

1204

BOSTON

---

FIELD BOOK

No. 385

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No. 2000 8/11/20 4/16



Cross Section Cherokee  
Myrtle to Bellingsport

321.3

80 ft side  
10' Cbr  
10' Qtr

NW BR

|                     |       |             |        |                                  |
|---------------------|-------|-------------|--------|----------------------------------|
| BM                  | 10.55 | 321.29      | 310.74 | 37.4                             |
|                     |       | N.W. Myrtle |        |                                  |
| F                   |       | 41          | 317.2  | Myrtle                           |
| Cb - S End Gas Curb |       | 43.1        | 316.98 | 60 ft side<br>10' Cbr<br>10' Qtr |
| Gutter              |       | 46          | 316.7  |                                  |
| "                   |       | 43          | 317.0  |                                  |
| L                   |       | 42          | 317.1  |                                  |
| "                   |       | 46          | 316.7  |                                  |
| Gutter              |       | 48          | 316.5  |                                  |
| Cb - S End Gas Curb |       | 42.1        | 317.03 |                                  |
| "                   |       | 46          | 316.7  |                                  |
|                     |       | N.Cb        |        |                                  |
| "                   |       | 52          | 316.1  |                                  |
| Cb                  |       | 50          | 316.3  |                                  |
| "                   |       | 46          | 316.7  |                                  |
| L                   |       | 43          | 317.0  |                                  |
| "                   |       | 43          | 317.0  |                                  |
| Cb                  |       | 49          | 316.4  |                                  |
| F                   |       | 47          | 317.1  |                                  |
|                     |       | "           |        |                                  |
| F                   |       | 44          | 316.9  |                                  |
| Cb                  |       | 50          | 316.3  |                                  |
| "                   |       | 43          | 317.0  |                                  |
| L                   |       | 44          | 316.9  |                                  |
| "                   |       | 59          | 315.4  |                                  |

Yardage  
Figured  
5/17/28

321.3

321.29

6.11.21  
S. 100  
S. 100  
S. 100

|    |  |           |       |
|----|--|-----------|-------|
| Cb |  | 51        | 316.2 |
| "  |  | 54        | 315.9 |
|    |  | N. Myrtle |       |
| "  |  | 60        | 315.3 |
| Cb |  | 56        | 315.7 |
| "  |  | 55        | 315.8 |
| "  |  | 51        | 316.2 |
| L  |  | 46        | 316.7 |
| "  |  | 46        | 316.7 |
| Cb |  | 53        | 316.6 |
| F  |  | 47        | 316.6 |
|    |  | "         |       |
| F  |  | 58        | 316.1 |
| Cb |  | 52        | 316.1 |
| "  |  | 50        | 316.3 |
| L  |  | 47        | 316.6 |
| "  |  | 57        | 315.6 |
| Cb |  | 60        | 315.3 |
| "  |  | 61        | 315.2 |
|    |  | S.Cb      |       |
| "  |  | 65        | 314.8 |
| Cb |  | 63        | 315.1 |
| "  |  | 62        | 315.1 |
| L  |  | 53        | 316.0 |
| "  |  | 55        | 315.8 |
| Cb |  | 55        | 315.8 |



Gberokre

321.3

321.29

|    |                       |          |  |
|----|-----------------------|----------|--|
| F  | 55                    | 315.8    |  |
|    | St Myrtle             | = 0 + 00 |  |
| F  | 58                    | 315.5    |  |
| Cb | 51                    | 315.7    |  |
| H  | 61                    | 315.2    |  |
| L  | 57                    | 315.6    |  |
| H  | 66                    | 314.7    |  |
| Cb | 61                    | 314.7    |  |
| H  | 69                    | 314.4    |  |
|    | 50 S of St. of Myrtle |          |  |
| H  | 84                    | 312.9    |  |
| Cb | 83                    | 313.0    | 95 S of St. of Myrtle<br>Cone Drill<br>9.20 312.99 |
| H  | 80                    | 313.3    |  |
| H  | 86                    | 312.7    |  |
| H  | 85                    | 312.8    |  |
| L  | 75                    | 313.8    |  |
| H  | 77                    | 313.6    |  |
| Cb | 74                    | 313.9    |  |
| F  | 71                    | 314.2    |  |
|    | 100 S                 |          |  |
| F  | 87                    | 312.6    |  |
| Cb | 88                    | 312.5    |  |
| H  | 92                    | 312.1    |  |
| H  | 97                    | 311.6    |  |
| L  | 93                    | 312.0    |  |
| H  | 100                   | 311.3    |  |

321.3

321.29

3

|  |       |       |   |
|--|-------|-------|---|
|  | 99    | 311.5 | 115 S of St. of Myrtle<br>Cone Drill<br>9.20 311.89 |
|  | 100   | 311.3 |   |
|  | 105   | 310.8 |   |
|  | 125 S |       |   |
|  | 116   | 309.7 |   |
|  | 110   | 310.3 |   |
|  | 107   | 310.6 |   |
|  | 112   | 310.1 |   |
|  | 110   | 310.3 |   |
|  | 105   | 310.8 |   |
|  | 104   | 310.9 |   |
|  | 105   | 310.8 |   |
|  | 100   | 311.3 |   |
|  | 99    | 311.4 |   |
|  | 150 S |       |   |
|  | 115   | 309.8 | 120 S of Myrtle<br>Cone Drill<br>11.19 309.6        |
|  | 113   | 310.0 |   |
|  | 116   | 309.7 |   |
|  | 114   | 309.9 | 159 S of Myrtle<br>Cone Drill<br>14.08 309.21       |
|  | 123   | 309.1 |   |
|  | 120   | 309.3 |   |
|  | 122   | 309.1 |   |
|  | 120   | 308.3 |   |
|  | 130   | 308.8 | 310.7   |
|  | 175 S |       |   |
|  | 40    | 306.7 |   |
|  | 32    | 307.5 |   |



Cheraka

310.7

310.7

3

310.66

310.66

|     |       |    |       |     |
|-----|-------|----|-------|-----|
| 48  | 175'S | 29 | 307.8 | 11  |
| 110 |       | 36 | 307.1 | 66  |
| 11  |       | 33 | 307.4 | F   |
| 43  |       | 25 | 308.2 |     |
| 8   |       | 22 | 308.5 | F   |
| 77  |       | 28 | 307.9 | 66  |
| 14  |       | 27 | 308.0 | 14  |
| 17  |       | 20 | 308.7 | +6  |
| 66  |       | 20 | 308.7 | 8   |
| F   |       | 21 | 308.3 | 110 |
|     | 200'S |    |       | 14  |
| F   |       | 14 | 306.3 | 12  |
| 66  |       | 41 | 306.6 | 11  |
| 14  |       | 44 | 306.3 | 66  |
| 8   |       | 43 | 306.4 | 11  |
| 14  |       | 16 | 306.1 |     |
| 15  |       | 51 | 305.6 | 11  |
| 66  |       | 53 | 305.4 | 66  |
| 11  |       | 60 | 304.7 | 14  |
|     | 325'S |    |       | +7  |
| 11  |       | 84 | 302.3 | 8   |
| 66  |       | 74 | 303.3 | 14  |
| +10 |       | 72 | 303.5 | 66  |
| 12  |       | 76 | 303.1 | F   |
| +6  |       | 61 | 304.6 |     |
| 8   |       | 60 | 304.7 | F   |

250'S

275'S

300'S

|     |       |
|-----|-------|
| 18  | 308.9 |
| 66  | 304.1 |
| 62  | 304.5 |
| 76  | 303.1 |
| 82  | 302.5 |
| 87  | 302.0 |
| 79  | 302.8 |
| 76  | 303.1 |
| 81  | 302.6 |
| 93  | 301.4 |
| 97  | 301.0 |
| 91  | 301.6 |
| 96  | 301.1 |
| 101 | 300.6 |
| 119 | 298.8 |
| 115 | 299.2 |
| 111 | 299.6 |
| 96  | 301.1 |
| 99  | 300.8 |
| 99  | 300.8 |
| 96  | 301.1 |
| 93  | 301.4 |
| 110 | 299.7 |



310.66

310.7

298.2

298.15

|     |      |                 |                 |
|-----|------|-----------------|-----------------|
| Cb  |      | 110             | 299.7           |
| 1/4 |      | 117             | 299.0           |
| 2   |      | 122             | 298.5           |
| 15  |      | 121             | 298.6           |
| 1/2 |      | 121             | 297.6           |
| 12  |      | 141             | 296.6           |
| 21  |      | 125             | 297.2           |
| Cb  |      | 123             | 296.4           |
| W   |      | 118             | 295.9           |
| TP  | 0.44 | 298.15<br>295.5 | 162.5<br>297.71 |
| W   |      | 48              | 293.4           |
| Cb  |      | 41              | 294.1           |
| 17  |      | 37              | 294.8           |
| 18  |      | 41              | 294.1           |
| 14  |      | 40              | 294.2           |
| 12  |      | 22              | 295.4           |
| 2   |      | 22              | 295.4           |
| 1/2 |      | 22              | 296.0           |
| Cb  |      | 17              | 296.8           |
| F   |      | 12              | 296.9           |
| F   | 0.50 | 29              | 293.8           |
| Cb  |      | 16              | 293.6           |
| 19  |      | 48              | 293.4           |
| 14  |      | 51              | 292.6           |

298.2

|     |  |     |       |
|-----|--|-----|-------|
| 5   |  | 58  | 292.4 |
| 1/2 |  | 49  | 292.4 |
| 1/4 |  | 65  | 291.7 |
| 12  |  | 50  | 292.3 |
| Cb  |  | 13  | 291.9 |
| W   |  | 70  | 291.2 |
| W   |  | 89  | 289.3 |
| Cb  |  | 86  | 289.6 |
| 1/2 |  | 83  | 289.9 |
| 1/4 |  | 86  | 289.6 |
| 12  |  | 79  | 289.3 |
| 2   |  | 80  | 290.2 |
| 1/4 |  | 82  | 290.0 |
| 15  |  | 72  | 291.0 |
| Cb  |  | 79  | 290.3 |
| F   |  | 69  | 291.3 |
| F   |  | 19  | 291.3 |
| Cb  |  | 79  | 290.8 |
| 18  |  | 78  | 290.4 |
| 1/4 |  | 80  | 290.2 |
| 2   |  | 88  | 289.4 |
| 1/4 |  | 93  | 288.9 |
| 12  |  | 102 | 288.0 |
| 15  |  | 94  | 288.8 |

298.15 - H. Bellingham

3708 5095 - H. Bellingham  
3857 5095 - H. Bellingham

Bellingham  
80  
11/2  
13/2



29815

2982

|          |               |              |                         |
|----------|---------------|--------------|-------------------------|
| Cb       | 10.3          | 287.9        |                         |
| H        | 10.5          | 287.7        |                         |
|          | N Cb (14) ES  | on 2/10/2002 |                         |
| H        | 12.0          | 286.2        |                         |
| Cb       | 11.1          | 287.1        |                         |
| +9       | 10.8          | 287.4        |                         |
| +10      | 11.6          | 286.6        |                         |
| 1/4      | 10.8          | 287.4        |                         |
| S        | 10.3          | 287.9        |                         |
| +10      | 10.0          | 288.2        |                         |
| 1/4      | 10.5          | 287.7        |                         |
| +1       | 9.4           | 288.8        |                         |
| Cb       | 9.0           | 289.2        |                         |
| F        | 8.7           | 289.5        | 5                       |
|          | N 1/4 (21) ES |              |                         |
| F        | 10.5          | 287.7        |                         |
| Cb       | 10.2          | 287.3        |                         |
| 1/4      | 11.5          | 286.7        |                         |
| S - M.H. | 11.9          | 286.3        | on 11/10/04 M.H. 286.11 |
| +3       | 12.4          | 285.8        |                         |
| +7       | 12.1          | 285.8        |                         |
| 1/2      | 13.0          | 285.2        |                         |
| +2       | 13.6          | 284.6        |                         |
| +5       | 12.1          | 285.6        |                         |
| Cb       | 12.9          | 285.3        |                         |
| H        | 14.0          | 284.2        |                         |

288.6

5

29815

|    |      |            |         |        |
|----|------|------------|---------|--------|
| TR | 1.24 | 284.52     | 12.81   | 285.34 |
|    |      | Ballingbom | (40) ES |        |
| H  |      |            | 4.0     | 282.6  |
| Cb |      |            | 3.3     | 283.3  |
|    |      |            | 3.8     | 283.8  |
|    |      |            | 3.9     | 282.7  |
|    |      |            | 3.8     | 282.8  |
|    |      |            | 2.5     | 284.1  |
|    |      |            | 4.2     | 284.6  |
|    |      |            | 2.7     | 283.9  |
|    |      |            | 1.5     | 285.1  |
|    |      |            | 1.2     | 285.4  |
|    |      |            | 0.2     | 285.8  |
|    |      | S 1/4      | (53) ES |        |
|    |      |            | 2.8     | 283.8  |
|    |      |            | 3.1     | 283.5  |
|    |      |            | 4.0     | 282.6  |
|    |      |            | 3.8     | 282.8  |
|    |      |            | 4.9     | 281.7  |
|    |      |            | 4.5     | 282.1  |
|    |      |            | 4.8     | 281.8  |
|    |      |            | 5.0     | 281.6  |
|    |      | S Cb       | (66) ES |        |
|    |      |            | 6.6     | 280.0  |
|    |      |            | 6.5     | 280.1  |
|    |      |            | 6.9     | 280.2  |



Cherokee

286.54

286.6

6

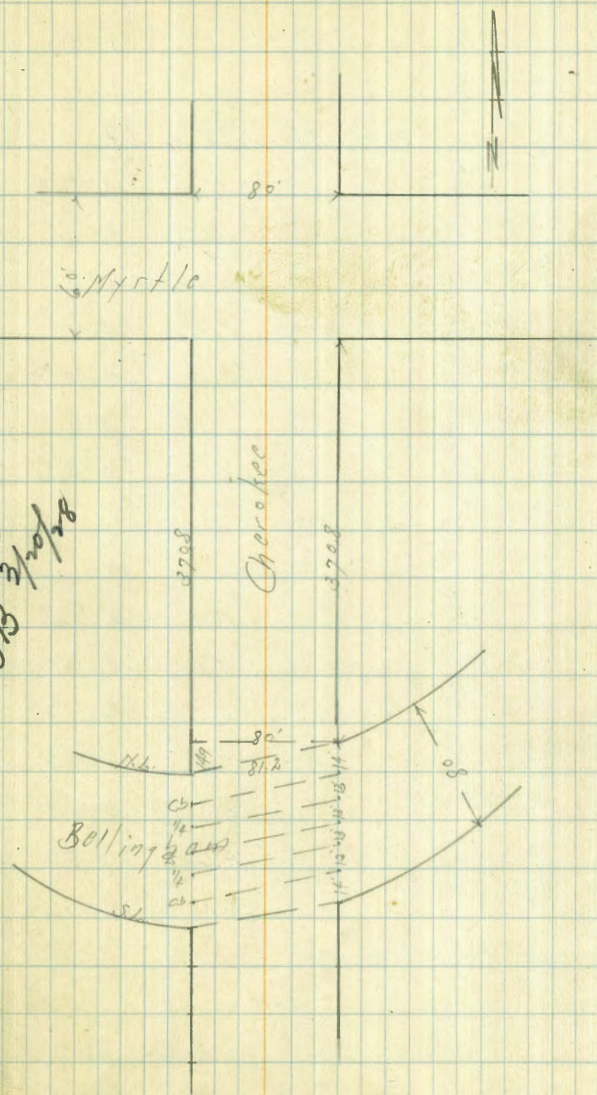
|    |    |       |
|----|----|-------|
| 14 | 67 | 279.9 |
| 17 | 55 | 281.1 |
| 2  | 53 | 281.3 |
| 11 | 52 | 281.4 |
| 14 | 51 | 281.0 |
| Ch | 50 | 281.4 |
| F  | 48 | 281.8 |

St. Bellingham Co. ES

|    |     |        |
|----|-----|--------|
| F  | 13  | 280.3  |
| Ch | 10  | 279.7  |
| 14 | 74  | 279.2  |
| 15 | 71  | 279.5  |
| 2  | 70  | 279.5  |
| 14 | 77  | 278.9  |
| Ch | 81  | 278.5  |
| 14 | 87  | 278.9  |
| 31 | 469 | 281.39 |

SE 1/4  
T10N R10E  
Cherokee  
Bellingham

Plotted  
JBB 3/10/28





Tolman  
7/26/67

Xsection of Myrtle Ave  
E.L. of Cherokee to E.L. of 37th

60' ft  
10' cbs  
10' cuts

321.66

7

10.92 3 21.66 310.74 B.N.B.P NW  
57th Cherokee

E.L. Cherokee St

|               |     |       |
|---------------|-----|-------|
| N.L           | 4.3 | 317.4 |
| cb            | 4.5 | 317.2 |
| $\frac{1}{4}$ | 4.6 | 317.1 |
| $\frac{1}{4}$ | 5.0 | 316.7 |
| $\frac{1}{4}$ | 5.5 | 316.2 |
| cb            | 5.9 | 315.9 |
| S.L           | 6.1 | 315.6 |

0+40

|               |     |       |
|---------------|-----|-------|
| S.L           | 5.9 | 315.8 |
| cb            | 5.5 | 316.2 |
| $\frac{1}{4}$ | 5.5 | 316.2 |
| $\frac{1}{4}$ | 5.1 | 316.6 |
| $\frac{1}{4}$ | 4.9 | 316.8 |
| cb            | 4.6 | 317.1 |
| N.L           | 4.4 | 317.3 |

0+60

|               |     |       |
|---------------|-----|-------|
| N.L           | 4.6 | 317.1 |
| cb            | 4.9 | 316.8 |
| $\frac{1}{4}$ | 5.2 | 316.5 |
| $\frac{1}{4}$ | 5.5 | 316.2 |

|               |     |       |
|---------------|-----|-------|
| $\frac{1}{4}$ | 5.7 | 316.0 |
| cb            | 6.2 | 315.5 |
| S.L           | 6.3 | 315.4 |

1+00

|               |     |       |
|---------------|-----|-------|
| S.L           | 7.5 | 314.2 |
| cb            | 7.2 | 314.5 |
| $\frac{1}{4}$ | 7.0 | 314.7 |
| $\frac{1}{4}$ | 6.9 | 314.8 |
| $\frac{1}{4}$ | 6.7 | 315.0 |
| cb            | 6.6 | 315.1 |
| N.L           | 6.2 | 315.5 |

1+40 = W.L. Alley

|               |     |       |
|---------------|-----|-------|
| N.L           | 7.7 | 314.0 |
| cb            | 8.1 | 313.6 |
| $\frac{1}{4}$ | 8.4 | 313.3 |
| $\frac{1}{4}$ | 8.2 | 313.1 |
| $\frac{1}{4}$ | 8.7 | 313.0 |
| cb            | 8.9 | 312.8 |
| S.L           | 9.2 | 312.5 |

1+60 = E.L. Alley

|               |     |       |
|---------------|-----|-------|
| S.L           | 9.7 | 312.0 |
| cb            | 9.6 | 312.1 |
| $\frac{1}{4}$ | 9.5 | 312.2 |



321.66

|               |     |       |
|---------------|-----|-------|
| ±             | 9.5 | 312.2 |
| $\frac{1}{4}$ | 9.1 | 312.6 |
| cb            | 8.5 | 313.2 |
| N.L.          | 8.1 | 313.6 |

1+80

|               |      |       |
|---------------|------|-------|
| N.L.          | 8.6  | 313.1 |
| cb            | 9.2  | 312.5 |
| $\frac{1}{4}$ | 9.1  | 312.6 |
| ±             | 9.7  | 312.0 |
| $\frac{1}{4}$ | 9.6  | 312.1 |
| cb            | 10.5 | 311.2 |
| S.L.          | 10.7 | 311.0 |

1+90

|               |      |       |
|---------------|------|-------|
| S.L.          | 11.6 | 310.1 |
| cb            | 11.2 | 310.5 |
| $\frac{1}{4}$ | 11.5 | 310.2 |
| ±             | 9.7  | 312.0 |
| $\frac{1}{4}$ | 9.4  | 312.3 |
| cb            | 9.0  | 312.7 |
| N.L.          | 8.8  | 312.9 |

|    |      |        |       |        |
|----|------|--------|-------|--------|
| TP | 2.77 | 314.09 | 10.34 | 311.32 |
|----|------|--------|-------|--------|

Myrtle Ave.

