1206

POST

FIELD BOOK

No. 1335

1206

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THE FREDERICK POST CO.

ENGINEERING and DRAFTING SUPPLIES

IRVING PARK STATION

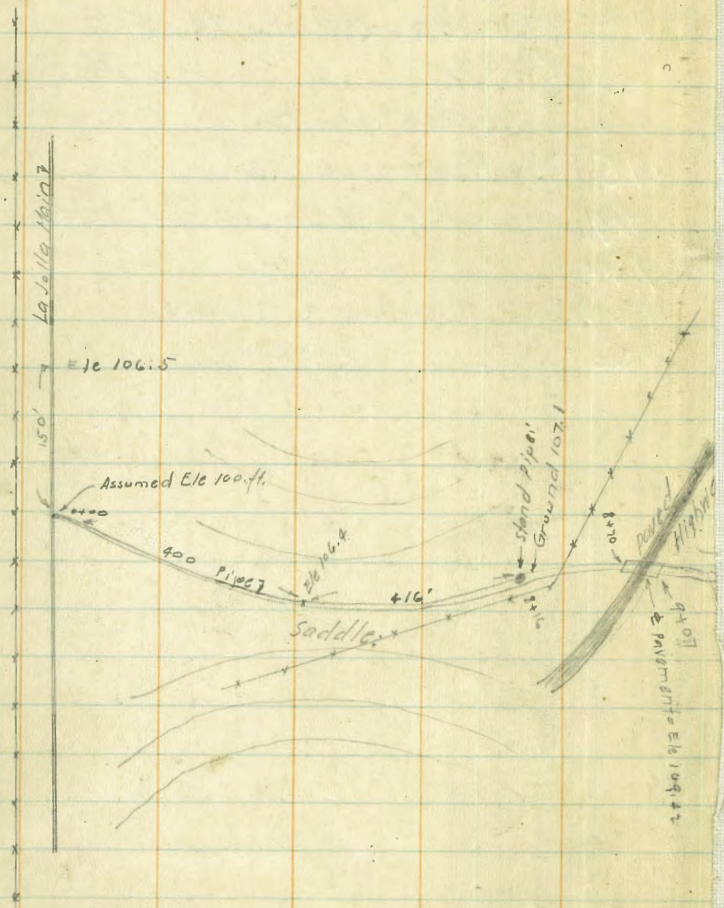
CHICAGO, ILL.

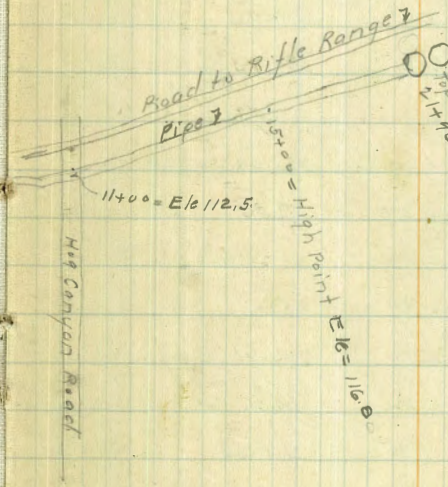
X Sec. Montecello & Alhambra Park	2
" " Wly Prod. of Monroe Ave.	3
" " Madison from alley West of Winona to 51st	4
" " Adams Ave. " Winona to 51st	7
" " Collier " " 50th	15
" " Sampson Colton " R.R.	19
U.S. Rifle Range pipe line	25
Hog Canyon or La Jolla Dr. Road Alinement	26
X Sec " " " —	34
cb Levels Kite Brooks to Upas	63
X Sec. Winona Univ. to Landis	65

Discontinued Dec 73 7/11/20 AA.

2" Pipe line from La Jolla Main to Marine Rifle range.

Bennan.
Osburne.
Flead. July 19th - 1927





	100.00	112.80
+	12.92	7.61
π	112.92	110.19 Top stand Pipe.
−	4.90	
Ele	108.02	112.8
+	4.78	5.7
π	112.80	107.1
−	0.57	
	112.23	
+	9.03	112.80
π	121.26	3.63
−	12.42	109.17 Road.
Ele	108.84	
+	1.48	112.80
π	110.32	.51
−	12.91	107.7 ° Pipe in Cul:
	97.41	
+	1.57	112.80
	98.98	3.38
−	12.81	109.42
π	86.17	
		110.32
		8.50
		101.82 Top Tank

Bottom tank Appe 93.0

	86.17
+	1.33
π	87.50
−	6.54
	80.96
+	5.69
	86.65

83 top Bldg 5

B.M.s for Section of Sts in Montecello & Alhambra Park

July 20-27 Dennan Osborn Flood.

	+	T	−	Elv.	
	12.59	369 .64		357.05	B.P. S.E. El Cajon & 49th
#	12.15	381 .02	0.77	368.87	Rock Alley.
#	6.20	385.99	1.23	379.79	Nails in Pole
#	4.17	382.31	8.25	377.74	Hub N.W. Cor Monroe and Winona
#	7.67	389.18	0.80	381.51	Nail/Fence Post
#	6.69	394.11	1.76	387.42	Rock.
#	5.48	396.54	3.05	391.06	Rock.
#	5.40	397.50	4.44	392.10	Rock.
#	3.02	394.95	5.57	391.93	Hub S.E. Cor Collier & Winona.
#			3.21	391.74	Hub S.W. Cor Collier & 50th.
#	4.10	395.71	3.29	391.66	Rock.
#	3.79	393.69	5.81	389.90	Rock.
#			2.19	391.54	Nail Cor fence 50th & Adams.
#	5.36	392.90	6.10	387.59	Rock.
#	3.54	392.02	4.47	388.48	Hub N.E. Cor 50th & Madison
#	4.60	386.13	10.49	381.53	Rock.
#	6.53	388.63	4.03	382.10	Rock.
#	6.05	391.70	2.98	385.65	Rock.
#	3.37	390.28	4.79	386.91	Curb El Cajon.
#	0.67	384.03	6.92	383.36	383.45 noted. Mon S.W. Cor El Cajon & 50th.
#	0.78	372.06	12.75	371.28	
#	4.32	363.91	12.47	359.59	
#			6.85	357.06 = 357.05	Initials

396.54 − 6.01 = 390.53 Hub N.E. Cor. Adams & Winona.

Xsectioned 60'
10' CBs
10' Qrts

July 20-27

Donnan.
Osborn.
Flood.

Monroe:

Xsection of the Westerly prolongation of Monroe Ave. from the east line of the alley west of Winona to a point 200' west: 60' wide: 10' CBs, 10' quarters:

+	π	−	Ele:
5.26	383.00		377.74 = Hub N.W. Cor Monroe and Winona: see page 2.
00 = E.L. Alley N.L			6.5 376.5
cb			6.0 377.0
¼			5.8 377.2
℄			5.6 377.4
¼			5.8 377.2
cb			5.7 377.3
S.L.			6.0 377.0
0+50 S.L			6.4 376.6
cb			6.6 376.4
¼			6.6 376.4
℄			6.7 376.3
¼			6.9 376.1
cb			7.2 375.8
N.L			7.1 375.9
1+00 N.L			8.5 374.5
cb			7.8 375.4
¼			8.0 375.0
℄			8.0 375.0
¼			7.9 375.1
cb			7.6 375.4
S.L.			7.6 375.4

Plotted
7/27/27
J. H. Hayes

+	π	−	Ele: 3
	383.00		
1+50 S.L		8.4	374.6
cb		8.4	374.6
¼		8.9	374.1
℄		8.8	374.2
¼		8.6	374.4
cb		8.5	374.5
N.L		9.2	373.8
1+50 N.L		10.4	372.6
cb		10.7	372.3
¼		10.7	372.3
℄		10.8	372.2
¼		10.4	372.6
cb		10.0	373.0
S.L		9.5	373.5

Co. st. 10 Cbs 10 Alts. July 20-27 Donnan Osborne Flood. Madison:

Xsection Madison Ave from the east line of the alley west of Winona Ave to 51st st

	+	⊼	−	Elc
	8.16	389.67		381.51 Nail fence post E side Winona between Madison and Monroe. See page 2.
0+00 = N.L. Winona Ave S.L.			7.4	382.3
cb			7.3	382.4
1/4			7.0	382.7
℄			6.4	383.3
1/4			6.7	383.0
cb			6.5	383.2
N.L.			6.4	383.3
0+50 N.L.			7.0	382.7
cb			7.3	382.4
1/4			7.2	382.5
℄			6.9	382.8
1/4			7.1	382.6
cb			7.7	382.0
S.L.			8.0	381.7
1+00 S.L.			8.4	381.3
cb			7.7	382.0
1/4			7.8	381.9
℄			8.1	381.6
1/4			7.6	382.1
cb			7.5	382.2
N.L.			7.1	382.6

	+	⊼	−	Elc
1+70 N 1+50 S = E.L. Alley, West of Winona				
N.L.			8.1	381.6
cb			8.5	381.2
1/4			8.9	380.8
℄			9.2	380.5
1/4			9.3	380.4
cb			9.3	380.4
S.L.			9.2	380.5
Intersection of Winona and Madison See Book Page:				
0+00 = E.L. Winona Ave. S.L.			6.3	383.4
cb			6.4	383.3
1/4			5.8	383.9
℄			6.1	383.6
1/4			5.9	383.8
cb			5.7	384.0
N.L.			5.0	384.7
0+50 N.L.			4.2	385.5
cb			4.7	385.0
1/4			4.9	384.8
℄			5.0	384.7
1/4			4.7	385.0
cb			5.2	384.5
S.L.			5.7	384.0
1+00 S.L.			4.3	385.4
cb			4.3	385.4

	+	T 389.67	−	Elc	Madison:
1+00 1/4			4.2	385.5	
℄			4.2	385.5	
1/4			4.1	385.6	
cb			3.8	385.9	
N.L			3.7	386.0	
1+50 N.L			2.9	386.8	
cb			2.7	387.0	
1/4			2.9	386.8	
℄			3.2	386.5	
1/4			2.9	386.8	
cb			2.1	387.6	
S.L			2.6	387.1	
2+00 S.L			2.7	387.0	
cb			2.4	387.3	
1/4			1.8	387.9	
℄			2.1	387.6	
1/4			2.3	387.4	
cb			1.6	388.1	
N.L			1.7	388.0	
2+50 N.L			1.6	388.1	
cb			1.5	388.2	
1/4			1.0	388.7	
℄			1.2	388.5	
1/4			1.8	387.9	
cb			1.9	387.8	
S.L			2.0	387.7	

	+	T 389.67	−	Elc	5
#	3.94	392.36	1.28	388.42	
2+70 = W.L. 50th sf. S.L.			4.9	387.5	
cb			4.6	387.8	
1/4			4.7	387.7	
℄			4.7	387.7	
1/4			4.5	387.9	
cb			5.0	387.4	
N.L			5.2	387.2	
0+00 = E.L. 50th sf. N.L			4.4	388.0	
cb			4.6	387.8	
1/4			5.0	387.4	
℄			4.7	387.7	
1/4			5.0	387.4	
cb			4.5	387.9	
S.L			4.4	388.0	
0+50 S.L			5.0	387.4	
cb			5.0	387.4	
1/4			5.0	387.4	
℄			4.8	~~387.6~~ 387.6	
1/4			5.0	387.4	
cb			5.1	387.3	
N.L			5.1	387.3	
1+00 N.L			4.4	388.0	
cb			4.7	387.7	
1/4			5.3	387.1	
℄			5.0	387.4	
1/4			5.2	387.2	

	+	T 392.36	−	E/e	Madison.
CL			5.1	387.3	
S.L			5.3	387.1	
1+50 S.L			5.5	386.9	
CL			5.3	387.1	
1/4			5.5	386.9	
℄			5.2	387.2	
1/4			5.5	386.9	
CL			5.5	386.9	
N.L			5.7	386.7	
2+00 N.L			6.3	386.1	
CL			6.0	386.4	
1/4			6.3	386.1	
℄			6.0	386.4	
1/4			6.2	386.2	
CL			6.0	386.4	
S.L			5.9	386.5	
2+50 S.L			6.5	385.9	
CL			6.4	386.0	
1/4			6.4	386.0	
℄			6.0	386.4	
1/4			6.4	386.0	
CL			6.2	386.2	
N.L			6.3	386.1	
2+70 = W.L Altadena Ave. N.L			5.8	386.6	
CL			5.5	386.9	
1/4			6.0	386.4	

	+	T 392.36	−	E/e	6
℄			6.2	386.2	
1/4			6.6	385.8	
CL			6.4	386.0	
S.L			6.2	386.2	
#		393.24	5.07	387.29	Nail fence Post NE Cor Altadena & Madison
0+00 = E.L Altadena Ave S.L			6.5	386.7	
CL			6.3	386.9	
1/4			6.0	387.2	
℄			6.3	386.9	
1/4			6.5	386.5	
CL			6.5	386.5	
N.L			6.6	386.6	
0+50 N.L			6.2	387.0	
CL			6.4	386.8	
1/4			6.5	386.7	
℄			6.1	387.1	
1/4			6.6	386.6	
CL			6.6	386.6	
S.L			6.4	386.8	
1+00 S.L			6.4	386.8	
CL			6.3	386.9	
1/4			6.2	387.0	
℄			5.8	387.4	
1/4			6.2	387.0	
CL			6.1	387.1	
N.L			5.7	387.5	

	+	π 393.24	−	Ele:	Madison:
1+50 N.L			5.4	387.8	
cb			5.6	387.6	
1/4			5.6	387.6	
℄			5.1	388.1	
1/4			5.5	387.7	
cb			5.6	387.6	
S.L.			5.4	387.8	
2+00 S.L.			5.0	388.2	
cb			5.1	388.1	
1/4			5.2	388.0	
℄			4.8	388.4	
1/4			5.3	387.9	
cb			5.1	388.1	
N.L.			4.9	388.3	
2+50			4.9	388.3	
cb			5.3	387.9	
1/4			5.4	387.8	
℄			5.1	388.1	
1/4			5.4	387.8	
cb			5.2	388.0	
S.L.			5.2	388.0	
2+70 = W.L. 51st St produced North S.L.			5.5	387.7	
cb			5.5	387.7	
1/4			5.7	387.5	
℄			5.3	387.9	
1/4			5.8	387.4	

	+	π 393.24	−	Ele:
cb.			5.6	387.6
N.L.			5.3	387.9
Intersection 51st St: 10' cbs. 10' gts each way:				
W. cb. 51st N.L.			5.3	387.9
cb			5.6	387.6
1/4			5.9	387.3
℄			5.5	387.7
1/4			5.8	387.4
cb			5.9	387.3
S.L.			5.8	387.4
W. 1/4 51st S.L.			5.7	387.5
cb			5.9	387.3
1/4			5.7	387.5
℄			5.7	387.5
1/4			6.0	387.2
cb			6.0	387.2
N.L			5.3	387.9
℄ L 51st N.L			5.1	388.1
cb			5.9	387.3
1/4			6.0	387.2
℄			5.7	387.5
1/4			6.0	387.2
cb			5.9	387.3
S.L			5.6	387.6
E 1/4 51st S.L.			6.0	387.2
cb			6.1	387.1

	+	T	−	Madison;
		393.24		
1+50	1/4		6.1	387.1
cb	℄		5.8	387.4
1/4	1/4		6.0	387.2
℄	cb		5.9	387.3
1/4	N.L.		5.1	388.1
cb	E C6.51st N.L.		5.4	387.8
S.L.	cb		5.8	387.8
2+00	1/4		6.2	387.0
cb	℄		6.0	387.2
1/4	1/4		6.3	386.9
℄	cb		6.4	386.8
1/4	S.L.		6.2	387.0
cb	E.L. 51st produced North S.L.		5.9	387.3
N.L.	cb		6.3	386.9
2+50	1/4		6.5	386.7
cb	℄		6.2	387.0
1/4	1/4		6.2	387.0
℄	cb		5.8	387.4
1/4	N.L.		5.5	387.7
cb	6.16	392.41	6.99	386.25
S.L.			3.94	388.47 = 388.40 See Page 2.
2+70 =				
cb				
1/4				
℄				
1/4				

Co'st
10'CGs
15'Afs

July 20-27 { Brennan, Osborn, Flood.

Adams:

Note: Not dedicated full width for entire length.

Xsection of Adams Ave from Alley west of Winona Ave to termination east of 51st St

	+	π	−	Ele:
0+00 = W.L. Winona Ave:				
#	4.93	394.16 ✓		390.53 Hub N.E Cor Winona and Adams
0+0 N.L.			5.0	390.5
cb			4.9	390.6
1/4			5.3	390.2
℄			5.7	389.8
1/4			5.7	389.8
cb			5.5	390.0
S.L.			5.7	389.8
0+50 S.L.			5.5	390.0
cb			5.7	389.8
1/4			4.9	390.6
℄			5.3	390.2
1/4			5.6	389.9
cb			5.7	389.8
N.L.			5.6	389.9
1+00 N.L.			5.6	389.9
cb			5.6	389.9
1/4			5.5	390.0
℄			6.1	389.9
1/4			6.1	389.4
cb.			6.1	389.4
S.L.			6.1	389.4

	+	π	−	Ele:
		394.46		
144.10 N 143.90 S = E.L. Alley lying west of Winona:				
S.L.			5.7	389.8
cb			5.8	389.7
1/4			5.8	389.7
℄			6.0	389.5
1/4			6.0	389.5
cb			5.8	389.7
N.L.			6.0	389.5
From Winona to 50th:				
0+00 = E.L. Winona Ave:				
N.L.			5.0	390.5
cb			5.0	390.5
1/4			5.5	390.0
℄			5.7	389.8
1/4			5.8	389.7
cb			6.0	389.5
S.L.			6.3	389.2
0+50 S.L.			6.3	389.2
cb			6.0	389.5
1/4			5.8	389.7
℄			5.9	389.6
1/4			6.0	389.5
cb			5.8	389.7
N.L.			5.6	389.9

	+	ℸ	−	Ele:
		395.46		Adams:
1+00 N.L.			5.5	390.0
CL			6.1	389.4
1/4			6.2	389.3
℄			6.2	389.3
1/4			6.2	389.3
CL			6.1	389.4
S.L.			5.7	389.8
1+50 S.L.			6.7	388.8
CL			6.6	388.9
1/4			6.5	389.0
℄			6.3	389.2
1/4			6.3	389.2
CL			6.2	389.3
N.L.			6.2	389.3
℄	4.47	393.66	6.27	389.19
2+00 N.L.			4.8	388.9
CL			4.7	388.8
1/4			5.0	388.7
℄			5.0	388.7
1/4			5.2	388.5
CL			5.1	388.6
S.L.			5.3	388.4
2+50 S.L.			5.0	388.7
CL			5.1	388.6
1/4			5.1	388.6
℄			4.7	389.0

	+	ℸ	−	Ele
		393.66		
1/4			4.2	389.5
CL			4.1	389.6
N.L.			4.6	389.1
2+70 = W.L. 50th St.				
N.L.			4.9	388.8
CL			5.2	388.5
1/4			5.0	388.7
℄			5.0	388.7
1/4			5.0	388.7
CL			5.1	388.6
S.L.			5.3	388.4
0+00 = E.L. 50th St.				
S.L.			4.2	389.5
CL			4.8	388.9
1/4			4.7	389.0
℄			4.6	389.1
1/4			4.0	389.7
CL			3.7	390.0
N.L.			4.1	389.6
0+50 N.L.			3.4	390.3
CL			3.7	390.0
1/4			4.2	389.5
℄			4.3	389.4
1/4			4.0	389.7
CL,			3.8	389.9
S.L.			3.7	390.0

	+	ℼ 393.66	−	Ele: Adams:
1+00 S.L			4.1	389.6
cb			4.0	389.7
1/4			3.9	389.8
℄			3.9	389.8
1/4			3.5	390.2
cb			3.3	390.4
N.L.			3.1	390.6
1+50 N.L.			3.2	390.5
cb			3.5	390.2
1/4			3.6	390.1
℄			3.5	390.2
1/4			3.6	390.1
cb			3.6	390.1
S.L.			3.7	390.0
2+00 S.L.			3.1	390.6
cb			3.5	390.2
1/4			3.7	390.0
℄			3.6	390.1
1/4			3.6	390.1
cb			3.5	390.2
N.L.			3.5	390.2
#	5.86	396.40	3.12	390.54 Hub S.W. Cor Adams & Altadena
2+50 N.L.			5.9	390.5
cb			5.9	390.5
1/4			5.8	390.6
℄			6.0	390.4

