}$	11.1	10.7
+3	12.3	9.5
2	12.5	9.3
$\frac{1}{4}$	12.2	9.6
cb	12.3	9.5
+7	11.5	0.3
+8	7.1	4.8
S	6.3	5.5

N.L. Conde st - 0+00

S	7.1	14.8
+2	7.9	14.0
+3	12.5	9.6
cb	13.9	8.6
$\frac{1}{4}$	13.3	8.6
2	13.4	8.4
+5	13.1	8.8
$\frac{1}{4}$	11.5	10.4

+1	10.9	10.9
+2	7.1	14.8
$\frac{1}{4}$	6.7	15.2
cb	5.7	16.2
N	4.7	17.2

T.P.	870	118.28	1247	10938
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0405

N	1.1	17.1
cb	1.4	16.7
+4	1.7	16.4
+7	3.2	14.9
$\frac{1}{4}$	8.6	9.5
+2	9.8	8.3
d	10.0	8.1
$\frac{1}{2}$	9.9	8.2
cb	9.9	8.2
+8	9.2	8.9
+9	3.9	14.2
S	3.6	14.5

0450

J	7.0	11.1
+2	8.7	9.4
+3	13.8	4.3
cb	14.4	3.7
$\frac{1}{4}$	14.7	3.9
d	14.4	3.7

$\frac{1}{2}$	14.6	3.5
+1	13.4	4.7
+2	8.0	10.1
cb	6.3	11.8
N	5.9	12.1

1400

N	10.5	07.6
+8	11.2	6.9
cb	16.7	1.4

T.P.	214	107.16	13.04	105.02
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cb +5	8.7	98.5
$\frac{1}{2}$	8.9	98.3
d	8.5	98.7
$\frac{1}{4}$	8.5	98.7
cb	9.1	98.1
+7	7.9	99.3
+8	3.2	04.0
S	1.5	5.7

1450

S	8.2	99.0
+2	8.9	98.3
+3	13.8	93.3
+7	14.2	93.0
+9	16.3	90.8
cb	16.3	90.8
+1	14.4	92.8

3 NAILS in SW. candle  
High Voltage from  
Elec. Pole St.

1/2	14.4	92.8
2	14.1	93.1
1/4	14.5	92.7
+5	14.3	92.9
cb	11.9	95.3
+3	10.0	97.2
+5	5.7	01.5
N	5.0	02.2
1+61		
N	7.2	00.0
+4	8.2	99.0
+7	12.0	95.2
cb	14.2	93.0
+3	15.9	91.3
1/4	15.9	91.3
2	15.2	92.0
1/2	15.6	91.6
+5	15.9	91.3
+6	17.1	90.1
cb	17.1	90.1
+2	15.4	91.8
+7	15.1	92.1
+8	9.7	99.5
5	9.8	97.4
1+70		
5	14.1	95.1

+2	11.5	95.7
+3	12.4	94.8
+4	16.2	91.0
+7	16.9	90.3
+8	17.9	89.3
cb	18.2	89.0
+2	16.7	90.5
1/4	16.6	90.6
2	16.5	90.7
1/4	16.8	90.4
+4	17.3	89.9
cb	15.9	91.2
+2	11.1	96.1
+4	7.4	99.8
N	6.7	00.5
1+87		
N	8.2	99.0
+6	9.1	98.1
+7	11.9	95.3
+8	17.2	90.0
T.P.	0.50	94.63
4	13.02	94.13
cb	5.1	89.5
+2	4.5	88.1
1/2	6.2	88.4
cb	6.0	88.6
1/2	6.1	88.5

z +5	6.2	88.4
+6	7.3	87.3
cb	7.3	87.3
+1	4.4	88.2
+5	6.0	88.6
+7	2.5	92.1
S	3.5	91.1

R+00

S	5.5	89.1
+3	5.1	89.5
+5	7.3	87.3
+6	7.6	87.0
+7	6.4	86.2
cb	6.7	85.9
$\frac{1}{2}$	7.9	86.7
$\frac{2}{2}$	7.9	86.7
$\frac{1}{4}$	8.0	86.6
+5	8.5	86.1
cb	6.7	87.9
+4	0.2	94.4
N	+0.3	94.9

R+41

N	5.1	89.4
+4	5.6	89.0
+6	7.6	87.0
+8	11.5	83.1

cb	13.1	81.5
$\frac{1}{2}$	13.8	80.8
$\frac{2}{2}$	13.9	80.7
$\frac{1}{4}$	13.8	80.8
+5	14.1	80.5
cb	15.2	79.4
+3	14.1	80.5
+6	13.6	81.0
S	14.5	80.1

R+56

S	17.5	77.1
+4	15.6	79.0
+6	16.3	78.3
+7	17.6	77.0
cb	16.9	77.7
+1	16.0	78.6
$\frac{1}{2}$	15.8	78.8
$\frac{2}{2}$	15.8	78.8
$\frac{1}{4}$	15.7	78.9
cb	15.8	78.8
N	8.9	87.7

R+62

N	7.8	86.8
+2	8.7	86.4
+3	10.0	84.6
cb	10.0	78.6

+1	16.9	77.7
$\frac{1}{2}$	16.9	77.7
2	16.8	77.8
$\frac{1}{4}$	16.9	77.7
cb	17.3	77.3
+1	18.2	76.4
+3	18.1	76.5
+4	17.3	77.3
+7	16.3	78.3
S	18.3	76.3

E-65

S	18.5	76.1
+3	16.6	78.0
+6	17.1	77.5
+7	18.9	77.7
+9	18.7	75.9
cb	17.1	77.5
$\frac{1}{4}$	16.8	77.8
2	16.7	77.9
$\frac{1}{4}$	16.7	77.9
+6	16.9	77.7
cb	15.9	78.7
+3	13.8	80.8
+6	9.3	85.3
N	8.6	86.0

E-76

N	11.3	83.3
+1	12.5	82.1
+2	13.7	81.4
+9	18.1	76.5
cb	18.1	76.5
$\frac{1}{4}$	18.5	76.1
2	18.6	76.0
$\frac{1}{4}$	18.7	75.9
+6	19.1	75.5
cb	20.3	74.3
+2	20.4	74.2
+5	18.8	75.8
S	21.1	73.5
-5	22.7	71.9
-5	23.9	70.7
S	22.7	71.9
+5	22.1	72.5
+6	20.6	74.0
+8	20.0	74.6
+9	22.0	72.6
cb	22.0	72.6
+1	20.4	74.2
$\frac{1}{4}$	19.8	74.8
2	19.7	74.9
$\frac{1}{2}$	19.7	74.9

94.63<sup>4</sup>

cb			194	74.2
+4			17.3	77.3
+7			131	81.5
N			122	82.4
T.P.	0.84	82.78 <sup>9</sup>	12.69	81.94 <sup>5</sup>
T.P.			11.11	71.67 <sup>8</sup>

21

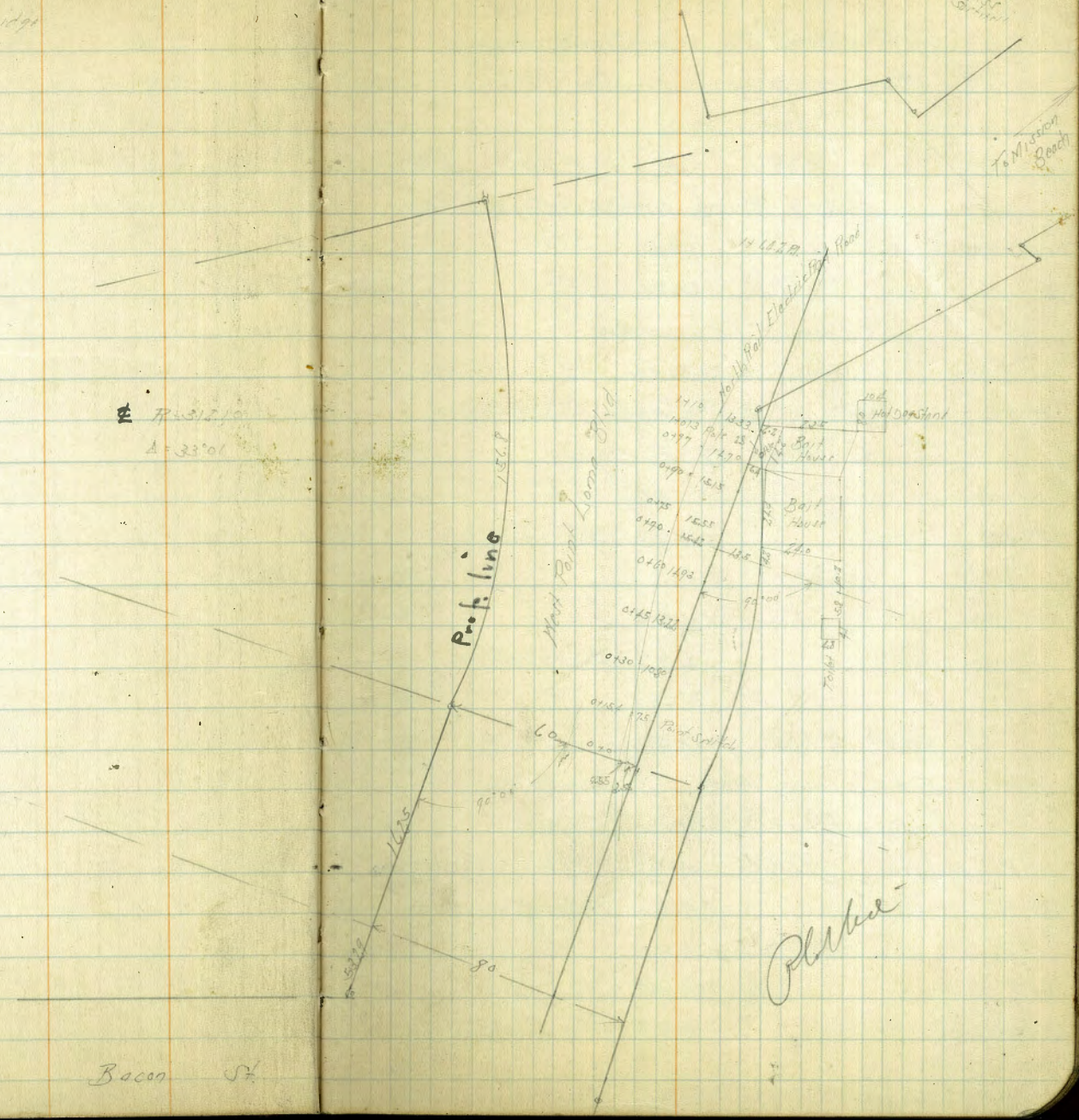


Location of Bail House  
 West Point Loma Blvd  
 South End Mission Bay Bridge

6-11-27  
 12:00  
 12:00  
 12:00

To Mission  
 Beach

# R-31210  
 A=33°01'



Bacon St.

Altadena Curb levels  
El Cajon Ave South

Sta	+	H.I	-	Elev	BM.
		392.8			
W. Prop line		5.26		387.5	
E .. ..		4.91		387.9	

S. Line El Cajon Ave

W.Cb		5.24		387.6	
Ecb		5.03		387.8	

50' S. of S.L. El Cajon

Wcb		5.26		387.5	
Ecb		4.93		387.9	

100' S

W.Cb		5.33		387.5	
Ecb		4.87		388.0	

50th St Curb levels

El Cajon Ave South

South cb line El Cajon

W. Prop line		388.6	5.87	382.8	
E .. ..			4.85	382.8	

S. L. El Cajon Ave

W.Cb		5.48		383.1	
E.Cb		5.03		383.6	

50' S. of S.L. El Cajon

Sta	+	H.I	-	Elev	BM
Wcb				5.91	382.7
Ecb				5.61	383.0

100' S

Wcb				6.42	382.2
Ecb				6.03	382.6

Wimona - St Curb levels

South Curb line El Cajon Ave

W. Prop		375.4	3.89	371.5	
E Prop			0.83	374.6	

S. Line El Cajon

W.Cb				3.26	371.6
Ecb				1.60	373.8

50' South

W.Cb				6.46	369.0
E.Cb				4.53	370.9

100' South

W.Cb				9.25	366.2
Ecb				7.44	368.0

150' South

Wcb				12.11	363.3
Ecb				10.35	365.1

182' South

Wcb					
Ecb				12.16	363.2 Break

5 Feet

Sta + HI - Elev BM

✓ 51 st curb Levels

Scubb line El Cajon Ave

W. Prop 393.76 5.20 388.56

E " No return

5. Line El Cajon Ave

W. cb 5.16 388.6

E cb 6.00 387.76

50' south

W cb 5.14 388.62

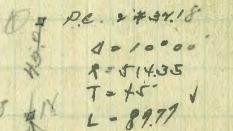
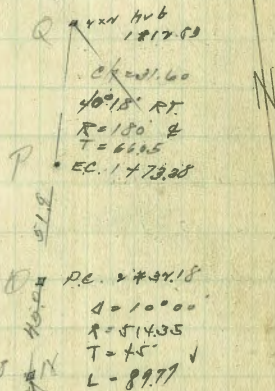
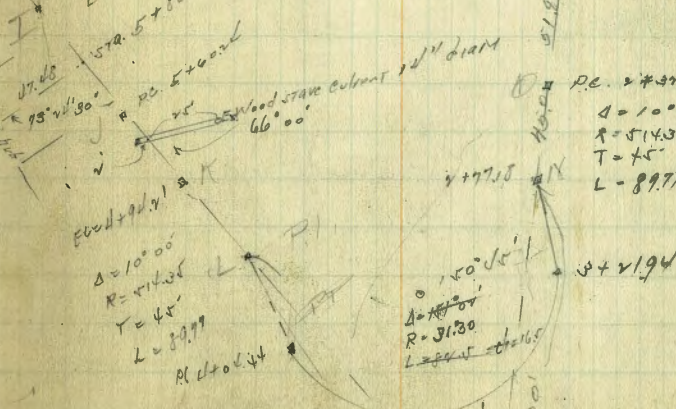
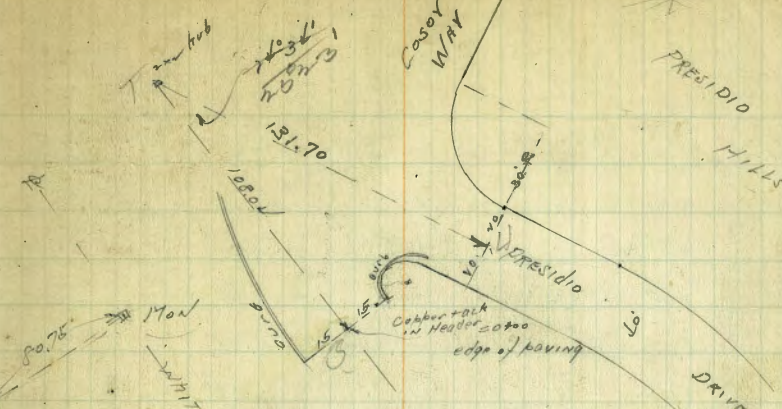
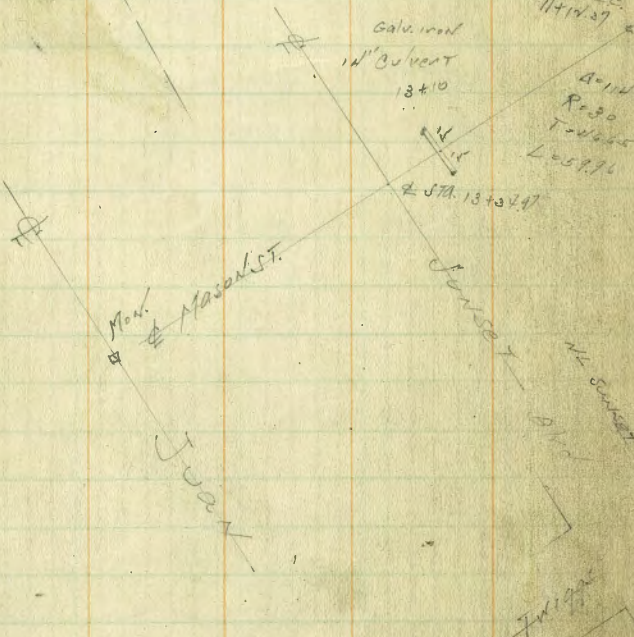
E cb 5.84 387.92