314.09

8

2+00

|               |     |       |
|---------------|-----|-------|
| N.L.          | 0.9 | 313.2 |
| cb            | 0.9 | 313.2 |
| $\frac{1}{4}$ | 2.5 | 311.6 |
| ±             | 6.2 | 307.9 |
| $\frac{1}{4}$ | 7.0 | 307.1 |
| cb            | 7.9 | 306.2 |
| +7            | 6.4 | 307.7 |
| S.L.          | 5.7 | 308.4 |

2+20

|               |      |       |
|---------------|------|-------|
| -4            | 6.5  | 307.6 |
| S.L.          | 8.7  | 305.4 |
| cb            | 13.6 | 300.5 |
| $\frac{1}{4}$ | 11.1 | 303.0 |
| ±             | 8.3  | 305.8 |
| $\frac{1}{4}$ | 3.2  | 310.9 |
| cb            | 1.9  | 312.2 |
| N.L.          | 0.7  | 313.4 |

2+40

|               |      |       |
|---------------|------|-------|
| N.L.          | 1.3  | 312.8 |
| cb            | 4.8  | 309.3 |
| $\frac{1}{4}$ | 8.9  | 305.2 |
| ±             | 11.8 | 302.3 |
| $\frac{1}{4}$ | 14.8 | 299.3 |



314.09

|     |      |       |
|-----|------|-------|
| cb  | 17.8 | 296.3 |
| S.L | 19.5 | 294.6 |
| +10 | 15.5 | 298.6 |
| +20 | 12.4 | 301.7 |

Σ+50

|               |      |       |
|---------------|------|-------|
| -30           | 21.1 | 293.0 |
| -10           | 19.0 | 295.1 |
| S.L           | 15.7 | 298.4 |
| cb            | 12.3 | 301.8 |
| $\frac{1}{4}$ | 10.2 | 303.7 |
| $\frac{1}{2}$ | 8.3  | 305.8 |
| $\frac{1}{4}$ | 6.7  | 307.4 |
| cb            | 3.5  | 310.6 |
| +4            | 1.4  | 312.7 |
| N.L           | 2.0  | 312.1 |

2x90

|               |      |       |
|---------------|------|-------|
| N.L           | 1.7  | 312.4 |
| cb            | 2.3  | 311.8 |
| $\frac{1}{4}$ | 2.9  | 311.4 |
| $\frac{1}{2}$ | 3.9  | 310.2 |
| $\frac{1}{4}$ | 4.8  | 309.3 |
| cb            | 7.2  | 306.8 |
| S.L           | 10.4 | 303.7 |
| +10           | 13.1 | 301.0 |

Myrtle Ave

99

+20

15.8

298.3

+300 = W.L. 374 sf

-20

11.6

302.5

-10

9.3

304.8

S.L

6.2

307.9

 $\frac{1}{4}$ 

5.0

309.1

cb

4.2

309.9

 $\frac{1}{2}$ 

4.0

310.1

 $\frac{1}{4}$ 

3.1

311.0

cb

1.9

312.2

N.L

1.1

313.0

3+14 = W.Cb Line

N.L Top Cb end

3.53

310.56

N.L Gutter

4.22

310.87

cb

4.5

309.6

 $\frac{1}{4}$ 

4.9

309.2

 $\frac{1}{2}$ 

5.0

309.1

 $\frac{1}{4}$ 

5.3

308.8

cb

5.8

308.3

S.L

6.1

308.0

+12

9.1

306.0 Break

3+27 = W.  $\frac{1}{4}$ 

S.L

5.2

308.9



314.09

|               |      |                  |
|---------------|------|------------------|
| cb            | 5.3  | 308.8            |
| $\frac{1}{4}$ | 4.9  | 309.2            |
| £             | 4.8  | 309.3            |
| $\frac{1}{4}$ | 4.5  | 309.6            |
| cb            | 4.1  | 310.0            |
| N.L.          | 3.65 | 310.44 on Paving |

3+40 £ of 37th St

|               |      |                  |
|---------------|------|------------------|
| N.L.          | 3.56 | 310.53 on Paving |
| cb            | 3.9  | 310.2            |
| $\frac{1}{4}$ | 4.3  | 309.8            |
| £             | 4.6  | 309.5            |
| $\frac{1}{4}$ | 5.2  | 308.9            |
| cb            | 5.6  | 308.5            |
| S.L.          | 5.7  | 308.4            |

3+53 W  $\frac{1}{4}$ 

|               |      |                  |
|---------------|------|------------------|
| S.L.          | 5.5  | 308.6            |
| cb            | 5.0  | 308.7            |
| $\frac{1}{4}$ | 5.2  | 308.9            |
| £             | 4.8  | 309.2            |
| $\frac{1}{4}$ | 4.5  | 309.6            |
| cb            | 4.2  | 309.9            |
| N.L.          | 3.86 | 310.23 on Paving |

314.09

Myrtle Ave. 10  
10

3+66 E cb line

|                 |      |        |
|-----------------|------|--------|
| N.L. Top cb end | 3.92 | 310.17 |
| Gutter paving   | 4.50 | 309.59 |
| cb              | 4.8  | 309.3  |
| $\frac{1}{4}$   | 4.5  | 309.6  |
| £               | 5.0  | 309.1  |
| $\frac{1}{4}$   | 5.3  | 308.8  |
| cb              | 5.5  | 308.6  |
| S.L.            | 5.2  | 308.9  |

3+80=N.L. 37th St

|               |     |                        |
|---------------|-----|------------------------|
| S.L.          | 3.7 | 310.4 on grass terrace |
| +3            | 5.3 | 308.8                  |
| cb            | 5.5 | 308.6                  |
| $\frac{1}{4}$ | 5.6 | 308.5                  |
| £             | 5.3 | 308.8                  |
| $\frac{1}{4}$ | 4.8 | 309.3                  |
| cb            | 4.5 | 309.6                  |
| N.L.          | 3.5 | 310.6                  |

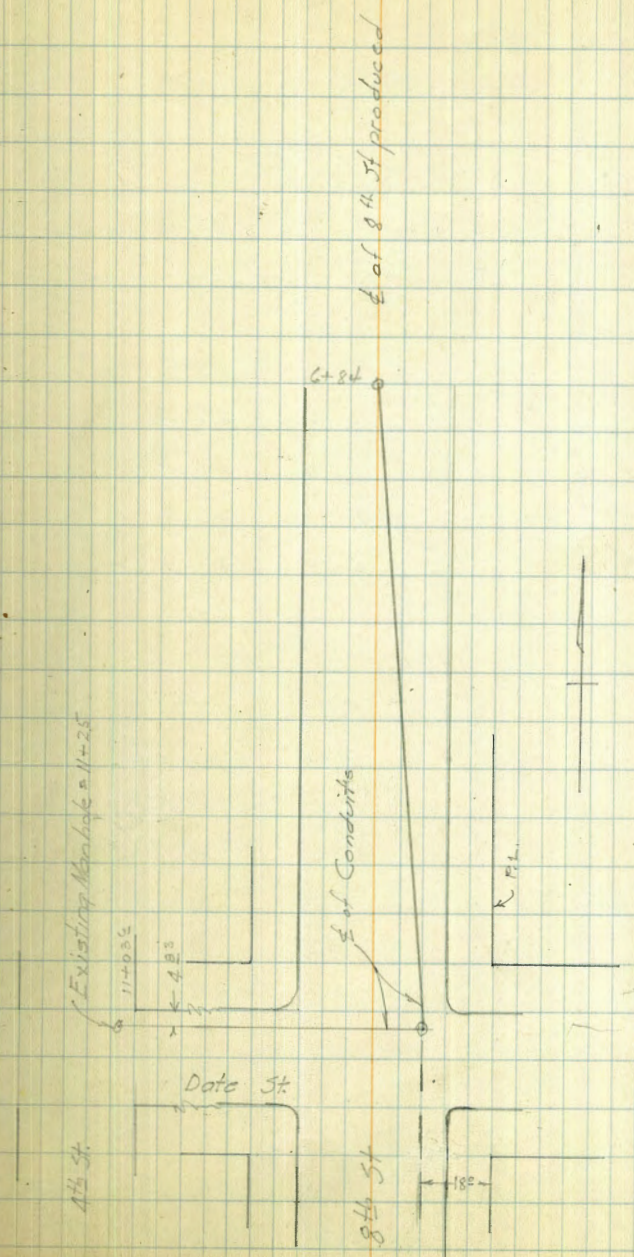


Talman  
7/27

Levels for Fire Dept. conduit from  
inters 8th & Date north into Balboa Park

|      | 7.94  | 161.58 | 153.64 | BPSW<br>8th & Cedar |
|------|-------|--------|--------|---------------------|
| 0+00 |       |        | 1.70   |                     |
| TP   | 12.81 | 173.56 | 0.88   | 160.70              |
| 1+00 |       |        | 11.5   |                     |
| 2+00 |       |        | 7.7    |                     |
| 3+00 |       |        | 4.0    |                     |
| 4+00 |       |        | 0.6    |                     |
| TP   | 10.37 | 183.38 | 0.55   | 173.01              |
| 5+00 |       |        | 6.8    |                     |
| 6+00 |       |        | 4.5    |                     |
| 6+84 |       |        | 2.6    |                     |

Note: See Mr. Collins, 10th & B St Station  
regarding details of these conduits









88.95

13

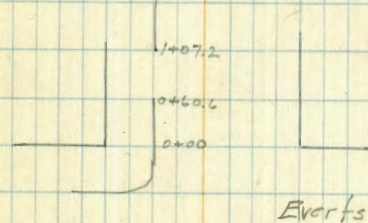
38.14

End ret NW 5.48 32.66

0+00 = Davis St E. Line

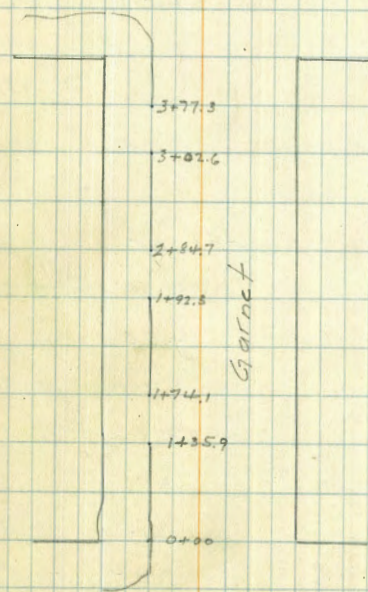
Blank spaces indicate where curb  
is missing or fallen over

|            |      |       |
|------------|------|-------|
| End ret SE | 5.51 | 32.63 |
| TC SE      | 5.21 | 32.93 |
| 10' S E    | 5.44 | 32.70 |
| E          | 5.35 | 32.79 |
| 10' N E    | 5.39 | 32.75 |
| TC NE      | 4.67 | 33.47 |
| End ret NE | 4.53 | 33.61 |



= 1+00 =

|         |      |       |
|---------|------|-------|
| T.C. N  | 3.54 | 34.60 |
| 10' N E | 4.16 | 33.98 |
| E       | 4.06 | 34.08 |
| 10' S E | 4.15 | 33.99 |
| TC S-   | 4.05 | 34.09 |



= 3+00 =

|         |        |       |
|---------|--------|-------|
| TC S    | 2.86   | 35.28 |
| 10' S E | 3.90   | 35.24 |
| E       | 2.79   | 35.35 |
| 10' N E | 2.99   | 35.25 |
| TC N-   | 66 out |       |

DAMES

TP 6.75 42.02 2.87 35.27



= 3+00 =

|         |       |      |       |
|---------|-------|------|-------|
| TC S-   | 42.02 | 5.57 | 36.45 |
| 10' S E |       | 5.60 | 36.42 |
| E       |       | 5.47 | 36.55 |
| 10' N E |       | 5.56 | 36.46 |
| TC N-   |       | 5.07 | 36.95 |

= 4+00 =

|         |  |      |       |
|---------|--|------|-------|
| TC N-   |  | 4.34 | 37.68 |
| 10' N E |  | 4.37 | 37.65 |
| E       |  | 4.26 | 37.76 |
| 10' S E |  | 4.27 | 37.75 |
| TC S-   |  | 3.90 | 38.12 |

WL Everts St

|               |  |      |       |                 |
|---------------|--|------|-------|-----------------|
| End ret. NW   |  | 2.38 | 39.64 |                 |
| TC N-         |  | 2.50 | 39.52 | BP. NW<br>39.53 |
| 10' N E       |  | 3.11 | 38.91 |                 |
| E             |  | 3.09 | 38.93 |                 |
| 10' S E       |  | 3.17 | 38.85 |                 |
| TC S-         |  | 3.14 | 38.88 |                 |
| End ret. S.W. |  | 3.45 | 38.57 |                 |

EL Everts (Narrower roadway)<sup>40'</sup>

|             |       |      |       |
|-------------|-------|------|-------|
| SE end ret. | 42.02 | 2.43 | 39.59 |
| TC S-       |       | 2.10 | 39.92 |
| 10' S E     |       | 2.20 | 39.82 |
| E           |       | 2.02 | 40.00 |
| 10' N E     |       | 2.12 | 39.90 |
| TC N-       |       | 1.57 | 40.45 |
| NE end ret. |       | 1.42 | 40.60 |

= 1+00 =

|         |  |      |       |
|---------|--|------|-------|
| TC N-   |  | out  |       |
| 10' N E |  | 1.03 | 40.99 |
| E       |  | 0.86 | 41.16 |
| 10' S E |  | 1.02 | 41.00 |
| TC S-   |  | 1.08 | 40.94 |

TP 7.81 48.75 1.08 40.94 (11005)

= 2+00 =

|         |  |      |       |
|---------|--|------|-------|
| TC S-   |  | 6.66 | 42.09 |
| 10' S E |  | 6.62 | 42.13 |
| E       |  | 6.49 | 42.26 |
| 10' N E |  | 6.64 | 42.11 |
| TC N-   |  | 6.22 | 42.53 |



= 3+00=

|         |       |      |       |
|---------|-------|------|-------|
| TC N-   | 48.75 | 4.91 | 43.84 |
| 10' N E |       | 5.48 | 43.27 |
| E       |       | 5.36 | 43.39 |
| 10' S E |       | 5.51 | 43.24 |
| TC S-   |       | 5.49 | 43.26 |

= 4+00

|         |  |      |       |
|---------|--|------|-------|
| TC S-   |  | 4.49 | 44.26 |
| 10' S E |  | 4.42 | 44.30 |
| E       |  | 4.24 | 44.51 |
| 10' N E |  | 4.36 | 44.39 |
| TC N-   |  | 4.01 | 44.74 |

WK Fandel

|            |  |      |       |
|------------|--|------|-------|
| NW end ret |  | 2.65 | 46.10 |
| TC N       |  | 2.75 | 46.00 |
| 10' N E    |  | 3.34 | 45.41 |
| E          |  | 3.33 | 45.42 |
| 10' S E    |  | 3.40 | 45.35 |
| TC S-      |  | 3.35 | 45.40 |
| SW end ret |  | 3.65 | 45.10 |

TP 1.75 52.85 3.65 45.10

FL Fandel

|            |       |      |       |
|------------|-------|------|-------|
| SE end ret | 52.85 | 6.85 | 46.00 |
| TC S       |       | 6.46 | 46.39 |
| 10' S E    |       | 6.51 | 46.34 |
| E          |       | 6.38 | 46.47 |
| 10' N E    |       | 6.45 | 46.40 |
| TC N       |       | 5.89 | 46.96 |
| NE end ret |       | 5.70 | 47.15 |

= 1+00=

|         |  |      |       |
|---------|--|------|-------|
| TC N-   |  | 4.99 | 47.86 |
| 10' N E |  | 5.53 | 47.32 |
| E       |  | 5.42 | 47.43 |
| 10' S E |  | 5.52 | 47.33 |
| TC S-   |  | 5.51 | 47.34 |

= 2+00

|         |  |      |       |
|---------|--|------|-------|
| TC S    |  | 4.51 | 48.34 |
| 10' S E |  | 4.60 | 48.25 |
| E       |  | 4.46 | 48.39 |
| 10' N E |  | 4.57 | 48.28 |
| TC N    |  | 4.05 | 48.00 |

= 3+10 - Break

|         |  |      |       |
|---------|--|------|-------|
| TC N    |  | 2.92 | 49.93 |
| 10' N E |  | 3.49 | 49.36 |
| E       |  | 3.36 | 49.49 |
| 10' S E |  | 3.50 | 49.35 |
| TC S    |  | 3.46 | 49.39 |



|        |      |        |       |       |
|--------|------|--------|-------|-------|
| T.P.   | 7.57 | 56.95  | 3.47  | 49.38 |
|        |      | - 4+00 |       |       |
| TCS    |      | 6.18   | 50.77 |       |
| 10'S & |      | 6.17   | 50.78 |       |
| 4      |      | 6.05   | 50.90 |       |
| 10'N & |      | 6.18   | 50.77 |       |
| TCN    |      | 5.70   | 51.25 |       |

## West Line Gresham

|               |      |       |  |  |
|---------------|------|-------|--|--|
| N.W. end ret. | 3.87 | 53.08 |  |  |
| TCN           | 3.99 | 52.96 |  |  |
| 10'N &        | 4.55 | 52.40 |  |  |
| 4             | 4.49 | 52.46 |  |  |
| 10'S &        | 4.68 | 52.27 |  |  |
| TCS           | 4.59 | 52.56 |  |  |
| S.W. end ret. | 4.90 | 52.05 |  |  |

## E. line Gresham

|               |      |       |  |  |
|---------------|------|-------|--|--|
| S.E. end ret. | 3.53 | 53.42 |  |  |
| T.C.S.        | 3.50 | 53.40 |  |  |
| 10'S &        | 3.52 | 53.43 |  |  |
| 4             | 3.40 | 53.55 |  |  |
| 10'N &        | 3.48 | 53.47 |  |  |
| TCN           | 2.96 | 53.99 |  |  |
| S.W. End ret. | 2.85 | 54.10 |  |  |

TP 9.01 65.09 0.87 56.08

|        |       |      |       |
|--------|-------|------|-------|
| TCN-   | 65.09 | 8.19 | 56.90 |
| 10'N & |       | 8.86 | 56.23 |
| 4      |       | 8.72 | 56.37 |
| 10'S & |       | 8.84 | 56.25 |
| TCS-   |       | 8.83 | 56.26 |

= 2+00 =

|        |  |      |       |
|--------|--|------|-------|
| TCS-   |  | 5.79 | 59.30 |
| 10'S & |  | 5.92 | 59.27 |
| 4      |  | 5.63 | 59.46 |
| 10'NE  |  | 5.80 | 59.29 |
| TCN-   |  | 5.28 | 59.81 |

= 3+00 =

|        |      |       |       |
|--------|------|-------|-------|
| TCN-   |      | 2.34  | 62.75 |
| 10'N & |      | 2.86  | 62.23 |
| 4      |      | 2.82  | 62.27 |
| 10'S & |      | 2.87  | 62.22 |
| TCS-   |      | 2.83  | 62.26 |
| TP     | 8.08 | 73.11 | 65.09 |

= 4+00 =

|        |  |      |       |
|--------|--|------|-------|
| TCS-   |  | 7.52 | 65.29 |
| 10'S & |  | 7.57 | 65.24 |
| 4      |  | 7.75 | 65.33 |
| 10'N & |  | 7.53 | 65.28 |



TCN 73.11 73.4 65.77

= W. L. Haines =

NW end rot 4.12 68.99  
 TCN- 4.11 69.00  
 10' N 4.89 68.22  
 4 4.80 68.21  
 10' S 4.92 68.19  
 TC S- 4.72 68.39  
 SW end rot 5.02 68.09

= E. L. Haines =

SE end rot 5.40 67.71  
 TC S- 5.25 67.86  
 10' S 5.27 67.84  
 4 5.19 67.94  
 10' N 5.15 67.96  
 TC N- 4.60 68.51  
 NE end rot 4.55 68.56

= 1+00 =

TCN- 5.67 67.44  
 10' N 6.30 66.81  
 4 6.16 66.95  
 10' S 6.30 66.81  
 TC S- 6.37 66.74  
 T.P. 3.13 69.87 6.37 66.74

= 2+00 =

TC S- 69.87 4.17 65.70  
 10' S 4.16 65.71  
 4 4.04 65.83  
 10' N 4.15 65.72  
 TCN- 3.54 66.33

= 3+00 =

TCN- 4.60 65.27  
 10' N 5.22 64.65  
 4 5.11 64.76  
 10' S 5.27 64.60  
 TC S- 5.26 64.61  
 T.P. 3.94 62.50 6.31 63.56

= 4+00 =

TC S- 3.96 63.54  
 10' S 3.95 63.55  
 4 3.82 63.68  
 10' N 3.97 63.53  
 TCN- 3.43 64.07

= W. L. Ingraham =

NW end rot 4.27 63.23  
 TCN 4.43 63.07  
 Top of gutter 4.83 62.67  
 10' N 5.01 62.47  
 4 4.93 62.57



|               |       |      |       |
|---------------|-------|------|-------|
| 10'S E        | 67.50 | 5.01 | 62.49 |
| Top of gutter |       | 5.63 | 61.87 |
| TC S-         |       | 5.07 | 62.43 |
| End ret SW    |       | 5.28 | 62.22 |

= F.L. Ingham =

|            |      |       |               |
|------------|------|-------|---------------|
| End ret SE | 5.07 | 62.43 |               |
| TC S       | 4.91 | 62.59 | 62.54<br>B.P. |
| Gutter     | 5.48 | 62.02 |               |
| 10'S E     | 4.88 | 62.62 |               |
|            | 4.85 | 62.65 |               |
| 10' N E    | 4.94 | 62.56 |               |
| Gutter     | 4.87 | 62.63 |               |
| 10' N E    | 4.49 | 63.01 |               |
| End ret NE | 4.30 | 63.20 |               |

= 1+00 =

|         |      |       |  |
|---------|------|-------|--|
| TC N-   | 3.00 | 64.50 |  |
| 10' N E | 3.33 | 64.17 |  |
| +       | 3.21 | 64.29 |  |
| 10' S E | 3.38 | 64.12 |  |
| TC S-   | 3.26 | 64.24 |  |

= 2+00 =

|         |      |       |  |
|---------|------|-------|--|
| TC S-   | 1.56 | 65.94 |  |
| 10' S E | 1.67 | 65.83 |  |
| +       | 1.55 | 65.95 |  |

|            |      |       |      |       |
|------------|------|-------|------|-------|
| 10' N E    |      |       | 1.66 | 65.84 |
| TC N- T.P. | 6.49 | 72.59 | 1.40 | 66.10 |

= 260 = Break

|         |  |  |      |       |
|---------|--|--|------|-------|
| TC N-   |  |  | 5.65 | 66.94 |
| 10' N E |  |  | 5.76 | 66.83 |
| +       |  |  | 5.62 | 66.97 |
| 10' S E |  |  | 5.74 | 66.85 |
| TC S-   |  |  | 5.66 | 66.93 |

= 3+00 =

|         |  |  |      |       |
|---------|--|--|------|-------|
| TC S-   |  |  | 5.31 | 67.28 |
| 10' S E |  |  | 5.38 | 67.20 |
| +       |  |  | 5.27 | 67.32 |
| 10' N E |  |  | 5.37 | 67.22 |
| TC N-   |  |  | 5.20 | 67.39 |

= 4+00 =

|         |      |       |      |                     |
|---------|------|-------|------|---------------------|
| TC N-   |      |       | 4.48 | 68.11               |
| 10' N E |      |       | 4.60 | 67.99               |
| +       |      |       | 4.51 | 68.08               |
| 10' S E |      |       | 4.64 | 67.95               |
| TC S-   |      |       | 4.59 | 68.00               |
| T.P.    | 3.57 | 72.26 | 3.90 | 68.63<br>B.P. 68.69 |

W.L. Jewell

|            |  |  |      |       |
|------------|--|--|------|-------|
| End ret SW |  |  | 3.66 | 68.60 |
| TC S-      |  |  | 3.57 | 68.69 |



(Clouds of Dist)

|            |       |      |       |
|------------|-------|------|-------|
| 10'S E     | 72.26 | 3.77 | 68.49 |
| E          |       | 3.65 | 68.61 |
| 10' N E    |       | 3.74 | 68.52 |
| TC N-      |       | 3.25 | 69.01 |
| End rot NW |       | 3.23 | 69.03 |

E L Jewell

|            |  |      |       |
|------------|--|------|-------|
| End rot NE |  | 3.98 | 68.28 |
| TC N       |  | 4.15 | 68.11 |
| 10' N E    |  | 4.50 | 67.76 |
| E          |  | 4.43 | 67.83 |
| 10'S E     |  | 4.53 | 67.73 |
| TC-S       |  | 4.50 | 67.76 |
| End rot SE |  | 4.52 | 67.74 |

= 1+00 =

|         |  |      |       |
|---------|--|------|-------|
| TC-S    |  | 4.86 | 67.40 |
| 10'S E  |  | 4.83 | 67.43 |
| E       |  | 4.71 | 67.55 |
| 10' N E |  | 4.86 | 67.40 |
| TC-N    |  | 4.55 | 67.71 |

= 2+00 =

|         |  |      |       |
|---------|--|------|-------|
| TC-N    |  | 5.03 | 67.23 |
| 10' N E |  | 5.23 | 67.03 |
| E       |  | 5.12 | 67.14 |

|        |       |      |       |
|--------|-------|------|-------|
| 10'S E | 72.26 | 5.27 | 66.99 |
| TC-S   |       | 5.24 | 67.02 |

= 3+00 =

|        |  |      |       |
|--------|--|------|-------|
| TC-S-  |  | 5.69 | 66.57 |
| 10'S E |  | 5.60 | 66.66 |
| E      |  | 5.48 | 66.78 |

|         |  |      |       |
|---------|--|------|-------|
| 10' N E |  | 5.62 | 66.64 |
|---------|--|------|-------|

|      |  |      |       |
|------|--|------|-------|
| TC N |  | 5.41 | 66.85 |
|------|--|------|-------|

|     |      |       |      |       |
|-----|------|-------|------|-------|
| T.P | 3.82 | 70.47 | 5.41 | 66.85 |
|-----|------|-------|------|-------|