	+	ℼ 396.40	−	℄/c
1/4			6.0	390.4
cb			5.9	390.5
S.L.			5.3	391.1
2+70 = N.L. Altadena Ave produced North:				
S.L.			5.9	390.5
cb			6.0	390.4
1/4			5.9	390.5
℄			5.9	390.5
1/4			5.8	390.6
cb			5.9	390.5
N.L.			6.1	390.3
#	5.90	396.40	5.86	390.54 Hub S.W. Cor Adams & Altadena
West Curb.				
N.L.			6.1	390.3
cb			5.8	390.6
1/4			5.7	390.7
℄			5.4	391.0
1/4			5.6	390.8
cb			5.7	390.7
S.L.			5.6	390.8
West 1/4				
S.L.			5.8	390.6
cb			5.5	390.9
1/4			5.6	390.8
℄			5.5	390.9
1/4			5.4	391.0

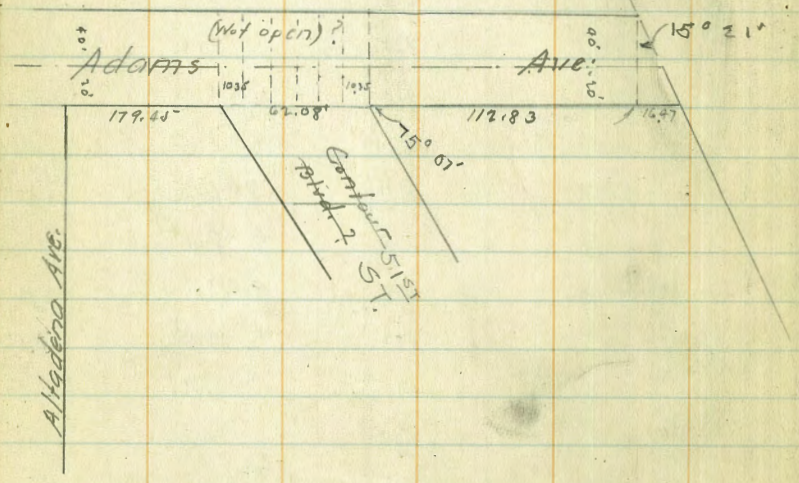
+	π 396.44	−	Adams:
cb		5.7	390.7
N.L.		5.6	390.8
	℄		
N.L.		5.5	390.9
cb		5.7	390.7
1/4		5.4	391.0
℄		5.4	391.0
1/4		5.6	390.8
cb		5.7	390.7
S.L.		5.7	390.7
	E 1/4		
S.L.		5.8	390.6
cb		5.9	390.5
1/4		5.8	390.6
℄		5.8	390.6
1/4		5.7	390.7
cb		5.5	390.9
N.L.		5.4	391.0
	E Curb:		
N.L.		5.4	391.0
cb		5.5	390.9
1/4		5.4	391.0
℄		5.5	390.9
1/4		5.8	390.6
cb		5.8	390.6
S.L.		5.6	390.8

+	π 396.44	−	℄/℄
			12
	℄ L. Altadena Ave produced North. = 0+00		
S.L.		5.7	390.7
cb		5.8	390.6
1/4		5.8	390.6
℄		5.9	390.5
1/4		5.8	390.6
cb		5.5	390.9
N.L.		5.5	390.9
0+50 N.L.		5.6	390.8
cb		5.7	390.7
1/4		5.7	390.7
℄		5.8	390.6
1/4		5.5	390.9
cb		5.4	391.0
S.L.		5.4	391.0
1+00 S.L.		6.1	390.3
cb		5.7	390.7
1/4		5.3	391.1
℄		5.2	391.2
1/4		5.5	390.9
cb		5.7	390.7
N.L.		5.7	390.7
# 4.37	395.64	5.17	391.27 Stone.
1+50 N.L.		5.5	390.1
cb		5.3	390.3
1/4		5.2	390.4

+	π 395.64	−	Adams:
℄		5.7	390.4
1/4		5.7	390.4
cb		5.3	390.3
S.L.		5.4	390.2
		5.5	390.1

1+79.45 = W.L. ~~Gentour~~ Blvd on the South (see sketch). 51 st ST.

cb		5.4	390.2
1/4		5.4	390.2
℄		5.4	390.2
1/4		5.8	389.8
cb		5.8	390.1
N.L.		5.6	390.0



W. cb

N.L.		5.6	390.0
cb		5.7	389.9
1/4		5.8	389.8

+	π 395.64	−	E/c
℄		5.4	390.2
1/4		5.3	390.3
cb		5.0	390.6
S.L.		5.1	390.5

West 1/4

S.L.		5.3	390.3
cb		5.7	390.4
1/4		5.3	390.3
℄		5.4	390.2
1/4		5.8	389.8
cb		5.8	389.8
N.L.		5.9	389.7

℄'

N.L.		5.9	389.7
cb		5.9	389.7
1/4		5.7	389.9
℄		5.7	389.9
1/4		5.7	389.9
cb		5.7	389.9
S.L.		5.7	389.9

E 1/4

S.L.		6.3	389.3
cb		6.2	389.4
1/4		6.2	389.4
℄		6.0	389.6
1/4		6.0	389.6

+	π 395.64	−	E/e
			Adams:
cb		6.0	389.6
N.L.		5.8	389.8
	E Cb:		
N.L.		6.1	389.5
cb		6.3	389.3
1/4		6.2	389.4
℄		6.1	389.5
1/2		6.3	389.3
cb		6.1	389.5
S.L.		6.3	389.3
	51st ST.		
0+00	E.L. Contour ~~Blvd~~ on the South.		
S.C.		6.4	389.2
cb.		6.3	389.3
1/2		6.1	389.5
℄		5.8	389.8
1/4		6.1	389.5
cb		6.6	389.0
N.L.		6.7	388.9
0+50 N.L.		8.6	387.0
cb		8.4	387.2
1/4		8.1	387.5
℄		7.9	387.7
1/4		7.9	387.7
cb		7.8	387.8
S.L.		7.6	387.8
#	4.15	389.72	9.87 385.77 Stone:

+	π 389.92	−	E/e
1+00	S.L.	5.5	384.4
	cb	5.5	384.4
	1/4	5.4	384.5
	℄	5.1	384.8
	1/4	5.5	384.4
	cb	6.0	383.9
	N.L.	7.5	382.4
1+12.83	See Sketch: N.L.	12.8	377.1
	cb	12.1	377.8
	1/4	9.1	380.8
	℄	8.2	381.7
	1/4	10.1	379.8
	cb	9.9	380.0
	S.L.	9.3	380.6
X { 11283 North / 12930 South	= Diagonal. See Sketch		
	S.L.	15.6	374.3
	cb	15.6	374.3
	1/4	13.4	376.5
	℄	11.7	378.2
	1/4	11.6	378.3
	cb	13.6	376.3
	N.L.	12.8	377.1
Note: Deep canyon; Improvements should end at 1+00			
#	6.18	395.41	0.69 389.23
#	4.45	395.17	4.69 390.72
			3.62 391.55 - 391.5 / See Page 1

+	π	−	E/c:	Collier.
July 22nd 27.	Donnan Osborne Flood.			

Xsection Collier from E.L. of alley West of Winona Ave to a line 17.2' east of 50th St.

Note: This St is only 30' in width but we xsectioned it 66' wide as it will probably be opened to that: 10' Cds 16' Qts:

6.33	398.26		391.93 Se Cor Hub Winona and Collier.

B/L from Winona to alley West of Winona

0+00 = W.L. of Winona Ave produced North.

0+00 S.L.		5.4	392.9
cb		5.3	393.0
1/4		5.5	392.7
℄		5.4	392.9
1/4		5.4	392.9
cb		5.3	393.0
N.L.		5.4	392.9
0+50 N.L.		4.5	393.8
cb		4.4	393.9
1/4		4.4	393.9
℄		4.7	393.6
1/4		4.6	393.7
cb		4.7	393.6
S.L.		4.9	393.4
1+00 S.L.		4.3	394.0
cb		4.3	394.0
1/4		4.5	393.8
℄		4.8	393.8

+	π	−	E/c
	398.26		

15

1/4		4.5	393.8
cb		4.2	394.1
N.L.		4.2	394.1
#	5.25	399.18	4.33 393.93

1+46.5 = E.L. of Alley lying west of Winona Ave: Alley line produced N.

1+46.5 S.L.		5.0	393.3
cb		5.0	393.3
1/4		4.9	393.4
℄		5.1	393.2
1/4		5.0	393.3
cb		5.0	393.3
N.L.		5.0	393.3

Intersection of Winona Ave and Collier 66' Wide: 10' Cds. 16' Qts.

6.31	398.24	391.93 S.E. Cor hub Winona and Collier.

W.L. of Winona Ave produced North

S.L.		5.4	392.9
cb		5.3	393.0
1/4		5.5	392.8
℄		5.4	392.9
1/4		5.4	392.9
cb		5.3	393.0
N.L.		5.4	392.9

West curb.

N.L.		5.4	392.9
cb		5.5	392.8

+	π 398.24	−	Elev.
			Collier
¼		5.0	392.7
℄		5.6	392.6
¼		5.4	392.8
cb		5.0	392.7
S.L.		5.0	392.7
	West ¼		
S.L.		5.6	392.6
cb		5.0	392.7
¼		5.4	392.8
℄		5.6	392.6
¼		5.6	392.6
cb		5.0	392.7
N.L.		5.0	393.2
	℄		
N.L.		5.3	392.9
cb		6.0	392.2
¼		5.8	392.4
℄		5.9	392.3
¼		5.6	392.6
cb		5.3	392.9
S.L.		5.1	393.1
	E ¼		
S.L.		5.6	392.6
cb		5.9	392.3
¼		5.8	392.4
℄		6.1	392.1

+	π 398.24	−	Elev.
¼		6.4	391.8
cb		6.2	392.0
N.L.		6.1	392.1
	East Curb		
N.L.		6.6	391.6
cb		6.7	391.5
¼		6.6	391.6
℄		6.4	391.8
¼		6.2	392.0
cb		6.0	392.2
S.L.		5.6	392.6
	E.L. of Winona Ave = 0+00		
S.L.		6.3	391.9
cb		6.2	392.0
¼		6.4	391.8
℄		6.7	391.5
¼		6.8	391.4
cb		6.8	391.4
N.L.		6.8	391.4
0+50 E.L.		7.4	390.8
cb		7.2	391.0
¼		7.2	391.0
℄		6.8	391.4
¼		7.1	391.1
cb		7.4	390.8
S.L.		7.5	390.7

	+	T 398.24	−	Elc
				Collier.
1+00 S.L.			7.9	390.3
cb			8.0	390.2
1/4			7.5	390.7
℄			7.6	390.6
1/2			7.6	390.6
cb			7.7	390.5
N.L.			7.5	390.7
1+50 N.L.			7.5	390.7
cb			7.6	390.6
1/4			7.6	390.6
℄			7.5	390.7
1/4			7.5	390.7
cb			7.8	390.4
S.L.			7.9	390.3
2+00 S.L.			7.6	390.6
cb			7.1	391.1
1/4			7.2	391.0
℄			7.3	390.9
1/2			7.2	391.0
cb			7.1	391.1
N.L.			6.9	391.3
2+50 N.L.			6.4	391.8
cb			6.5	391.7
1/4			6.6	391.6
℄			6.5	391.7
1/2			6.5	391.7

	+	T 398.24	−	Elc
				17
cb			6.5	391.7
S.L.			6.8	391.4
2+70 = W.L. 50th St produceded North.				391.7
S.L.			6.50	391.74 = Hub S.W. Cor. See Page 1
cb			6.1	392.1
1/4			5.9	392.3
℄			6.2	392.0
1/4			6.4	391.8
cb			6.3	391.9
N.L.			6.5	391.7
# 6.00		397.74	6.50	391.74
Intersection of 50th St. 60 wide 10 Cbs 16 Qts; West Curb 50th St				
N.L.			5.6	392.1
cb			5.7	392.0
1/4			5.8	391.9
℄			5.8	391.9
1/4			5.7	392.0
cb			5.9	391.8
S.L.			6.0	391.7
W 1/4				
S.L.			5.9	391.8
cb			5.6	392.1
1/4			5.5	392.2
℄			5.7	392.0
1/4			5.4	392.3

+	π 397.74	−	Collier.
cb		5.6	392.1
N.L.		5.5	392.2
	℄		
N.L.		5.0	392.7
cb		5.7	392.5
1/4		5.5	392.2
℄		5.4	392.3
1/4		5.4	392.3
cb		5.3	392.4
S.L.		5.4	392.3
	E 1/4		
S.L.		5.6	392.1
cb		5.6	392.1
1/4		5.4	392.3
℄		5.3	392.4
1/4		5.4	392.3
cb		4.7	393.0
N.L.		4.7	393.0
	E Cb		
N.L.		5.3	392.4
Cb		5.7	392.5
1/4		5.4	392.3
℄		5.5	392.2
1/4		5.4	392.3
Cb		5.6	392.1
S.L.		5.6	392.1

+	π 397.74	−	E/C;
			18
0+00 = E.L. 50th St produceded North.			
S.L.		5.7	391.99 Hub S.E. Cor
cb		5.6	392.1
1/4		5.5	392.2
℄		5.7	392.0
1/4		5.8	391.9
cb		5.5	392.2
N.L.		5.5	392.2
0+17 = End of St.			
N.L.		5.6	392.1
cb		5.5	392.2
1/4		5.7	392.0
℄		5.6	392.1
1/4		5.7	392.0
cb		5.7	392.0
S.E.		5.9	391.8
#			0+00 = 391.74 = 391.74 Hub S.W. Cor 50th & Collier; See Page 1.

+	π	−	Elc:	Dennan Osborne Flood
			July 23-27	

Xsection Sampson St from Colton to A.T.S.F. ℄

1.01	31.66		29.99 B.P.N.W. Cor Sampson & Main
2.05	25.47	9.18	22.42

Intersection of Colton and Sampson: Colton 80' - 14 Cbs 13' ets: Sampson = 6, 10' Cbs, 10' ats.

Yardage in YB. 12 pg 295 1-25-29 F.C.

N.L. Colton:

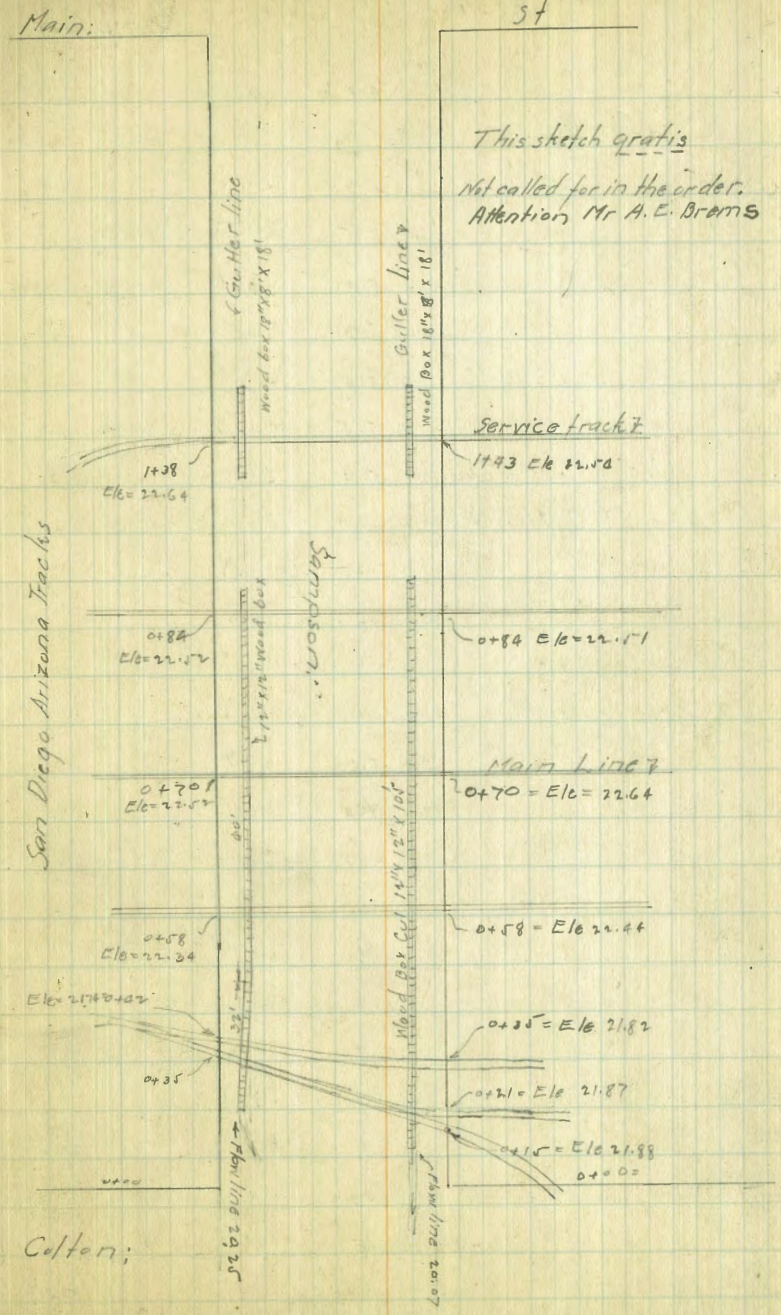
E.L.		4.1	21.4
cb		5.1	20.4
1/4		5.0	20.5
℄		4.6	20.9
1/4		5.0	20.5
cb		5.0	20.5
W.L.		4.2	21.3

N.C6 Colton

W.L.		4.7	20.8
cb		5.1	20.4
1/4		5.2	20.3
℄		5.0	20.5
1/4		5.3	20.2
cb		5.3	20.2
E.L.		5.1	20.4

N 1/4 Colton:

E.L.		5.3	20.2
cb		5.6	19.9
1/4		5.4	20.1
cb		5.3	20.2
1/4		5.2	20.3
cb		5.1	20.4



+	T 25.47	−	E/L:
			Sampson
W.L.		4.9	20.6
	℄ Colton:		
W.L.		4.9	20.6
cb		5.5	20.0
1/4		5.4	20.1
℄		5.3	20.2
1/2		5.4	20.1
cb		5.5	20.0
E.L.		5.4	20.1
	5 1/4 Colton:		
E.L.		5.2	20.3
cb		5.5	20.0
1/2		6.0	19.5
℄		6.0	19.5
1/2		5.1	20.4
cb		5.4	20.1
W.L.		4.7	20.8
	Scd Colton		
W.L.		4.9	20.6
cb.		4.9	20.6
1/4		4.9	20.6
℄		5.7	19.8
1/2		6.7	18.8
cb		6.3	19.2
E.L.		5.5	20.0

+	T 25.47	−	E/L
	S.L Colton = 0+00		
E.L.		5.7	19.8
cb		6.6	18.9
1/4		6.7	18.8
+8		6.4	19.1
℄		5.8	19.7
+4		5.1	20.4
1/4		5.0	20.5
cb		4.9	20.6
W.L.		5.0	20.0
	0+50		
W.L.		6.4	19.1
cb		6.3	19.2
1/4		6.3	19.2
℄		6.2	19.3
+3		7.3	18.2
1/4		7.4	18.1
cb		7.6	17.9
E.L.		7.1	18.4
	1+00		
E.L.		8.4	17.1
cb		8.5	17.0
1/4		8.0	17.5
+8		8.0	17.5
℄		6.3	19.2
+8		6.5	19.0
1/4		7.6	17.9

+	π 25.47	−	Sampson.
cb		7.4	18.1
W.L.		7.4	18.1
1+50 W.L.		8.0	17.0
1+50 W.L. = Elev on Sewer manhole Rim		8.24	17.23
" " " " Flow line Sewer		16.04	9.43
cb		8.6	16.9
1/4		8.0	17.0
+7		7.9	17.6
℄		9.1	16.4
1/4		9.3	16.2
cb		9.1	16.4
E.L.		9.0	16.5
2+00 E.L.		10.7	14.8
cb		11.0	14.0
1/4		12.2	13.3
+7		11.6	13.9
℄		9.2	16.3
1/4		10.0	15.5
cb		9.8	15.7
W.L.		9.6	15.9
#	1.90	10.22	15.15
2+50 W.L.	17.05	2.9	14.2
cb		2.5	14.6
1/4		2.7	14.4
℄		2.3	14.8
+2		4.1	13.0

+	π 17.05	−	Elev
1/4		4.4	12.7
cb		4.4	12.7
E.L.		3.9	13.2
3+01.8 – N.L. Railroad Ave on the east:			
Intersection Railroad Ave 80' 14' CBs 13' CRs:			
E.L.		4.7	12.4
cb		5.0	12.0
1/4		5.0	12.0
48		4.9	12.2
℄		3.2	13.9
1/4		3.7	13.4
cb		3.5	13.6
W.L.		3.3	13.8
North Curb of Railroad Ave			
W.L.		3.6	13.5
cb		3.7	13.4
1/4		3.9	13.2
℄		4.2	12.9
+3		5.1	12.0
1/4		5.1	12.0
cb		5.1	12.0
E.L.		4.4	12.7
N 1/4 of Railroad Ave:			
E.L.		4.8	12.3
cb		5.2	11.9
1/4		5.2	11.9

Sampson.

