

1209

DASTY

FIELD BOOK

No. 335

1209

MICROFILMED
DEC 22 1964

No. 380 7/11/30 (M.A.)

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

Our Leather Bound Engineers Note Books are carried in the following rulings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

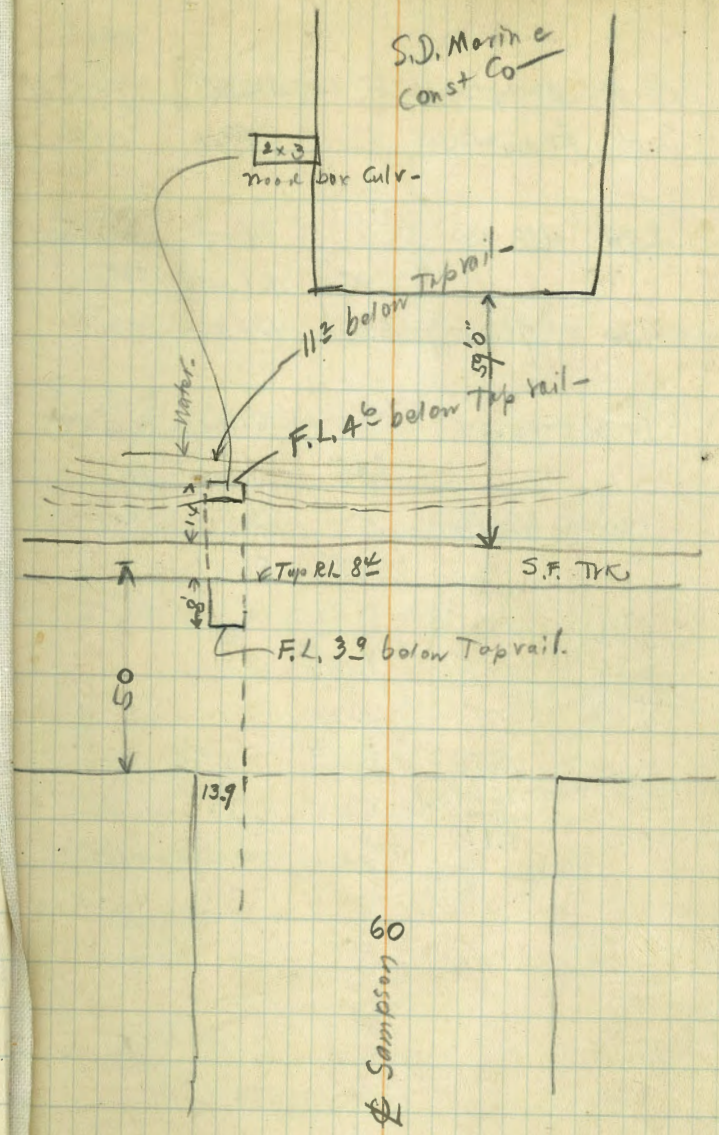
THE FREDERICK POST CO.
ENGINEERING and DRAFTING SUPPLIES
IRVING PARK STATION
CHICAGO, ILL.

-58
-57
+71
-53
-59
-68

Index

Sampson St	11
N ^o St - Drainage	2-20
Yama St -	21
N ^o St	22-38
M ^o St 27 th St	39
37 th Main	40
Sanleigh Place - Miss Blvd.	41
Pulboa Court	42-48
Seal ✓	43
Kingston -	44
Nantasket	45
La Jolla Blvd	46-57
Allison + Turq -	47
64 th Breaks -	49+71
Allison - Pac	50-53
Pierce - Portsmouth	51-59
Rockaway	52
Ala - St	54-68
Vanitie Ct.	55
Whitwig ✓	56
Sierra - Maine Place	58
Wetherby - Atlantic	60
Alberta Place	62
Essex St	62

Salem Ct	61
6th and Brooks Culvert	71 + 49
Cape May Av	66
Alley - Olive - Palm - 30' x 21'	67
Alabama St.	68
Cottonwood - Ann -	69
Herbert - Pa -	70
2 nd St 30 + 31 st	72
Fern - Goupe	73
Johnson - Hayes -	74
Park Blvd + Union - Bk 19v	75



N.W. 25th + 26th -
S.E. Ernst + N

54.28

65.01

54.2

31

54.09

53.91

.18

8.90 63.30

2.25

54.20

61.05

N.W. curb
25th + N. Sts.

TP

9.20 70.25

5.03

65.32

5.03 70.04

8.98

65.01

61.06

Br. H. S.E.
Ernst & N.

TP

2.40 63.56

9.55

53.91

7.02

8.50

4.37

5.45

4.66

3.05

~~8.15~~
~~3.00~~

5.45

4.30

5.36

7.66

6.95

8.38

8.12

2.65

3.02

3.9

.37

N.W. 7th pr 17 + 26 - tied No. tan Imp -
100' Cap tk

N.W. 7th 18" 50' N. Cap Tk

Kearney - N.L. & S.L. N - 50' to' on Kearney -

at 19 - N.W. 7th pr - tied 65' N. Cap tk -

at 20 - N.W. 7th pr - tied 10' tan Imp -

at 21 - N.W. 7th pr - Cap tk in

on J. 25th + 26 - C.O. Bno + curb -
on Hensley - Pr. Ref N -
Curb Inlets -

8/15/27
2/28

			102.00	
1.30	103.30			
Sub. fr. G.O.	95 50 C. 112	10.3 8.3	93.0 95.0	low for T. St.
3.84	89.89		86.-	
4.27		4.87	85.02	
		5.82	84.07	
		8.80	81.09	

4.52	90.52		86.00
		9.52	81.00

5.43	91.43		86.00
		12.60	80.80

5.42 91.42

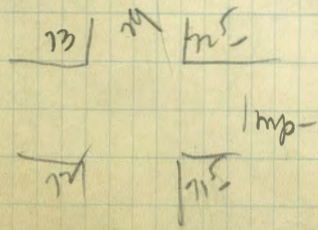
S.M. 28" Hk 85.-

5115 9016

	7.67	82.29	stk-
Grd-		73	
		C-9.3	
11±	6.43	83.73	
Grd-		720	
		C-11.4	

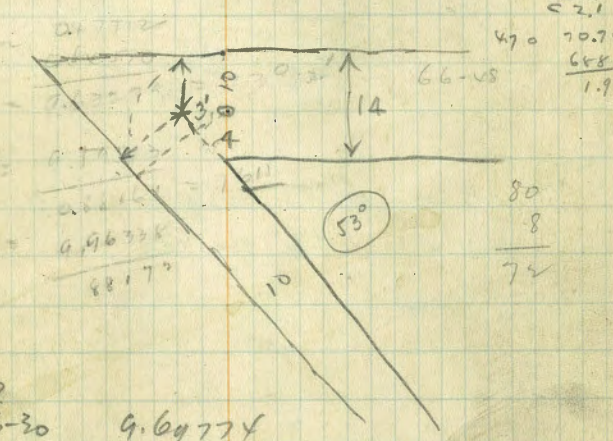
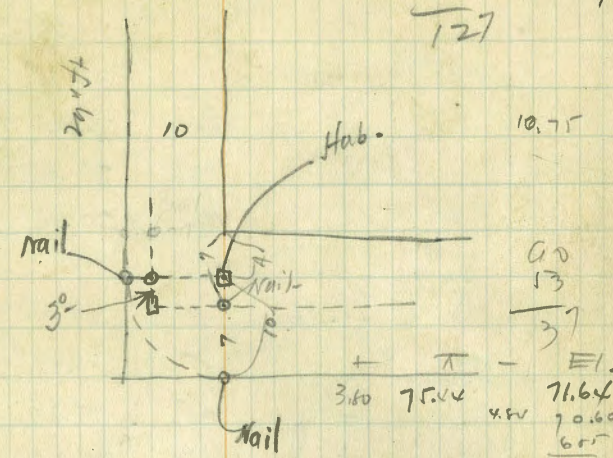
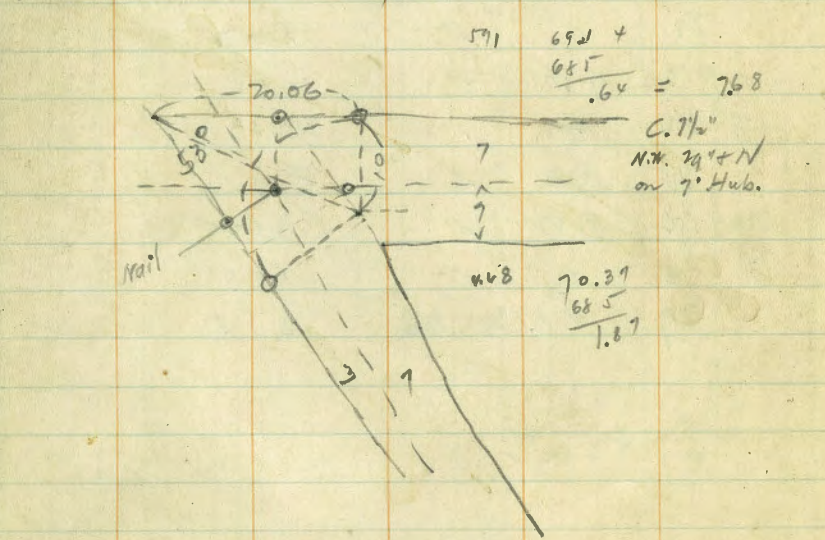
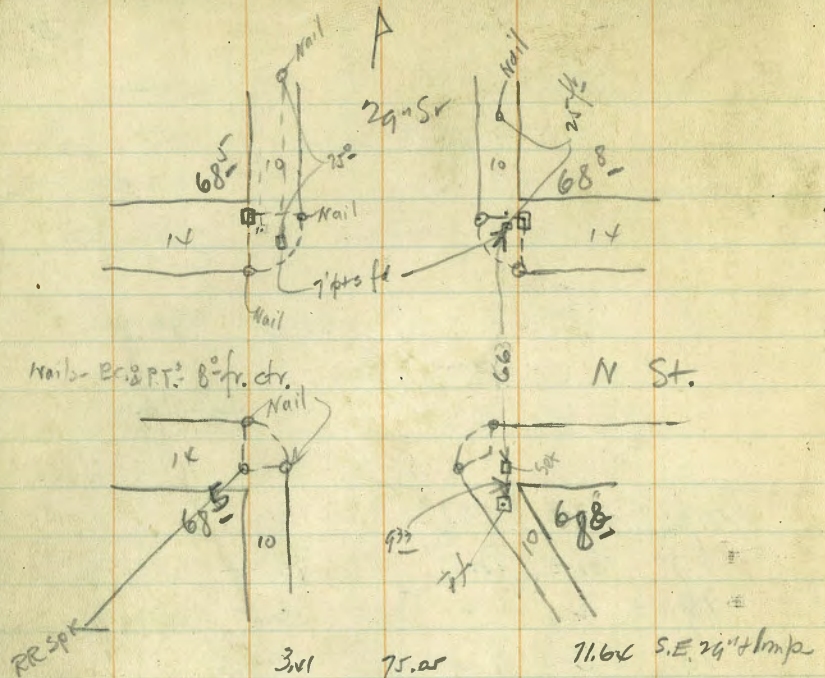
Imp. Are P, M²

17"	N.E.	P.P.	36.-
19	✓	✓	56.97
20	✓	✓	57.03
21	-	✓	55.03
22	N.W.	✓	56.08
24	✓	✓	56.97
25	N.E.	✓	58.94
26	N.W.	✓	63.92
30	✓	✓	74.97
29	✓	R. Spk. Pole	72.84



N^o St. Impr-

140
53
127 4



2/53
tan 26-30 = 9.69774
10 = 1 / 1.30226 = 70.06
h_m = 9.64953 / 1.35047 = 71.41

N. St

4.57 76.01 71.5 S.E. M 8 29
 3.41 72.60 N.E
 296 73.05 NW
 395 72.06 SW

75.96

6.52 69.42
 6.85 69.11 68.61

560
 7036
 688
 1.56

681

7.15 68.81

7.46

7.56 68.40

6880

68.5

75.96

7.16

7.46

5.96

70.00

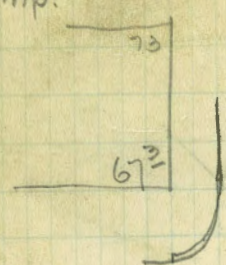
61.5

1.5

2 1/2" N - S.E. cor - cut 1' 7" nail ctr.

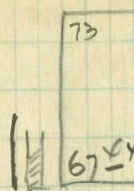
SW ✓ - 1' 6" spx ctr.

Imp.



7X

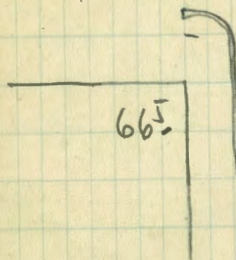
28"



4
 0 23
 0 8
 0 8
 0 8

N. St

for type 2-10 ft.



66 1/2

40

68

73
 2.22
 74.22
 0.3

6.67

67.55 ✓

67

66

67.26

5.13

5.11

67.26

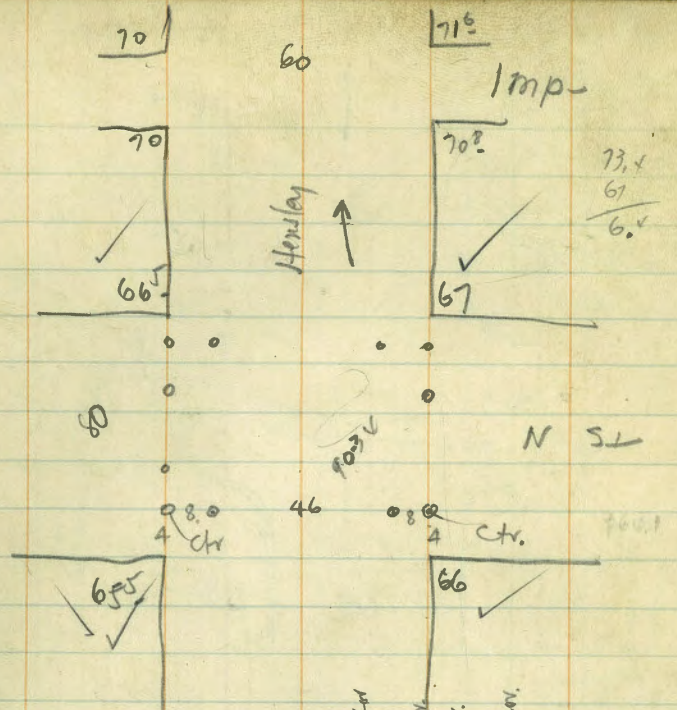
67.29

67.27

J.18

72.67

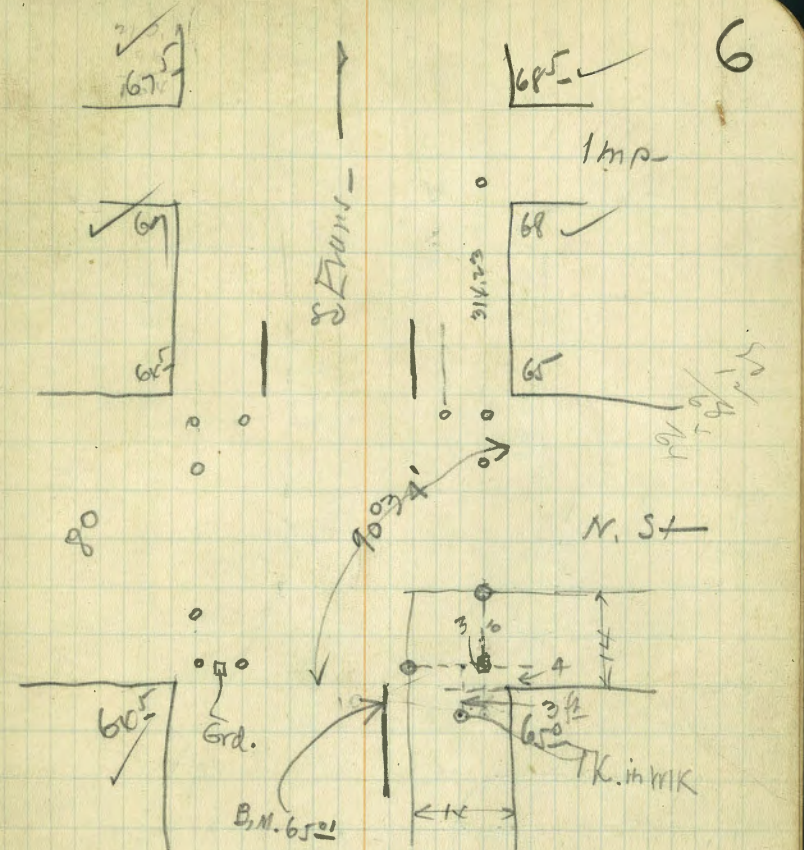
2 1/2" / 3/8"



3.40	70 =	73.40	41.
76		70.80	N.W.
1.75		71.65	N.E.
76		70.80	S.E.
73.40			
65.5		7.9	
66.1		7.4	
66.5		6.9	

65.01	S.E. BM
65.50	S.W. S.K. Ch
66.00	S.W. S.E. Cor.
67.	S.W. N.E. Cor.
66.50	S.W. N.W. Cor.

4.70	69.11
------	-------



4.65	69.66	65.01	S.E. BM
65.01		64.95	N.E. Cor.
4.14		4.90	N.W. Cor.
69.20	HI	5.16	S.W. S.K.
64.76			
26	cut 3		

B.M. N.W. - 27' + Imp - 63.92

4.31	68.23 ✓	63.99	
	3.23		
4.66	69.66 ✓	65.00 ✓	
	5.05	64.61	S.W. - 27' + Imp
	4.10	64.86	N.W. - ✓
	4.19	65.47	N.E. ✓
	4.69	64.97	S.E. ✓
	7.55	62.11	Mon. B.M. - 27' + N
7.20	69.45	64.46	
16.71	4.99		
.54	15.97		
63.92			
64.46			

Imp.

11088

69.15
5.37
63.78

4.99 70.00
7.40 70.07
4.66 69.15

17.05

18.13

1.08
65.01
63.93 ✓

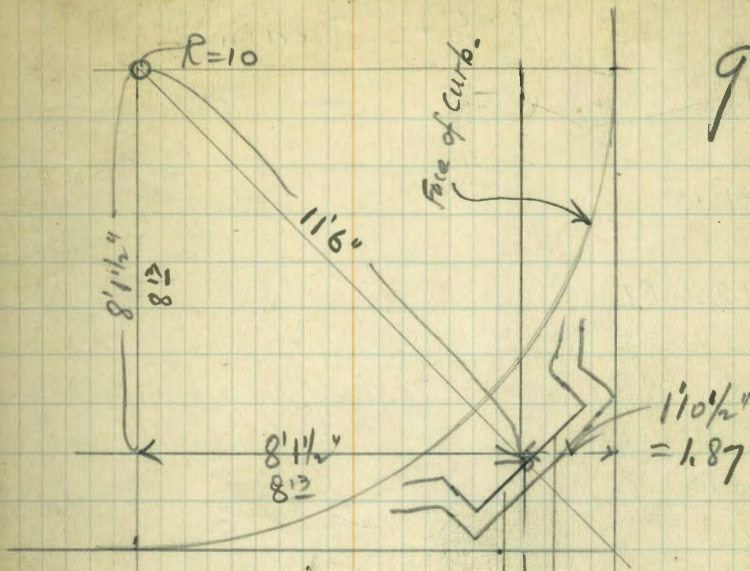
B.M. -
6501 S.E. Evans + N.
733 62.67 Mon. - 27' + N.
558 64.49 T.P.
522 63.93 B.M. 63⁹²

Check Levels - "N" St
Imp. Pr.

