

1214

1214

MICROFILMED  
DEC 22 1964

ENGINEERING DEPARTMENT,  
SAN DIEGO,  
CITY OF CALIFORNIA.

2	50	30
	21	37
	10	52
	89	60
	79	08

This included 6/17/30 H.H.

32.5  
41.48  
73.98

Our Leather Bound Engineers Note Books are carried in the following ratings:

- No. 380 LEVEL BOOK. Left and Right Hand Page the same as Left Hand Page of this Book.
- No. 382 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 4 x 4 to the inch, Center Line Red.
- No. 384 MINING TRANSIT BOOK. Left Hand Page as in this Book, Right Hand Page 8x8 to the inch, Center Line Red.
- No. 385 FIELD BOOK. Left Hand Page as in this Book, Right Hand Page 8 vertical and 4 horizontal lines to the inch, Center Line Red.

We also carry the Note Books listed above, bound in extra strong Fabri-Hide (otherwise the same quality of book), which can be furnished at a somewhat lower price.

In ordering Fabri-Hide covered books, add the letter "F" to catalog number.

**THE FREDERICK POST CO.**  
ENGINEERING and DRAFTING SUPPLIES  
IRVING PARK STATION  
CHICAGO, ILL.

ENGINEERING DEPARTMENT,  
SAN DIEGO,  
CITY OF CALIFORNIA.

## INDEX.

PAGE

✓ X. Section Scimitar St. - Barb to Klauber	Book 1225 - P. 1	28
" " ORANGE St. - Minnet. to MAULARD	Book 1225 Page 34	36
" " MAULARD St. - MARIPOSA to 69 <sup>th</sup>	✓ X 9.	74
" " Minnet St. - ORANGE to Scimitar	Book 1225 Page 69	
" " ATMIX St. - RADIO to Klauber	Book 1225 Page 30	
" " PARADISE St. - MARIPOSA to RADIO	Book 1225 Page 63	
" " 69 <sup>th</sup> St. - Mallard to Gibson		19.
" " ZEBBAR St. - Klauber to Gibson		35.
" " PLOVER " - " " " "		✓ 41
" " HILGER " - " " " "		✓ 49
" " BITTERN " - " " MAOERA		✓ 74
" " EIDER " - Minnet " Klauber		158
" " WREN " - Scimitar " " "		✓ 69.

Radio Dr

Nails in Tel Pole E. Line Klauber  
 15 S. of 1st & W. of Atlix  
 BM 408.37  
 0.15  
 X 408.52  
 4.76  
 BM 403.76 Pipe & Klauber + Hilger  
 12.55  
 X 416.31  
 0.23  
 416.28  
 12.90  
 X 429.18  
 0.06  
 429.12  
 13.04  
 442.18  
 8.36  
 BM 436.82 Hub L + Flower  
 442.07  
 452.06  
 11.56  
 X 451.01  
 0.33  
 BM 440.50 Hub Klauber + Zeller  
 451.74  
 12.91  
 464.65  
 0.25  
 464.40  
 5.77  
 X 468.17  
 8.21  
 469.96  
 2.88  
 X 468.84  
 3.47  
 BM 465.17 Mon 69<sup>th</sup> + Mallard  
  
 465.55  
 5.48  
 BM 460.07 Prop Hub S.E. Mallard + Orange  
  
 463.71  
 7.95  
 BM 443.76 S.E. Prop Hub Mallard + Mariposa  
  
 388.09  
 2.96  
 BM 385.13 N.W. BIK Cor. Hub 69<sup>th</sup> + Gibson St.  
  
 BM 363.35 N.W. BIK Cor. Hub Zeller + Gibson  
  
 BM 357.23 NW BIK cor Hub Flower + Gibson  
  
 BM 322.52 N.E. BIK Cor Hub Hilger + Gibson

THIS PIPE -  
 435.07  
 4.23  
 BM 430.84 Pipe at SW cor Klauber + Scimitar  
  
 397.46  
 4.64  
 BM 385.78 Pipe S.E. Cor Klauber + Bittern  
 BM 386.00 Nails in Pole opposite above BM.  
  
 336.18  
 6.98  
 BM 329.20 S.W. BIK Cor. Hub Wren + Klauber  
  
 399.33  
 6.21  
 BM 373.12 N.E. BIK Cor Hub Winnet + Scimitar  
  
 410.44  
 5.08  
 BM 405.36 S.W. BIK Cor Hub Scimitar + Wren St

B.M. Hub N.W. Orange + Swan. Sts. 401.28  
 B.M. " N.W. Radio + Paradise 351.36  
 B.M. " N.W. Paradise + Orange 433.74

2.13  
 433.74

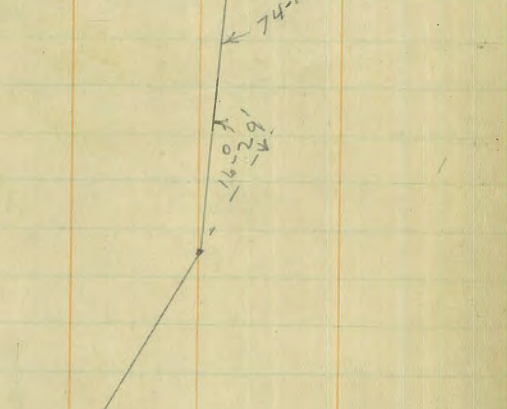
8-15-36 3" Water Line from Upas.  
 + Richmond. South to N. Entrance  
 of Zoo. To serve Deer Mesa.

Mellin  
 Walker  
 Bliss  
 Nathan

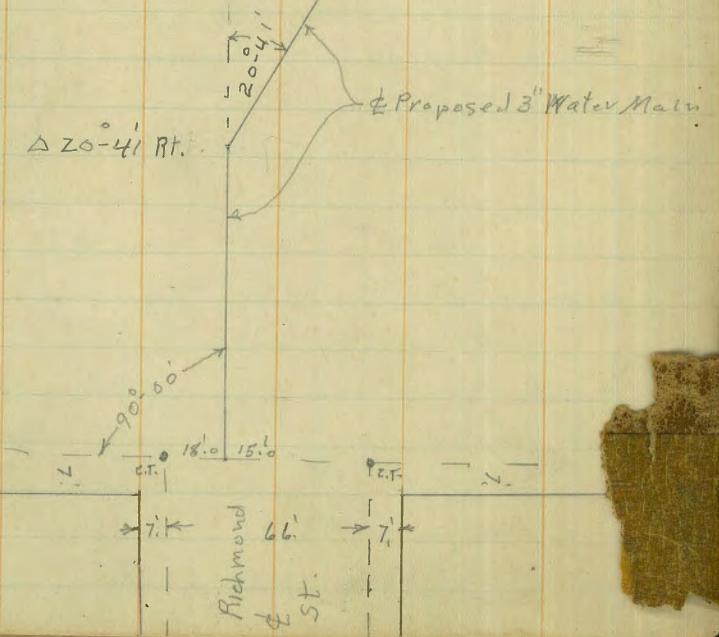


6+62 N. Fence of Zoo.

4+66 Δ 16-29 Lt



1+66 Δ 20-41 Rt.



Found to be 0.87 High  
 Probably raised since these notes were taken. C.B. 1/4/41  
 Grid Book 100-5  
 6-4-41

B.M. 433.44. SW. BIK. Cor. Hub. Eider + Klauber

T	435.07
	12.85
X	422.22
	0.32
T	421.90
	12.10
X	410.01
	0.22
X	410.23
	12.96
X	397.27
	0.19
X	397.46
	12.74
X	384.72
	0.61
X	385.33
	11.90
X	373.43
	0.52
T	373.95
	12.36
X	361.59
	0.25
X	361.84
	12.78
X	348.06
	0.08
X	348.74
	12.91
X	335.98
	0.20
X	336.48
	13.11
X	323.07
	0.23
T	324.00
	2.99

B.M. 315.01 Spk. 6" 6 1/2" Each  
 314.97 Bk Has been  
 Gravel Disturbed

T	324.00
	2.19
X	321.81
	6.90
X	328.72
	12.22
X	315.85
	0.40
X	316.25
	12.46
X	308.79
	0.21
X	304.10
	12.72
X	291.28
	0.24
T	291.52
	12.12
X	279.40
	5.27
X	282.67
	6.27

B.M. 276.38 SW. BIK. Cor. Bittern + Madara

434.33 B. Min Post. N. Line of  
 Curve #5 on Scimitar

X	434.68
	7.74
X	426.94
	1.03
X	427.97
	12.24
X	415.73
	6.03
X	416.76
	12.47
X	404.29
	0.43
X	404.72
	7.29

B.M. 396.93 Elev. B.M. P.C. Curve #2  
 on hub } South Side of Curve

X	404.72
	12.87
X	391.84
	10.50
X	382.34
	11.93
X	380.36
	0.36
X	380.72
	12.61
X	367.11
	0.24
X	368.35
	4.87

B.M. 363.48 B.M. on hub. N. line Cor. of Garage

X	368.35
	12.87
X	355.48
	0.21
X	355.69
	12.26
X	343.43
	0.92
X	344.35
	6.62

B.M. 337.73 Spike in pole SE Cor 63rd + Bacc.

X	334.35
	0.50
X	343.85
	3.80
X	347.65
	13.00
X	334.65
	0.22
X	334.57
	12.93
X	341.74
	3.39
X	322.27
	7.20

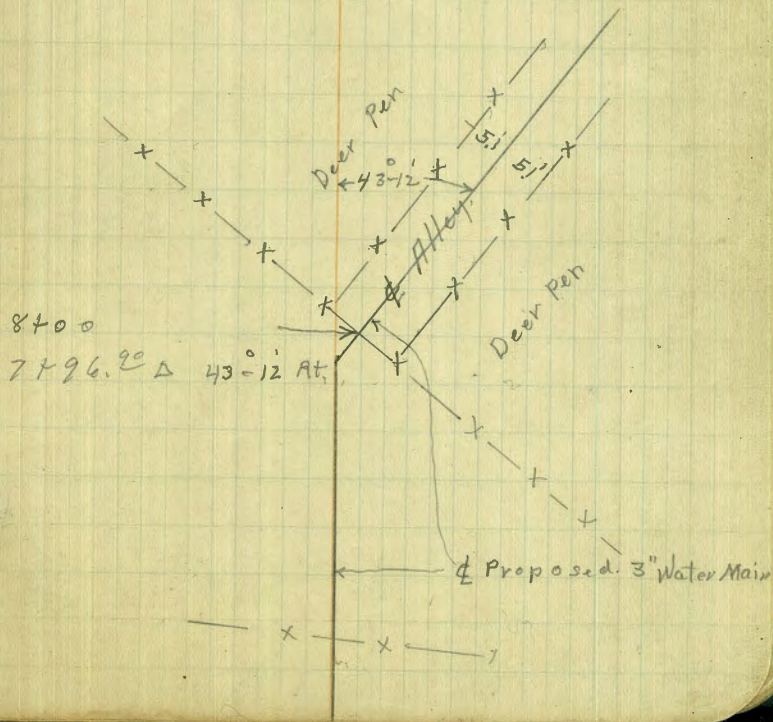
315.07 Spike in pole at 65th  
 Bacc.  
 Elev. 315.01