= 4+00 =

|      |  |      |       |
|------|--|------|-------|
| TC-N |  | 4.09 | 66.58 |
|------|--|------|-------|

|         |  |      |       |
|---------|--|------|-------|
| 10' N E |  | 4.31 | 66.36 |
|---------|--|------|-------|

|   |  |      |       |
|---|--|------|-------|
| E |  | 4.21 | 66.46 |
|---|--|------|-------|

|        |  |      |       |
|--------|--|------|-------|
| 10'S E |  | 4.31 | 66.36 |
|--------|--|------|-------|

|      |  |      |       |
|------|--|------|-------|
| TC-S |  | 4.50 | 66.17 |
|------|--|------|-------|

Y L Kendall

|            |  |      |       |
|------------|--|------|-------|
| End rot SW |  | 5.56 | 65.11 |
|------------|--|------|-------|

|      |  |      |           |
|------|--|------|-----------|
| TC-S |  | 4.79 | 65.88 B.P |
|------|--|------|-----------|

|        |  |      |       |
|--------|--|------|-------|
| 10'S E |  | 4.72 | 65.95 |
|--------|--|------|-------|

|   |  |      |       |
|---|--|------|-------|
| E |  | 4.64 | 66.03 |
|---|--|------|-------|

|         |  |      |       |
|---------|--|------|-------|
| 10' N E |  | 4.73 | 65.94 |
|---------|--|------|-------|

|      |  |      |       |
|------|--|------|-------|
| TC-N |  | 4.52 | 66.15 |
|------|--|------|-------|

|            |  |      |       |
|------------|--|------|-------|
| End rot NW |  | 4.52 | 66.15 |
|------------|--|------|-------|



|            | 70.67 | FL Kendall |       |
|------------|-------|------------|-------|
| End ret NE |       | 4.31       | 66.36 |
| TC N       |       | 4.61       | 66.07 |
| 10' N E    |       | 4.61       | 66.06 |
| E          |       | 4.67       | 66.00 |
| 10' S E    |       | 4.80       | 65.87 |
| TC-S       |       | 4.76       | 65.91 |
| End ret SE |       | 5.62       | 65.05 |

= 1+00 =

|         |     |       |       |
|---------|-----|-------|-------|
| TC-S    |     | 4.84  | 65.83 |
| 10' S E |     | 4.75  | 65.92 |
| E       |     | 4.60  | 66.07 |
| 10' N E |     | 4.75  | 65.92 |
| TC-N    |     | 4.46  | 66.21 |
| T.P.    | 485 | 71.06 | 4.46  |
|         |     |       | 66.21 |

= 2+00 =

|         |  |      |       |
|---------|--|------|-------|
| TC-N    |  | 4.60 | 66.66 |
| 10' N E |  | 4.95 | 66.11 |
| E       |  | 4.85 | 66.21 |
| 10' S E |  | 4.98 | 66.08 |
| TC-S    |  | 5.23 | 65.89 |

= 3+00 =

|         |  |      |       |
|---------|--|------|-------|
| TC S    |  | 5.21 | 65.85 |
| 10' S E |  | 4.84 | 66.22 |

|      | 71.06 | 4.75 | 66.31 |
|------|-------|------|-------|
| E    |       | 4.87 | 66.19 |
| TC N |       | 4.35 | 66.71 |

= 4+00 =

|         |      |       |       |
|---------|------|-------|-------|
| TC N    |      | 4.19  | 66.87 |
| 10' N E |      | 4.78  | 66.28 |
| E       |      | 4.67  | 66.39 |
| 10' S E |      | 4.79  | 66.27 |
| TC S    |      | 5.25  | 65.81 |
| T.P.    | 5.83 | 71.18 | 5.21  |

NW Lament

|                      |  |      |       |
|----------------------|--|------|-------|
| SW end ret           |  | 5.83 | 65.85 |
| TC-S                 |  | 5.86 | 65.82 |
| 10' S E              |  | 5.42 | 66.26 |
| E                    |  | 5.33 | 66.35 |
| 10' N E              |  | 5.32 | 66.36 |
| TC N                 |  | 4.71 | 66.96 |
| NW end ret           |  | 4.41 | 67.27 |
| End cb. at 20 radius |  | 4.30 | 67.38 |

E L Lament

|            |  |      |       |
|------------|--|------|-------|
| NE end ret |  | 4.72 | 66.96 |
| TC-N       |  | 4.70 | 66.98 |
| 10' N E    |  | 5.44 | 66.24 |
| E          |  | 5.33 | 66.35 |
| 10' S E    |  | 5.42 | 66.26 |



TC 5                    71.68     5.81     65.87  
 SE end ref.                    5.83     65.85

= 1+00 =

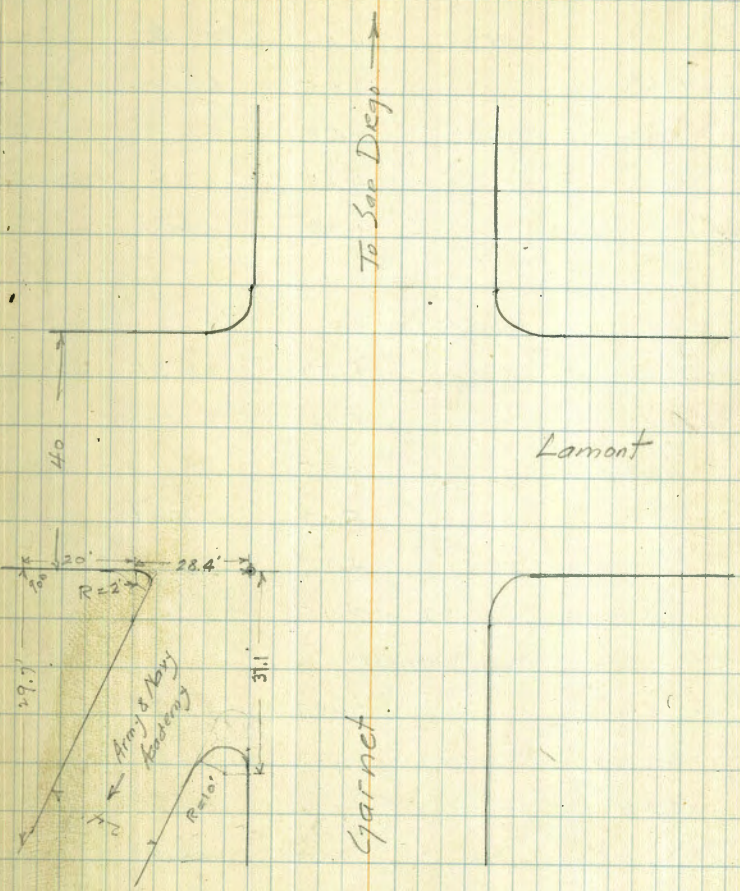
TC 5                    5.26     66.42  
 10'SE                    4.95     66.72  
 E                    4.86     66.82  
 10'NE                    5.00     66.68  
 TC N                    4.38     67.30

= 2+00 =

TC N                    3.99     67.69  
 10'NE                    4.38     67.30  
 E                    4.41     67.27  
 10'SE                    4.53     67.15  
 TC S-

= 1+50 = Break?

TC S-                    4.80     66.88  
 10'SE                    4.53     67.15  
 E                    4.41     67.27  
 10'NE                    4.49     67.19  
 TC N-





= 3+00 =

|         |       |      |       |
|---------|-------|------|-------|
| TCN-    | 71.68 | 4.36 | 67.32 |
| 10' N E |       | 4.65 | 67.03 |
| £       |       | 4.58 | 67.10 |
| 10' S E |       | 4.68 | 67.10 |
| TC S-   |       | 4.98 | 66.70 |

= 4+00 =

|         |      |       |       |
|---------|------|-------|-------|
| TC S-   |      | 5.37  | 66.31 |
| 10' S E |      | 5.04  | 66.64 |
| £       |      | 4.95  | 66.73 |
| 10' N E |      | 5.07  | 66.61 |
| TC N-   |      | 4.95  | 66.73 |
| TP      | 2.10 | 68.83 | 4.95  |

= WL. Morrell =

|            |  |      |       |
|------------|--|------|-------|
| NW end rot |  | 2.47 | 66.34 |
| TC N       |  | 2.53 | 66.30 |
| 10' N E    |  | 2.70 | 65.93 |
| £          |  | 2.80 | 66.03 |
| 10' S E    |  | 2.83 | 66.00 |
| TC S       |  | 2.89 | 65.94 |
| SE end rot |  | 3.00 | 65.83 |

= EL Morrell =

|            |  |      |       |
|------------|--|------|-------|
| SE end rot |  | 4.31 | 64.52 |
| TC S       |  | 4.30 | 64.53 |

10' S E

68.83

4.31

64.52

1 E

4.22

64.61

10' N E

4.33

64.50

TC N-

4.25

64.70

NE end rot

3.92

64.91

= 1+00 =

TC N

4.64

64.19

10' N E

5.12

63.71

£

4.96

63.87

10' S E

5.12

63.71

TC S-

4.83

64.00

= 2+00 =

TC S

5.40

63.43

10' S E

5.65

63.18

£

5.52

63.31

10' N E

5.62

63.21

TC N

5.26

63.57

= 3+00 =

68.83

TC N

5.77

63.05

10' N E

6.10

62.73

£

6.01

62.82

10' S E

6.16

62.67

TC S

6.00

62.83



|             |     |                    |      |       |
|-------------|-----|--------------------|------|-------|
| T.P.        | 395 | 66.78<br>= 47.00 = | 6.00 | 62.83 |
| T.C.S.      |     |                    | 4.46 | 62.32 |
| 10'S $\phi$ |     |                    | 4.55 | 62.23 |
| $\phi$      |     |                    | 4.39 | 62.39 |
| 10'S $\phi$ |     |                    | 4.43 | 62.35 |
| T.C.N.      |     |                    | 4.26 | 62.32 |

58.44  
= 1+00

|             |      |       |
|-------------|------|-------|
| NTC         | 1.68 | 56.76 |
| 10'N $\phi$ | 2.03 | 56.41 |
| $\phi$      | 1.90 | 56.54 |
| 10'S $\phi$ | 1.99 | 56.45 |
| T.C.S.      | 1.85 | 56.59 |

## W. Line Noyes

|              |      |       |               |
|--------------|------|-------|---------------|
| N.W. end ret | 4.87 |       |               |
| T.C.N.       | 4.78 | 62.00 | 62.00<br>B.P. |
| 10'N $\phi$  | 5.29 | 61.49 |               |
| $\phi$       | 5.25 | 61.53 |               |
| 10'S $\phi$  | 5.35 | 61.43 |               |
| T.C.S.       | 5.05 | 61.73 |               |
| S.W. end ret | 4.97 | 61.81 |               |

= 2+00 =

|             |      |       |
|-------------|------|-------|
| T.C.S.      | 5.30 | 53.14 |
| 10'S $\phi$ | 5.28 | 53.16 |
| $\phi$      | 5.15 | 53.29 |
| 10'N $\phi$ | 5.25 | 53.19 |
| T.C.N.      | 4.73 | 53.71 |

= 3+00 =

## E. Line Noyes

|              |       |       |
|--------------|-------|-------|
| S.E. end ret | 6.75  | 60.03 |
| T.C.S.       | 6.76  | 60.02 |
| 10'S $\phi$  | 6.90  | 59.88 |
| $\phi$       | 6.77  | 60.01 |
| 10'N $\phi$  | 6.90  | 59.88 |
| T.C.N.       | 6.86  | 59.92 |
| N.E. end ret | 6.83  | 59.95 |
| T.P.         | 2.03  | 58.44 |
|              | 10.37 | 56.41 |

|             |      |       |
|-------------|------|-------|
| T.C.N.      | 7.61 | 50.83 |
| 10'N $\phi$ | 8.18 | 50.21 |
| $\phi$      | 8.07 | 50.37 |
| 10'S $\phi$ | 8.24 | 50.20 |
| T.C.S.      | 8.20 | 50.24 |

= 11+00 =

|             |       |       |
|-------------|-------|-------|
| T.C.S.      | 11.13 | 47.31 |
| 10'S $\phi$ | 11.15 | 47.29 |
| $\phi$      | 11.07 | 47.37 |
| 10'N $\phi$ | 11.20 | 47.24 |

58.44



TCH 5844 10.55 47.89

T.P. 2.67 50.06 11.05 47.39

## W L Olney

N End ret 5.03 45.03

TCH 4.97 45.09 B.P. <sup>45.10</sup>

10' N E 5.81 44.25

E 5.82 44.24

10' S E 5.98 44.08

TCS 5.80 44.26

S End ret 5.86 44.20

## E L Olney

SE end ret 7.96 42.10

TCS 7.67 42.39

10' S E 7.45 42.61

E 7.34 42.72

10' N E 7.39 42.67

TCH 7.45 42.61

N End ret 7.11 42.95

T.P. 1.07 46.16 4.97 45.09 B.P. <sup>45.10</sup>

= 1 + 00 =

TCH-N- 3.88 42.28

10' N E 4.27 41.89

E 4.15 42.01

10' S E 4.25 41.91

TCS- 46.16 443 41.73

= 5 + 00 =

TCS 5.10 41.06

10' S E 4.75 41.41

E 4.66 41.50

10' N E 4.70 41.46

TCH 4.22 41.94

= 2 + 70 = Break (?)

TCH- 4.45 41.71

10' N E 5.00 44.16

E 5.00 41.16

10' S E 5.19 40.97

TCS- 5.67 40.49

TCS at sta. 2+87 5.89 40.27

= 2 + 87 = End curb on south line

= 3 + 00 =

10' S E 5.63 40.53

E 5.50 40.66

10' N E 5.42 40.74

TCH 4.99 41.17

T.P. 2.02 42.49 5.89 40.27



= 4400

|              |           |       |                 |
|--------------|-----------|-------|-----------------|
| TCN          | 42.29     | 3.32  | 38.97           |
| 10' N $\phi$ |           | 3.94  | 38.35           |
| $\phi$       |           | 3.82  | 38.47           |
| 10' S $\phi$ |           | 3.94  | 38.35           |
| W.L          | Pendleton |       |                 |
| 10' S $\phi$ |           | 6.41  | 35.88           |
| $\phi$       |           | 6.36  | 35.93           |
| 10' N $\phi$ |           | 6.38  | 35.91           |
| TCN          |           | 5.58  | 36.71           |
| T.P          | 5.41      | 45.94 | 1.76            |
| BM           |           | 0.84  | 45.10 check out |



Cross Section of Curve = 1.0 Super.  
La Jolla Cañon Drive

146.81

26

286 146.81 143.5

PL. 95+105.6 = 473° 51' RT  
R = 500

|       |     |       |
|-------|-----|-------|
| 20 RT | 2.9 | 143.9 |
| 10 RT | 1.4 | 145.4 |
| C     | 1.0 | 145.8 |
| 10 LT | 0.8 | 146.0 |
| 20 LT | 2.3 | 144.5 |

95+15.1

|       |     |       |
|-------|-----|-------|
| 20 LT | 1.5 | 145.3 |
| 10 LT | 1.5 | 145.3 |
| C     | 2.1 | 144.7 |
| 10 RT | 2.6 | 144.2 |
| 20 RT | 3.6 | 143.2 |

96+00

|       |     |       |
|-------|-----|-------|
| 20 RT | 8.3 | 138.5 |
| 10 RT | 4.4 | 142.6 |
| C     | 3.6 | 143.2 |
| 10 LT | 2.7 | 144.1 |
| 20 LT | 4.4 | 144.4 |

96+50

|       |      |       |
|-------|------|-------|
| 20 LT | 3.9  | 142.9 |
| 10 LT | 4.6  | 142.2 |
| C     | 5.3  | 141.5 |
| 10 RT | 6.7  | 140.1 |
| 20 RT | 11.9 | 134.9 |
| 25 RT | 11.9 | 134.9 |

97+00

|       |      |       |
|-------|------|-------|
| 30 RT | 15.4 | 131.4 |
| 20 RT | 10.4 | 132.4 |
| 10 RT | 9.0  | 137.8 |
| C     | 7.7  | 139.1 |
| 10 LT | 6.5  | 140.3 |
| 20 LT | 5.7  | 141.1 |

97+50

|       |      |       |
|-------|------|-------|
| 20 LT | 8.3  | 138.5 |
| 10 LT | 8.3  | 138.5 |
| C     | 9.4  | 137.4 |
| 10 RT | 10.4 | 136.6 |
| 20 RT | 12.9 | 133.9 |
| 30 RT | 17.7 | 129.1 |

98+00

|       |      |       |
|-------|------|-------|
| 36 RT | 21.0 | 125.8 |
| 25 RT | 13.4 | 133.4 |
| 20 RT | 10.9 | 133.9 |
| 10 RT | 10.3 | 134.5 |
| C     | 11.3 | 135.5 |
| 10 LT | 10.9 | 135.9 |
| 20 LT | 10.1 | 136.7 |

98+50.75

|       |      |       |
|-------|------|-------|
| 20 LT | 5.0  | 141.8 |
| 10 LT | 13.0 | 133.8 |
| C     | 13.6 | 133.2 |



146.81

|       |             |       |        |
|-------|-------------|-------|--------|
| 10 RT |             | 13.9  | 132.9  |
| 20 RT |             | 14.7  | 132.1  |
|       | 99+01.48    |       |        |
| 20 RT |             | 16.5  | 130.3  |
| 10 RT |             | 16.2  | 130.6  |
| 6     |             | 16.4  | 130.4  |
| 10 LT |             | 11.5  | 131.3  |
| 20 LT |             | 5.2   | 141.6  |
|       | 99+5.22     |       |        |
| 20 LT |             | 10.1  | 136.7  |
| 10 LT |             | 12.7  | 135.1  |
| T.P.  | 0.32 134.48 | 12.65 | 134.16 |
| C     |             | 6.3   | 128.2  |
| 10 RT |             | 6.5   | 128.0  |
| 20 RT |             | 6.4   | 128.1  |
|       | 100+0.96    |       |        |
| 20 RT |             | 8.9   | 125.6  |
| 10 RT |             | 8.9   | 125.6  |
| C     |             | 9.5   | 125.0  |
| 10 LT |             | 5.4   | 130.1  |
| 20 LT |             | 1.6   | 132.9  |
|       | 100+53.70   |       |        |
| 20 LT |             | 4.4   | 132.1  |
| 10 LT |             | 7.2   | 127.3  |
| C     |             | 7.4   | 123.1  |
| 10 RT |             | 10.9  | 123.6  |

134.48

27

|       |                |      |        |
|-------|----------------|------|--------|
| 20 RT |                | 11.0 | 123.5  |
|       | 101+0.22       |      |        |
| 20 RT |                | 13.5 | 121.0  |
| 10 RT |                | 13.0 | 121.5  |
| C     |                | 13.2 | 121.3  |
| 2 LT  |                | 13.7 | 121.3  |
| 10 LT |                | 9.7  | 124.8  |
| 20 LT |                | 1.3  | 133.20 |
|       | 101+55.58 = EC |      |        |
| 20 LT |                | 12.2 | 122.2  |
| 10 LT |                | 15.3 | 119.2  |
| C     |                | 15.2 | 119.30 |
| 10 RT |                | 15.4 | 119.1  |
| 20 RT |                | 16.0 | 118.5  |

$$\begin{array}{r}
 12.2 \\
 122.18 \\
 119.50 \\
 \hline
 12.68 = 47.6
 \end{array}$$



## X Section Cherokee

390.74

Madison to E/ Cajohn

5+00 (35.65 wide) 5.43

0+00 = N.L. Monroe

wcb 5.93 3848

B.M. S.E.B.R. Monroe + Cherokee 386.68

Gut 6.5

T.P. 4.06 390.74

 $\frac{1}{4}$  6.0Sec taken on diagonal w/ station 6+42 E.L. station 5+45<sup>12</sup> $\frac{1}{4}$  5.7

wcb 6.54 3842

 $\frac{1}{4}$  5.8

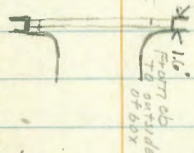
Gut. on Flowline of 6" iron pipe running from SL

Gut 6.1

Madison to N.L. Madison Both ends set in cement

Ecb 5.62 3851

box



4+50 (35.55 wide)

Ecb 5.59 385.2

F Lot pipe 7.38

Gut 6.1

 $\frac{1}{4}$  6.6 $\frac{1}{4}$  5.8 $\frac{1}{4}$  6.1 $\frac{1}{4}$  5.6 $\frac{1}{4}$  6.1 $\frac{1}{4}$  5.8

Gut 6.4

Gut 6.4

Ecb 5.75 385.0

wcb 5.75 385.0

5+45<sup>12</sup> (East line) (35.5 wide)

4+00 (35.65 wide)

Ecb 5.75 385.0

wcb 5.64 385.1

Gut 6.4

4+00 (35.65 wide)

 $\frac{1}{4}$  6.0

wcb 5.64 385.1

 $\frac{1}{4}$  5.9

Gut 6.1

 $\frac{1}{4}$  6.2 $\frac{1}{4}$  5.8

Gut 6.5

 $\frac{1}{4}$  5.8

wcb 6.18 384.6

 $\frac{1}{4}$  5.6 $\frac{1}{4}$  5.6

Gut 5.8

Ecb 5.78 385.3

Ecb 5.78 385.3

3+50 (35.60 wide)



|               |              |      |                              |
|---------------|--------------|------|------------------------------|
| E cb          | 390.74       | 5.26 | 3855                         |
| Gut           |              | 5.8  |                              |
| $\frac{1}{4}$ |              | 5.5  |                              |
| $\frac{1}{4}$ |              | 5.2  |                              |
| $\frac{1}{4}$ |              | 5.4  |                              |
| Gut           |              | 5.7  |                              |
| w cb          |              | 5.33 | 3854                         |
| 3+00          | (35.65 wide) |      |                              |
| w cb          |              | 5.21 | 3855                         |
| Gut           |              | 5.7  |                              |
| $\frac{1}{4}$ |              | 5.4  |                              |
| $\frac{1}{4}$ |              | 5.1  |                              |
| $\frac{1}{4}$ |              | 5.3  |                              |
| Gut           |              | 5.7  |                              |
| E cb          |              | 5.14 | 3856                         |
| 2+44          | (35.65 wide) |      | = 4' 10" corr. drive on East |
| E Gut         |              | 5.31 |                              |
| $\frac{1}{4}$ |              | 5.1  |                              |
| $\frac{1}{4}$ |              | 4.8  |                              |
| $\frac{1}{4}$ |              | 5.1  |                              |
| Gut           |              | 5.5  |                              |
| w cb          |              | 4.86 | 3859                         |
| 2+00          | (35.65 wide) |      |                              |
| w cb          |              | 4.69 | 3861                         |
| Gut           |              | 5.4  |                              |
| $\frac{1}{4}$ |              | 4.8  |                              |

|                 |                              |      |              |
|-----------------|------------------------------|------|--------------|
|                 | 390.74                       |      |              |
| $\frac{1}{4}$   |                              | 4.7  |              |
| $\frac{1}{4}$   |                              | 4.9  |              |
| Gut             |                              | 5.3  |              |
| E cb            |                              | 4.67 | 3861         |
| 1+50            | (35.50 wide)                 |      |              |
| E cb            |                              | 4.50 | 3862         |
| Gut             |                              | 5.1  |              |
| $\frac{1}{4}$   |                              | 4.7  |              |
| $\frac{1}{4}$   |                              | 4.5  |              |
| $\frac{1}{4}$   |                              | 4.7  |              |
| Gut             |                              | 5.1  |              |
| w cb            |                              | 4.45 | 3863         |
| 0+93            | = 4' 10" corr. drive on East |      | (35.50 wide) |
| w cb            |                              | 4.13 | 3866         |
| Gut             |                              | 5.0  |              |
| $\frac{1}{4}$   |                              | 4.5  |              |
| $\frac{1}{4}$   |                              | 4.2  |              |
| $\frac{1}{4}$   |                              | 4.5  |              |
| Gut or concrete |                              | 4.84 |              |
| 0+44            | = 4' 8" corr. drive on East  |      | (35.65 wide) |
| E Gut           |                              | 4.53 |              |
| $\frac{1}{4}$   |                              | 4.3  |              |
| $\frac{1}{4}$   |                              | 4.0  |              |
| $\frac{1}{4}$   |                              | 4.3  |              |
| Gut             |                              | 4.6  |              |