	+	π 17.0	−	Ele:
+8			5.2	11.9
℄			4.0	13.1
1/4			4.2	12.9
cb			4.0	13.1
W.L.			4.0	13.1
	℄ Railroad Ave			
W.L.			4.3	12.8
cb			4.3	12.8
1/4			4.1	13.0
℄			4.3	12.8
+3			5.4	11.7
1/4			5.4	11.7
cb			5.3	11.8
E.L.			4.9	12.2
	S 1/4 Railroad Ave:			
E.L.			4.9	12.2
cb			5.6	11.5
1/4			5.6	11.5
℄			5.6	11.5
+2			4.2	12.9
1/4			4.4	12.7
cb			4.5	12.6
W.L.			4.3	12.8
	S curb Railroad Ave:			
W.L.			4.7	12.4
cb			4.8	12.3

	+	π 17.0	−	Ele
1/4			4.8	12.3
+8			4.9	12.2
℄			5.9	11.2
1/4			5.8	11.3
cb			5.8	11.3
E.L.			5.4	11.7
0+00 = S.L Railroad Ave on the east:				
E.L.			5.8	11.3
cb			6.0	11.1
1/4			6.0	11.1
℄			6.0	11.1
+2			4.6	12.5
1/4			5.0	12.1
cb			5.0	12.1
W.L.			4.9	12.2
0+50 W.L.			6.0	11.1
cb			5.9	11.2
1/4			5.7	11.4
℄			6.0	11.1
1/4			6.3	10.8
cb			6.3	10.8
E.L.			6.3	10.8
1+00 E.L.			6.2	10.9
cb			6.3	10.8
1/4			6.4	10.7
℄			6.6	10.5

	+	π	−	Elc.
		17.05		Sampson:
℄			7.1	10.0
cb			6.7	10.4
W.L.			6.9	10.2
1+32 W.L.	Top cut		8.5	8.6
cb			10.3	6.8
℄			8.4	8.7
+7			8.0	9.1
℄			5.4	11.7
℄			4.8	12.3
+6			4.8	12.3
+7			11.8	5.3
+9			11.8	5.3
cb			5.0	12.1
E.L.			5.2	11.9
#	3.88	17.28	8.65	8.40 On Track
E.L.			5.7	6.6

1+38 = ditch & turn cut; on gutter line; culvert under A.T. & S.F. R.R. Timber 2'x3'x26' opening 16' N of ℄ of tracks.

cb			7.85	4.4
℄			5.5	6.8
℄			6.7	5.7
℄			6.7	5.7
℄			6.4	5.9
cb			6.0	6.3
W.L.			5.9	6.4

1+44 on A.T. & S.F. Roadbed:

W.L.			4.85	7.8

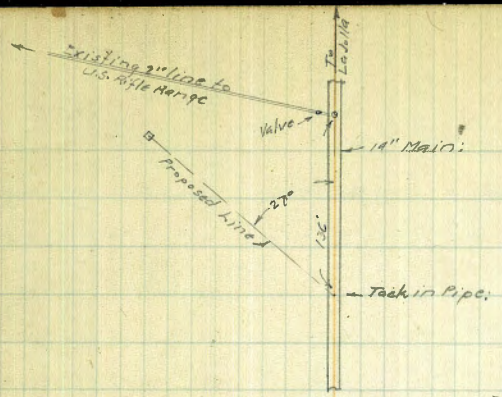
	+	π	−	Elc.
		12.28		
cb			4.4	7.9
℄			4.2	8.1
℄			4.6	7.7
℄			4.4	7.9
cb			4.85	7.8
S.L.			4.7	7.6

1+48.7 ± = ℄ A.T. & S.F. R.R.

#	9.82	18.22	3.88	9.40 Rail
#	9.22	25.44	1.00	17.22
#	9.41	31.92	2.93	22.51
			1.95	29.97 = 29.99 initial BM

Note: this improvement should not go beyond the A.T. & S.F. ℄

	Rt.	Lt.
19+90		34° 40'
17+80		18° 30'
15+32		26° 10'
12+40		15° 55'
9+35	30° 0'	
4+20		46° 10'
2+40		29° 20'
0+00 Tack Pipe		27° 0'



El assumed.

U.S. Rifle Range Pipe Line

Sep 6-1927

Pennan Flood Bichet

	+	⊼	−	El	
	11.58	111.58		100.00 Assumed Top of main See Page 1.	
0+00 Top of main at takeoff			6.93	104.65	102.00
1			4.7	106.9	+4.0 102.90
2			5.9	105.7	+2.9 102.80
2+40 Δ Lt			6.7.9	104.79	+2.0 hub: 102.76
3			5.9	105.7	+3.0 102.70
4			7.0	104.6	+2.0 102.60
# 4+20 Δ Lt	6.68	111.35	6.91	104.67	102.58 hub: +2.1
5			5.1	106.3	+3.8 102.50
6			4.8	106.6	+4.2 102.40
7			5.4	106.0	+3.7 102.30
8			4.8	106.6	+4.4 102.20
9			4.6	106.8	+4.7 102.10
9+35 Δ Rt	8.38	119.60	4.13	107.22	+5.16 hub: 102.06
10			6.4	109.2	+7.2 102.00
10+03 = Edge pavement			6.37	109.23	+7.23 102.00
10+37 = " "			5.64	109.96	+8.0 101.96
11			5.0	110.6	+8.7 101.90
11+75 ± Hog canyon Road:			3.6	117.0	+10.2 101.82
12			5.4	110.2	+8.4 101.80
# 12+40 Δ Lt	1.38	110.00	6.98	108.62	+6.86 hub: 101.76
13			3.4	106.6	+4.9 101.70
13+40 Break					101.66
14			8.6	101.40	100.26 +1.1
15			11.0	88.00	97.93 +1.1
# 15+92 Δ Lt	2.21	102.01	10.20	99.80	Stake +1.46
			4.76	97.25	95.79

	+	⊼	−	El	
		102.01			25
16			5.1	96.9	95.60 +1.3
17			5.7	96.8	95.40 +1.4
# 17+80 Δ Lt	6.76	102.60	6.17	95.84 hub	95.24 +0.60
18			6.8	95.8	95.20 +0.6
19			5.1	97.0	95.00 +2.0
19+90 Δ Lt	4.62	100.49	6.73	95.87 hub	94.82 +1.05
20			4.2	96.1	94.80 +1.3
21			3.6	96.9	94.59 +2.3
22			4.6	95.9	94.38 +1.0
23			4.9	95.6	94.17 +1.4
24			5.9	94.6	93.96 +0.6
# 24 +50	4.87	100.08	5.28	95.21	
25			5.0	95.1	93.86 +1.2
25 +35			3.6	96.5	93.76 +2.7
			4.7	95.4	93.68 +1.7
25+75 end Line at tanks			4.75	95.3	hub: 93.60 +1.73
26			2.20	97.38 Nail Pole:	
13 Hom of intake pipe to tank			6.20	93.88	

Book 1034

Location of Hog Canyon or La Jolla Canyon Drive Road Dennan, Flood. Bichet

Sep 1927.

44+66.27 P.T.

43+16.06 P.I. R=1400' Δ 12°24' Lt E=8.23' T=152.08' L=302.99'

41+63.98 P.C.

40+42.49 P.O.T.

39+94.19 P.O.T.

30+00 P.O.T.

22+00 P.O.T.

16+73.06 P.O.T.

7+00 P.O.T.

2+52.63 P.T.

6 Chords 50.48'

1° 2'
2° 4'
3° 6'
4° 8'
5° 10'
6° 12'

44+16.47
43+65.97
43+15.48
42+64.98
42+14.48

P.I. Δ 9°39' Rt. E 5.12 R=1500' T=126.40 L=252.63

Power P. Con pavement no tack

60-43-30
60 43 30/0
121-27-0
2/121-26
60-44

50' 40'

40' 1001

2411 73°57' 32.5 285 Found Hub book 1034 PGG

40' 88°52 40

30' 40'

40' 40'

Power pole Cop tack: 53.03' Found pine Hub. 28.78' Tel Pole cop tack See Book 1034 Page 66

13.10' 24'

45.0

60° Ht

To San Diego

Tack. & pavement.

58.85'

Tack. 36.76'

See Book 1024 Page 66

Curve

Curve

12'

Tack pavement End curve existing Pavement.

Hog Canyon.

60+20 25 P.C.C.

1 Chord of 14.48' = d of 2° 11' 00"

R=190'
Δ=41° 0'
T=71.04'
L=135.96'

2 Chords of 50'

d= 7° 33' 40"
? 15° 7' 20"
21° 0' 00"

59+34 44
59+84 59
60+20 25

59+55 83 P.I. Rt 41°00'

58+84 29 R.C.C.

7 Chords 50.98'

2° 51' 9"
5 42 18
8 33 27
11 24 36
14 15 45
17° 06 54
19° 58' 00"

55+79 51
56+30.31
56+81 10
57+31 90
57+82 70
58+33 49
58+84 29

57+14 96 P.I Δ Rt 39°56'
R=510.18'
T=185.35'
L=355.58'

55+28 21 P.C

55+00 P.O.T.

52+17

P.T. 51+40 41

50+82 82
50+28 22
49+67 63

50+28 33 P.I 6°0' Lt.
R=2200
T=110.30
E=3.01
L=220.38'

4 chords 57.59'
0° 45'
1° 30'
2° 15'
3° 00'

49+10 03 P.C.

49+00 P.O.T

88' 35' on slope.

40°45'

65' 46 along slope.

47.7

35°

on S.T.

44°45 32.8'

30' Cor Cut

Nail.

50' 77' along slope.

42.7'

Nail.

18' Cor Cut.

36°26 38'

50' 40'

50' on slope of ground. 50'

70+61.84 P.C.

72+28.00

71+00.87 P.T.

6 chords of 53.08'

d = 5° 4' 30" = 68+35.10
10 9 00 = 68+88.25
15 13 30 = 69+41.44
20 18 00 = 69+94.58
25 22 30 = 70+47.73
30 27 00 = 71+00.87

P.I 69+58.36 Δ 60°54' Lt.
R = 200'
T = 176.36'
E = 48.00

68+14.2 on S.T.

67+82.00 P.C.

64+20.19 P.T.

Δ = 29°24'
R = 200'
T = 78.70'
E = 10.15'
L = 153.94'

3 chords of 51.25'

d = 4° 54' = 64+17.05
" = 9° 48' = 64+68.87
" = 14° 42' = 64+20.19

64+44.95 P.I Δ 29°24' Lt.

64+26.85 on S.T.

P.C. 62+66.29 Lt P.C.

P.T. = 62+35.29

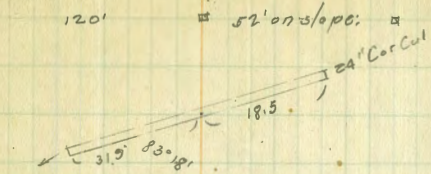
Δ = 16°10'
R = 761.98'
T = 108.27'
L = 215.00

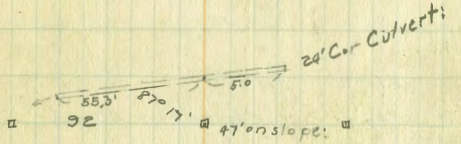
4 chords of 53.74

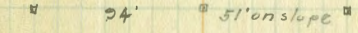
d = 2° 1' 10" = 60+74.00
4° 2' 30 = 61+27.74
6° 3' 45" = 61+81.50
8° 5' 00 = 62+35.29

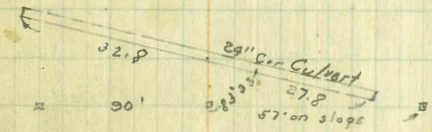
P.I. 61+28.47 Δ R.t. 16°10'

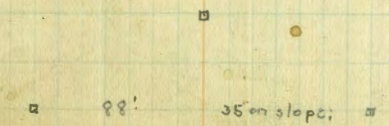
60+20.29 P.C.C.











Hog Canyon.

88+91.55 P.C. R1.

88+11.56

81+34.45 P.T.

30° 34'

P.I 80+17.35 Δ R+ 30°44'
R= 450'
T= 122.97'
E= 16.50'
L= 240.07'

6 Chords of 40.00'

d= 2° 32' 50" = 79+34.39
" = 5° 05' 40" = 79+74.40
" = 7° 38' 30" = 80+14.21
" = 10 11' 20" = 80+54.43
" 12 44 10" = 80+94.44
" 15 17 00" = 81+34.45

~~P.E.~~ 78+94.08 P.C.

78+65.29

78+06.19 P.T.

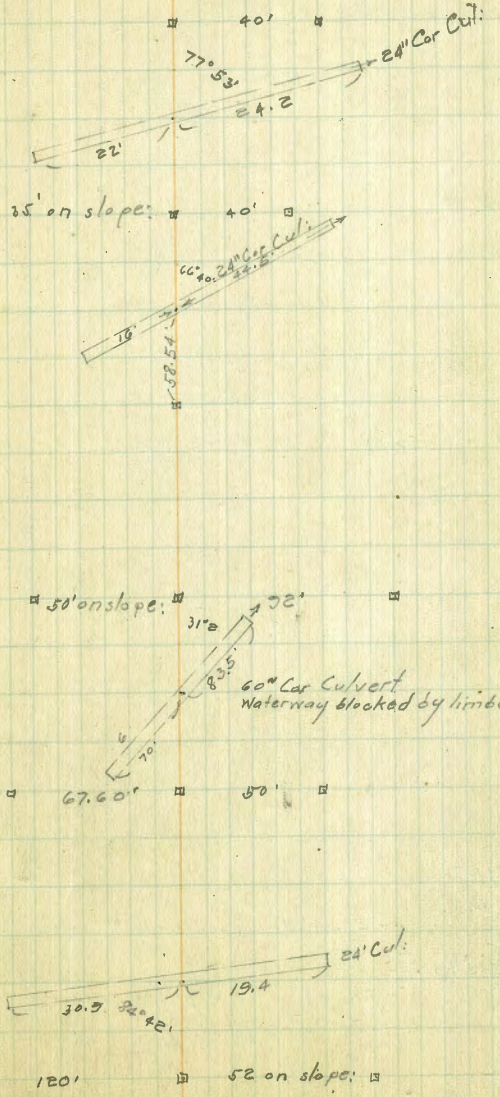
5 Chords of 48.84'

76+87.96 P.I Δ 35° 00' Lt.
R= 400'
T= 126.12'
E= 19.41'
L= 244.35'

d= 3° 30' = 76+10.71
" 7° 00' = 76+59.58
" 10° 30' = 77+08.45
" 14° 00' = 77+57.32
" 17° 30' = 78+06.19

76+38.64 on S.T.

75+61.84 P.C.



102+76.16 PT.

Hog Canyon.

On St:

3 Chords of 50.10'

d = 1° 41' 20" = 99+75.87
" = 3° 22' 40" = 100+25.54
" = 5° 4' 00" = 100+75.66
" = 6° 45' 20" = 101+25.78
" = 8° 26' 40" = 101+75.91
" = 10° 08' 00" = 102+26.03
" = 11° 49' 30" = 102+76.16

101+03.26 P.I 23° 39' Rt.
R = 850'
E = 18.43'
T = 177.96'
L = 350.86'

99+36.30 on S.T.

99+25.30 R.C Rt

98+40.13 P.T.

6 chords of 43.68'

d = 4° 11' = 96+21.09
" = 8° 22' = 96+69.30
" = 12° 33' = 97+08.71
" = 16° 44' = 97+52.41
" = 20° 55' = 97+96.32
" = 25° 06' = 98+40.13

97+17.81 P.I. Δ Rt 50° 12'
R = 300'
T = 140.53'
E = 31.28'
L = 262.85'

96+30.10 on S.T.

95+77.28 R.C Rt.

90+46.80

P.T. 89+81.15

Δ = 2° 34 Rt
R = 2000'
E = 0.50'
L = 89.60
T = 44.80

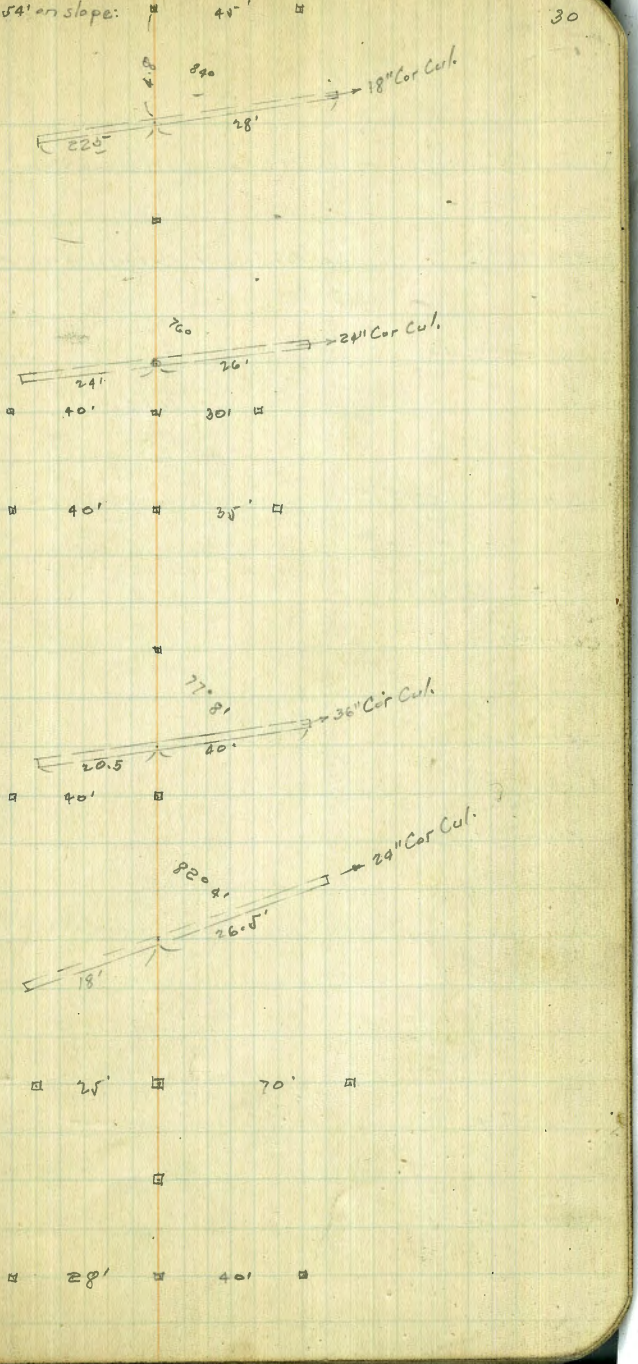
2 Chords of 44.80

d = 0° 38' 30" = 89+36.35
" = 1° 17' 00" = 89+81.15

P.I. 89+36.35 Rt

88+91.55 R.C

54' on slope:



131+08.85

~~130+58.5~~ Approximate P.C. of existing pavement

129+94.57

~~129+44.57~~ P.O.T. Nail in header board Eastedge of existing paving:

127+47.04

~~126+97.04~~ P.T.

C Chords of 46.85

	d = 1° 40' 48"	= 124+62.77
	" = 3° 21' 20"	= 125+09.63
	" = 5° 02' 00"	= 125+56.48
	" = 6° 42' 40"	= 126+03.33
	" = 8° 23' 20"	= 126+50.19
	" = 10° 04' 00"	= 126+97.04

126+07.34

~~125+57.34~~ P.I. 20° 8' Lt

R = 800'

T = 142.02'

L = 281.12'

E = 12.51'

124+65.97

~~124+10.97~~ P.C. Lt

123+47.1

~~122+97.1~~ P.O.T.