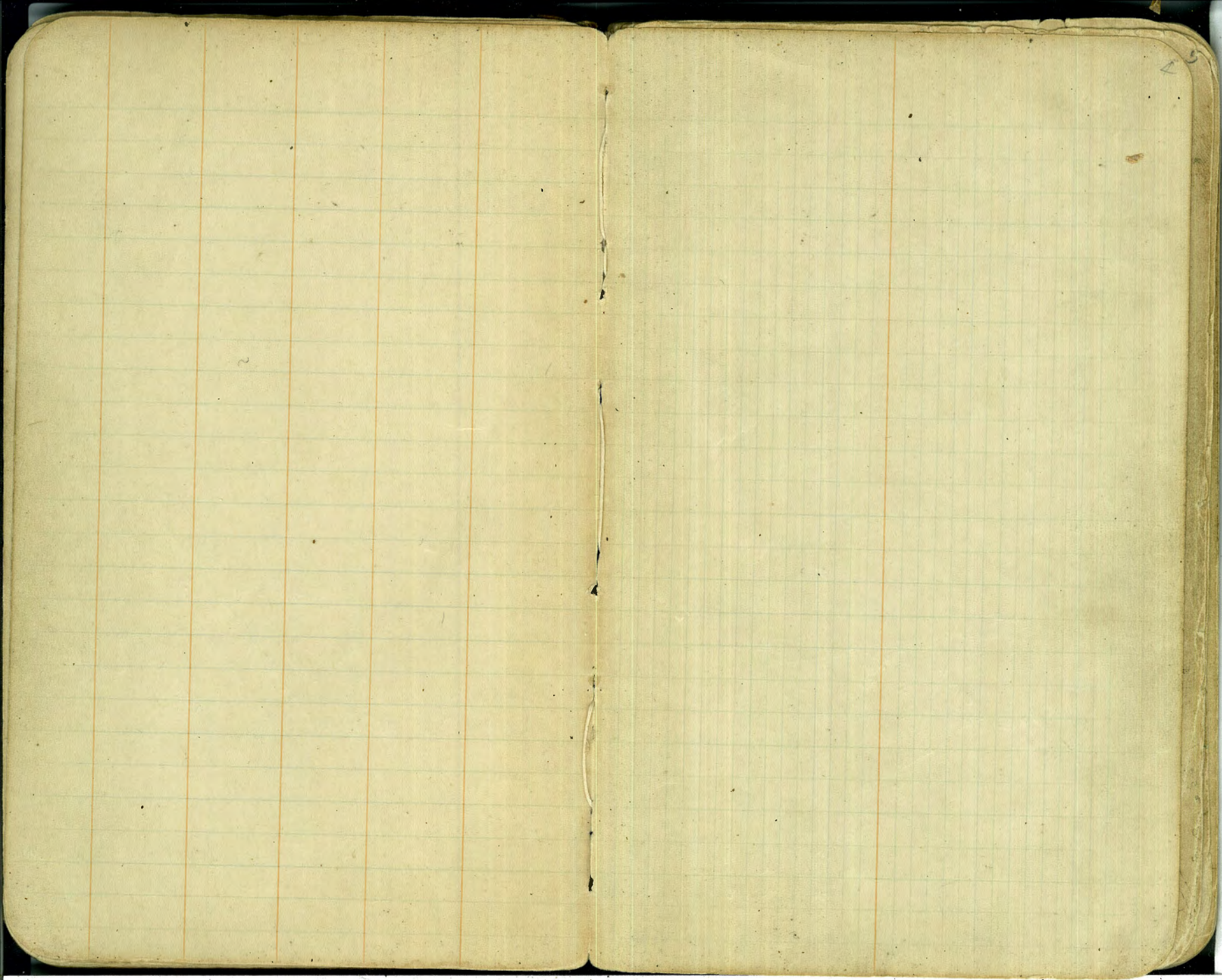
indexed  
C.S.K. Laid

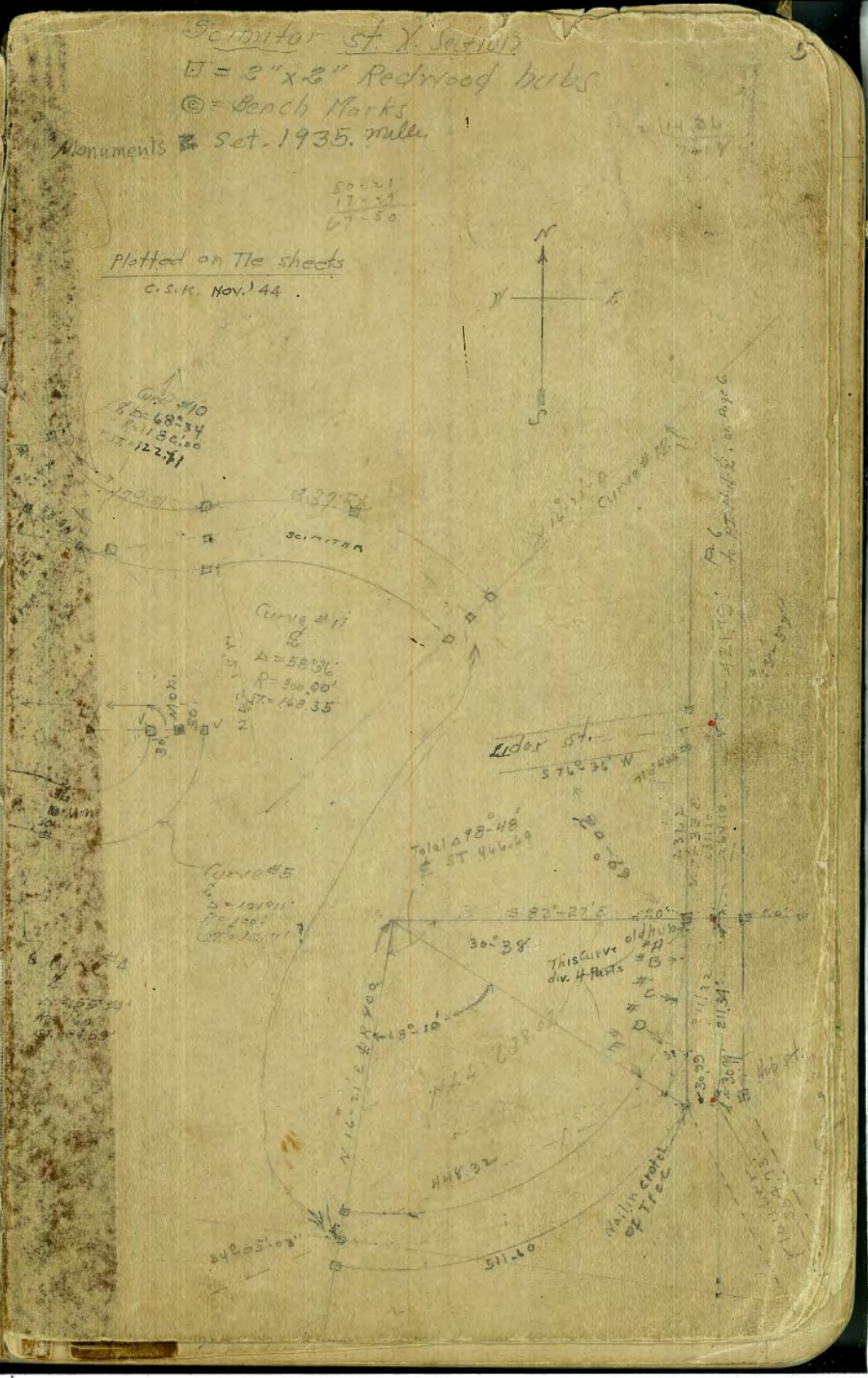
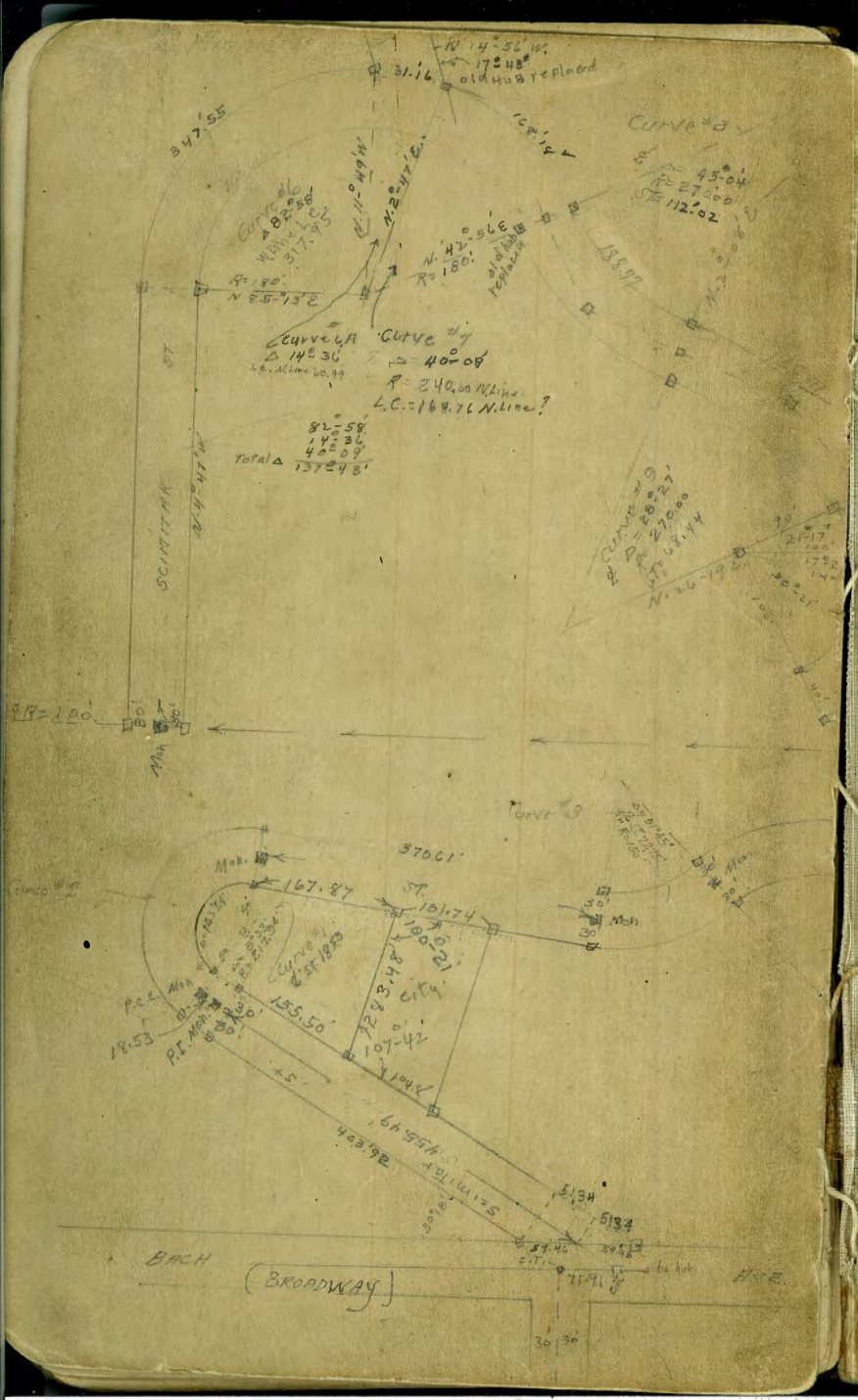
9

B.M. 393.12 N.E. BIK Cor. Scimitar + Winnet  
 397  
 X 397.09  
 12.30  
 384.79  
 0.40  
 X 385.19  
 12.15  
 373.04  
 0.20  
 X 373.24  
 12.50  
 360.74  
 0.44  
 X 361.18  
 13.01  
 348.17  
 0.58  
 X 348.72  
 12.31  
 336.41  
 0.64  
 X 336.55  
 12.94  
 323.61  
 0.67  
 X 324.28  
 12.75  
 311.53  
 0.32  
 X 312.05  
 12.96  
 299.29  
 9.08  
 X 308.37  
 7.73  
 B.M. 300.64 on hub N.E. Cor. Winnet + Radio Drive  
 X 305.37  
 0.51  
 307.86  
 13.04  
 X 320.90  
 0.38  
 320.52  
 12.82  
 X 333.34  
 2.78  
 B.M. 330.56 on hub N.E. Cor. Winnet + Orange  
 X 333.34  
 0.44  
 332.90  
 12.24  
 X 345.34  
 0.83  
 344.51  
 12.48  
 X 357.00  
 0.33  
 356.67  
 9.11  
 X 360.78  
 12.65  
 348.13  
 1.30  
 349.43

X 349.43  
 10.61  
 338.82  
 1.55  
 X 340.37  
 10.51  
 B.M. 329.86 S.W. Cor. Orange +  
 on hub Roosevelt or  
 Oriato







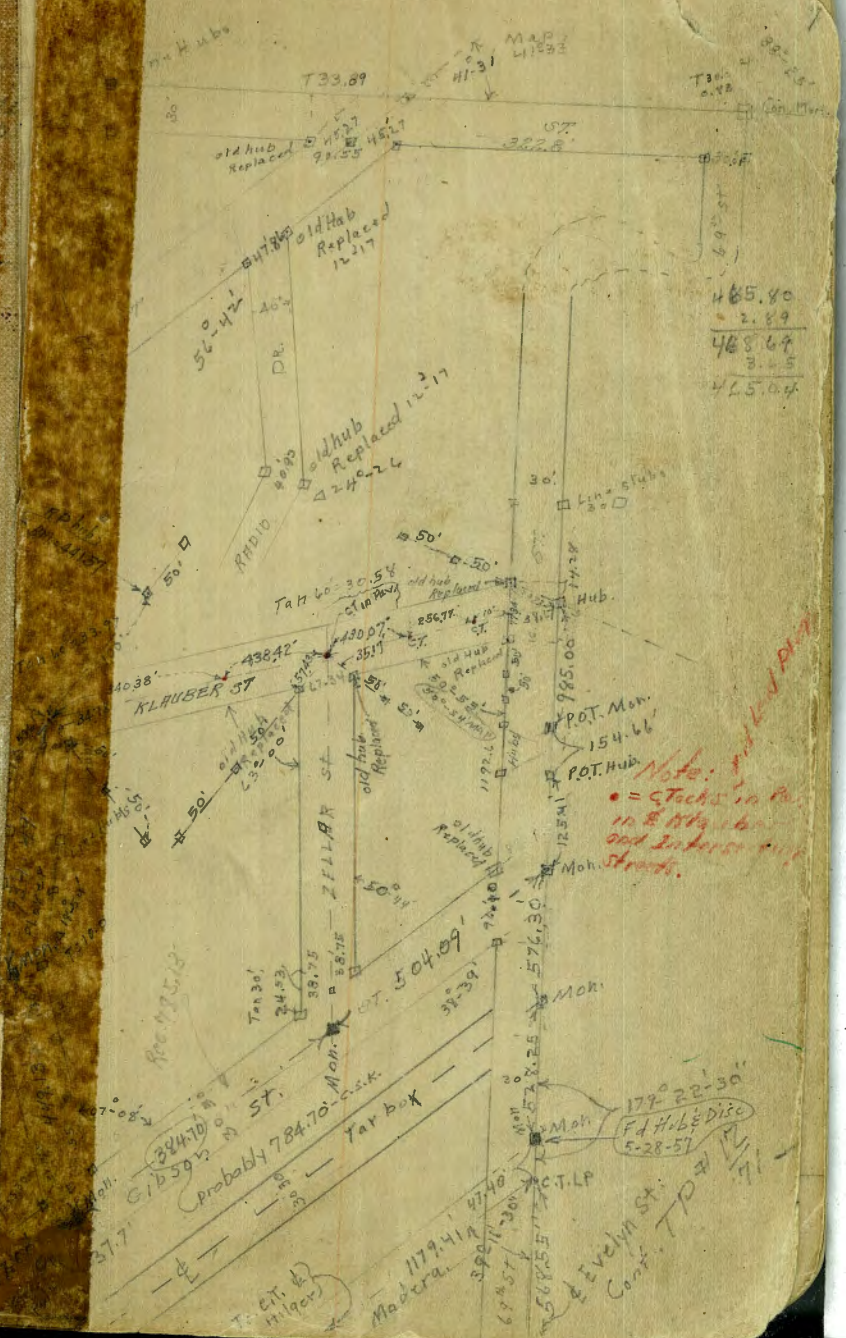




Plotted on tie sheets  
C.S.K. Nov. 144



Monuments Set. 1935.





40 wide  
 2 B. line  
 N.C. Boundary  
 10 cl  
 10 1/2

Mallard St Sec

From W. line of 69th St (60 wide x 10' ds 10' ds E. line  
 Being 30' E. of E. Boundary of City) West to  
 W. Line of Mariposa St

12-15-25  
 Miller

Mon N.E. Cor City  
 at 69th & Mallard

B.M. 0.38 465.55 465.17

00' W. Line 69th St on diagonal

N	2.3	463.3
cl	2.2	463.4
1/4	1.7	463.9
C	1.5	464.1
1/4	1.5	464.1
cl	1.5	464.1
S	1.7	463.9

Plotted 3-15-28  
 C.B.H.

30' W. on S = 31.66 W. on N = 90°

S	3.2	462.4
cl	2.7	462.9
1/4	2.3	463.3
C	2.5	463.1
1/4	2.5	463.1
cl	2.7	462.9
N	2.7	462.9

50' W. on S

N	4.2	461.4
cl	4.8	460.8
1/4	5.0	460.6
C	3.2	462.4
1/4	2.7	462.9
cl	3.0	462.6
1/2	1.8	463.8
S	2.3	463.3

City Boundary

City Boundary

City Boundary

465.55

70' W on S

S	6.1	459.5
cl	5.2	460.4
1/4	5.1	460.5
C	4.1	459.5
1/4	6.4	459.0
cl	6.4	459.0
N	6.4	459.2

City Boundary

100' W on S

N	6.3	459.3
cl	6.2	459.4
1/4	7.8	457.8
C	7.3	458.3
1/4	7.3	458.3
cl	7.6	458.0
S	7.2	458.4

120' W

S	6.1	459.5
1/8	6.5	459.1
cl	8.5	457.1
1/4	8.8	456.8
C	9.1	456.5
1/4	9.6	456.0
cl	9.1	456.5
N	9.3	456.3

465.55

135' W

N	11.4	454.2
cl	10.8	454.8
114	10.5	453.1
c	10.1	453.5
114	9.7	453.9
cl	9.6	456.0
S	8.7	456.9

155' W

S	8.4	457.2
+4	9.2	456.4
cl	11.0	454.6
114	11.2	454.4
c	11.2	454.4
114	10.3	453.3
cl	10.5	453.1
N	11.6	454.0

175' W

N	14.0	451.6
cl	13.3	452.3
114	12.9	452.7
c	12.5	453.1
114	12.3	453.3
cl	12.0	453.6
S	11.0	454.6

465.55

Mallard

10

200' W

S	10.8	454.8
cl	11.8	453.8
114	12.1	453.5
c	12.1	453.5
114	12.8	452.8
cl	13.2	452.4
N	13.6	452.0

220' W

N	12.8	452.8
cl	12.5	453.1
114	12.4	453.2
c	11.7	453.9 city boundary
114	11.6	454.0
cl	11.0	454.6
S	10.3	453.3

260' W

S	7.8	457.8
cl	8.2	457.4
114	8.8	456.8
c	8.7	456.9
114	8.1	457.5
cl	9.3	456.3
S	9.4	456.2

300' W

N	7.0	458.6
cl	6.6	459.0

465.55

300' W. (con)

1/4	6.3	459.3
c	5.9	459.7
1/4	5.8	459.8
cl	5.4	460.2
S	5.6	460.0

322.8 W. on S-E. Line Orange Ave to S. 15.09' E. S.  
 90.55' wide on Diagonal  
 15.09' E. S.  
 1/4 S.

Sections 90° from Line of Mallard

S	5.5	460.1
cl	5.8	459.8
1/4	5.8	459.8
c	5.5	460.1
1/4	5.4	460.2
cl	5.2	460.4
N	5.2	460.4

~~E. cl~~

N	4.8	460.8
cl	5.0	460.6
1/4	5.3	460.3
c	5.9	459.7
1/4	5.9	459.7
cl	5.4	460.2
S.	5.3	460.3

E. 1/4

S	5.3	460.3
cl	5.3	460.3
1/4	5.4	460.2

465.55

Mallard

c	5.8	459.8
1/4	5.9	459.7
cl	5.7	459.9
N	5.4	460.2

Orange

N	6.2	459.4
cl	6.3	459.3
1/4	6.0	459.6
c	5.8	459.8 city Boundary
1/4	5.7	459.9
cl	5.5	460.1
S	6.0	459.6

W 1/4

S	7.3	458.3
cl	6.6	459.0
1/4	6.6	459.0
c	6.4	459.2
1/4	6.6	459.0
cl	6.6	459.0
N	6.9	458.7

N. cl.

N	4.8	458.8
cl	6.8	458.8
1/4	6.5	459.1
c	5.8	459.8
+3	5.9	459.7
+5	7.3	458.3
1/4	6.9	458.7

465.55

W. eb. (con)

cl	7.1	458.5
S	6.8	458.8
oo = W. Line Orange		
S	6.9	458.7
cl	7.4	458.2
"4	7.6	458.0
H4	7.8	457.8
C	7.0	458.8
"4	6.9	458.7
cl	6.9	458.7
N	7.2	458.4
25' W		
N	7.6	458.0
cl	8.0	457.6
"4	8.1	457.5
C	7.8	457.9
"4	7.8	457.8
cl	7.5	458.1
S	8.6	457.0
55' W		
S	6.6	459.0
cl	7.8	457.8
"4	8.0	457.6
C	8.0	457.6
"4	7.7	457.9
cl	7.2	458.4
N	7.2	458.4

465.55

Mallard

12

80' W

N	7.3	458.3
cl	7.5	458.1
"4	7.9	457.7
C	8.1	457.5
"4	8.2	457.4
cl	8.4	457.2
S	8.6	457.0
100' W		
S	7.0	458.6
cl	7.0	458.6
"4	7.7	457.9
C	7.6	458.0
"4	7.9	457.7
cl	7.6	458.0
N	7.2	458.4
150' W		
N	5.8	459.8
cl	5.7	459.9
"4	6.1	459.5
C	6.6	459.0
"4	6.2	459.4
cl	6.0	459.6
S	5.8	459.8
200' W		
S	4.2	461.4
cl	4.3	461.3

city boundary

465.55  
200' W. (con)

1/4	4.8	460.8
C	5.0	460.6
1/4	4.5	461.1
cl	4.2	461.4
N	4.4	461.2

230' W.