Mon - 27" + N. St.	62.67		
7.27 69.94			
5.94 64.00		N.E. Stk	
6.37 63.63		27" + N.	
5.84 64.50		N.W. ✓ sm	
4.92	65.02	S.W. Error	4.72
			65.01

6.30 71.64	614		
	61.50	✓	
✓ SE ✓ 5.63	66.00	✓	
✓ NE ✓ 4.63	67.00		
✓ NW ✓ 5.14	66.50		
Curb - S.E. 28" + N	4.94	66.70	ck

7.86 74.56			
S.W. 29" + N.	4.28	70.28	
		4.78	cut 1' 9"
		68.50	
S.E. do	3.91	70.65	T.P.
		1.85	cut 1' 10"
		68.8	
4.32 74.97			
	3.33	71.64	T.P.
			SE 29" + Imp
5.53 77.17			
	5.08	72.09	TP
6.84 78.93	3.87	75.96	B.M.
			74.97



Location - Type G. Inlet.

$$\frac{10}{813} = .87$$

Imp.

11088

27" + N.
8/17/27
Mg

"N" St. Drain—

Sta + π - El. El.

Grade ³⁴⁶ 0 -

Def.

6-30- 25

13-00- 25

19-30 25

26-00 27.2

10

~~107.9~~

20+19.10

60.7 X

21+21.8 P.T.

60.29

22

59.98

+50

59.78

23

59.58

+50

59.38

24

59.19

+50

58.99

25

58.79

+50

58.59

26

58.40

+50

58.20

27

58.00

+50

57.80

28

57.60

+50

57.40

29

57.21

+50

57.01

30

56.81

+50

56.61

31

56.42

+50

56.22

32

56.02

+50

55.82

33

+50

34

+50

35

+10! E.L. Henley

+50

+70! M.L. Henley-

36

+10! 0

+50 0 9/2

37

+50 0 x

+94 E. L. Evans-

38

+32

+50

+86

5.95

70.96

560

65.01
65.36
73.81
11.55

3100

5.20

70.21

466

413

4.17

65.01
65.55
53.61
66.08
50.14
66.04
52.40
11.64

5.71

70.22

454

36+50

65.01
66.18
54.14 C 12.04

3.74

68.75

3.10

3.75

3.73

3.45

3.74

3.75

B.M. -
65.01 Evans & N.

65.65 C. 11.2

65.50 C 11.4

65.53

65.30 C 11.5

65.01 C 11.5

65.06

1.5
2.2

654
662
1016
658

55.62

55.43

55.23

55.03

54.83

54.63

54.44

54.40 X

54.14 Grd 0 653

53.81

53.49

53.20

53.16

52.94

52.83

52.60

4.65

69.66

Grd 39+13
5.62
Grd 38+26

4.80

69.81

77.94

4.89

69.89

78.34

5.89

4.19

69.20

4.22

5.76

4.07

3.81

65.01
64.01
52.92 C. 11.58
64.04
52.60 C. 11.44

65.01
63.91
53.20 C = 10.2

64.12
57.44
64.80
52.96
11.06

65.01
65.08
53.20
11.88
64.06
52.45
11.15
65.13
53.49
11.64
65.39
53.81
11.58

12

		68.75	-		
34	o	5.38	63.37	C 10.9	
+13					
+50	o	5.44	63.38	C 11.1	
+94.7	o 9/18	Ang. Pt.	L 2°54'	L 6.05	62.70 C 10.9
40					
+50	o 9/18	6.22	62.53	C 11.0	
41	o x 9/18	6.31	62.44	C 11.2	
+57	o 9/18	Cleanout	6.55	62.20	C 11.4
44	o 9/10		7.03	61.72	C 11.2
+50	o x 3.01	63.87	7.89	60.86	P. 9.10.7
43	o x	L R-1-46	3.41	60.46	C 10.6
+49.7	o x	L R-1-46	Cleanout	3.46	60.03 C 10.4
44	o	3.60	60.21	C 11.1	
+50	o A	3.52	60.35	C 11.4	

79 3.64 68.65 7.32 65.01
60.93
51.53
9.40
67.27 61.28
51.53
19.85

5.12 62.83
51.84
10.98
5.39 63.26
51.85
11.41
5.37 63.28
52.18
11.10
5.43 63.22
52.18
14.04

3.13 61.14
6.04 62.10
5.77 62.55
5.08 63.06
5.18 62.96
11.86
51.20
11.76

16.18 48.54 = 45.00
6.66 66.47 59.81
1.47 65.11 B.M.
5.70 60.77
49.57
11.20

5.27 59.81
60.05 11.13
48.92 Grade
4.96 60.36
11.46

39+94.7
2-52
2-50
3-20
1-26
43+00
1-44
43+49.7
1-36

Franklin

48+ — 57.89
 + 6.51
 x 60.40
 47.94
 — 16.46

37.36 .64
 +
 6.18 60.08
 53.10 14

63.87
 45 x

64.40
 47.53
 16.87
 12
 4.87

48.59

+50 x x
 +60 x
 63.10
 48.20
 14.90
 12
 4.87

60- 11.8

48.26

48.20 +

Sta-72+73 =
 cut 5.8

x6

47.94

4.89 49.53
 48+10 3.23
 48 2.90

+50

47.61

+62 1/2 W.L. 76" St. L 4 0 2 1/2

4.6 19.3 C11.8

47.53

5.79 56.43
 stakes - mark H to high - 1/4 47+50 3.47
 46.64
 46.30
 46.63

47 0 0

5.19 58.68 C11.2

47.28

+50 0 x Set Grd

5.75 58.12 C11.1

46.96

stick - 6.65
 5.24 63.92
 53.93
 9.99

48 0 Set Grd

5.98 57.89 C11.3

46.63 ✓

+50 0 Set Grd

6.37 57.50 C11.2

46.30 ✓

49 0 ✓ Set Grd

7.26 56.61 C10.6

45.98 ✓

+50 0 ✓ Set Grd

8.50 55.37 C9.8

45.65 ✓

8.6
 10.03
 49.59
 47.1

50 0 Set Grd

8.78 55.09 C9.8

45.32 ✓

-3.39
 50.11
 5.47
 5.78
 53.10
 46.64 ± cond.
 46.83

+57 = Exist. 4x4 Drain -
 Top - 10.39

53.50

44.92

4.79
 4.46
 45.37
 45.65

464 98.94 SW
 9430
 93.2
 50
 12.8
 719 91.75
 75.64
 13.11
 8.65 90.30
 78.44
 11.86

SW
 266
 2.57
 8.35

2105 85.57
 SW 10+ 75.28 c 10.29
 0.70 86.9
 SW 9+10 76.7 c 10.2

Grade

7.71 100.51
 7.58 92.93
 6.20 93.30
 6.60 93.70
 81.9
 11.8

15

6.12 98.87
 5.57 93.30
 46 94.3
 7.12 91.45
 7.22 94.75
 8.15

5070
 106
 7964
 153
 78.11

6+96¹ E.S. 4. out.

9430

84.0

C. 7.5 = 7'-5"

8'2"

7+71² B.C. x
 7+82

6.12 93.30

81.9
 81.8

C 11.4

5.09 99.39

9430

7.63 92.75

S.C. 5.22

94.17

8+10⁶ E.S. on Cb. PL.

1.43 94.30
 93.95

80.70
 2.34
 80.36

C 13.6
 13.2

5.22
 4.70

94.70
 4.69
 99.39

07 9+ x in.

6.12 89.26

79.64
 78.44
 78.14

C 11.1

5.22
 7+71.2 93.80
 81.9
 11.94

07 9+50

7.62 87.76

143
 95.98
 76.71

11.0

6.25 93.10
 7+82 81.6
 11.54

05 10+

9.15 85.53

75.28
 143

C 10.2

95.38

11297
11+20
10 72
72

4.96 82.37 77.41
12+50 = 67.58 4.53 77.84 = 12+50
10.42 4.37 73.00
13+ = 65.89 5.25 77.12
11.23

Grade

7.23 85.90 78.67

16

7.57 78.33
415 7046
81.75
72.42
9.23
1.74 84.08
73.57
10.51

0310+50 9/12/17
12.26 95.38 0.52 83.02 TP

73.85
1.43
2.42

0311+ 9/12
1.79 81.75 72.42

C 9.7
C 7.7

5.86 74.22 68.36

+37 Mcb h. K. St

11+ 50 9/12

12

Mcb h. K
S v v

4.67 78.69
6.18 77.61

71.60
70.96

0512+50 5.7 77.82 67.58

C 10.2

61.24
48
60.31

13+

65.89

+ T - E1.

6.0x 67.41

013+50 8.42 75.12 64.21

C 10.9

0514+ 9.94 83.54 0.38 73.60 TP 63.22

C 10.4

4.80 68.65
338 67.58
1.69 18.9
9.22

0514+50 1.77 72.21 64.26

C 9.9

4.37 69.18
65.89 58.35
10.83

0515 +15 M. v S. Coline. Lsv 5.00 68.98
5.62 68.36
6.59 67.41

61.29
- 61.01
1.67

C 7.7
C 7.4

4.90 68.55
57.37
11.18

0516 5.22 68.76 59.33

C 9.5

0916+50 A 5.01 68.97 58.35

C 10.6

73.98

196 9/12

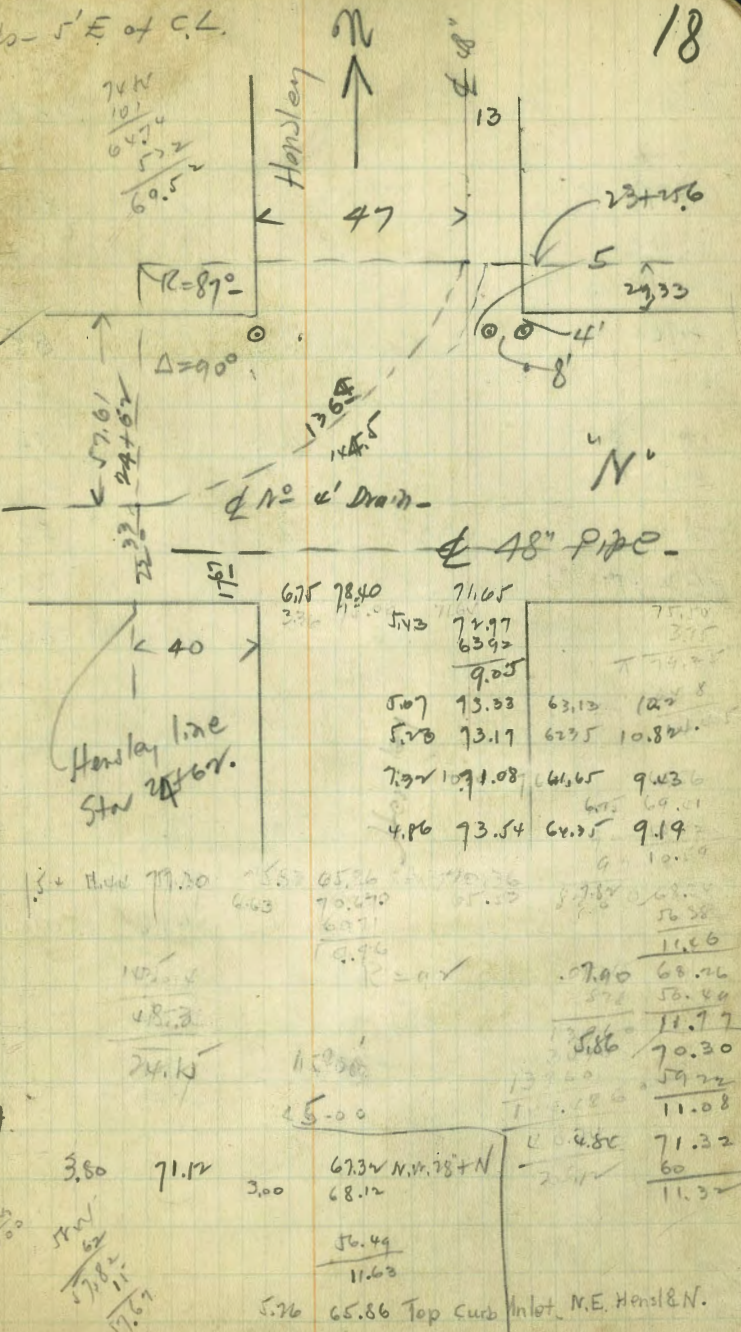
122	19+60 140 21+00	+	π	36 12 48	El.
0517					7.78 66.20
0517+50	x				6.09 67.89
0318+	x				7.48 66.50
0518+50		8.48	73.93	0.77	TP 65.50
				1.60	64.47
18+95	N.C.B.L. Imp. 210			5.89	60.38
19+47	S			6.86	59.41
0520+	10			3.87	62.40
		7.50	66.00	58.94	EM.
20+50				5.22	61.05
0521	x			6.71	59.56
21+50				8.37	57.90
0522				10.12	56.15
22+50.6	N.L.N'ST.			11.20	55.07
23+38.6	End				
		7.33	66.27	58.94	
					NE 15' W

Grade	cut	53.60 33 53.27	55.41 11.08 6.51	Tap 4x4 Drain	55.97
57.77	C 8.8		6.51	60.01	12.51 x 7.50 x 9 C 2.6
56.39	C 11.5				8.55 51.06 x 5.33 C 6.13
55.41	C 11.1	1.96 0/6			
54.43	C 10.0				46.00 10.00 56.00
53.60	C 6.8		10.30 4.64		44.90
52.60	C 6.8		14.94	59.84	70.2
51.56	C 10.9		6.22	59.72	53.50 58.52
50.56	C 10.0				0.22
48.60	C 9.0	1.96 0/6	4.87	65.27	60.38 64.48 54.43
47.67	C 8.5				0.79 10.84 33 11.17 15.00 10.19 9.21 53.27 55.08 56.06
46.47	C 8.6				18.00
44.9					4.37 54.90 47.62 7.10 47.27 7.45

Hensley St - Line

Stns - 5' E of C.L.

Station	Offset	Elevation	Grade	Notes
17+54.9	P.T. □	73.55	65.40	8.7 C 8.1
18+	□	73.27	64.70	9.0 C 8.6
+50	○ ✓	72.50	63.92	C 8.6
19+	○ ✓	72.78	63.13	C 9.7
19+50	○ ✓	72.64	62.35	C 10.3
20	○	71.01	60.00	C 11.0
+50	○ 19 1/3	70.19	59.22	C 11.0
22	○	69.24	58.44	C 10.9
+50	○	69.13	57.66	C 11.4
23	○		56.88	
1		73.76		



23 5.22 68.04 56.88 C 11.1

23+25⁶ P.S. 5.4 67.8 56.49 C 11.1

23+45 @ 10% 56.18

23+94 P. X under 14" Semu = 65.98 55.43 C 9.3

20 55.33

+ 22 P.O.C. 7.05 66.21 55.00 C 11.2

+ 50 54.54

24+14 55.16

462 P.T. 54.40

8.25 73.26 65.01 B.M. Frons + N.

2467 P.T. 54.40

6.25 81.95 75.50 S.A. Horsley + L.

3.96 78.

4.59 77.38

67.6 Grade & L.

67.6

65.9

11.05

67.6
65.9
1.7

5.55 70.56 65.01
9.20 61.26 T.V.P. 19
1.33
59.93 But pipe

2.76 68.30
27+45 = 56.18 C. 12.12
3.48 67.08
27+65 = 55.88 C. 11.20

5.04 65.52
T.V. 24+14 = 55.16 C. 10.36
27+76 = 68
27+94 = Semu - & N. 54
27+62 = 68
4.14 66.02

Sta 17

14.44
1.77
15.16
10.00 75.86 65.86

6.47 78.46 4.37 71.49 Cont. N.E. Horsley + Imp

7.50 70.66 S.E. Horsley + Imp

5.44 73.02 19+50 62.35 C 10.67

23 = 56.88 5.29 = 73.17
+ 44 = 55.43 19+00 63.13 C 10.04

1.05
54.38 7.60 70.86
& Imp = 61.35 C 9.51

281 St- \leftarrow M.V. 28+K

5.53 91.53

86.0 86.0

74.4

070	M.L. K. St		86.0	74.4	C 11.6
+					
00		5.37	86.16	75.19	C 11.0
1+		5.27	86.31	75.98	C 10.3
10		5.09	86.44	76.77	C 9.7
2+		4.95	86.58	77.56	C 9.0
60	Inter. Cont. \leftarrow 86.81	4.58	86.95	78.56	C 8.4

M.L. K. St 0+00
 ✓ 0+35
 S.L. ✓ 0+60

4.41 90.41

4.65

86.00

85.76
 73.9
 11.86

1.50%
 74.4
 73.9
 73.4

20

5.01 91.01

86.-

9.71	81.30
	74.25
	7.05
4.93	86.08
	72.3
	78.85
	4.12
	74.73
11.18	79.83
	73.9
	5.93 C.
5.23	85.73
	73.4
	12.3
6.45	84.56
7.75	11.3
6.3	73.26

Ek

$$0+10 = \frac{74.4}{15} = 0+10$$

$$10.58 \quad \frac{80.43}{44} = 76.0$$

$$.33 \times 760 = .81$$

$$.33 \times 100 = \frac{13}{100} = .13$$

$$605 \quad \frac{13}{100} = .13$$

$$6.5 \quad 4.96$$

86.-

87.09
 86.87 .22

69
 44
 113

16 + T - El.
 S.M. Hensley & L. 75.50
 6.73 82.23
 11.82 70.61 Bot. 16" C.L.
 Water Main -

Allow 48 cu. yd. lowering Grd. 48" pipe -

17 5.5 76.7 65.25 Grad
 11.5

See page 32

574

72

517 70.18 65.01
 12.32 57.84
 62
 F 6.16

11.41
 10
 13.31 56.87
 632
 6.33

12.22
 2
 14.22 55.96
 62
 6.04

Grd. of Clew 74³

5162 81.14 75.50 S.M. Hensley & L.
 7.18 73.96
 723
 .34

grades at $\&$ Track Crossings

N.W. 26th & N. E. side 26th 27

curb
El. 60.0

26th

curb 59.0

55.0

34'

grade at $\&$ = 52°

60'

49.8

N.W. 27th & N. E. side 27th

curb 64.0

curb 63.6

58.2

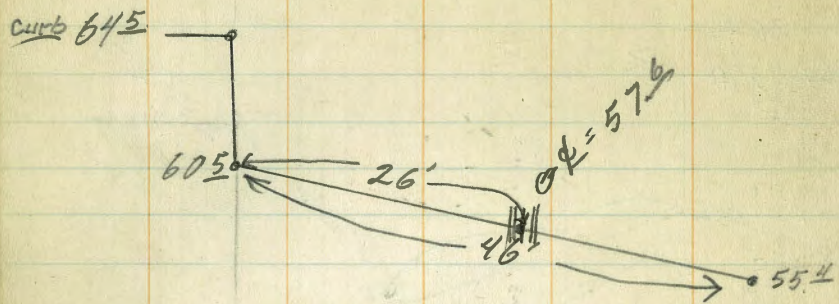
26'

grade at $\&$ = 56°

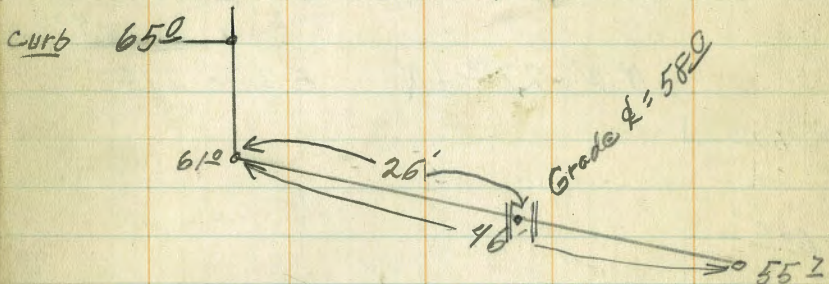
46'