118+90.80

~~118+40.80~~ P.T.

8 Chords of 49.44'

	d = 1°	25' = 114+94.64
	" = 2°	50' = 115+44.09
	" = 4°	15' = 115+93.54
	" = 5°	40' = 116+42.98
	" = 7°	05' = 116+92.43
	" = 8°	30' = 117+41.89
	" = 9°	55' = 117+91.34
	" = 11°	20' = 118+40.80

116+95.61

~~116+45.61~~ P.I. 22° 40' Rt.

R = 1000

T = 200.42'

E = 19.89

L = 395.61'

114+95.19

~~114+45.19~~ P.C. Rt.

106+50

~~106+00~~

P.T. 102+76.16

+ chisel mark ± existing paving:

30' 40'

30' 38'

C&G 43.

27'

2 - 36" Con Pipes:

231

40' 40' 22'

30' 27'

50' C.

18" Cor Cul

25'

54" on slope: 45'

Hog Canyon:

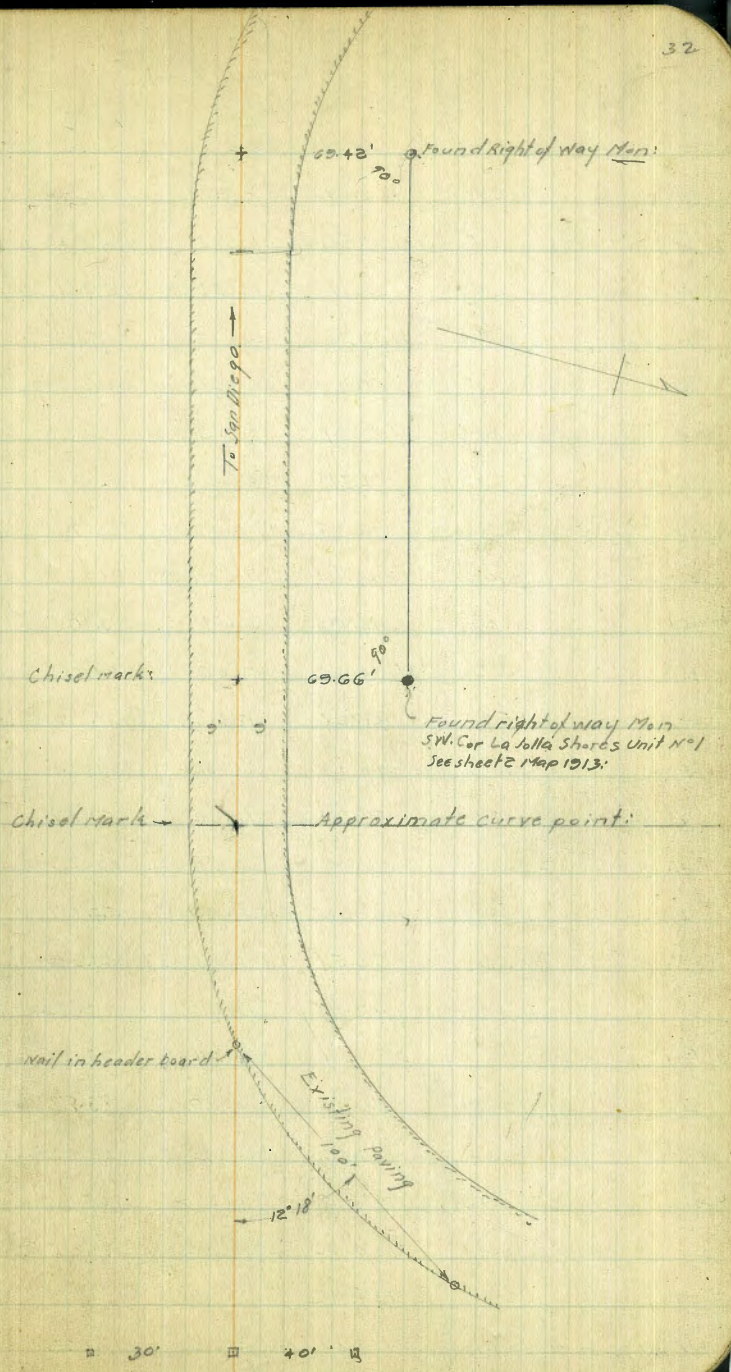
135+43.49

132+19.85 P.O.T.

130+58.85 P.O.T.

129+44.50 P.O.T.

126+37.04 P.T.



B.M. Line for Hog Canyon Road, or La Jolla Canyon Drive.

	+	π	−	Ele	
#	12.23	144.31		132.08	B.P. South
#	7.96	152.19	0.08	144.23	on North
#	0.18	139.52	12.85	139.34	on East
#	0.70	127.71	12.51	127.01	" West
#	1.40	116.66	12.45	115.26	" "
#	1.35	105.20	12.81	103.85	" "
#	0.49	93.69	12.00	93.20	" "
#	6.05	89.51	10.23	83.46	" "
#	12.30	99.28	2.53	86.96	" "
#	3.96	102.61	0.63	98.65	" N.W.
#	3.46	96.56	9.51	93.10	" West
#	1.23	90.33	7.46	89.10	Bent Nail
#	1.58	81.28	10.63	79.70	Nail in
#	0.18	70.13	11.33	69.95	" "
# ✓	0.87	58.34	12.66	57.47	" Spk
#	8.76	56.08	11.02	47.32	
#	5.37	61.06	0.39	55.69	
#	11.53	72.59	0.00	61.06	
#	11.42	83.95	0.06	72.53	
⊙			5.49	78.46	
#	12.77	96.64	0.08	83.87	
#	12.74	105.66	3.72	92.92	
#	12.70	118.08	0.28	105.38	
#	12.31	129.96	0.43	117.65	
#	12.85	137.43	5.38	124.58	
#	11.21	148.44	0.20	137.23	

Cor Prospect Place and Park Row. from official bench book.

curb Prospect Place: 1

x Torrey Pines Road. South of entrance to private road. 2

" " " " 75's of end curve: 3

" " " " North side of private driveway 4

walk at North Cor driveway to House No 1628 5

Curb Torrey Pines Road at South line of Cypress hedge-Capri: 6

" " " " 25' South of curb inlet 7

" " " " North cor of grated curb inlet 8

Cor of sidewalk at Hillside Drive: 9

edge of paving nail N/4 of Newport Terrace 10

W " " " South end of crack in pavement: 11

header board W side pavement opposite pole # 2280 12

" " " " " " brick house 13

in pole # 2350 Torrey Road and Calle Del Plata (La shores B.M. 57.115 christo) 14

40' Rt R.P. for 126+97.04 P.T. 15

Nail in top of North post of Rt guard fence for Cul at 122+97 16

Nail in peg 17' Lt 119+18 17

Nail in Road 116+00

30' Lt R.P. for 114+45.12 P.C. Rt 18

Rock 110+28 in Road: 5' Rt of ℄

Peg Rt of 106+20 at foot of embankment: 19

" " " 103 in field 20

Rock in Road 101+70

30' Rt 99+25.30 P.C. Rt: 21

Rt of 97+50 Nail in 4th post from S end of guard fence: 22

	+	π 148.44	−	Ele:	
#	10.79	158.74	0.49	147.95	
#	11.67	168.39	2.02	156.72	
#	12.10	180.29	0.20	168.19	
#	11.80	192.05	0.04	180.25	
#	12.57	204.52	0.10	191.95	
#	10.05	213.87	0.70	203.82	
⊙			3.97	209.90	
#	10.40	220.17	0.10	213.77	
#	12.74	236.42	0.49	223.68	
#	12.28	248.34	0.36	236.06	
#	12.35	260.58	0.11	248.23	
#	12.36	272.66	0.28	260.30	
#	11.40	283.34	0.77	271.94	
#	12.75	295.50	0.59	282.75	
#	10.87	305.97	0.35	295.10	
#	11.29	317.19	0.07	305.90	
#	11.91	328.59	0.51	316.68	
⊙			1.49	327.10	327.69 0.15 error
#	12.11	340.51	0.19	328.40	
#	11.28	351.64	0.15	340.36	
#	12.00	363.43	0.21	351.43	
⊙			4.60	358.83	
#	12.13	375.55	0.01	363.42	
#	7.94	383.11	0.38	375.17	
#	6.23	387.88	1.46	381.65	
#	9.04	396.15	0.77	387.11	

Lt of 94+15 second post from North end of guard fence 23

Rt of 90+00 Peg at toe of slope. 24

17' Lt 88+75 Peg; 25

Rock in Road 5' Rt 86+70

" " " 8' " 84+30

" " " 10' " 81+65

Rt of 80+65 Nail in top of post South end guard fence. 26

Lt of 79+05 " " side " " " " " " " 27

Peg in gutter Rt of 75+70 28

" " " " " 72+70 29

2nd post from N end, Lt 68+15 30

Peg on Lt edge fill 65+61 31

on center post of guard fence for Cul 64+26.85 Nail in top of 32

Nail in hard pan Rt gutter 61+00 33

Cen Post of guard fence for Cul: Appe 58+40 34

Peg in Rt gutter Sta 55+28.71 P.C. 35

" " " " " 53+00 36

Nail in top of cen pos guard fence for Cul at 52+17 37

Peg in Rt gutter 50+95 38

" " " " 48+85 39

" " " nail 46+40 40

50' E.R.P. for 94+66.97 P.T. 41

Nail in bottom of ditch Lt 43+20 42

Nail in south post of guard for cul Lt of 40+60 43

" " fence post Lt 35+70 44

" " " " " 31+37 45

	+	ℸ 396.14	−	Elc.
#	8.36	404.41	0.10	396.05
#	9.34	412.65	1.10	403.31
#	6.50	416.97	2.18	410.47
#	4.35	416.07	5.25	411.72
#	0.23	407.99	8.31	407.76
#	4.52	401.48	11.03	396.96
#			2.60	398.88
			7.04	394.84

Check to Davis B.M.

5.64	408.95		403.31 = 47 above:
2.89	401.03	10.81	398.14
0.02	393.48	7.56	393.47
3.45	384.41	12.53	380.96
		6.57	377.84 = 377.24 # Book 1011 Page 2

Check to Moores B.M at Princess and Spindrift

0.75			86.96 = 8# Page 33:
1.07	78.89	9.89	77.82
		9.78	69.11 = 69.06

Check to Gregory's B.M = 21 R.R. Page 53 Book 1034 = Elc 392.57

1.73	400.61		398.88 = 52# see above:
		7.36	393.25 = dif 0.68

Nail fence Post Lt 27+40	46
Stake Rt 22+15.	47
Nail pole # 20219 tie Rt 28.78 for P.O.T. 16+73.06	48
Nail fence Post Rt 10+70	49
" Cor " " Lt 5+05	50
3 nails in west post of No Shooting-sign	51
Nail in top of South end of East ground sill for water tank probably used as B.M. - Nail scribed around by circle; on pavement at cop tack marked 1# on page 36	52 53

Xsection of Hog Canyon Road

Denman Flood Bichet. Sep 1927

375.17 BM #3 Page 34

	+	T	−	
39+94 19 P.O.T.	3.64	378.81		
20 Rt Top of fill			3.0	375.8 ✓
℄			2.7	376.1 ✓
13 Lt			2.7	376.1
20 Lt. Top fill				
Intake flow Line	40+42 Cul		9.03	369.78
Outlet " "	41+00		9.93	368.88
23 Lt Top fill			5.1	373.7 ✓
13 Lt			4.1	374.7
℄			4.0	374.8 ✓
10 Rt			4.0	374.8
20 Rt top fill				✓
	41+63 98 P.C. #			
22 Rt gutter			5.5	373.3 ✓
10' Rt			5.1	373.7
℄			5.1	373.7 ✓
15 Lt			5.4	373.4
20 Lt Top fill			5.8	373.0 ✓
	42+14 48			
22 Lt Top of fill			7.2	371.6 ✓
15 Lt			7.1	371.7
℄			7.1	371.7 ✓
10 Rt			7.2	371.6
18 Rt Gutter			7.7	371.1 ✓
	42+64 98			

	+	T	−	E/E
		378.81		
18' Rt Gutter			10.2	368.6
8 Rt			9.6	369.2
℄			9.4	369.4 ✓
23 Lt Top fill			9.8	369.0 ✓
	43+15 48			
24 Lt Top fill			11.8	367.0 ✓
℄			12.0	366.8 ✓
16 Rt			11.9	366.9
16 Rt gutter			12.6	3662 ✓
# 1.26	367.68		12.57	366.24
	43+65 97			
23 Lt = Top fill			3.3	364.2 ✓
17 Lt			2.7	364.8
℄			2.9	364.6 ✓
17 Rt = Toe of cut			3.1	364.4 ✓
	44+16 47			
20 Rt Toe of cut			5.4	362.1 ✓
10 Rt			5.3	362.2
℄			5.0	362.5 ✓
23 Lt Top of fill			5.3	362.2 ✓
	44+66 97 P.T.			
25 Lt Top of fill			7.9	359.6 ✓
18 Lt			7.3	360.2
℄			7.3	360.2 ✓
13 Rt			7.7	359.8
24 Rt Bottom of Bank			7.1	360.4 ✓

	+	π 367.50	−	E/E	
		45+00			
20 Rt = Bottom of bank			8.5		359.0 ✓
13 Rt			9.2		358.3
℄			8.8		358.7 ✓
25 Lt Top of fill			9.7		357.8
		45+50			
24 Lt " " "			12.2		355.3 ✓
15 Lt			11.3		356.2
℄			11.2		356.3 ✓
5 Rt			11.2		356.3
20 Rt			12.1		355.4 ✓
30 Rt Borrow pit			11.8		355.7
#	0.78	355.49	12.79	354.71	
		46+00			
35 Rt in borrow pit			1.9		353.6
20 Rt			2.2		353.3 ✓
10 Rt			1.9		353.6
℄			1.6		353.9 ✓
15 Lt			1.7		353.8
25 Lt Top of fill			2.5		353.0 ✓
		46+50			
28 Lt Top of fill			4.9		350.6 ✓
15 Lt			3.8		351.7
℄			3.8		351.7 ✓
7 Rt			3.7		351.8
20 Rt			4.3		351.2 ✓

	+	π 355.49	−	
30 Rt in borrow pit			4.3	351.2
		47+00		
20 Rt in borrow pit			6.2	349.3
20 Rt			6.6	348.9 ✓
6 Rt			5.7	349.8
℄			5.9	349.6 ✓
15 Lt			6.0	349.5
22 Lt			6.8	348.7 ✓
28 Lt Top of fill			6.7	348.8
		47+50		
27 Lt Top of fill			9.2	346.3 ✓
15 Lt			8.2	347.3
℄			8.2	347.3 ✓
17 Rt can go out more than 30 by moving a little loose dirt			8.2	347.3
		48+00		
20 Rt			10.4	345.1 ✓
12 Rt			11.0	344.5
℄			10.6	344.9 ✓
14 Lt			10.5	345.0
22 Lt			11.2	344.3 ✓
26 Lt Top fill			10.7	344.8
#	0.34	343.59	12.24	343.25
		48+50		
25 Lt Top of fill			1.6	342.0 ✓
11 Lt			0.7	342.9
℄			1.0	342.6 ✓

	+	π 343.59	−	E/e
18 Rt			1.3	342.3 ✓
49+00				
20' Rt bottom of cut - Borrow pit West			3.7	339.9
10' Rt			3.3	340.3
℄			3.1	340.5 ✓
10 Lt			3.0	340.6
23 Lt Top of fill			3.9	339.7
49+10.03 P.C. Lt				
22 Lt Top of fill			4.3	339.3 ✓
10 Lt			3.4	340.2
℄			3.5	340.1 ✓
10 Rt			3.8	339.8
20 Rt bottom cut			4.1	339.5 ✓
49+67.63				
20 Rt bottom cut			6.7	336.9 ✓
℄			6.7	336.9 ✓
13 Lt			6.6	337.0
25 Lt Top of fill			7.2	336.4 ✓
50+25.22				
23 Lt Top of fill			10.8	332.8 ✓
10 Lt			9.8	333.8
℄			9.9	333.7 ✓
13 Rt			10.1	333.5
20 Rt bottom cut			10.9	332.7 ✓
#	0.44	331.12	12.91	330.68
50+82.82				

	+	π 331.12	−	E/e
20 Rt bottom cut			1.8	329.3 ✓
13 Rt			1.2 ✓	329.9
℄			1.1	330.0 ✓
10 Lt			1.0	330.1
18 Lt Top of fill			1.4	329.7 ✓
51+40.41 P.T.				
23 Lt Top of fill			4.8	326.3
10 Lt			4.5	326.6
℄			4.6	326.5 ✓
10 Rt			4.5	326.6
21 Rt bottom of cut			5.4	325.7 ✓
52+00				
22 Rt bottom cut			9.0	322.1 ✓
10 Rt			8.1	323.0
℄			8.0	323.1 ✓
10 Lt			8.3	322.8
22 Lt Top of fill			8.7	322.4 ✓
52+17 culvert				
flow line intake			10.92	320.20
" " outlet			14.72	316.40 316.40
52+50				
21 Lt Top fill			11.3	319.8 ✓
13 Lt			11.0	320.1
℄			10.7	320.4 ✓
8 Rt			10.8	320.3
20 Rt bottom Cut			11.8	319.3 ✓

	+	℄ 331.12	−	E/e
	1.01	319.68	12.45	318.67
		53+00		
20 Rt bottom cut			2.7	317.0 ✓
10 Rt			1.8	317.9
℄			1.7	318.0 ✓
10 Lt			2.2	317.5
25 Lt Top of fill			2.8	316.9 ✓
		53+50		
23 Lt Top of fill			5.0	314.7 ✓
12 Lt			4.4	315.3
℄			4.2	315.5 ✓
10 Rt			4.5	315.2
19 Rt bottom cut			5.2	314.5 ✓
		54+00		
20 Rt bottom cut			7.6	312.1 ✓
10 Rt			7.0	312.7
℄			6.8	312.9 ✓
10 Lt			6.9	312.8
22 Lt Top of fill			7.1	312.6 ✓
		54+50		
28 Lt Top of fill			9.4	310.3 ✓
15 Lt			9.9	309.8
10 Lt			9.4	310.3
℄			9.3	310.4 ✓
10 Rt			9.4	310.3
22 Rt Bottom of cut:			10.2	309.5 ✓

	+	℄ 319.68	−	E/e
		55+00		
25 Rt bottom of cut			12.9	306.8 ✓
15 Rt			11.8	307.9
℄			11.6	308.1 ✓
10 Lt			11.7	308.0
15 Lt			12.0	307.7 ✓
26 Lt Top of fill			11.2	308.5
#	0.71	308.14	12.25	307.43
		55+28 P.C Rt.		
23 Lt Top of fill			0.5	307.6 ✓
13 Lt			1.4	306.7
℄			1.3	306.8 ✓
15 Rt			1.4	306.7
23 R Bottom of cut			2.3	305.8 ✓
		55+79 51		
20 Rt Bottom cut			4.8	303.3 ✓
10 Rt			4.3	303.8
℄			3.7	304.4 ✓
7 Lt			3.4	304.5
15 Lt			3.9	304.2
18.6 Lt = end fence:				
24 Lt Top of fill			3.4	304.7 ✓
		56+20 31		
25 Lt = Top of fill			5.5	302.6 ✓
22 Lt = guard fence				
15 Lt			6.0	302.1

+	π 308.17	−	
9 Lt		5.7	302.4
℄		6.1	302.0 ✓
16 Rt	Bottom of cut.	6.8	301.6 ✓
	56+81.10		
16 Rt	Bottom of cut	9.2	298.9 ✓
℄		8.7	299.4 ✓
10 Lt		8.2	299.9
22.5 Lt to Guard fence			300.0 ✓
25 Lt Top of fill		8.1	
	57+31.90		
25 Lt Top of fill		10.5	297.6 ✓
18.5 Lt = Guard fence			
19 Lt		10.5	297.6
℄		10.8	297.3 ✓
15 Rt		11.5	296.6
23 Rt		12.0	296.1 ✓
	57+82.20		
25 Rt Bottom of cut		13.7	294.4 ✓
15 Rt		12.9	295.2
℄		12.3	295.8 ✓
10 Lt		12.1	296.0
17 Lt = Guard fence			
22 Lt = Top of fill		12.2	295.9
# 0.76	295.90	13.00	295.14
	58+33.49		
18 Rt = Bottom cut		2.6	293.3 ✓

+	π 295.90	−		40
℄		1.6		294.3 ✓
10 Lt		1.2		294.7
205 Lt = Guard fence				
23 Lt Top of fill		1.7		294.2 ✓
Flow line culvert (30") intake		7.27		288.63
" " " Outlet	See sketch	10.00		285.90
	58+84.29 P.C.C.			
29 Lt = Top of fill		2.8		293.1 ✓
24.5 Lt = guard fence				
10 Lt		2.6		293.3
℄		3.4		292.5 ✓
14 Rt Bottom of cut		4.3		291.6 ✓
# 0.23	295.37	0.76	295.14	
	59+34.44			
18 Rt bottom cut		4.7		290.7 ✓
13 Rt "		5.5		289.9
℄		4.5		290.9 ✓
8 Lt		3.9		291.5 ✓
24.5 Lt to guard fence				
27 Lt to Top of slope		3.3		292.1
	59+84.59			
24 Lt Top of slope		6.2		289.2 ✓
20 Lt to guard fence				
15 Lt		5.8		289.6
℄		6.6		288.8 ✓

+	π 295.37	−	Ele	
21 Rt bottom of cut:		7.4		288.0 ✓
60+20 25 PCC.				
20 Rt bottom of cut		9.0		286.4
℄		8.0		287.4 ✓
8 Lt		7.4		288.0
21 Lt fence				
24 Lt Top of fill		7.3		288.1 ✓
60+74				
22 Lt Top of fill		10.2		285.2 ✓
19 Lt guard fence				
8 Lt		9.9		285.5
℄		10.2 ✓		285.2 ✓
18 Rt bottom of cut:		11.3		284.1 ✓
# 0.19	282.93	12.62	282.74 = 282.75 = 33	
61+27 25				
19 Rt bottom of cut		1.5		281.4 ✓
℄		0.1		282.8 ✓
16 Lt guard fence		0.0		282.9
20 Lt Top of fill		0.3		282.6 ✓
61+81 50				
22 Lt Top of fill		2.2		280.7 ✓
17 Lt guard fence				
10 Lt		1.8		281.1
℄		2.2		280.7 ✓
17 Rt bottom of cut:		2.9		280.0 ✓
62+35 25 PT.				