N.	5.4	460.2
cl	6.0	469.6
1/4	6.7	468.9
C	6.7	468.9
+2	6.4	469.2
+3	7.1	468.0
1/4	6.7	468.9
cl	6.5	469.1
S	7.1	468.5

265' W.

S	11.0	454.6
cl	10.3	465.3
1/4	10.8	454.8
+5	11.2	454.4
C	10.7	454.9
1/4	10.1	455.5
cl	9.8	455.8
N	9.6	456.0
T.P.	0.24 453.71	12.78 452.77

453.71

Mallard

25

300' W.

N	0.8	452.9
cl	1.2	452.5
1/4	1.6	452.1
C	1.9	452.8
+3	2.0	451.7
+5	2.7	451.0
1/4	2.3	451.4
cl	2.2	451.5
S	2.4	451.3

325' W.

S	5.2	448.5
cl	4.1	449.6
1/4	3.9	449.8
+5	4.6	449.1
+8	2.6	451.1
C	2.4	451.3
1/4	2.5	451.2
cl	2.8	450.9
N	2.7	451.0

345' W.

N	3.6	450.1
cl	4.2	449.5
1/4	4.7	449.0
C	5.3	448.4
+3	5.4	448.3
+5	6.0	447.7



453.71  
345' W. (cont)

14	5.3	448.4
cl	5.6	448.1
S	5.7	448.0
360' W		
S	6.5	447.2
cl	6.3	447.4
114	6.5	447.2
+5	7.0	446.7
+7	5.7	448.0
C	5.4	448.3
114	4.9	448.8
cl	4.6	449.1
N	4.8	448.9
373' W.		
N	5.4	448.3
cl	5.2	448.5
114	5.0	448.7
C	5.1	448.6
+3	5.5	449.2
+5	7.8	448.9
114	7.4	446.3
cl	7.3	446.4
S	8.2	445.5
390' W		
S	9.7	444.0
cl	8.9	444.8

453.71

Mallard

14	8.7	445.0
+5	9.1	444.6
+7	8.4	445.3
C	8.3	445.4
114	7.8	445.9
cl	7.0	446.7
N	6.6	447.1
415' W.		
N	5.5	448.2
cl	6.8	448.9
114	8.6	445.1
C	9.1	444.6
city boundary		
+4	9.3	444.4
+6	10.5	443.2
114	10.1	443.6
cl	9.7	444.0
S	10.4	443.3
435' W.		
S.	13.3	440.4
cl	12.2	441.5
114	11.8	441.9
+4	12.1	441.6
+5	10.0	443.7
C	9.4	444.3
114	9.0	444.7
cl	9.2	444.5
N	8.8	444.9

453.71

450' W

N	8.3	445.4
cl	9.7	444.0
"4	10.9	442.8
c	11.7	442.0
+4	11.9	441.8
+6	13.1	440.6
"4	12.7	441.0
cl	12.7	441.0
S	14.0	439.7

475' W

S	15.4	438.3
cl	14.3	439.4
"4	13.8	439.9
+5	13.6	440.1
+8	12.4	441.3
c	12.2	441.5
"4	11.4	442.3
cl	10.6	443.1
N	10.2	443.5

485' W

N	9.6	444.1
cl	10.7	443.0
"4	11.4	442.3
c	12.0	441.7
+3	12.3	441.4
+5	13.9	439.8

453.71

Mallard.

15

"4	14.0	439.7
cl	14.8	438.9
S	15.6	438.1

500' W

S	15.8	437.9
cl	14.9	438.8
"4	14.1	439.6
+5	14.3	439.4
c	13.4	440.3
"4	12.5	441.2
cl	11.3	442.4
N	9.8	443.9

513' W

N	11.2	442.5
cl	11.3	442.4
"4	11.8	441.9
-c	12.9	440.8
+2	13.0	440.7
+5	14.3	439.4
"4	14.3	439.4
cl	14.7	439.0
S	15.9	437.8

535' W

S	15.4	438.3
cl	14.5	439.4
"4	14.2	439.5

453.71

535' W. (con)

+5	14.4	439.3
+7	13.4	440.3
c	13.4	440.3
'14	12.7	441.0
cb	11.9	441.8
N	11.5	442.2

560' W.

N	10.9	442.8
cb	10.2	443.5
'14	10.9	442.8
c	11.8	441.9
+3	12.2	441.5
+5	13.9	439.8
'14	13.4	440.3
cb	13.8	439.9
S	15.2	438.0

567' W. to 595' W. shadens. 3.8 in st.

575' W.

S	14.2	439.5
cb	13.2	440.5
'14	13.2	440.5
+5	13.3	440.7
+7	12.3	441.4
c	12.3	441.4
'14	11.3	442.4
cb	11.0	442.7
N	10.4	443.3

453.71

Mallard

16

600' W.

N	9.3	444.4
cb	8.8	444.9
'14	9.9	443.8
c	10.9	442.8
+3	11.2	442.5
+5	12.5	441.2
'14	12.3	441.4
cb	12.5	441.2
S	12.6	441.1

620' W.

S	12.0	441.9
cb	11.4	442.3
'14	11.3	442.4
+5	11.7	442.0
c	10.6	443.1 city boundary
'14	10.3	443.4
cb	10.0	443.7
N	10.0	443.7

645' W.

N	7.8	445.9
cb	8.2	445.5
'14	9.2	444.5
c	8.8	444.9
+5	9.9	443.8
'14	9.9	443.8
cb	9.9	443.8
S	10.9	442.8

453.71

657.4 W = E. Line Mariposa

90.55 W, d. on Diagonal  
15.09 cl  
15.09 1.45

S.	10.0	443.7
cl	9.7	444.0
114	9.4	444.3
+5	9.6	444.1
c	9.4	444.3
114	9.6	444.1
cl	9.4	444.3
N	9.5	444.2
E. cl		
N.	9.0	444.7
cl	9.1	444.7
114	9.4	444.3
c	9.2	444.5
114	8.7	445.0
cl	8.9	444.8
S	9.7	444.0
E. 114		
S	9.4	444.3
cl	9.0	444.7
114	9.0	444.7
c	9.2	444.5
114	9.2	444.5
cl	7.7	446.0
N	7.3	446.4
c		
N	7.8	445.9

453.71

Mallard.

cl	8.5	445.2
114	9.2	444.5
c	9.2	444.5
114	9.0	444.7
cl	8.5	445.2
S	8.9	444.8
W. 114		
S	8.8	444.9
cl	8.3	445.4
114	8.6	445.1
c	8.8	444.9
114	9.0	444.7
cl	9.1	444.6
N	9.2	444.5
W. cl.		
N	8.8	444.9
cl	8.2	445.5
114	7.7	446.0
c	7.7	446.0 city Boundary
114	8.4	445.3
114	8.1	445.6
cl	8.4	445.3
S	8.2	445.5
W. Line Mariposa.		
S	8.4	445.3
cl	8.0	445.7

453.71  
W. Line Mariposa (con)

S 114	7.8	445.9
16	8.0	445.7
2	7.1	446.6
114	7.3	446.4
26	8.0	445.7
N	8.4	445.3

60' W

N	4.4	449.3
26	4.2	449.5
114	4.2	449.5
18	4.2	449.5
2	4.8	448.9
114	4.7	449.0
26	4.6	449.1
S	4.8	448.9

city boundary

T.P.	11.67	465.31	0.07	453.64 ✓
check original B.M.			0.14	465.17 ✓

Mallard

18

60' wide  
10' elev  
16' 11" 5  
30' in City  
30' out of City

69th St X Sec  
From N. line Mallard (60' wide Being 20' N. of  
N. City Boundary

12-16-27  
Miller

B.M.	3.54	468.71	465.17	Mon N.E. cor. City
N. line Mallard - 30' N. of City Boundary				
E		2.3	466.4	
cb		2.5	466.2	
"4		3.2	465.5	
C		3.2	465.5	
"4		4.1	464.6	
cb		4.8	463.9	
W		5.5	463.2	
N. cb				
W		5.5	463.2	
cb		4.9	463.8	
"4		4.2	464.5	
C		3.6	465.1	
"4		3.2	465.5	
cb		2.6	466.1	
E		2.1	466.6	
N. "4				
E		2.0	466.7	
cb		2.5	466.2	
"4		3.0	465.7	
C		3.6	465.1	
"4		4.2	464.5	
cb		5.1	463.6	
W		4.9	463.8	

Plotted  
E.S.H.

468.71

± = N. City Boundary

W		4.7	464.0	
cb		4.5	464.2	
"4		4.5	464.2	Mon N.E. cor
C		3.6	465.1	City
"4		3.0	465.7	
cb		2.5	466.2	
E		2.0	466.7	
S. "4				
E		2.0	466.7	
cb		2.3	466.4	
"4		2.8	465.9	
C		3.5	465.2	line City
"4		4.1	464.6	
cb		4.4	464.3	
W		4.8	463.9	
S. cb				
W		4.7	464.0	
cb		4.3	464.4	
"4		4.1	464.6	
C		3.5	465.2	line City
"4		2.8	464.9	
cb		2.2	466.5	
E		1.6	467.1	
S. line Mallard 1° 35' off 90°. 0 to 2				
E		1.5	467.2	
cb		2.0	466.7	

448.71  
S. Line Mallard. (con)

1/4	2.8	465.9
e	3.8	465.9
1/4	3.8	465.9
ch	4.2	464.5
w	5.0	463.7

20' S. on W. line

w	5.0	463.7
ch	4.2	464.5
1/4	3.5	465.2
c	3.8	464.9
1/4	2.4	466.1
ch	1.9	466.8
e	1.4	467.3

45' S. on W. line

e	1.2	467.5
ch	1.8	466.9
1/4	2.4	466.3
c	3.4	465.3
1/4	3.4	465.3
ch	3.7	465.0
1/6	3.7	465.0
1/7	2.3	466.4
w	2.3	466.4

70' S

w	3.3	465.4
ch	3.0	465.7

448.71

69<sup>th</sup> St

20

1/4	2.6	466.1
c	3.1	465.6
1/4	2.5	465.2
ch	1.7	467.0
e	1.4	467.5

100' S

e	1.3	467.4
ch	2.0	466.7
1/4	2.5	466.2
c	2.7	466.7
1/4	2.3	466.4
ch	3.1	465.6
w	3.8	464.9

140' S

w	4.6	464.1
ch	3.6	465.1
1/4	2.6	466.1
c	2.6	466.1
1/4	2.5	466.2
ch	2.1	466.6
e	1.6	467.1

180' S

e	2.0	466.7
ch	2.3	466.4
1/4	2.7	466.0
c	3.3	465.4

468.71  
180'.S (cont)

1/4	2.8	465.9
eb	3.0	465.7
+3	3.2	465.5
+5	2.2	466.5
W	2.5	466.2

200'.S

W	3.6	465.1
eb	3.5	465.2
1/4	3.2	465.5
E	3.6	465.1
1/4	2.9	465.8
eb	2.6	466.1
E	2.3	466.4

235'.S

E	2.8	465.9
eb	3.0	465.7
1/4	3.3	465.4
E	3.7	465.0
1/4	3.5	465.2
eb	3.8	464.9
W	3.5	465.2

255'.S

W	3.7	465.0
eb	4.1	464.6
1/4	3.3	465.4
E	2.9	465.8

468.71

69<sup>th</sup> St

+2	3.0	465.7
+3	3.7	465.0
1/4	3.4	465.3
eb	3.2	465.5
E	3.0	465.7

300'.S

E	3.4	465.3
eb	3.8	464.9
1/4	4.3	464.4
E	4.7	464.0
1/4	4.1	464.6
eb	4.0	464.7
W	4.4	464.3

350'.S

W	5.0	463.7
eb	4.9	463.9
1/4	4.8	463.9
E	5.0	463.7
1/4	4.7	464.0
eb	4.3	464.4
E	4.0	464.7

400'.S

E	4.4	464.3
eb	4.8	463.9
1/4	5.1	463.6
E	5.0	463.7



448.71

400' S. (con)

1/4	5.2	463.5
ch	5.1	463.6
W	5.0	463.7

430' S.

W	6.4	462.8
ch	6.4	462.3
1/4	5.2	463.5
C	4.7	464.0
1/4	5.4	463.3
ch	5.0	463.7
E	4.7	464.0

470' S

E	5.0	463.7
ch	5.2	463.5
1/4	6.1	462.6
C	5.2	463.5
1/4	5.6	463.1
ch	6.8	461.9
W	6.4	462.1

500' S

W	6.9	461.8
ch	6.3	462.4
1/4	7.1	461.6
C	7.2	461.5
1/4	7.4	461.3
1/4	6.3	462.4

468.71

69' ST

77

ch	5.9	462.8
E	5.4	463.3

540' S

E	5.9	462.8
ch	6.4	462.3
1/4	7.0	461.7
1/5	8.3	460.4
C	8.1	460.6
1/4	8.3	460.4
ch	9.6	459.1
W	10.5	458.2

560' S

W	11.1	457.6
ch	9.3	459.4
1/4	8.3	460.4
C	7.9	460.8
1/4	8.4	460.3
1/4	7.3	461.4
ch	6.7	462.0
E	6.2	462.4

600' S

E	6.0	462.7
ch	6.7	462.0
1/4	7.6	461.1
1/6	9.0	459.7
C	8.9	459.8

469.71

600' S. (cont)

114	9.2	459.5
cl	10.8	457.9
W	11.6	457.1

625' S.

W	10.2	458.5
cl	8.6	460.1
114	9.0	459.7
E	8.8	459.9
+4	8.8	459.9
114	7.3	461.4
cl	6.4	462.3
E	5.9	462.8

640' S.

E	5.8	462.9
cl	6.3	462.4
114	7.2	461.6
+6	8.5	460.2
E	8.6	460.1
114	9.0	459.7
cl	9.8	458.9
W	11.6	457.1

665' S.