54.4

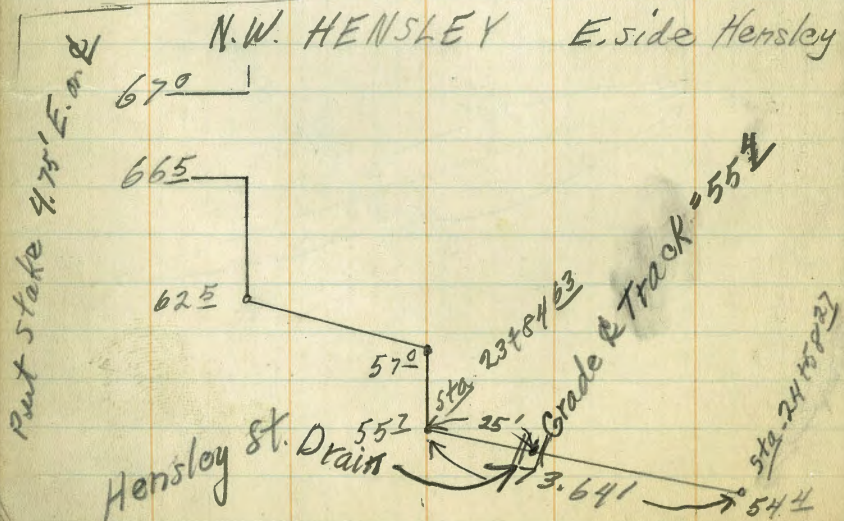
N.W. EVANS + N



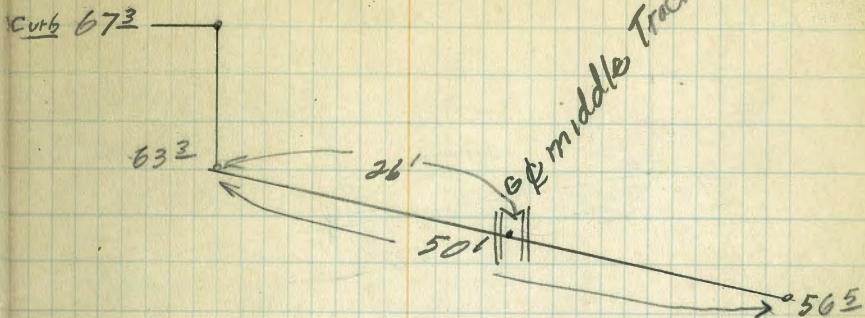
N.E. EVANS + N



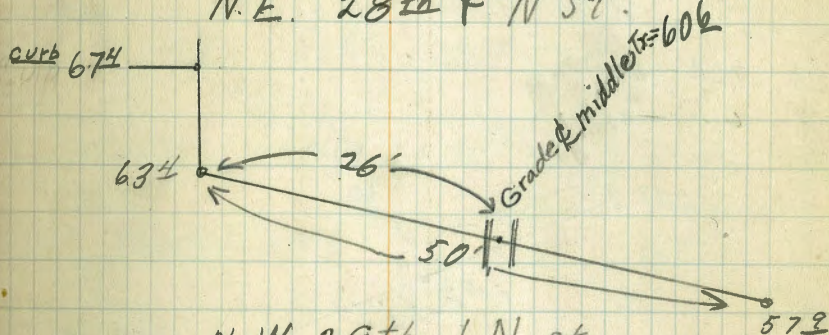
N.W. HENSLEY E. side Hensley



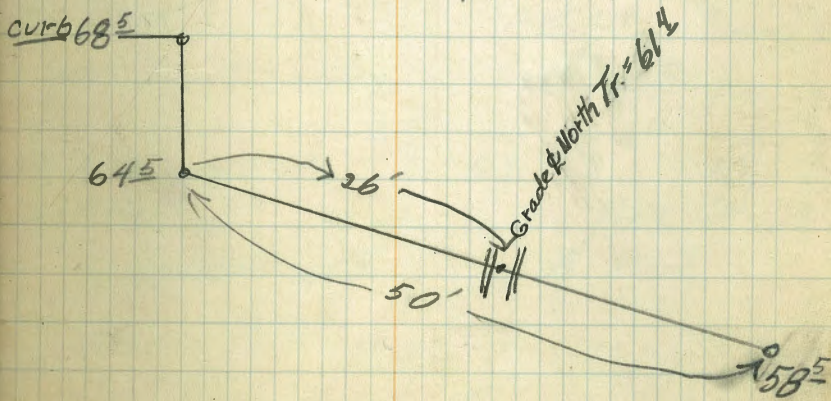
N.W. 28th + N



N.E. 28th + N st.

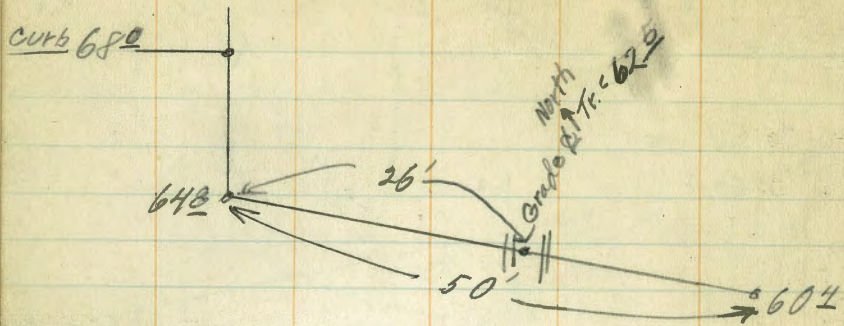


N.W. 29th + N st.

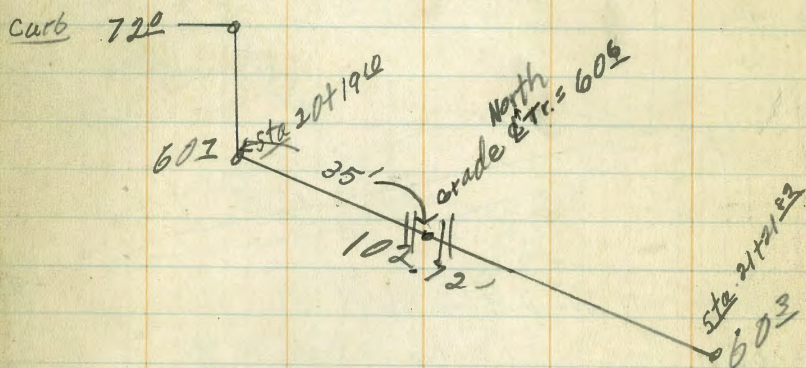


24

N.E. 29th + N St.



N.W. 30th + N St.



Track is 2' South of Road

Butzine &
DAVIES 25

Cut stakes

N.W. 26th St. & Track	4.64	63.64	59.42
grade = 52°		cut 7 1/2	
N.W. 27th St. & Track	3.71	68.72	63.54
grade = 56°		cut 7 1/2	
N.W. Evans St. & Track	4.21	69.22	64.27
grade = 57 1/2°		cut 6 1/2	
NE Evans St. & Track	5.11	70.12	64.54
grade = 58°		cut 6 1/2	
N.W. Hensley & Track	5.48	70.02	65.83
grade = 55 1/2°		cut 10 1/2	

B.M.
S.E. Evans

B.M.
S.E. Evans

B.M.

& Tr.

Fl. 24" Pipe under Marker St. 110.25

3.16 113.41

2.29 111.02 \pm Alley -
 $\frac{5.45}{106.}$ Grd \pm Alley -

1460

9.48 103.93 Top Sensor -
Make Fl. 104.4

1493

10.02 103.39 Tap

1450

6.25 107.16 Hub -
Grd $\frac{104.5}{2.7}$

N.W. Hensley + N

t	H.I.	-	Elev _{B.M.}
5.61	70.62		65.01

Inlet #13 5.74
 grade = 56.9 Cut 8.3

N.E. Hensley + N
 5.97 71.35 65.38

5.40
 grade = 57.2 Cut 8.2

N.W. 28 + N.
 5.04 72.34 67.3^{curb}

Track 5.16 67.18
 grade = 59.8 Cut 7.4

N.E. 28 + N.
 5.21 72.51 67.3
 Track 4.96 67.55

grade = 60.6 Cut 7.0

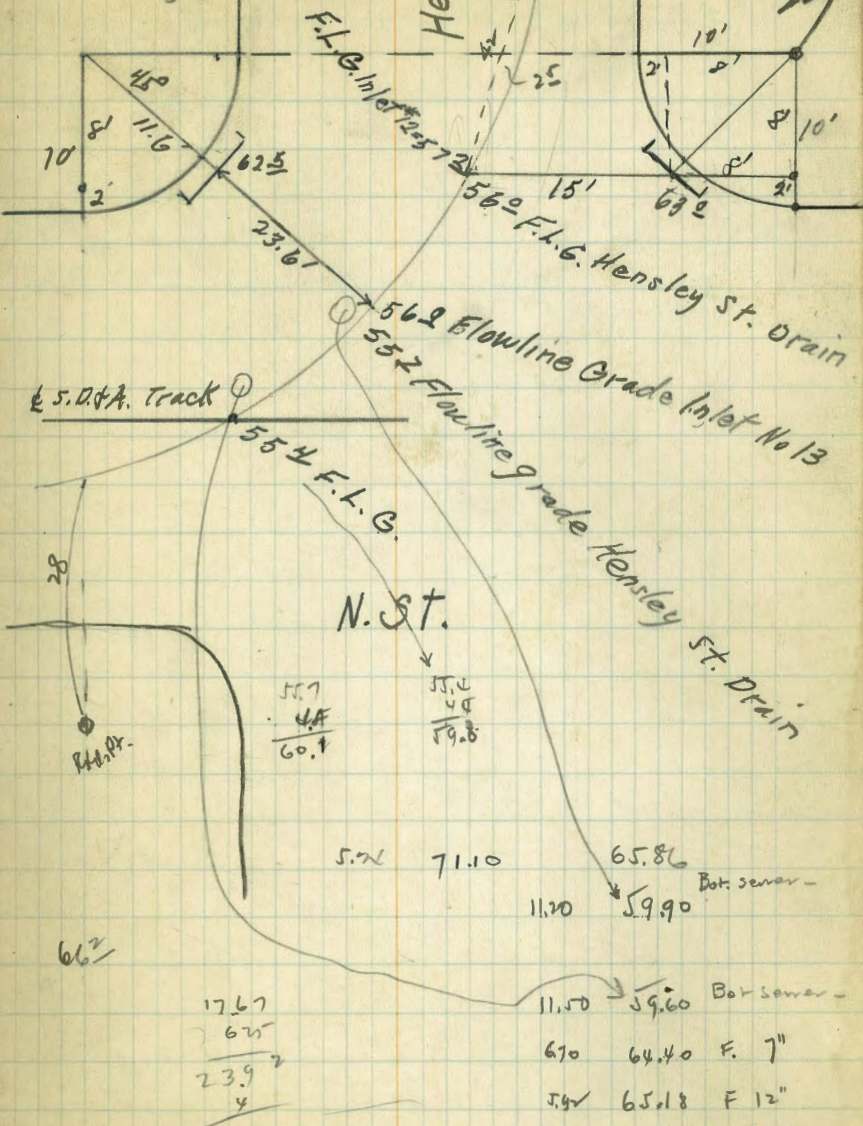
N.W. 29 + N.
 3.10 74.74 71.64^{S.E. 29 + N.}

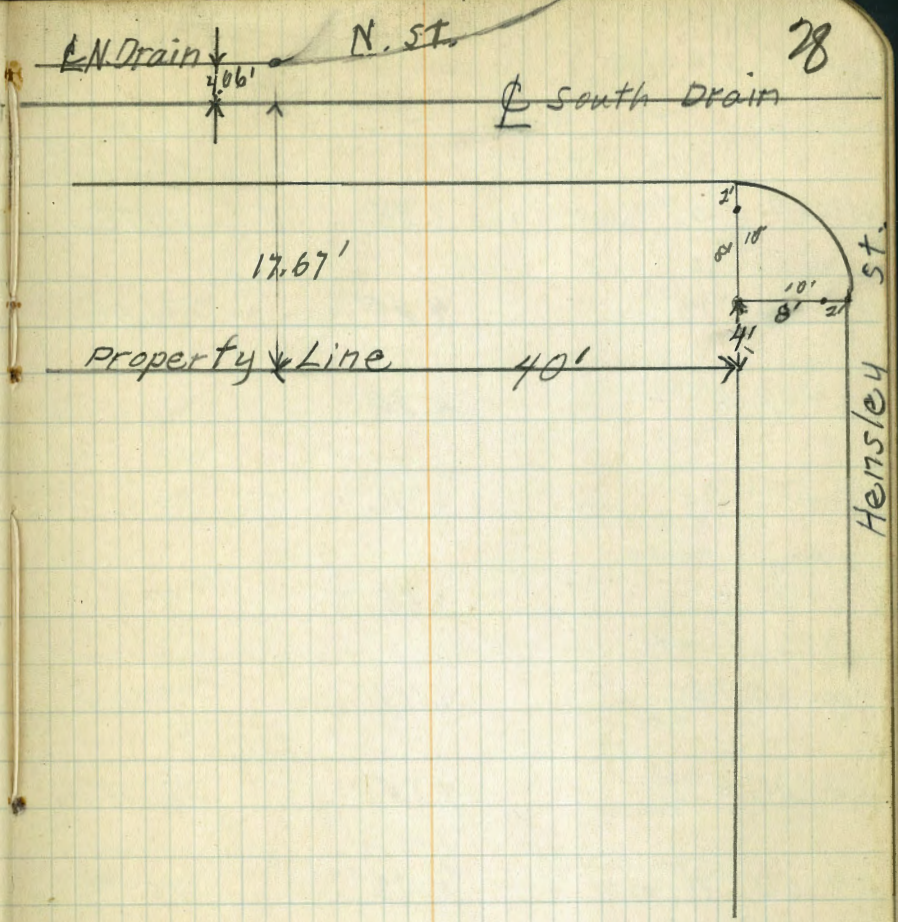
Track 4.43 70.51
 grade = 61.4 Cut 8.9

N.E. 29 + N.
 3.10 74.74 71.64
 4.19 70.55

grade = 62.5 Cut 8.0

N.W. Hensley + N





Butzine, H. π
 Kiernan, P. 29
 29/5/27

Sta.	γ	H.I.	Elev.	grade	Cut
	3.55	75.55	72.00 ^{curb} 30" π		
21+21 $\frac{8}{28.5}$ E.O. $\frac{10}{15}$		3.85	71.70	60.3	11.4
21+50 $\frac{10}{15}$		4.00	71.55	60.18	11.4
22+00 $\frac{10}{15}$		4.00	71.55	59.98	11.6
22+50 $\frac{10}{15}$		4.18	71.37	59.78	11.6
23+00 $\frac{10}{15}$		3.55	72.00	59.58	12.4
23+50 $\frac{10}{15}$		4.47	71.08	59.38	11.7
24+00 $\frac{10}{15}$		4.58	70.97	59.19	11.8
24+50 $\frac{10}{15}$		4.76	70.79	58.99	11.8
25+00 $\frac{10}{15}$		4.80	70.75	58.79	12.0
25+50 $\frac{10}{15}$		5.08	70.47	58.59	11.4
26+00 $\frac{10}{15}$		4.93	70.62	58.40	12.2
26+50 $\frac{10}{15}$		5.00	70.55	58.20	12.3

5.27 π
 72.00
 70.63
 59.79
 71.00
 70.80
 59.38
 71.02
 71.38
 59.58
 11.80
 71.18
 59.78
 11.40
 71.28
 59.98
 11.20
 71.06
 60.18
 10.88
 71.00
 60.3
 10.7
 66.27
 72.03
 10.76
 66.30
 6" Pine
 .8
 66.50
 10.14
 66.92
 4"
 66.4

	H.I.	-	Elev.
27+00 ^{10/22}		5.29	70.26
27+40		5.42	70.13
27+46 ⁶ E.L. 29th			
28+06 ⁶ W.L. 29th			
+40	75.55		
28+50 T.P.		5.45	70.10
299	73.09		
29+00		3.75	69.34
+05			
29+50		4.44	68.65
+76			
30+00		4.84	68.25
+50 ^{10/11/21}		5.12	67.97
31+00 ^{10/11/21}		5.43	67.66
+79			
+50 ^{10/5/21}		5.69	67.40
32 ^{10/4}		6.11	66.98
+50 ^{10/1}		6.60	66.49
33+00		6.45	66.64
33+00.1 E.L. 25th			

27+00
170
292.72
25

27+46
75.8
75.0
2363

109

J.E. 28" + Imp - 71.64

grade	Cut
58.00	12.3
57.84	12.3
57.8	
57.60	
57.44	
57.40	12.7
57.21	12.1
57.20	
57.01	11.6
56.91	
56.81	11.4
56.61	11.4
56.42	11.2
56.3	
56.22	11.2
56.02	11.0
55.82	10.7
55.62	11.0

4%
10%

688
65.0
578
10.2
5.1

3.80

27+46.6
50
2796.6

1295

584

Butzine, H. X
Kiernan, P. Red

30

SE 28" + N. 66.70

NR. 28" + N. 67.22

75.24

75.18

75.91

70.42

71.13

78.24

12.69

71.64

67.24

57.60

9.64

68.00

52

10.1

67.37

65.93

66.80

.87

T.P. J.E. Carb 25' N	73.09	6.65	66.44	grade	cut	
415	70.59					
33+60 ^L W.L. 28 th	70.85	4.02	66.83	55.38	11.4	
34+00		3.87	66.98	55.23	11.8	
+80		3.00	67.85	55.03	12.8	
+70				54.95		
35+00		4.88	65.97	54.83	11.1	
35+10 ^L E.L. Hensley				54.79		
+50		5.40	65.45	54.63	10.8	
35+70 ^L W.L. Hensley						
36+00				54.44		
+10		5.10	65.75	54.4	11.4	

π
 $\frac{65.76}{-5.92}$
 $\frac{59.84}{55.92}$
 $\frac{4.00}{55.63}$
 $\frac{3.81}{15.79}$
 $\frac{3.65}{57.95}$
 $\frac{3.69}{78.6}$
 $\frac{56.62}{56.62}$
 $\frac{56.62}{56.03 = 34 + 50}$
 $\frac{56.23 = 34$
 $\frac{56.43 = 37 + 10}$
 $\frac{2.65}{2.65}$

f	H.I	-	Elev.	Top of Drain		
-3.71	49.79		53.50		55.23	45.98
					54.83	49.79
					.40	45.98
4.96	76.96				55.02	3.81
					.08	49.79
					55.95	45.65
						4.14
						49.79
						46.30
						3.49

$\frac{72.03 \text{ m.w. } 70' + N}{65.22}$
 $\frac{4.2}{61.0} = 62.7$
 K.L. 10' pipe
 culvert

371 78.68
 74.97
 $\frac{72.03 \text{ m.w. cor. } 30' + N}{6.65}$

	+	T	-	
16+20	-1.02	69.38		70.40

Bot. 16°C. 1-
water
on L. St.

16+27	Gl. main	Sub. Grd.	Nov 65.36	65.1 65.5
-------	----------	-----------	-----------	--------------

17			6.93	65.65
+30			5.20	64.85

+50	P.T.			64.36
				86

18+50				63.5
-------	--	--	--	------

9.03	84.53	75.50
------	-------	-------

16.9	67.6
------	------

15+62	P.T. Grd - 68.5	16.7	67.8	Sub Grd
-------	-----------------	------	------	---------

19.2	65.3
------	------

6x15
27
64.58

17
73
27

4.22	11.96
9.50	11.43
13.95	13.89

9.27
13.89

105
90
15

187.50
16+27
22.3 = .9
2

32

69.38	69.38
65.1	64.18
4.28	5.20
	4.5

S. W. Hamley + L.

3.11 78.61

13.59	64.72
13.05	64.66
6.07	72.54

18+50 = 77.50

28" St - Se of N.