39074

wcb 3.95 386.8

0+00 = NL Manhole (35.65 wide)

wcb 3.66 387.1

Gut 4.1

 $\frac{1}{4}$  4.1 $\frac{1}{2}$  3.9 $\frac{1}{4}$  4.0

Gut 4.3

Ecb 4.00 386.7

Curb = 6' iron pipe crossing from E.L. Cherokee to  
W.L. Cherokee Both ends set in concrete

EL on cb 4.09

EL on FL of pipe 5.20

cb 4.1

 $\frac{1}{4}$  3.8 $\frac{1}{2}$  3.8 $\frac{1}{4}$  3.9

cb 4.1

WL on FL of pipe 4.49

WL on cb 3.52

Quarter

WL 3.8

cb 3.8

 $\frac{1}{4}$  3.7 $\frac{1}{2}$  3.8 $\frac{1}{4}$  3.8

cb 3.8

EL 4.0

Center

EL 4.0

cb 3.8

 $\frac{1}{4}$  3.7 $\frac{1}{2}$  3.7 $\frac{1}{4}$  3.7

cb 3.6

WL 3.7

Quarter

WL 3.8

cb 3.7

 $\frac{1}{4}$  3.7 $\frac{1}{2}$  3.8 $\frac{1}{4}$  3.8

cb 3.8

EL 4.2

Curb

EL on cb 4.02

EL Gut 4.5

cb 4.0



39084

|              |                          |             |            |
|--------------|--------------------------|-------------|------------|
| 7            |                          | 3.8         |            |
| 2            |                          | 3.8         |            |
| 1/4          |                          | 3.9         |            |
| cb           |                          | 4.0         |            |
| W.L. on Gut  |                          | 4.3         |            |
| W.L. on cb   |                          | 3.54        |            |
| T.P.         | 4.16                     | 39084       | 4.06 38668 |
| 6+00 =       | SL MONROE                | (35.5 wide) |            |
| Wcb          |                          | 3.83        | 3870       |
| Gut          |                          | 4.4         |            |
| 1/4          |                          | 4.3         |            |
| 2            |                          | 4.1         |            |
| 1/4          |                          | 4.3         |            |
| Gut          |                          | 4.5         |            |
| E cb         |                          | 4.9         | 3859 ?     |
| 5+64 =       | 2 9.7' con drive on west | (35.5 wide) |            |
| Ecb          |                          | 4.35        | 3865       |
| Gut          |                          | 5.0         |            |
| 1/4          |                          | 4.5         |            |
| 2            |                          | 4.4         |            |
| 1/4          |                          | 4.4         |            |
| W Gut on con |                          | 4.65        |            |
| 5+30 =       | 2 9.7' con drive on west |             |            |
| Gut on con   |                          | 4.84        |            |
| 4+91-50 =    | 2 8.5' con drive on west | (35.7 wide) |            |

|            |                        |      |       |
|------------|------------------------|------|-------|
| W Gut      |                        | 4.87 |       |
| 7          |                        | 4.7  |       |
| 2          |                        | 4.6  |       |
| 1/4        |                        | 4.8  |       |
| Gut        |                        | 5.3  |       |
| E cb       |                        | 4.74 | 386.1 |
| 4+65 =     | 2 9' con drive on East |      |       |
| Gut on con |                        | 5.35 |       |
| 4+50       | (35.60) wide           |      |       |
| Ecb        |                        | 4.87 | 3860  |
| Gut        |                        | 5.7  |       |
| 1/4        |                        | 5.1  |       |
| 2          |                        | 4.9  |       |
| 1/4        |                        | 5.0  |       |
| Gut        |                        | 5.3  |       |
| Wcb        |                        | 4.68 | 3862  |
| 4+00       | (35.7 wide)            |      |       |
| Wcb        |                        | 4.92 | 385.9 |
| Gut        |                        | 5.5  |       |
| 1/4        |                        | 5.3  |       |
| 2          |                        | 5.1  |       |
| 1/4        |                        | 5.3  |       |
| Gut        |                        | 5.8  |       |
| Ecb        |                        | 5.17 | 385.7 |
| 3+50       | (35.75 wide)           |      |       |



390.84

|   |             |  |             |
|---|-------------|--|-------------|
| E cb  |             | 5.69                                   | 385.2       |
| Gut   |             | 6.3                                    |             |
| $\frac{1}{4}$                               |             | 5.6                                    |             |
| $\frac{1}{4}$                               |             | 5.3                                    |             |
| $\frac{1}{4}$                               |             | 5.3                                    |             |
| Gut   |             | 5.9                                    |             |
| wcb   |             | 5.21                                   | 385.6       |
| 3+14  | (35.7 wide) | = $\frac{1}{4}$ 9.2' con drive on west |             |
| w. Gut                                      |             | 5.91                                   |             |
| $\frac{1}{4}$                               |             | 5.7                                    |             |
| $\frac{1}{4}$                               |             | 5.4                                    |             |
| $\frac{1}{4}$                               |             | 5.8                                    |             |
| Gut   |             | 6.5                                    |             |
| E cb  |             | 5.77                                   | 385.1       |
| 2+42  | (35.6 wide) | = $\frac{1}{4}$ 16' con drive on East  |             |
| E Gut                                       |             | 6.63                                   |             |
| $\frac{1}{4}$                               |             | 6.2                                    |             |
| $\frac{1}{4}$                               |             | 5.9                                    |             |
| $\frac{1}{4}$                               |             | 6.2                                    |             |
| Gut   |             | 6.7                                    |             |
| wcb   |             | 5.97                                   | 384.9       |
| T.P.  | 4.39        | 389.52                                 | 5.71 385.13 |
| (2+06 = $\frac{1}{4}$ 9.6 con drive on East |             |  |             |
| { Gut on con.                               |             | 5.50                                   |             |
| 2+00  | (35.4 wide) |  |             |
| wcb   |             | 4.82                                   | 384.1       |

389.52

32

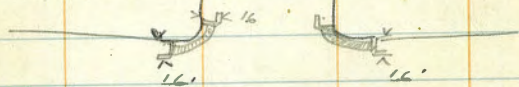
|  |              |      |       |
|--|--------------|------|-------|
| Gut  |              | 5.3  |       |
| $\frac{1}{4}$  |              | 5.1  |       |
| $\frac{1}{4}$  |              | 4.9  |       |
| $\frac{1}{4}$  |              | 5.2  |       |
| Gut  |              | 5.1  |       |
| E cb   |              | 5.02 | 384.5 |
| 1+50   | (35.45 wide) |      |       |
| E cb   |              | 5.31 | 384.2 |
| Gut  |              | 5.9  |       |
| $\frac{1}{4}$  |              | 5.4  |       |
| $\frac{1}{4}$  |              | 5.1  |       |
| $\frac{1}{4}$  |              | 5.2  |       |
| Gut  |              | 5.5  |       |
| wcb  |              | 4.86 | 384.7 |
| 1+00   | (35.4 wide)  |      |       |
| wcb  |              | 5.19 | 384.3 |
| Gut  |              | 5.8  |       |
| $\frac{1}{4}$  |              | 5.5  |       |
| $\frac{1}{4}$  |              | 5.4  |       |
| $\frac{1}{4}$  |              | 5.7  |       |
| Gut  |              | 6.1  |       |
| E cb   |              | 5.52 | 384.8 |
| (0+56 (35.9 wide) = $\frac{1}{4}$ 10.2 drive on East |              |      |       |
| { Gut on con   |              | 6.30 |       |
| $\frac{1}{4}$  |              | 5.9  |       |



389.52

|     |          |
|-----|----------|
| ¢   | 56       |
| ¢   | 5.6      |
| Gut | 60       |
| Wcb | 536 3842 |

0+00 = N<sup>h</sup> OLIVE (35.86 wide) = 8" iron pipe running  
around both East & West Returns. Ends of pipe set in con



olive st Meade Ave.

|   |      |        |      |        |
|---|------|--------|------|--------|
| Wcb                                     | 5.61 | 3839   |      |        |
| EL PIPE                                 | 6.57 |        |      |        |
| ¢                                       | 5.8  |        |      |        |
| ¢                                       | 5.9  |        |      |        |
| ¢                                       | 5.9  |        |      |        |
| EL pipe                                 | 6.96 |        |      |        |
| Ecb                                     | 6.02 | 383.5  |      |        |
| Curb                                    |      |        |      |        |
| ELcb                                    | 5.97 |        |      |        |
| EL FL pipe                              | 6.99 |        |      |        |
| WL cb                                   | 5.47 |        |      |        |
| WL FL pipe                              | 6.95 |        |      |        |
| T.P.                                    | 2.45 | 387.19 | 4.78 | 384.74 |
| 0+08 = S <sup>h</sup> OLIVE (35.8 wide) |      |        |      |        |
| Ecb                                     | 2.63 | 384.6  |      |        |
| Gut                                     | 2.9  |        |      |        |

387.19

|                  |      |       |
|------------------|------|-------|
| ¢                | 2.5  |       |
| ¢                | 2.3  |       |
| ¢                | 2.5  |       |
| Gut              | 2.8  |       |
| Wcb              | 2.23 | 385.0 |
| 5+50 (35.7 wide) |      |       |
| Wcb              | 3.01 | 384.2 |
| Gut              | 3.7  |       |
| ¢                | 3.3  |       |
| ¢                | 3.4  |       |
| ¢                | 3.4  |       |
| Gut              | 3.9  |       |
| Ecb              | 3.41 | 383.8 |
| 5+00 (35.7 wide) |      |       |
| Ecb              | 4.09 | 383.1 |
| Gut              | 4.6  |       |
| ¢                | 4.1  |       |
| ¢                | 3.8  |       |
| ¢                | 3.9  |       |
| Gut              | 4.5  |       |
| Wcb              | 3.71 | 383.5 |
| 4+50 (35.7 wide) |      |       |
| Wcb              | 4.42 | 382.8 |
| Gut              | 5.1  |       |
| ¢                | 4.6  |       |



387.19

|   |  |       |
|---|--|-------|
| ¢   | 43   |       |
| $\frac{1}{4}$                               | 47   |       |
| Gut   | 53   |       |
| E cb  | 472  | 382.5 |
| 4+15 <sup>50</sup>                          | (35.6 wide) ¢ <sup>10'</sup> con drive on west |       |
| E cb  | 5.22   | 382.0 |
| Gut   | 5.8  |       |
| $\frac{1}{4}$                               | 5.3  |       |
| ¢   | 4.9  |       |
| $\frac{1}{4}$                               | 5.1  |       |
| WGut on con                                 | 5.37   |       |
| 3+50  | (35.6 wide)                                    |       |
| wcb   | 5.01   | 381.6 |
| Gut   | 6.5  |       |
| $\frac{1}{4}$                               | 6.0  |       |
| ¢   | 5.9  |       |
| $\frac{1}{4}$                               | 6.2  |       |
| Gut   | 6.7  |       |
| E cb  | 6.07   | 381.1 |
| 3+28 = ¢ con drive on west                  |  |       |
| { Gut on drive                              | 6.52   |       |
| 3+20 = ¢ 95' con drive on east              |  |       |
| { Gut on con                                | 6.89   |       |
| 2+94 <sup>50</sup> = ¢ 9' con drive on west | (35.65 wide)                                   |       |
| E cb  | 6.78   | 380.4 |

387.19

|   |      |        |
|---|------|--------|
| Gut   | 76   |        |
| $\frac{1}{4}$                                 | 7.0  |        |
| ¢   | 6.7  |        |
| $\frac{1}{4}$                                 | 6.8  |        |
| Gut on con                                    | 6.90 |        |
| 2+68 <sup>50</sup> = ¢ 92' con drive on East  |      |        |
| { Gut on con                                  | 7.54 |        |
| 2+62 = ¢ 9' con drive on west                 |      |        |
| { Gut on con                                  | 7.34 |        |
| 2+20 (35.65 wide) ¢ 10' con drive on East     |      |        |
| wcb   | 7.42 | 379.8  |
| Gut   | 8.2  |        |
| $\frac{1}{4}$                                 | 7.7  |        |
| ¢   | 7.7  |        |
| $\frac{1}{4}$                                 | 7.9  |        |
| E Gut on con                                  | 8.14 |        |
| 2+15 = ¢ 10' con drive on west                |      |        |
| { Gut on con                                  | 8.08 |        |
| T.P.  | 3.67 | 382.36 |
| 1+57 <sup>40</sup> = NL 15' Alley (35.7 wide) |      |        |
| EL on cb                                      | 3.62 | 378.7  |
| EL on ground                                  | 3.6  |        |
| cb  | 3.70 |        |
| Gut   | 4.2  |        |
| $\frac{1}{4}$                                 | 4.0  |        |



382.36

|                               |      |       |
|-------------------------------|------|-------|
| ♀                             | 3.8  |       |
| ♂                             | 3.9  |       |
| Gut                           | 4.1  |       |
| w cb                          | 3.54 | 378.8 |
| WL oncb                       | 3.29 |       |
| WL on ground                  | 3.3  |       |
| 1+42 <sup>60</sup> = SL Alley |      |       |
| WL oncb                       | 3.48 |       |
| WL on ground                  | 3.5  |       |
| cb                            | 3.77 | 378.6 |
| Gut                           | 4.3  |       |
| ♂                             | 4.0  |       |
| ♀                             | 3.9  |       |
| ♂                             | 4.2  |       |
| Gut                           | 4.3  |       |
| cb                            | 4.12 | 378.2 |
| EL oncb                       | 3.87 | 378.5 |
| EL on ground                  | 3.9  |       |
| 1+00 (35.7 wide)              |      |       |
| E cb                          | 4.69 | 377.7 |
| Gut                           | 5.1  |       |
| ♂                             | 4.9  |       |
| ♀                             | 4.6  |       |
| ♂                             | 4.7  |       |
| Gut                           | 5.2  |       |

382.36

35

|                                  |      |        |
|----------------------------------|------|--------|
| w cb                             | 4.43 | 377.9  |
| 0+50 (35.65 wide)                |      |        |
| w cb                             | 4.97 | 377.4  |
| Gut                              | 5.7  |        |
| ♂                                | 5.4  |        |
| ♀                                | 5.3  |        |
| ♂                                | 5.6  |        |
| Gut                              | 6.0  |        |
| E cb                             | 5.46 | 376.9  |
| 0+00 (35.85 wide) = NL. EL Cajon |      |        |
| E cb                             | 6.06 | 376.3  |
| Gut                              | 6.57 |        |
| ♂                                | 6.14 |        |
| ♀                                | 5.89 |        |
| ♂                                | 6.01 |        |
| Gut                              | 6.24 |        |
| w cb                             | 5.67 | 376.7  |
| T.P.                             | 9.06 | 376.41 |
| T.P.                             | 1.01 | 376.35 |
|                                  | 3.74 | 376.67 |
|                                  |      | 376.68 |
| B.M. SE.B.P. Monroe + Cherokee   |      | .01    |



26.00 wide at WL 35<sup>th</sup>

X Sec Polk 35<sup>th</sup> to Wabash

All intersections paraded

0+00 = WL 35<sup>th</sup>

B.M. = NWBB Orange 35 378.12

T.P. 1.53 379.65

T.P. 4.64 375.17 912 370.53

0+00 on diagonal

Ncb 4.60 370.57

Gut 5.27 369.90

$\frac{1}{4}$  5.13

$\frac{1}{4}$  5.09

$\frac{1}{4}$  5.20

Gut 5.57 369.60

S cb 5.15 370.02

0+00 (RRS) + 8 $\frac{1}{2}$ ' on Ncb

S cb 5.15 370.02

Gut 5.57

$\frac{1}{4}$  5.2

$\frac{1}{4}$  4.9

$\frac{1}{4}$  5.2

Gut 5.1

Ncb 4.67 370.50

0+50 (26.80 wide)

Ncb 4.82 370.35

Gut 5.4

$\frac{1}{4}$  5.1

375.11

36

$\frac{1}{4}$  4.9

$\frac{1}{4}$  5.2

Gut 5.6

S cb 5.24

369.93

{ 10+72<sup>69</sup> =  $\frac{1}{4}$  12' on drive on North

{ Gut on drive 5.29

0+95 (26.85 wide =  $\frac{1}{4}$  9' drive on South

Gut on drive 5.88 369.29

$\frac{1}{4}$  5.4

$\frac{1}{4}$  5.1

$\frac{1}{4}$  5.2

Gut 5.3

Ncb 4.89 370.28

1+15<sup>70</sup> = EL Alley on North (Ncb) 4.96 <sup>370.21</sup> (26.80 wide)

1+38<sup>30</sup> = WL Alley on North & EL Alley on South

Ncb 5.10 370.07

Gut 5.43

$\frac{1}{4}$  5.3

$\frac{1}{4}$  5.3

$\frac{1}{4}$  5.5

Gut 5.9

S cb 5.48 369.69

1+50<sup>70</sup> =  $\frac{1}{4}$  M.H.

S cb + 13' 5.42

{ 1+52 = WL Alley on South

{ S cb 5.48 369.69

Plotted  
H.C.H.  
A/3/28



|  |              |                                     |                            |
|--|--------------|-------------------------------------|----------------------------|
| 9+55 <sup>SD</sup> = 2 19' curb drive on North |              |                                     |                            |
| Gut  | on drive     | 5.67                                |                            |
| 2+00   | (26.50) wide | curb on North from this point on is | falling away from sidewalk |
| S cb   |              | 5.54                                | 369.63                     |
| Gut  |              | 6.2                                 |                            |
| $\frac{1}{4}$                                  |              | 5.7                                 |                            |
| $\phi$   |              | 5.6                                 |                            |
| $\frac{1}{4}$                                  |              | 5.8                                 |                            |
| Gut  |              | 5.6                                 |                            |
| N cb   |              | 5.30                                | 369.87                     |

|                              |             |        |             |
|------------------------------|-------------|--------|-------------|
| 2+06 = 2 11' drive on South  |             |        |             |
| Gut                          | on drive    | 6.27   |             |
| 2+50                         | (26.6 wide) |        |             |
| N cb                         |             | 5.48   | 369.74      |
| Gut                          |             | 5.7    |             |
| $\frac{1}{4}$                |             | 5.9    |             |
| $\phi$                       |             | 5.9    |             |
| $\frac{1}{4}$                |             | 6.2    |             |
| Gut                          |             | 6.3    |             |
| S cb                         |             | 5.83   | 369.34      |
| T.P.                         | 4.02        | 373.30 | 5.83 369.34 |
| 2+99 = EL SWIFT (26.70 wide) |             |        |             |
| S cb                         |             | 4.17   | 369.19      |
| Gut                          |             | 4.64   | 368.72      |
| $\frac{1}{4}$                |             | 4.37   |             |
| $\phi$                       |             | 4.25   |             |

|                              |  |      |        |
|------------------------------|--|------|--------|
| $\frac{1}{4}$                |  | 4.25 |        |
| Gut                          |  | 4.39 | 368.97 |
| N cb                         |  | 3.79 | 369.67 |
| 0+00 = NL SWIFT (26.65 wide) |  |      |        |
| N cb                         |  | 4.27 | 369.09 |
| Gut                          |  | 5.10 | 368.26 |
| $\frac{1}{4}$                |  | 4.80 |        |
| $\phi$                       |  | 4.87 |        |
| $\frac{1}{4}$                |  | 4.97 |        |
| Gut                          |  | 5.18 | 368.18 |
| S cb                         |  | 4.71 | 368.65 |
| 0+50 (26.65 wide)            |  |      |        |
| S cb                         |  | 5.55 | 367.81 |
| Gut                          |  | 6.0  |        |
| $\frac{1}{4}$                |  | 5.7  |        |
| $\phi$                       |  | 5.4  |        |
| $\frac{1}{4}$                |  | 5.5  |        |
| Gut                          |  | 6.0  |        |
| N cb                         |  | 5.18 | 368.18 |
| 1+00 (26.70 wide)            |  |      |        |
| N cb                         |  | 5.93 | 367.43 |
| Gut                          |  | 6.8  |        |
| $\frac{1}{4}$                |  | 6.4  |        |
| $\phi$                       |  | 6.3  |        |
| $\frac{1}{4}$                |  | 6.6  |        |



573.32

38

|     |      |        |
|-----|------|--------|
| Gut | 6.9  |        |
| Scb | 6.34 | 367.02 |

(1+31) + 2 9.5' on drive on south

|              |      |  |
|--------------|------|--|
| Gut on drive | 7.17 |  |
|--------------|------|--|

1+38 = E.L. La Verne Place. Paved up to S.L. Polk

|              |      |        |
|--------------|------|--------|
| SL on paving | 6.81 | 366.55 |
|--------------|------|--------|

|     |      |        |
|-----|------|--------|
| Scb | 6.85 | 366.51 |
|-----|------|--------|

|     |     |  |
|-----|-----|--|
| Gut | 7.1 |  |
|-----|-----|--|

|               |     |  |
|---------------|-----|--|
| $\frac{1}{4}$ | 7.0 |  |
|---------------|-----|--|

|               |     |  |
|---------------|-----|--|
| $\frac{1}{2}$ | 6.8 |  |
|---------------|-----|--|

|               |     |  |
|---------------|-----|--|
| $\frac{3}{4}$ | 6.8 |  |
|---------------|-----|--|

|     |     |  |
|-----|-----|--|
| Gut | 7.2 |  |
|-----|-----|--|

|     |      |        |
|-----|------|--------|
| Ncb | 6.52 | 366.84 |
|-----|------|--------|

|          |      |  |
|----------|------|--|
| NL on cb | 6.97 |  |
|----------|------|--|

|              |     |  |
|--------------|-----|--|
| NL on ground | 6.5 |  |
|--------------|-----|--|

1+97<sup>85</sup> S

|              |      |        |
|--------------|------|--------|
| NL on paving | 7.08 | 366.28 |
|--------------|------|--------|

|         |      |        |
|---------|------|--------|
| Gut " " | 7.27 | 366.09 |
|---------|------|--------|

|                   |      |  |
|-------------------|------|--|
| $\frac{1}{4}$ " " | 6.88 |  |
|-------------------|------|--|

|                   |      |        |
|-------------------|------|--------|
| $\frac{1}{2}$ " " | 6.78 | 366.58 |
|-------------------|------|--------|

|                   |      |  |
|-------------------|------|--|
| $\frac{3}{4}$ " " | 7.07 |  |
|-------------------|------|--|

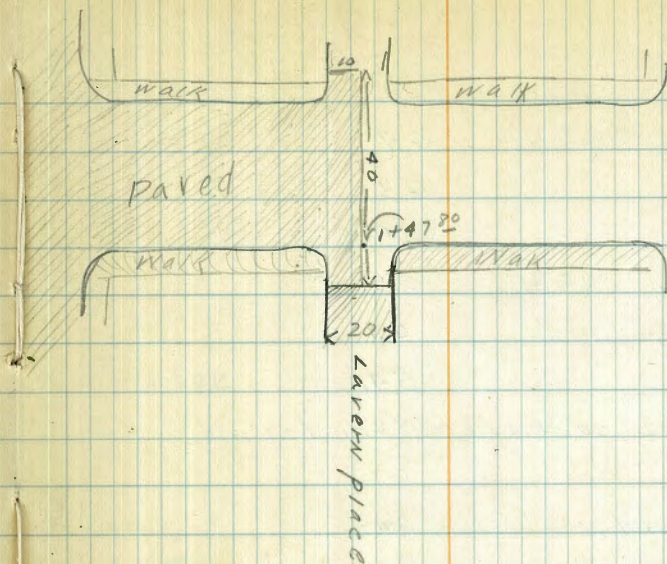
|         |      |        |
|---------|------|--------|
| Gut " " | 7.75 | 365.61 |
|---------|------|--------|

|        |      |        |
|--------|------|--------|
| SL " " | 7.40 | 365.96 |
|--------|------|--------|

|           |        |      |        |
|-----------|--------|------|--------|
| T.P. 1.84 | 366.25 | 8.95 | 364.91 |
|-----------|--------|------|--------|

0+00 = W.L. Scott (26.80 wide) (or 34<sup>th</sup>)

|     |      |        |
|-----|------|--------|
| Scb | 3.20 | 363.05 |
|-----|------|--------|



|       |      |        |
|-------|------|--------|
| S Gut | 3.31 | 362.94 |
|-------|------|--------|

|               |      |  |
|---------------|------|--|
| $\frac{1}{4}$ | 3.09 |  |
|---------------|------|--|

|               |      |  |
|---------------|------|--|
| $\frac{1}{2}$ | 2.97 |  |
|---------------|------|--|

|               |      |  |
|---------------|------|--|
| $\frac{3}{4}$ | 2.96 |  |
|---------------|------|--|

|     |      |        |
|-----|------|--------|
| Gut | 3.01 | 363.24 |
|-----|------|--------|

|     |      |        |
|-----|------|--------|
| Ncb | 2.85 | 363.40 |
|-----|------|--------|

0+50 (26.80 wide)

|     |      |        |
|-----|------|--------|
| Ncb | 4.10 | 362.15 |
|-----|------|--------|

|     |     |  |
|-----|-----|--|
| Gut | 4.7 |  |
|-----|-----|--|

|               |     |  |
|---------------|-----|--|
| $\frac{1}{4}$ | 4.6 |  |
|---------------|-----|--|

|               |     |  |
|---------------|-----|--|
| $\frac{1}{2}$ | 4.6 |  |
|---------------|-----|--|

|               |     |  |
|---------------|-----|--|
| $\frac{3}{4}$ | 4.8 |  |
|---------------|-----|--|

|     |     |  |
|-----|-----|--|
| Gut | 5.8 |  |
|-----|-----|--|

|     |      |        |
|-----|------|--------|
| Scb | 4.86 | 361.39 |
|-----|------|--------|

1+00 (26.80 wide)



S cb 6.41 357.84

Gut 6.9

$\frac{1}{4}$  6.3

$\frac{1}{4}$  5.9

$\frac{1}{4}$  5.9

Gut 6.1

N cb 5.41 360.84

1+3960 = EL 20' Alley on North (27' wide)

NL on cb 6.08

NL on ground 6.4

N cb 6.33 359.92

Gut 7.2

$\frac{1}{4}$  7.0

$\frac{1}{4}$  6.9

$\frac{1}{4}$  7.4

Gut 7.8

S cb 7.54 358.71

{ 1+50 = 4 M.H.