+	π 282.93	−	Ele	41
Rx				
15 Lt Bottom of cut:		5.5		277.4 ✓
℄		4.8		278.1 ✓
10 Lt		4.2 ✓		278.7
22 Lt guard fence				
25 Lt Top of fill		4.2		278.7 ✓
63+00				
21 Lt Top of fill		8.3		274.6 ✓
18 Lt guard fence				
10 Lt		7.9		275.0
℄		8.1		274.8 ✓
10 Rt		8.3		274.6
19 Rt bottom of cut:		9.0		273.9 ✓
63+66 25 P.C Lt				
26 Rt Bottom of cut		12.3		270.6 ✓
20 Rt		11.8		271.1
℄		11.8		271.1 ✓
10 Lt		12.0		270.9
15 guard fence				
17 Lt Top of bank:		12.8		270.1
# 0.33	282.25	11.01	271.92 = T.B 32 = 271.94	
64+17 66				
30 Rt guard fence for Cul Line of cut 35 Rt		4.8		268.1 ✓
10 Rt		3.4		268.9
℄		4.0		268.3 ✓
15 Lt at guard fence for cul		4.3		268.0
18 Lt Top of bank:		5.0		267.3 ✓

+	ℸ	−	Elc	
	272.25			
Flow line 24" Cul intake:		8.87		263.38
" " " " Outlet		11.41		260.84
	64+68.87			
20 Lt Top of fill		6.9		265.4 ✓
16 Lt guard fence				
12 Lt		6.4		265.9
℄		6.6		265.7 ✓
10 Rt		6.0		266.3
24 Rt bott of cut		6.6		265.7 ✓
65+00 end of guard fence				
	65+20.19 Pt.			
17 Rt bottom of cut		9.7		262.6 ✓
7 Rt		8.9		263.4
℄		8.9		263.4 ✓
12 Lt		9.1		263.2
21 Lt Top of fill,		10.4		261.9 ✓
	65+50			
23 Lt Top of fill		11.7		260.6 ✓
10 Lt		10.5		261.8
℄		10.5		261.8 ✓
10 Rt		10.8		261.5
20 Rt bottom of cut		11.2		261.1 ✓
#	0.40 260.68	11.97	260.28	
	66+00			
17 Rt bottom of cut.		1.8		258.9 ✓

+	ℸ 260.68	−	Elc	
8 Rt		1.4		259.3
℄		1.1		259.6 ✓
12 Lt		0.9		259.8
24 Lt Top of bank:		1.4		259.3 ✓
	66+50			
26 Lt Top of fill		4.0		256.7 ✓
12 Lt		3.2		257.5
℄		3.3		257.4 ✓
15 Rt Bottom of cut		3.7		258.0 ✓
	67+00			
15 Rt bottom of cut		5.7		255.0 ✓
℄		5.6		255.1 ✓
13 Lt		5.7		255.0
25 Lt Top of slope		6.7		254.0 ✓
	67+82 P.C			
26 Lt Top of slope		10.4		250.3 ✓
15 Lt		9.9		250.8
℄		9.9		250.8 ✓
8 Rt		9.7		251.0
17 Rt bottom of cut:		10.2		250.5 ✓
#	0.06 248.28	12.46	248.22	= T.P. #30 = 248.23
68+12 guard fence commences:				
	68+35 N			
20 Rt Bottom of cut		0.9		247.3 ✓
10 Rt		0.2		248.1
℄		0.4		247.9 ✓

+	π 248.28	−	Ele
13 Lt		0.5	247.8
22 Lt = guard fence		1.1	247.2 ✓
25 Lt Top of slope		1.1	247.2
68+88.29			
20 Lt Top of bank:		4.2	244.1 ✓
17 Lt = guard fence			
10 Lt		3.4	244.9
℄		3.1	245.2 ✓
10 Rt		2.6	245.7
20 Rt		2.7	245.6 ✓
28 Rt Bottom of cut		3.6	244.7
Intake flowline 20" Cul		7.47	240.81
Outlet " " " "		10.84	237.44
69+44.44			
28 Rt bottom of cut		5.4	242.9 ✓
22 Rt		5.9	242.4
15 Rt		4.8	243.5
℄		5.2	243.1 ✓
14 Lt to guard fence		6.1	242.2
17 Lt Top of slope;		6.6	241.7 ✓
69+94.58			
20 Lt Top of slope		7.6	240.7
16 Lt guard fence:			
℄		6.9	241.4 ✓
11 Rt		6.2	242.1
18 Rt		6.6	241.7 ✓
24 Rt bottom of cut		7.9	240.4

+	π 248.28	−	Ele
70+47.58 = End of fence			
70+97.73			
22 Rt Bottom of cut		9.0	239.3 ✓
13 Rt		8.0	240.3
℄		8.4	239.9 ✓
19.5 Lt Line of fence			
22 Lt Top of fill		9.1	239.2
71+00.87 P.T.			
20 Lt Top of bank		10.8	237.5 ✓
12 Lt		10.3	238.0
℄		9.9	238.4 ✓
10 Rt		9.8	238.5
23 Rt Bottom of cut		10.8	237.5 ✓
71+50			
25 Rt Bottom of cut		11.8	236.5 ✓
10 Rt		10.8	237.5
℄		10.9	237.4 ✓
10 Lt		11.3	237.0
21 Lt Top of fill		11.9	236.4 ✓
# 1.35 237.39		12.24	236.04 − 29 = 236.06
72+00			
24 Lt top of fill		2.1	235.3 ✓
10 Lt		1.4	236.0
℄		1.2	236.2 ✓
10 Rt		1.3	236.1
20 Rt Bot. of cut		2.0	235.4 ✓

+	⊼ 237.39	−	Elc	
	72+50			
20 Rt	Bottom of cut:	2.2		235.2 ✓
17 Rt		3.1		234.3
10 Rt		2.7		234.7
℄		2.3		235.1 ✓
12 Lt		2.5⁻		234.9
24 Lt	Top of fill	3.3		234.1 ✓
	73+00			
26 Lt	Top of fill	4.5⁻		232.9 ✓
13 Lt		3.8		233.6
℄		3.8		233.6 ✓
10 Rt		4.2		233.2
16 Rt	Bottom of cut:	4.8		232.6 ✓
	73+28 24" Cul			
Elec line intake:		8.34		229.05
" "	Outlet,	10.95		226.44
	73+50			
15 Rt	Bottom of cut	6.1		231.3 ✓
8 Rt		5.7		231.7
℄		5.3		232.1 ✓
12 Lt		5.4		232.0
27 Lt	Top of fill	5.7		231.7 ✓
	74+00			
28 Lt	Top of fill	7.8		229.6 ✓
13 Lt		7.2		230.2

Keep away from this fill with Location: It's not even a 1 to 1 slope; and a stranger of wash.

+	⊼ 237.39	−	Elc	
℄		7.1		230.3 ✓
9 Rt	edge of diving	7.4		230.0
12 Rt		7.7		229.7
17 Rt	Bottom of cut	6.8		230.6 ✓
	74+50			
18 Rt	Bottom of cut	8.5		228.9 ✓
15 Rt		9.7		227.7
9 Rt		9.0		228.4
℄		8.6		228.8 ✓
13 Lt		8.8		228.6
25 Lt	Top of fill	9.4		228.0 ✓
	75+00			
23 Lt	Top of fill	10.5⁻		226.9 ✓
13 Lt		10.4		227.0
℄		10.3		227.1 ✓
15 Rt		11.2		226.2
20 Rt	Bottom of cut:	10.2		227.2 ✓
	75+50			
21 Rt	Bottom of cut	12.3		225.1 ✓
25 Rt		13.2		224.2
10 Rt		12.6		224.8
℄		12.2		225.2 ✓
13 Lt		12.4		225.0
22 Lt	Top of fill	13.0		224.4 ✓
#	0.51	225.05⁻	12.85⁻	224.5⁻4
	75+61.84 P.C.			

	+	⊼ 237.39	−	Ele
		72+50		
20 Rt	Bottom of cut:		2.2	235.2 ✓
17 Rt			3.1	234.3
10 Rt			2.7	234.7
℄			2.3	235.1 ✓
12 Lt			2.5	234.9
24 Lt	Top of fill		3.3	234.1 ✓
		73+00		
26 Lt	Top of fill		4.5	232.9 ✓
13 Lt			3.8	233.6
℄			3.8	233.6
10 Rt			4.2	233.2
16 Rt	Bottom of cut:		4.8	232.6 ✓
	73+28 24" Cul			
Flume line intake:			8.34	229.05
" "	Outlet,		10.95	226.44
		73+50		
15 Rt	Bottom of cut		6.1	231.3 ✓
8 Rt			5.7	231.7
℄			5.3	232.1 ✓
12 Lt			5.4	232.0
27 Lt	Top of fill		5.7	231.7 ✓
		74+00		
28 Lt	Top of fill		7.8	229.6 ✓
13 Lt			7.2	230.2

Keep away from this fill with Location. It is not even a fair slope, and a danger of wash.

	+	⊼ 237.39	−	Ele
℄			7.1	230.3 ✓
9 Rt	edge of diving		7.4	230.0
12 Rt			7.7	229.7
17 Rt	Bottom of cut		6.8	230.6 ✓
		74+50		
18 Rt	Bottom of cut		8.5	228.9 ✓
14 Rt			9.7	227.7
9 Rt			9.0	228.4
℄			8.6	228.8 ✓
13 Lt			8.8	228.6
25 Lt	Top of fill		9.4	228.0 ✓
		75+00		
23 Lt	Top of fill		10.5	226.9 ✓
13 Lt			10.4	227.0
℄			10.3	227.1 ✓
15 Rt			11.2	226.2
20 Rt	Bottom of cut:		10.2	227.2 ✓
		75+50		
21 Rt	Bottom of cut		12.3	225.1 ✓
25 Rt			13.2	224.2
10 Rt			12.6	224.8
℄			12.2	225.2 ✓
13 Lt			12.4	225.0
22 Lt	Top of fill		13.0	224.4 ✓
#	0.51	225.05	12.85	224.54
		75+61.84 P.C.		

	+	π 225.05	−	Elev
22 Lt Top of slope			0.8	224.2
℄			0.3	224.7
9 Rt			0.7	224.3
15 Rt			1.3	223.7
22 Rt Bottom of cut: 76+10.71 P.O.C. ~~76+70.71 P.C.~~			0.4	224.6
23 Rt bottom of cut			2.1	222.5
19 Rt			3.2	221.8
8 Rt			2.2	222.8
℄			2.3	222.7
10 Lt			2.6	222.4
20 Lt Top of slope			3.2	221.81
Inlet flow line 24" Cul.			7.31	217.74
Outlet " " " " 76+59.58 P.O.C. ~~76+10.71~~ this section in through cut			9.18	215.87
18 Lt Top of cut			3.5	221.5
12 Lt Bottom of cut			9.5	220.5
℄			9.4	220.6
10 Rt			2.9	222.1
26 Rt Bottom of cut:			4.3	220.7
76+84 Fence starts on Lt; Appe 10 Lt of ℄				
77+08 45 P.O.C. this section in through cut;				
26 Rt to bottom of bank			6.3	218.7
10 Rt			5.6	219.4
℄			6.0	219.0
13 Lt to fence				

	+	π 225.05	−	Elev
15 Lt to bottom of cut			6.1	218.9
16 Lt to top of cut			4.3	220.7
20 Lt " " " "			4.9	220.1
At 77+35 on Rt guard fence begins: 20' from ℄				
77+57 32 P.O.C.				
17 Lt Top of fill			7.5	217.5
145 Lt guard fence				
℄			7.0	217.5
10 Rt			7.1	217.9
19 Rt guard fence			7.0	217.5
25 Rt			8.1	216.9
30 Rt Bottom of cut			7.5	217.5
78+06 19 P.T.				
30 Rt in old Road			9.0	216.0
20 Rt			9.0	216.0
18 Rt guard fence			8.6	216.4
4 Rt			8.7	216.3
℄			9.0	216.0
15 5 Lt guard fence and top of fill			9.5	215.5
78+65 29=60" Cor Cul				
Flow line inlet of cul			25.20	199.85
" " outlet " "			36.0	189.05
78+99 38 P.T Rt:				
25 Lt bottom of cut			12.1	212.9
19 Lt guard fence			12.2	212.8
10 Lt			12.0	213.0

+	T 225.05	−	E/E	
℄		12.5		212.5 ✓
14 Rt guard fence		12.8		212.2
20 Rt Top of fill		13.2		211.8 V
#	0.10	213.86	11.29	213.76 - TP 17 = 213.77
79+05 = End of fence on Lt.				
79+34.39				
17 Rt Top of fill		3.7		210.2 ✓
13.5 Rt guard fence		3.1		210.8
℄		2.6		211.3 ✓
12 Lt		2.1		211.8
24 Lt bottom of cut		3.0		210.9 ✓
79+79.90				
21 Lt Bottom of cut.		4.2		209.7 ✓
6 Lt		3.4		210.5
℄		3.8		210.1 ✓
16 Rt = Guard fence				
20 Rt Top of slope		4.4		209.5 ✓
80+14.41				
25 Rt Top of slope		5.2		208.7
18 Rt Guard fence:				
10 Rt		5.1		208.8
℄		4.9		209.0 ✓
6 Lt		4.6		209.3
19 Lt Bottom of cut		5.2		208.7
80+54.92 Thru cut:				
17 Lt Bottom of cut		6.0		207.9 ✓

+	T 213.86	−	E/E	
6 Lt		5.8		208.1
℄		6.1		207.8 ✓
10 Rt		6.3		207.6
19 Rt guard fence				
22 Rt Bottom of cut		6.4		207.5 ✓
23 Rt Top of cut		5.1		208.8
80+67 end of fence on Rt				
Flow line 24" Cor Cul inlet		10.10		203.76
" " " " " Outlet		14.21		199.65
80+94.43 Thru cut:				
25 Rt Top of cut		6.5		207.4
21 Rt Bottom of cut		8.0		205.9 ✓
10 Rt		7.7		206.2
℄		7.4		206.5 ✓
7 Lt		7.2		206.7
17 Lt Bottom of cut:		8.2		205.7 ✓
81+34.95 Rt. Thru cut:				
18 Lt Bottom of cut		9.2		204.7 ✓
7 Lt		8.0		205.4
℄		8.8		205.1 ✓
12 Rt		9.0		204.9
20 Rt bottom of cut		9.5		204.4 ✓
24' Rt Top of cut:		7.4		206.5
82+00				
23 Rt Top of cut		11.1		202.8
18 Rt Bottom of cut		12.0		201.9 ✓

+		213.86	−		
10 Rt			11.4		202.5
℄			11.2		202.7 ✓
10 Lt			11.0		202.9
18 Lt to bottom of cut.			11.8		202.1 ✓
#	0.55	201.71	12.70	201.16	
		83+00 Thru Cut.			
19 Lt Bottom cut			3.7		198.0 ✓
10 Lt			3.0		198.7
℄			3.1		198.6 ✓
12 Rt			2.2		199.5
20 Rt Bottom of cut			3.8		197.9 ✓
27 Rt Top of cut:			+1.0		202.7
		84+00 Thru cut			
22 Rt Top of cut			8.9		192.8
20 Rt Bottom of cut			9.4		192.3 ✓
10 Rt			8.1		193.6
℄			8.0		193.7 ✓
10 Lt			8.1		193.6
20 Lt Bottom of cut:			8.9		192.8 ✓
#	1.11	190.25	12.57	189.14	
		85+00 Thru cut.			
20 Lt Bottom of cut			2.3		187.9 ✓
10 Lt			1.7		188.5
℄			1.6		188.6 ✓
11 Rt			1.9		188.3
20 Rt Bottom of cut			2.4		187.8 ✓

+		190.25	−		Elc	47
26 Rt Top of cut.			+1.6		191.8	
		86+00 Thru cut:				
25 Rt Top of cut.			4.6		185.6	
19 Rt Bottom of cut			7.2		183.0 ✓	
12 Rt			6.7		183.5	
℄			6.4		183.8 ✓	
10 Lt			6.4		183.8	
19 Lt Bottom of cut			7.0		183.2 ✓	
#	0.68	180.91	10.02	180.23 = 180.25 T.P. Rock:		
		87+00				
19 Lt Bottom of cut			2.8		178.1 ✓	
10 Lt			2.0		178.9	
℄			2.0		178.9 ✓	
10 Rt			2.1		178.8	
18 Rt Top of fill			2.8		178.1 ✓	
		88+00				
15 Rt Top of fill			8.6		172.3 ✓	
12 Rt			7.8		173.1	
℄			7.9		173.0 ✓	
10 Lt			7.7		173.2	
18 Lt edge Road			8.8		172.1 ✓	
88+11.56 = 24" intake E.L.			12.50		168.41	
Outlet "			14.47		166.44	
#	0.61	168.78	12.74	168.17 = T.P. # 25 = 168.19		
		88+91.5 P.C. Rt.				
18 Lt Bottom of cut			1.4		167.4 ✓	

+	℄ 168.78	−	Elc
9 Lt		0.5	168.3
℄		0.6	168.2 ✓
12 Rt		1.1	167.7
20 Rt Top of fill		2.0	166.8 ✓
89+36 30			
20 Rt Top of fill		4.6	164.2 ✓
15 Rt		3.7	165.1
℄		3.2	165.6 ✓
8 Lt		3.2	165.6
17 Lt Bottom of cut		4.3	164.5 ✓
89+81 15 P.T.			
18 Lt Bottom of cut		6.9	161.9 ✓
7 Lt		6.4	163.4
℄		5.3	163.5 ✓
18 Rt Top of bank:		5.8	163.0 ✓
90+00			
20 Rt Top of bank:		7.4	161.4 ✓
18 Rt		6.7	162.1
℄		6.3	162.5 ✓
8 Lt		6.3	162.5
18 Lt Bottom of cut.		7.5	161.3 ✓
90+46 80			
Flow line intake 24" Cul		12.34	156.44
" " Outlet " "		14.58	154.20
# 1.16	157.86	12.08	156.70 = 24" = 156.72
91+00			