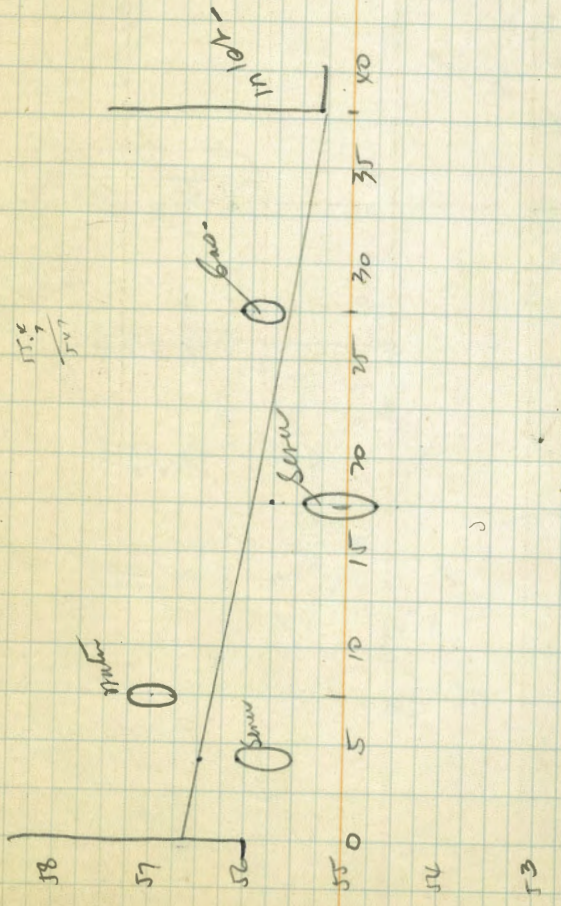
33

			Cut.	Grade
0+00	S. Co. Webster Ave - Ch. Pl. 692		4.5	64.50 1.21
0+52	N. Co. Webster El. 682		3.1	63.29 1.12
1+				62.17 1.16
+50				61.01 1.16
2+				59.85 1.14
+66	S.P.L. Valley Pl -	67.4	7.7	59.71
+73.6	N. Co. L ✓	67.2	8.2	59.01 1.23
+46	N.P.L ✓			58.78 1.26
3+				57.53 1.24
+66	S.P.L. N. St	66.7	10.7	55.981
+83.7	= 39+45' - 48" Drain -			55.601
SE cor 28" + N. 662				8.90
				382
				2320%

M.E. 76" + N		60.00
u. 54	6x. 54	
0+00 F.L. Inlet-	8.58	55.96
0+04 Tap Sewer- 4"	8.39	56.15
0+07 ² Tap 4" C.I. water-	7.37	57.17
0+17 Tap 6" Sewer-	9.10	55.46
0+27 Tap 4" Gas-	8.43	56.11
0+38 F.L. Inlet. W.S. 76" St.	9.27	55.27

56.15
- 25

56.20



55.4
- 5.27

55.27

• Grid main 47.5

260

30.87

1000
4.2026

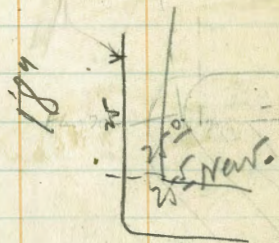
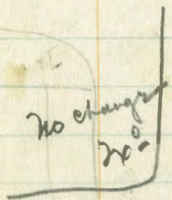
9.1x

26.23

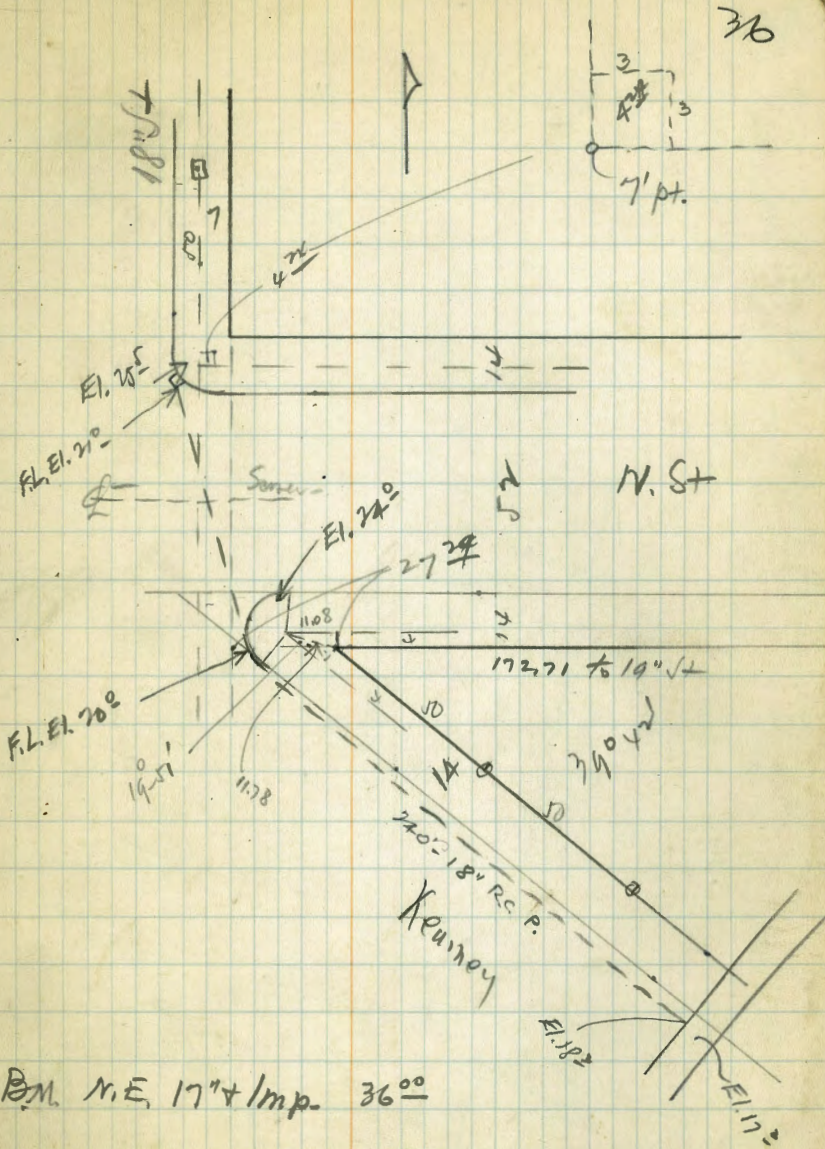
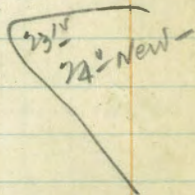
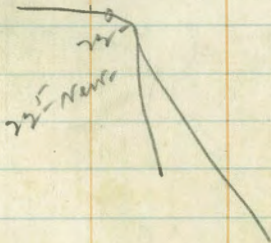
21.73 Top Server -

1.9
20.8

19"

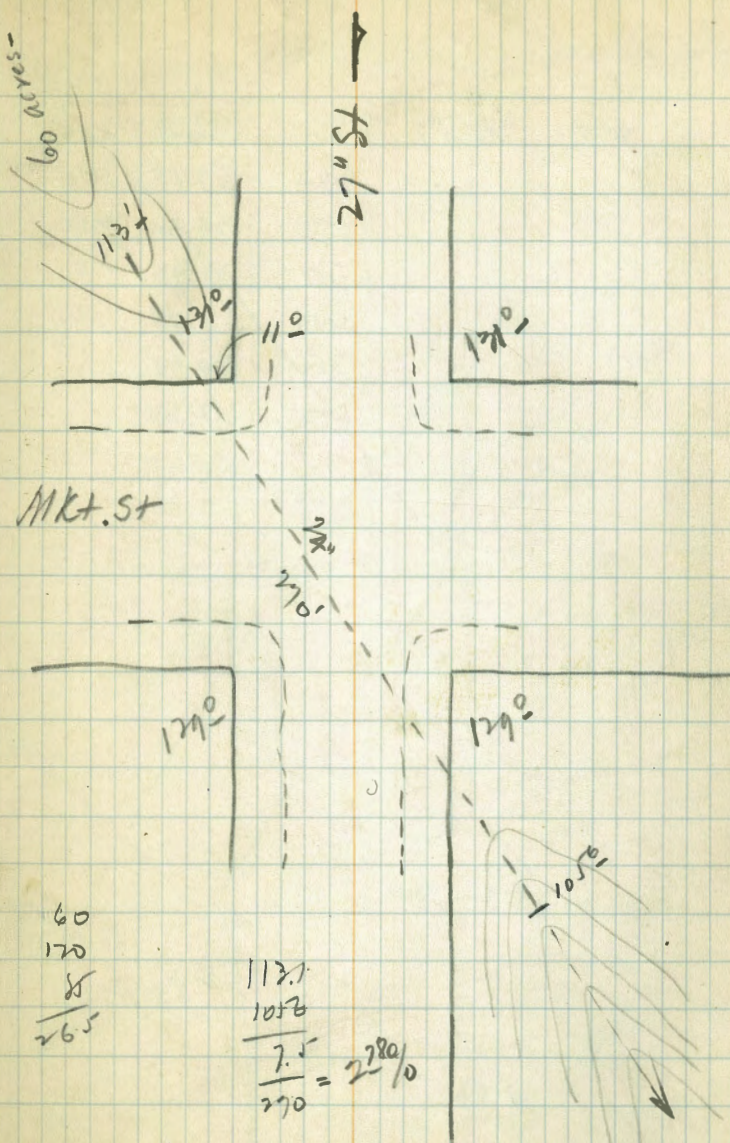


Kearney N



11.3

39



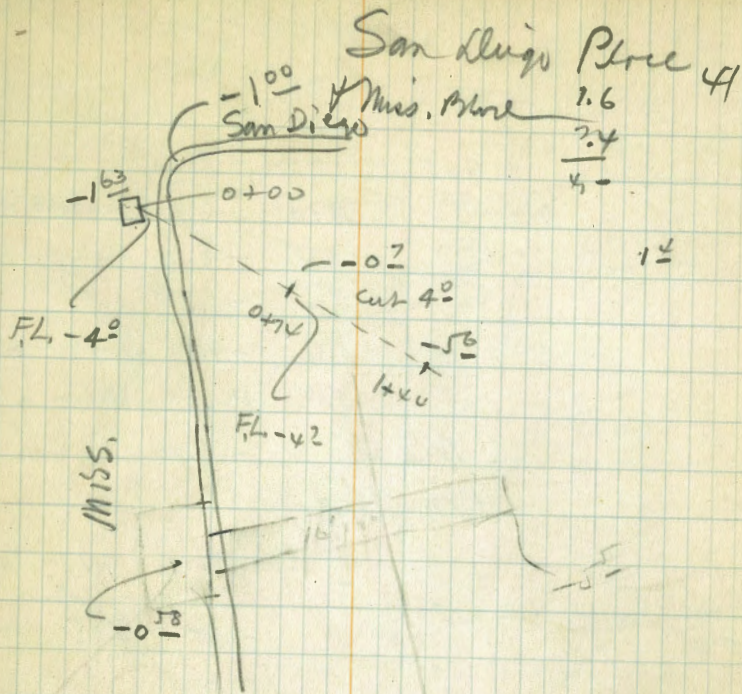
60
170
8
—
265

1131
1058
—
7.5
290 = 2780/0

2nd line 40 c.f.s. probably large enough —

2/12/1917

5.37	+4.37	-1.00	
6.00	-1.63	0+00	
5.1	-0.7	0+70	
10.0	-56	1+24	
4.95	-.58		



cut 2°

Bar - 4

1/17/28 DLB

6.40 + 4.90

1+58
35
1+23

6.11
1.73

5.88 + 4.38

0+00
0+20 curb
0+40 curb
0+60
1+23

1+58 1/26/28

2
+50
3
3+41
3+60
4
4+37
5+

Mark

6.55	-1.50		
6.70	-1.65		
6.-	-1.10	mark	
5.40	-.50		
5.40	-.50		
5.04	-1.50		
	-.66	Tie	
		Grade	Cut.
5.27	-1.73	-3.2	1.67
5.34	-.89	-3.46	2.57
6.15	-.96	-3.53	2.57
5.48	-1.10	-3.58	1.81
		-3.60	2.30
		-3.90	
5.58	-1.20	-4.13	2.93
5.43	-1.05	-4.26	3.71
5.19	-.81	-4.41	3.60
4.44	-.56	-4.59	4.03
4.69	-.31	-4.77	4.46
4.60	-.24	-4.92	4.70
4.40	-.04	-5.00	4.98
4.60	-.24	-5.15	4.93
4.84	-.44	-5.27	4.83
		-5.50	
5.16	-.78	-5.50	2.77

1.75% 5.90 + 4.40

0+14
1+20

6.45

8.15

-1.50
-2.05 Grate S. Gabriel -
-3.60 Grate pipe cut. 1.55
-3.75 Top Sewer

43

Deal

1+58

0+00

-34 MISS -

0+60

-15

8 pipes -

Grate

12 pipe

Deal

-4

2+00

37%

3+00

3+51

Positive

3+57

4+37

4+44

5+00

6.50

80

55
3.4
1.6

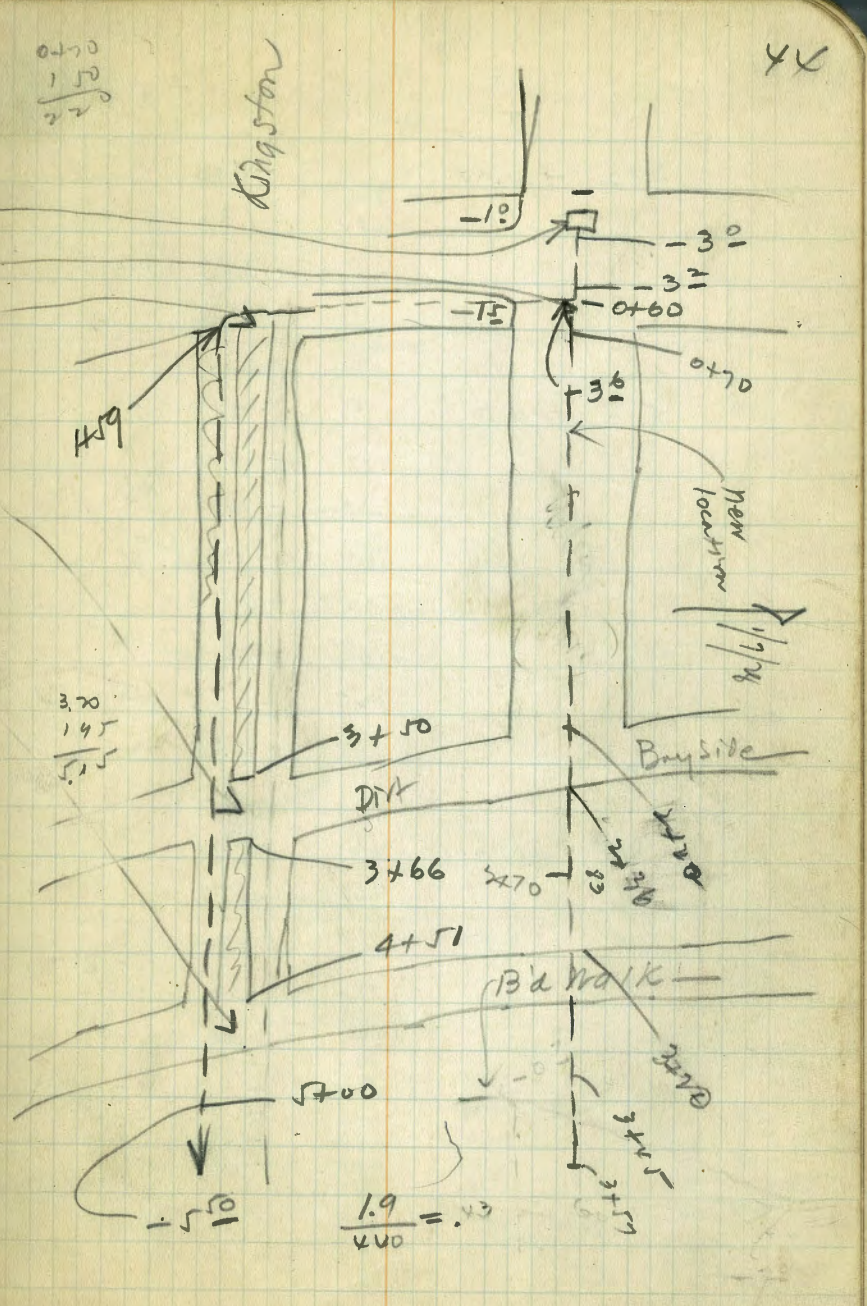
$$\frac{1.6}{4.0} = .363\%$$

.108

4.57
1.8
4.77

Water

501	+3.50	51	-1.50	
		523	-1.6	
		51	-1.73 1470	
		548	-1.6 7420	
		612	-1.98	
		4.20	-2.62 2470	
			-1.30	
557	+4.07		-1.50	
		547	-1.40	
		590	-1.83	
5.00	+3.50	535	-1.50 Gate	
0+30		4.04	-0.54	
0+70		5.00	-1.90	
1+70		4.72	-1.62	
1+70		5.76	-1.76	
2+70		5.14	-1.64	
+30	Top Sewer	8.80	-5.30	
0+70		6.20	-2.70	
3+70		4.85	-1.35	
3+45		4.1	-0.6	
3+59		6.6	-3.1	
0+40	Top Water Main	7.21	-3.71	
✓ curb		4.78	-0.88	
0+70 curb		4.34	-0.84	
2+36		5.55	-2.05	
0+00			-1.40	cut
+20			-0.85	
3+28			-0.88	
+60				
+70	P.L.		-1.90	
1+70			-1.62	
1+70			-1.76	
2+20			-1.64	
2+36			-2.05	
2+70			-2.72	
3+70			-1.25	
3+45			-0.60	
3+57			-3.10	