{ S cb + 13.5 7.23

1+5960 = NL Alley on North

S cb 8.04 358.21

Gut 8.7

$\frac{1}{4}$  8.1

$\frac{1}{4}$  7.6

$\frac{1}{4}$  7.6

Gut 7.7

N cb 7.00 359.25

NL on cb 6.82

NL on ground 7.1

2+00 (26.90 wide)

N cb 8.21 358.04

Gut 9.2

$\frac{1}{4}$  8.8

$\frac{1}{4}$  8.8

$\frac{1}{4}$  9.4

Gut 10.2

S cb 9.19 357.06

2+2810 = PC on South (27' wide)

S cb 10.08 356.17

Gut 10.5

$\frac{1}{4}$  10.0

$\frac{1}{4}$  9.6

$\frac{1}{4}$  9.8

Gut 9.8

N cb 9.10 357.15

2+62<sup>21</sup> This station is a production of the Curb Line on South, past the PC. to the existing pavement of Wakash.

N cb 10.40 355.85

Gut 11.03 355.22

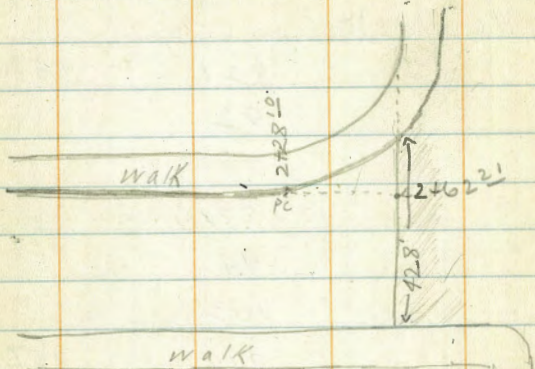
10' south 10.97

20' south 11.10



366.25

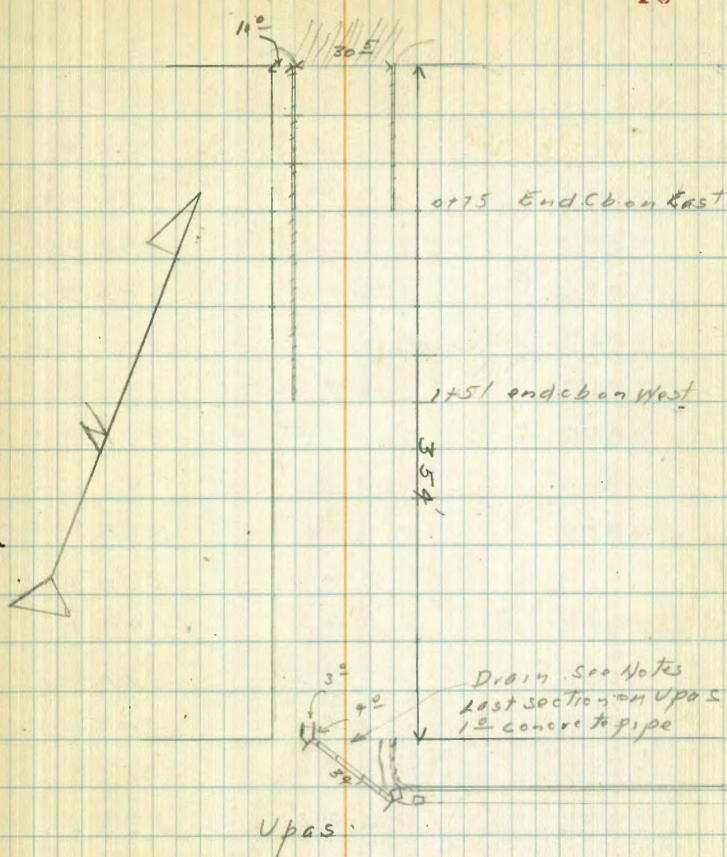
|                   |       |        |
|-------------------|-------|--------|
| 30' south         | 11.30 | 354.91 |
| 42.8' south = Gut | 11.84 | 354.41 |
| 42.8' south = cb  | 11.19 | 355.06 |



|      |          |                         |      |        |
|------|----------|-------------------------|------|--------|
| TR   | 1268     | 376.76                  | 2.17 | 364.08 |
| T.P. | 6.41     | 280.79                  | 238. | 274.38 |
| T.P. |          |                         | 273  | 278.06 |
| BM   | N.W.B.P. | 35 <sup>th</sup> Change |      | 278.12 |
|      |          |                         |      | 06     |

40

Myrtle St





Bliss  
Isbell  
Lowden  
9/10/28  
BM NW BP  
Myrtle Villa Terrace

x Sections of Villa Terrace from  
The S. Line of Myrtle to the N Line of Upas

50.57  
70.062  
7.5103

4.5  
1.4  
- 3.3  
2.6  
- 1.7

30457.41

Platted A-21-1928  
C.B. Fougere

|         |           |                       |             |        |        |
|---------|-----------|-----------------------|-------------|--------|--------|
| 964     | 309.57    | 299.93                | Gutter      | 4.6    | 300.0  |
|         | on Paving | 0100 S Line of Myrtle | 40? E Topcb | 4.20   | 300.37 |
| W Topcb | 4.61      | 299.96                | 50'S        |        |        |
| Gutter  | 5.14      | 299.43                | E Topcb     | 4.81   | 299.76 |
| 1/4     | 4.68      | 299.89                | Gutter      | 5.3    | 299.3  |
| 1/2     | 4.35      | 300.22                | 1/4         | 5.5    | 299.1  |
| 3/4     | 4.19      | 300.48                | 1/2         | 5.5    | 299.1  |
| Gutter  | 4.32      | 300.25                | 1/4         | 6.1    | 298.5  |
| E Topcb | 3.58      | 300.99                | Gutter      | 6.6    | 298.0  |
|         | 08'S      |                       | T.P. 2.25   | 300.68 | 6.14   |
| E Topcb | 3.80      | 300.77                | N Topcb     | 1.85   | 298.83 |
| Gutter  | 4.4       | 300.2                 | 75'S        |        |        |
| 1/5     | 4.7       | 299.9                 | N Topcb     | 2.44   | 298.24 |
| 1/4     | 4.5       | 300.1                 | Gutter      | 3.2    | 297.5  |
| 1/5     | 4.5       | 300.1                 | 1/4         | 2.7    | 298.0  |
| 1/2     | 4.6       | 300.0                 | 1/2         | 2.1    | 298.6  |
| 1/5     | 4.8       | 299.8                 | 1/4         | 2.2    | 298.5  |
| 1/4     | 5.1       | 299.5                 | Gutter      | 1.9    | 298.8  |
| Gutter  | 5.4       | 299.2                 | E Topcb     | 1.50   | 299.18 |
| Topcb   | 4.81      | 299.76                | E           | 1.2    | 299.5  |
|         | 25'S      |                       | 77'S        |        |        |
| W Topcb | 5.20      | 299.37                | E           | 1.7    | 299.0  |
| Gutter  | 6.0       | 298.6                 | E + 7       | 1.2    | 299.5  |
| 1/4     | 5.5       | 299.2                 | cb          | 1.9    | 298.8  |
| 1/2     | 5.0       | 299.6                 | 1/2         | 2.2    | 298.5  |
| 1/4     | 5.0       | 299.6                 | 1/4         | 2.2    | 298.5  |



7  
300.68

30412

42

|        |      |        |                |        |       |       |
|--------|------|--------|----------------|--------|-------|-------|
| 2      |      | 2.2    | 298.5          | 1/4    | 7.9   | 2962  |
| 1/4    |      | 2.7    | 298.0          | +3     | 8.2   | 2959  |
| Gutter |      | 3.3    | 297.4          | Gutter | 8.2   | 2959  |
| WT.pcb |      | 2.99   | 298.19         | Topcb  | 7.99  | 29663 |
| TF     | 6.99 | 304.18 | 3.05           | W      | 7.2   | 2969  |
|        |      | 100'S  |                |        | 200'S |       |
| WT.pcb |      | 6.98   | 297.64         | W      | 8.9   | 295.7 |
| Gutter |      | 7.2    | 296.9          | cb     | 8.8   | 295.3 |
| +2     |      | 7.2    | 296.9          | +2     | 9.0   | 295.1 |
| 1/4    |      | 6.9    | 297.2          | 1/4    | 9.1   | 295.0 |
| 2      |      | 6.2    | 297.9          | 2      | 8.4   | 295.7 |
| +4     |      | 6.1    | 298.0          | +3     | 8.3   | 295.8 |
| 1/4    |      | 6.1    | 298.0          | 1/4    | 8.3   | 295.8 |
| cb     |      | 6.0    | 298.1          | +3     | 8.5   | 295.6 |
| +1     |      | 5.5    | 298.6          | +6     | 8.6   | 295.5 |
| +6     |      | 5.1    | 299.0          | cb     | 8.0   | 296.1 |
| E      |      | 3.0    | 301.1          | +8     | 7.6   | 296.5 |
|        |      | 151'S  | End cb on West | E      | 6.8   | 297.3 |
| E      |      | 4.2    | 299.9          |        | 250'S |       |
| +9     |      | 6.2    | 297.9          | E      | 8.2   | 295.9 |
| +8     |      | 6.3    | 297.8          | +2     | 8.8   | 295.3 |
| cb     |      | 7.0    | 297.1          | +7     | 8.8   | 295.3 |
| +2     |      | 7.4    | 296.7          | cb     | 9.2   | 294.9 |
| +5     |      | 7.5    | 296.6          | +1     | 9.6   | 294.5 |
| 1/4    |      | 7.2    | 296.9          | 1/4    | 9.8   | 294.3 |
| 2      |      | 7.3    | 296.8          | 1/4    | 9.5   | 294.6 |



309.12

|     |       |       |
|-----|-------|-------|
| +5  | 9.5   | 294.6 |
| ±   | 9.5   | 294.6 |
| 1/4 | 10.2  | 293.9 |
| 1/4 | 10.8  | 293.3 |
| cb  | 10.0  | 294.1 |
| W   | 9.9   | 294.2 |
|     | 300'S |       |
| W   | 11.0  | 293.1 |
| +7  | 11.0  | 293.1 |
| cb  | 11.3  | 292.8 |
| +3  | 11.7  | 292.4 |
| 1/4 | 11.4  | 292.7 |
| ±   | 10.7  | 293.4 |
| 1/4 | 10.6  | 293.5 |
| +4  | 11.1  | 293.0 |
| cb  | 10.8  | 293.5 |
| +4  | 10.1  | 293.0 |
| ±   | 9.6   | 294.5 |
|     | 335'S |       |
| E   | 10.5  | 293.6 |
| +7  | 10.9  | 293.2 |
| cb  | 11.9  | 292.7 |
| +3  | 11.6  | 292.5 |
| 1/4 | 11.2  | 292.9 |
| ±   | 11.2  | 292.9 |
| 1/4 | 11.8  | 292.3 |

309.12

43

|                                       |                       |        |
|---------------------------------------|-----------------------|--------|
| +4                                    | 12.0                  | 292.1  |
| cb                                    | 11.8                  | 292.3  |
| +4                                    | 11.6                  | 292.5  |
| W                                     | 11.7                  | 292.4  |
| TP                                    | 5.60                  | 298.26 |
|                                       | 11.96                 | 292.66 |
|                                       | 354'S. N Line of Upas |        |
| W                                     | 7.5                   | 290.8  |
| +7                                    | 6.0                   | 292.3  |
| cb                                    | 5.9                   | 292.4  |
| +1. Top Box                           | 6.50                  | 291.76 |
| +1. Bottom Box                        | 7.91                  | 290.35 |
| +3. Edge Box                          | 8.06                  | 290.20 |
| +3 Top                                | 6.50                  | 291.76 |
| Flowline Drain 1 <sup>st</sup> Drain  | 8.09                  | 290.17 |
| +5                                    | 5.6                   | 292.7  |
| 1/4                                   | 5.1                   | 293.2  |
| ±                                     | 5.5                   | 292.8  |
| +3                                    | 5.4                   | 292.9  |
| 1/4                                   | 5.7                   | 292.6  |
| +4.5 edge concrete Cutoff             | 5.72                  | 292.54 |
| Cutoff                                | 5.98                  | 292.28 |
| E Top of                              | 5.29                  | 292.97 |
| Set B.M. on N.E. Return Villa Terrace |                       |        |
| + Upas                                | 5.29                  | 292.97 |



Bliss  
Isbell  
Lowden  
4/20/28  
BN SW. Return  
Myrtle + Pershing

X Sections of Upas from  
the W Curb Line of Pershing to the W Line  
of Villa Terrace

80.57  
20.06  
10.14

0+10.3 flow line 8" 1" - 9.76  
326.39

Platted A-21-1928  
C.B. Hoag 9 b

|      |        |        |               |       |        |
|------|--------|--------|---------------|-------|--------|
| 4.41 | 330.39 | 325.98 | +7            | 4.5   |        |
| 2.43 | 326.39 | 323.96 | 1/4           | 4.3   |        |
|      |        |        | cb            | 4.7   |        |
|      |        |        | +7            | 5.0   |        |
|      |        |        | 5.            | 5.2   | 321.2  |
|      |        |        |               | 50' W |        |
|      |        |        | 5             | 5.8   | 320.6  |
|      |        |        | +5            | 5.9   |        |
|      |        |        | +6            | 7.2   |        |
|      |        |        | +8            | 7.4   |        |
|      |        |        | +10           | 5.9   |        |
|      |        |        | cb            | 5.9   |        |
|      |        |        | 1/4           | 6.2   |        |
|      |        |        | +7            | 6.1   |        |
|      |        |        | cut on paving | 6.85  | 319.54 |
|      |        |        | 1/4           | 6.72  |        |
|      |        |        | Gutter        | 7.01  |        |
|      |        |        | N Top cb      | 6.36  | 320.03 |
|      |        |        |               | 59' W |        |
|      |        |        | N Top cb      | 7.09  | 319.30 |
|      |        |        | Gutter        | 7.79  |        |
|      |        |        | 1/4           | 7.78  |        |
|      |        |        | cut           | 7.59  | 318.80 |
|      |        |        | +2            | 7.0   |        |
|      |        |        | 1/6           | 6.8   |        |
|      |        |        | cb            | 6.8   |        |



326.39

326.39

45

|           |          |        |
|-----------|----------|--------|
| +11       | 6.8      |        |
| +12       | 7.7      |        |
| +14       | 7.8      |        |
| +15       | 6.8      |        |
| +17       | 6.3      |        |
| S.        | 6.9      | 3200   |
|           | 75' West |        |
| S         | 8.9      | 3180   |
| +3        | 7.9      |        |
| +5        | 8.9      |        |
| +7        | 8.9      |        |
| +8        | 8.1      |        |
| cb        | 8.9      |        |
| 1/4       | 8.1      |        |
| +7        | 8.0      |        |
| on paving | 8.74     | 317.65 |
| 1/4       | 8.76     |        |
| Gutter    | 8.94     |        |
| N Top cb  | 8.31     | 318.08 |
|           | 92'S     |        |
| N Top cb  | 9.59     | 316.80 |
| Gutter    | 10.25    |        |
| 1/4       | 10.03    |        |
| on paving | 10.09    | 316.30 |
| +2        | 9.2      |        |
| 1/4       | 9.4      |        |

|           |           |        |
|-----------|-----------|--------|
| +7        | 9.5       |        |
| cb        | 9.3       |        |
| +13       | 8.9       |        |
| +14       | 10.2      |        |
| +16       | 10.1      |        |
| +17       | 8.9       |        |
| S         | 9.2       | 317.2  |
|           | 100' West |        |
| S         | 9.8       | 316.6  |
| +4        | 9.5       |        |
| +5        | 10.9      |        |
| +7        | 10.9      |        |
| +8        | 9.6       |        |
| cb        | 9.8       |        |
| 1/4       | 10.4      |        |
| +5        | 10.1      |        |
| on paving | 10.73     | 315.66 |
| 1/4       | 10.66     |        |
| Gutter    | 10.9      |        |
| N Top cb  | 10.19     | 316.20 |
|           | 116' W    |        |
| N Top cb  | 11.46     | 314.93 |
| Gutter    | 12.2      |        |
| 1/4       | 11.98     |        |
| on paving | 12.07     | 314.52 |
| +9        | 11.6      |        |



326.39

|             |      |       |        |
|-------------|------|-------|--------|
| 1/4         |      | 11.6  |        |
| cb          |      | 11.6  |        |
| +13         |      | 11.6  |        |
| +14         |      | 12.0  |        |
| +16         |      | 12.0  |        |
| +17         |      | 11.6  |        |
| S           |      | 11.9  | 315.0  |
| TP          | 0.15 | 11.76 | 314.63 |
|             |      | 125.5 |        |
| S           |      | 0.7   | 314.1  |
| +2          |      | 0.9   |        |
| +4          |      | 1.4   |        |
| +6          |      | 1.4   |        |
| +7          |      | 0.8   |        |
| cb          |      | 0.8   |        |
| 1/4         |      | 0.7   |        |
| £ on paving |      | 1.05  | 313.73 |
| 1/4         |      | 1.00  |        |
| Gutter      |      | 1.22  |        |
| Topch       |      | 0.50  | 314.28 |
|             |      | 1.40  |        |
| N. Topch    |      | 1.88  | 312.90 |
| Gutter      |      | 2.56  |        |
| 1/4         |      | 2.28  |        |
| £           |      | 2.35  | 312.43 |
| +6          |      | 1.7   |        |

314.78

46

|             |  |        |        |
|-------------|--|--------|--------|
| 1/4         |  | 2.3    |        |
| cb          |  | 2.01   |        |
| +14         |  | 2.3    |        |
| +16         |  | 3.2    |        |
| S           |  | 2.2    | 312.6  |
|             |  | 153' W |        |
| S           |  | 3.2    | 311.6  |
| +1          |  | 3.2    |        |
| +2          |  | 4.1    |        |
| +4          |  | 4.1    |        |
| +5          |  | 3.2    |        |
| +11         |  | 2.8    |        |
| +17         |  | 2.8    |        |
| cb          |  | 3.3    |        |
| +4          |  | 3.6    |        |
| +7          |  | 2.7    |        |
| 1/4         |  | 2.9    |        |
| +5          |  | 3.6    |        |
| £ on paving |  | 9.08   | 310.70 |
| 1/4         |  | 9.01   |        |
| Gutter      |  | 9.48   |        |
| N. Topch    |  | 3.69   | 311.09 |
|             |  | 161' W |        |
| N. Topch    |  | 4.88   | 309.90 |
| Gutter      |  | 5.65   |        |
| 1/4         |  | 5.22   |        |



314.78

\$ 5.22 309.56  
 +3 9.5  
 1/4 3.9  
 +5 3.5  
 cb 3.8  
 +14 9.2  
 +15 4.9  
 +18 4.9  
 S 3.9

310.9

180' W

S 7.1 307.7  
 +3 7.6  
 +5 6.1  
 cb 6.2  
 +7 6.2  
 1/4 6.9  
 +7 7.3

306.65

\$ on paving 8.13  
 1/4 8.15  
 cutter 8.50  
 N Top cb 7.74

307.04

200' W

10.90 303.88  
 cutter 11.55  
 1/4 11.14  
 \$ 11.09 303.69

314.78

47

14 10.6  
 cb 9.7  
 +3 9.0  
 +15 9.9  
 +16 10.8  
 +18 10.5  
 +19 9.7  
 S 9.8

305.0

212' W

S 11.8  
 T.P. 0.55 306.08 9.25  
 +1 2.8  
 +2 4.4  
 +5 4.6  
 +7 2.9  
 +16 2.3

303.0

305.53

cb 3.0  
 14 3.2  
 +8 3.7

303.08

\$ on paving 4.11  
 14 4.17  
 +7 4.28

301.97

cutter 4.64  
 Top cb 3.88  
 225' W

302.20

N Top cb 5.79

300.29



306.08

|        |       |        |
|--------|-------|--------|
| Gutter | 6.59  |        |
| +3     | 6.26  |        |
| 1/4    | 6.16  |        |
| ϕ      | 6.09  | 299.99 |
| +9     | 5.6   |        |
| 1/4    | 5.6   |        |
| CB     | 5.1   |        |
| +13    | 5.7   |        |
| +15    | 7.6   |        |
| +18    | 7.9   |        |
| +19    | 6.2   |        |
| S      | 6.4   | 299.7  |
| S+10   | 7.2   |        |
|        | 293'W |        |
| S-15   | 11.5  |        |
| S      | 10.2  | 295.3  |
| +3     | 9.8   |        |
| +4     | 12.0  |        |
| +8     | 12.8  |        |
| +9     | 9.9   |        |
| +13    | 7.2   |        |
| +15    | 6.9   |        |
| CB     | 8.1   |        |
| 1/4    | 2.3   |        |
| +8     | 2.2   |        |
| ϕ      | 8.65  | 298.43 |

306.08

48

|          |                               |        |
|----------|-------------------------------|--------|
| 1/4      | 8.75                          |        |
| +7       | 9.0                           |        |
| Gutter   | 9.25                          |        |
| N Top cb | 8.98                          | 297.60 |
|          | 258'W                         |        |
| N Top cb | 10.69                         | 295.44 |
| Gutter   | 11.91                         |        |
| +3       | 11.18                         |        |
| 1/4      | 10.91                         |        |
| ϕ        | 10.81                         | 295.27 |
| 1/4      | 10.0                          |        |
| CB       | 9.8                           |        |
| +3       | 9.9                           |        |
| +9       | 12.0                          |        |
| +13      | 15.2                          |        |
| +15      | 15.1                          |        |
| +17      | 13.9                          |        |
| S        | 14.6                          | 291.5  |
| S+15     | 16.0                          |        |
| T.P.     | 2.26                          | 295.77 |
|          | 12.57                         | 293.51 |
|          | 273' West E. Line of U. Pass. |        |
| S-15     | 9.0                           |        |
| S.       | 7.2                           | 288.6  |
| +3       | 6.9                           |        |
| +4       | 7.6                           |        |
| +8       | 7.8                           |        |



X  
295.77

49

|             |                          |      |        |
|-------------|--------------------------|------|--------|
| +11         |                          | 4.9  |        |
| cb          |                          | 3.3  |        |
| 14          |                          | 2.1  |        |
| ⊕           | on Ground                | 1.5  | 294.3  |
| ⊕           | " Paving                 | 2.86 | 292.91 |
| 14          |                          | 2.97 | 292.80 |
| Gutter      |                          | 3.37 | 292.40 |
| Top cb      |                          | 2.76 | 293.01 |
| Check on AM | section section of pipes | 2.80 | 292.97 |

Note: X sec called for Inter section. But the intersection has been X-sectioned recently judging from splinters.