100' south

W cb 5.10 388.66

E cb 5.80 387.96

Survey + Levels of Old Town Grade 4' wide  
 From Whitman + Mason To Presidio Drive  
 9/16/77



113  
 75  
 70

25

Cross Section of 16' wide Old Town Grade

1709.98

SE width for return 1.38	248.64	247.26
TP 0.04	236.14	236.08
TP 0.31	223.54	223.03
TP 0.67	211.11	210.44
TP 0.04	198.10	198.06
TP 0.76	185.91	185.15
TP 0.30	173.21	172.91
TP Cop. Tank 160	162.10	160.50

Chocoma  
H. M. Budia

20 RT	15.8	46.2
15 R	13.8	49.3
C	13.2	48.9
20 L	14.4	49.7
T.P. 1.23	150.40	129.3

1741.58

PC. NE Cor  
Whitcomb's Tr. app

20 L	3.0	47.4
C	4.1	46.3
20 R	5.4	45.2

0+00 = South edge paving

15' LT Top curb	4.98	157.1
" " " paving	5.30	156.8
" " " "	5.23	156.9
15' RT " "	5.25	156.8
" " " curb	4.24	157.4

1773.38 = FC

20 R	7.9	42.5
10 R	6.0	44.4
C	7.6	42.8
15 L	7.8	42.6
20 L	3.0	47.4

0+46.78 = PC

20' R	11.4	150.7
15' R	8.1	154.0
C	8.0	54.1
20 L	7.4	54.9

2+00

20 L	3.1	47.3
15 L	1.8	45.6
12 L	10.2	40.2
C	10.0	40.4
11 R	9.5	40.9
20 R	13.4	37.0

0+73.38

20 L	9.5	52.4
C	10.4	51.7
15 R	10.9	51.2
20	12.8	49.6

2+32.15 = PC

20 R	12.1	36.3
"	13.0	37.4

150.0

8 V		13.3	137.1
14 L		6.1	443
20 L		4.0	464
	$2+77.0 = M. of Curve$		
20 L		7.0	434
16 L		7.8	426
T.P.	0.05	127.5	137.4
14 L		4.2	333
C		4.3	332
20 R		4.2	333
	$3+21.9 = P.P.C.$		
20 R		8.0	295
C		7.8	297
12 L		8.4	291
14 L		1.7	358
20 L		0.9	366
	$3+38.4$		
20 L		7.0	305
17 V		7.2	303
15 L		9.8	277
14 V		8.6	289
C		9.4	281
20 R		9.4	281
	$3+54.9$		
20 R		10.2	273
15 R		11.6	259

137.5

57

C		11.5	126.1		
20 L		10.8	26.7		
	$3+71.4$				
20 L		12.8	24.7		
C		13.2	23.8		
15 R		13.3	24.2		
20 R		9.4	28.1		
T.P.	1.0	126.9	11.8	125.7	P.I. Sub
	$3+87.9$				
20 R		0.0	26.9		
15 R		4.5	22.4		
C		5.0	21.9		
20 L		4.5	22.3		
	$1+40.4 = P.P.C.$				
20 L		8.7	19.2		
13 L		6.4	20.5		
C		6.8	20.1		
10 R		6.3	20.6		
20 R		0.0	26.9		
	$4+49.3 = M. of Curve$				
20 R		7.6	19.3		
14 R		8.8	18.1		
15 R		17.2	14.7		
C		11.6	15.3		
6 L		11.5	15.4		
12 V		15.1	11.9		
20 L		17.5	10.9		

126.90

115.18

38

T.P.	103	115.18	1275	114.15
	4+94.21 = EC			
20 L		10.6	104.6	
C		3.3	111.9	
20 R		4.5	111.7	
	5+25 = 4 Culvert			
inlet		7.18	Flowline	
outlet		10.45	108.1	
	5+25			
20 R		6.4	109.0	
5 R		7.5	107.7	
0		10.7	104.5	
10 L		14.8	100.4	
15 L		14.1	103.1	
20 L		12.5	102.7	
	5+25			
20 L		19.1	96.1	
15 L		15.6	99.6	
C		9.0	86.2	
16 R		5.8	86.4	
20 R		6.8	88.4	
	5+60.24 = DC			
20 R		3.8	111.4	
17 R		4.8	110.4	
16 R		5.2	107.2	
12 R		11.1	104.1	

0		11.4	104.0
10 L		11.0	104.2
20 L		13.8	101.4
	6+08.41		
20 L		16.6	98.6
13 L		14.6	100.6
C		15.1	100.1
17 R		15.1	111.1
20 R		8.8	106.4
T.P.	2.85	104.97	130.6
	6+56.58		
20 R		3.5	191.5
13 R		3.4	101.6
10 R		10.4	94.8
C		10.0	95.0
17 L		9.6	95.4
20 L		10.8	94.2
	7+06.95		
20 L		17.5	87.5
16 L		15.8	89.4
C		15.1	89.9
10 R		15.1	89.9
15 R		9.7	95.3
20 R		7.8	97.2
	7+57.92 = EC		
20 R		11.6	93.4

17R			14.4	92.6
T.P.	104	93.51	12.50	94.4
14R			9.7	83.6
C			9.8	83.7
16L			9.6	83.9
20L			11.5	82.0
	8400			
20L			14.1	79.4
C			14.8	78.7
10R			14.6	78.9
14R			9.4	84.1
20R			2.5	86.0
	8450			
20R			13.9	79.6
13R			14.5	79.0
T.P.	081	81.81	12.51	81.00
10R			10.1	71.7
C			7.9	73.9
20L			7.7	74.1
	9400			
20L			12.3	69.5
C			13.5	68.3
14R			13.7	68.1
7R			15.1	66.7
15R			2.7	74.1
20R			2.1	74.7

T.P.	088	69.70	12.99	68.80
	9450			
20R			5.4	64.3
17R			8.7	61.0
15R			6.4	63.3
C			6.6	63.1
20L			6.5	63.2
	10400			
20L			11.9	57.8
C			11.2	58.1
15R			11.2	58.1
20R			13.0	56.7
T.P.	141	58.46	12.65	57.25
	Culvert 10 + 49.3 = 46.5 Length			
inlet		4.85		Flowline
outlet		8.4		"
	10 + 52.4 = PC.			
20R			3.7	54.8
C			5.2	53.3
10L			6.1	52.4
20L			5.9	52.8
	10 + 82.39 M of Curves			
20R			6.8	51.7
15L			9.9	49.6
14L			7.5	51.0
C			6.4	52.1
20R			7.0	51.5



11+12.37-EC

20 R	11.0	47.5
10 R	8.6	49.9
C	8.4	50.1
13 L	8.6	49.9
15 L	12.3	46.2
17 L	8.5	50.0
20 L	7.6	50.9

11+50

20 L	10.0	48.5
15 L	15.7	42.8
14 L	11.7	46.8
C	11.5	47.0
10 R	11.5	47.0
20 R	14.6	49.9
T.P.	0.68	46.52
	12.62	45.84

12+00

20 R	9.5	37.0
8 R	5.0	41.5
C	4.5	42.0
15 L	4.6	41.9
17 L	7.1	39.4
20 L	1.8	44.7

12+50

20 L	8.4	38.1
15 L	11.8	34.7

13 L	10.1	36.4
C	10.1	36.4
7 R	10.2	36.3
20 R	14.9	31.6
T.P.	0.25	33.95
	12.82	33.70
	1.92	

20 R	5.7	28.3
8 R	4.7	31.3
C	4.7	31.3
20 L	4.7	31.3

13+10 = Calvinon Culvert

INlet 15' L	4.28	29.7
OUTlet 15' R	6.14	37.4

13+34.97 = E SUNSET Blvd

20 L	4.0	30.0
15 L	6.1	27.9
14 L	5.5	28.5
C	5.7	28.3
5 R	6.2	28.0
20 R	10.9	23.1

13+6.5

20 R	11.2	22.8
10 R	7.5	26.5
C	7.6	26.4
14 L	8.2	25.8
17 L	6.4	27.6
20 L	5.2	28.8

14+00

20 L	8.3	23.7
18 L	8.7	25.3
15 L	10.6	23.6
C	9.8	24.2
10 R	10.1	23.9
20 R	13.3	20.7

14+30

20 R	14.9	19.1
12 R	14.0	20.0
10 R	11.2	22.5
C	11.3	22.7
20 L	11.0	23.0

14+65

proposed 24" Culvert

25 L inlet	11.6	23.0
20 L	11.2	22.8
C	11.9	22.1
5 R	13.8	20.2
20 R	14.0	20.0
30 R outlet	14.4	19.6

15+00

20 R	12.5	21.5
8 R	11.3	22.7
C	11.4	22.5
20 L	11.0	23.0
T.P.	7.61	20.54
	11.07	24.93

15+50

20 L	6.9	23.6
18 L	7.6	22.9
C	7.9	22.6
5 R	7.8	22.7
20 R	9.2	21.3

16+00

20 R	8.3	22.2
10 R	6.8	23.7
C	7.0	23.5
13 L	7.0	23.5
20 L	6.1	24.4

16+50

20 L	4.1	26.4
15 L	5.4	25.1
C	5.6	24.9
15 R	5.4	25.1
20 R	6.5	24.0

16+60 = NE line of Juan St

20 R	6.3	24.2
15 R	5.0	25.5
C	4.9	25.6
15 L	4.5	26.0
20 L	3.6	26.9

16+85 = E Juan

20 L	3.1	27.4
------	-----	------

3054

325

C Mod.

3.8

26.7

20 R

4.7

25.8

TP 0.35

19.25

11.44

18.90

12.15

6.10

6.48

SE Tab Hyd

Taylor + Wood

Tolman  
10-1-27

Xsection of Lantana Drive  
Euclid to its end

50' Sta.  
10' base

T.P.	3.06	343.74	4.38	340.68	NYBP Euclid & Univ.
T.P.	5.21	344.57	4.07	339.36	
T.P.	7.79	348.29	7.55	340.50	
	7.55	<u>348.05</u>			

E.L. Euclid

North TC. 15' out	737	340.68
Gut.	787	40.18
E	741	40.64
Gut.	6.95	41.10
South TC. 38' out	6.41	41.64

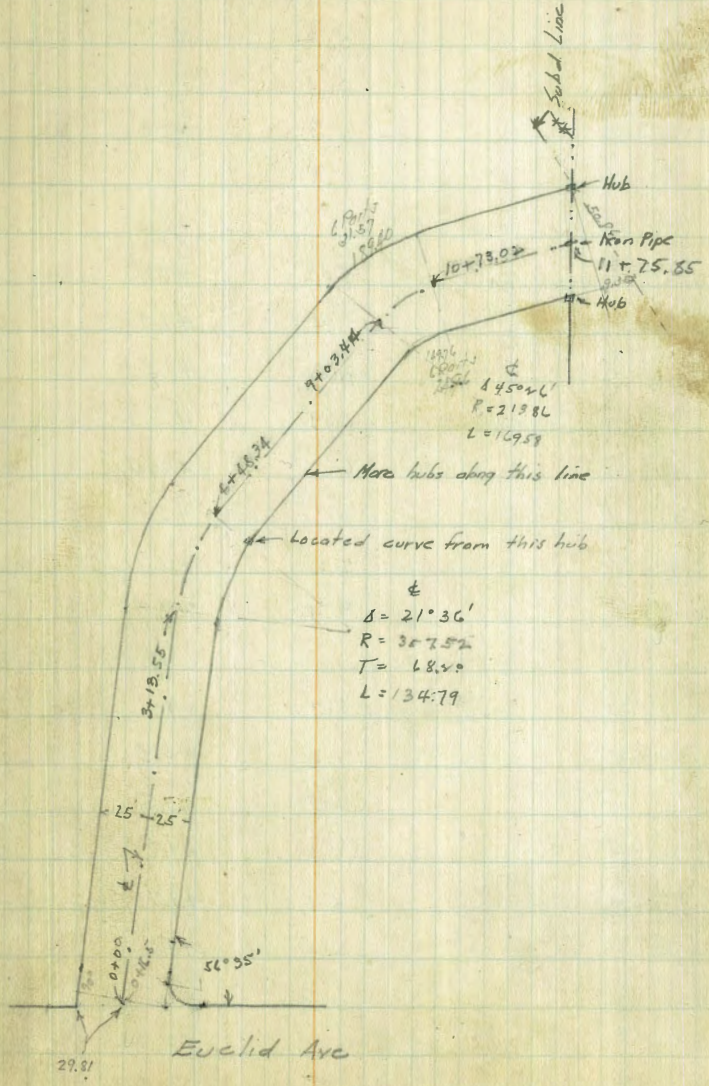
0+16.5 R/L to E

-5	7.0	41.1
SL	4.9	43.2
cb	5.3	42.8
K4	5.3	42.8
E	5.4	42.7
K4	5.4	42.7
cb	5.6	42.5
FS (Pence)	6.1	42.0
NL	6.8	41.3

Plotted  
11/16/27  
D.C. Milner.