W	9.3	459.4
cl	8.0	460.7
114	8.5	460.2
E	8.1	460.6

468.71

690' S

23

114	7.1	461.6
cl	6.2	462.5
E	5.6	463.1

690' S.

E	5.6	463.1
cl	6.1	462.6
114	6.6	462.1
E	7.1	461.6
114	7.8	460.9
+2	8.1	460.6
+7	10.1	458.6
cl	10.5	458.2
W	11.6	457.1

725' S.

W	11.4	457.3
cl	8.1	460.6
+16	7.5	461.2
+7	8.2	460.5
114	7.9	460.8
E	8.0	460.7
+4	8.1	460.6
114	6.9	461.8
cl	3.1	462.6
E	5.7	463.0

468.71  
760'.5

E		5.7	463.0
ch		6.3	462.4
"4		7.1	461.6
C		7.7	461.0
"4		8.8	459.9
+6		10.7	458.0
ch		11.1	457.6
W		12.0	456.7
T.P.	4.82	465.31'	8.22 460.49'

800'.5

W		7.7	457.6
ch		7.4	457.9
"4		5.4	459.9
C		4.7	460.6
+5		4.9	460.4
"4		3.9	461.4
ch		3.0	462.3
E		2.3	463.0

825'.5

E		2.3	463.0
ch		2.9	462.4
"4		3.7	461.6
+7		5.0	460.3
C		4.8	460.5
"4		4.9	460.4
ch		5.1	460.2

465.31

69<sup>th</sup> ST.

24

W		6.6	458.7
		8.70'.5	
N		4.3	461.0
ch		3.8	461.5
"4		3.4	461.9
C		3.0	462.3
+5		3.3	462.0
"4		2.5	462.8
ch		2.0	463.3
E		1.4	463.9

900'.5

E		0.8	464.5
ch		1.3	464.0
"4		1.6	463.7
+5		2.5	462.8
C		2.1	463.2
"4		2.7	462.6
ch		3.4	461.9
N		3.8	461.5

940'.5

N		2.4	462.9
ch		2.2	463.1
"4		1.4	463.5
C		1.2	464.1
"4		1.5	463.8
ch		0.4	464.5
E		0.3	465.0

465.31

970'S

E	0.2	465.1
eb	0.4	464.7
"4	1.1	464.2
F5	2.2	463.1
E	2.0	463.3
"4	1.5	463.5
eb	1.4	463.9
W	1.5	463.8

1000'S

W	2.7	462.6
eb	2.7	462.6
"4	2.7	462.6
E	2.4	462.9
+4	2.9	462.4
"4	1.7	463.6
eb	1.3	464.0
E	0.8	464.5

1030'S

E	3.2	462.1
eb	3.2	462.1
"4	3.7	461.6
E	4.4	460.9
"4	4.2	461.1
eb	4.0	461.3
W	3.7	461.6

465.31

1055'S

W	5.3	460.0
eb	5.4	459.9
F2	6.3	459.0
"4	6.2	459.1
E	6.2	459.1
F4	6.5	458.8
eb	6.9	458.4
E	7.0	459.3

1067'S = 90° from N.W. Cor. 69<sup>th</sup> + Klauker

E	9.5	455.8
eb	9.2	456.1
eb	8.8	456.5
E	8.1	457.2
"4	7.6	457.7
eb	7.7	457.6
W. on Hub B.M.	7.42	457.89 = 457.90 + Klauker

N. eb. at 90° from line of 69<sup>th</sup>

N	9.3	456.0
eb	9.1	456.2
"4	9.2	456.1
E	10.3	455.0
"4	10.9	454.4
eb	11.4	453.9
E	11.7	453.6

69<sup>th</sup> ST

25

on diagonal

77.34 wide  
11.9 eb-3  
12.9 445N.W. Cor 69<sup>th</sup>

46531

N. 114

E	13.4	451.9
cl	13.6	451.7
114	13.1	452.2
E	12.4	452.9
114	11.0	454.3
cl	10.1	455.2
W	10.2	455.1

Klauber

W	10.5	454.8
cl	11.4	453.9
114	12.6	452.7
C	14.0	451.3
114	15.4	449.9
cl	15.7	449.6
E	15.2	450.1

S. 114

E	17.2	448.1
cl	17.6	447.7
114	16.7	448.6
E	15.2	450.1
114	14.0	451.3
cl	13.9	451.4
W	12.6	452.7

T.P. 0.65 453.27<sup>v</sup> 12.69 452.62

S. cl

W 1.7 451.6

453.27

69.25

26

cl.	3.0	450.3
114	3.6	449.7
E	4.1	449.4
114	6.4	446.9
cl	8.4	444.9
E	8.7	444.6

0.0 - S. line of Klauber at 90° from 69<sup>th</sup>

E	12.0	441.3
cl	10.2	443.1
114	8.6	444.7
E	7.0	446.3
114	4.7	448.6
cl	4.3	449.0
15	1.7	451.6
W.	1.7	451.6

30'S

W	3.4	449.9
cl	5.5	447.8
13	6.3	447.0
114	6.2	447.1
14	6.2	447.1
E	7.9	445.4
114	9.9	443.4
cl	12.0	441.3
E	14.7	438.6

45' S. of S. line Klanber

E	10.2	437.1
d	13.1	440.2
114	11.0	442.3
C	8.8	444.5
+5	6.6	446.7
114	6.6	446.7
+6	6.6	446.7
cl	4.7	448.6
W	3.3	450.0

65' S

W	3.2	450.1
cl	4.8	448.5
+3	6.7	446.6
114	6.6	446.7
+6	6.6	446.7
C	7.6	445.7
114	11.0	442.3
cl	13.7	439.6
C	16.1	437.2

85' S

E	17.5	435.8
cl	17.5	438.8
114	11.5	441.8
C	8.8	444.5
+	6.6	446.7
114	6.6	446.7

+6	6.5	446.8
cl	4.7	448.6
W	3.4	449.9

110' S

W	2.9	450.4
cl	4.3	449.0
+4	6.6	446.7
114	6.3	447.0
+8	6.1	447.2
C	7.3	446.0
114	9.5	443.8
cl	13.2	440.1
E	16.9	436.4

140' S

E	18.3	435.0
cl	15.1	438.2
114	11.9	441.4
C	8.8	444.5
+5	6.8	446.5
114	6.9	446.4
+	6.9	446.4
cl	4.8	448.5
W	3.6	449.7

160' S

W	3.4	449.9
cl	4.1	449.2

453.27  
160' S. (cont)

+4	7.5	445.8
"4	7.5	445.8
+6	7.7	445.6
c	9.5	443.8
"4	12.0	441.3
cl	14.3	439.0
E	17.1	436.2

200' S

E	18.8	434.5
cl	16.4	436.9
"4	14.1	439.2
c	11.7	441.6
+5	9.2	444.1
"4	9.1	444.2
+6	9.2	444.1
cl	6.1	447.2
W	5.5	447.8

225' S

W	6.4	446.9
cl	7.9	445.4
+4	10.9	442.4
"4	10.7	442.6
+5	10.8	442.5
c	12.6	440.7
"4	15.0	438.3
cl	17.9	435.4
E	20.6	432.7

453.27  
260' S

69" 5"

36

E	23.5	429.8
cl	20.5	432.8
"4	18.0	435.3
c	15.7	437.6
+5	13.3	440.0
"4	13.5	439.8
+5	13.4	439.9
cl	10.6	442.7
W	9.1	444.2

300' S

W	12.2	441.1	
T.P. 2.06	442.47	12.86	440.41
cl	3.3	439.2	
+3	5.7	436.8	
"4	6.0	436.5	
+3	6.0	436.5	
c	9.0	433.5	
"4	12.6	429.9	
cl	15.0	427.5	
E	17.2	425.3	

315' S

E	18.8	423.7
cl	16.8	425.7
"4	14.0	428.5
c	9.6	432.9
+6	7.0	435.5

442.47

315' S (con)

"4	7.6	434.9
+8	7.6	434.9
ch	5.8	436.7
+2	4.3	438.2
W	2.8	439.7

345' S

W	8.0	434.5
+3	8.0	434.5
ch	12.3	420.2
"4	12.4	420.1

T.P. R.31 431.88 12.90 429.57 ✓

E 4.7 427.2 city boundary

"4	6.8	425.1
ch	9.3	422.6
E	11.6	420.3

375' E

E	15.0	416.9
ch	12.8	419.1
"4	10.3	421.6
E	8.7	423.2
"4	5.2	426.7
ch	5.0	426.9
+2	2.8	429.1
W	0.4	431.5

431.88

69<sup>th</sup> ST

69

400' S

W	1.4	430.5
+7	3.6	428.3
ch	6.4	425.5
"4	7.4	424.5
+6	8.5	423.4
E	10.1	421.8
"4	13.1	418.8
ch	15.8	416.1
E	18.2	413.7

450' S

E	20.5	411.4
ch	18.0	413.9
"4	15.1	416.8
E	12.0	419.9
"4	8.3	423.6
ch	7.3	424.6
+2	7.3	424.6
W	2.8	429.1

500' S

W	40.6	432.5
ch	2.4	429.5
+4	5.5	426.4
"4	5.9	426.0
+7	6.2	425.7
E	7.7	424.0
"4	11.5	420.4



431.88

500' S. con

cb	14.0	417.9
E	16.8	415.1

520' S

E	15.9	416.0
cb	12.7	419.2
"4	9.4	422.5
C	6.0	425.9
+3	4.9	427.0
"4	5.2	426.7
+4	5.0	426.9
cb	1.9	43.9
W	+1.0	432.9

545' S.

W	+1.8	433.7
cb	1.2	430.7
+4	4.1	427.8
"4	4.3	427.6
+6	4.6	427.3
E	6.2	425.7
"4	8.9	423.0
cb	11.7	420.2
E	14.8	417.1

575' S.

E	12.7	419.2
cb	9.9	422.0
"4	7.2	424.7

431.88

29<sup>th</sup> 54

30

C	4.5	427.4
+4	2.8	429.1
"4	2.7	429.2
+6	2.6	429.3
T.P.	8.35	437.91
cb	5.9	432.0
W	3.0	434.9

600' S.

W	2.2	435.7
cb	5.1	432.8
+6	7.7	430.2
"4	8.0	429.9
+7	7.8	420.1
C	9.2	428.7
"4	12.4	426.5
cb	14.8	423.1
E	17.4	420.5

650' S

E	15.6	422.3
cb	13.0	424.9
"4	10.4	427.5
C	8.1	429.8
+4	6.3	431.6
"4	6.3	431.6
+4	6.1	431.8
cb	3.4	434.5
W	1.4	436.5

437.91

690's

N	1.0	436.9
cb	2.9	435.0
+5	4.4	434.5
"4	4.6	433.3
+6	4.8	433.4
c	6.4	431.5
"4	9.2	428.7
cb	11.7	426.2
E	13.9	424.0

725's

E	12.6	425.3
cb	10.3	427.6
"4	7.7	430.2
c	4.0	433.9
+3	2.7	435.2
"4	2.9	435.0
+4	2.9	435.0
cb	0.0	437.9
W	+1.4	439.3

760's

W	1.9	436.0
cb	3.2	435.7
"4	4.3	435.6
+6	4.8	433.1
c	6.0	431.9
"4	8.3	429.6

437.91

690's

3)

cb	10.2	427.7
E	12.0	425.9

800's

E	11.3	426.6
cb	9.6	428.3
"4	8.0	429.9
c	6.0	431.9
+5	5.3	432.6
"4	5.3	432.6
+5	5.3	432.6
cb	3.6	434.3
W	2.6	435.3

850's

W	4.3	433.6
cb	4.9	433.0
"4	5.9	432.0
c	6.2	431.7
"4	7.9	430.9
cb	8.9	429.0
E	10.0	427.9

900's

E	10.8	427.1
cb	9.4	428.5
"4	8.3	429.6
c	7.2	430.7
"4	6.9	431.0

437.91

900' S (con)

cb	6.7	431.2
W	6.8	431.1
925' S		
W	8.5	429.4
cb	8.5	429.4
"14	8.2	429.7
E	8.3	429.6
"14	9.1	428.8
cb	10.1	427.8
E	11.5	426.4

955' S

E	13.0	424.9
cb	12.0	425.9
"14	11.3	426.6
E	10.9	427.0
"14	10.7	427.2
cb	10.5	427.4
W	10.6	427.3
T.P.	0.59	425.46
	13.04	424.87

1000' S

W	4.2	421.3
cb	3.1	422.4
"14	2.7	422.8
E	2.4	423.1
"14	2.8	422.7
cb	3.5	422.0
E	4.0	421.5

425.46

1025' S

E	5.0	420.5
cb	5.3	420.2
"14	5.3	420.2
E	5.1	420.4
"14	5.8	419.7
cb	5.5	420.0
W	6.5	419.0

1040' S

W	12.4	413.1
cb	11.7	413.8
"14	11.6	413.9
E	11.3	414.2
"14	11.2	414.3
cb	11.4	414.1
E	11.9	413.6
T.P.	0.21	412.71
	12.96	412.50

1100' S

E	5.7	407.0
cb	5.1	407.6
"14	4.7	408.0
E	4.4	408.3
"14	5.5	407.2
cb	5.1	407.6
W	6.2	406.5
T.P.	0.09	400.54
	12.26	400.45

69<sup>th</sup> St

32

400.54

1150.5

W	6.5	394.0
cb	5.9	393.6
"14	5.5	395.0
c	4.9	395.6
"14	4.7	395.8
cb	4.8	395.7
E	5.4	395.1

1192.6 S. = N. Line Gibson 90° from line of 19<sup>th</sup>

T.P.	0.44	388.09	12.89	387.65
E			1.7	386.4
cb			1.5	386.6
"14			1.5	386.6
c			1.7	386.4
"14			2.4	385.7
cb			2.2	385.9
W			3.0	385.1

N. 26

W	6.2	381.9
cb	5.6	382.5
"14	5.9	382.2
c	5.2	382.9
"14	4.9	383.2
cb	5.0	383.1
E	5.2	382.9

388.09

19<sup>th</sup> ST

N. 14

E	8.3	379.8
cb	8.2	379.9
"14	8.3	379.8
c	8.3	379.8
"14	8.7	379.4
cb	9.0	379.1
W	9.3	378.8

E Gibson

W	12.6	375.5		
cb	12.2	375.9		
"14	11.5	376.6		
c	11.4	376.7		
"14	11.3	376.8		
cb	11.1	377.0		
E	11.4	376.7		
T.P.	0.14	375.27	12.96	375.13

S. 14

E	1.6	373.7
cb	1.7	373.6
"14	1.5	373.8
c	1.5	373.8
"14	1.4	373.9
cb	1.9	373.4
W	2.8	372.5

5 cb.

W	5.6	369.7
cb	4.9	370.4
114	4.3	370.0
E	4.5	370.8
1/4	4.7	370.9
cb	4.8	370.5
E	4.6	370.7

S. Line Gibson

E	7.7	377.6
cb	7.2	377.6
114	7.5	377.8
E	7.9	377.4
1/4	8.1	377.2
cb	8.2	377.1
W	8.8	376.5

sw. cor 69<sup>th</sup>  
+ Gibson

50'5'

W	17.0	358.3
E	16.7	359.6
E	15.9	359.4
T.P.	1.10	363.55
T.P.		12.82
	0.20	363.35

N.W. 21K Hub  
Zeller + Gibson

60' w. d.  
10' d. s.  
10' 1/4 s.

ZELLAR ST X Sec  
Gibson to Klauber

12-16-27  
Miller

T.P. Page 34

13.05 376.40

363.35

N.W. 1/4 Hub  
Zellar + Gibson

N. Line Gibson on diagonal

77.50 w. d.  
12.9 d. s.  
12.9 1/4 s.