+	℄ 157.86	−	Elc.
17 Lt Bottom of cut		0.2	157.7 ✓
8 Lt		+0.2	158.1
℄		+0.1	158.0 ✓
11 Rt		0.0	157.9
20 Rt Top of fill		0.9	157.0 ✓
92+00			
20 Rt Top of fill		5.0	152.9 ✓
13 Rt		3.7	154.2
℄		3.3	154.6 ✓
10 Lt		3.0	154.9
17 Lt Bottom of cut:		3.6	154.3 ✓
93+00			
19 Lt Bottom of cut		7.3	150.6 ✓
10 Lt		6.8	151.1
℄		7.1	150.8 ✓
10 Rt		7.3	150.6
18 Rt Top of fill		8.1	149.8 ✓
94+00			
20 Rt Top of fill		11.5	146.4 ✓
10 Rt		10.2	147.7
℄		9.9	148.0 ✓
10 Lt		9.9	148.0
19 Lt Bottom of cut:		10.8	148.1 ✓
# 0.68	148.64	9.90	147.96 = T.P. 23 = 147.95
194+08 begins fence 16' Lt			
95+00			

+	π 148.64	−	E/e
17 Lt Top of fill		3.1	145.5
15 Lt guard fence		2.2	146.4
℄		2.7	145.9 ✓
10 Rt		3.0	145.6
20 Rt Top of fill		4.3	144.3 ✓
95+77.38 PC Rt			
21 Rt Top of fill		5.5	143.1 ✓
10 Rt		5.0	143.6
℄		4.4	144.2 ✓
19 Lt guard fence		3.7	144.9
16 Lt Top of fill		3.9	144.7 ✓
95+91 on Rt guard fence begins; 19' Rt.			
96+21.09			
17 Lt Top of fill		6.8	141.8 ✓
15 Lt guard fence		4.4	144.2
℄		5.3	143.4 ✓
10 Rt		6.1	142.5
18 Rt guard fence			
20 Rt Top of fill		7.0	141.6 ✓
96+64.98			
18 Rt Top of fill		8.3	140.3 ✓
15 Rt guard fence		7.8	140.8
7 Rt		7.7	140.9
℄		6.9	141.7 ✓
10 Lt		6.2	142.4
20 Lt guard fence Top of 2' fill		5.8	142.8 ✓
96+84 end of fence on Lt			

+	π 148.64	−	E/e
97+08.71			
22 Lt bottom of cut		8.3	140.3 ✓
17 Lt		7.7	140.9
10 Lt		7.9	140.7
℄		8.4	140.2 ✓
5 Rt		9.3	139.3
15 Rt fence		9.8	138.8
19 Rt Top of fill		10.3	138.3 ✓
97+52.51			
22 Rt Top of fill		12.1	136.5 ✓
165 Rt guard fence		12.0	136.6
5 Rt		11.0	137.6
℄		10.4	138.2 ✓
5 Lt		9.9	138.7
18 Lt bottom of cut		10.3	138.3 ✓
Flow line 36" cul intake		11.92	see sketch for location 136.72
" " " " outlet		16.25	132.39
# 0.14 137.38		11.40	137.24 = #22 = 137.23
97+73 fence ends on Rt			
97+96.32			
21 Lt bottom of cut		0.5	136.9 ✓
17 Lt		1.3	136.1
5 Lt		1.1	136.3
℄		1.5	136.9 ✓
10 Rt		2.5	134.9
21 Rt Top of fill		3.2	134.2 ✓

+	↑ 137.38	−	
	98+40 13 PT.		
21 Rt Top of fill		5.1	132.3 ✓
℄		3.8	133.6 ✓
10 Lt		3.2	134.2
20 Lt bottom of cut		3.5	133.9 ✓
	99+00		
21 Lt bottom of cut		6.9	130.9 ✓
17 Lt		6.8	130.6
10 Lt		6.5	130.9
℄		6.8	130.6 ✓
20 Rt Top of fill		8.1	129.3 ✓
	99+25.30 PC Rt		
20 Rt Top of fill		8.7	128.7 ✓
℄		8.0	129.4 ✓
10 Lt		7.9	129.5
21 Lt bottom of cut		8.1	129.3 ✓
Intake 24 culvert flow line		12.34	125.04
Outlet " " " "		14.72 10.72 ✓	122.66
	99+75.92		
29 Lt bottom of cut		10.0	127.4
19 Lt Existing gutter		11.1	126.3 ✓
10 Lt		10.3	127.1
℄		10.5	126.9 ✓
10 Rt		11.1	126.3
19 Rt Top of fill		15.2	127.2
# 1.74	126.32	12.80	12 9.58 = 21" = 124.58

+	↑ 126.32	−	℄	50
	100+25.54			
17 Rt Top of fill		3.0		123.3 ✓
10 Rt		2.5		123.8
℄		1.8		124.5 ✓
10 Lt		1.6		124.7
19 Lt existing gutter		2.2		124.1
24 Lt bottom of cut		2.0		124.3 ✓
	100+75.66			
20 Lt bottom of cut		4.2		122.1 ✓
18 Lt existing gutter		4.2		122.1
10 Lt		3.6		122.7
℄		3.8		122.5 ✓
12 Rt		4.6		121.7
18 Rt Top of fill		4.7		121.6 ✓
	101+25.79			
18 Rt Top of fill		6.8		119.5 ✓
10 Rt		6.8		119.5
℄		6.1		120.2 ✓
10 Lt		5.8		120.5
18 Lt bottom of cut and existing gutter		6.2		120.1 ✓
	101+75.91			
19 Lt bottom of cut and existing gutter		8.6		117.7 ✓
10 Lt		8.0		118.3
℄		8.4		117.9 ✓
10 Rt		9.1		117.2
17.5 Rt Top of fill		9.6		116.7 ✓

+	℄ 126.32 ✓	−	Ele
	102+26.03		
18 Rt Top of fill	11.8		114.5 ✓
10 Rt	11.2		115.1
℄	10.6		115.7 ✓
10 Lt	10.5		115.8
19 Lt bottom of cut and existing gutter	11.1		115.1 ✓
# 0.18 114.17	12.33	113.99	
Intake flowline 18" Cul; see sketch	3.50		110.67
Outlet " " " "	5.45		108.72
	102+76.16 P.T. guard fence		
18 Lt bottom of cut and line culvert,	0.5		113.7 ✓
10	0.3		113.9
℄	0.6		113.6 ✓
10 Rt	1.1		113.1
19 Rt Top of fill	1.4		112.8 ✓
~~103+00~~	=103+00		
19 Rt Top of fill	2.8		111.4 ✓
10 Rt	2.2		112.0
℄	1.7		112.5 ✓
10 Lt	1.5		112.7
19 Lt bottom of cut	1.7		112.5 ✓
~~103+00~~	=103+50		
20 Lt bottom of cut	4.2		110.0 ✓
10 Lt	3.8		110.4
℄	4.0		110.2 ✓
10 Rt	4.6		109.6

+	℄ 114.17	−	Ele
20 Rt Top of fill	5.0		109.2
~~104+00~~	=104+50		
20 Rt Top of fill	9.5		104.7 ✓
10 Rt	8.9		105.3
℄	8.4		105.9 ✓
10 Lt	8.1		106.1
20 Lt bottom of cut	8.7		105.5 ✓
~~105+00~~	=105+50		
20 Lt bottom of cut	12.8		101.4 ✓
10 Lt	12.3		101.9
℄	12.4		101.8 ✓
10 Rt	12.8		101.4
20 Rt Top of fill	13.1		101.1 ✓
# 0.72 102.38	12.55	101.62	
~~106+00~~	=106+50		
Intake flowline 18" Cul	7.53		94.85
Outlet " " " "	9.38		93.00
19 Rt Top of fill	2.9		97.5 ✓
10 Rt	4.5		97.9
℄	4.1		98.3 ✓
10 Lt	4.0		98.4
19 Lt guard fence for cul	4.8		97.6 ✓
~~107+00~~	=107+50		
19 Lt bottom of cut	7.9		94.5 ✓
10 Lt	7.5		94.9
℄	7.5		94.9 ✓

102.38

10 Rt		7.8	94.6
21 Rt	outer 3' of fill not good. Top of fill	8.4	94.0
	~~108+00~~	=108+50	
23 Rt	Top of fill.	11.3	91.1 ✓
10 Rt		10.7	91.7
℄		10.4	92.0 ✓
10 Lt		10.6	91.8
19 Lt	bottom of cut.	10.9	91.5 ✓
#	0.80 90.51	12.67 89.71	
	~~109+00~~	=109+50	
19 Lt	bottom of slope	2.9	87.6 ✓
10 Lt		2.3	88.2
℄		2.3	88.2 ✓
10 Rt		2.6	87.9
21 Rt	Top of slope	3.0	87.5 ✓
	~~110+00~~	=110+50	
22 Rt	Top of slope	6.8	83.7 ✓
10 Rt		5.9	83.6
℄		5.6	83.9 ✓
10 Lt		5.7	83.8
19 Lt	bottom of cut	6.0	84.0
	~~111+00~~	=111+50	
23 Lt	bottom of cut	9.5	81.0 ✓
10 Lt		8.0	82.0
℄		8.6	81.9 ✓
10 Rt		8.8	81.7

+ π 90.51 — ℄/c: 5-2

20 Rt	Top of slope	9.2	81.3 ✓
#	3.46 83.06	10.61 79.90	
#	3.85 82.30	4.61 78.45 = #18 = 78.26	
	~~112+00~~	=112+50	
20 Rt	Top of slope	3.0	79.3 ✓
10 Rt		2.7	79.6
℄		2.4	79.9 ✓
10 Lt		2.4	79.9
20 Lt	bottom of cut.	3.3	79.0 ✓
	~~113+00~~	=113+50	
18 Lt	bottom of cut.	4.6	77.7 ✓
10 Lt		4.2	78.1
℄		4.1	78.2 ✓
10 Rt		4.6	77.7
20 Rt	Top of slope	5.5	76.8 ✓
	~~114+00~~ Thru cut	=114+50	
18 Rt	bottom of cut.	7.5	74.8 ✓
10 Rt		6.9	75.4
℄		6.6	75.7 ✓
10 Lt		6.3	76.0
18 Lt	bottom of cut.	6.8	75.5 ✓
	~~114+45~~ 19 P.C. Rt Thru cut	=114+95 19	
18 Lt	bottom of cut	7.5	74.8 ✓
10 Lt		7.2	75.1
℄		7.8	74.7 ✓
10 Rt		8.1	74.2
18 Rt	bottom of cut	8.4	73.9

+	π 82.30	−	Elev.
~~114+94.64~~ Thru cut			= 115 + 44.64
18 Rt bottom of cut	10.1		72.1 ✓
10 Rt	9.4		72.8
℄	9.0		73.3 ✓
10 Lt	8.7		73.6
19 Lt bottom of cut	9.1		73.2 ✓
~~114+44.09~~ Thru cut			= 115 + 94.09
21 Lt bottom of cut	10.7		71.6 ✓
10 Lt	10.1		72.2
℄	10.5		71.8 ✓
10 Rt	11.1		71.2
17 Rt bottom of cut	11.5		70.8 ✓
~~114+93.54~~ Thru cut			= 116 + 43.54
18 Rt bottom of cut	13.0		69.3 ✓
10 Rt	12.7		69.6
℄	12.1		70.2 ✓
10 Lt	11.7		70.6
20 Lt bottom of cut	12.4		69.9 ✓
#	0.45	69.89	12.86 69.44
~~116+43.99~~ Thru cut:			= 116 + 92.99
19 Lt bottom of cut	1.7		68.2 ✓
10 Lt	0.9		69.0
℄	1.1		68.8 ✓
10 Rt	1.6		68.3
17 Rt bottom of slight cut	2.0		67.9
~~116+92.44~~ End of cut on both sides			= 117 + 42.44

+	π 69.89	−	Elev.
			53
18 Rt	3.3		66.6 ✓
10 Rt	3.0		66.9
℄	2.4		67.3 ✓
10 Lt	2.7		67.7
20 Rt	2.8		67.1 ✓
~~117+41.89~~ Level out either side:			= 117 + 91.89
20 Rt	4.6		65.3 ✓
10 Rt	4.4		65.5
℄	3.9		66.0 ✓
10 Lt	3.6		66.3
20 Lt	3.9		66.0 ✓
~~117+91.34~~ Level out on either side			= 118 + 41.34
20 Lt	5.5		64.4 ✓
10 Lt	5.0		64.9
℄	5.2		64.7 ✓
10 Rt	5.6		64.6
14 Rt edge of Road	5.8		64.1
20 Rt	6.6		63.3
~~118+40.80~~ Rt.			= 118 + 90.80
6.1 Rt bottom of fill	8.6		61.3 ✓
17 Rt Top of fill	7.2		62.7
10 Rt	6.9		63.0
℄	6.7		63.2 ✓
10 Lt	6.4		63.5
20 Lt	6.7		63.2
~~118+00~~			= 119 + 50

+	π 69.89	−	℄/e	
20 Lt Top of fill		8.4		61.5
10 Lt		8.1		61.8
℄		8.2		61.7 ✓
10 Rt		8.4		61.5
20 Rt Top of fill		8.9		61.0
~~120+00~~		= 120+50		
Note: from 119+70 to 122+82 = Cul, there is a ditch on the Lt, that might wash:				
20 Rt Top of fill		12.0		57.9 ✓
10 Rt		11.3		58.4
℄		11.1		58.8 ✓
10 Lt		11.0		58.9
20 Lt Top of fill.		11.3		58.6 ✓
#	0.06	57.74	12.21	57.68 Rock
~~121+00~~		= 121+50		
20 Lt Top of fill		1.8		55.9 ✓
10 Lt		1.4		56.3
℄		1.2		56.2 ✓
10 Rt		1.9		55.8
20 Rt Top of fill		2.4		55.3 ✓
~~122+00~~		= 122+50		
20 Rt Top of fill		5.2		52.5 ✓
15 Rt		4.2		53.5
10 Rt		3.9		53.8
℄		3.2		54.2 ✓
10 Lt		3.6		54.1
18 Lt Top of fill		3.7		54.0 ✓

+	π 57.74	−	℄/e	54
~~122+97~~ double barred cul-de-sac Twin 36"				= 123+47 4
Intake flow line		10.24		47.50
Outlet " "		11.55		46.19
~~123+00~~		= 123+50		
18 Lt Top of fill		5.3		52.4 ✓
10 Lt		5.4		52.3
℄		5.3		52.4 ✓
10 Rt		5.4		52.3
18 Rt Top of fill		6.0		51.7 ✓
~~124+00~~		= 124+50		
18 Rt Top of fill		7.4		50.3 ✓
10 Rt		6.8		51.2
℄		6.4		51.3 ✓
10 Lt		6.7		51.5
18 Lt Top of fill:		6.4		51.3 ✓
124+15 92 P.C Lt.		= 124+65 92		
18 Lt Top of fill		6.6		51.1 ✓
10 Lt		6.3		51.4
℄		6.4		51.3 ✓
10 Rt		6.6		51.1
20 Rt Top of fill		7.1		50.6 ✓
124+62 77		= 125+12 77		
19 Rt Top of fill		7.5		50.7 ✓
10 Rt		6.8		50.9
℄		6.5		51.2 ✓
10 Lt		6.6		51.1
18 Lt Top of fill		6.9		50.8 ✓

+	π 57.74	−	E/e	
~~125+00~~		= 125+59 63		
19 Lt Top of fill		7.1		50.6 ✓
10 Lt		7.1		50.6
℄		6.7		51.0 ✓
10 Rt		7.8		50.7
19 Rt Top of fill		8.1		49.6 ✓
#	4.49 57.50	6.73	51.01	Rock:
~~126+06 48~~		= 126+06 48		
18 Rt Top of fill		5.7		49.8 ✓
10 Rt		5.0		50.5
℄		4.9		50.6 ✓
10 Lt		5.5		49.5
20 Lt (Level out)		4.9		50.6
~~126+53 33~~		= 126+53 33		
20 Lt (Level out)		4.9		50.6 ✓
10 Lt		5.7		49.8
℄		5.2		50.3 ✓
10 Rt		4.8		50.7
20 Rt Top of fill		5.5		50.0
~~126+50 19~~		= 127+00 19		
19 Rt Top of fill		5.3		50.2 ✓
10 Rt		4.9		50.6
℄		4.9		50.6 ✓
13 Lt		5.7		49.8
15 Lt		4.5		51.0
20 Lt (Level out)		4.0		51.5

+	π 54.50	−	E/e	55
~~126+97 54~~ P.T.		= 127+47 04		
20 Lt (Level out)		4.0		51.5 ✓
15 Lt		4.4		51.1
13 Lt		5.5		50.0
℄		4.7		50.8 ✓
10 Rt		4.8		50.7
20 Rt Top of fill		5.1		50.4 ✓
~~127+50~~		= 128+00		
20 Rt Top of fill		5.7		49.8 ✓
10 Rt		5.0		50.5
℄		4.8		50.7 ✓
13 Lt		5.6		50.9
17 Lt		4.4		51.1
20 Lt (Level out)		4.1		51.4 ✓
~~128+00~~		= 128+50		
20 Lt (Level out)		4.3		51.2 ✓
15 Lt		5.6		49.9
7 Lt		4.7		50.8
℄		4.7		50.8 ✓
10 Rt		5.1		50.4
20 Rt		5.5		50.0 ✓
46 Rt approx to ℄ existing pavement		7.50		48.0
~~128+50~~		= 129+00		
32 Rt approx ℄ existing pavement		6.42		49.08 ✓
22 Rt " edge " "		6.12		49.38 ✓
20 Rt		5.9		49.6 ✓
10 Rt		5.2		50.3

	+	π 55.50	−	Elc	
	℄		9.7		50.8 ✓
19	10 Lt		4.5		51.0
10	20 Lt in road (Level out):		9.6		50.9 ✓
	~~129+00~~		= 129+50		
1	20 Ct (Level out)		3.5		52.0 ✓
1	10 Lt		3.6		51.9
#	℄		4.0		51.5 ✓
	8 Rt Approximate edge of existing paving		4.34		51.16
1	# 10.90	62.70	3.70	51.80	Rock.
1	~~129+44.50~~ P.O.T.		= 129+94.50		
℄	10 Rt Approximate existing pavement		10.21		52.40 ✓
1	℄ = edge " "		9.93		52.77 ✓
	10 Lt		9.4		53.3
	17 Lt Top of fill		9.4		53.5 ✓
	~~130+55.50~~ Approximate Rt. existing pavement:		= 131+08.50		
	20 Lt ground		5.3		57.4
	9 Lt edge of existing pavement		5.46		57.24
1	℄ " "		5.70		57.0 ✓
	# 12.22	69.67	5.25	57.45 = 14# = 57.47	
	# 12.14	81.15	0.66	69.01	
	# 11.92	91.60	1.47	79.68 = 12# = 79.70	
	# 8.23	97.32	2.51	89.09 = 11# = 89.10	
	# 11.87	104.94	9.25	93.07 = 10# = 93.10	
1	# 0.42	99.03	6.33	98.61 = 9# = 98.65	
1	# 3.14	90.06	12.11	86.92 = 8# = 86.96	
2	# 12.81	96.23	6.64	83.42 = 7# = 83.46	

	−	+	π 96.23	−	Elc:	56
	#	12.97	108.98	0.22	96.01	
	#	9.94	118.51	0.41	108.57	
	#	11.15	129.64	0.07 ✓	118.49	
	#	11.67	140.73	0.58	129.06	
	#	11.94	151.23	1.44	139.29 = 2# = 139.34	
	#	1.13	146.56	5.80	145.43	
	#	1.68	136.90	11.34	135.22 ✓	
	⊙			4.91	131.99 = 132.08 = initial B.M. see page 33	
	#	0.60	129.14	8.36	128.54	
	#	1.24	120.85	9.53	119.61	
	⊙			7.48	113.37 = 113.11 B.R. N.W. Cor Cave and Prospect	
1		1.61	115.06	7.40	113.45	
	#	2.25	110.91	6.40	108.66 = 108.46 B.R. S.E. Cave and Ivanhoe	
	#			5.69	105.22 = 105.04 B.R. S.W. Cor Ivanhoe and Prospect	

for Xsections from 0+00 to 129+94.19 See page 57

Xsection of Hog Canyon Road
From Sta 0+00 to 39+94.18
See Page 36 for sections from 39+94.18 to 130+58.85

Donnan
Flood.
Sonnermeyer.
Oct-12-27

	+	T	−	Ele:	
	3.38	402.23		398.88 = 52 = Page 35	
		0+00			
20 Lt	ground		3.6		398.6
8 Lt	on edge existing pavement		3.43		398.80
℄	"	"	3.30		398.93
8 Rt	"	"	3.40		398.83
20 Rt	ground		3.10		399.13
Appe 74.8 on S.T. = end of exising pavement.					
20 Rt	on exising pavement		5.02		397.18
8 Rt	"	"	4.84		397.39
℄	"	"	4.78		397.45
8 Lt	"	"	4.7		397.48
20 Lt	ground		4.7		397.5
	1+26.31 = Center of curve:				
20 Lt			6.0		396.2
10 Lt			5.0		397.2
℄			5.1		397.1
10 Rt			5.3		396.9
20 Rt			5.7		396.5
20 Rt. 1+80 Fence begins:					
	1+89.97				
20 Rt	fenceline		5.6		396.6
10 Rt			4.8		397.4
℄			4.7		397.5
10 Lt			4.6		397.6
20 Lt			5.9		396.3

* These shots on south edge of existing pavement.