0+41.5

NL	6.5	41.6
cb	5.5	42.6



0741.5

1/4	5.5	342.6
E	5.2	42.9
1/4	5.1	43.0
cb	4.5	43.3
PL S	4.0	44.1

1700

SPL	5.0	43.1
cb	6.4	41.7
1/4	6.3	41.8
E	5.9	42.2
1/4	6.1	42.0
HLcb	6.1	42.0
NL	7.2	40.9
+10	8.4	39.7

1725

-10	8.7	39.4
NL	7.8	40.3
cb	6.5	41.6
1/4	6.6	41.5
E	6.4	41.7
1/4	6.5	41.6
cb	6.6	41.5
SL	5.2	42.84

1750

SL	5.2	42.9
cb	6.6	41.5
1/4	7.0	41.1
E	6.8	41.3
1/4	7.0	41.1
cb	6.9	41.2
NL	9.1	39.0
+10	10.0	38.1

1775

-10	10.6	37.5
NL	9.1	39.0
cb	7.7	40.7
1/4	6.9	41.2
E	6.9	41.2
1/4	7.0	41.1
cb	6.5	41.6
SL	5.1	43.0

2400

SL	4.9	43.2
cb	5.6	42.6
1/4	6.7	41.7
E	6.7	41.4
1/4	7.0	41.1
cb	7.3	40.8
NL	7.6	40.5
+10	10.4	37.7

		348.05	
T.P	5.65	346.86	6.84
		2+25	341.21
-10		8.8	338.1
NL		6.9	40.0
cb		5.8	41.1
1/4		5.9	41.0
ϕ		5.6	41.3
1/4		5.7	41.5
cb		4.7	42.2
SL		4.0	42.9
		2+50	
SL		3.6	43.3
cb		5.1	41.8
1/4		5.6	41.3
ϕ		5.6	41.3
1/4		5.6	41.3
cb		6.0	40.9
NL		7.0	39.9
tio		8.9	38.0
		2+75	
-10		8.4	38.5
NL		5.9	41.0
cb		5.3	41.6
1/4		5.2	41.7
ϕ		5.2	41.7
1/4		5.5	41.4
cb		4.9	42.0

		346.86	
		=2+75 =	
		3+00	
SL		3.6	43.3
SL		3.2	43.7
cb		4.6	42.3
1/4		5.1	41.8
ϕ		5.0	41.9
1/4		5.0	41.9
cb		5.5	41.4
NL		7.5	39.4
tio		8.1	38.8
		=3+13.55 = Bc	
-10		7.9	39.0
NL		7.1	39.8
cb		6.0	40.9
1/4		5.2	41.7
ϕ		5.1	41.8
1/4		5.1	41.8
cb		5.1	41.8
SL		3.5	43.4
		=3+50 =	
SL		3.4	43.5
cb		5.3	41.6
1/4		5.1	41.8
ϕ		5.1	41.8
1/4		5.4	41.5
cb		6.4	40.5
NL		7.2	39.7
tio		8.2	38.7

= 3775 =

-10	5.2	33.8.7
NL	7.2	39.7
cb	5.9	41.0
1/4	6.0	40.9
φ	5.3	41.6
1/4	5.1	41.8
cb	4.7	42.2
SL	3.0	43.9

4700

SL	3.0	43.9
cb	4.5	42.4
1/4	4.7	42.2
φ	5.0	41.9
1/4	5.6	41.3
cb	6.1	40.8
NL	7.8	39.1
t10	9.1	37.8

= 4725 =

-10	9.3	37.6
NL	7.4	39.5
cb	5.2	41.7
1/4	5.2	41.7
φ	5.0	41.9
1/4	4.8	42.1
cb	4.3	42.6
SL	3.9	43.0

4+48.34 = FC

SL	2.7	344.2
cb	4.0	42.9
1/4	4.6	42.3
φ	4.7	42.2
1/4	5.1	41.8
cb	5.0	41.9
+3	5.2	41.7
NL	8.0	38.9
710	7.8	37.1

= 4775 =

-10	10.2	36.7
NL	8.9	38.0
cb	6.1	40.8
+4	5.2	41.7
1/4	4.8	42.1
φ	4.5	42.4
1/4	4.7	42.2
cb	4.2	42.7
SL	2.8	44.1

= 5700 =

SL	2.8	44.1
cb	4.4	42.5
1/4	4.6	42.3
φ	4.4	42.5

Lantana Dr No 346.86

= 5' + 00 =

1/4	4.8	42.1
cb	6.0	40.9
NL	8.5	38.4
+10	10.6	36.3

= 5' + 25 =

-10	9.8	37.1
NL	7.5	39.1
cb	5.4	41.5
1/4	4.7	42.2
♀	4.7	42.2
1/4	4.7	42.2
cb	4.5	42.4
SL	2.9	44.0

= 5' + 50 =

SL	3.0	43.9
cb	4.4	42.5
1/4	4.6	42.3
♀	4.3	42.6
1/4	4.4	42.5
cb	5.7	41.2
NL	7.6	39.3
+10	10.1	36.8

T.P.	5.05	347.53	4.38	342.48
T.P.	on walk	Norner House	4.817	
	2.82	341.91	3.41	344.12

346.94

600'S

-10 - dirt walk

F " "

cb

1/4

♀

1/4

+6

cb

X

X

+8

cb

1/4

♀

1/4

cb

F

+10

-10

F

cb

1/4

♀

50' wide  
10' cbs  
25' qts

11.4.27  
37  
5' 15"  
8' 15"  
Kanggy

10.1 336.8

79 39.0

59 41.0

49 42.0

49 42.0

48 42.1

49 42.0

38 43.1

32 43.7

150'S

32 43.7

38 43.1

45 42.4

48 42.1

49 42.0

52 41.7

57 41.2

79 39.0

91 37.8

700'S

84 38.5

71 39.3

65 40.4

49 42.0

47 42.2

56's on xld.  
Cone Walk  
2.94

123'S on xld.  
Cone Walk  
3.02



346.94

1/4	48	342.1
Cb	46	42.3
H	3.7	43.2
750.5		
H	3.9	43.0
15	1.1	42.8
Cb	4.9	42.0
1/4	4.5	42.4
2	4.8	42.1
1/4	5.0	41.9
Cb	6.2	40.7
F	7.4	39.5
+10	9.0	39.9
800.5		
-10	2.1	37.8
F	7.6	39.3
+5	6.8	40.1
Cb	5.5	41.4
1/4	5.6	41.3
2	5.3	41.6
1/4	5.7	41.5
Cb	5.2	41.7
H	4.6	42.3
850.5		
H	5.0	41.9
Cb	5.1	41.3
1/4	5.5	41.4

346.94

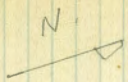
2	5.7	341.2
1/4	5.9	41.0
+3	5.9	41.0
Cb	6.9	40.0
F	8.0	38.9
+10	9.4	37.5
903.11 - P.C.R.		
-10	11.5	35.4
F	10.2	36.7
Cb	8.0	38.9
+5	7.1	39.8
1/4	6.8	40.1
2	6.7	40.2
1/4	6.7	40.2
Cb	6.6	40.3
+5	6.1	40.8
H	6.0	40.9
BM	11.58	343.06
Part 1		
31.57 500 F		
1496 500 H		
H	3.7	40.4
Cb	3.3	39.8
1/4	3.3	39.8
2	3.3	39.8
1/4	3.4	39.7
Cb	3.9	39.2

6 Packs 10 Cans

H 2496

F 3157

No 1 Pails  
#146  
S. of house 4879Cont. on Page 18



Bliss 8/10/27 X:sec's Fir Street. From Fern to  
160' East 28' Roadway 6' curbs 7' outs

SW Spike Fern Fir 2.09 263.72 261.68

N	3.5
cb	3.72
Gutter	4.18
1/4	4.16
ctr	4.28
1/4	4.59
Gutter	5.09
cb	4.77
S	4.5

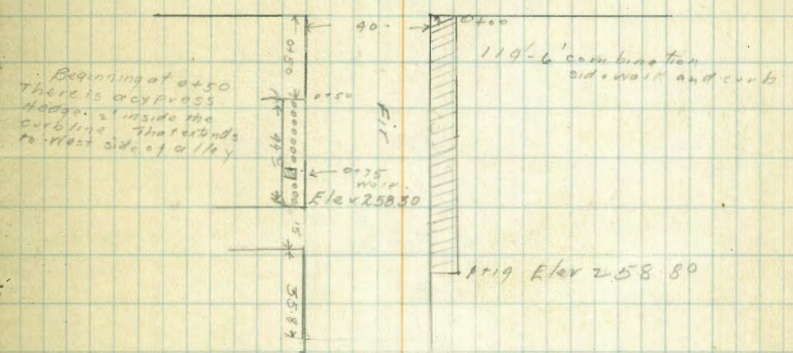
0+10

S	4.9
cb	4.9
1/4	5.0
ctr	4.4
1/4	4.3
Gut	4.0
cb	3.81
N	3.6

0+50

N	4.1
cb	4.22
Gut	4.7
1/4	5.1
ctr	5.2

Fern



1/4		5.2	
cb		5.4	
S		5.2	
	0+99 <sup>2</sup>		
S		6.2	
cb		5.9	
1/4		5.7	
d.		5.7	
1/4		5.6	
cut		5.1	
cb		4.8	
N		4.6	
	1+14 <sup>2</sup>		
N		5.3	
cb		5.7	
1/4		6.0	
ctr		6.2	
1/4		6.4	
cb		6.5	
S		6.5	
T.P.	119	259.35	5.51
			258.21
	1+25		
S		3.20	
cb		3.4	
1/4		3.5	

+2		3.5	
ctr		2.9	
1/4		2.7	
cb		2.9	
S.N		1.6	
	1+90		
N		2.2	
+1		4.5	
cb		4.7	
1/4		5.5	
ctr		5.4	
1/4		5.3	
cb		5.8	
S		5.2	
	1+50		
S		9.1	
cb		8.6	
1/4		7.6	
+2		7.3	
ctr		7.5	
+5		6.6	
1/4		6.5	
cb		6.5	
N		6.6	
	1+60		

25935

1460

N.			7.7	
cb.			8.0	
1/4			8.9	
t2			9.5	
ctr			9.0	
1/4			10.0	
cb.			10.8	
S.			10.8	
T.P.	538	263.88	0.85	258.50
BM			220	261.68

## Lantana Drive Cross Sections

56' wide  
10' CBS  
7.5 Qts

34306

11-4-27  
42

## Part 1.

34306 Get Ford From Page 38

F	51	338.0
+10	69	36.7

## Part 2

70	86	34.5
F	65	36.6
Cb	5.0	38.1
1/4	4.6	38.5
1/2	4.0	39.1
1/4	3.7	39.4
Cb	3.9	39.2
+5	3.2	39.9
H	3.2	39.9

## Part 3

H	37	39.4
Cb	40	39.1
+8	47	38.4
1/4	45	38.6
1/2	3.8	39.3
1/4	47	38.3
Cb	5.2	37.8
F	66	36.5
+10	82	34.9

## Part 4

+10	77	35.4
F	62	36.9

Cb	50	338.1
1/4	48	38.3
1/2	46	38.5
1/4	51	38.0
Cb	57	37.4
+3	45	38.6
H	42	38.9

## Part 5

H	49	38.2
+8	50	38.1
Cb	62	36.8
1/4	58	37.3
1/2	54	37.7
1/4	54	37.7
Cb	55	37.6
F	66	36.5
+10	79	35.2

## Part 6 = F.C.

+10	84	34.7
F	75	35.6
Cb	66	36.5
1/4	62	36.9
1/2	62	36.9
1/4	68	36.3
Cb	70	36.1
+2	57	37.4

343.06

H	4.5	337.6
	50 S of E.C.	
H	6.7	336.4
+8	7.2	335.9
Cb	8.0	335.1
+6	8.4	334.7
1/4	8.0	335.1
1/2	7.6	335.5
1/4	7.9	335.2
Cb	8.3	334.8
E	9.1	334.0
+10	9.9	333.2
	98.48 S = Sub. 4.02 E	
-10	11.8	331.3
E	10.6	332.5
Cb	9.8	333.3
1/4	9.1	334.0
1/2	8.8	334.3
1/4	8.8	334.3
Cb	9.2	333.9
+5	8.1	335.0
H	7.8	336.3
	98.48 S of E 107.77 S on H = S. L. Pt. Sub. 11012	
H	8.0	335.1
+6	8.5	334.6
Cb	9.5	333.6

343.06

1/4	9.0	334.1
1/2	9.0	334.1
1/4	9.0	333.8
Cb	9.9	333.2
E	10.6	332.5
+10	11.8	331.3
1/4	2.99	335.22
	N. L. Point Haven on H	1082
	21.02 S on E	332.24
-10		330.9
E		320
Cb		336
1/4		332
1/2		337
1/4		339
Cb		337
H		348
	25 S	
1/2		342
Cb		338
1/4		328
1/2		325
1/4		323
Cb		314
E		309
+10		293
	50 S	