↑
 4.80 + 3.00 - 1.80
 4.32 - 1.32 Gutter -
 6. - - 3.00 Ditch -

5.00 + 4.50 - 0.50

5.58 - 1.08
 5.38 - 0.88
 5.67 - 1.17
 5.32 - 0.82
 5.3 - 0.8
 6.95 - 2.25
 4.65 - 0.15

n Tie 4.87
 4.56
 + .31
 Grade = 2
 cut 2.31

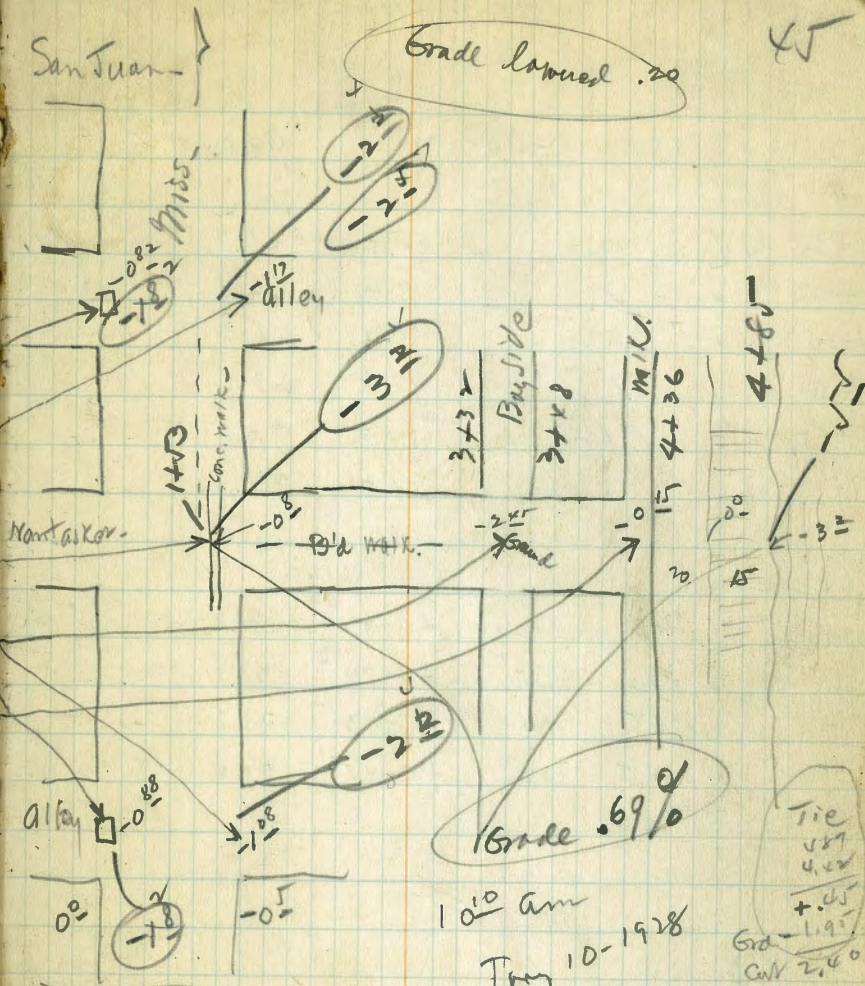
20' E of BANK. 4.6 - 0.1
 7.7 - 3.2

5.27 + 4.87 - 0.50

0+00 }
 0+20 } on
 0+40 } North-
 0+60 }
 1+
 1+53
 2+
 +50
 3+
 +50
 4+
 +76
 4+85

Station	Grade	Cut
5.51	- .64	1.16
4.54	.00	1.90
4.87	.00	2. -
5.84	- .95	2.20
5.27	- .35	2.80
5.30	- .40	+ 3.20
5.85	- .98	3.52
6.50	- 1.93	3.86
7.05	- 2.18	4.31
7.12	- 2.28	4.55
6.14	- 1.27	4.90
5.15	- .28	5.10

San Juan



Allen 0+08
 0+08
 0+08
 0+08
 0+08

on South + 4.87

0+00
 0+20
 0+40
 0+60
 1+
 1+53

10¹⁰ am
 July 10-1928

Station	Grade	Cut
5.60	- .93	1.80
4.90	.00	1.90
4.40	.00	2. -
5.76	- .87	2.20
5.30	- .23	2.37
5.30	- .43	3.00

Tie 4.87
 4.42
 + .45
 End - 1.95
 Cut 2.40

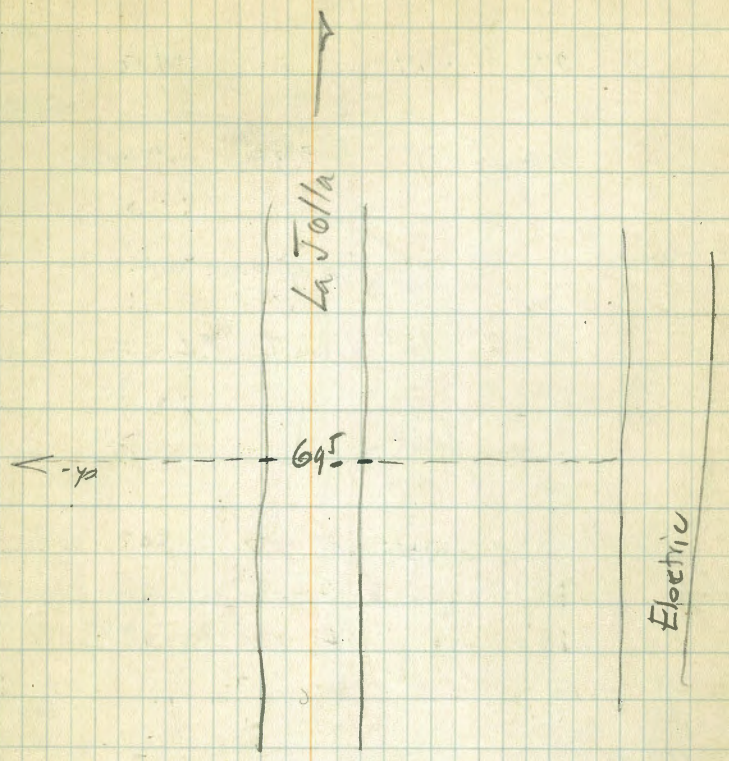
	5.05	74.95		69.50
+30 fr. g. West		5.7		69.2
+50 - ✓ ✓		8.-		66.9
+100 - - ✓		9.6		65.3
+150 - ✓ ✓		11.2		63.6
+50 - ✓ East		4.8		70.6
+ - ✓ ✓		1.7		73.2

(53)

(69.5)

312	209-00	+2-03 ^{11"}	80.7	1/2" Culv. RyTRK
230	235	+1-50 ^{12"}	76.8	ch
165	209	+1-03 ^{3"}	73.3	ch
145	202	+0-45 ^{12"}	71.4	ch Turno S9

1/6/28



52

0.7 101.7

101.0

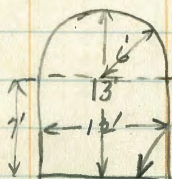
are P...
Turn 5+
100 ft. of Bridge

510 \angle 59° -3° 76.5
70.0

96.5

Top of abut. calc. up for T.K.

16² down to F.L. = 53.7

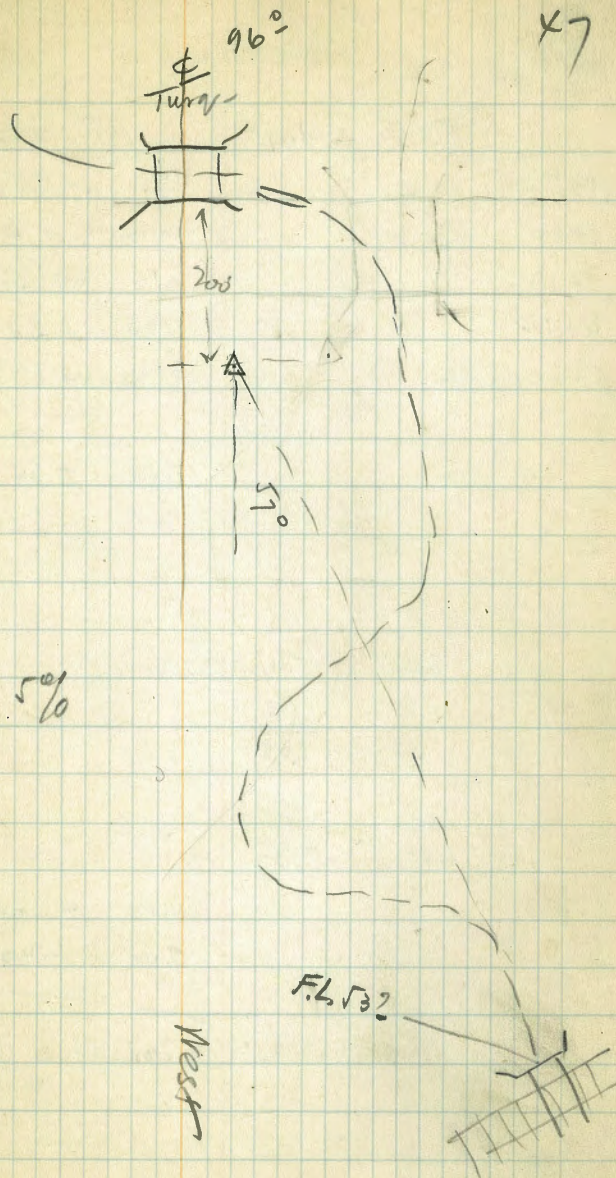


1/6/28

5.96	7.96	+ 2.00
	5.-	+ 2.96

5.05	8.02	6.02
------	------	------

x7



$$\frac{96}{\frac{52}{42}} = \frac{50}{10}$$

Bachan

48

Grade Cur

	5.95	+ 3.05	- 2.00		
1+52	5.50	- 7.55	- 4.50	2.95	
2+52	4.50	- 0.45	- 4.73	4.28	
3+52	3.19	+ 0.76	- 4.96	5.12	
4+52	1.40	+ 2.05	+ 5.19	7.24	
5+52	2.00	+ 1.11	- 5.02	6.53	

5.49 - 1.54 E. curb Rq

5.45 - 1.50 M. ✓ ✓

7.10

5.86	5.11
4.88	98
<u>98</u>	<u>6.09</u>

5.37 + 3.37

4.40 - 1.02 - 4.10 3.07

2.40 - 4.03

Interf. trench

5.86	2.16	- 2.00
		4.88
5.11	8.09	6.09
		2.98
		2.00

6.06 4.06

8.34

- 2.00

- 4.28

1.1
5.38

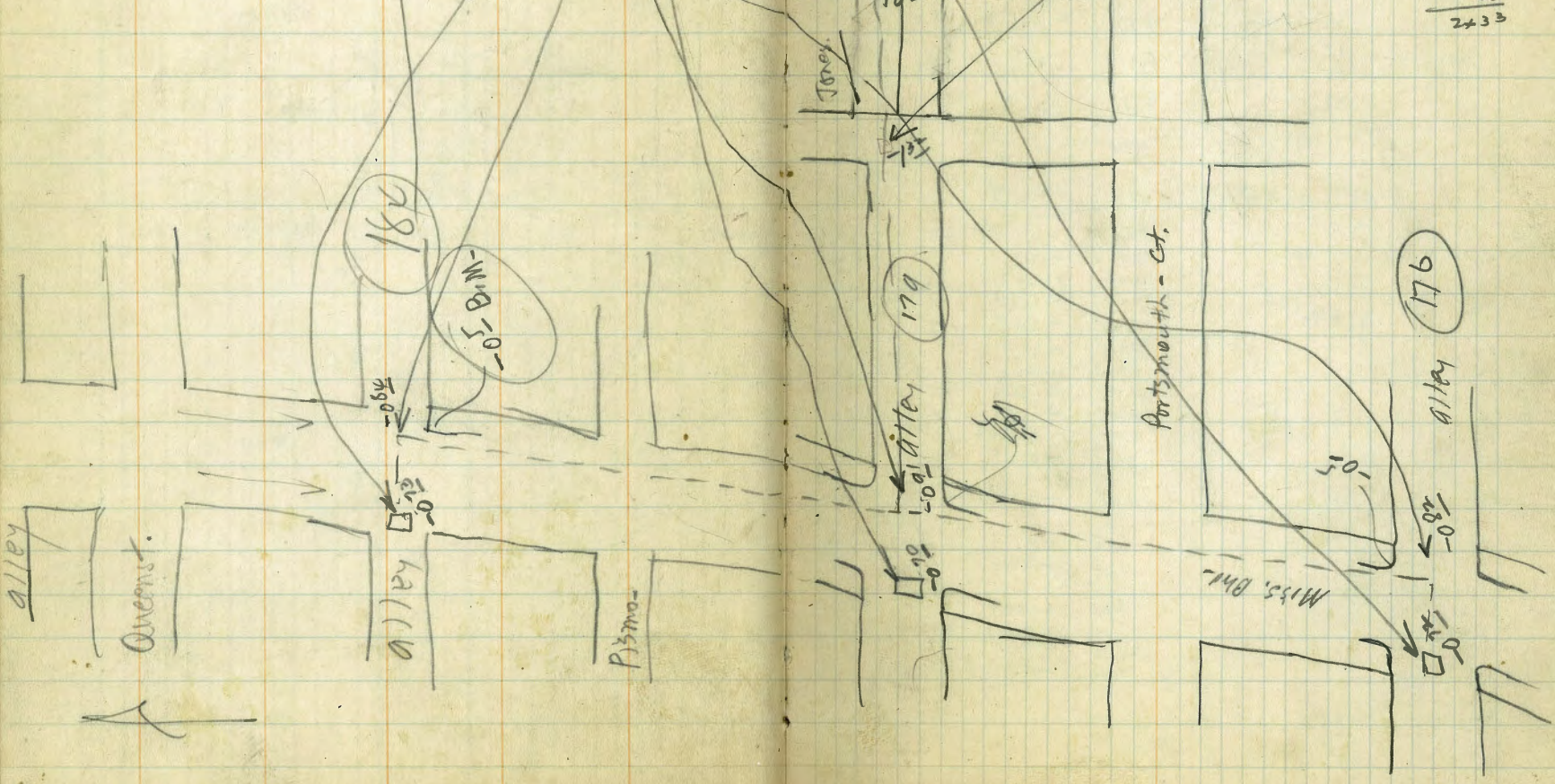
Gr

- 2

7/18/78	5.44	+ 4.94	- 0.50
+ 4.45	+ 4.45	- 0.50	
576	- .81	2433	
578			- 0.84
567			- 0.73
564			- 0.70
571			- 0.91
566			0.72
576			- 0.84

448	+ 4.38	- 0.50
570		1.32
316		+ 0.42
7.00		- 2.62
10.7		- .63

P.L. 1443
 10
 2433



For Scripps Drain - 4th - (Allison)

53

5.27 + 3.59

- 1.80

6.95

- 3.26

F.L. 4th
at Ditch

6.57

- 2.98

F.L. Inlet.

965 to N.L. Alley

456	270.05	5.13	265.92	
5.47	263.48		258.01	N.M. alad Retinson
		5.57	257.93	
			- 14.7	
			243.23	
Grade 76.6 ala.			242.96	c .27
		80' main	242.00	

456	270.05	265.49	B.M.
10.07	260.02		Top
13.47	256.58		F.L. 76'
10.52	259.49		Top
			Cl. water
4.87	265.18		S. Pole
4.83	265.22		N. V
4.88	265.17		on Paron at Cl. out.
4.47	265.58		on curb

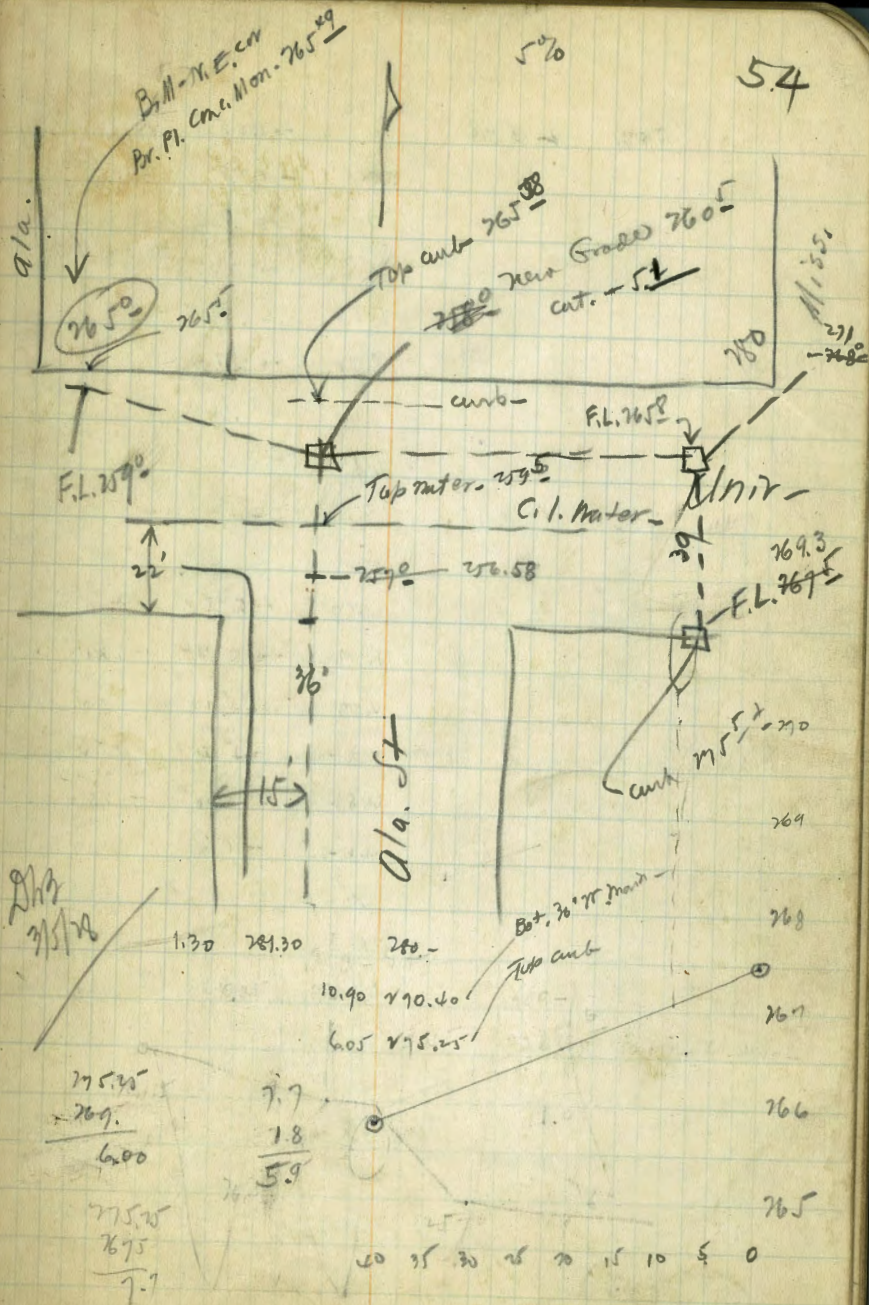
279.0
766
13.