W	12.1	364.3
cb	13.1	363.3
"4	16.0	360.4
E	17.4	359.0
"4	19.0	357.4
cb	21.0	355.4
E	21.6	354.8
00 =	4 2.06 Non W = opposite N.E. Cor	
E	21.6	354.8
cb	20.5	355.9
"4	18.2	358.2
E	16.2	360.2
"4	13.2	363.2
cb	10.9	365.5
W	8.4	368.0

50' N. of 00

W	2.4	374.4
cb	5.6	370.8
"4	9.5	366.9
E	12.3	364.1
"4	14.8	361.6
cb	17.1	359.3
E	18.7	357.7

Platted 3-13-28  
C. H. Hough

376.40

100' N. of 0.0

35

E	16.3	360.1
cb	14.0	362.4
"4	11.7	364.7
E	9.4	367.0
"4	7.0	369.4
cb	3.8	372.6
W	0.2	376.2

150' N of 00

W	0.1	376.3
cb	3.5	372.9
"4	5.4	371.0
E	7.3	369.1
"4	8.9	367.5
cb	11.6	364.8
E	14.1	362.3

175' N

E	14.4	362.0
cb	12.1	364.3
"4	10.0	366.4
E	7.9	368.5
"4	2.3	374.1
cb	0.1	376.3
W	+2.5	378.9

T.P. 12.14 379.76 8.78 367.62

379.76

200' N. of 00.

W	1.3	378.5
cb	5.1	374.7
"4	8.2	371.6
C	11.1	368.7
"4	13.3	366.5
cb	15.4	364.4
E	17.3	362.5

250' N

E	16.8	363.0
cb	14.3	365.5
"4	12.5	367.3
C	10.5	369.3
"4	8.2	371.6
cb	5.8	374.0
W	2.8	377.0

300' N

W	3.7	376.1
cb	5.7	374.1
"4	7.6	372.2
C	10.2	369.1
"4	12.0	367.8
cb	13.8	366.0
E	15.8	364.0

350' N

E	15.2	364.6
cb	13.1	366.7

379.76

Zellar. St

36

"4	11.2	368.6
C	9.5	370.3
"4	7.3	372.5
cb	5.4	374.4
W	3.6	376.2

400' N

W	4.1	375.7
cb	5.6	374.2
"4	7.1	372.7
C	8.6	371.2
"4	9.9	369.9
cb	11.6	368.2
E	13.5	366.3

450' N

E	12.6	367.2
cb	11.2	368.6
"4	9.6	370.2
C	8.4	371.4
"4	6.7	373.1
cb	5.6	374.2
W	4.2	375.6

500' N

W	4.4	375.2
cb	6.0	373.8
"4	7.6	372.2
C	8.9	370.9

379.76  
500' N. (con)

'14	9.7	370.1
cl	10.7	369.1
E	11.7	368.1

550' N

E	9.0	370.8
cl	7.6	372.2
'14	6.7	373.1
C	6.4	373.4
'14	5.6	374.2
cl	4.8	375.0
W	3.6	376.2

600' N

W	0.2	379.6
cl	1.2	378.6
'14	2.2	377.6
C	3.2	376.6
'14	4.0	375.8
cl	4.7	375.1
E	5.7	374.1

650' N

E	1.2	378.6			
cl	0.1	379.7			
T.P.	13.04	392.80	0.00	379.76	Nail in Post
'14			12.5	380.3	
C			11.7	381.1	
'14			10.9	381.9	

392.80

Zellar St

37

cl	9.9	382.9
W	8.6	384.2

700' N

W	2.5	392.3
cl	3.4	389.4
'14	4.6	388.2
C	5.4	387.4
'14	6.4	386.4
+3	7.9	384.9
cl	7.6	385.2
E	9.3	383.5

750' N

E	3.0	389.8		
cl	1.0	391.8		
T.P.	12.84	405.27	0.37	392.43
'14			13.2	392.1
+1			11.6	393.7
C			10.0	395.3
'14			8.4	396.9
cl			6.9	398.4
W			5.3	400.0

800' N

W	+4.8	410.1
cl	+2.0	407.3
'14	0.2	405.1
C	2.8	402.5



405.27

800' N con

1/4	5.0	400.3
+2	6.8	398.5
cb	7.0	398.3
E	8.9	396.4

835' N

E	5.0	400.3
W	2.7	402.6
+6	2.5	402.8
+8	0.7	404.6

TP	12.72	417.66	0.33	404.94
----	-------	--------	------	--------

1/4	12.5	405.2
C	10.6	407.7
1/4	7.7	410.0
cb	4.9	412.8
W	1.6	416.1

865' N

W	+2.6	420.3
cb	+0.5	418.2
1/4	3.2	414.5
C	5.9	411.8
1/4	8.3	409.4
+3	9.0	408.7
+5	10.9	406.8
cb	10.9	406.8
+3	11.3	406.4
E	14.5	403.2

417.66

900' N

E	9.9	417.8
cb	6.7	411.0
+6	6.4	411.3
+8	4.4	413.3
1/4	3.7	414.0

C	0.6	417.1
---	-----	-------

T.P.	12.70	430.18	0.18	417.48
------	-------	--------	------	--------

1/4	10.7	419.5
-----	------	-------

cb	8.1	422.1
----	-----	-------

W	5.4	424.8
---	-----	-------

925' N

W	3.4	426.8
---	-----	-------

cb	5.8	424.8
----	-----	-------

1/4	8.2	422.0
-----	-----	-------

C	11.1	419.1
---	------	-------

+8	14.0	416.2
----	------	-------

1/4	16.3	413.9
-----	------	-------

cb	17.2	413.0
----	------	-------

E	19.2	411.0
---	------	-------

950' N

E	15.3	414.9
---	------	-------

cb	13.6	416.6
----	------	-------

1/4	12.7	417.5
-----	------	-------

+2	11.2	419.0
----	------	-------

C	9.4	420.8
---	-----	-------

1/4	6.6	423.6
-----	-----	-------

Zellar St

38

430.18

950' N (con)

cb		3.9	426.3
W		2.5	427.7
1000' N			
W		42.0	432.2
cb		40.4	430.6
1/4		1.1	429.1
C		2.0	428.2
1/4		3.4	426.8
+1		4.2	426.0
cb		4.4	425.8
E		5.4	424.8
T.P.	12.42 442.51	0.09	430.09

1050' N

E		8.8	433.7
cb		8.5	434.0
1/4		8.2	434.3
+1		7.8	434.7
C		7.5	435.0
1/4		6.7	435.8
cb		5.9	436.6
W		4.4	438.1

1075' N

W		1.9	440.6
cb		2.9	439.6
1/4		3.8	438.7
C		4.3	438.2

442.51

Zellar St

39

1/4		4.5	438.0
+1		5.4	437.1
cb		5.3	437.2
E		4.7	437.8
1095' N			
E		2.1	440.4
cb		2.5	440.0
1/4		3.0	439.5
C		3.0	439.5
1/4		3.0	439.5
cb		2.5	440.0
W		2.0	440.5

1110.5' N = 90° from S.W. Cor Zellar + Klauber  
 = 20.58' S. of S.E. Cor of Zellar + Klauber

W		3.3	439.2 + Klauber
cb		3.4	439.1
1/4		3.2	439.3
C		2.8	439.7
1/4		2.3	440.2
cb		2.0	440.5
E		1.4	441.1
S. line Klauber { 67.34 wide on diagonal 112' etc 112' 1/2			
E		1.7	440.8 + Klauber
cb		2.4	440.1
1/4		3.0	439.5
C		3.3	439.2
1/4		3.4	439.1

442.51

S. Line Klauber (con)

W

3.7

438.8

S.W. Cor Zellar

W

3.3

439.2

4 Klauber

PhKonEM

2.01

440.50

Zellar + Klauber

Zellar ST

40



449.69

100' S. com

"4	4.4	445.1
cl	6.4	443.3
W	7.4	442.3

120' S.

W	6.9	442.8
cl	6.6	443.1
"4	5.5	444.2
C	4.8	444.9
"4	4.8	444.9
cl	3.7	446.0
E	2.2	447.8

140' S.

E	3.6	446.1
cl	4.2	445.5
"4	4.7	445.0
C	4.7	445.0
"4	5.3	444.4
cl	5.9	443.8
W	4.4	443.3

165' S.

W	6.1	443.6
cl	5.4	444.3
"4	4.4	445.3
C	4.3	445.4
"4	4.1	445.6
cl	3.8	445.9
E	3.2	446.5

449.69

185' S

E	1.7	448.0
cl	1.8	447.9
"4	3.9	445.8
C	4.5	445.2
"4	4.7	445.0
cl	5.4	444.3
W	6.1	443.6

200' S

W	5.9	443.8
cl	5.2	444.5
"4	4.3	445.4
C	4.3	445.4
"4	3.9	445.8
cl	2.8	446.9
E	2.5	447.2

250' S

E	3.1	446.6
cl	4.0	445.7
"4	4.0	445.7
C	4.5	445.2
"4	5.0	444.7
cl	5.7	444.0
W	6.3	443.4

300' S

W	7.9	441.8
cl	8.0	441.7

Plover

46

449.69

300' S. 20h

14	7.7	442.0
C	7.8	441.9
+4	7.4	441.9
+7	6.4	443.3
14	6.1	443.6
cl	5.5	444.2
E	4.9	444.8
T.P.	4.26	443.36
	10.59	439.10

350' S.

E	1.5	441.9
cl	2.1	441.3
14	2.5	440.9
+3	3.0	440.4
+4	4.1	439.3
E	3.8	439.6
14	4.6	438.8
cl	5.1	438.3
W	5.5	437.9

375' S.

W	7.9	435.5
cl	7.3	436.1
14	6.5	436.9
C	6.3	437.1
+5	6.2	437.2
+7	4.8	438.6
14	4.7	438.7

443.36

Plover ST

43

cl	3.5	439.9
E	2.9	440.6

410' S

E	4.8	438.6
cl	6.1	437.3
14	7.6	436.8
+2	8.4	435.0
C	8.5	434.9
14	8.9	434.5
cl	9.6	433.8
W	10.8	432.6

455' S

W	11.0	429.4
cl	12.6	430.8
14	11.1	432.3
C	10.4	433.0
+5	10.4	433.0
14	9.1	434.3
cl	8.1	435.3
E	6.6	436.8

500' S

E	7.1	436.3
cl	8.3	438.1
14	10.5	432.9
C	10.6	432.8
cl	10.8	432.6

443.36  
500's. (con)

ch	13.3	430.1
w	14.7	428.7

550's.

w	12.5	430.9
ch	11.3	432.1
"4	9.6	433.8
c	9.7	433.7
"4	8.7	434.7
ch	6.7	436.7
e	5.1	438.3

600' E

e	2.7	440.7
ch	4.0	439.4
"4	5.1	438.3
"4	6.2	437.2
c	6.7	436.7
"4	6.9	436.5
ch	7.9	435.5
w	8.6	434.8

625's.

w	7.3	436.1
ch	6.4	437.0
"4	5.5	437.9
c	5.1	438.3
+5	5.1	438.3
"4	3.2	440.2

443.36

Plover St.

44

ch	2.5	440.9
E	1.3	442.1

665's.

E	1.0	442.4
ch	1.7	441.7
"4	2.5	440.9
c	3.3	440.1
"4	4.0	439.4
ch	4.7	438.7
w	5.3	438.1

715's

w	4.8	438.6
ch	4.3	439.1
"4	3.6	439.8
c	3.5	439.9
"4	2.5	440.9
ch	1.9	441.5
E	1.3	442.1

765' E.

E	3.4	440.0
ch	4.0	439.4
"4	4.6	438.8
c	5.3	428.1
"4	5.5	437.9
ch	6.0	437.4
w	6.2	437.2

443.36

800' S.

W	7.4	436.0
cl	7.2	436.2
"4	7.2	436.2
c	7.2	436.2
"4	6.8	436.6
cl	6.4	437.0
E	6.2	437.2

825' S.

E	8.0	435.4
cl	8.4	435.0
"4	8.3	435.1
C	9.0	434.4
T.P.	1.31	435.62
"4	9.05	434.31
"4	1.0	434.6
cl	0.8	434.8
W	1.4	434.2

860' S.

W	3.7	431.9
cl	3.8	431.8
"4	4.6	431.0
C	4.3	431.3
"4	3.5	432.1
cl	3.8	431.8
E	3.8	431.8

435.62

878.9' S. on E + 888.9' S. on W =  $\Delta$  18° 54' on split Tah for 60' = 10.0

Flower St

45

E	6.3	429.3
cl	6.1	429.5
"4	6.4	429.2
C	6.86	428.76
"4	6.5	429.1
cl	6.5	429.1
W	6.7	428.9

90° from  $\Delta$  on E. Line = 10' S. of  $\Delta$  on W. Line = 5th 0.00  
 30' S. of  $\Delta$  on E = 40' S. of  $\Delta$  on W = 30' S. of op

W	10.9	424.7
cl	10.6	425.0
"4	11.5	424.1
C	11.8	423.8
+2	11.8	423.8
+3	10.1	425.7
"4	10.0	425.6
cl	10.2	425.4
C	10.3	425.3

T.P. 0.12 423.33 12.41 423.21<sup>u</sup>

60' S. of 0.0

E	4.3	419.0
cl	4.4	418.9
"4	4.4	418.9
C	5.2	418.1
"4	5.2	418.1
cl	4.7	418.6
W	4.2	419.1



423.33

61'. S of 00

w	4.6	418.7
cb	5.0	418.3
"4	5.6	417.7
c	5.6	417.7
"4	4.8	418.5
cb	4.6	418.7
+5	5.4	417.9
+7	7.5	415.8
E	7.9	415.4

80'. S

E	9.3	414.0
cb	9.4	413.9
"4	9.4	413.9
c	9.2	414.1
"4	9.1	414.2
cb	8.8	414.5
w	8.3	415.0
T.P.	0.49	411.01 ✓
	12.91	420.52 ✓

110'. S

w	1.9	409.1
cb	1.8	409.2
"4	2.3	408.7
c	2.6	409.4
"4	3.4	407.6
cb	4.3	406.7
E	4.1	406.9

411.01

145'. S

E	13.0	398.0
cb	12.2	398.8
"4	11.1	399.9
c	11.0	400.0
"4	10.7	400.3
+5	10.9	400.6
cb	9.2	401.8
w	8.7	402.3
T.P.	0.54	398.65
	12.90	398.11 ✓

175'. S

w	2.2	396.5
cb	3.0	395.7
+7	4.5	394.2
"4	4.5	394.2
c	4.6	394.1
"4	5.4	393.3
cb	6.8	391.9
E	7.1	391.6

200'. S

c	13.7	385.0
cb	12.6	386.1
"4	11.3	387.4
c	9.9	388.8
"4	8.9	389.8
+4	9.0	389.7
cb	7.6	391.1
w	6.7	392.0

Plover St

46

398.65  
235'S.

W		10.8	387.9
ch		11.7	387.0
+5		13.6	385.1
"4		13.8	384.9
+2		13.8	384.9
T.P.	0.66	386.36	12.95 385.70
C		3.6	382.8
"4		6.2	380.2
ch		9.0	377.4
E		9.6	376.9

265'S

E		16.2	370.2
ch		13.7	372.7
"4		11.4	375.0
C		9.0	377.4
+7		6.4	380.0
"4		6.4	380.0
+5		6.0	380.4
ch		2.8	383.6
W		1.8	384.6

300'S.

W		5.8	380.6
ch		7.4	379.0
+5		7.0	375.4
"4		11.2	375.2
+2		11.2	375.2

386.36

Plover St.