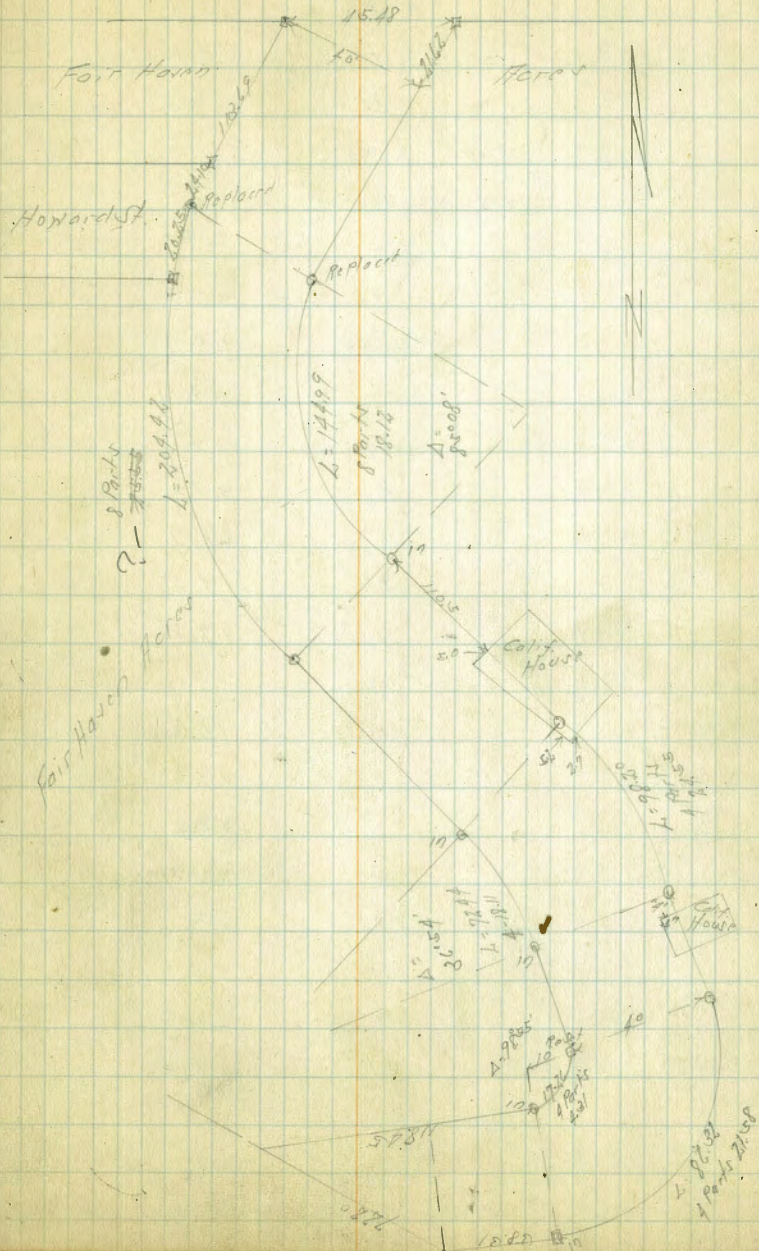
From Here  
to tide  
650  
720 ft

335.23

		45' wide 5' curb 750' L
-10	7.6	327.6
E	6.2	29.0
Cb	5.4	29.8
1/4	3.9	32.3
1/2	4.2	31.0
3/4	4.2	31.0
15	4.1	31.1
Cb	2.8	32.4
1/4	2.2	33.0
65.5		
1/4	3.1	32.0
Cb	3.6	31.6
15	5.9	29.3
1/4	5.4	29.8
1/2	5.5	29.7
3/4	5.2	30.0
Cb	7.4	27.8
E	8.4	26.8
110	9.5	25.7
100.5		
-10	15.2	20.0
E	13.8	21.4
Cb	8.9	26.3
1/4	11.4	22.8
1/2	9.3	25.9
3/4	9.2	26.0

## Re. Sub Blks 1-12 Fairmount

44



33523

+3		9.6	25.6
cb		8.0	27.2
H		6.4	28.8
TP	a.o.s.	32777	754
		32769	
	1137 S.M.L. Harvard From Harl.		
H		0.7	27.1
cb		2.6	25.2
1/4		6.5	24.3
2		3.6	24.2
+5		3.7	24.1
1/4		4.6	23.2
cb		6.9	20.9
F		8.7	19.1
+15		10.0	17.8
	120'S		
+5		11.6	16.2
F		9.8	18.6
cb		7.6	20.2
1/4		5.1	22.7
2		4.2	23.6
1/4		3.7	24.1
cb		3.1	24.7
H		2.6	25.2
	1378'S = BE.		
H		4.1	23.7
cb		4.1	23.4

Curve 1010  
8 Parts  
25.55 00N  
18/12/92

33777

11-5-27

45

1/4		5.2	32.26
2		5.8	22.0
1/4		6.6	21.2
cb		8.8	19.0
F		10.2	17.6
+20		14.8	13.0
	25.55'Soon 18/12'Soon = Part 1		
30		33.6	04.2
F		11.6	16.2
cb		8.6	19.2
+5		7.1	20.7
1/4		6.8	21.0
2		6.9	20.9
1/4		6.7	21.1
cb		6.3	21.5
+20 = Top Dry Wall		4.5	23.3
H		4.2	23.6
	Part 2		
H		4.7	22.9
+20 = Top Dry Wall		4.9	22.7
cb		7.1	20.7
1/4		7.1	20.7
2		7.2	20.6
1/4		7.2	20.6
+3		7.8	20.6
cb		11.5	16.3



32777

F	13.7	314.1
+15	19.2	308.6
+35	28.0	299.8

## Part 3

-25	23.0	304.8
F	13.8	14.0
Cb	12.0	15.8
1/4	8.2	19.6
+3	7.1	20.7
2	7.1	20.7
1/4	7.2	20.6
Cb	7.2	20.6
+3 - Top Dry Hall	4.9	22.9
H	4.6	23.2

## Part 4

H	4.8	23.0
+3 - Top Dry Hall	4.9	22.9
Cb	6.6	21.2
1/4	7.3	20.5
2	7.3	20.5
+5	7.5	20.3
1/4	8.8	19.0
Cb	12.1	15.7
F	14.2	13.6
+25	22.2	05.6

## Part 5

32777

46

-25	19.6	308.2
F	14.1	13.7
Cb	13.0	14.8
1/4	10.3	17.6
2	7.1	20.4
1/4	7.1	20.4
Cb	7.3	20.5
H	5.1	22.7

## Part 6

H	4.2	23.6
13	4.8	23.0
Cb	6.1	21.7
+3	7.3	20.5
1/4	7.7	20.1
2	7.5	20.3
1/4	9.5	18.3
Cb	12.1	15.7
F	13.6	12.2
+25	18.8	09.0

## Part 7

+25	21.2	06.6
F	14.8	13.0
+3	14.2	13.6
Cb	12.1	15.2
1/4	10.2	17.6
2	8.1	19.4

327.77

1/4	8.0	319.8
cb	7.8	20.0
N	5.2	22.6

Part 8 - F.C.

N	9.3	18.5
cb	9.6	18.2
1/4	9.3	18.5
2	9.7	18.1
1/4	12.2	15.5
cb	13.6	14.2
F	14.1	13.2
+20	19.3	88.5
TP	all	316.68
		11.75
		316.02

RES of F.C.

-20	11.1	85.6
F	5.8	10.9
cb	4.6	12.1
1/4	3.9	12.8
2	1.6	15.1
1/4	0.2	16.5
cb	0.8	15.9
N	1.0	15.7

50.5

N	4.1	12.6
cb	4.1	12.6
1/4	3.4	13.3

316.68

2	4.2	312.5
1/4	5.6	11.1
cb	6.7	10.0
F	7.1	89.6
+15	10.0	86.7

75.5

-15	12.2	84.5
F	9.9	86.8
cb	8.7	88.0
1/4	8.1	88.6
2	6.6	10.1
1/4	6.7	10.0
cb	7.2	89.5
N	7.5	89.2

100.5

N	10.0	86.7
cb	10.5	86.2
1/4	10.5	86.2
2	10.0	86.7
1/4	9.8	86.9
cb	11.8	84.9
F	12.6	84.1
+15	16.0	300.7

129.5 = BC

F Under House	12.3	84.4
cb	11.3	85.4

Correct late  
4 Parts  
12.11 on N  
27.55 on E

316.68

304.10

+5		14.6	302.1
Cb on Wood Porch		13.05	03.33
1/4		14.6	02.1
1/2		14.9	01.8
1/4		14.7	02.0
Cb		13.9	02.8
+3		13.0	04.7
N		11.8	04.9
TP	0.29	304.10	138.7
		18.115	303.81
	Part 1 - 24555 cost of EC		
N		11	03.0
Cb		7.1	02.0
+5		4.4	299.7
1/4		5.2	98.9
+3		4.6	99.5
1/2		4.9	99.2
1/4		5.0	99.1
Cb		6.7	97.4
E		8.3	95.8
+20		13.3	90.8
	Part 2		
-15		15.4	88.7
E		11.8	93.3
Cb		10.3	93.8
1/4		8.1	96.0
1/2		8.0	96.1

1/4		7.6	296.5
+5		5.3	298.8
Cb		4.7	299.4
N		3.3	300.8
	Part 3		
N		5.5	298.6
Cb		6.7	97.4
+2		7.3	96.8
+5		9.8	94.3
1/4		10.5	93.6
1/2		10.7	93.4
1/4		10.8	93.3
Cb		14.0	90.1
E		16.0	88.1
11.5		18.6	85.5
TP	5.54	297.54	12.10
			292.00
	Part 4 - EC		
+15		15.2	82.3
E		11.7	85.8
Cb		10.9	86.6
1/4		7.3	90.2
1/2		7.0	90.5
1/4		6.5	91.0
Cb		2.4	95.1
N		1.2	96.2
	25th of EC		

Part 1 - 24555 cost of EC

Part 3

Part 4 - EC

10'S cost Wood Porch 7.19 = 290.41

277.51

49

285.53

N		4.5	293.0	♀	31	282.4	
Cb		5.8	91.7	+15	30	82.5	
1/4		9.2	88.3	1/4	40	81.5	
♀		10.6	86.9	+15	44	81.1	
1/4		11.0	86.5	Cb	55	80.0	
+15		12.2	85.3	♀	66	78.9	
Cb		14.0	83.5	+15	10.9	74.6	
F		14.8	82.7				
+10		15.8	81.7	-15	13.1	73.4	
+15		18.0	79.5	F	7.3	78.2	
	500 of F.c			Cb	5.6	79.9	
-15		20.4	77.1	+15	4.9	80.9	
F		16.8	80.7	1/4	5.1	80.4	
Cb		16.1	81.4	♀	5.0	80.5	
1/4		13.2	84.3	1/4	4.5	81.0	
+3		13.8	84.9	Cb	3.0	82.5	
♀		13.8	84.7	N	1.8	83.7	
1/4		12.9	84.6				
Cb		9.9	87.6				
N		8.8	88.7	N	2.4	83.3	
TP	190	286.81	12.62	284.91	1/4	6.0	79.5
BN	503	285.53	6.31	280.50	♀	6.2	79.2
		69.555 = BCP			1/4	6.2	78.7
N		0.8	84.7	Cur + 10 late 4 Part 1	7.6	77.9	
Cb		1.7	83.8	1.310 2N	8.0	77.5	
1/4		3.6	81.9	21.58	10.9	74.6	

1.315 00N  
21.515 005 = Part 1

Part 2

28553

28553

Part 3

-15	12.2	273.3
F	10.6	74.9
Cb	8.9	76.6
1/4	7.6	77.9
2	7.7	77.8
1/4	7.2	78.3
Cb	3.9	81.6
H	2.8	82.7

Cb		6.8	278.7
H		5.2	80.3
TP	119	274.30	12.22
		50.21	273.11
H		7.8	72.5
Cb		3.6	70.7
1/4		6.0	68.3
2		6.2	68.1
1/4		8.7	65.6

Part 4 - EC - st. ends at this point.

NH	2.8	82.7
Cb	7.7	81.1
1/4	7.6	77.9
2	8.5	77.0
1/4	8.8	76.7
Cb	11.8	74.3
SF	13.7	71.8
+20	19.5	66.0

See Fairhaven Acres Map D.C.M.

Cb		10.7	63.6
S		11.8	62.5
1/6		14.5	59.8
1/5		21.7	52.6
1/30		21.4	52.9
		58.31' N = S.L. Tract 025	
30		20.2	54.1
15		21.2	53.1
S		14.7	59.6

25' N of EC

-20	27.3	58.2
-15	22.5	63.0
S	17.3	68.2
Cb	14.8	70.7
1/4	11.9	73.6
2	10.2	74.7
1/4	10.0	75.5

Cb		12.5	61.8
1/4		10.7	63.6
2		8.4	65.9
1/4		7.5	66.8
Cb		6.5	67.8
H		5.0	69.3
		118.45' N on N	
		58.31' N on S.L. Tract	
		Taken on Diagonal 7720 135494	
		15.2	59.1

902 96

Lantana Drive

51

27400

cb			16.7	259.4
1/4			14.9	59.4
2			14.9	59.4
1/4			14.1	59.9
cb			15.4	58.9
S			14.7	59.6
TP	1246	284.31	1.15	271.85
TP	1243	296.64	0.10	284.21
TP	1307	309.66	0.05	296.59
TP	1310	322.59	0.17	309.49
TP	1248	334.93	0.14	322.45
TP	1053	342.57	2.89	332.04
TP	125	346.54	0.28	342.19
TP	305	343.21	6.38	340.16
BM			2.54	340.67

NIM BP

4471 x Field  
340.68

Colton St. Cross Sections  
3rd St + 1st St.

80' wide  
14 Cbs  
13 Qts

43.23  
43.2

57  
11.7.27  
5.000  
91.55  
Kamoy  
1/4 + 2.5 Top Rail  
7.43

BM	9.81	43.23	33.12	SE Mon Colton St 31 <sup>st</sup> St.	N	7.6	35.6
		EL 32 <sup>nd</sup> St.		32 <sup>nd</sup> St 60' wide 10 Cbs 10 Qts	N	7.6	35.6
S		43.2	9.9		Cb	7.8	35.4
Cb			9.4		1/4	8.2	35.0
1/4			8.8		1/4	8.5	34.7
1/2			8.7		1/4	9.0	34.2
Corp. Walk			8.20		Cb	9.2	34.0
1/4			8.4		S	9.6	33.6
Cb			7.9				
N			7.6		S	9.1	33.6
		FCb			Cb	9.2	34.0
N			8.1		1/4	8.8	34.4
Cb			8.4		1/4	8.6	34.6
1/4			8.7		1/4	8.1	35.1
1/2			9.1		Cb	7.8	35.4
1/4			9.5		N	7.3	35.9
Cb			9.8				
S			10.5		N	7.5	35.7
		1/4			Cb	7.7	35.5
S			9.6		1/4	8.0	35.2
Cb			9.3		1/4	8.2	35.0
1/4			9.0		1/4	8.5	34.7
1/2			8.6		Cb	8.9	34.3
1/4			8.2		S	9.6	33.6
Cb			7.9				

1/4 + 2.5 E Rail  
0.75  
9.11

7' W of N 1/4

N Cb

43.23

S	8.3	34.9
Cb	8.6	34.6
1/4	8.9	34.9
2/8	8.0	35.2
1/4	8.0	35.2
Cb	7.7	35.8
H	6.1	37.1
N.L. 3200' N		
H	6.1	37.1 ✓
Cb	6.2	37.0
1/4	7.3	35.9
2/8	7.2	36.0 ✓
1/4	7.6	35.6
Cb	7.8	35.4
S	8.2	35.0 ✓
1.5' N of N.L. of 3200'		
S	7.7	35.5 ✓
Cb	7.2	36.0
1/4	6.8	36.4
1/4	7.2	36.0
2/8	6.5	36.7 ✓
1/4	6.3	36.9
1/8	5.9	37.3
Cb	4.6	38.6
H	4.0	39.2 ✓