	+	T	−	Ele:	
		402.23			
		2+52.63 P.T.			
20 Lt			4.1		398.1
10 Lt			3.3		398.9
℄			3.3		398.9
10 Rt			3.5		398.7
20 Rt	Fence line		4.0		398.2
		3+00			
20 Rt	Fenceline		2.4		399.8
10 Rt			2.0		400.2
℄			1.8		400.4
10 Lt			1.9		400.3
20 Lt			2.3		399.9
3+03 fence on Rt jogs from 20 to 24 from ℄					
℄	10.78	412.91 4+00	0.10	402.13	
20 Lt			9.1		403.8
15 Lt			10.0		402.9
℄			9.4		403.5
10 Rt			9.4		403.5
20 Rt			9.6		403.3
24 Rt = Fence:			9.2		403.7
		5+00			
24 Rt = F			6.7		406.2
10 Rt			6.4		406.5
℄			6.4		406.5
10 Lt			6.6		406.3
15 Lt			7.1		405.8
20 Lt			6.6		406.4

+	π	−	Elev
	412.91		
5+02 on Lt fence begins 175± from ℄			
6+00			
18± Lt = Fence		4.4	408.5 ✓
15 Lt		5.0	407.9
℄		4.5	408.4 ✓
15 Rt		4.7	408.2
24 Rt = Fence		4.9	408.0 ✓
7+00 P.O.T.			
24 Rt = Fence		3.5	409.4 ✓
15 R =		2.8	410.1
℄		2.7	410.2 ✓
15 Lt		3.4	409.5
19± Lt Fence		3.4	409.5 ✓
8+00			
20 Lt F		1.1	411.8 ✓
15 Lt		2.2	410.7
℄		1.6	411.3 ✓
15 Rt		1.8	411.1
24 Rt = Fence		2.5	410.4 ✓
# 5.82	416.71	2.02	410.89
9+00			
24 Rt = Fence		5.6	411.1 ✓
15 Rt		4.7	411.8
℄		4.6	412.1 ✓
15 Lt		5.2	411.5
21 Lt = Fence		4.0	412.7 ✓

+	π	−	Elev
	416.71		
10+00			
22 Lt = Fence		3.8	412.9 ✓
17 Lt		4.1	412.6
15 Lt		5.1	411.6
℄		4.5	412.2 ✓
15 Rt		4.9	411.8
24 Rt = Fence		5.9	410.8
11+00			
23 Rt = Fence		6.0	410.7 ✓
15 Rt		5.2	411.5
℄		4.6	412.1 ✓
10 Lt		4.5	412.2
15 Lt		4.9	411.8
17 Lt		3.9	412.8 413.1
23 Lt = Fence		3.5	413.5 ✓
# 4.53	416.31	4.93	411.78 = 49# 411.72
12+00			
24± Lt = Fence		3.0	413.3 ✓
17 Lt		3.6	412.7
15 Lt		4.4	411.8
℄		4.4	411.9 ✓
15 Rt		4.9	411.4
23± Rt = Fence		5.8	410.5 ✓
13+00			
23 Rt = Fence		5.7	410.6 ✓
15 Rt		4.9	411.4
℄		4.2	412.1 ✓

+	HI 416.31	−	E/E	
10 Lt		4.1		412.2
15 Lt		4.6		411.7
25.2 Lt = Fence		3.2		413.1 ✓
	14+00			
26.2 Lt = Fence		3.2		413.1 ✓
22 Lt		3.3		413.0
20 Lt		4.7		411.6
10 Lt		4.6		411.9
℄		4.3		412.0 ✓
15 Rt		4.9		411.4
23 Rt = Fence:		5.4		410.9
	15+00			
23 Rt = Fence		5.6		410.7 ✓
15 Rt		5.0		411.3
℄		4.6		411.7 ✓
10 Lt		4.5		411.8
22 Lt		5.2		411.1 ✓
23 Lt		3.7		412.6
27 Lt = Fence		3.4		412.8
℄	3.37	414.57	5.11	411.20 Nail
15+75 on the Lt fence ends, 28' Lt of ℄				
	16+00			
28 Lt		2.2		412.4
25 Lt		2.4		412.2
23 Lt		4.0		410.6 ✓
10 Lt		3.3		411.3

+	HI 414.57	−	E/E	
℄		3.3		411.3 ✓
10 Rt		3.5		411.1
15 Rt		3.9		410.7
23 Rt Fence		4.7		409.9 ✓
	17+00			
27 Rt = Fence		5.8		408.8 ✓
10 Rt		4.7		409.9
℄		4.2		410.4 ✓
10 Lt		4.4		410.2
23 Lt		5.0		409.6 ✓
26 Lt		2.8		411.8
28 Lt		2.8		411.8
17+10 = beginning of fence line on Lt = 28' Lt of ℄				
	18+00			
26 Lt = Fence		5.2		409.4
24 Lt		5.4		409.2
23 Lt		6.0		408.1 ✓
10 Lt		5.6		409.0
℄		5.6		409.0 ✓
10 Rt		6.0		408.6
22.5 Rt = Fence		7.4		407.2 ✓
	19+00			
22.3 Rt = Fence		9.2		405.4 ✓
18 Rt =		8.9		405.7
10 Rt		7.3		407.3
℄		6.8		407.8 ✓

	+	π	−	Elc	
		414.57			
10 Lt			6.0		409.1
23 Lt			7.5		407.1 ✓
25 Lt			6.6		408.0
268 Lt = Fence			6.5		408.1
#	3.04	410.36	2.25	407.37 ✓	
		20+00			
265 Lt = Fence			3.1		407.3
24 Lt			3.2		407.2
22 Lt			3.9		406.5 ✓
10 Lt			3.4		407.0
℄			3.5		406.9 ✓
10 Rt			3.8		406.6
22 Rt = Fence			5.4		405.0 ✓
20+18 fence ends on Lt - 26½ from ℄					
20+30 " " " Rt 22 " ℄					
		21+00			
20 Rt			5.7		404.7 ✓
10 Rt			5.0		405.4
℄			4.5		405.9 ✓
10 Lt			4.5		405.9
21 Lt			5.4		405.0 ✓
23 Lt			3.5		406.9
28 Lt			3.5		406.9
		22+00			
27 Lt			4.3		406.1
25 Lt			4.4		406.0

	+	π	−	Elc	
		410.36			
21 Lt			6.5		403.9 ✓
10 Lt			5.8		404.6
℄			5.8		404.6 ✓
10 Rt			6.1		404.3
20 Rt			6.5		403.9 ✓
2,269 fence begins on Lt, 25½ from ℄					
		23+00			
20 Rt			8.4		402.0 ✓
10 Rt			7.7		402.7
℄			7.4		403.0 ✓
10 Lt			7.4		403.0
21 Lt			8.5		401.9 ✓
23 Lt			6.3		404.1
25.4 Lt			6.3		404.1
#	0.89	402.0 ✓	9.23	401.13	
		24+00			
265 Lt Fence			1.0		401.0
23 Lt			1.1		400.9
21 Lt			2.1		399.9 ✓
10 Lt			0.9		401.1
℄			1.0		401.0 ✓
10 Rt			1.4		400.6
20 Rt			2.6		399.6 ✓
		25+00			
20 Rt			4.5		397.5 ✓
10 Rt			3.5		398.5
℄			3.2		398.8 ✓

+	⊼ 402.02	−	Ele.
10 Lt		2.6	399.4
22 Lt		3.9	398.1 ✓
23 Lt		3.4	398.6
26.5 Lt = Fence		3.3	398.7
	26+00		
26 Lt = Fence		4.7	397.3
23 Lt		4.7	397.3
21 Lt		5.6	396.4 ✓
10 Lt		4.4	397.6
℄		4.8	397.2 ✓
10 Rt		5.1	396.9
20 Rt		5.6	396.4 ✓
	27+00		
25 Rt		6.7	395.3
20 Rt		6.8	395.2 ✓
18 Rt		7.4	394.6
10 Rt		6.9	395.1
℄		6.5	395.5 ✓
10 Lt		6.1	395.9
21 Lt		7.5	394.5 ✓
23 Lt		5.7	396.3
27.5 Lt = Fence		5.7	396.3
	28+00		
28.3 Lt = Fence		7.6	394.4
23 Lt		8.2	393.8
21 Lt		9.3	392.7 ✓

+	⊼ 402.02 ✓	−	Ele
10 Lt		7.9	394.1
℄		8.2	393.8 ✓
10 Rt		8.6	393.4
20 Rt		9.1	392.9 ✓
22 Rt		8.5	393.5
25 Rt		8.2	393.8
# 0.65	392.72	9.95	392.02
	29+00		
25 Rt		1.6	391.1
20 Rt		1.8	390.9 ✓
10 Rt		1.2	391.5
℄		0.9	391.8 ✓
10 Lt		0.7	392.0
24 Lt		1.9	390.8 ✓
26 Lt		1.3	391.4
29 Lt = Fence		1.3	391.4
	30+00		
29.5 Lt = Fence		4.1	388.6
22 Lt		4.5	388.2 ✓
10 Lt		3.0	389.7
℄		2.7	390.0 ✓
10 Rt		3.0	389.7
20 Rt		4.3	388.4 ✓
	31+00		
20 Rt		6.2	386.5 ✓
10 Rt		5.0	387.7

+	ℸ 392.7	-	Elev	
		4.8	387.9	
℄		4.9	387.8	
10 Lt		6.3	386.4	
22 Lt		6.0	386.7	
30 Lt = Fence				
	32+00			
20 Lt = Fence		7.7	385.0	
23 Lt		7.9	384.8	
11 Lt		6.7	386.0	
℄		6.6	386.1	
10 Rt		6.8	385.9	
20 Rt		7.6	385.1	
	33+00			
20 Rt Top of fill		9.7	383.0	
10 Rt		8.5	384.2	
℄		8.2	384.5	
11 Lt		8.3	384.4	
25 Lt		10.2	382.5	
27 Lt		9.4	383.3	
31 Lt = Fence		9.4	383.2	
# 1.60	380.50	8.72	384.00	
	34+00			
32 Lt = Fence		4.2	381.3	
29 Lt		4.3	381.2	
28 Lt		5.0	380.5	
24 Lt		5.0	380.5	
12 Lt		3.7	381.8	

+	ℸ 385.50	-	Elev 6
℄		2.6	382.9
15 Rt		3.3	382.2
20 Rt Top of fill		4.1	381.4
	35+00		
20 Rt Top of fill		4.9	380.6
10 Rt		4.2	381.3
℄		3.9	381.6
12 Lt		4.2	381.3
22 Lt		6.3	379.2
30 Lt		5.0	380.5
36 Lt = Fence		4.9	380.6
	36+00		
38 Lt = Fence		6.2	379.3
27 Lt		6.3	379.2
25 Lt		7.2	378.3
21 Lt		7.2	378.3
12 Lt		5.5	380.0
℄		5.2	380.3
10 Rt		5.4	380.1
20 Rt Top of fill		6.0	379.5
	37+00		
20 Rt Top of fill		7.6	377.9
10 Rt		6.3	379.2
℄		6.0	379.5
13 Lt		6.3	379.2
28 Lt		8.2	377.3

+	π	−	Elc
	385.00		
30 Lt		6.9	378.6
33 Lt = Fence		6.8	378.7
#	3.05	7.20	378.30
	38+00		
338 Lt = Fence		3.0	377.8
30 Lt		3.7	377.6
28 Lt		4.8	376.5
24 Lt		5.0	376.3
16 Lt		3.4	377.9
11 Lt		3.0	378.3
℄		2.9	378.4
10 Rt		3.2	378.1
20 Rt = Top of fill		3.9	377.4
	39+00		
20 Rt Top of fill		4.8	376.5
10 Rt		4.3	377.0
℄		4.0	377.3
12 Lt		4.2	377.1
21 Lt		5.0	376.3
29 Lt		6.6	374.7
30 Lt		6.3	375.0
32 Lt		5.2	376.1
34 Lt = Fence		5.0	376.3

Note: at 39+75 Fence angles about 10° to Lt and leaves Road;
39+94 T.P.O.T. See page 36 for continued Levels;

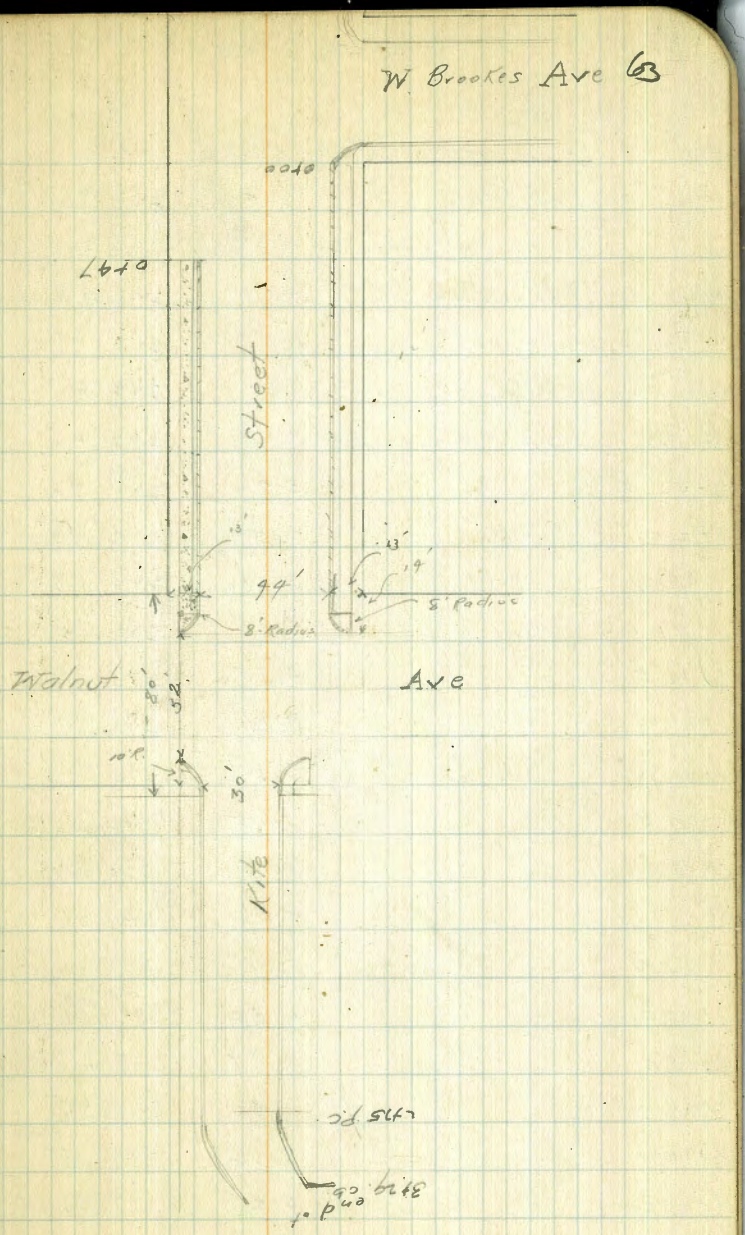
20 Lt		5.4	375.8
13 Lt		5.3	376.1

+	π	−	Elc
	381.35		
℄		5.1	376.3
20 Rt = Top of fill		5.5	375.9
#		6.14	375.21 = 43 # = 375.17

Bliss
Isbell
Pearson

Curb Levels on Kite Street from the S Line of Brookes to the N Line of Upas

	+	+	-	Elev
B.M. 6" E Bolt on Hy. S.E. Brooks & Kite	2.07	258.10		256.03
0+00 E			2.16	255.94
0+25 E			2.42	255.68
0+47 E = 00 on West Side			2.72	255.38
0+47 W = 00 on West Side			2.07	256.03
0+75 W			3.37	254.73
0+75 E			3.98	254.12
1+00 E			5.09	253.01
1+00 W			4.41	253.69
1+25 W			5.60	252.50
1+25 E			6.38	251.72
1+50 E			7.65	250.45
1+50 W			6.78	251.32
1+75 W			7.99	250.11
1+75 E			8.90	249.20
2+00 E			10.17	247.93
2+00 W			9.20	248.90
2+25 W			10.45	247.65
2+25 E			11.42	246.68
2+50 E			12.65	245.45
2+50 W			11.66	246.44
2+75 W			12.86	245.24
T.P	0.12	245.36	12.86	245.24
2+75 E			1.18	244.18
3+00 E N Line of Walnut			2.42	242.94
East end of Return			2.51	242.85



245.36

3+00 W. N Line of Walnut	1.35	244.01
West end of Return	1.90	243.96
S. Line of Walnut = 0.0		
West end of Return on W	1.83	243.53
Return of S. Line of Walnut on W	1.88	243.48
East end of Return on E	2.89	242.47
Return on S Line of Walnut on East	2.93	242.43
0+25 E	3.46	241.90
0+25 W	2.54	242.82
0+50 W	3.17	242.19
0+50 E	4.01	241.35
0+75 E	4.57	240.79
0+75 W	3.82	241.54
1+00 W	4.43	240.93
1+00 E	5.15	240.21
1+25 E	5.75	239.61
1+25 W	5.15	240.21
1+50 W	5.75	239.61
1+50 E	6.30	239.06
1+75 E	6.89	338.47
1+75 W	6.40	238.96
2+00 W	7.00	238.36
2+00 E	7.44	237.92
2+25 E	8.00	237.36
2+25 W	7.70	237.66
2+50 W	8.35	237.01

245.36

N.W. 26655
Contr. Prot.

2+50 E	8.59	236.77
2+75 E PC to L.	9.14	236.22
TP. 495 240.67	9.14	236.22
2+75 W PC. to L.	9.28	236.39
2+93 W	9.76	235.91
2+93 E	9.84	235.83
3+11 E	5.27	235.40
3+11 W	5.21	235.46
3+29 W End of Cb	5.71	234.96
3+29 E End of Cb	5.70	234.97
Check on B.M. NE opposite	5.62	235.05

X- Section WINONA from S.L. University to S.L. Landis, 60' wide, 12' S.W. 9' Cu.