64.66

|                      |       |       |
|----------------------|-------|-------|
| cb                   | 12.96 |       |
| W.L.                 | 13.18 | 51.48 |
| N gutter             |       |       |
| W.L.                 | 12.7  | 52.0  |
| cb                   | 12.9  |       |
| $\frac{1}{4}$        | 12.2  |       |
| $\frac{1}{2}$        | 12.1  | 54.6  |
| $\frac{3}{4}$        | 12.2  |       |
| cb                   | 12.5  |       |
| E.L.                 | 12.0  | 52.7  |
| N cb.                |       |       |
| E.L.                 | 10.8  | 53.9  |
| cb                   | 11.2  |       |
| gut                  | 12.5  |       |
| $\frac{1}{4}$        | 12.4  |       |
| $\frac{1}{2}$        | 12.0  | 52.7  |
| $\frac{3}{4}$        | 12.2  |       |
| gut                  | 12.9  |       |
| cb                   | 12.9  |       |
| W.L. Top of cutb     | 12.70 | 51.96 |
| 0+00=N.H. of Diamond |       |       |
| W.L.                 | 12.6  | 52.1  |
| cb - top curb        | 12.62 | 52.04 |
| gut                  | 12.4  |       |
| $\frac{1}{4}$        | 11.3  |       |
| $\frac{1}{2}$        | 10.9  | 53.8  |

64.66

52

|                                       |       |         |
|---------------------------------------|-------|---------|
| $\frac{3}{4}$                         | 11.1  |         |
| gut                                   | 11.6  |         |
| cb                                    | 10.6  |         |
| E.L.                                  | 10.1  | 54.6    |
| Top of wall 4' inst. 0+01             | 11.42 | 53.24 ✓ |
| 0+50                                  |       |         |
| E.L.                                  | 9.3   | 55.1    |
| cb                                    | 9.2   |         |
| gut                                   | 10.3  |         |
| $\frac{1}{4}$                         | 9.9   |         |
| $\frac{1}{2}$                         | 9.7   | 55.0    |
| $\frac{3}{4}$                         | 10.0  |         |
| gut                                   | 10.8  |         |
| cb                                    | 10.0  |         |
| W.L.                                  | 10.5  | 54.2    |
| 0+75 = Dirt Floor of Garage - 7' back |       |         |
| 10' Floor                             | 9.95  | 54.71 ✓ |
| 1+00                                  |       |         |
| W.L.                                  | 9.6   | 55.1    |
| cb                                    | 9.3   |         |
| gut                                   | 10.1  |         |
| $\frac{1}{4}$                         | 9.2   |         |
| $\frac{1}{2}$                         | 9.2   | 55.5    |
| $\frac{3}{4}$                         | 9.3   |         |
| gut                                   | 9.3   |         |
| cb                                    | 9.7   |         |



6466

|               |     |      |
|---------------|-----|------|
| E.L.          | 8.3 | 56.4 |
| 1750          |     |      |
| E.L.          | 7.5 | 57.2 |
| cb            | 7.4 |      |
| gut           | 8.6 |      |
| $\frac{1}{4}$ | 8.3 |      |
| $\frac{1}{2}$ | 8.4 | 56.9 |
| $\frac{3}{4}$ | 8.5 |      |
| gut           | 9.2 |      |
| cb            | 8.2 |      |
| w.L.          | 8.9 | 55.8 |
| 2700          |     |      |
| w.L.          | 7.4 | 57.3 |
| cb            | 7.1 |      |
| gut           | 7.8 |      |
| $\frac{1}{4}$ | 7.5 |      |
| $\frac{1}{2}$ | 7.1 | 57.6 |
| $\frac{3}{4}$ | 6.9 |      |
| gut           | 7.7 |      |
| cb            | 6.4 |      |
| E.L.          | 6.1 | 58.6 |
| 2750          |     |      |
| E.L.          | 5.0 | 59.7 |
| cb            | 5.0 |      |
| gut           | 6.3 |      |
| $\frac{1}{4}$ | 5.5 |      |

6466

53

|                         |                                     |      |
|-------------------------|-------------------------------------|------|
| $\frac{1}{2}$           | 5.4                                 | 59.3 |
| $\frac{3}{4}$           | 5.8                                 |      |
| gut                     | 6.2                                 |      |
| cb                      | 5.7                                 |      |
| w.L.                    | 6.2                                 | 58.5 |
| 2770 = S.L. Missouri st | = 80' st. 20' cbs 10' $\frac{1}{4}$ |      |
| w.L.                    | 5.8                                 | 58.9 |
| cb                      | 5.1                                 |      |
| gut                     | 5.8                                 |      |
| $\frac{1}{4}$           | 5.4                                 |      |
| $\frac{1}{2}$           | 5.0                                 | 59.7 |
| $\frac{3}{4}$           | 5.3                                 |      |
| gut                     | 5.6                                 |      |
| cb                      | 4.5                                 |      |
| E.L.                    | 4.5                                 | 60.2 |
| Subline Miss.           |                                     |      |
| E.L.                    | 4.0                                 | 60.7 |
| cb.                     | 4.8                                 |      |
| gut                     | 5.2                                 |      |
| $\frac{1}{4}$           | 4.9                                 |      |
| $\frac{1}{2}$           | 4.6                                 | 60.1 |
| $\frac{3}{4}$           | 4.9                                 |      |
| gut                     | 4.4                                 |      |
| cb                      | 4.7                                 |      |
| w.L.                    | 5.3                                 | 59.4 |



6466

|                              |     |      |
|------------------------------|-----|------|
| S $\frac{1}{4}$ Miss.        | 5.1 |      |
| w.L.                         | 5.1 | 59.6 |
| cb                           | 4.8 |      |
| gut                          | 5.0 |      |
| $\frac{1}{4}$                | 4.2 |      |
| e                            | 4.4 | 60.3 |
| <del>gut</del> $\frac{1}{4}$ | 4.7 |      |
| gut                          | 4.4 |      |
| cb                           | 4.4 |      |
| E.L.                         | 4.0 | 60.7 |
| E Miss.                      |     |      |
| E.L.                         | 3.9 | 60.8 |
| cb                           | 4.2 |      |
| gut                          | 4.6 |      |
| $\frac{1}{4}$                | 4.4 |      |
| e                            | 4.2 | 60.5 |
| $\frac{1}{4}$                | 4.6 |      |
| gut                          | 4.9 |      |
| cb                           | 4.2 |      |
| w.L.                         | 4.9 | 59.8 |
| N. $\frac{1}{4}$ Miss.       |     |      |
| w.L.                         | 4.6 | 60.1 |
| cb                           | 4.0 |      |
| gut                          | 4.6 |      |
| $\frac{1}{4}$                | 4.3 |      |
| e                            | 4.0 | 60.7 |

6466

54

|                          |     |      |
|--------------------------|-----|------|
| $\frac{1}{4}$            | 4.2 |      |
| gut                      | 4.4 |      |
| cb                       | 3.9 |      |
| E.L.                     | 3.5 | 61.2 |
| Ncb Miss                 |     |      |
| E.L.                     | 3.7 | 61.0 |
| cb                       | 3.8 |      |
| gut                      | 3.8 |      |
| $\frac{1}{4}$            | 3.9 |      |
| e                        | 3.2 | 60.9 |
| $\frac{1}{4}$            | 4.1 |      |
| gut                      | 4.4 |      |
| cb                       | 3.9 |      |
| w.L.                     | 4.4 | 60.3 |
| 0+00 = N.L. Missouri st. |     |      |
| w.L.                     | 4.0 | 60.7 |
| cb                       | 3.6 |      |
| gut                      | 4.0 |      |
| $\frac{1}{4}$            | 3.6 |      |
| e                        | 3.4 | 61.3 |
| $\frac{1}{4}$            | 3.6 |      |
| gut                      | 4.0 |      |
| cb                       | 3.4 |      |
| E.L.                     | 2.9 | 61.8 |
| 0+50                     |     |      |
| E.L.                     | 2.3 | 62.4 |



64.66

|               |       |       |      |       |
|---------------|-------|-------|------|-------|
| cb            |       |       | 2.3  |       |
| +4            |       |       | 3.4  |       |
| $\frac{1}{4}$ |       |       | 2.7  |       |
| ♀             |       |       | 2.6  | 62.1  |
| ♂             |       |       | 2.5  |       |
| gut           |       |       | 3.0  |       |
| cb            |       |       | 2.4  |       |
| w.l.          |       |       | 2.8  | 61.9  |
| 1+00          |       |       |      |       |
| w.l.          |       |       | 1.4  | 63.3  |
| cb            |       |       | 0.9  |       |
| gut           |       |       | 1.8  |       |
| $\frac{1}{4}$ |       |       | 1.3  |       |
| ♀             |       |       | 1.0  | 63.7  |
| $\frac{1}{4}$ |       |       | 1.0  |       |
| +6            |       |       | 1.9  |       |
| cb            |       |       | 0.8  |       |
| E.L.          |       |       | 0.1  | 64.6  |
| T.P.          | 10.87 | 75.53 | 0.00 | 64.66 |
| 1+50          |       |       |      |       |
| E.L.          |       |       | 9.6  | 65.9  |
| cb            |       |       | 10.1 |       |
| +4            |       |       | 10.9 |       |
| $\frac{1}{4}$ |       |       | 10.2 |       |
| ♀             |       |       | 10.1 | 65.4  |
| $\frac{1}{4}$ |       |       | 10.5 |       |

75.53

55

|   |  |  |      |      |
|---|--|--|------|------|
| gut   |  |  | 11.1 |      |
| cb  |  |  | 10.3 |      |
| w.l.  |  |  | 10.2 | 64.7 |
| 2+00  |  |  |      |      |
| w.l.  |  |  | 9.2  | 66.3 |
| cb+18   |  |  | 8.8  |      |
| cb  |  |  | 9.8  |      |
| $\frac{1}{4}$   |  |  | 8.9  |      |
| ♀   |  |  | 8.6  | 66.9 |
| $\frac{1}{4}$   |  |  | 8.7  |      |
| +7  |  |  | 9.3  |      |
| cb  |  |  | 8.4  |      |
| E.L.  |  |  | 8.0  | 67.5 |
| 2+50  |  |  |      |      |
| E.L.  |  |  | 6.6  | 68.9 |
| cb  |  |  | 7.0  |      |
| +2  |  |  | 8.1  |      |
| $\frac{1}{4}$   |  |  | 7.5  |      |
| ♀   |  |  | 7.2  | 68.3 |
| $\frac{1}{4}$   |  |  | 7.7  |      |
| cb  |  |  | 8.3  |      |
| +1  |  |  | 7.6  |      |
| w.l.  |  |  | 4.0  | 67.5 |
| 2+70 = S.L. Chalcidomy = 80' st. 20' cb 10' $\frac{1}{4}$ |  |  |      |      |
| w.l.  |  |  | 7.6  | 67.9 |
| +18   |  |  | 7.1  |      |



|               |     |      |
|---------------|-----|------|
| cb            | 8.0 |      |
| $\frac{1}{4}$ | 7.2 |      |
| E             | 6.8 | 68.7 |
| $\frac{1}{4}$ | 7.0 |      |
| +8            | 7.5 |      |
| cb            | 6.4 |      |
| E.L.          | 6.0 | 69.5 |

s cb line at chal.

|               |     |      |
|---------------|-----|------|
| E.L.          | 5.5 | 70.0 |
| cb            | 5.9 |      |
| gut           | 6.7 |      |
| $\frac{1}{4}$ | 6.5 |      |
| E             | 6.4 | 69.1 |
| $\frac{1}{4}$ | 6.7 |      |
| gut           | 7.7 |      |
| cb            | 6.5 |      |
| W.L.          | 6.7 | 68.8 |

s  $\frac{1}{4}$  chal.

|               |     |      |
|---------------|-----|------|
| W.L.          | 6.3 | 69.2 |
| cb            | 6.3 |      |
| gut           | 6.8 |      |
| $\frac{1}{4}$ | 6.4 |      |
| E             | 6.0 | 69.5 |
| $\frac{1}{4}$ | 6.1 |      |
| +8            | 6.2 |      |
| cb            | 6.0 |      |

|      |     |      |
|------|-----|------|
| E.L. | 5.3 | 70.2 |
|------|-----|------|

E Chal

|               |     |      |
|---------------|-----|------|
| E.L.          | 5.1 | 70.4 |
| cb            | 5.5 |      |
| +3            | 5.8 |      |
| $\frac{1}{4}$ | 5.9 |      |
| E             | 5.8 | 69.7 |
| $\frac{1}{4}$ | 6.1 |      |

|        |     |      |
|--------|-----|------|
| cb gut | 7.0 |      |
| cb     | 6.2 |      |
| W.L.   | 6.2 | 69.3 |

N.  $\frac{1}{4}$  chal.

|               |     |      |
|---------------|-----|------|
| W.L.          | 6.2 | 69.3 |
| cb            | 6.1 |      |
| gut           | 6.5 |      |
| $\frac{1}{4}$ | 5.9 |      |
| E             | 5.6 | 69.9 |
| $\frac{1}{4}$ | 5.7 |      |
| +7            | 5.7 |      |
| cb            | 5.3 |      |

|      |     |      |
|------|-----|------|
| E.L. | 4.9 | 70.6 |
|------|-----|------|

N cb Chal.

|               |     |      |
|---------------|-----|------|
| E.L.          | 4.6 | 70.9 |
| cb            | 4.8 |      |
| +2            | 5.8 |      |
| $\frac{1}{4}$ | 5.4 |      |



75.53

|                            |     |      |
|----------------------------|-----|------|
| e                          | 5.3 | 70.2 |
| 1/4                        | 5.6 |      |
| gut                        | 6.0 |      |
| cb                         | 5.6 |      |
| W.L.                       | 6.0 | 69.5 |
| 0+00 = N.L. chalcydomy st. |     |      |
| W.L.                       | 5.5 | 70.0 |
| cb                         | 5.1 |      |
| gut                        | 5.7 |      |
| 1/4                        | 5.3 |      |
| e                          | 4.9 | 70.6 |
| 1/4                        | 4.9 |      |
| +7                         | 5.4 |      |
| cb.                        | 4.2 |      |
| E.L.                       | 4.1 | 71.4 |
| 0+50                       |     |      |
| E.L.                       | 2.9 | 72.6 |
| cb                         | 3.0 |      |
| +5                         | 3.9 |      |
| 1/4                        | 3.7 |      |
| e                          | 3.7 | 71.8 |
| 1/4                        | 4.1 |      |
| +3                         | 4.5 |      |
| +6                         | 3.1 |      |
| cb                         | 4.0 |      |
| W.L.                       | 4.1 | 71.4 |

75.53

57

|             |       |       |
|-------------|-------|-------|
| 1+00        |       |       |
| W.L.        | 3.9   | 71.6  |
| cb          | 3.2   |       |
| +3          | 3.0   |       |
| +6          | 3.0   |       |
| 1/4         | 3.2   |       |
| e           | 2.9   | 72.6  |
| 1/4         | 2.9   |       |
| +6          | 3.3   |       |
| cb          | 2.6   |       |
| E.L.        | 2.0   | 73.5  |
| -1+50       |       |       |
| E.L.        | 1.3   | 74.2  |
| cb          | 1.5   |       |
| +3          | 2.3   |       |
| 1/4         | 2.2   |       |
| e           | 2.3   | 73.2  |
| 1/4         | 2.7   |       |
| +2          | 2.7   |       |
| +3          | 2.2   |       |
| cb          | 2.1   |       |
| W.L.        | 2.8   | 72.7  |
| 1+70        |       |       |
| T.P. impola | 9.84  | 84.87 |
| 0.00        | 75.53 |       |
| 2+00        |       |       |
| W.L.        | 11.4  | 73.5  |
| cb          | 11.3  |       |



84.87

|      |      |      |
|------|------|------|
| 1/4  | 11.1 |      |
| E    | 10.8 | 73.1 |
| 1/4  | 11.0 |      |
| +7   | 11.2 |      |
| cb   | 11.4 |      |
| E.L. | 11.3 | 73.6 |

1+50

|      |      |      |
|------|------|------|
| E.L. | 9.8  | 75.1 |
| cb   | 9.7  |      |
| +2   | 10.6 |      |
| 1/4  | 10.3 |      |
| E    | 10.1 | 74.8 |
| 1/4  | 10.4 |      |
| cb   | 10.4 |      |
| W.L. | 10.4 | 74.5 |

2 +70 = S.L. LAW. - 80' st 20' cbs 10' 1/4

|      |      |      |
|------|------|------|
| W.L. | 10.2 | 74.7 |
| cb   | 10.0 |      |
| 1/4  | 10.0 |      |
| E    | 9.7  | 75.2 |
| 1/4  | 10.0 |      |
| +7   | 10.1 |      |
| cb   | 9.5  |      |
| E.L. | 9.1  | 75.8 |

5 cb Line of LAW. = 20' N.

|      |     |      |
|------|-----|------|
| E.L. | 8.8 | 76.1 |
|------|-----|------|

84.87

58

|      |     |      |
|------|-----|------|
| cb   | 9.0 |      |
| +4   | 9.9 |      |
| 1/4  | 9.7 |      |
| E    | 9.4 | 75.5 |
| 1/4  | 9.5 |      |
| cb   | 9.7 |      |
| W.L. | 9.8 | 75.1 |

S 1/4 LAW. = 30' N.

|      |     |      |
|------|-----|------|
| W.L. | 9.7 | 75.2 |
| cb   | 9.3 |      |
| 1/4  | 9.4 |      |
| E    | 9.2 | 75.7 |
| 1/4  | 9.4 |      |
| +7   | 9.7 |      |
| cb   | 9.8 |      |
| E.L. | 8.6 | 76.3 |

E LAW.

|      |     |      |
|------|-----|------|
| E.L. | 8.3 | 76.6 |
| cb   | 8.7 |      |
| +3   | 9.4 |      |
| 1/4  | 9.2 |      |
| E    | 9.1 | 75.8 |
| 1/4  | 9.0 |      |
| cb   | 9.1 |      |
| W.L. | 9.4 | 75.5 |

N. 1/4 LAW



84.87

|               |     |      |
|---------------|-----|------|
| W.L.          | 9.2 | 75.7 |
| cb            | 9.0 |      |
| $\frac{1}{2}$ | 9.0 |      |
| e             | 8.8 | 76.1 |
| $\frac{1}{4}$ | 8.0 |      |
| +7            | 9.1 |      |
| cb            | 8.1 |      |
| E.L.          | 7.9 | 77.0 |

N. cb Line LAW

|               |     |      |
|---------------|-----|------|
| E.L.          | 7.6 | 77.3 |
| cb            | 8.0 |      |
| +3            | 8.7 |      |
| $\frac{1}{4}$ | 8.3 |      |
| e             | 8.5 | 76.4 |
| $\frac{1}{2}$ | 8.8 |      |
| cb            | 8.6 |      |
| W.L.          | 8.9 | 76.0 |

0+00 = N.L. LAW st.

|               |     |      |
|---------------|-----|------|
| W.L.          | 8.3 | 76.6 |
| cb            | 8.0 |      |
| $\frac{1}{2}$ | 8.4 |      |
| e             | 8.1 | 76.8 |
| $\frac{1}{4}$ | 7.9 |      |
| +7            | 7.9 |      |
| cb            | 7.4 |      |
| E.L.          | 7.3 | 77.6 |

84.87

59

|               |     |      |
|---------------|-----|------|
| 0+50          |     |      |
| E.L.          | 5.8 | 79.1 |
| cb            | 5.1 |      |
| +3            | 6.5 |      |
| $\frac{1}{4}$ | 6.5 |      |
| e             | 6.3 | 78.6 |
| $\frac{1}{2}$ | 6.4 |      |
| cb            | 6.9 |      |
| W.L.          | 7.1 | 72.8 |

1+00

|               |     |      |
|---------------|-----|------|
| W.L.          | 5.9 | 79.0 |
| cb            | 5.6 |      |
| $\frac{1}{4}$ | 5.4 |      |
| e             | 5.3 | 79.6 |
| $\frac{1}{2}$ | 5.4 |      |
| +7            | 5.5 |      |
| cb            | 4.9 |      |
| E.L.          | 4.7 | 80.2 |

1+50

|               |     |      |
|---------------|-----|------|
| E.L.          | 4.0 | 80.9 |
| cb            | 4.1 |      |
| got           | 5.0 |      |
| $\frac{1}{2}$ | 4.7 |      |
| e             | 4.6 | 80.3 |
| $\frac{1}{4}$ | 4.6 |      |
| cb            | 4.5 |      |



84.87

|  |     |      |
|--|-----|------|
| W.L.   | 4.9 | 800  |
| 2+00   |     |      |
| W.L.   | 3.9 | 810  |
| cb   | 3.4 |      |
| $\frac{1}{4}$  | 3.5 |      |
| $\frac{1}{2}$  | 3.4 | 81.5 |
| $\frac{3}{4}$  | 3.6 |      |
| got  | 4.0 |      |
| cb   | 3.2 |      |
| E.L.   | 2.8 | 821  |
| 2+50   |     |      |
| E.L.   | 2.1 | 828  |
| cb   | 2.1 |      |
| +3   | 3.1 |      |
| $\frac{1}{4}$  | 2.7 |      |
| $\frac{1}{2}$  | 2.6 | 823  |
| $\frac{3}{4}$  | 2.8 |      |
| cb   | 2.7 |      |
| W.L.   | 3.0 | 819  |
| 2+70 = S.L. Beryl = 80' st 20' cbs 10' $\frac{1}{4}$ |     |      |
| W.L.   | 2.7 | 822  |
| cb   | 2.7 |      |
| $\frac{1}{4}$  | 2.3 |      |
| $\frac{1}{2}$  | 2.2 | 827  |
| $\frac{3}{4}$  | 2.3 |      |
| +2   | 2.7 |      |

84.87

|                       |       |            |
|-----------------------|-------|------------|
| cb                    | 1.7   |            |
| E.L.                  | 1.6   | 833        |
| T.P. 1261             | 97.36 | 0.12 84.75 |
| B.M. spike mark SE    | 12.19 | 85.17      |
| S cb Line Beryl       |       |            |
| E.L.                  | 13.6  | 838        |
| cb.                   | 13.7  |            |
| +3                    | 14.7  |            |
| $\frac{1}{4}$         | 14.3  |            |
| $\frac{1}{2}$         | 14.1  | 833        |
| $\frac{3}{4}$         | 14.2  |            |
| cb                    | 14.2  |            |
| W.L.                  | 14.2  | 832        |
| S $\frac{1}{4}$ Beryl |       |            |
| W.L.                  | 14.2  | 832        |
| cb                    | 14.4  |            |
| $\frac{1}{4}$         | 14.1  |            |
| $\frac{1}{2}$         | 13.8  | 836        |
| $\frac{3}{4}$         | 13.9  |            |
| cb                    | 13.8  |            |
| E.L.                  | 13.4  | 840        |
| $\frac{1}{2}$ Berl    |       |            |
| E.L.                  | 12.8  | 846        |
| cb                    | 13.0  |            |
| $\frac{1}{4}$         | 13.1  |            |
| $\frac{1}{2}$         | 13.0  | 844        |