50' N

43.2

H	3.1	39.6
Cb	4.1	38.6
1/4	5.4	37.8
2/8	6.0	37.2
1/4	6.2	37.0 ✓
2/8	6.9	36.3
1/4	6.3	36.9
Cb	6.8	36.4
S	7.4	35.8 ✓
100' N		
S	7.2	36.0 ✓
Cb	5.9	37.3
1/4	5.7	37.5
2/8	5.6	37.6 ✓
1/4	4.9	38.3
Cb	4.0	39.2
H	3.2	40.0
150' N		
H	3.2	39.9
Cb	4.0	39.2
1/4	4.8	38.4
2/8	5.2	38.0 ✓
1/4	5.4	37.8
Cb	5.6	37.6
S	5.9	37.3 ✓

200' N

11' N - Palm Tree  
13' N of S.L.125' N - Palm  
13' N of S.L.152.5' N on S  
Brick Walk  
6' 6"165' N - Palm  
18' N of S.L.198' N on S  
Conc. Walk  
5' 4"



4323  
43.2

4323

S	54	37.8 ✓	
Cb	52	38.0	232 W on N
1/4	49	38.3	Conc Walk 323
S	46	38.6 ✓	
1/4	44	38.8	334 W on S Brick Walk
Cb	36	39.6	637
N	29	40.3 ✓	
250' W			
N	35	39.7 ✓	245 W - long side 12 W of S
Cb	41	39.1	
1/4	47	38.5	
S	52	38.0 ✓	180 W on S Brick Walk
1/4	54	37.8	650
Cb	57	37.5	
S	62	37.0 ✓	
300' W			
S	72	36.0 ✓	268 W on N Conc Walk 370
Cb	68	36.4	
1/4	64	36.8	
S	60	37.2 ✓	
1/4	55	37.7	316 W on N Conc Walk
Cb	48	38.9	481
N	47	38.5 ✓	
350' W			
N	50	38.2 ✓	351 W on N Conc Walk 498
Cb	57	37.5	

1/4	63	36.9	
S	66	36.6 ✓	
1/4	71	36.1	356 W on S Conc Walk 803
Cb	75	35.7	
S	79	35.3 ✓	
400' W			
S	85	34.7 ✓	
Cb	79	35.3	
1/4	73	35.9	
S	69	36.3 ✓	
1/4	65	36.7	382 W on N Conc Walk 432
Cb	57	37.5	
N	48	38.4 ✓	
TP	5.30	41.71	1.86
150' W			
N	43	38.4 ✓	493 W on S Conc Walk 768
Cb	51	36.6	
1/4	59	35.8	
S	62	35.5 ✓	
1/4	67	35.0	
Cb	68	34.9	
S	77	34.0 ✓	
500' W			
S	78	33.9 ✓	
Cb	73	34.4	
1/4	71	34.6	

4171

1/2	6.8	34.9 ✓	
1/4	6.6	35.1	496 N. 6. 27. 6
Cb	6.0	35.7	Case. 10/14 199
N	5.0	36.7	317 N. 10. 14/14 10 Cas 12914
	5.30 N = F. 4. 31/14		
N	5.0	36.7 ✓	538 N = 19/107 13 1/2 of 26.
Cb	6.4	35.3	
1/4	6.6	35.1	
1/2	6.6	35.1 ✓	
1/4	7.1	34.6	
Cb	7.8	33.3	
S	8.0	33.7 ✓	
	FCb		
S	8.4	33.3	
Cb	7.7	34.0	
1/4	7.2	34.5	
1/2	6.6	35.1	
1/4	6.1	35.6	
Cb	6.2	35.5	
N	5.7	36.0	
	1/4		
N	5.5	36.2	
Cb	5.8	35.3	
1/4	6.0	35.7	
1/2	6.7	35.0	
1/4	7.5	34.2	

4171

Cb	8.2	33.5	
S	8.7	33.0	
	1/2 31/14		
N	8.6	33.1	
Cb	8.0	33.7	
1/4	7.3	34.4	
1/2	6.7	35.0	
1/4	6.3	35.5	
Cb	6.0	35.7	
N	5.6	36.1	
	N 1/4		
N	5.5	36.2	
Cb	6.1	35.6	
1/4	6.5	35.2	
1/2	6.9	34.8	
1/4	7.6	34.1	
Cb	8.1	33.6	
S	8.7	33.0	
	N Cb		
N	8.9	32.8	
Cb	8.1	33.6	
1/4	7.6	34.1	
1/2	7.0	34.7	
1/4	6.5	35.2	
Cb	6.2	35.5	
N	5.6	36.1	

Cotton

41.71

41.6 31<sup>st</sup> 51

11	59	35.8
66	66	35.1
11	66	35.1
2	73	34.4
14	80	33.7
66	82	33.5
5	88	32.9

56

31<sup>st</sup> St. Gass Sections  
Colton to Main

41.71 31.50  
N.L. Colton

F	50	36.7 ✓
Cb	57	36.0
1/4	55	36.2
2	56	36.1
1/4	55	36.2
Cb	56	36.1
N	59	35.8

50 N of N.L. Colton

N	44	37.3
Cb	42	37.5
1/4	42	37.5
2	41	37.6
1/4	41	37.6
Cb	39	37.8
F	36	38.1 ✓

100 N

F	25	38.9 ✓
Cb	30	38.7
1/4	32	38.5
2	32	38.5
1/4	36	38.1
Cb	35	38.2
N	34	38.3

150 N

N	16	40.1
---	----	------

72 N on T.L.  
Conceptual  
29

41.71

Cb	15	40.2
1/4	22	39.5
2 = N.H.	200	39.65
1/4	15	40.2
Cb	14	40.3
F	12	40.5 ✓
TP	714	4800
		0.95
		1086

200 N

F	56	42.9 ✓
Cb	61	41.9
1/4	65	41.5
2	66	41.4
1/4	67	41.3
Cb	65	41.5
N	63	41.7

225 N

N	57	42.3
Cb	59	42.1
1/4	60	42.0
2	62	41.8
1/4	60	42.0
Cb	55	42.5
25	42	43.8
F	43	43.7 ✓

250 N

F	34	44.6 ✓
---	----	--------

48.00

15	3.4	44.6
cb	4.1	43.6
1/4	5.3	42.7
2	5.6	42.4
1/4	5.5	42.5
cb	5.5	42.5
W	5.1	42.9

275.11

11	4.8	43.2
cb	4.9	43.1
1/4	5.0	43.0
2	4.9	43.1
1/4	4.8	43.2
17	4.8	43.2
18	3.8	44.2
cb	3.7	44.3
F	2.9	45.1 ✓

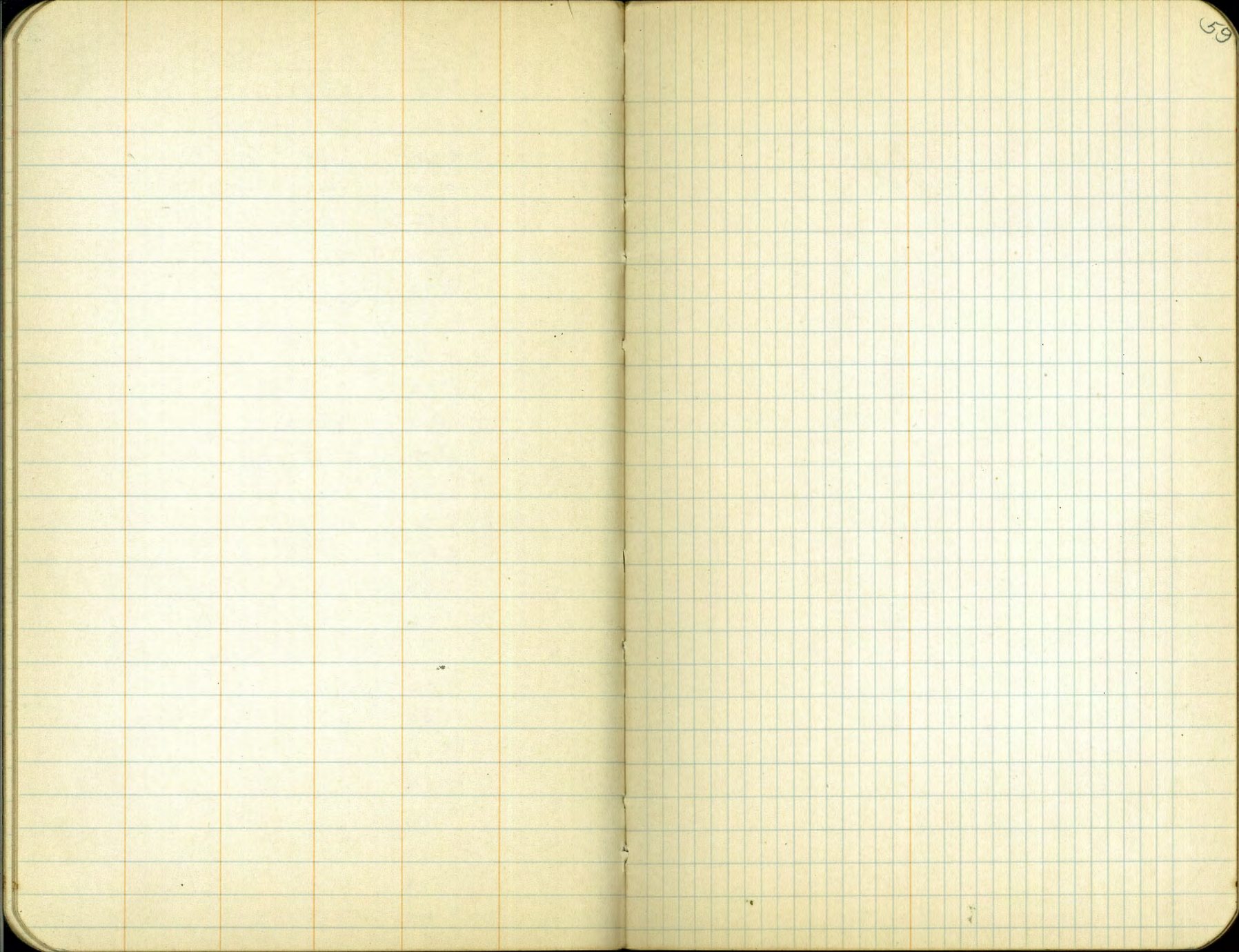
Good = SL Main NY

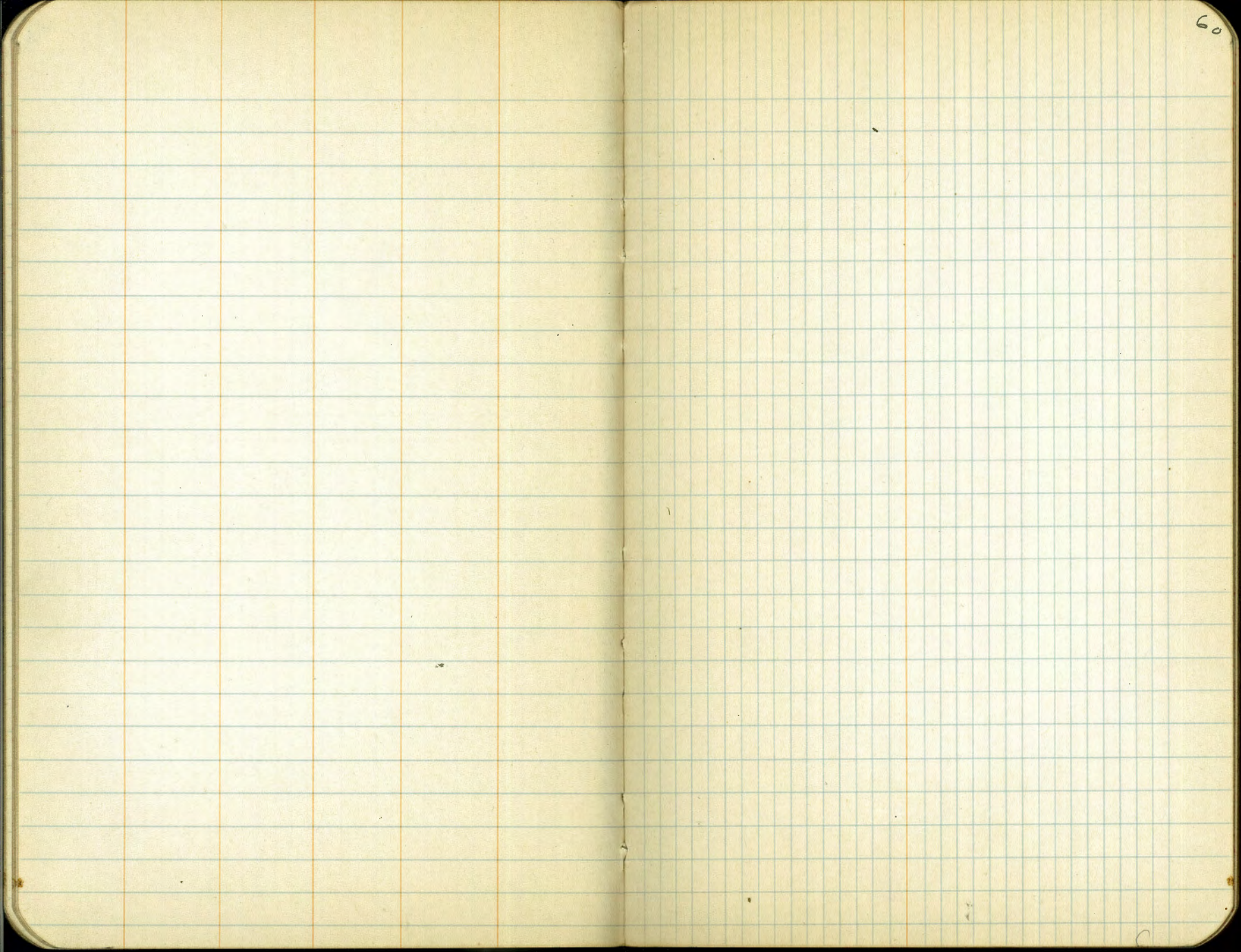
E	3.9	44.1	Note SW 155
cb	4.13	43.81	Carb. P. 100 110
Gutter - Paving	4.70	43.30	
1/4 "	4.54	43.46	
2 "	4.33	43.67	
1/4 "	4.41	43.59	
Gutter - Top Ck & Paving	4.49	43.51	
11	4.3	43.7	