47

C		13.8	372.6
T.P.	0.22	373.55	13.03 373.33
"4		3.6	370.0
ch		5.8	367.8
E		7.8	365.8
			350'S.
E		15.2	358.4
ch		13.3	360.3
"4		11.5	362.1
C		9.2	362.4
+6		6.4	367.0
"4		6.8	366.8
+5		6.5	367.1
ch		2.7	370.9
W		1.7	371.9

399.15 = 90° from N.E. Cor Plover +

W		11.7	361.9
ch		12.9	360.7
T.P.	0.36	361.30	12.61 360.94
+5		2.9	358.4
"4		2.9	358.4
+4		2.9	358.4
C		4.3	357.0
"4		6.3	355.0
ch		8.3	353.0
E		10.0	351.3

N.E. Cor Plover  
& Gibson

361.30

3991 s.on E. - 4.4 s.on W = N. Line Gibson } 1.51 wid on diagonal

E 10.0 351.3 N.E. Cor Plover  
& Gibson

cb 8.6 352.7

14 7.5 352.8

c 6.3 355.0

14 5.5 355.8

75 6.3 355.0

cb 4.0 357.3

N.W. Cor Plover &amp; Gibson 4.07 357.23 on Hub

T.P. 0.67 354.20 7.77 353.53

T.P. 0.38 341.65 12.93 341.27

T.P. 0.44 329.45 12.64 329.01

T.P. on N.E. Blk Cor 6.93 322.52 Hilger &amp; Gibson

Plover St

32.85

625.10

10.85

43.80

48

60' wide  
10' ch  
10' 1/2"

Hilger St X see  
Gibson to Klauber

12-19-27  
mills

N.E. Hub Hilger  
& Gibson

56.7 width diagonal  
110.3  
100' 1/2"

B.M.	4.88	327.40	322.52
00: 70° from S.E. cor Gibson & Hilger - Gibson			
W	15.2	312.2	
ch	14.5	312.9	
1/4	13.6	313.8	
c	12.3	315.1	
1/4	11.9	315.5	
ch	10.7	316.7	
E	7.6	317.8	
	S ch		
E	9.0	318.4	
ch	10.3	317.1	
1/4	11.3	316.1	
c	11.9	315.5	
1/4	13.1	314.3	
ch	14.0	313.4	
W	14.9	312.5	
	S. 1/4		
W	14.4	313.0	
ch	13.5	313.9	
1/4	12.6	314.8	
c	11.5	315.9	
1/4	11.0	316.4	
ch	9.7	317.7	
E	8.4	319.0	

Plotted 9-14-1928  
C.B.H.

Indexed

327.40

49

E Gibson 90° from line of Hilger

E	7.8	319.6
ch	8.9	318.5
1/4	10.1	317.3
c	10.9	316.5
1/4	11.9	315.5
ch	13.0	314.4
W	13.9	313.5
	N. 1/4	
W	13.4	314.0
ch	12.5	314.9
1/4	11.2	316.2
c	10.1	317.3
1/4	9.1	318.3
ch	8.5	318.9
E	7.2	320.2
	N. ch.	
E	6.7	320.7
ch	7.8	319.6
1/4	8.5	328.9
c	9.7	317.7
1/4	10.8	316.6
ch	12.0	315.4
W	13.0	314.4

00 = N line Gibson 90° from N.E. cor Gibson + Hilger.

W	12.4	315.0
cb	11.5	316.9
114	10.3	317.1
C	9.2	318.2
114	7.9	319.5
cb	7.2	320.2
+5	7.1	320.3
E	5.0	322.4

50' N of 00

E	2.1	325.3
+3	3.6	323.8
cb	4.1	323.3
114	4.8	322.6
C	6.4	321.0
114	7.8	319.6
cb	9.2	318.2
W	9.8	317.6

100' N of 00

W	7.5	319.9
cb	6.3	321.1
114	5.2	322.2
C	3.4	324.0
114	1.7	325.7
cb	0.9	326.6
+8	0.5	326.9
E	+1.5	328.9

T.P. 13.01 340.41 0.00 327.40  
150' N.

E	9.0	331.4
+2	10.8	329.6
cb	11.2	329.2
+	11.3	329.1
114	12.6	327.8
C	14.0	326.4
114	15.3	325.1
cb	16.6	323.8
W	18.1	322.3

200' N

W	15.6	324.8
cb	14.2	326.2
114	12.8	327.6
C	11.1	329.3
114	9.3	331.1
+5	8.4	332.0
cb	8.1	332.3
+9	7.4	332.8
E	5.6	333.8

250' N

E	2.8	337.6
+2	5.0	335.4
cb	5.3	335.1
+5	5.8	334.6

340.41

250' N. con

'4	6.9	333.5
c	8.7	331.7
'4	10.2	330.2
cl	11.8	328.6
w	13.3	327.1

300' N

w	11.5	328.9
cl	10.0	330.4
'4	8.4	332.0
c	6.4	334.0
'4	4.3	336.1
+4	3.0	337.4
cl	2.5	337.9
+7	2.0	338.4
c	+1.0	341.4

350' N

E	+3.0	343.4
+4	6.0	340.4
cl	0.3	340.1
+7	0.9	339.5
'4	2.0	338.4
c	4.2	336.2
'4	5.9	334.5
cl	7.8	332.6
w	9.4	330.8

340.41

Hilger St. 51

400' N

w	8.9	331.5
cl	7.0	333.4
'4	4.9	335.5
c	2.7	337.7
'4	0.9	339.5
T.P.	8.79	347.19
+3	6.3	340.9
cl	6.0	341.2
+5	5.8	341.4
E	3.4	343.8

450' N

E	2.5	344.7
+4	4.5	342.7
cl	5.1	342.1
+7	5.2	342.0
'4	6.3	340.9
c	8.5	338.7
'4	10.3	336.9
cl	13.0	334.2
w	14.8	332.4

490.8 N. on E - 507.0 N. on W - A section on split

w	15.5	331.7
cl	12.5	334.7
'4	9.1	338.1
c	7.0	340.2
'4	5.2	342.0

34719'

△ (con)

+	3.5	43.7
+	3.5	7
	3.3	9
o 12	0.0	
	20' = 0.0	
E	1.1	
+2	1.	35.8
+3	2.5	
c	2.7	
1 5	2.5	
'14	3.	
c	5.5	
'14	7.5	
cb	9.	
u	12.6	46
	'N 0	
	13.6	
c	12.0	3
1	8.	338.
c	6.0	3 1.2
114	4.0	343.2
+6	2.1	344.8
cb	2.1	345.1
+7	1.9	345.3
c	0.5	46

347.19

55'

Hilg-rst

E	0.8	3 6.
+2	2.0	2 52
cb	2.5	3447
+4	2.7	344.8
'14	4.6	3426
c	7.3	3 9.9
'14	8.9	3383
'	9.	33 3
'	11.6	336
	7.9	
	9.1	338.1
c	6.9	3403
'14	6.0	3412
c	4.4	218
'	3.3	34 9
+5	2.0	3452
cb	1.8	34 4
	1.7	3
E	0.7	4 5
	0.0'N	
E	+2.3	349.5
+4	+0.8	348.0
c	+1.3	348.5
'14	1.3	348.5
c	0.0	7.2
'14	1.8	3 5.

347.19

100' N. (cont)

ch	4.8	342.4
W	6.9	340.3

150' N

W	2.2	348.0		
T.P.	12.87	359.60	0.46	346.73
ch	11.9	347.7		
"4	9.4	350.2		
E	7.6	352.0		
"4	6.0	353.6		
ch	6.1	353.5		
+4	4.1	353.5		
E	4.0	355.6		

200' N

E	10.7	360.3
+5	6.8	357.8
ch	1.8	357.8
"4	2.1	357.5
E	4.1	355.5
"4	5.9	353.7
ch	8.4	351.2
W	11.9	347.7

250' N

W	7.7	351.9
ch	4.7	355.9
"4	2.5	357.1
E	0.5	359.1

359.60

Hilger St.

53

T.P.	12.87	372.47	0.00	359.60
"4			12.0	360.5
+3			10.5	362.0
ch			10.3	362.2
+6			10.2	362.3
E			7.4	365.1

300' N

E	4.5	368.0
+4	6.8	366.7
ch	7.2	365.3
+6	7.4	365.1
"4	8.7	363.8
E	10.6	361.9
"4	12.4	360.1
ch	14.6	357.9
W	17.5	355.0

350' N

W	13.2	359.3
ch	10.8	361.7
"4	8.9	363.6
E	7.5	365.0
"4	5.7	366.8
+2	4.6	367.9
ch	4.4	368.1
+6	4.0	368.5
E	0.7	371.8



372.47  
375' N

e	+0.2	373.7
+4	2.4	370.1
cb	2.7	369.8
+6	3.0	369.5
'14	4.3	368.2
e	6.5	366.0
'14	8.4	364.1
cb	10.4	362.1
w	12.7	359.8

400' N

w	10.6	361.9
cb	8.6	361.9
'14	6.9	365.6
e	5.3	367.2
'14	3.0	369.5
+2	1.5	371.0
cb	1.2	371.3
+6	0.9	371.6
T.P.	6.80	378.87
e	0.40	372.07
E	4.5	374.4

450' N

E	3.3	375.6
+3	5.7	373.2
cb	5.7	373.2
+8	6.0	372.9
'14	6.8	372.1

378.87

419.57, 54

e	8.2	370.7
'14	10.0	368.9
cb	12.1	366.8
w	13.8	366.1

490' N

w	10.4	368.3
cb	9.3	369.6
'14	8.3	370.6
e	7.1	371.8
'14	5.9	373.0
+3	4.5	374.4
cb	4.1	374.8
+7	4.0	374.9
e	1.3	377.6

515' N

E	1.2	377.7
+3	3.3	375.6
cb	3.4	375.5
+6	3.6	375.3
'14	4.5	374.4
e	6.3	372.6
'14	7.4	371.3
cb	8.7	370.2
w	9.9	369.0

378.87

550' N

W	9.9	369.0
cl	8.4	370.5
"4	6.8	372.1
C	5.9	373.0
"4	4.8	374.1
+3	3.9	375.0
cl	3.6	375.3
+7	3.6	375.3
E	1.5	377.4

580' N

E	2.0	376.9
+4	3.9	375.0
cl	3.8	375.1
+6	3.7	375.2
"4	5.0	373.9
C	5.8	373.1
"4	6.2	372.7
cl	7.4	371.5
W	10.0	368.9

600' N

W	13.0	365.9
cl	9.9	369.0
"4	7.8	371.1
C	6.4	372.5
"4	5.3	373.6
+3	4.2	374.7

378.87

Hilger St 53

cl	4.2	374.7
+6	4.5	374.4
E	2.6	376.3

620' N

E	2.5	376.4
+5	5.1	373.8
cl	4.8	374.1
+6	4.8	374.1
"4	5.8	373.1
C	7.7	371.2
"4	9.9	369.0
cl	12.1	366.8
W	12.4	366.5

635' N

W	11.5	367.4
cl	11.4	367.5
"4	11.0	367.9
C	9.7	369.2
"4	7.3	371.6
+5	5.8	373.1
cl	6.0	372.9
+5	6.0	372.9
E	3.0	375.9

660' N

E	5.7	373.2
+5	6.6	372.3

378.87

660' N. (con)

cl	6.9	372.0
"4	7.8	371.1
c	8.4	370.5
"4	8.6	370.3
cl	7.5	371.4
w	6.8	372.1

700' N

w	+0.8	379.7
cl	0.0	378.9
"4	1.4	377.5
c	2.9	376.0
"4	4.0	374.9
cl	5.3	373.6
E	5.3	373.6
T.P.	13.05	391.60
	0.32	378.55

Top Fence Post

735' N

E	11.8	379.8
+3	12.4	379.2
cl	11.2	380.4
"4	10.4	381.2
c	9.5	382.1
"4	8.6	383.0
cl	7.5	384.1
w.	7.0	384.6

391.60

770' N.

w	2.8	388.8
cl	3.5	388.1
"4	4.4	387.2
c	5.3	386.3
"4	6.2	385.4
cl	7.3	384.3
+5	8.0	383.6
E.	8.2	383.4

800' N

E	4.2	387.4
+4	4.3	387.3
cl	4.0	387.6
+5	4.0	387.6
"4	3.1	388.5
E.	2.1	389.5
"4	1.0	390.6

T.P.	12.97	404.50	0.07	391.53
cl			12.8	391.7
w.			12.5	392.0

850' N

w	8.5	396.0
cl	9.4	395.1
"4	9.9	394.6
c	10.5	393.0
"4	11.0	392.5
+5	11.6	392.9

Hilger

H

404.50

850 N. (con)

ch	11.7	3928
+4	12.2	3923
E	12.0	3921.5

900' N.

W	7.8	3967
+5	8.0	3968
ch	7.8	3967
+5	7.6	3969
14	6.5	398.0
C	6.0	398.5
14	5.4	399.1
ch	5.0	399.5
W	5.0	399.5

917.4 N. = 90° 00' from S.W. Cor. Hilger + Klauber

W	3.2	401.3	sw. cor Hilger + Klauber
ch	4.2	400.3	
14	4.2	400.3	
E	4.7	399.8	
14	5.0	399.5	
+5	6.1	398.4	
ch	6.3	398.2	
+6	6.5	398.0	
E	6.1	398.4	

404.50

Hilger

57

5. Line Klauber { 4896 wide on diagonal  
11.5 ch  
11.5 14s.

E	3.6	400.9	S.E. Cor Hilger + Klauber
ch	4.4	400.1	
+9	4.5	400.0	
14	3.4	401.1	
E	3.0	401.5	
14	3.1	401.4	
ch	3.4	401.1	
W	3.2	401.3	S.W. Cor Hilger + Klauber

chk on BM. Pipe of Hilger + Klauber 0.76 403.74 = 403.76

40 wide  
5' d.s.  
7.5' 1/4 S

EIDER STX sec

Klauber to Winnct.

See page C

12-20-27  
miller

1/2 nails in Pole E. Klauber  
Δ W. of H11X

B.M.	13.09	421.46		408.37	
T.P.	12.80	434.23	0.03	421.43	
					41.24 wide on diagonal 5.25' d.s. 8.03' 1/4 S.
					W. line Klauber
N.		5.4	428.8		N.W. Eider + Klauber
cb		4.9	429.3		
14		4.1	430.1		
C		3.6	430.6		
14		3.6	430.6		
+6		3.1	431.1		
cb		1.6	432.6		SW 211 Cor
Set B.M. S.	T.P.	6.74	440.18	0.79	433.44 Eider + Klauber
					15.38 W. on N = 00 = 90° 00' from SW Cor Eider + Klauber
S		6.7	433.5		SW Cor Eider + Klauber
cb		7.3	432.9		
+2		8.9	431.3		
14		9.3	430.9		
C		9.0	431.2		
14		9.0	431.2		
cb		10.0	430.2		
N		10.7	429.5		
					25' W. of 00
N		9.7	430.5		
cb		8.9	431.3		
14		7.8	432.4		
+3		6.7	433.5		
C		7.4	432.8		

Platted  
9-15-28  
C.B.H.

Indexed

440.18

58

14	7.2	437.0
+3	6.8	437.4
cb	4.6	435.6
S	3.6	436.6
		75' W. of 00
S	1.0	439.2
cb	2.0	438.2
+5	3.0	437.2
14	5.0	435.2
C	5.0	435.2
+5	4.0	436.2
14	5.0	435.2
cb	6.3	433.9
N	7.0	433.2
		113' W
N	7.8	432.4
cb	6.9	433.3
14	5.1	435.1
+5	6.3	433.9
C	6.2	434.0 ✓
14	6.0	434.2
+3	3.1	437.1
cb	2.1	438.1
S	1.0	429.2

440.18

120' W

S	1.0	439.2
cl	2.2	438.0
+5	3.1	437.1
114	6.0	434.2
C	6.5	433.7
114	7.8	432.4
cl	8.9	431.3
N	9.6	430.6

132.85 W = 90° from N.E. cor East Drive 52' wide on diagonal

N	10.2	430.0
cl	9.2	431.0
114	7.9	432.3
C	6.6	433.6
114	6.2	434.0
+3	3.5	436.7
cl	2.8	437.4
S	1.7	438.5

26' W of above = 1/2 East Drive

S	3.2	437.0
cl	4.7	435.5
+3	6.6	433.6
114	7.1	433.1
C	7.3	432.9
114	8.0	432.2
+3	9.5	430.7
cl	10.1	430.1

440.18

Eider St

59

N	11.7	428.5
00 = 90° from N.W. cor Eider + East Drive		
N	12.8	427.4
cl	11.5	428.7
+3	10.9	429.3
114	9.1	431.1
+3	8.3	431.9
C	8.3	431.9
114	8.1	432.0
+3	7.6	432.6
cl	5.4	434.8
S	4.6	435.6

50' W.