97.36

|           |      |      |
|-----------|------|------|
| 7         | 13.4 |      |
| cb        | 13.5 |      |
| W.L.      | 12.6 | 83.8 |
| N 7 Beryl |      |      |
| W.L.      | 13.2 | 84.1 |
| cb        | 13.3 |      |
| 7         | 13.0 |      |
| z         | 12.7 | 84.7 |
| 7         | 12.6 |      |
| cb        | 12.5 |      |
| E.L.      | 12.3 | 85.1 |

N cb line Beryl

|      |      |      |
|------|------|------|
| E.L. | 11.4 | 86.0 |
| cb   | 11.2 |      |
| +3   | 12.5 |      |
| 7    | 12.1 |      |
| z    | 12.1 | 85.3 |
| 7    | 12.6 |      |
| cb   | 12.6 |      |
| W.L. | 12.5 | 84.9 |

0+00 = N.L. Beryl

|      |      |      |
|------|------|------|
| W.L. | 11.7 | 85.7 |
| cb   | 11.6 |      |
| 7    | 11.5 |      |
| z    | 11.2 | 86.2 |
| 7    | 11.1 |      |

97.36

62

|      |      |      |
|------|------|------|
| +7   | 11.7 |      |
| cb   | 16.5 |      |
| E.L. | 10.3 | 87.1 |
| 0+50 |      |      |
| E.L. | 8.5  | 88.9 |
| cb   | 8.6  |      |
| +3   | 9.6  |      |
| 7    | 9.0  |      |
| z    | 9.3  | 88.1 |
| 7    | 9.6  |      |
| cb   | 9.9  |      |
| W.L. | 10.3 | 87.1 |

1+00

|      |     |      |
|------|-----|------|
| W.L. | 8.8 | 88.6 |
| cb   | 8.6 |      |
| 7    | 8.4 |      |
| z    | 8.2 | 89.2 |
| 7    | 8.1 |      |
| +6   | 8.3 |      |
| cb   | 7.1 |      |
| E.L. | 7.1 | 90.3 |

1+50

|      |     |      |
|------|-----|------|
| E.L. | 5.9 | 91.5 |
| cb   | 6.1 |      |
| +5   | 6.9 |      |
| 7    | 6.8 |      |



97.36

|               |     |      |
|---------------|-----|------|
| E             | 7.0 | 90.4 |
| $\frac{1}{4}$ | 7.1 |      |
| cb            | 7.2 |      |
| W.L.          | 7.8 | 89.6 |

2+00

|               |     |      |
|---------------|-----|------|
| W.L.          | 6.7 | 90.7 |
| cb            | 6.0 |      |
| $\frac{1}{4}$ | 5.3 |      |
| E             | 5.0 | 92.4 |
| $\frac{1}{4}$ | 5.0 |      |
| +5            | 5.8 |      |
| cb            | 4.5 |      |
| E.L.          | 4.6 | 92.8 |

2+50

|               |     |      |
|---------------|-----|------|
| E.L.          | 3.3 | 94.1 |
| cb            | 3.7 |      |
| +3            | 5.0 |      |
| $\frac{1}{4}$ | 4.3 |      |
| E             | 4.4 | 93.0 |
| $\frac{1}{4}$ | 4.6 |      |
| cb            | 4.9 |      |
| W.L.          | 5.8 | 91.6 |

2+70 = S.L. Wilbur = 90' at 20' cb. 10'  $\frac{1}{4}$ 

|               |     |      |
|---------------|-----|------|
| W.L.          | 5.7 | 91.7 |
| cb            | 4.7 |      |
| $\frac{1}{4}$ | 4.5 |      |

97.36

63

|               |     |      |
|---------------|-----|------|
| E             | 4.1 | 93.3 |
| $\frac{1}{4}$ | 4.0 |      |
| +6            | 4.7 |      |
| cb            | 3.1 |      |
| E.L.          | 3.0 | 94.4 |

s cb line Wilbur

|               |     |      |
|---------------|-----|------|
| E.L.          | 2.8 | 94.6 |
| cb            | 3.0 |      |
| +4            | 4.2 |      |
| $\frac{1}{4}$ | 3.8 |      |
| E             | 3.7 | 93.7 |
| $\frac{1}{4}$ | 4.2 |      |
| cb            | 4.5 |      |
| W.L.          | 6.2 | 91.2 |

s  $\frac{1}{4}$  Wilbur

|               |     |      |
|---------------|-----|------|
| W.L.          | 5.9 | 91.5 |
| cb            | 4.5 |      |
| $\frac{1}{4}$ | 4.0 |      |
| E             | 2.6 | 93.8 |
| $\frac{1}{4}$ | 3.5 |      |
| +7            | 4.0 |      |
| cb            | 2.8 |      |
| E.L.          | 1.9 | 95.5 |

E Wilbur

|      |     |      |
|------|-----|------|
| E.L. | 1.1 | 96.3 |
| cb   | 2.3 |      |



|                        |     |      |
|------------------------|-----|------|
| +4                     | 3.9 |      |
| $\frac{1}{4}$          | 3.3 |      |
| E                      | 3.4 | 94.0 |
| $\frac{1}{4}$          | 3.8 |      |
| cb                     | 4.3 |      |
| W.L.                   | 5.4 | 92.0 |
| N $\frac{1}{4}$ Wilbur |     |      |
| W.L.                   | 5.5 | 91.9 |
| cb                     | 4.2 |      |
| $\frac{1}{4}$          | 3.7 |      |
| E                      | 3.2 | 94.2 |
| $\frac{1}{4}$          | 3.0 |      |
| +5                     | 3.7 |      |
| cb                     | 2.0 |      |
| E.L.                   | 1.7 | 95.7 |
| N cb line Wilbur       |     |      |
| E.L.                   | 1.9 | 95.5 |
| cb                     | 2.3 |      |
| +4                     | 3.3 |      |
| $\frac{1}{4}$          | 2.9 |      |
| E                      | 3.2 | 94.2 |
| $\frac{1}{4}$          | 3.1 |      |
| cb                     | 4.3 |      |
| W.L.                   | 5.9 | 91.5 |
| a+00 = N.L. Wilbur     |     |      |
| W.L.                   | 5.1 | 92.3 |

|               |       |        |       |                  |
|---------------|-------|--------|-------|------------------|
| cb            |       |        | 4.2   |                  |
| $\frac{1}{4}$ |       |        | 2.4   |                  |
| E             |       |        | 2.8   | 94.6             |
| $\frac{1}{4}$ |       |        | 2.7   |                  |
| +6            |       |        | 2.9   |                  |
| cb            |       |        | 1.8   |                  |
| E.L.          |       |        | 1.2   | 96.2             |
| 0+50          |       |        |       |                  |
| E.L.          |       |        | 0.6   | 97.4             |
| cb            |       |        | 0.9   |                  |
| +3            |       |        | 2.3   |                  |
| $\frac{1}{4}$ |       |        | 1.8   |                  |
| E             |       |        | 1.8   | 95.6             |
| $\frac{1}{4}$ |       |        | 1.6   |                  |
| cb            |       |        | 2.0   |                  |
| W.L.          |       |        | 3.1   | 94.3             |
| B.M. on Hub   |       |        |       |                  |
| T.P.          | 4.89  | 102.13 | 0.12  | 97.24            |
|               | 61.6  | 89.72  | 12.57 | 89.56            |
|               | 0.22  | 7704   | 12.90 | 76.82            |
|               |       |        | 10.06 | 66.92 - 67.03    |
|               |       |        |       | 97.24 = T.P.     |
|               |       |        |       | NE cor<br>return |
|               | 11.71 | 108.95 | 1.80  | 107.15 = T.P.    |
|               | 1.86  | 109.01 |       |                  |
| +100          |       |        |       |                  |
| W.L.          |       |        | 11.7  | 97.3             |



109.01

|               |      |      |
|---------------|------|------|
| cb            | 11.6 |      |
| $\frac{1}{4}$ | 11.4 |      |
| d             | 11.3 | 97.7 |
| $\frac{1}{4}$ | 11.2 |      |
| + 5           | 11.2 |      |
| cb            | 10.2 |      |
| E.L.          | 9.5  | 99.5 |

1+50

|               |     |       |
|---------------|-----|-------|
| E.L.          | 7.1 | 101.9 |
| cb            | 7.5 |       |
| +4            | 8.7 |       |
| $\frac{1}{4}$ | 8.6 |       |
| e             | 8.6 | 100.4 |
| $\frac{1}{4}$ | 8.9 |       |
| cb            | 8.8 |       |
| W.L.          | 9.6 | 99.4  |

2+00

|               |     |       |
|---------------|-----|-------|
| W.L.          | 7.6 | 101.4 |
| cb            | 7.3 |       |
| $\frac{1}{4}$ | 7.2 |       |
| e             | 6.7 | 102.3 |
| $\frac{1}{4}$ | 6.7 |       |
| + 2           | 7.1 |       |
| cb            | 6.3 |       |
| E.L.          | 4.5 | 104.5 |

2+30

109.01

65

|               |     |       |
|---------------|-----|-------|
| E.L.          | 4.1 | 104.9 |
| cb            | 5.5 |       |
| +3            | 6.2 |       |
| $\frac{1}{4}$ | 5.7 |       |
| e             | 5.4 | 103.6 |
| $\frac{1}{4}$ | 5.9 |       |
| cb            | 6.3 |       |
| W.L.          | 6.5 | 102.5 |

2+70 = S.L. of Loring st. - Paved

|                         |      |        |
|-------------------------|------|--------|
| W.L.                    | 5.6  | 103.5  |
| cb - top cement         | 5.43 | 103.58 |
| gut                     | 5.99 | 103.02 |
| $\frac{1}{4}$ on paving | 5.38 |        |
| e                       | 4.97 | 104.04 |
| $\frac{1}{4}$           | 4.89 |        |
| gut                     | 5.01 | 104.00 |
| Top Carb                | 4.38 | 104.63 |
| E.L.                    | 3.1  | 105.9  |

N.L. of paving 100' wide

|               |      |        |
|---------------|------|--------|
| E.L.          | 1.3  | 107.7  |
| Top Cb        | 1.86 | 107.15 |
| gut           | 2.53 | 106.48 |
| $\frac{1}{4}$ | 2.55 |        |
| e             | 2.73 | 106.28 |
| $\frac{1}{4}$ | 3.23 |        |
| gut           | 3.92 | 105.09 |



109.01

|                                    |        |               |
|------------------------------------|--------|---------------|
| Top cb                             | 3.33   | 105.68        |
| W.L.                               | 3.7    | 105.3         |
| 0+00 = N.L. of Loring - see sketch |        |               |
| W.L.                               | 2.8    | 106.2         |
| cb                                 | 2.5    |               |
| $\frac{1}{4}$                      | 1.9    |               |
| e                                  | 1.3    | 107.7         |
| $\frac{1}{4}$                      | 1.5    |               |
| cb                                 | 2.9    |               |
| E.L.                               | 0.2    | 108.8         |
| 11.15                              | 118.30 | 107.15 = 317. |
| 0+50                               |        |               |
| E.L.                               | 8.4    | 109.9         |
| cb                                 | 9.2    |               |
| $\frac{1}{4}$                      | 9.5    |               |
| e                                  | 9.6    | 108.7         |
| $\frac{1}{4}$                      | 9.9    |               |
| cb                                 | 10.6   |               |
| W.L.                               | 11.1   | 107.2         |
| 1+00                               |        |               |
| W.L.                               | 9.8    | 108.5         |
| cb                                 | 9.4    |               |
| $\frac{1}{4}$                      | 8.8    |               |
| e                                  | 8.4    | 109.9         |
| $\frac{1}{4}$                      | 8.4    |               |
| cb                                 | 8.1    |               |

118.30

66

|  |     |       |
|--|-----|-------|
| E.L.   | 7.5 | 110.8 |
| 1+50   |     |       |
| E.L.   | 6.2 | 112.1 |
| cb   | 6.8 |       |
| $\frac{1}{4}$  | 7.2 |       |
| e  | 7.2 | 111.1 |
| $\frac{1}{4}$  | 7.6 |       |
| cb   | 8.7 |       |
| W.L.   | 8.3 | 110.0 |
| 2+00   |     |       |
| W.L.   | 6.9 | 111.4 |
| cb   | 7.3 |       |
| $\frac{1}{4}$  | 6.0 |       |
| e  | 5.9 | 112.4 |
| $\frac{1}{4}$  | 5.8 |       |
| cb   | 5.3 |       |
| E.L.   | 4.7 | 113.6 |
| 2+65 = S.L. of hyacinth = 70' st 15' cbs 10' $\frac{1}{4}$ |     |       |
| E.L.   | 3.0 | 115.3 |
| cb   | 3.6 |       |
| $\frac{1}{4}$  | 4.2 |       |
| e  | 4.1 | 114.2 |
| $\frac{1}{4}$  | 4.3 |       |
| cb   | 5.5 |       |
| W.L.   | 5.4 | 112.9 |
| S cb Line hyacinth   |     |       |



118.30

|                           |     |       |
|---------------------------|-----|-------|
| W.L.                      | 5.1 | 113.2 |
| cb                        | 5.0 |       |
| $\frac{1}{4}$             | 3.8 |       |
| E                         | 3.8 | 114.5 |
| $\frac{1}{4}$             | 4.0 |       |
| cb                        | 3.4 |       |
| E.L.                      | 2.6 | 115.7 |
| S $\frac{1}{4}$ hyacinth. |     |       |
| E.L.                      | 2.6 | 115.7 |
| cb                        | 3.2 |       |
| $\frac{1}{4}$             | 3.7 |       |
| E                         | 3.7 | 114.6 |
| $\frac{1}{4}$             | 3.7 |       |
| cb                        | 4.7 |       |
| W.L.                      | 5.0 | 113.3 |
| E hyacinth                |     |       |
| W.L.                      | 4.2 | 114.1 |
| cb                        | 4.7 |       |
| $\frac{1}{4}$             | 3.6 |       |
| E                         | 3.5 | 114.8 |
| $\frac{1}{4}$             | 3.4 |       |
| cb                        | 5.8 |       |
| E.L.                      | 2.0 | 116.3 |
| N. $\frac{1}{4}$ hyacinth |     |       |
| E.L.                      | 1.7 | 116.6 |
| cb                        | 2.9 |       |

118.30

67

|                    |     |       |
|--------------------|-----|-------|
| $\frac{1}{4}$      | 3.5 |       |
| E                  | 3.5 | 114.8 |
| $\frac{1}{4}$      | 4.3 |       |
| cb                 | 4.3 |       |
| W.L.               | 5.2 | 113.1 |
| N cb live hyacinth |     |       |
| W.L.               | 5.1 | 113.2 |
| + 80               | 3.8 |       |
| cb                 | 4.5 |       |
| $\frac{1}{4}$      | 3.4 |       |
| E                  | 3.5 | 114.8 |
| $\frac{1}{4}$      | 3.2 |       |
| cb                 | 2.2 |       |
| E.L.               | 1.7 | 116.6 |
| N.L. hyacinth      |     |       |
| E.L.               | 1.6 | 116.7 |
| cb                 | 2.3 |       |
| $\frac{1}{4}$      | 3.0 |       |
| E                  | 3.2 | 115.1 |
| $\frac{1}{4}$      | 3.3 |       |
| cb                 | 4.4 |       |
| + 10               | 4.0 |       |
| W.L.               | 4.4 | 113.9 |



X section of Wilbur st. from Cass to W.L.N. shore Highway  
 80' st 20' cbs 10' 4'

92.96

68

91.64 = BM. NW. Cor. Wilbur Dr.

1.32 92.96

0+00 = W.E.L. Cass

|      |      |      |
|------|------|------|
| s.l. | 11.4 | 81.5 |
| cb   | 11.2 | "    |
| 1/4  | 10.9 |      |
| ±    | 10.4 | 82.5 |
| 1/4  | 10.3 |      |
| cb   | 10.1 |      |
| N.L. | 9.9  | 83.0 |
| 0+50 |      |      |
| N.L. | 10.0 | 82.9 |
| cb   | 9.5  |      |
| 1/4  | 9.5  |      |
| ±    | 9.5  | 83.4 |
| 1/4  | 10.1 |      |
| cb   | 10.4 |      |
| s.l. | 10.9 | 82.0 |
| 1+00 |      |      |
| s.l. | 9.7  | 83.2 |
| cb   | 9.4  |      |
| 1/4  | 9.0  |      |
| ±    | 8.5  | 84.4 |
| 1/4  | 8.7  |      |
| cb   | 8.9  |      |
| N.L. | 7.8  | 85.1 |

Plotted 10-6-1928 C.B.H.

|                               |      |         |
|-------------------------------|------|---------|
| 1+50                          |      |         |
| N.L.                          | 7.0  | 85.9    |
| +17                           | 7.6  |         |
| cb                            | 8.1  |         |
| 1/4                           | 7.7  |         |
| ±                             | 7.6  | 85.3    |
| 1/4                           | 8.1  |         |
| gut                           | 8.8  |         |
| cb                            | 8.5  |         |
| s.l.                          | 8.9  | 84.0    |
| ON South 4' IN ST.            |      |         |
| 1+77 = 2' cement Walk on cem. | 8.23 | 84.73 ✓ |
| 2+00                          |      |         |
| s.l.                          | 8.0  | 84.9    |
| cb                            | 7.4  |         |
| gut                           | 7.7  |         |
| 1/4                           | 7.1  |         |
| ±                             | 6.5  | 86.4    |
| 1/4                           | 6.7  |         |
| cb                            | 7.2  |         |
| +4                            | 6.4  |         |
| N.L.                          | 5.8  | 87.1    |
| 2+50                          |      |         |
| N.L.                          | 5.0  | 87.9    |
| +15                           | 3.6  |         |
| cb                            | 6.4  |         |
| 1/4                           | 5.9  |         |



92.96

E 5.0 87.1

E 6.4

cb 7.0

s.L. 7.5 85.4

3+00

s.L. 6.0 86.1

cb 5.9

gut 6.5

E 5.7

E 5.0 87.9

E 5.1

cb 5.3

+4 4.3

N.L. 4.0 88.9

3+50

N.L. 3.2 89.7

cb 4.3

gut 4.9

E 4.6

E 4.6 88.3

E 5.5

gut 6.2

cb 5.9

s.L. 6.2 86.7

8+51 = 2' com. walk 4' out on South

end of walk 6.21 ✓ 86.75

92.96

69

4+00

s.L. 3.6 87.3

cb 5.2

gut 5.6

E 4.9

E 4.1 88.8

E 4.0

gut 4.1

cb 3.5

N.L. 3.0 89.9

4+50

N.L. 2.2 90.7

cb 2.7

gut 3.5

E 3.2

E 3.0 89.9

E 3.7

gut 4.3

cb 3.9

s.L. 4.0 88.9

4+98 = W.L. Dawes see Dawes x sec. for intersection

s.L. 1.4 91.5

cb 1.4

gut 2.0

E 1.5

E 1.0 91.9



92.96

|                   |        |              |
|-------------------|--------|--------------|
| 1/4               | 1.1    |              |
| gut               | 1.5    |              |
| cb                | 0.8    |              |
| N.L.              | 2.7    | 92.2         |
| E.L. Dawes        |        |              |
| 12.22             | 103.92 | 91.64 = B.M. |
| 2+00 = E.L. Dawes |        |              |
| N.L.              | 2.8    | 96.1         |
| cb                | 2.0    |              |
| +1                | 8.5    |              |
| 1/4               | 9.3    |              |
| 2                 | 7.5    | 96.4         |
| 1/4               | 8.5    |              |
| cb                | 9.4    |              |
| +3                | 9.1    |              |
| s.L.              | 9.5    | 94.4         |
| 2+50              |        |              |
| s.L.              | 8.5    | 95.4         |
| +16               | 8.0    |              |
| cb                | 8.6    |              |
| 1/4               | 7.8    |              |
| 2                 | 6.5    | 97.4         |
| 1/4               | 7.0    |              |
| +6                | 7.9    |              |
| cb                | 7.5    |              |
| +6                | 6.4    |              |

103.92

70

|      |     |       |
|------|-----|-------|
| N.L. | 6.1 | 97.8  |
| 1+00 |     |       |
| N.L. | 5.0 | 98.9  |
| +14  | 5.3 |       |
| cb   | 6.5 |       |
| +3   | 6.8 |       |
| 1/4  | 6.3 |       |
| 2    | 5.6 | 98.3  |
| 1/4  | 5.6 |       |
| cb   | 7.6 |       |
| +4   | 6.8 |       |
| s.L. | 7.3 | 96.6  |
| 1+50 |     |       |
| s.L. | 6.3 | 97.6  |
| +16  | 5.7 |       |
| cb   | 6.5 |       |
| 1/4  | 5.6 |       |
| 2    | 4.8 | 99.1  |
| 1/4  | 5.0 |       |
| cb   | 5.5 |       |
| +6   | 4.9 |       |
| N.L. | 4.2 | 99.7  |
| 2+00 |     |       |
| N.L. | 2.7 | 101.2 |
| +14  | 3.2 |       |
| cb   | 4.0 |       |



103.92

|      |      |        |      |        |
|------|------|--------|------|--------|
| 1/4  |      |        | 3.9  |        |
| E    |      |        | 3.6  | 100.3  |
| 1/4  |      |        | 4.6  |        |
| cb   |      |        | 5.1  |        |
| +3   |      |        | 4.6  |        |
| s.L. |      |        | 5.2  | 98.7   |
|      | 2+50 |        |      |        |
| s.L. |      |        | 3.3  | 100.6  |
| +17  |      |        | 2.8  |        |
| cb   |      |        | 3.5  |        |
| 1/4  |      |        | 3.0  |        |
| E    |      |        | 1.6  | 102.3  |
| 1/4  |      |        | 1.8  |        |
| cb   |      |        | 2.6  |        |
| +7   |      |        | 0.9  |        |
| N.L. |      |        | 0.6  | 103.3  |
| T.P. | 6.17 | 110.09 | 2.00 | 103.92 |
|      | 3+00 |        |      |        |
| N.L. |      |        | 5.6  | 104.5  |
| +14  |      |        | 5.7  |        |
| cb.  |      |        | 7.1  |        |
| 1/4  |      |        | 6.4  |        |
| E    |      |        | 6.1  | 103.9  |
| 1/4  |      |        | 7.1  |        |
| cb   |      |        | 8.0  |        |
| +3   |      |        | 7.3  |        |

110.09

8

1

|                 |      |                                     |      |        |
|-----------------|------|-------------------------------------|------|--------|
| s.L.            |      |                                     | 8.3  | 101.8  |
|                 | 3+50 |                                     |      |        |
| s.L.            |      |                                     | 6.1  | 103.9  |
| cb              |      |                                     | 6.5  |        |
| +1              |      |                                     | 7.1  |        |
| 1/4             |      |                                     | 6.0  |        |
| E               |      |                                     | 5.2  | 104.9  |
| 1/4             |      |                                     | 5.0  |        |
| cb              |      |                                     | 4.9  |        |
| N.L.            |      |                                     | 4.0  | 106.1  |
|                 | 3+25 |                                     |      |        |
| N.L.            |      |                                     | 3.8  | 106.3  |
| cb              |      |                                     | 4.2  |        |
| 1/4             |      |                                     | 4.0  |        |
| E               |      |                                     | 4.2  | 105.9  |
| 1/4             |      |                                     | 5.1  |        |
| +9              |      |                                     | 6.2  |        |
| cb              |      |                                     | 5.8  |        |
| s.L.            |      |                                     | 5.2  | 104.9  |
|                 | 4+15 | N.L. Natth Shore Highlands - Paving |      |        |
| s.L.            |      |                                     | 5.0  | 104.1  |
| Top cb.         |      |                                     | 5.19 | 104.90 |
| gut - on paving |      |                                     | 5.74 | 104.35 |
| 1/4             |      |                                     | 5.18 |        |
| E               |      |                                     | 4.88 | 105.11 |
| 1/4             |      |                                     | 4.79 |        |



110.09

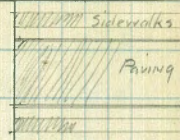
|         |  |      |        |
|---------|--|------|--------|
| gut     |  | 4.95 | 105.04 |
| Top Cb. |  | 4.23 | 105.86 |
| N.L.    |  | 3.9  | 106.2  |

50' East of W.L. N.S.H.

|               |      |        |         |
|---------------|------|--------|---------|
| N. cb Top Cb. |      | 2.99   | 107.10  |
| s Top Cb.     |      | 4.07   | 105.92  |
| T.P.          | 0.52 | 100.61 | 100.09  |
|               |      | 8.97   | 91.64 L |

Grass

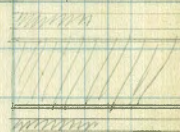
2' Law



Grass

20' Chalcidomy

Rough grading



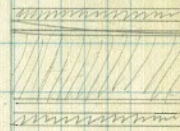
Dunes

61.97 Nail fence

Grass

60 Missouri

Rough grading



W.L. North Shore Highlands



X section of Beryl from Cass to W. L. North Shore Highlands

05:43

80' s + 20' cbs 10'  $\frac{1}{4}$

79

85.17 - BM spike in pole

$\frac{1}{4}$

9.5

75.9

0.26 85.43

cb

9.9

75.5

0+00 = E.L. Cass

s.l.