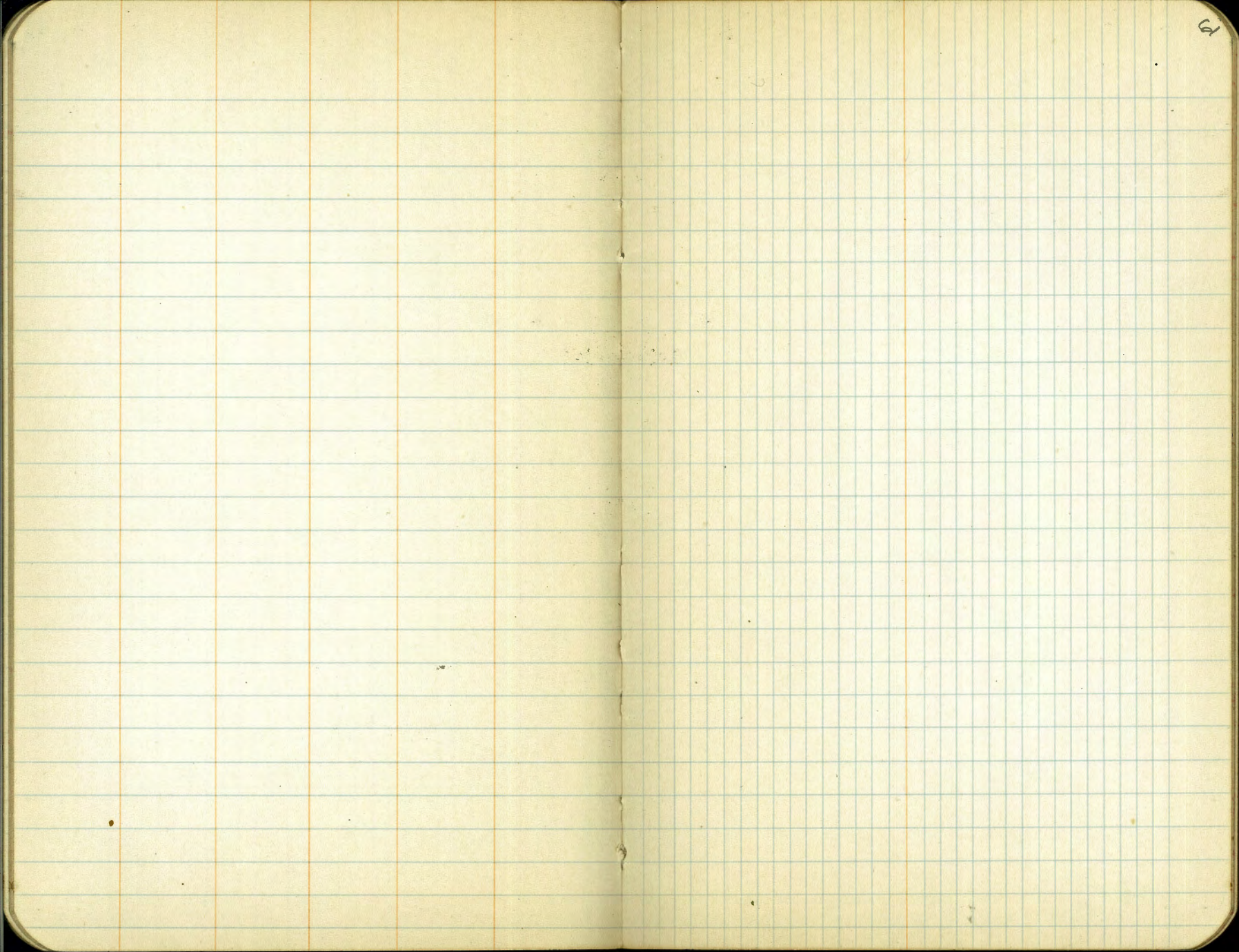
48.00

BN	3.04	44.96
TP	2.31	40.87
	9.43	38.56
BN	7.47	33.40

NW 8P  
Main 2.31  
45.05  
SE 11/17  
Cotton 1.31  
33.48

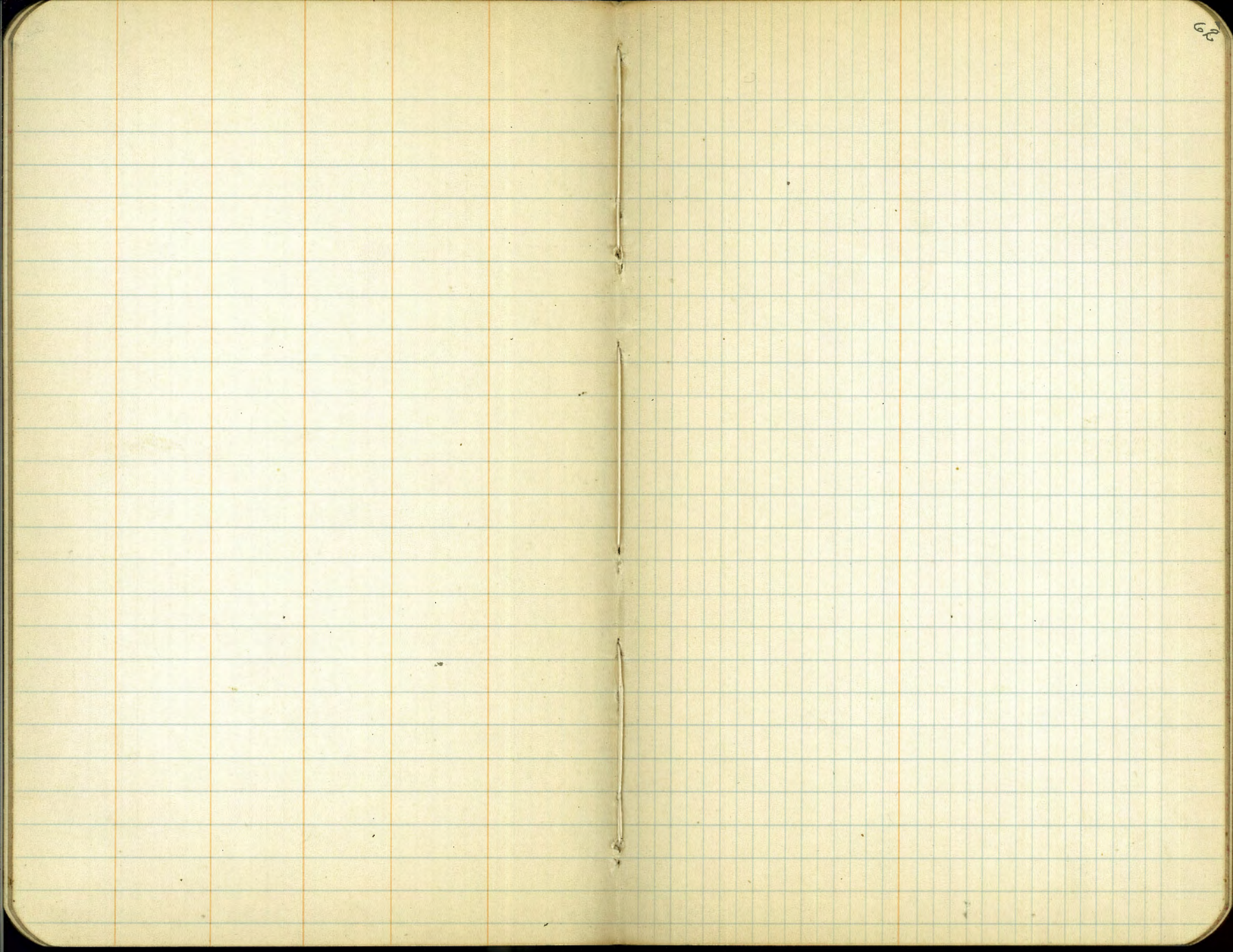


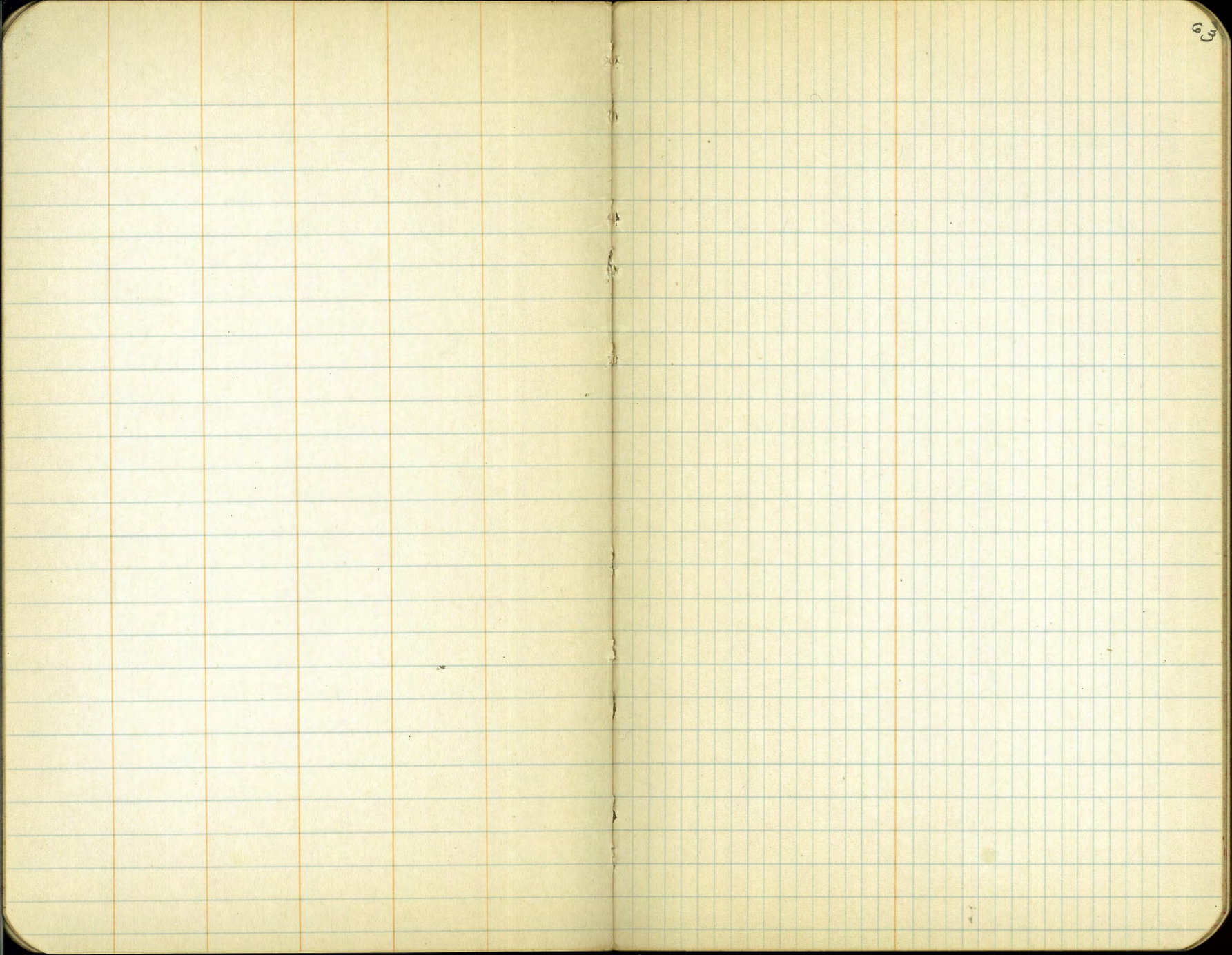




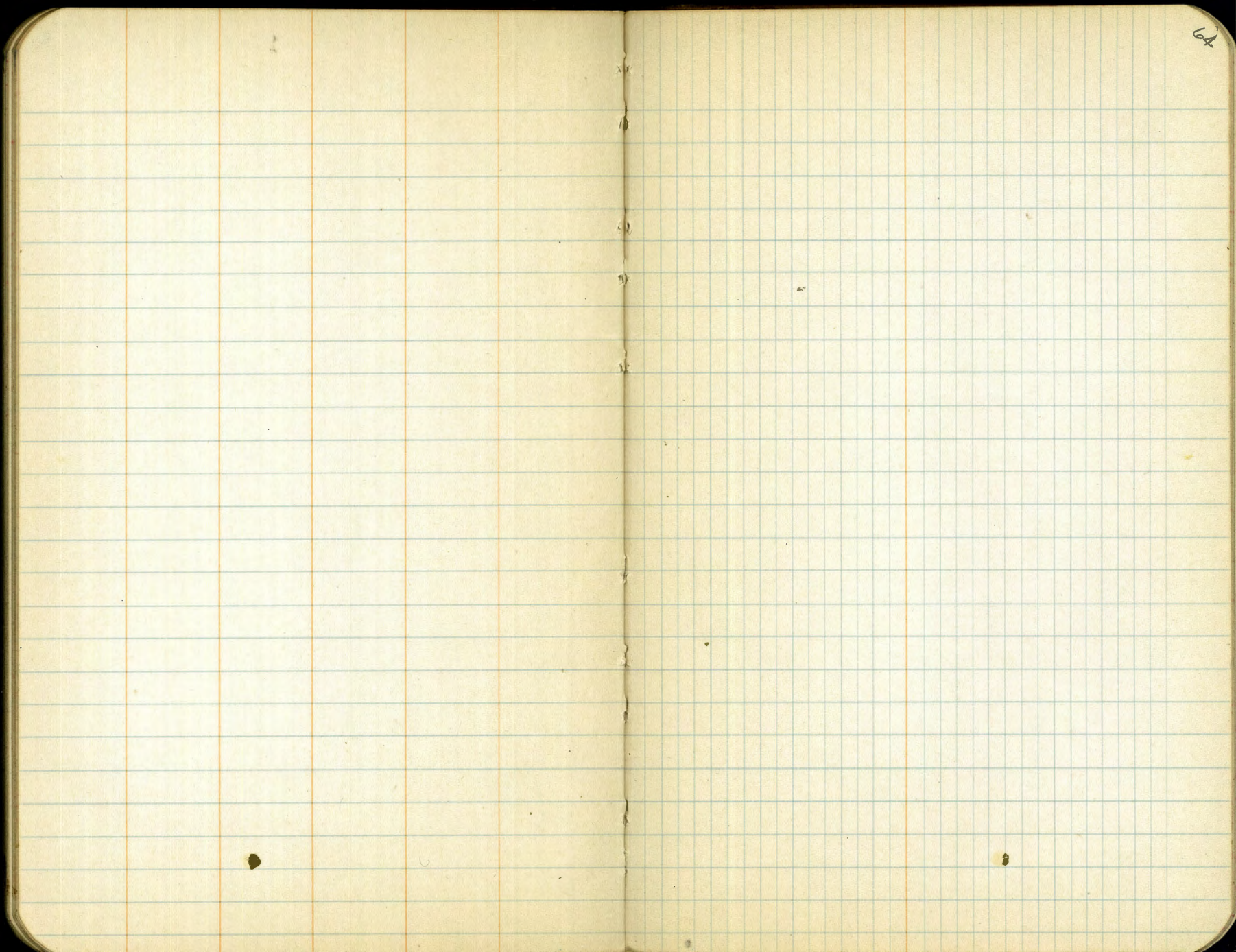
62



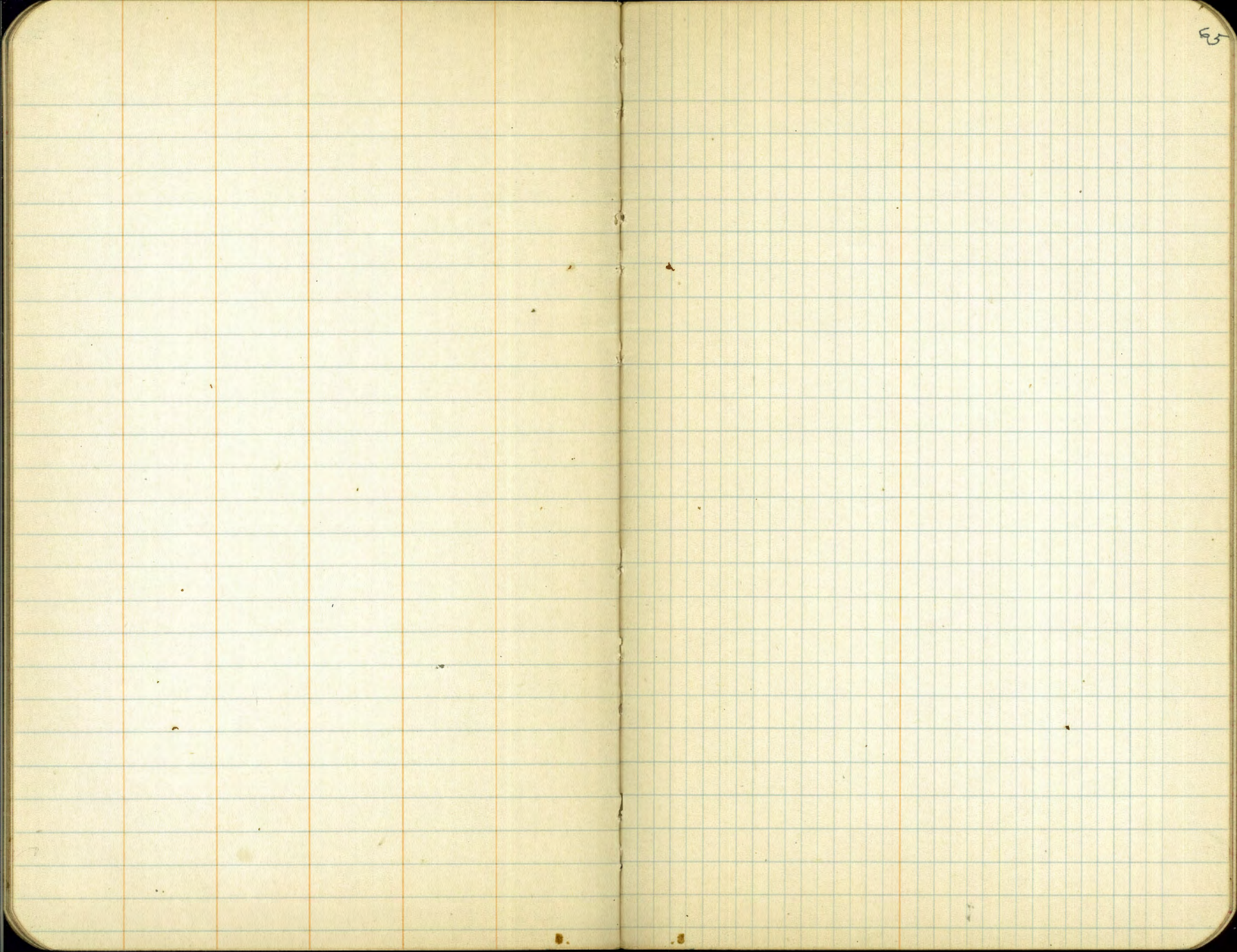




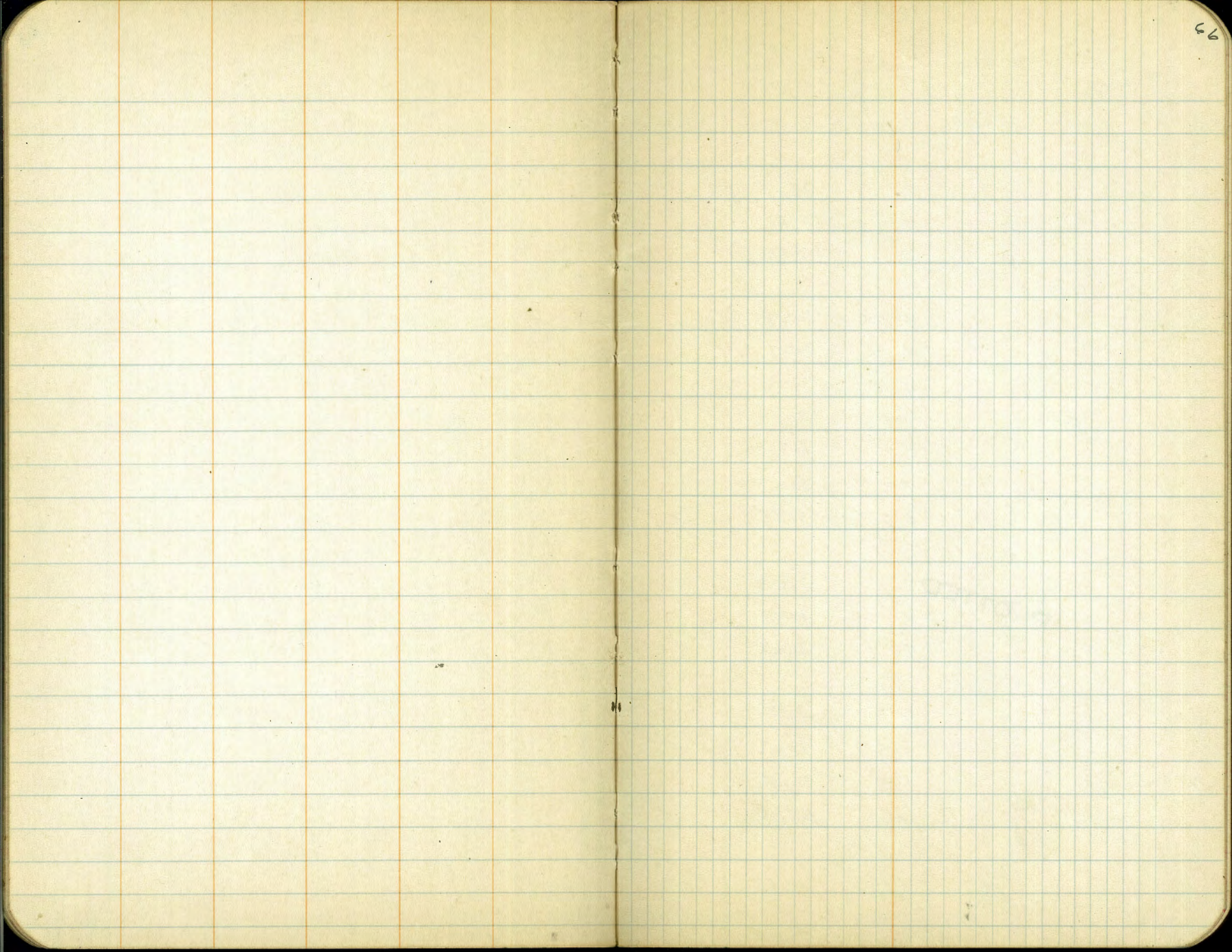
63



64



65



Bliss  
Isa bell  
Morgan  
10/27/47

X Sections Alley Block 77 Park Villas  
between Arnoldy Arizona Univ to Wightman

67

BM 0.55 306.96 306.91

0+00  
Staircase

E 4.91 302.05 ✓

C 5.15 301.81 ✓

N 5.15 301.81 ✓

0+10

W 4.2 302.8 ✓

C 4.3 302.7 ✓

E 4.4 302.6 ✓

0+25

E 3.9 303.1 ✓

E 4.3 302.7 ✓

W 4.2 302.8 ✓

0+45

W 4.7 302.3 ✓

E 4.7 302.3 ✓

E 4.7 302.3 ✓

**PLOTTED**  
10/11/47, MB

0+65

E 5.3 301.7 ✓

C 5.5 301.5 ✓

W 5.2 301.8 ✓

0+79 Garage Floor Westside  
Concrete  
Flush with Prop. 4.67 302.19 ✓

0+79 Garage Floor Eastside  
Concrete  
Flush with Prop. 5.39 301.57 ✓

306.96

0+85

W		5.8	301.2	✓
P		5.9	301.1	✓
E		5.9	301.1	✓
	0+97 Concrete Steps	5.57	301.39	✓

1.0 Back East Side

1+00

E		6.8	300.2	✓	
P		6.6	300.4	✓	
W		6.7	300.4	✓	
T.P.	2.18	302.21	6.93	300.03	✓

2:7. Fast Side  
Back to top.

Garage	1+10 Concrete floor	2.35	299.86	✓
--------	---------------------	------	--------	---

10' Back West Side

Garage	1+20 Concrete Floor	2.58	299.63	✓
--------	---------------------	------	--------	---

W	1+20	2.3	299.9	✓
---	------	-----	-------	---

PLOTTED  
1/11/77 NPK

E		2.6	299.6	✓
---	--	-----	-------	---

E		2.6	299.6	✓
---	--	-----	-------	---