S	5.4	434.8
cl	7.2	433.0
+1	8.0	432.2
114	8.4	431.8
C	8.5	431.7
114	9.0	431.2
cl	12.0	428.2
N	13.2	427.0

70' N

N	13.0	429.2
cl	11.8	428.4
114	9.0	431.2
C	8.8	431.4

440.18

70' W. (con)

'4	8.7	431.5
+4	6.7	433.5
cl	6.7	433.5
S	6.2	434.0

100' W.

S	5.0	435.2
cl	5.7	434.5
+3	6.4	433.8
'4	8.4	431.8
C	8.6	431.6 ✓
'4	8.4	431.8
cl	11.5	428.7
N	13.0	427.2

150' W

N	10.2	430.0
cl	9.3	430.9
'4	6.7	433.5
C	7.4	432.8 ✓
'4	7.4	432.8
cl	4.4	435.8
S	3.0	437.2

200' W

S	2.6	437.6
cl	3.3	436.9
'4	5.5	434.7
+3	6.2	434.0 ✓

440.18

Eider St

60

C	5.9	434.3
'4	5.5	434.7
cl	7.9	432.3
N	8.7	431.5

220' W

N	7.9	432.3
cl	6.6	433.6
'4	4.2	436.0
C	5.7	435.1 ✓
+5	5.5	3 @ 4.7
'4	4.2	436.0
T.P.	7.79	443.32 ✓
cl	4.0	438.7
S	3.3	440.0

240' W

S	4.0	439.3
cl	4.5	438.8
+3	5.0	438.3
'4	7.7	435.6
C	7.5	435.8 ✓
'4	7.0	436.8
cl	10.1	433.2
N	11.0	432.3

443.32  
288.7 W = P.C. Δ 12° 20' R = 180.

N	11.2	432.1
cb	10.0	433.3
1/4	7.9	435.4
+4	6.4	436.9
e	6.8	436.5 ✓
1/4	7.4	435.9
+3	7.4	435.9
cb	4.5	435.8
S	3.3	440.0
00 = <del>9</del> <del>9</del> <sup>W.L.</sup>		
S	3.6	439.7
cb	4.7	438.6
+4	7.8	435.5
1/4	7.7	435.6
c	7.2	436.1 ✓
+4	6.7	432.6
1/4	8.3	435.0
cb	10.6	432.7
N	11.5	431.8
45' W.		
N	12.5	430.8
cb	11.4	431.9
1/4	8.0	435.3
c	8.7	434.6 ✓
1/4	8.7	434.6
+3	4.8	438.5

443.32

Eider St 61

cb	4.4	438.9
S	3.8	439.5
75' W.		
S	5.9	437.4
cb	6.7	436.6
+3	7.4	435.9
1/4	10.4	432.9
c	10.2	433.1
1/4	10.0	433.3
cb	13.6	429.7
N	15.1	428.2
100' W.		
N	16.8	426.5
cb	15.1	428.2
1/4	11.0	432.3
c	11.3	432.0 ✓
1/4	11.5	431.8
+3	8.4	434.9
cb	7.1	436.2
S	5.7	437.6
120' W.		
S	8.6	436.7
cb	7.0	436.7
+5	9.3	434.0
1/4	4.7	431.6
c	11.9	431.4 ✓



443.32  
120' W. (con)

"4	11.6	431.7	
cb	13.8	429.5	
N	15.1	428.2	

145' W.

N	17.2	426.7	
cb	15.7	427.6	
"4	12.1	431.2	
c	12.3	431.0	✓
+5	12.4	430.9	
"4	11.0	432.3	
+2	9.0	434.3	
cb	7.3	436.0	
S	6.3	437.0	

200' W

S.	8.4	434.9	
cb	9.3	434.0	
+2	9.7	433.6	
"4	14.2	429.1	
c	14.0	429.3	✓
"4	13.9	429.4	

T.P.	6.54	437.00	12.86	430.46	✓
cb			11.8	425.2	
N			13.4	423.6	

240' W.

N	12.8	424.2	
cb	12.3	424.7	

437.00

Eider St 62

+4	11.2	425.8	
"4	9.8	427.2	
+3	8.4	428.6	
c	8.4	428.6	
"4	8.5	428.5	✓
+2	6.2	430.8	
cb	4.4	432.6	
S	3.1	434.9	

275' W (9410.55)

S	1.0	436.0	
cb	2.9	434.1	
+3	3.7	433.3	
"4	6.9	430.1	
c	7.6	429.4	✓
+5	7.3	429.7	
"4	7.4	427.6	
cb	13.5	423.5	
N	15.1	421.9	

283.7 W = P.C. Δ 56° 40' 120' Rad This curved divided 4-PARTS

N	14.9	422.1	
cb	13.2	423.8	
"4	8.8	428.2	
+2	7.5	429.5	
c	7.7	429.3	
"4	7.6	429.4	
+5	3.5	433.5	

437.00

P.C. (con)

cl	3.0	434.0
S	2.2	434.8
	#1	
S	1.6	435.4
cl	3.1	433.9
"4	7.7	429.6
E	7.8	429.2
"4	8.0	429.0
cl	12.7	424.3
N	14.5	422.5
	#2 = ctr curve	
N	14.2	422.8
cl	12.0	425.0
"4	7.6	429.4
E	7.6	429.4
"4	7.5	429.5
+4	4.0	433.0
cl	2.3	434.7
S	1.3	435.7
	#3	
S	0.8	436.2
cl	2.7	434.3
+2	3.0	434.0
"4	5.1	431.9
+3	7.7	429.3
C	7.8	429.2

 $\Delta L = 24.73$  $\Delta = 10^{\circ}14'$  $\Delta L = 24.73$  $\Delta = 10^{\circ}14'$  $\Delta L = 24.73$  $\Delta = 10^{\circ}14'$ 

Eider St

63

437.00

11.4	8.1	428.9
cl	12.1	424.9
N	13.2	423.8
	#4 = E.C.	
N	13.3	423.7
cl	11.1	425.9
+4	7.9	429.1
"4	7.9	429.1
E	8.0	429.0
+4	8.0	429.0
"4	7.3	432.7
cl	2.8	434.2
S	2.2	434.8
	37' W	
S	1.8	435.2
cl	3.0	434.0
+4	3.7	433.3
"4	6.2	430.8
+3	8.3	428.7
E	8.2	428.8
"4	8.3	428.7
cl	11.4	425.4
N	12.4	424.6

 $\Delta L = 24.73$  $\Delta = 10^{\circ}14'$

437.00  
 74.1 N = P C Δ 41 000 R = 180. This curve divided into 4 parts

N	11.9	425.1
cb	11.3	425.7
1/4	8.8	428.2
c	8.8	428.2
1/4	8.8	428.2
+2	8.8	428.2
1/4	6.2	430.8
cb	5.4	431.6
S	4.2	432.8

#1

S	4.8	432.2
cb	5.4	431.2
+5	9.3	427.7
1/4	9.3	427.7
c	9.1	427.9
1/4	8.8	428.2
+3	11.4	425.6
cb	11.6	425.4
N	12.1	424.9

#2 = cb Curve

N	13.8	423.2
cb	13.5	423.5
1/4	10.8	426.2
c	10.8	426.2
1/4	10.8	426.2
cb	7.5	429.5

437.00

Eider St

68

S	6.4	420.6
1/4	8.3	424.7
cb	9.9	427.1
1/4	12.8	424.2
c	12.7	424.3
1/4	12.0	425.0
cb	13.6	423.4
N	15.6	421.4

00 = #4 = E.C

N	18.2	418.8	
cb	16.1	420.9	
+5	13.6	423.4	
1/4	14.1	422.9	
c	14.3	422.7	
1/4	14.2	422.8	
+3	11.8	425.2	
cb	10.5	426.5	
S, T.P. on hub 0.94	424.62	9.32	427.68

#5'N

S	2.3	426.3
cb	3.2	425.4
1/4	4.6	420.0
c	9.0	419.6
1/4	9.0	419.6
+3	8.8	419.8

428.62

45' W. (cont)

cb	11.0	417.6
N	13.2	415.4
60' W		
N	15.2	413.4
cb	13.4	415.2
+4	10.2	418.4
4	10.1	418.5
C	10.3	418.3
4	9.8	418.8
+3	6.7	421.9
cb	5.5	423.1
S	4.1	424.5 424.5

80' W

S	3.5	425.1
cb	4.3	424.3
+3	5.2	423.4
4	10.5	418.1
C	11.3	417.3
4	11.3	417.3
cb	14.2	414.4
N	17.1	411.5

100' W

N	17.2	411.4
cb	15.8	412.8
4	12.1	416.5
C	12.5	416.1

428.62

Eider St.

65

4	12.3	416.3
+3	8.4	420.2
cb	7.1	421.5
S	6.0	422.6

140' W

S	8.0	420.6? 428.6?
cb	9.3	428.3?
+4	10.4	418.2
4	13.5	415.1
C	13.9	414.7
4	13.5	415.1
cb	17.6	411.0
N	18.4	410.2

160' W

N	18.2	410.4
cb	16.0	412.6
4	13.9	414.7
C	14.5	414.1
4	14.5	414.1
+2	14.5	414.1
cb	9.7	418.9
S	8.6	420.0

162' W = E. Edge garage on N. e. N of N line,

S	8.8	419.8
cb	9.8	418.8
+5	14.5	424.1

428.62  
162' W. con

14	14.6	414.0
c	14.6	414.0
64	14.4	414.2
ch	15.0	413.6
N	15.3	413.3

182' W = W. end of garage on N. 1.7 14 st at this end

N	15.5	413.1	in garage
cl	15.4	413.2	
14	15.2	413.4	
cl	15.3	413.3	
14	15.3	413.3	
+5	15.0	413.6	
cl	10.8	418.8	
S	10.0	418.6	

184' W

S	10.1	418.5
cl	11.0	419.6
+3	15.0	412.6
14	15.3	413.3
e	15.3	413.3
14	15.3	413.3
+3	15.3	413.3

T.P. on P.C. Hub	0.20	417.51	11.31	417.31	✓	S. side Eider
cl			7.4	410.1		
N			10.8	406.7		

417.51

Eider St 66

189.50 ft = P.C.  $\Delta = 31^{\circ} 35'$  R = 140'. This curve divided into 4 parts

N	10.8	406.7
cl	7.9	409.6
14	6.0	411.5
+2	4.2	413.3
c	4.4	413.1
14	4.2	413.3
d	3.4	414.1
s	0.2	417.3

s	1.2	416.3
+2	1.4	416.0
cl	4.3	413.2
14	5.1	412.4
c	5.6	411.9
+3	5.6	411.9
14	8.0	409.5
cl	7.8	407.7
N	10.6	406.9

$\Delta L = 27.53'$   
 $\Delta = 7^{\circ} 53' 15''$

$\Delta L = 27.53'$   
 $\Delta = 7^{\circ} 53' 15''$

#2 = clv curve

11	13.1	404.4
cl	10.8	406.7
+5	10.7	406.8
14	8.7	408.8
+4	7.4	410.1
c	7.8	409.7
14	7.6	409.9

417.51

# 2 (con)

cb		6.9	410.6
S		3.5	414.0
	# 3		
S		6.1	411.4
cb		7.1	410.4
+5		11.8	405.7
"4		11.5	406.0
C		11.4	406.1
+5		11.0	406.5
"4		12.5	405.0
cb		13.3	404.2
N		14.8	400.7
	Midway bet # 3 & E.C.		
N		16.7	400.8
cb		15.8	401.7
"4		15.0	402.5
C		13.8	403.7
"4		13.6	403.9
cb		7.6	409.9
S		6.1	410.4
	# 4 = E.C.		
S		7.4	410.1
cb		9.1	408.4
+3		9.8	407.7
TP	1.15	405.77	12.89
"4			3.3

27.54  
Δ = 7° 53' 15"L = 27.53'  
Δ = 7° 53' 15"

405.77

Eider St

C		3.1	402.7
"4		3.4	402.4
cb		6.5	399.3
N		7.6	398.2
	35' W. of E.C.		
N		11.2	394.6
cb		9.7	396.1
"4		6.5	399.3
C		6.6	399.2
"4		5.6	400.2
+2		5.6	400.2
+4		2.8	403.0
cb		2.1	403.7
S		0.5	406.3
	60' W		
S		4.1	401.7
cb		5.3	400.5
+2		5.7	400.1
+4		7.5	398.3
"4		7.6	398.2
C		8.5	397.3
"4		7.5	398.3
cb		9.9	395.9
N		11.5	394.3

405.77

75' W

N	12.1	393.7
cb	10.7	395.1
"4	9.4	396.4
c	9.4	396.0
"4	9.4	396.0
r3	8.9	396.9
cb	5.7	400.1
S	4.5	401.3

105' W

S	8.6	397.2
cb	9.5	396.3
"4	11.3	394.5
c	11.9	393.9
r5	11.2	394.6
"4	12.6	393.2
cb	15.4	390.4
N	16.6	389.2
T.P.	5.92	399.33
	12.36	393.41

140' W

N	13.2	396.1
cb	11.6	397.7
"4	9.2	390.1
+4	6.0	393.3
c	5.8	393.5
"4	5.8	393.5
cb	5.0	394.3

399.33

Eider ST

68

S	3.4	395.9
196.2 N. on S. = E. Line winnett on diagonal		
		{ 44.77 wide on diagonal 5.6 dls 8.4 44
S	4.5	394.8
cb	4.2	393.1
"4	6.1	393.5
c	6.3	393.0
"4	10.0	389.3
cb	12.4	386.9
N	13.1	386.2
T.P.	13.02	406.06 ✓
T.P.	4.51	410.47 ✓
		6.29 393.04 ✓
		0.13 405.93 ✓

40' wide  
5' cbs  
7.5' lbs

WREN STX Sec  
Scimitar to Klauber.