5.07
3.4
1.67

See also

66

F.L. = 760' cut. 5.07
5.48



275.25
- 209.
6.00

7.7
1.8
5.9

275.25
2675
7.7

40 35 30 25 20 15 10 5 0

506 + 4.56 - 0.50

5.24 - 0.78

5.22 - 0.76 *Grate alley
So. Yanitic Ct.*

5.51 - 0.95

5.70 - 1.14

5.70 - .64

7.8 - 3.2

10.4 - 5.8

Grade

Curb-

4.98 + 4.48 - 4.50

0400
+ 30 curb
+ 30 Tie
+ 40 Curb
+ 69 = 1781

750

3

+ 10

4

727

0400 alley S Yanitic

0421 curb

0430 curb

0440 curb

+ 62

400 0461 on curb 4.86 = -33

7+50

1+81

Curb-

5.27 - 0.74 - 2.60 1.81

4.61 - 0.13 - 2.70 2.57

4.53 - 0.10 - 2.51 2.70

4.64 - 0.18 - 3.60 3.42

5.48 - 1.00 - 4.10 3.10

5.48 - 1.00 - 4.40 3.00

5.48 - 1.00 - 4.60 3.60

6.01 - 1.53 - 4.60 3.27

5.53 - 1.05 - 5.00 3.95

5.25 - 0.67 - 5.20 4.23

8.50 4.00 - 5.30 1.30

5.24 - 0.81 - 2.60 1.79

4.63 - 0.15 - 2.70 2.55

4.48 - 0.00 - 2.80 2.80

4.64 - 0.16 - 3.00 2.84

5.40 - 0.92 - 3.60 2.68

4.98 - 0.50 - 3.79 3.28

- 4.00

4.90 - .42 - 4.08 3.63

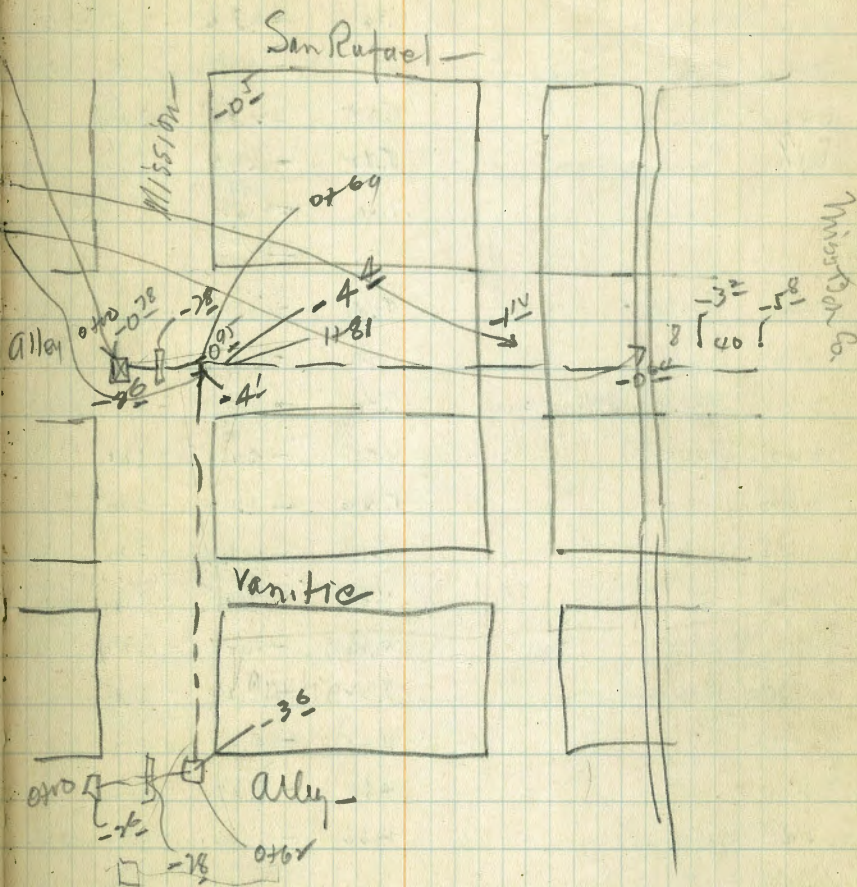
5.48 - 4.10

.176

3.8
.2
- 4.00

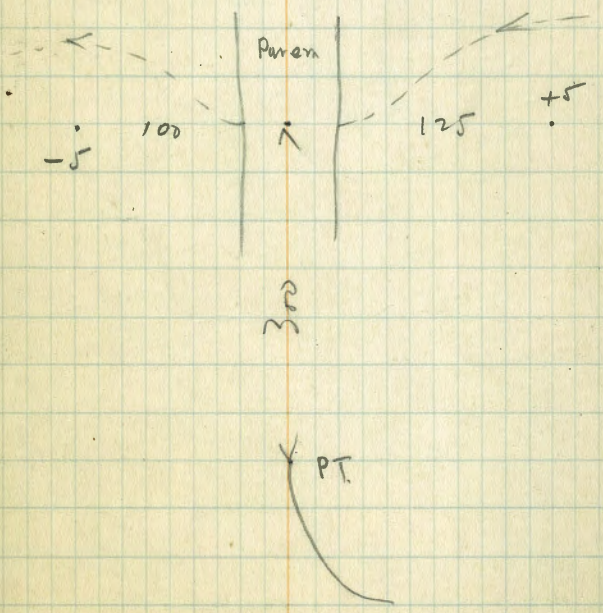
250
181
69

55

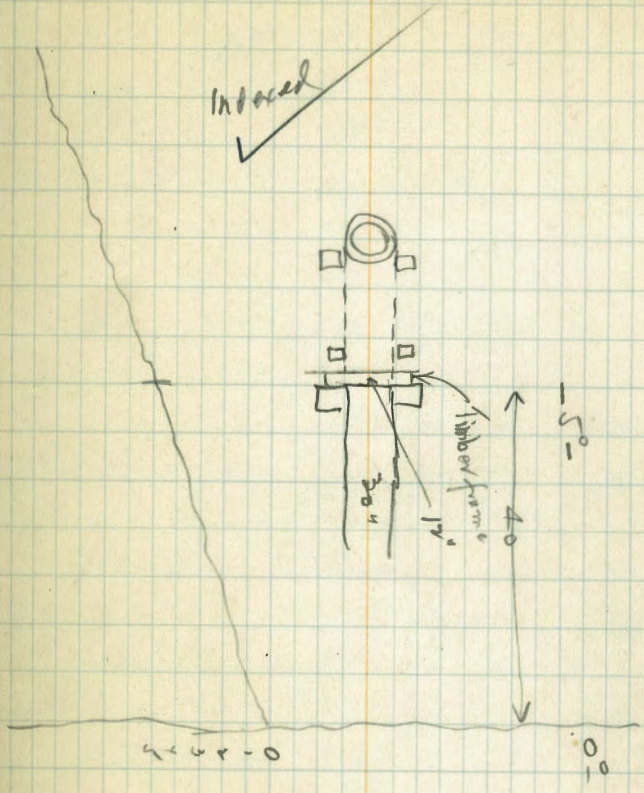


Joy	+ 4.79	-0.25	
		5.67	-0.88
		5.58	- .79
		5.1	-0.21
+ 70'		4.9	- .10
+ 40'		10.1	-5.3
		5	- .2
		5.5	- .7
		5.7	- .9
		5.35	- .56
		5.22	(.43)

Grot. alley
 So. Wind - M.S.
 Grot. alley
 So. Wind - E.S.
 Bay side Lane
 Whit. Ct -
 Bay side
 Grand - Whit -
 Es Miss
 Grot. alley
 So. Whit. E.S.
 Miss -
 Grot. alley
 So. Whit -
 M.S. Miss -



La Jolla -



Prts. Risins Cant

See (57)

	4.95	+4.45	-0.50		Cut
1+23 F.P.L. Miss.	5.40	-0.95	-4.70		3.75
2+33	5.76	-0.81	-4.78		3.97
+83	5.74	-0.84	-4.86		4.04
3+33	5.13	-0.68	-4.94		4.26
+83	5.60	-1.15	-5.02		3.87
4+33	5.70	-1.25	-5.10		3.85
+83	4.65	-0.20	-5.18		4.98
5+	4.12	+0.23	-5.20		5.53
0+70	5.40	-0.95	-4.40		3.45
0+10 cut	4.57	-0.12	-3.88		3.76
0+25 Tie	4.15	+0.30	-3.60		3.96
0+20 curb	4.54	-0.09	-3.54		3.45
0+00 Grate	5.16	-0.71	-3.70		2.49
	4.645				Cut
0+00 Grate	5.73	-0.78	-3.00		2.22
+70	4.18	-0.13	-3.16		3.03
+75	4.18	+0.27	-3.19		3.46
0+60 gutter	5.25	-0.90	-3.47		2.57
0+70 P.L.	4.78	-0.33	-3.15		3.22
1+70 Portsmouth	4.86	-0.39	-4.30		3.91
1+80			-4.4		

$$\frac{5}{320} = .16$$

$$\frac{5}{180} = .28$$

$$\frac{1.87}{320} = .58$$

59

$$\frac{1.2}{1.7}$$

$$\frac{750}{34} = 22.06$$

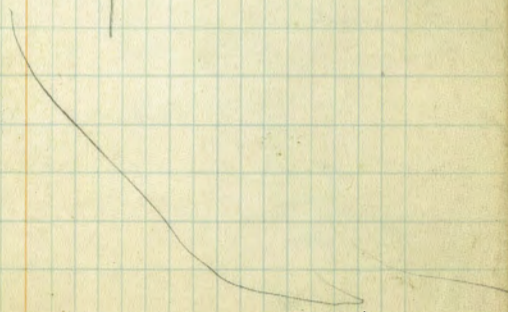
$$\frac{1.4}{1.0} = 1.4$$

$$\frac{1.4}{1.0} = 1.4$$

$$\frac{3.94}{4.41}$$

↑

	+4.45	El.	Prop. Grade	Cut	
0+00 Grate		-.75	5.20	-3.40	2.25
+70 curb		-.08	4.52	-3.16	3.08
+75 Tie		+.32	4.13	-3.14	3.51
+60 curb		-.14	4.59	-3.30	3.16
+60 gutter		-.97	5.37	-3.47	2.55
+70 P.L.		-.40	4.65	-3.55	3.15
1+70 Coast-Risins		-.45	4.40	-3.94	3.49
1+80				-4.40	



Witherby - Atlantic

4.90

6.50

1.60

8.10 ✓ -1.90

8.90 ✓ -2.40

6.76 - .26

8.70 ✓ -2.20

F.L. pipe 18"

N.S. Witherby

F.L. 2-16"

S.S. Witherby

Grate

30' N. With-

F.L. 18"

30' N. With-

4.44 1.76

4.90 1.63 .87

5.33

N.W. curb - Witherby & Atlantic

4.44

4.9x

6.54

1.60

8.9v -2.40

8.40 -1.86

8.2v -1.7

120' N. Witherby

8.7x -2.20

1/17/28

6.00

7.60

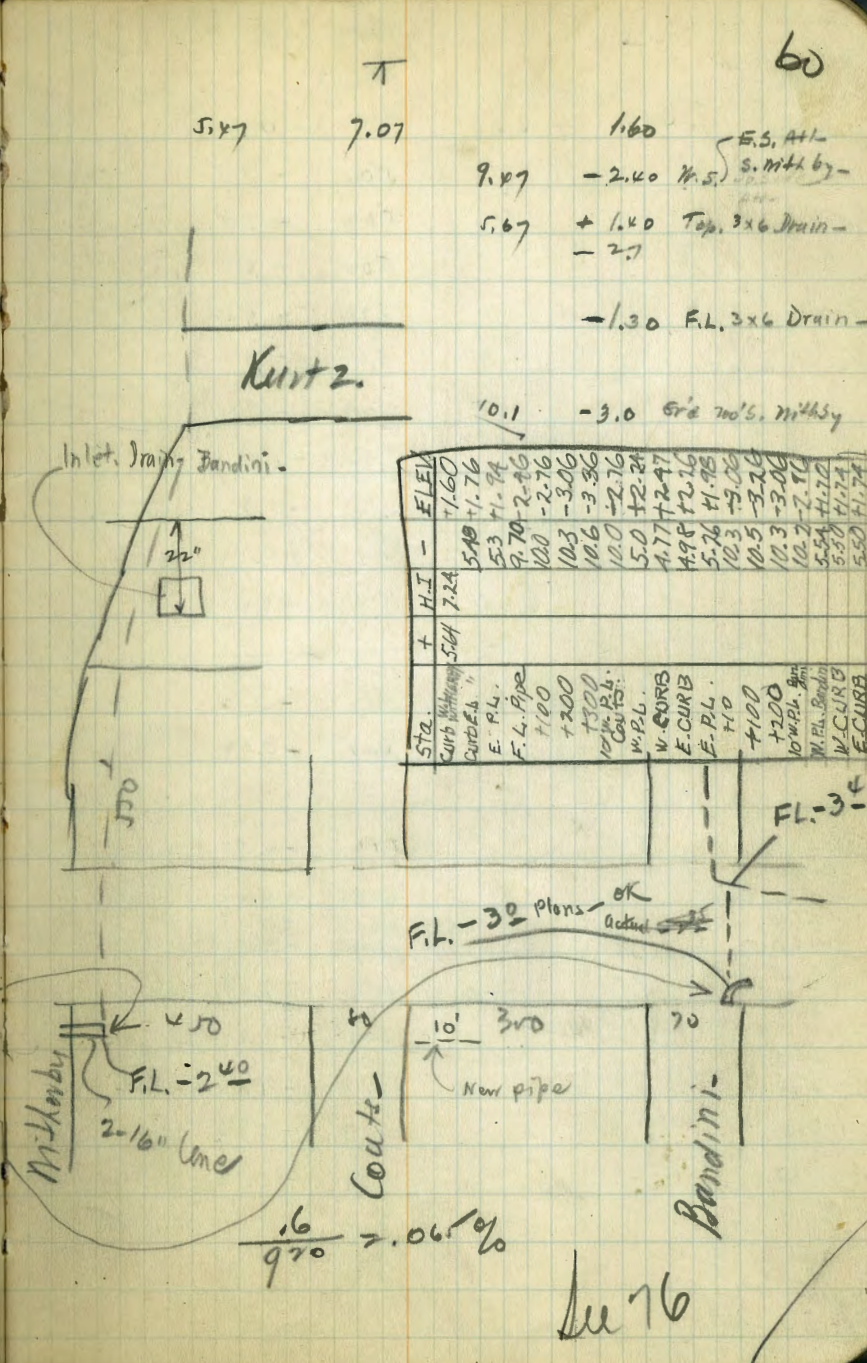
1.60

10.00 -2.40

F.L.

10.45 -2.45

F.L.



60

5.47

7.07

1.60

9.47 -2.40

E.S. At-

S. Witherby

5.67 +1.40

Top. 3x6 Drain-

-2.7

-1.30 F.L. 3x6 Drain-

10.1 -3.0

Grate 70's. Witherby

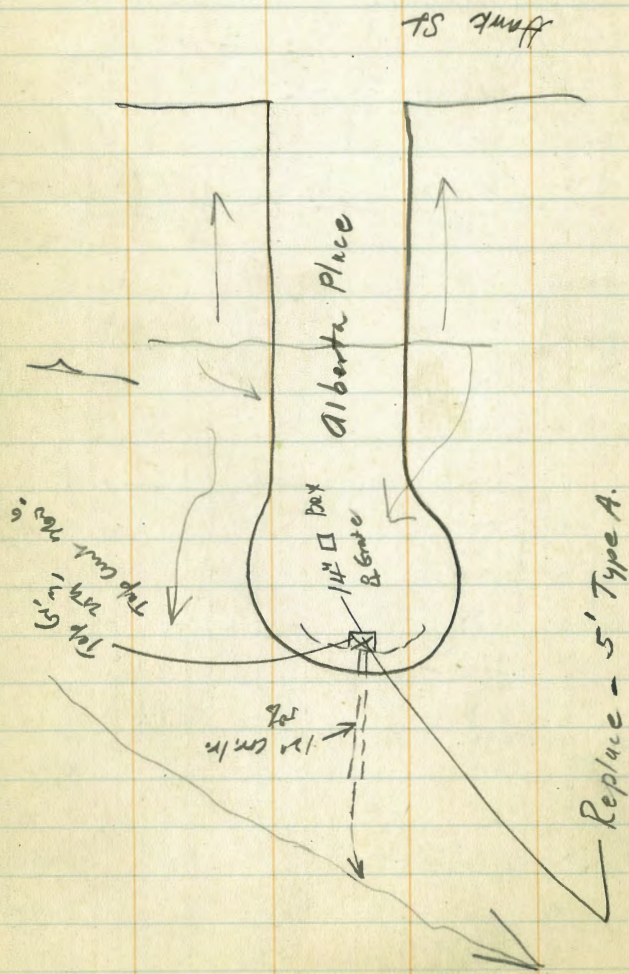
FL-34

FL-32 plan

Bandini

See 76

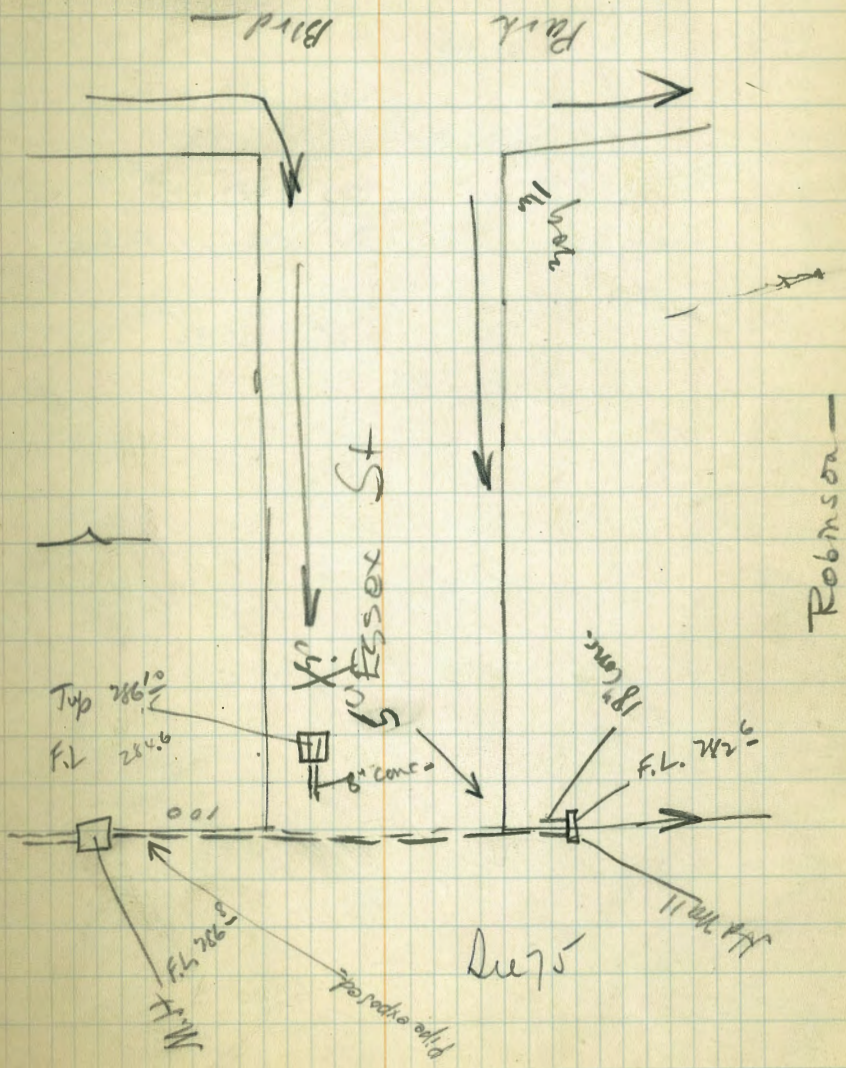
8/11/42



Replace - 5' Type A.

69

8/18/42



Robinson

9/12/78

ESSAY St

63

T

0.51 310.11 309.30

11.53 298.28 ✓

0.37 298.65 12.17 286.88 ✓

6.77 293.25 ✓

7.95 10.63 282.62 Fib. 18" Conc.

34.63 7.15 286.10 Top Grate

304.3
26.66
277.64

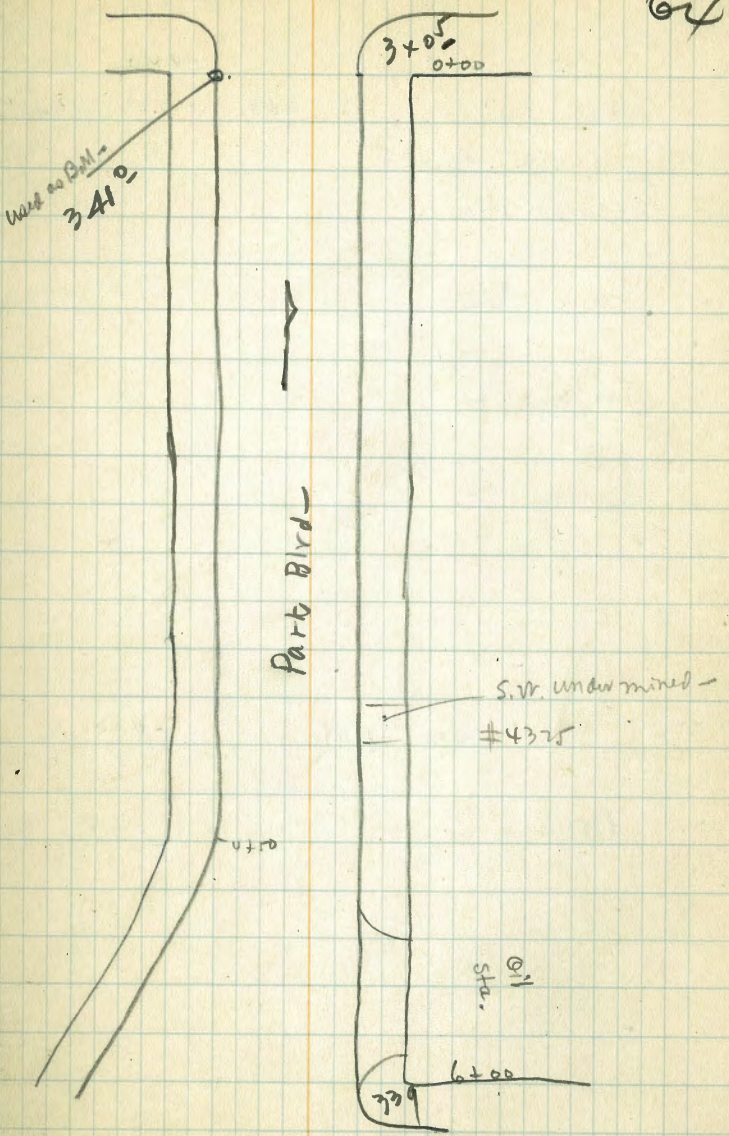
6.85 286.80 Fib. M.H.