Garage	1+20 Concrete floor East side	2.00	300.21	✓
--------	-------------------------------	------	--------	---

11.0 Back

1+39

E		3.1	299.1	✓
---	--	-----	-------	---

P		2.9	299.3	✓
---	--	-----	-------	---

+9		2.9	299.3	✓
----	--	-----	-------	---

W		2.6	299.6	✓
---	--	-----	-------	---

1+97

W		3.3	298.9	✓
---	--	-----	-------	---

P		3.5	298.7	✓
---	--	-----	-------	---

E		3.6	298.6	✓
---	--	-----	-------	---

302.21

Gauge      BACK 10.6 east side  
 1+60.      concrete  
             lip              3.67      298.54 ✓

17.60

E                              9.2      298.0 ✓  
 S                              9.1      298.1 ✓  
 W                              3.9      298.3 ✓

17.76

W                              9.7      297.5 ✓  
 S                              9.5      297.7 ✓  
 E                              7.6      297.6 ✓

17.82

E                              9.8      297.4 ✓  
 S                              5.0      297.2 ✓  
 +3.5                              9.9      297.3 ✓  
 W                              9.9      297.8 ✓

PLOTTED  
 10/11/22/1966

Garageon Concrete 1+93.      4.05      298.16 ✓

floor is 90' chicken Ho use from 1+60 to 2+00. at in alley  
 2+00

W                              5.3      296.9 ✓  
 S                              5.5      296.7 ✓  
 E                              5.2      297.0 ✓

2+20

E                              5.3      296.9 ✓  
 +2                              5.7      296.5 ✓  
 S                              5.8      296.4 ✓  
 W                              5.9      296.3 ✓