10.9

74.6

N.L. 10.2

75.2

1+25 = Cem. walk online 2' wide on North ↓

+18 10.3

75.1

N.L.

6.98

78.45

cb 11.0

74.4

1+50

$\frac{1}{4}$  11.1

74.3

s.l.

9.1

76.3

E 11.5

73.9

cb

8.7

76.7

$\frac{1}{4}$  11.2

74.2

$\frac{1}{4}$

8.6

76.8

cb 11.3

74.1

E

8.0

77.4

s.l. 12.5

72.9

$\frac{1}{4}$

7.9

77.5

0+40 = Edge of Concrete Driveway on South 10' wide online

cb

7.3

78.1

Top Cem. 11.37

74.06 ✓

N.L.

6.9

78.5

0+50 =

2+00

s.l. 11.4

74.0

N.L.

6.4

79.0

cb 11.2

74.2

cb

6.1

78.5

$\frac{1}{4}$  10.7

74.7

$\frac{1}{4}$

7.3

78.1

E 10.2

75.2

E

7.0

78.4

$\frac{1}{4}$  10.0

75.4

$\frac{1}{4}$

7.4

78.0

cb 9.6

75.8

cb

7.4

78.0

N.L. 8.8

76.6

s.l.

7.5

77.9

1+00

2+50

N.L. edge of Cem. Walk 2' wide 7.56

see sketch ↓ 77.87

s.l.

6.5

78.9

cb 8.5

76.9

cb

5.9

79.5

$\frac{1}{4}$  8.1

76.6

$\frac{1}{4}$

5.9

79.5

E 9.0

76.4

E

5.8

79.6

Plotted 10-6-28.  
CBA



|               |     |      |
|---------------|-----|------|
| $\frac{1}{4}$ | 6.1 | 79.3 |
| cb            | 5.6 | 79.8 |
| N.L.          | 5.3 | 80.1 |
| 3+00          |     |      |
| N.L.          | 3.9 | 81.5 |
| cb            | 4.7 | 80.7 |
| $\frac{1}{4}$ | 5.0 | 80.4 |
| e             | 4.9 | 80.5 |
| $\frac{1}{4}$ | 5.4 | 80.0 |
| cb            | 5.3 | 80.1 |
| s.l.          | 5.9 | 79.5 |
| 3+50          |     |      |
| s.l.          | 5.0 | 80.4 |
| cb            | 4.2 | 81.2 |
| $\frac{1}{4}$ | 4.2 | 81.2 |
| e             | 3.9 | 81.5 |
| $\frac{1}{4}$ | 4.1 | 81.3 |
| cb            | 3.6 | 81.8 |
| N.L.          | 2.7 | 82.7 |
| 4+00          |     |      |
| N.L.          | 1.7 | 83.7 |
| cb            | 1.8 | 83.6 |
| $\frac{1}{4}$ | 2.6 | 82.8 |
| e             | 2.9 | 82.5 |
| $\frac{1}{4}$ | 3.4 | 82.0 |
| cb            | 3.4 | 82.0 |

|                   |      | 73   |
|-------------------|------|------|
| s.l.              | 4.1  | 81.3 |
| 4+50              |      |      |
| s.l.              | 2.6  | 81.8 |
| cb                | 2.8  | 82.6 |
| $\frac{1}{4}$     | 2.5  | 82.9 |
| e                 | 2.2  | 83.2 |
| $\frac{1}{4}$     | 2.1  | 83.3 |
| cb                | 1.7  | 83.7 |
| N.L.              | 0.8  | 84.6 |
| 4+98 = W.L. Dawes |      |      |
| N.L.              | 0.0  | 85.4 |
| cb                | 0.6  | 84.8 |
| $\frac{1}{4}$     | 1.3  | 84.1 |
| e                 | 1.7  | 83.7 |
| $\frac{1}{4}$     | 2.2  | 83.2 |
| cb                | 2.0  | 83.4 |
| s.l.              | 3.1  | 82.3 |
| 85.17 = B.M.      |      |      |
| 11.43      96.60  |      |      |
| 0+00 = E.L. Dawes |      |      |
| s.l.              | 12.2 | 84.4 |
| cb                | 11.7 |      |
| $\frac{1}{4}$     | 11.4 |      |
| e                 | 11.9 | 84.7 |
| $\frac{1}{4}$     | 10.5 |      |
| cb                | 9.7  |      |



96.60

N.L. 8.3 883

0+50

N.L. 7.7 889

cb 8.8

 $\frac{1}{4}$  9.7

E 10.0 866

 $\frac{1}{4}$  10.6

cb 10.6

s.L. 11.2 854

1+00

s.L. 9.0 876

cb 8.8

 $\frac{1}{4}$  8.9

E 8.8 878

 $\frac{1}{4}$  8.3

cb 8.2

N.L. 6.8 898

1+50

N.L. 5.2 914

cb 5.2

 $\frac{1}{4}$  6.1

E 6.1 90.5

 $\frac{1}{4}$  6.5

cb 6.2

s.L. 6.6 900

2+00

96.60

s.L. 5.2

743

914

cb 4.4

 $\frac{1}{4}$  4.9

E 4.5

92.1

 $\frac{1}{4}$  4.5

cb 3.7

N.L. 3.3

93.3

2+50

N.L. 2.4

94.2

cb 2.8

 $\frac{1}{4}$  3.4

E 3.5

93.1

 $\frac{1}{4}$  3.8

cb 3.5

s.L. 4.0

92.6

3+00

s.L. 3.0

93.6

cb 2.3

 $\frac{1}{4}$  2.4

E 2.1

94.5

 $\frac{1}{4}$  2.1

cb 1.7

N.L. 1.1

95.5

3+50

N.L. 0.1

96.5

cb 0.6



9660

|      |      |        |
|------|------|--------|
| 1/4  | 1.0  |        |
| e    | 1.0  | 95.6   |
| 1/4  | 1.2  |        |
| cb   | 1.4  |        |
| s.l. | 1.8  | 94.8   |
| T.P. | 5.49 | 100.99 |
|      | 1.10 | 96.50  |

4+13 = W.L. North Shore Highlands Paveding.

|               |      |       |
|---------------|------|-------|
| s.l.          | 4.7  | 96.3  |
| Top cb.       | 4.98 | 96.01 |
| gut on paving | 5.55 | 99.44 |
| 1/4           | 4.97 |       |
| e             | 4.63 | 96.36 |
| 1/4           | 4.55 |       |
| gut.          | 4.69 | 96.90 |
| Top cb.       | 2.95 | 97.04 |
| N.L.          | 3.5  | 97.5  |

50 East of W.L. N.S.H.

|            |      |       |
|------------|------|-------|
| N. cb. Top | 2.63 | 98.36 |
| s. cb. Top | 3.62 | 97.97 |

X section LAW st From Cass to W.L. N.S.H.  
80' st, 20' cas 10'.

75

~~74~~

75.5'3" = B.M.

|                |      |       |      |
|----------------|------|-------|------|
|                | 3.50 | 79.03 |      |
| 0+00 E.L. Cass |      |       |      |
| N.L.           |      | 10.1  | 68.9 |
| cb             |      | 10.4  |      |
| 1/4            |      | 10.5  |      |
| e              |      | 10.4  | 68.6 |
| 1/4            |      | 10.7  |      |
| cb             |      | 11.0  |      |
| s.l.           |      | 11.3  | 67.7 |
| 0+50           |      |       |      |
| s.l.           |      | 10.6  | 68.4 |
| cb             |      | 10.4  |      |
| 1/4            |      | 10.2  |      |
| e              |      | 10.2  | 68.8 |
| 1/4            |      | 10.2  |      |
| cb             |      | 10.1  |      |
| N.L.           |      | 9.9   | 69.1 |
| 1+00           |      |       |      |
| N.L.           |      | 9.4   | 69.6 |
| cb             |      | 9.7   |      |
| 1/4            |      | 9.8   |      |
| e              |      | 9.8   | 69.2 |
| 1/4            |      | 9.9   |      |
| cb             |      | 10.0  |      |
| s.l.           |      | 10.1  | 68.9 |

Plotted 10-6-28 G.B.H.



79.03

|               |     |      |
|---------------|-----|------|
| 1+50          |     |      |
| s.l.          | 9.1 | 69.9 |
| cb            | 8.7 |      |
| $\frac{1}{4}$ | 8.8 |      |
| $\frac{1}{2}$ | 8.5 | 70.5 |
| $\frac{3}{4}$ | 8.4 |      |
| cb            | 8.2 |      |
| N.L.          | 7.9 | 71.1 |
| 2+00          |     |      |
| N.L.          | 6.8 | 72.2 |
| cb            | 7.4 |      |
| $\frac{1}{4}$ | 7.5 |      |
| $\frac{1}{2}$ | 7.2 | 71.2 |
| $\frac{3}{4}$ | 7.8 |      |
| cb            | 8.1 |      |
| s.l.          | 8.3 | 70.7 |
| 2+50          |     |      |
| s.l.          | 7.5 | 71.5 |
| cb            | 7.3 |      |
| $\frac{1}{4}$ | 7.1 |      |
| $\frac{1}{2}$ | 6.8 | 72.2 |
| $\frac{3}{4}$ | 6.6 |      |
| cb            | 6.8 |      |
| N.L.          | 6.0 | 73.0 |
| 3+00          |     |      |
| N.L.          | 5.3 | 73.7 |

79.03

77

|               |     |      |
|---------------|-----|------|
| cb            | 5.7 |      |
| $\frac{1}{4}$ | 5.8 |      |
| $\frac{1}{2}$ | 5.9 | 73.1 |
| $\frac{3}{4}$ | 6.1 |      |
| cb            | 6.2 |      |
| s.l.          | 6.6 | 72.4 |
| 3+50          |     |      |
| s.l.          | 5.8 | 73.2 |
| cb            | 5.0 |      |
| $\frac{1}{4}$ | 5.0 |      |
| $\frac{1}{2}$ | 5.0 | 74.0 |
| $\frac{3}{4}$ | 5.0 |      |
| cb            | 4.8 |      |
| N.L.          | 4.7 | 74.3 |
| 4+00          |     |      |
| N.L.          | 4.1 | 74.9 |
| cb            | 4.3 |      |
| $\frac{1}{4}$ | 4.4 |      |
| $\frac{1}{2}$ | 4.6 | 74.4 |
| $\frac{3}{4}$ | 4.7 |      |
| cb            | 4.9 |      |
| s.l.          | 5.2 | 73.8 |
| 4+50          |     |      |
| s.l.          | 4.5 | 74.5 |
| cb            | 4.5 |      |
| $\frac{1}{4}$ | 4.2 |      |



79.03

|                   |     |      |
|-------------------|-----|------|
| d                 | 4.1 | 74.9 |
| $\frac{1}{4}$     | 4.0 |      |
| cb                | 3.8 |      |
| N.L.              | 3.5 | 75.5 |
| 4+98 = W.L. Dawes |     |      |
| N.L.              | 2.5 | 76.5 |
| cb                | 2.1 |      |
| $\frac{1}{2}$     | 3.4 |      |
| e                 | 3.6 | 75.4 |
| $\frac{1}{4}$     | 3.9 |      |
| cb                | 4.0 |      |
| s.L.              | 4.4 | 74.6 |

11.89 87.42

0+20 = E.L. Dawes

|               |      |      |
|---------------|------|------|
| s.L.          | 11.6 | 75.8 |
| cb            | 11.3 |      |
| $\frac{1}{4}$ | 11.1 |      |
| e             | 10.8 | 76.6 |
| $\frac{1}{4}$ | 10.5 |      |
| cb            | 10.7 |      |
| N.L.          | 9.7  | 77.7 |
| 0+50          |      |      |
| N.L.          | 8.1  | 79.3 |
| cb            | 8.4  |      |
| $\frac{1}{4}$ | 8.7  |      |
| e             | 8.4  | 78.5 |

87.42

77

|               |      |      |
|---------------|------|------|
| $\frac{1}{4}$ | 9.2  |      |
| cb            | 9.4  |      |
| s.L.          | 10.0 | 77.4 |
| 1700          |      |      |
| s.L.          | 8.3  | 79.1 |
| cb            | 7.7  |      |
| $\frac{1}{4}$ | 7.6  |      |
| e             | 7.1  | 80.3 |
| $\frac{1}{4}$ | 6.7  |      |
| cb            | 6.6  |      |
| N.L.          | 6.2  | 81.4 |
| 1750          |      |      |
| N.L.          | 4.6  | 82.8 |
| cb            | 5.3  |      |
| $\frac{1}{4}$ | 5.6  |      |
| e             | 5.9  | 81.5 |
| $\frac{1}{4}$ | 6.2  |      |
| cb            | 6.5  |      |
| s.L.          | 7.0  | 80.4 |
| 2+00          |      |      |
| s.L.          | 7.3  | 80.1 |
| cb            | 6.9  |      |
| $\frac{1}{4}$ | 6.6  |      |
| e             | 6.2  | 81.2 |
| $\frac{1}{4}$ | 5.7  |      |
| cb            | 5.2  |      |



87.42

|               |     |      |
|---------------|-----|------|
| N.L.          | 4.0 | 83.4 |
| 2+50          |     |      |
| N.L.          | 4.0 | 83.4 |
| cb            | 5.6 |      |
| $\frac{1}{4}$ | 6.1 |      |
| $\frac{1}{2}$ | 6.5 | 80.9 |
| $\frac{3}{4}$ | 6.7 |      |
| cb            | 6.9 |      |
| s.L.          | 7.1 | 80.3 |
| 3+00          |     |      |
| s.L.          | 6.4 | 81.0 |
| cb            | 6.3 |      |
| $\frac{1}{4}$ | 5.7 |      |
| $\frac{1}{2}$ | 5.8 | 81.6 |
| $\frac{3}{4}$ | 5.5 |      |
| cb            | 5.1 |      |
| N.L.          | 3.8 | 83.6 |
| 3+50          |     |      |
| N.L.          | 2.6 | 84.8 |
| cb            | 3.1 |      |
| gut           | 4.0 |      |
| $\frac{1}{4}$ | 3.0 |      |
| $\frac{1}{2}$ | 2.8 | 84.6 |
| $\frac{3}{4}$ | 3.2 |      |
| gut           | 5.2 |      |
| cb            | 4.1 |      |

87.42

77

|                         |        |       |
|-------------------------|--------|-------|
| s.L.                    | 4.4    | 83.0  |
| 3+80                    |        |       |
| s.L.                    | 3.3    | 84.1  |
| cb                      | 3.0    |       |
| gut                     | 3.9    |       |
| $\frac{1}{4}$           | 2.3    |       |
| $\frac{1}{2}$           | 1.9    | 85.5  |
| $\frac{3}{4}$           | 1.8    |       |
| gut                     | 2.5    |       |
| cb                      | 2.0    |       |
| N.L.                    | 2.0    | 85.4  |
| 4+13 = W.L. N.S.H.      | paving |       |
| N.L.                    | 2.3    | 85.1  |
| Top cb                  | 2.64   | 84.78 |
| gut                     | 3.34   | 84.08 |
| $\frac{1}{4}$           | 3.21   |       |
| $\frac{1}{2}$           | 3.31   | 84.11 |
| $\frac{3}{4}$           | 3.46   |       |
| gut                     | 4.23   | 83.19 |
| Top cb.                 | 3.64   | 83.78 |
| s.L.                    | 3.4    | 84.0  |
| 50' East of W.L. N.S.H. |        |       |
| s. Top cb.              | 2.73   | 84.69 |
| N. Top cb.              | 1.73   | 85.69 |



X section of Chalcedony from Cass to W.L. N.S.H.  
 20' st 20' cb 10'

75.33 = B.M.

|      |                  |       |      |       |
|------|------------------|-------|------|-------|
| T.P. | 0.15             | 75.68 | 7.25 | 68.43 |
|      | 2.26             | 70.69 |      |       |
|      | 0+00 = H.L. Cass |       |      |       |
| N.L. |                  | 8.2   |      | 62.5  |
| cb   |                  | 8.8   |      |       |
| 1/4  |                  | 9.0   |      |       |
| 1/2  |                  | 9.4   |      | 61.3  |
| 3/4  |                  | 9.7   |      |       |
| cb   |                  | 10.2  |      |       |
| s.L. |                  | 10.7  |      | 60.0  |
|      | 0+50             |       |      |       |
| s.L. |                  | 10.4  |      | 60.3  |
| cb   |                  | 9.7   |      |       |
| 1/4  |                  | 9.5   |      |       |
| 1/2  |                  | 9.2   |      | 61.5  |
| 3/4  |                  | 9.0   |      |       |
| cb   |                  | 8.7   |      |       |
| N.L. |                  | 8.0   |      | 62.7  |
|      | 1+00             |       |      |       |
| N.L. |                  | 7.3   |      | 63.4  |
| cb   |                  | 7.9   |      |       |
| 1/4  |                  | 8.7   |      |       |
| 1/2  |                  | 9.0   |      | 61.7  |
| 3/4  |                  | 9.3   |      |       |
| cb   |                  | 9.7   |      |       |

Plotted 10-6-28 - C.B.H.

70.69

|      |      |      |  |        |
|------|------|------|--|--------|
| s.L. |      | 10.0 |  | 7960.6 |
|      | 1+50 |      |  |        |
| s.L. |      | 9.4  |  | 61.3   |
| cb   |      | 8.9  |  |        |
| 1/4  |      | 8.5  |  |        |
| 1/2  |      | 8.3  |  | 62.4   |
| 3/4  |      | 7.9  |  |        |
| cb   |      | 7.6  |  |        |
| N.L. |      | 7.2  |  | 63.5   |
|      | 2+00 |      |  |        |
| N.L. |      | 6.4  |  | 64.3   |
| cb   |      | 6.2  |  |        |
| 1/4  |      | 6.9  |  |        |
| 1/2  |      | 7.1  |  | 63.6   |
| 3/4  |      | 7.3  |  |        |
| cb   |      | 7.7  |  |        |
| s.L. |      | 7.9  |  | 62.8   |
|      | 2+50 |      |  |        |
| s.L. |      | 6.6  |  | 64.1   |
| cb   |      | 6.3  |  |        |
| 1/4  |      | 6.2  |  |        |
| 1/2  |      | 6.1  |  | 64.6   |
| 3/4  |      | 6.0  |  |        |
| cb   |      | 5.8  |  |        |
| N.L. |      | 5.5  |  | 65.2   |
|      | 3+00 |      |  |        |



70.64

|               |     |      |
|---------------|-----|------|
| N.L.          | 4.4 | 66.3 |
| cb            | 4.8 |      |
| $\frac{1}{4}$ | 5.0 |      |
| $\frac{1}{2}$ | 5.1 | 65.6 |
| $\frac{3}{4}$ | 5.3 |      |
| cb            | 5.5 |      |
| s.l.          | 6.0 | 64.7 |
| 3+50          |     |      |
| s.l.          | 5.6 | 65.1 |
| cb            | 4.7 |      |
| $\frac{1}{4}$ | 4.5 |      |
| $\frac{1}{2}$ | 4.1 | 66.6 |
| $\frac{3}{4}$ | 3.7 |      |
| cb            | 3.6 |      |
| N.L.          | 3.3 | 67.4 |
| 4+00          |     |      |
| N.L.          | 2.2 | 68.5 |
| cb            | 2.7 |      |
| $\frac{1}{4}$ | 3.0 |      |
| $\frac{1}{2}$ | 3.5 | 67.2 |
| $\frac{3}{4}$ | 3.7 |      |
| cb            | 4.1 |      |
| s.l.          | 4.6 | 66.1 |

See Book 1277 - Page 7  
for the rest of the Streets.

## DIRECTIONS FOR USE OF TABLES

TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1% to 1%. If ground is nearly level, the cut or fill at side stake is located by the double-entry method in left column and top row. The number in body

of table in same row and column gives distance from side stake to slope stake. If ground is not

level, the distance from side stake to slope stake is found by adding to the amount if cut, or subtracting if fill, the amount to cut or fill and find in table. Set up rod at this point and line of sight should cut

target. **AND**

target. **INFORMATION**

necessary.

TABLE No. 2

To find Tangent and External for curve of any other degree, divide by degree of curve and

add correction found in column of corrections.

Degree of curve with a given  $T$  may be found by dividing tangent (or external), opposite  $T$  by

given tangent (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.



27433.8  
 641  
 280.79  
 273  
 273.06

ENGINEERING DEPARTMENT,  
 CITY OF SAN DIEGO  
 CALIFORNIA.

46 522.30  
 06 55.00  
 51.00

4 24.00  
 66

378.12  
 133  
 379.65  
 912  
 37053  
 469  
 37517  
 533  
 369.34  
 402  
 373.36  
 895  
 36441  
 184  
 36625  
 217  
 364.08  
 1268  
 376.76  
 238  
 274.88

310.74  
 10.72  
 321.46  
 10.32  
 311.14  
 2.77  
 314.09  
 3.35  
 310.74  
 52  
 78  
 100+53.70  
 50.72  
 101404.74  
 101+55.18

60  
 40  
 40  
 2670  
 1330

25 52  
 36  
 61  
 45.09  
 5.99  
 39.10  
 2.02  
 47.22  
 40  
 12  
 53  
 18  
 26  
 14  
 22

4616  
 5.99  
 49.47  
 202  
 49.44  
 1.91  
 40.48  
 541  
 45.89  
 45.87  
 77  
 45.02

45.10  
 056  
 45.94  
 541  
 46.53  
 432  
 44.81  
 814  
 36.71

60  
 355  
 245

42.29  
 5.61  
 56.49  
 42.49  
 36.71  
 5.58

42.29  
 40.53  
 1.76

50

40.53