7/17/78 *AB*
Parting

	π		
Top cb	+576	346.8	341.0
	G.	6.8	340.0 F.L.
100 S - N. side	cb	5.5	341.3
	G.	6.2	340.6
200 S. ✓	cb	5.3	341.5
	G.	6.0	340.8
300 S	cb	5.1	341.7
	G.	5.8	341.0
400 S.	cb	4.7	342.1
	G.	5.4	341.4
4+50 Any pt.	cb	4.6	347.2
	G.	5.2	341.6
0+00 E. side.	cb	6.3	340.5
	G.	7.4	339.4
100 S. ✓	cb	6.6	340.2
	G.	7.4	339.4
	S.W.	6.3	340.5
200 S ✓	cb	6.8	340.0
	G.	7.6	339.2
	S.W.	6.6	340.2
300 S.	cb	6.4	339.9
	G.	7.2	339.0
400 S.	SW	6.9	339.9
	cb	6.9	339.9
	G.	8.0	338.8
	S.W.	7.3	339.5
500 S.	cb	6.9	339.9
	G.	8.1	338.7
	SW	7.5	339.3
600 S	cb	7.1	339.7
	G.	8.1	338.7
	S.W.	7.6	339.2

Meete Ave-

64



El Cajon Ave

Miss Bay

Tide Line

4.71 + 3.31

-1.40

1st Ave Ct

3.68

-0.37

412 + 3.75

Jamaica Cr

Sta Barb

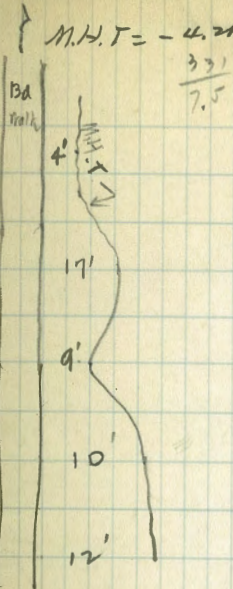
Jersey Ct

Kennobec Ct

4.20 + 3.70

-0.50

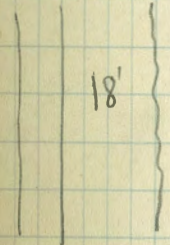
Ormond Cr



4.21
3.75
7.96

65

+3.70
-4.21
7.9



Sta- 15' So. E. Drain -

Cape May Ave.

0+0 E.L. Bairn -

0+60 C.O. M.L. ✓

1+

+50

2

+50

3

+50

4

+50

5

+50

6

+50 E.L. Abbott

7+20 M.L. ✓

+50

8

+50

9

+50

10

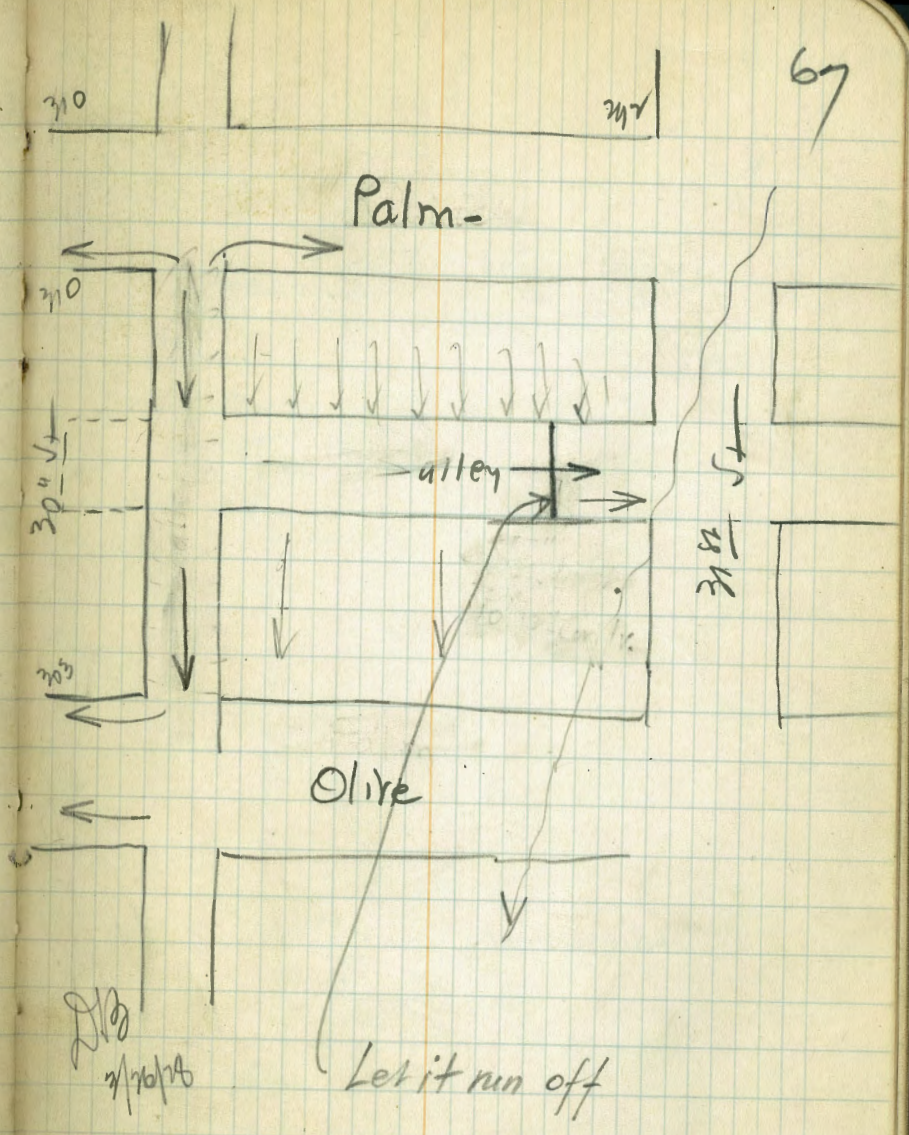
+50

11

+50

N.E. Drain - Cape May - 6.76

66



Palm-

alley

Olive

Let it run off

30'0"

30'0"

30'0"

30'5"

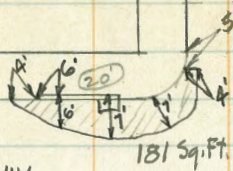
30'

30'5"

30'5"



Alabama

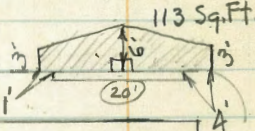


UNIV.

8' Radius - center on curb face at $\frac{1}{4}$ of inlet.

10659. Ft.

AVE.

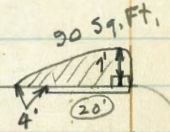


113 Sq. Ft.

Alabama St.

See 52

MISSISSIPPI



30 Sq. Ft.

UNIV. AVE.

2.07 16.07

9.20 1.4 -
6.87
~~6.80~~ Bot. 6" C.I.
6.76

9.17 6.60
8
5.80 Bot. 6" C.I.
6. -

7.64 8.43
1.69
6.5

9.15 6.22
1.67
6.55
4.10
2.5

42
24
16

16.33

6.80
1.59
8.69
4.3
2.6

9.23 7.10 Top. 6" C.I. meter
8
6.3

7.85 8.48 Top. stk. side
CB = 10.40 F = 1.92
= 1.11"

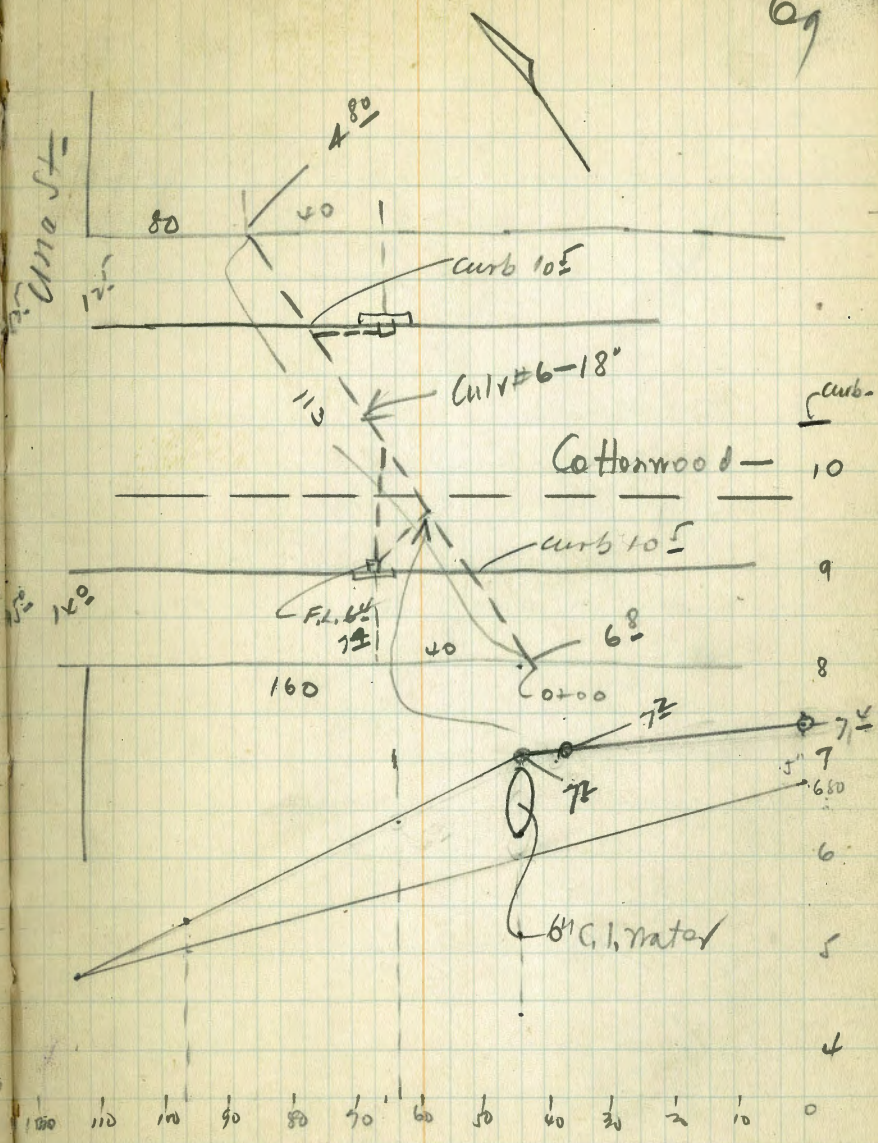
9.23 7.60 Top. stk. N. side
CB 10.40 F = 3.20
= 2.20"

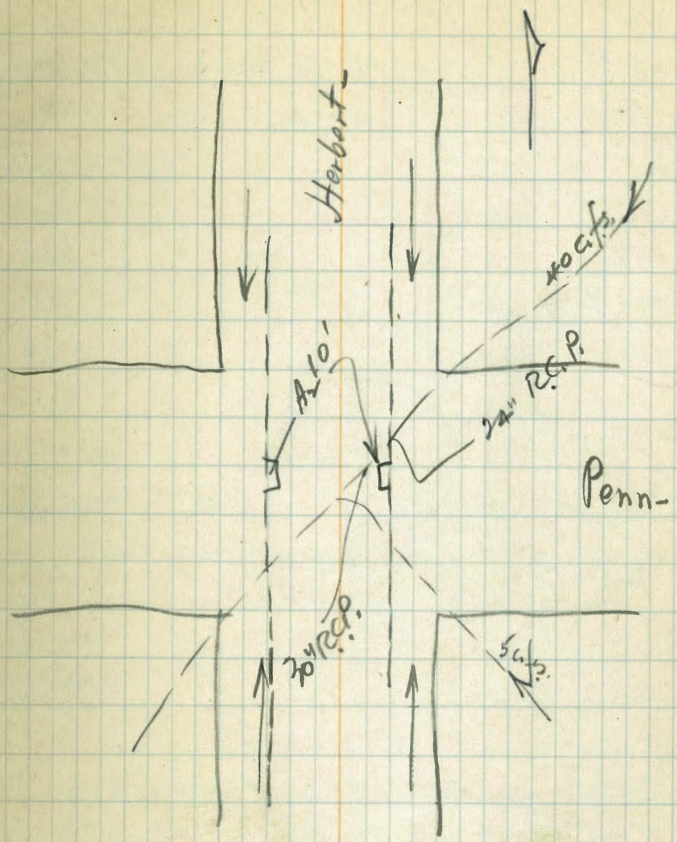
9.15
11/28

8.18
7.0
1.18

7.10
5.2
1.9

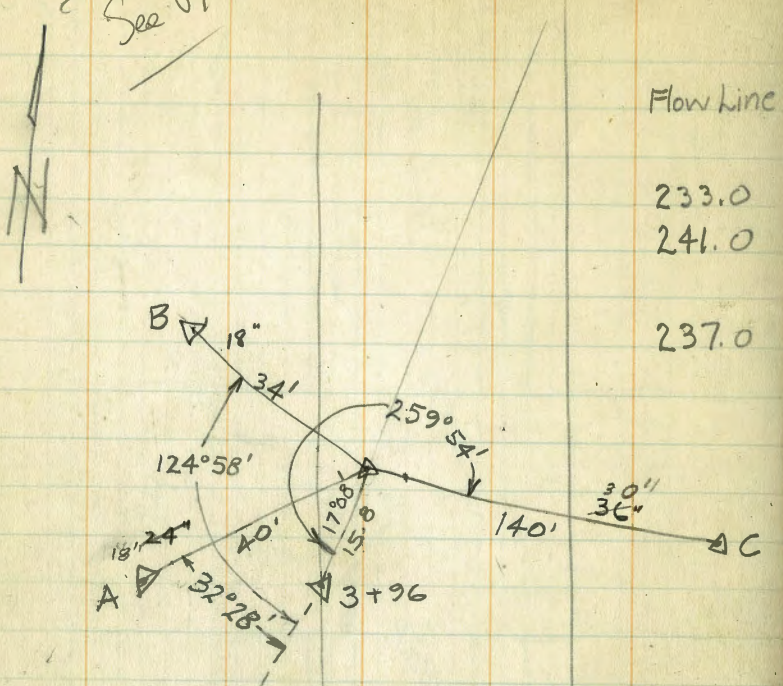
69





2/20/78

See Pg. 44



Flow line	BM. Top of Manhole		
	6.51	241.51	
233.0	Junction	5.0	236.5 C-3.5
241.0	"A"	+0.3	241.8 C-0.8
	+20	2.1	239.4
237.0	"B"	4.1	237.4 C-0.4
	+7	4.4	237.1
	+24	4.5	
	+27	7.0	
	Junction +15	8.3	
	+30 Water Pipe 4" C.I.	9.3	232.2
	+62	11.3	
	+84	9.4	
228.0	"C"	13.0	228.5 C-0.5

Put $\frac{1}{4}$ of Curb Inlet opening
10' East of Junction Stake
other opening 61' East of
Junction Stake

	Ground	Grade	Cut
Junction	236.5	233.0	3.5
+50	234.0	231.2	2.8
+100	233.7	229.4	4.3
+140	230.5	228.0	2.5
+30	232.2	231.9	0.3

Cut at Manhole = 2.8 ✓

1742/62
Schnitz
& Co.