302.21

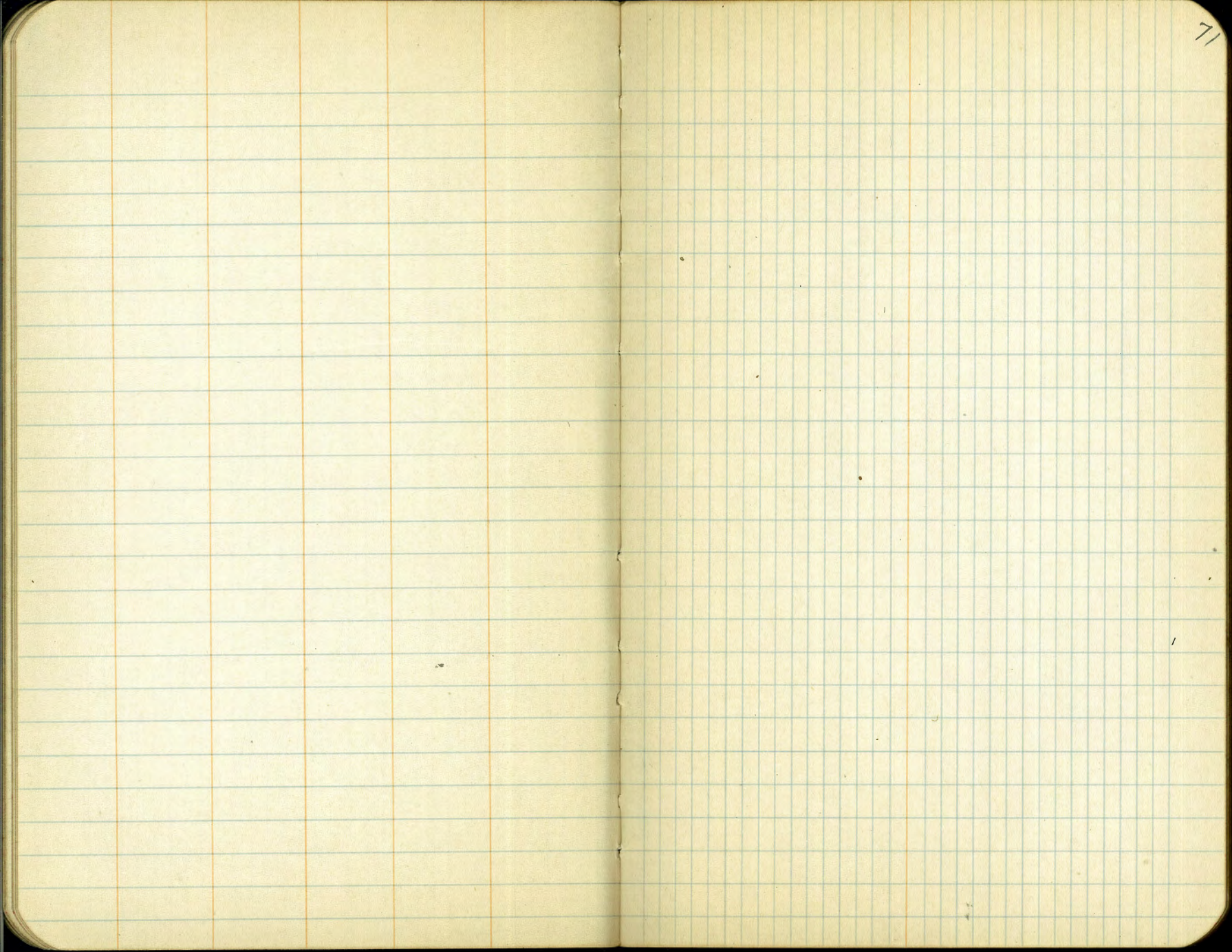
2745

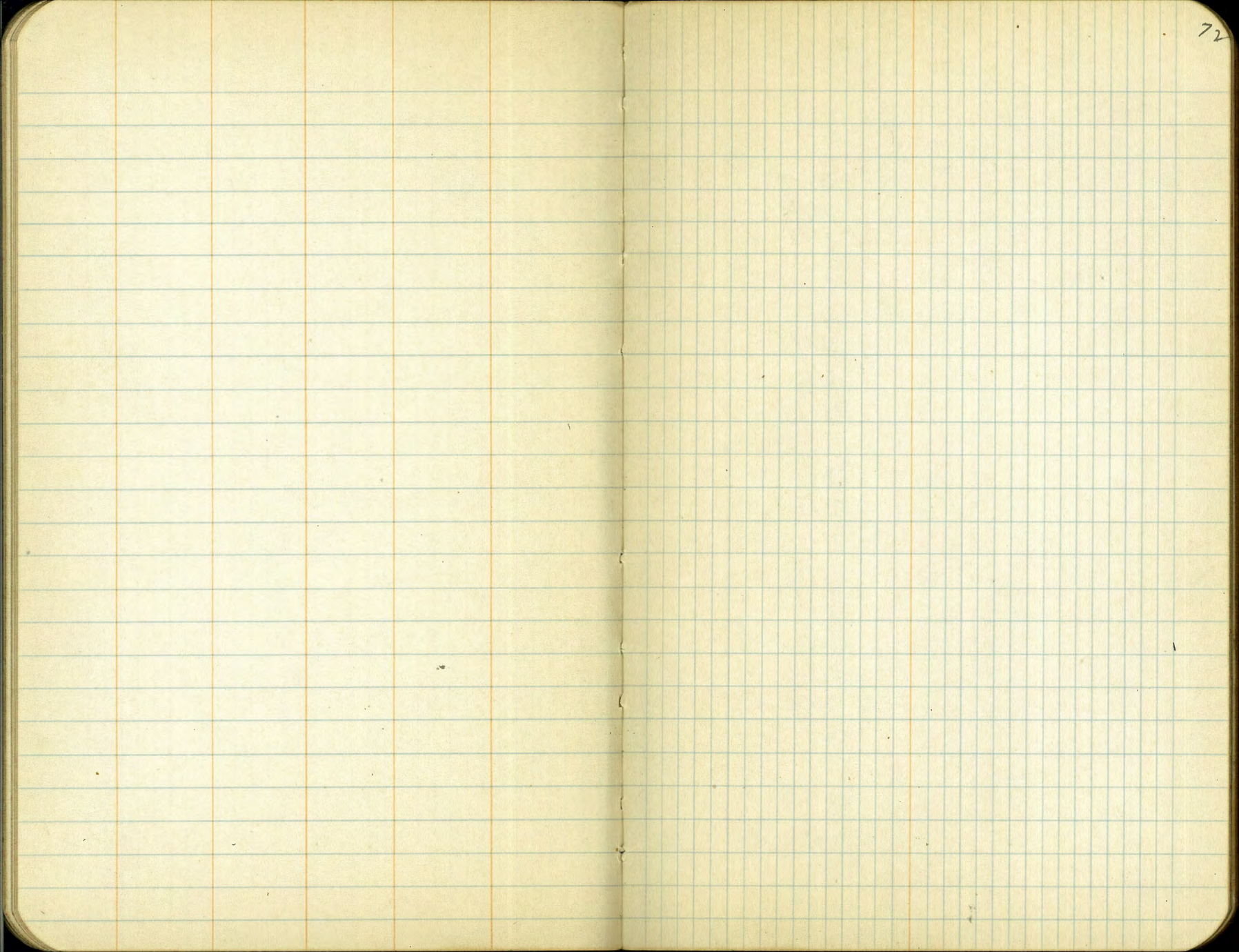
W		6.1	2961	✓
+5		6.2	2960	
±		6.2	2960	✓
E		5.7	2965	

2150 N Line Wittman

Ob.		6.89	29537	✓
Gutter		7.14	29507	✓
±		7.97	29424	✓
Gutter		7.17	29504	
Corb		7.08	29513	
TP.	5.96	307.15	1.02	301.19
B.M.		0.74	306.91	✓

PLOTTED  
 10/16/77  
 NAG





X sections Alley Block 26  
 University Hts  
 Between Adams & Madison  
 Campus North

BM	369	359.65	355.96	
		<u>359.2</u>		
E. Top Curb		4.99	354.2	✓
Ch		5.04	354.2	✓
West Top Curb		5.12	354.6	✓
S. Prop Adams	0+00			
W. Top Curb		5.09	354.6	✓
Gulch		5.2	354.5	✓
Ch		5.0	354.7	✓
East		5.1	354.6	✓
	0+50			
E		5.6	354.1	✓
Ch		5.4	354.3	✓
W		5.00	354.7	✓
Garage	Concrete Lip			
	N. End 0+53	5.09	354.6	✓
	Ch on Prop	5.06	354.6	✓
	South End Lip path	5.08	354.6	✓
Concrete Driveway	0+69 to 0+77	5.03	354.1	✓
	0+77	5.10	354.8	✓
Garage	0+74 to North End	4.53	355.2	✓
	0+88 S. End	4.55	355.1	✓
	1+00			
-2.4	on concrete side	5.97	353.7	✓
W	Walk	5.8	353.9	✓
Ch		5.3	354.4	✓
E		5.3	354.4	✓

3.3 in Alley West side

3.6 in Alley West side

5.2 Back on East side

35965 5597

E	1+14	5.9	3543	✓
ctr		5.3	3544	✓
+7		5.7	3540	✓
W		6.0	3537	✓
-24	concrete walk	6.10	3556	✓
Garage	1+16 on East	5.3	3544	✓
Garage	1+21 1/2 on East	5.33	3544	✓
	9+29 26 Back Concrete to P...	5.33	3546	✓
T.P.	4.60	35893 5.32	359.33	
Garage	1+20 to on West	5.86	3590	✓
	1+28 Concrete on Floor Prop	5.86	3590	✓
	1+39			
W		5.9	3530	✓
+45		5.1	3538	✓
ctr		4.9	3540	✓
E		4.8	3541	✓
	1+75			
E		5.0	3539	✓
ctr		5.2	3537	✓
+5		5.2	3537	✓
W		6.2	3546	✓
	2+00			
W		6.6	3543	✓
+3		6.4	3545	✓
+5		5.3	3536	✓

358.93 5589

ctr		5.2	3537	✓
E		5.1	3538	✓
	2+18			
E		5.3	3536	✓
ctr		5.3	3536	✓
+5		5.4	3535	✓
+7		6.4	3545	✓
W		6.5	3544	✓
	2+19			
W		5.9	3535	✓
ctr		5.3	3536	✓
E		5.3	3536	✓
	2+50			
E		5.5	3534	✓
ctr		5.5	3534	✓
W		5.4	3535	✓
TP	46	357.98		
Garage	2+87 on East	5.57	353.36	
		3580	3534	✓
	3+00			
W		4.7	3533	✓
ctr		4.7	3533	✓
E		4.9	3531	✓
5 Car Garage	3+71 N End	4.80	3534	✓
ctr Garage	3+45 on Prop	4.94	3531	✓
Garage	3+50 on East & Back	4.7	3533	✓

357.98

3+50 358°

E	9.8	3537	✓
ctr	9.9	3532	✓
W	9.9	3532	✓
End 5 car Garage	5.02	3532	✓
	4+00		

W	5.1	3549	✓
ctr	5.0	3550	✓
E	5.1	3549	✓
3 Car Garage	4.78	3550	✓
4+15 NE	4.72	3553	✓
9+44 S End			
	4+50		

E	5.1	3549	✓
ctr	5.1	3549	✓
W	5.0	3550	✓

4+68 N Prop Madison

W Edge Paving	5.06	3549	✓
ctr Paving	5.35	3546	✓
East Edge Paving	5.20	3548	✓

T.P.	6.03	35885	5.16	352.82
B.M.			2.91	355.94

Potted (Nov 1, 1927)  
Henny

(see page 76)

Alley 26 U. H. (copied from F.B. 1219) ISK

B711	6.35	357.75	357 <sup>8</sup>	357.40	
					5 Ch L Madrasa Cove
EL Alley on Paving			5.95	357 <sup>8</sup>	
E	"	"	5.94	351 <sup>9</sup>	
W	"	"	5.91	351 <sup>9</sup>	
					N L Madrasa
E Top Ch + Paving			5.10	352	
E	"	Memhole	5.13	351 <sup>1</sup>	
W			4.93	352 <sup>9</sup>	
TP	5.78	359.20	4.33	353.42	
					5 L Adama
W on N + S Conc Walk			4.85	3563	Adama Cove not paved
E		Ground	4.8	3544	
E		"	4.7	3548	There is a 24" Conc. Crosswalk S. Side Adama.
					5. Ch line Adama
E on Top Link			4.82	3542	
E		Ground	5.5	3532	
W on Top Link			4.98	3542	
TP	4.15	357.04	4.31	354.89	
			5.16	353.88	

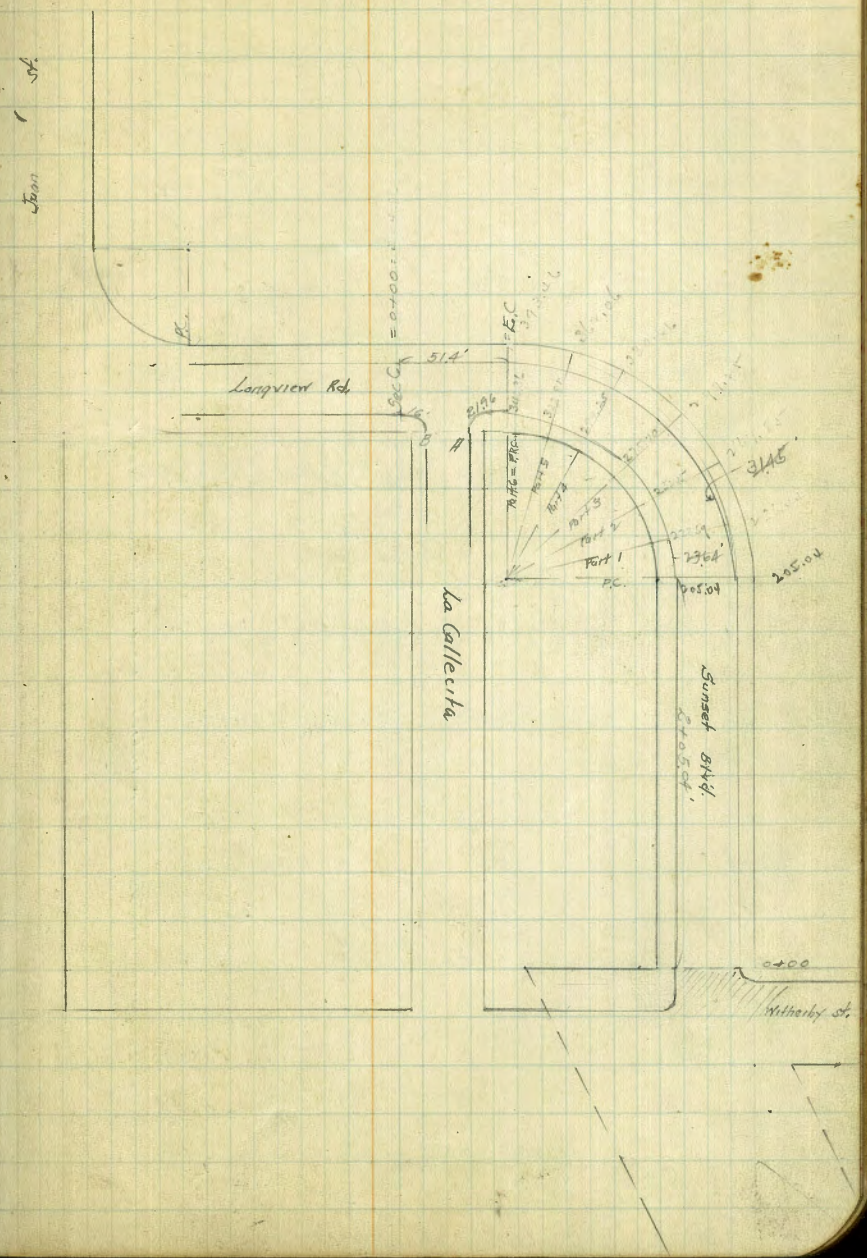






CURB LEVELS ON SUNSET BLVD.  
AND LONGVIEW ROAD

N.E.B.P.			
Sunset & Witherby	0.33	261.35	261.02
0+00 = N.L. Witherby St.			
N top cb		1.34	260.01
S " "		0.33	261.02
0+35			
S " "		1.57	259.83
N " "		2.41	258.94
0+71			
N " "		4.55	256.80
S " "		4.00	257.35
1+00			
S " "		6.99	254.86
N " "		6.78	254.57
1+50			
N " "		10.54	250.61
S " "		10.89	250.46
1+75			
S " "		17.84	248.51
N " "		17.30	249.05
T.P.	0.44	248.80	248.36
2+05.4 = P.C.			
N top cb		1.45	247.35
S " "		2.21	246.59
Part 1			
S " "		3.55	245.25
N " "		2.75	246.05



	Part 2 =		
N top cb	3.68	245.12	
S " "	4.41	244.39	
	Part 3 =		
S " "	5.03	243.77	
N " "	4.31	244.49	
	Part 4 =		
N " "	5.13	243.67	
S " "	5.63	243.17	
	Part 5 =		
S " "	6.17	242.23	
N " "	5.93	242.87	
	Part 6 = EC =		
N " "	6.46	242.34	
S " " = PR	6.75	242.05	
N top cb	7.04	241.76	
S B " " "	7.72	241.08	
	Sec C = $\frac{0+50}{2} = 25$		
S top cb	8.30	240.50	
N " "	8.49	240.31	
T.P.	0.14	236.06	12.88
	0+50 =		
N top cb	1.50	234.56	
S " "	0.98	235.08	
	1+1860 = PC =		
S " "	8.49	227.57	
N " "	7.44	228.42	

Note: cb stands for Longview at JMWV cut are in Cross Sections Notes on Page 1

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1%. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level, the amount of cut or fill at side stake is found by amount of cut or fill and find in table. Set up rod at this point, and line of sight should cut target.

IMPROVED TABLES AND INFORMATION

To find Tangent and Extension for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given T may be found by dividing tangent (or extension) opposite T by given tangent (or extension).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

2364  
31.45

6x2x

15.59

Hong

7  
13  
124  
x7  
175  
95  
120

- 5.32  
+ 4.60

416

263.72  
551  
258.22  
263.72

258.21  
114  
259.35

1110

261.68  
1110  
27278.11  
4.76  
268.02