STA	+	H.I.	−	Elev
B.M. B.P. SW. Estrella & University				326.68
T.P.	12.71	339.39 ✓	9.11	330.28
S.L. University				
W.L. Bank Top			4.6	3348
✓ Bott.			10.7	328.7
W. Curb Top			11.3	3281
✓ Bott.			11.79	327.6
W 1/4			11.03	328.4
℄			10.50	328.9
E 1/4			10.32	3291
E. Curb Bott.			10.31	329.1
✓ Top			9.65	329.7
E.L. Bank Top			5.30	334.1
✓ Bott.			9.10	330.3
0+00				
W.L.				
W. Curb			4.7	334.7
+3'			6.5	332.9
+6'			10.7	328.7
W 1/4			11.0	328.4
℄			10.✓	3292
E. 1/4			9.8	329.6
+1'			9.6	3298
+3'			5.4	334.0
E. Curb			5.2	334.2

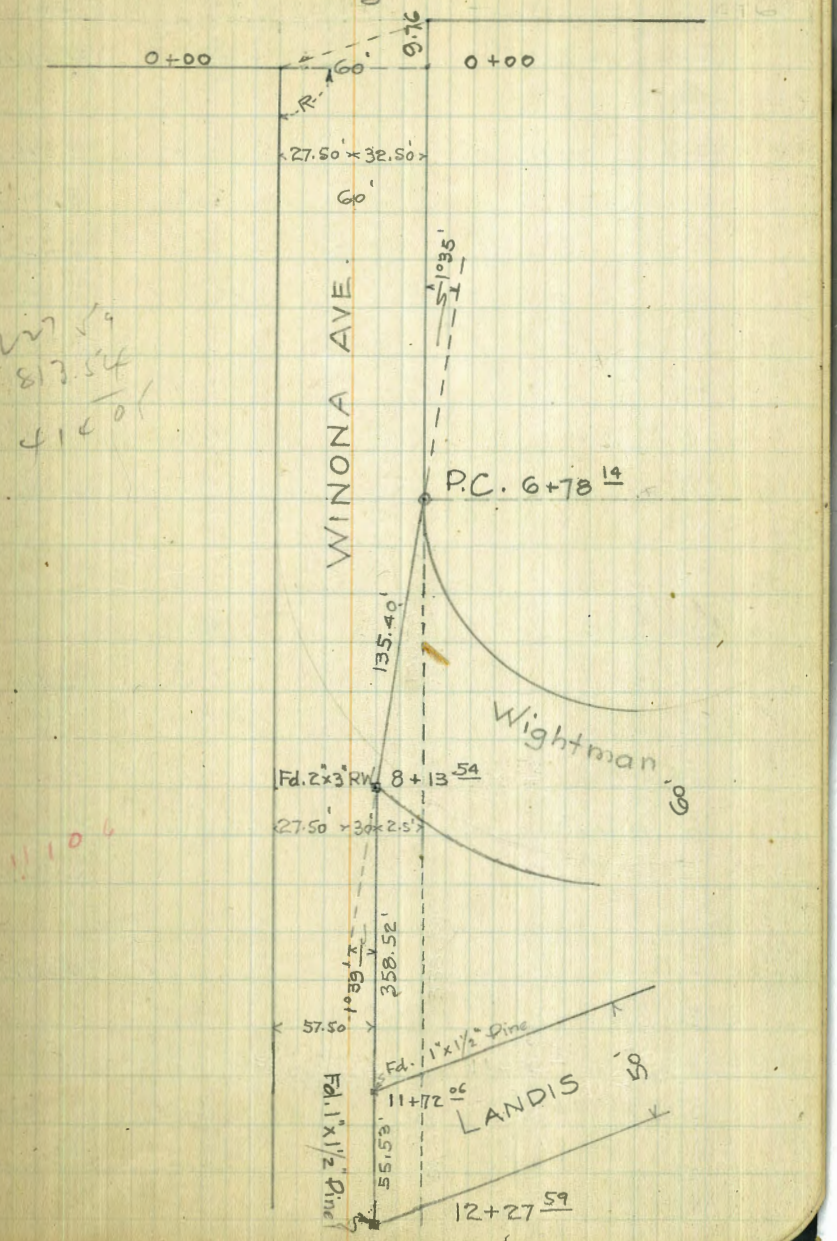
Plotted 9-28-1928 C.B.H.

JAEGER
Bailey
Claver +
Brooks

Sept. 25th 1928.

68

University



339.39

Sta	+	H.I.	−	Elev.
E.L.			5.0	334.4
0+30				
E.L.			5.0	334.4
E. Curb			5.4	334.0
E'/a			5.5	333.9
℄			6.0	333.4
W'/4			5.7	333.7
+3'			5.0	334.4
W. Curb			4.6	334.8
W.L.			4.7	334.7
0+50				
W.L.			4.8	334.6
W. Curb			4.9	334.5
W'/a			4.9	334.5
℄			5.0	334.4
E'/4			4.9	334.5
E. Curb			5.3	334.1
E.L.			5.8	333.6
1+06				
E.L.			5.7	333.7
E. Curb			5.7	33.7
+3'			5.9	33.5
E'/a			5.6	33.8
℄			5.5	333.9
W'/4			5.7	33.7

339.39 (6c)

Sta	+	H.I.	−	Elev.
+6'			5.8	33.6
W. Curb			4.9	34.5
W.L.			4.8	334.6
1+50				
W.L.			6.1	333.3
+10'			6.0	33.4
W. Curb			6.5	32.9
W'/4			6.0	33.4
℄			6.1	333.3
E'/4			6.5	32.9
+3'			6.6	32.8
E. Curb			6.1	333.
E.L.			6.2	333.2
2+00				
E.L.			6.9	332.5
E. Curb			6.8	32.6
+5'			7.3	32.1
E'/4			7.1	32.3
℄			6.8	332.6
W'/4			6.8	32.6
+8'			7.2	32.2
W. Curb			6.5	32.9
W.L.			7.0	332.4
	3.86	334.14		
T.P.			12.26	321.88

33414

Sta	+	H.I.	−	Elev.
2+50				
W.L.			2.8	331.3
+10'			2.6	31.5
W.Curb			3.1	31.0
W¼			2.5	31.6
℄			2.3	331.8
E¼			2.8	31.3
+3'			2.3	31.8
E.Curb			2.1	32.0
E.L.			2.3	331.8
3+00				
E.L.			2.8	331.3
E.Curb			2.7	31.4
E¼			3.6	30.5
℄			3.2	330.8
W¼			3.5	330.6
+7'			4.0	330.1
W.Curb			3.8	330.3
W.L.			3.9	330.3
3+50				
W.L.			5.8	328.3
+11'			5.0	329.1
W.Curb			5.2	328.9
W¼			4.6	329.5
℄			4.4	329.7

33414

67

Sta	+	H.I.	−	Elev.
E¼			4.9	329.2
+6'			4.1	330.0
E.Curb			3.9	330.2
E.L.			3.7	330.4
4+00				
E.L.			4.5	329.6
E.Curb			5.3	328.8
+2'			5.2	328.9
+6'			6.1	328.0
E¼			5.8	328.3
℄			5.7	328.4
W¼			5.8	328.3
W.Curb			6.5	327.6
+3'			7.3	326.8
W.L.			8.2	325.9
4+50				
+10'			12.2	321.9
W.L.			10.8	323.3
W.Curb			8.7	325.4
+2'			8.3	325.8
W¼			8.1	326.0
℄			7.7	326.4
E¼			7.6	326.5
+3'			6.8	326.3
E.Curb			6.7	326.4

Sta	+	H.I.	−	Elev.
E.L.			6.0	328.1
5+00				
E.L.			7.6	326.5
E. Curb			8.2	25.9
+5'			8.6	25.5
E'/4			10.1	24.0
℄			9.9	324.2
W'/4			10.3	23.8
+6'			10.1	24.0
W. Curb			11.3	22.8
W.L.			13.1	321.0
+10'			14.7	319.4
	4.11	325.99 ✓		
T.P.			13.05	312.94
5+50				
+16'			9.7	16.3
W.L.			8.3	317.7
+9'			6.8	19.2
W. Curb			5.6	20.4
+3'			4.7	21.3
W'/4			4.5	21.5
℄			4.5	321.5
E'/4			4.7	21.3
+2'			2.6	23.4
E. Curb			1.8	24.2

Sta	+	H.I.	−	Elev.
E.L.			0.8	325.2
6+00				
E.L.			3.5	322.5
E. Curb			5.8	20.2
+3'			6.2	19.8
+7'			9.3	16.7
E'/4			8.6	17.4
℄			8.7	317.3
W'/4			8.7	17.3
+4'			8.7	17.3
W. Curb			10.1	15.9
W.L.			12.6	313.4
+10'			14.0	12.0
6+50				
T.P.			13.05	312.94
Hand Level	0.20	313.14		
+10'			8.2	04.9
+4'			5.0	08.1
W.L.			4.5	308.6
W. Curb			2.4	10.7
+6'	Instr.	325.99 ✓	13.2	12.8
W'/4			13.1	12.9
℄			13.0	313.0
E'/4			12.5	13.5
+3			13.7	12.3

325.99

Sta		+	H.I.	−	Elev.
	+7'			11.5	314.5
	E. Curb			11.0	15.0
	E.L.			8.0	318.0
		2.52	315.46 ✓		
	T.P. Hub at Sta. 8+13.59			11.15	304.31
6+78.14	P.C.				
	E.L.			0.89	314.6
	E. Curb			2.7	12.8
	+2'			3.1	12.4
	+3'			5.1	10.4
	+6'			4.7	10.8
	E'/a			4.7	10.8
	℄			4.8	310.7
	+7'			4.6	10.9
	W'/a			5.0	10.5
	W. Curb			7.0	08.5
	W.L.			10.0	305.5
	+10'			12.3	3.2
	+15'			13.6	1.9
	+20'			17.0	298.5
7+00	T.P.			13.0	302.46
	Hand Level	1.0	303.46		
	+20'			6.5	297.0
	+10'			3.2	300.3
	W.L.	Instr.	315.46 ✓	12.5	303.0

315.46

69

Sta		+	H.I.	−	Elev.
	W. Curb			9.4	306.1
	W'/a			6.8	308.7
	+4'			6.0	309.5
	℄			6.0	309.5
	E'/a			6.0	309.5
	+5'			6.1	309.4
	+7'			6.9	308.6
	E. Curb			5.4	311.1
	E.L.			3.4	312.1
7+50					
	E.L.			8.8	306.7
	+21'			8.8	306.7
	+30'			11.3	304.2
	T.P.			13.0	302.46
	Hand Level	0.9	303.36		
	+50'			8.1	295.3
	+60' T.P.			11.8	291.56 ✓
		1.20	292.76		
	+80'			9.2	283.6
	Instr.	1.95	306.26 ✓		
	T.P.			12.97	293.29
7+85					
	+20'			1.5	304.8
	E.L.			0.8	305.5
	+10'			1.5	304.8

STA	+	H.I.	−	Elev.
+19'			6.0	300.3
+30'			10.0	296.3
T.P.			12.50	293.76
Hand Level	0.50	294.26		
+50'			6.5	287.8
T.P.			13.0	281.26
	0.30	281.56		
+70'			3.2	278.4
+80'			6.0	275.6
+100' Bottom Canyon			9.1	272.5
8+13 54	Instr.	306.26 ✓		
+20'			1.9	304.4
E.L.			2.0	304.3
+16'			3.8	302.5
+24'			7.6	298.7
+32'			11.8	294.5
T.P.			13.0	293.26
Hand Level	0.7	293.96		
+50'			7.8	286.1
+60' T.P.			13.0	280.96
	0.30	281.26		
+80'			8.0	272.3
+100' Bottom Canyon			10.8	270.5
8+50	Instr.	306.26 ✓		
+20'			5.0	301.3

306.26

STA	+	H.I.	−	Elev.
E.L.			4.9	301.4
+12'			6.6	
+20'			10.2	
+26' T.P.			13.0	293.26
Hand Level	0.0	293.26		
+38'			4.0	
+55'			11.0	281.3
+60' T.P			13.0	280.26
+80'	0.8	281.06	7.4	
+100' Bottom Canyon			11.7	
	5.14	298.43 ✓		
T.P.			13.19	285.24
9+00				
+25'			3.2	
+22'			3.5	
+16'			5.6	
E.L.			5.7	292.7
+2'			4.8	
+30'			7.5	290.9
+40'			10.6	
+49' T.P.			13.0	285.43
Hand Level	0.4	285.83		
+68'			8.2	277.6
+80' T.P.			13.0	272.83
	1.70	274.53		

Sta	+	H.I.	−	Elev.
+90'			5.4	
+100' Bottom Canyon			6.6	
9+50	Instr.	298.43 ✓		
+20'			8.6	
+7'			8.7	
E.L.			11.0	287.4
+17'			11.1	
+18'			10.3	
+40'			11.6	286.8
+46' T.P.			13.0	285.43
Hand Level	1.20	286.63		
+67'			5.5	281.1
+77'			11.2	
T.P.			13.0	273.63
	0.10	273.73		
+97'			8.2	
+100' Bottom Canyon			11.0	
+105'			9.6	
+110'			9.4	
	3.22	288.46 ✓		
T.P.			13.11	275.35
9+70				
+30'			0.4	
E.L.			0.7	287.8
+5'			2.5	

288.46

11

Sta	+	H.I.	−	Elev.
+26'			2.9	
+28'			2.4	286.1
+60'			6.2	282.3
+70' T.P.			13.0	275.46
Hand Level	2.30	277.76		
+85'			10.3	
+93'			14.7	
+97' Bottom Canyon			13.6	
+100' ✓ ✓			13.6	
9+90	Instr.	288.46 ✓		
+25'			5.7	
E.L.			2.8	285.7
+14'			2.8	
+17'			5.2	
+19'			4.2	284.3
+40'			6.0	282.5
+43'			5.5	283.0
+75'			10.7	277.8
+79' T.P.			13.0	275.46
Hand Level	0.10	275.56		
+88'			6.3	
+100'			13.6	
+102'			12.3	
+110' Bottom Canyon			11.7	

STA	+	H.I.	−	Elev.
	2.97	278.32 ✓		
T.P.			12.55	265.77
10+50				
+20'			11.9	
E.L.			11.2	267.1
+21'			9.2	269.1
+45'			5.0	273.3
+65'			6.2	272.1
+83'			7.5	
+91'			10.8	
+92' T.P.			13.0	265.32
Hand Level	4.50	269.82		
+96'			5.9	
+97'			9.2	
+100'			8.2	
+110' Bottom Canyon			7.5	
	6.36	272.13 ✓		
T.P.			12.65	259.48
11+00				
+30'			11.30	
E.L.			10.4	261.7
+43'			8.3	263.8
+50'			5.8	266.3
+62'			6.1	266.0
+71'			8.0	
+73'			12.3	
+77'			12.3	
+78' Bottom Canyon			8.8	
	7.74	267.22 ✓		
11+50				
+30'			7.6	
+25'			8.2	
+23' Bottom Creek			10.0	
+17' " "			10.6	
+13'			8.0	
E.L.			7.5	259.7
+40'			6.6	260.6
+48'			5.5	
+53'			5.1	
+57'			9.0	258.2
+60'			8.9	
+65'			5.7	
11+72.06 N.L. Landis				
+30' On N.L. Landis			8.6	
+26' " "			9.3	
+22' " " Bottom Creek			11.1	
+15' " "			10.1	
E.L.			8.6	258.6
+19'			7.7	

267.22

Sta	+	H.I.	−	Elev.
+51'			7.5	259.7
+52'			9.3	
+56'			7.9	259.3
+70'			8.2	
11+99 82'	℄ Landis			
+25' On ℄	"		8.1	
+19' "	"		8.8	
+14' "	"		7.9	
E.L.			8.4	258.8
+14'			8.2	
+17'			9.8	
+23'			10.8	
+35'			9.6	257.6
+42'			8.2	
+48'			8.5	
+51'			10.9	
+56'			8.7	258.5
+62'			8.9	
12+27 59'	S.L. Landis			
+20' On "	"		8.4	
E.L.			8.9	258.3
+12'			8.4	
+35'			8.9	258.3
+36'			10.9	
+45'			11.3	
+50'			10.0	
+60'			11.6	255.6
+63'			9.4	
+70'			9.2	

Sta	+	H.I.	−	Elev.

Sta	+	H.I.	−	Elev.

Sta	+	H.I.	−	Elev.

Sta	+	H.I.	−	Elev.

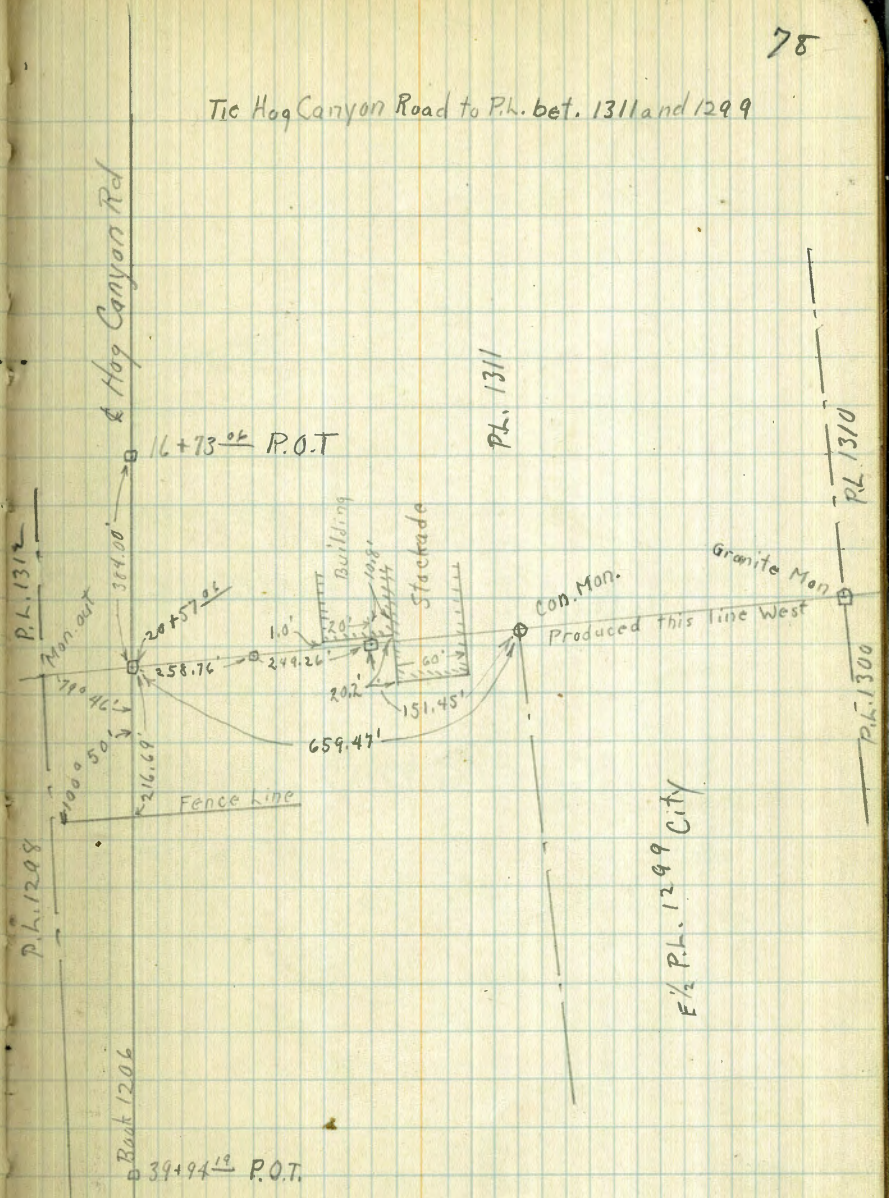
STA	+	H.I.	−	Elev.
—				

STA	+	H.I.	−	Elev.

STA

1

Tie Hog Canyon Road to P.L. bet. 1311 and 1299



DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

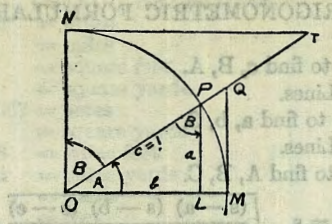


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

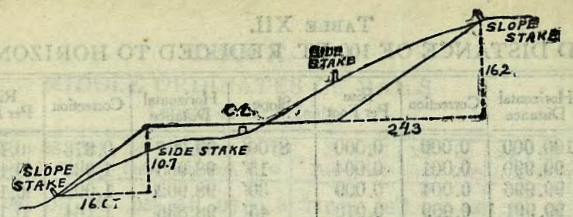
$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5 10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6 75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13 65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19.35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45 90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51 90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54 15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55 95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58 95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65.40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66 75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

6+78.14
1 35.40
8+13.54

2 | 55.53
27.76
11 72.06
11+99.82

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO.
CALIFORNIA.

179 60
60 54
119 06
59 39

89.88
1300

106 [illegible]
53° 4'

22°40'
E 19.89
R = 1000
T = 200.42

gas station

gas station

125 x 125
250
625
15625 ✓

185 x 185
1480
925
34225
15625
186100 = 136.38
86 : 23 x 3
69
1700 : 266 x 6
1596
10400 : 2723 x 3
8169
223100 : 27268 x 8
218144
4956

326.68
12.71
339.39
- 8.11
330.28
3.86
334.14
12.26
321.88
4.11
325.99
- 13.05
312.94
+ 2.52
315.46
- 11.15
304.31
+ 1.95
306.26
- 12.97
293.29
5.14
298.43
13.19
285.24
3.22
288.46
13.11
275.35
2.97
278.32
12.55
265.77
6.36
272.13

303.36
11.80
291.56
306.26
12.50
293.76

272.13
12.65
259.48
7.74
267.22