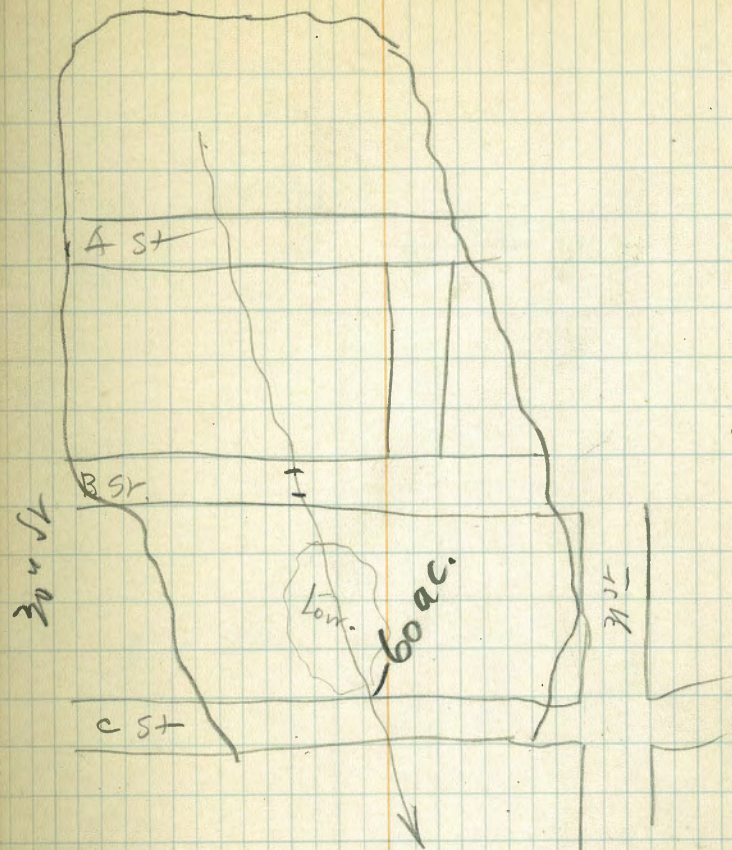
0700
IVY

+1
0

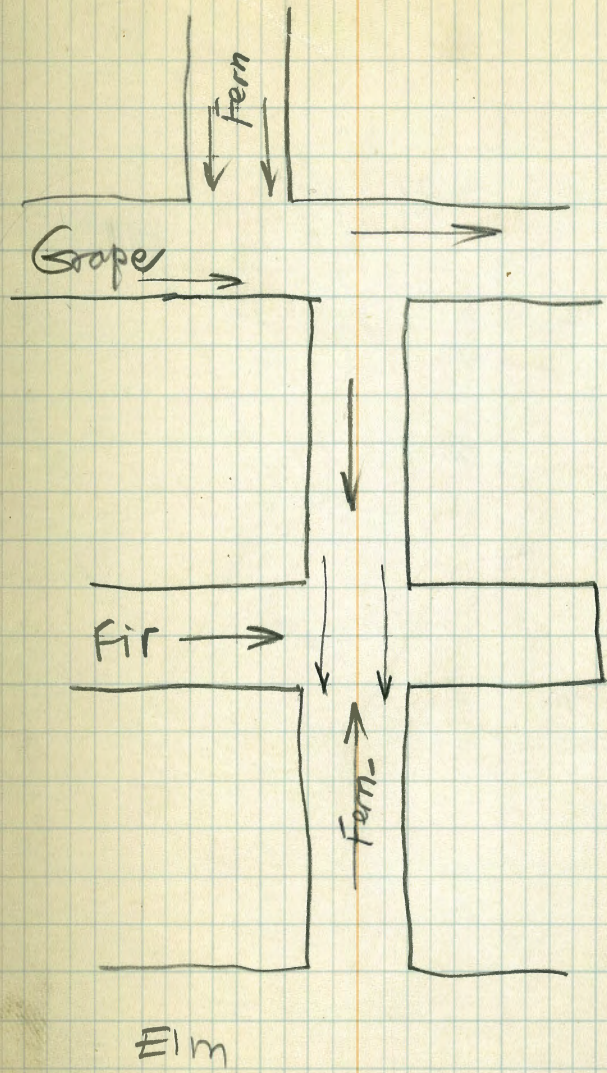
LANE

Buck

72

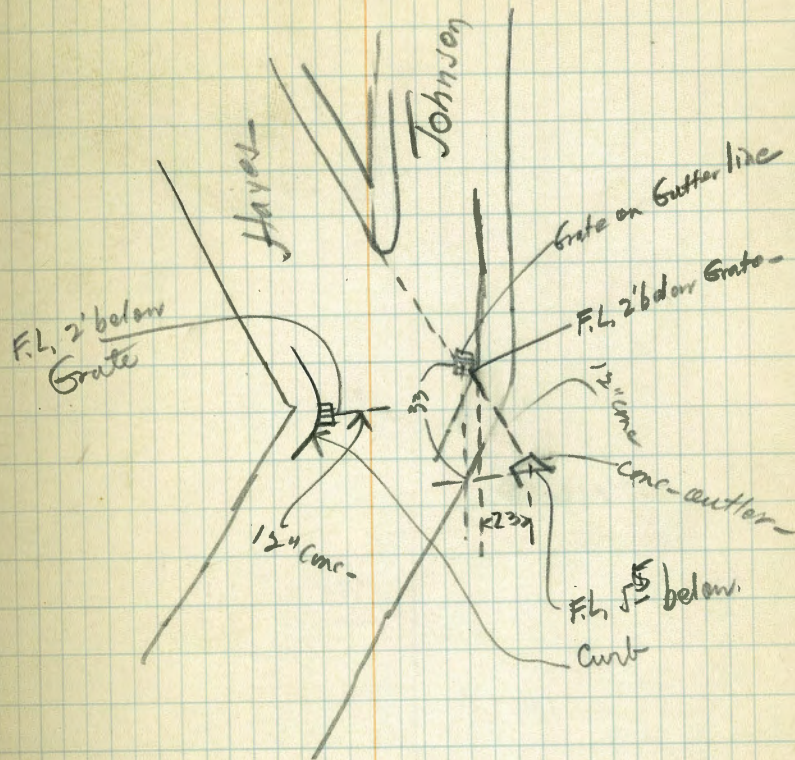


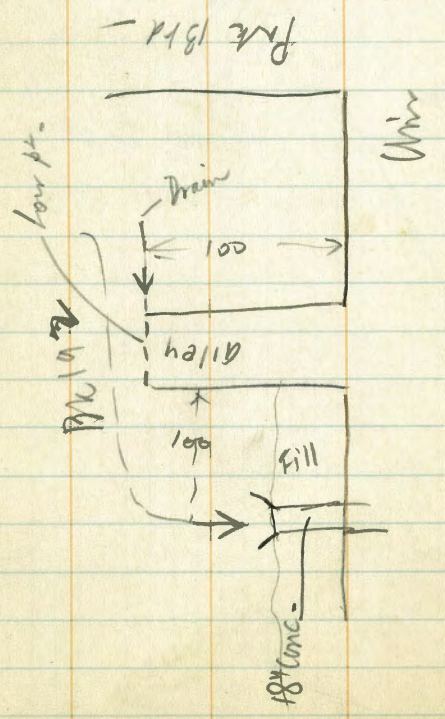
300 REP-
35%



6/17/28

74



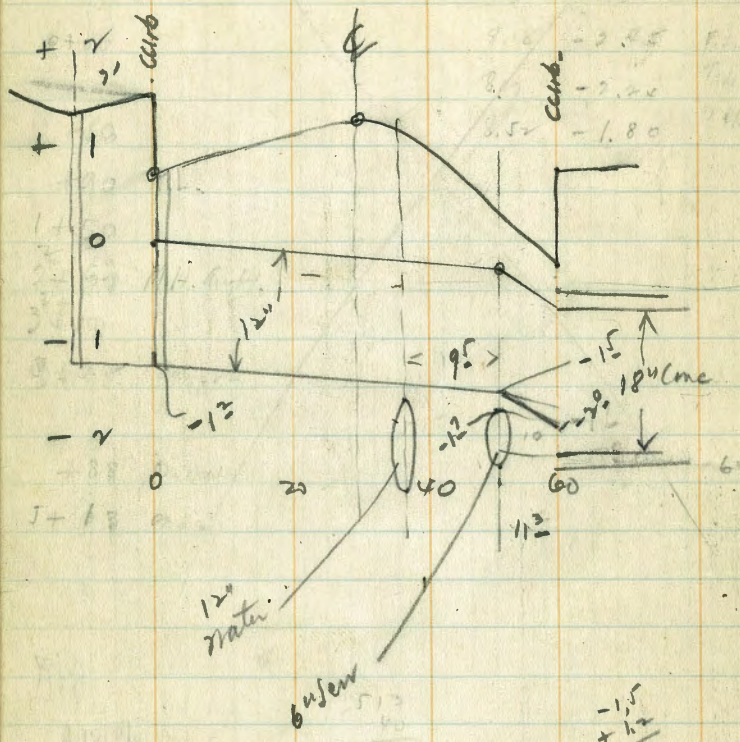


Section 60

July 29/29

E. 5.33 - 6.73 W

4.42 - 1.81
 9.16 - 2.55
 8.52 - 2.24
 3.52 - 1.80



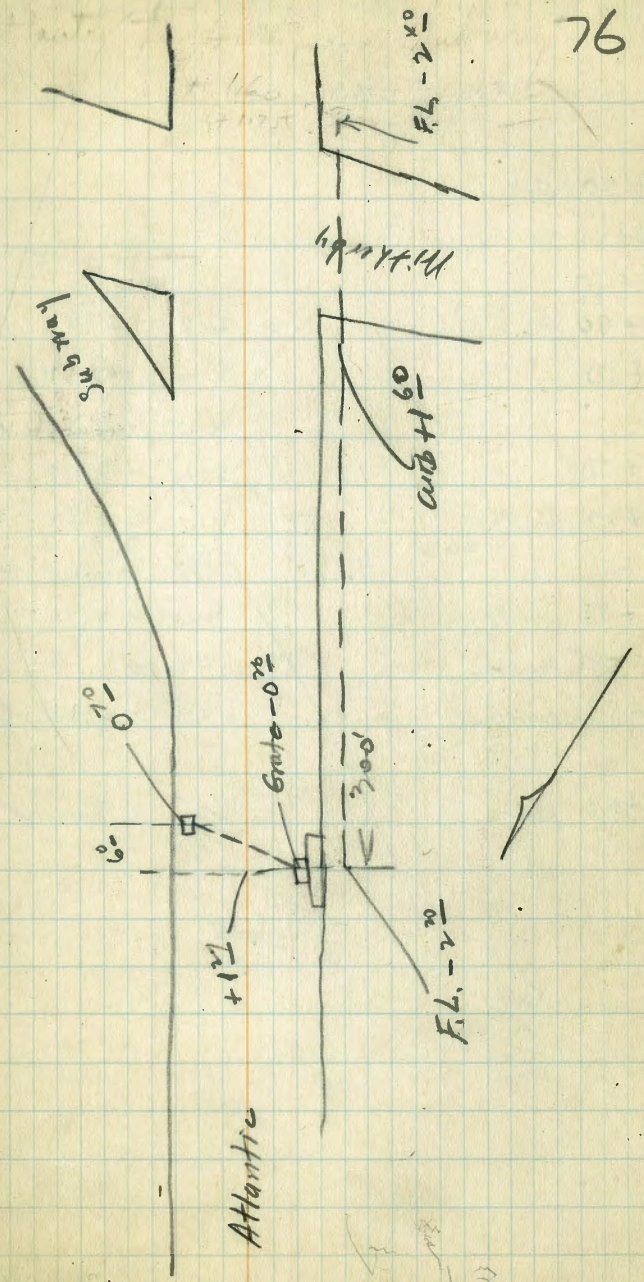
$$\begin{array}{r} -2.20 \\ 1.7 \\ \hline -0.5 \end{array}$$

$$\begin{array}{r} 20.8 \\ 6.7 \\ \hline 27.5 \end{array}$$

$$\begin{array}{r} -1.5 \\ +1.2 \\ \hline -0.3 \end{array}$$

See also Book 1503/77 1521/76
 G.B 186/64

76



2/28 9/17/48

Train on Wetherly at Atlantic -

5.13 +6.73 +1.60

0400 M.H

0440

0450

0490 P.L.

1450

2

+50

+77 Aug Pt.

3+

+50

+95 Aug Pt.

4483 Overall

5408 end -

on Parem -
5.22 +1.49 C 6.58 ✓
5.28 +1.55 C 6.76 ✓

4.74 +1.99 C 7.46 ✓

4.85 +2.28 C 7.96 ✓

4.70 +2.47 C 8.37 ✓

4.15 +2.58 C 8.60 ✓

T.P. 7.19 ✓ 4.59 +2.60 C 8.72 ✓

4.45 +2.74 C 9.07 ✓

4.76 +2.93 C 9.45 ✓

4.58 +2.61 C 9.51 ✓

14.25 -7.06 ✓

Grade

-2.40

-5.00

-5.09

-5.21

-5.47

-5.68

-5.90

-6.02

-6.12

-6.33

-6.52

-6.90 ✓

-7.00 ✓

77

2.5
8
21.0

1.81

5.23

H.L. = 7.04

10.7

-3.7

$\frac{2}{4.58} = .437$
21.4

5.60
865
14.25

9/17/80

At. St. Drain from Mithaby to Caatts - St -

	M.H.	El.	Cut.	Grade
0+00	M.H.			-2.40
+13	M.H.	5.17	+1.87	4.28
+50		5.12	1.92	4.20
1+		5.02	2.02	4.00
+50		4.95	2.09	4.86
2		4.80	2.22	4.58
+70		4.70	2.34	4.36
3		4.70	2.34	4.36
+50		4.60	2.44	4.16
4		4.50	2.52	4.00
+70		4.40	2.64	3.76
+78		4.50	2.52	4.00
5+		4.75	2.29	4.46
15	M.H.	4.70	+2.32	5.02
55	End.	10.70	-3.66	-3.70

$$\frac{13}{55} = .0585$$

FL 2-16" Conc. pipes -

6.24 306.84

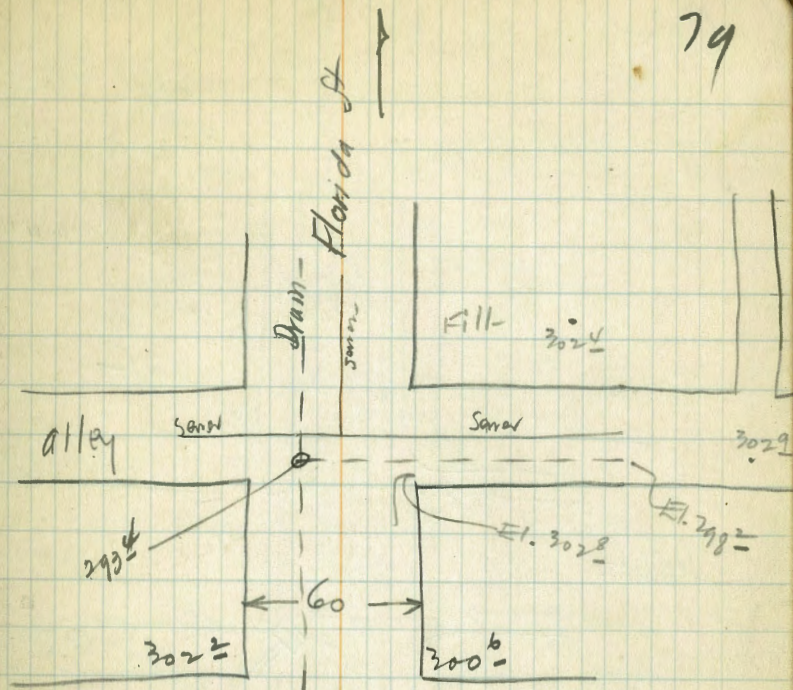
300.60 N.E. El Caj
+ Fla

4.06 302.78 curb-alley-

8.6 298.2

3.9 302.9

4.4 302.4



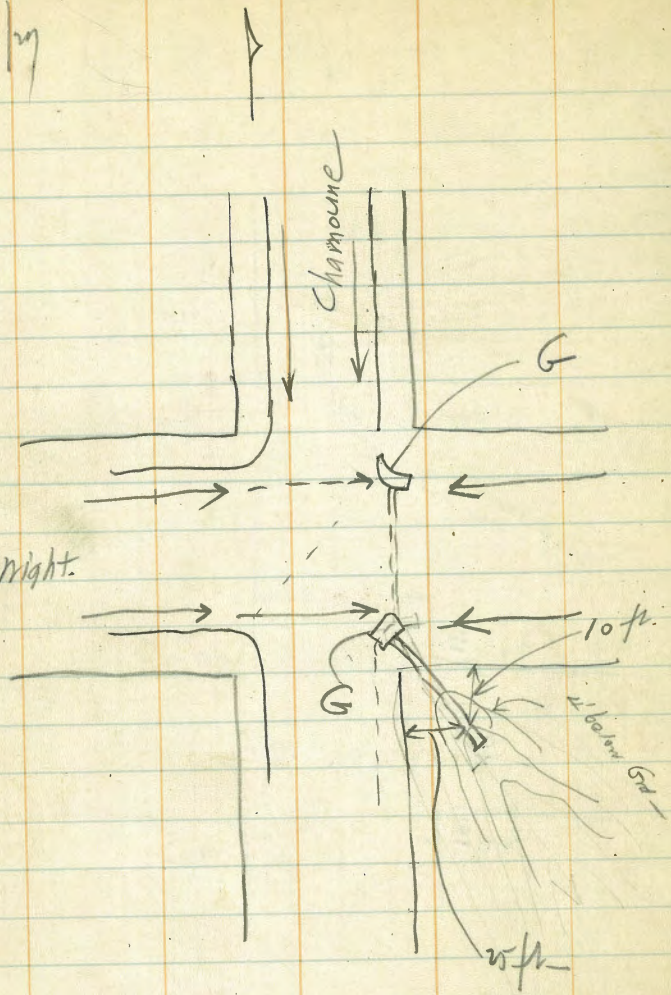
El Cajon Ave

300.6

299.0

9/23/24

Dringt.

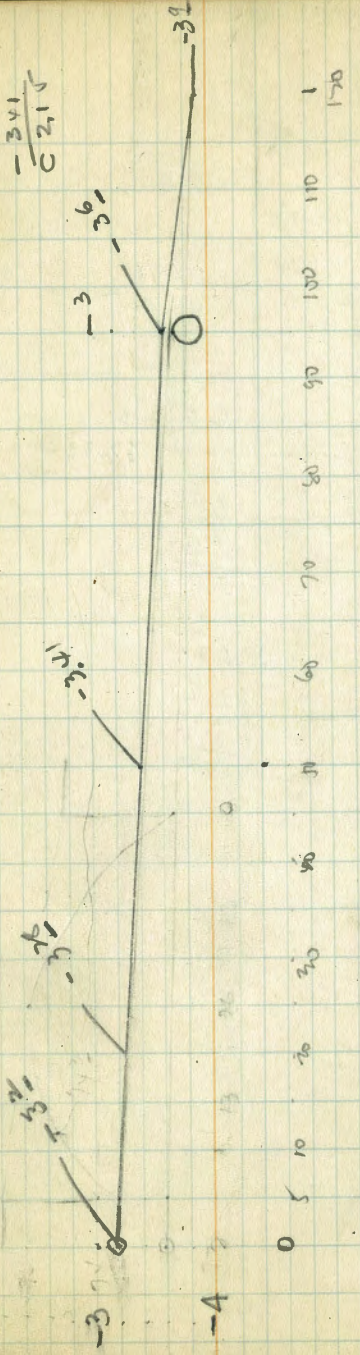


$$\frac{10}{2.6} = \frac{0.1}{0.1}$$

$$\begin{array}{r} 570 \\ -130 \\ \hline 440 \end{array}$$

$$\begin{array}{r} 570 \\ -126 \\ \hline 444 \end{array}$$

Grant and Baker



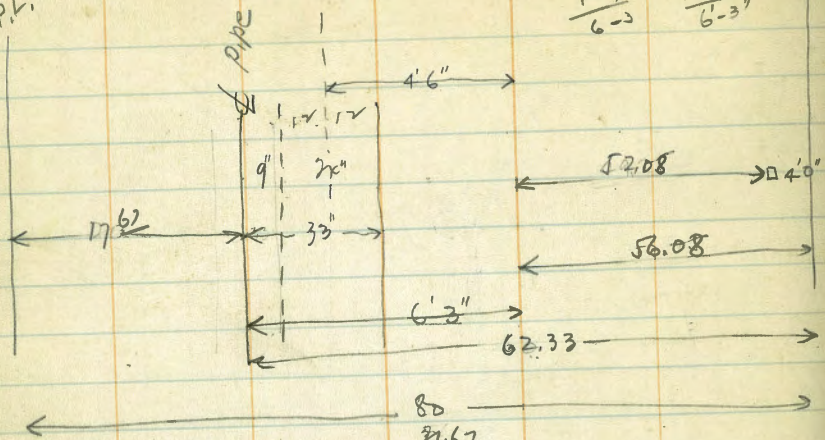
83

P.L.

P.L.

$$\begin{array}{r} v-6 \\ 1-9 \\ \hline 6-3 \end{array}$$

$$\begin{array}{r} 5-6 \\ 6-3 \\ \hline 9 \end{array}$$



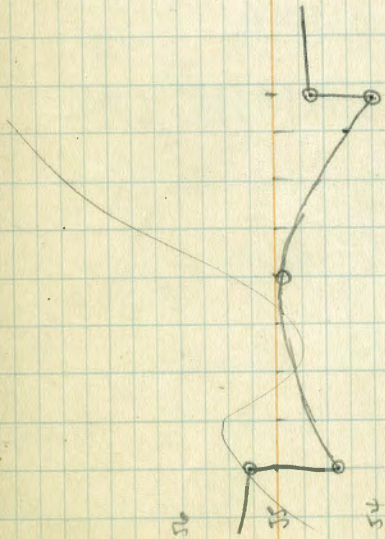
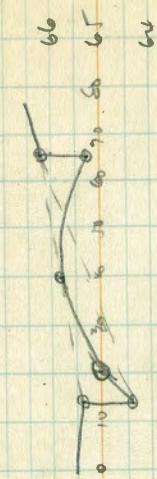
$$\begin{array}{r} 80 \\ 1767 \\ \hline 62.33 \\ 625 \\ \hline 56.08 \\ 4 \\ \hline 52.08 \end{array}$$

$$\begin{array}{r} 80 \\ 31.67 \\ \hline 58.33 \\ 6.25 \\ \hline 52.08 \end{array}$$

$$\begin{array}{r} 62.33 \\ 4 \\ \hline 58.33 \end{array}$$

$$\begin{array}{r} 100 \\ 37 \\ \hline 68 \end{array}$$

81



565 570 578

533 538

565 575

57

525

ENGINEERING DEPARTMENT,
CITY OF SAN DIEGO,
CALIFORNIA.

Rob. & Glu - N.W. B.P. - 258.01

241.51

3.28

238.23

237

4.12

80

72

4

21.75

6.12

65.23

56.9

8.3

52

9