12-22-27  
mills

410.44 Page 68

S. line Scimitar on arc 5.4' wide 6.75' cbs 10.12' lbs  
S.W. Cor Wren  
& Scimitar

W. line Wren	5.1	405.3
W cb	4.1	406.3
" 1/4	3.5	406.9
c	3.5	406.9
" 1/4	1.3	409.1
cb	0.8	409.6

E. line Scimitar 0.1 410.3

This section on Radial line From S.E. Cor Scimitar & Wren P.C. on S.E. line 40'

E. line Wren	0.1	410.3
cb	1.1	409.3
" 1/4	2.0	408.4
c	3.0	407.4
" 1/4	6.4	404.0
cb	7.3	403.1
W.	7.7	402.7

Plotted 3-16  
C.B.H. 1928

This Curve divided into 5 Parts - Δ 10'-04'-12" Part #

W	9.6	400.8
cb	8.4	402.0
" 1/4	7.0	403.4
c	6.0	404.4
" 1/4	2.7	407.7
cb	1.9	408.5
E	7.6	408.8

1958 A.C. M.W.  
Per Section

25.41 lbs. on E.  
Per Section

E	4.0	406.4
cb	4.6	405.8

Indexed

410.44

69

" 1/4	5.6	404.8
c	7.0	403.4
" 1/4	7.5	400.9
cb	10.1	400.3
W	10.4	400.0

# 3

W	12.7	397.7
cb	12.6	397.8
" 1/4	11.6	398.8
c	10.3	400.1
" 1/4	8.6	400.8
cb	8.7	401.7
c	8.3	402.1

# 4

c	11.8	498.6
cb	12.0	498.4
" 1/4	12.7	497.7
T.P.	0.48	397.85
c	13.07	397.37 ✓
c	0.7	397.2
" 1/4	2.5	395.4
cb	3.1	394.8
W	3.4	394.5

# 5 = P.R.C.

W	7.0	390.9
cb	6.4	391.5
" 1/4	6.4	391.5



397.85

397.85  
Sec #5 = R.R.C. (con)

+4	6.6	391.3
0	4.9	393.0
1/4	3.6	394.3
0	3.1	394.8
E	2.8	395.1

This Curve  $\Delta$  88-52<sup>0</sup> N. line R602.62 divided into 12 Parts R602.67  
#1

0	6.0	391.9
0	7.0	390.9
1/4	9.0	388.9
0	9.3	388.6
1/4	10.2	387.7
0	11.4	386.5
W	12.4	385.5

#2

W	14.4	383.5
0	14.2	383.7
1/4	12.8	385.1
+2	11.8	386.1
0	11.7	386.2
1/4	11.5	386.4
0	11.5	386.4
E	10.0	387.9

#3

0	13.3	384.6
0	13.9	384.0

1/4	14.2	383.7	
0	14.5	383.4	
T.P. 0.19	385.06	12.98	384.87
1/4	4.7	380.4	
0	6.2	378.9	
W	7.1	378.0	

#4

W	11.0	374.1
0	9.5	376.4
1/4	8.1	377.0
0	6.8	378.3
+4	6.3	377.8
1/4	4.6	380.5
0	3.6	381.5
E	3.3	381.8

#5

E	5.4	379.7
+2	6.4	378.9
0	6.3	378.8
1/4	6.9	378.2
0	8.9	376.2
1/4	10.6	374.5
0	12.4	372.7
W	13.4	371.7

385.06

#6

W.	17.0	368.1
cl	15.9	369.2
"4	14.4	370.7
c	12.4	372.3
"4	11.4	373.7
cl	11.4	373.7
E	9.2	375.9

#7

E	12.7	373.4
T.P.	0.18	372.34
+2	2.5	369.8
cl	2.6	369.7
"4	2.9	369.4
c	3.9	368.4
"4	5.2	367.1
cl	6.8	365.5
W	7.5	364.8

#8

W	10.7	351.6
cl	10.1	362.2
"4	8.8	363.5
c	7.5	364.8
"4	7.2	365.1
"4	6.8	365.5
cl	4.8	367.5
E	4.3	368.0

372.34

#9

E.	6.3	366.0
cl	7.5	364.8
"4	9.7	362.6
c	10.5	361.8
"4	11.5	360.8
cl	12.5	359.8
W	13.1	359.2

#10

W	15.6	358.7
cl	15.2	357.1
"4	14.5	357.8
c	13.1	359.2
"4	12.1	360.2
cl	11.0	361.3
E	10.3	362.0

#11

E	12.1	360.2
cl	12.8	359.5
T.P.	2.02	361.63
"4	12.73	359.61
"4	3.3	368.3
c	4.2	367.4
"4	5.3	366.3
cl	6.4	365.2
W	7.1	364.5

Wren st.

71

361.63

#1/2 = E.C. on W. on Radial Line

			on Pipe at P.I. of Curve & Tangent on W
W.	8.89	352.74	
cl	7.8	353.8	
1/4	6.8	354.8	
C	6.1	355.5	
1/4	5.2	356.4	
cl	3.8	357.8	
E	3.2	358.4	

00 = 26.64 S.E. of P.I. of Curve & Tangent on W = 90°00' from P.I.  
of Curve & Tangent on E.  
From Here to Klauber St is 30' wide

N.E.	3.2	358.4
cl	5.3	357.3
S.W.	6.9	354.7

50' S.E. of 00

S.W.	5.5	356.1
cl	4.1	357.5
N.E.	2.2	359.4

100' S.E. of 00

N.E.	3.2	358.4
cl	4.7	356.9
S.W.	6.5	355.1

145' S.E.

S.W.	8.5	353.1
cl	6.8	354.8
N.E.	5.5	356.1

361.63

Wren. St.

7/8

175' S.E.

N.E.	7.1	354.5
cl	9.5	352.1
S.W.	10.0	357.6

225' S.E.

S.W.	15.1	346.5
cl	13.2	348.4
N.E.	11.6	350.0

T.P. 0.17 348.76 13.04 348.59

260' S.E.

N.E.	3.7	345.1
cl	5.9	342.9
S.W.	8.0	340.8

300' S.E.

S.W.	15.8	333.0
cl	13.9	334.9
N.E.	10.5	338.3

T.P. 0.86 336.60 13.02 335.74

350' S.E.

N.E.	11.7	324.9		
cl	13.7	322.9		
T.P.	0.75	325.33	12.02	324.58

S.W. 4.3 321.0

400' S.E.

S.W.	15.1	310.2
cl	14.3	311.0
N.E.	12.9	312.4

325.33

T.P.	0.90	313.41	12.82	312.51
		440' S.E.		
N.E.			8.7	304.7
⊥			10.2	303.2
S.W.			11.6	307.8
		460' S.E.		
S.W.			11.8	301.6
⊥			10.9	302.5
N.E.			10.7	302.7
		490' S.E.		
N.E.			10.7	302.7
⊥			10.9	302.5
S.W.			11.2	302.2
		495' S.E.		
S.W.			9.0	304.4
⊥			8.8	304.6
N.E.			8.6	304.8
		510' S.E.		
N.E.			4.4	309.0
⊥			4.1	309.3
S.W.			4.1	309.3
		530' S.E.		
S.W.			1.4	312.0
⊥			1.0	312.4
N.E.			0.4	313.0
T.P.	11.59	324.82	0.18	313.23

324.82

N. 2nd St.

73

570' S.E.

N.E.			6.4	318.4
⊥			7.4	317.4
S.W.			8.2	316.6
		600' S.E.		
S.W.			3.6	321.2
⊥			2.7	322.1
N.E.			1.8	323.0
T.P.	10.68	332.99	2.51	322.31
		635' S.E. = N.W. Line Klauber Ave		
N.E.			1.3	331.7
⊥			2.5	330.6
S.W.			3.3	329.7
chk on Hub B.M.			3.77	329.22 = 329.20 + Klauber

60' wide  
10' elev  
10' elev

Bittern St & Sec  
Klauber To Madera

12-27-27  
mills

B.M.	13.02	289.40	276.38	S.W. BIK Coy Bittern & Madera
S		12.8	276.6	
+8		12.4	276.6	
el		14.5	274.9	
1/4		15.0	274.4	
C		15.2	274.2	
1/4		15.6	273.8	
el		15.8	273.6	
N		15.6	273.8	

= West side

= East side  
Plotted 9-29-1928  
A.B.H.

45' W

N		8.9	280.8
el		8.8	280.6
1/4		8.5	280.9
C		7.7	281.7
1/4		7.6	281.8
el		7.5	281.9
S		7.5	281.9

60' W

S		5.1	284.3
el		4.0	285.4
1/4		4.5	284.9
C		5.0	284.4
1/4		5.8	283.6
el		6.0	283.4
N		6.5	282.9

Indeped

289.40

74

70' W

N		3.8	285.6	
el		2.8	286.6	
1/4		2.8	286.6	
C		1.7	287.7	
1/4		2.1	287.3	
el		2.4	287.0	
S		2.4	287.0	
T.P.	12.14	301.44	0.10	289.30

95' W

S		6.0	295.4
el		6.3	295.1
+3		8.4	293.0
1/4		8.1	293.3
+8		7.7	293.7
C		6.0	295.4
1/4		5.8	295.6
el		5.7	295.7
N		6.1	295.3

120' W

N		1.8	299.6
el		1.3	300.1
1/4		0.7	300.7
C		1.8	299.6
+2		3.5	297.9
1/4		3.7	297.7
+6		4.2	297.2

301.44

120' W. (COH)

cb		2.0	299.4
S		2.2	299.2
T.P.	12.51	313.65	0.30 301.14

140' W

S		11.6	302.1
cb		11.6	302.1
+4		14.0	299.7
114		13.6	300.1
C		13.5	300.2
114		12.1	301.6
cb		12.0	301.7
N		12.3	301.4

160' W

N		11.2	302.5
cb		11.0	302.7
114		11.1	302.6
+2		11.4	301.9
C		11.8	301.9
114		12.0	301.7
+		12.4	301.3
cb		11.5	302.2
S		11.3	302.4

210' W

S		8.8	304.9
cb		9.1	304.6
114		8.4	305.3

313.65

BITTERN ST

75

C		8.0	305.7
114		8.0	305.7
cb		8.3	305.4
N		8.5	305.2

260' W

N		4.0	309.7
cb		4.0	309.7
114		4.9	308.8
C		4.7	309.0
114		5.1	308.6
cb		5.1	308.6
S		5.4	308.3

300' W

S		2.1	311.6
cb		2.1	311.6
+5		3.1	310.6
114		2.4	311.3
C		2.6	311.1
114		2.4	311.3
cb		1.9	311.8
N		2.0	311.7

T.P.	13.01	324.61	0.05	313.60
------	-------	--------	------	--------

350' W

N		12.5	314.1
cb		12.7	313.9
114		12.7	313.9

326.61

350' W (con)

c	12.2	314.4
14	12.3	314.3
+5	12.9	313.7
cl	11.8	314.8
s	11.6	314.8

400' W

s	7.8	318.8
cl	8.1	318.5
+5	9.4	317.2
14	8.8	317.8
c	8.6	318.0
14	9.1	317.5
cl	9.3	317.3
N	9.5	317.1

450' W

N	6.0	320.6
cl	5.5	321.1
14	5.3	321.3
c	4.4	322.2
14	4.0	322.6
+4	5.0	321.6
cl	3.0	323.6
s	2.3	324.3
T.P.	12.73	339.20
	0.14	326.47

339.20

Bittern St

76

500' W

s	9.0	330.2
cl	10.1	329.1
+2	10.4	328.8
+5	12.5	326.7
14	11.4	327.8
c	11.5	327.7
14	12.4	326.8
cl	13.3	325.9
N	13.0	326.2

550' W

N	8.8	330.4
cl	7.3	331.9
14	6.7	332.5
c	5.8	333.4
14	5.8	333.4
+5	6.4	332.8
cl	4.0	335.2
s	2.7	336.5
T.P.	12.73	351.87
	0.06	339.14

600' W

s	9.4	342.5
cl	10.6	341.3
+5	13.3	338.6
14	12.4	339.5
c	12.6	339.3
14	14.0	337.9

351.87

600' W. 2014

cl	15.0	336.9
N	16.5	335.4
625' W.		
N	12.8	339.1
cl	12.0	339.9
"4	11.3	340.6
e	9.7	342.2
"4	9.6	342.3
+5	9.8	342.1
cl	7.1	344.8
S	6.2	345.7
650' W.		
S	2.5	349.4
cl	4.0	347.9
+5	6.7	345.2
"4	6.4	345.5
e	6.5	345.4
"4	6.6	345.3
cl	7.3	344.6
N	8.7	343.2
700' W.		
N	1.8	350.1
cl	0.4	351.1
"4	0.2	351.7
T.P.	12.68	364.29
C	11.7	352.6

364.29

Bittern St

77

"4	11.1	363.2
+4	11.6	352.7
+8	9.0	355.3
cl	9.4	354.9
S	8.1	356.2
740' W.		
S	3.0	361.3
cl	4.1	360.2
+2	4.2	360.1
+5	6.3	358.0
"4	5.2	359.1
e	5.8	358.5
"4	6.5	357.8
cl	7.1	357.2
N	7.5	356.8
770' W.		
N	4.2	360.1
cl	3.1	361.2
"4	3.0	361.3
e	2.5	361.8
"4	2.2	362.1
+5	2.5	361.8
+7	0.7	363.6
cl	0.8	365.5
S	+0.5	364.8
T.P.	12.91	376.86
C	0.34	363.95



376.46

800'W

S	8.8	368.1
cb	9.6	367.3
+3	9.7	367.2
+5	11.3	365.6
14	11.6	365.3
C	12.1	364.8
14	13.0	363.9
cb	13.4	363.5
N	14.4	362.5

8.50'W

N	9.8	367.1
cb	9.3	367.6
14	8.3	368.6
C	7.3	369.6
14	6.9	370.0
+4	7.2	369.7
+7	4.2	372.7
cb	4.2	372.7
S	3.9	373.0

900'W

S	0.1	376.8
cb	1.4	375.5
+5	2.9	374.0
14	2.7	374.2
C	2.4	374.5
14	5.0	371.9

376.86

Bittern St 78

cb	6.0	370.9
N	7.1	369.8

950'W

N	6.1	370.8
cb	4.3	372.6
14	3.0	373.9
+6	2.1	374.8
C	0.7	376.2
14	0.6	376.3
+5	0.5	376.4

T.P. 13.02 389.33" 0.55 376.31

cb	11.0	378.3
S	10.2	379.1

1000'W

S	8.6	380.7
cb	9.7	379.6
+4	11.5	377.8
14	11.7	377.6
C	11.7	377.6
+5	13.5	375.8
14	14.6	374.7
cb	16.0	373.3
N	17.8	371.5

1050'W

N	15.8	373.5
cb	13.6	375.7

389.33

1050' W (E.H.)

1/4	12.5	376.8
+5	11.5	377.8
C	10.0	379.3
1/4	10.0	379.3
+5	9.6	379.7
ch	8.0	381.3
S	7.0	382.3

1095.4 W = E. Line Klauber on si. at 90° from Bittern

chkon B.M.	3.53	385.80	P. & S. Klauber & Bittern 385.74
S	3.8	385.5	
ch	5.5	383.8	
1/4	6.3	383.0	
C	6.2	383.1	
1/4	7.8	381.5	
ch	8.7	380.6	
N	9.7	379.6	

17.86 W = P.I. S. ch Bittern + E. Line Klauber

N	7.1	382.2
ch	5.9	383.4
1/4	5.0	384.3
C	3.8	385.5
1/4	4.0	385.3
S. ch + E. Line Klauber	2.9	386.4

17.86 W = P.I. S. 1/4 Bittern + E. Line Klauber

S. 1/4 + E. Line Klauber	1.9	387.4
C	2.2	387.1

389.33

Bittern St 79

1/4	3.3	386.0		
ch	3.8	385.5		
N	4.5	384.8		
T.P.	6.60	394.69	1.24	388.09
17.85 W = P.I. $\frac{1}{4}$ Bittern + E. Line Klauber				
N	7.8	386.9		
ch	7.3	387.4		
1/4	6.8	387.9		
$\frac{1}{4}$ Bittern + E. Line Klauber	5.8	388.9		
17.86 W = N. 1/4 Bittern + E. Line Klauber				
N 1/4 Bittern + E. Line Klauber	5.2	389.5		
N. ch.	5.2	389.5		
N	5.5	389.2		
17.86 W = P.I. N. ch. Bittern + E. Line Klauber				
N	4.0	390.7		
N. ch. Bittern + E. Line Klauber	3.9	390.8		
17.86 W = P.E. N. Line Bittern + E. Line Klauber				
N	2.6	392.1		

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder  
stake for any width roadway, slope 1 1/2 to 1.  
If ground is nearly level, the cut or fill at the  
stake is located by the double entry method in  
left column and top row. The number in body  
of table is same for any column and row.  
From side stake to slope stake. If ground is not

**IMPROVED TABLES  
AND  
INFORMATION**

TABLE No. 2.

To find Tangent and External for curve of  
any other degree, divide by degree of curve and  
add connection found in column of constants.  
Degree of curve with a given  $L$  may be found  
by dividing tangent (or external), opposite  $L$  by  
given tangent (or external).  
The distance from a point on the tangent to  
the curve is very nearly the square of the tangent  
length divided by twice the radius.

TABLE II—Continued  
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III

INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{7}{8}$	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{7}{8}$
$\frac{15}{16}$	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{15}{16}$
$\frac{1}{16}$	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	$\frac{1}{16}$
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV  
USEFUL RELATIONS.

Lineal feet	× .00019	= miles
Lineal yards	× .0006	= miles
Square inches	× .007	= square feet
Square feet	× .111	= square yards
Square yards	× .0002067	= acres
Acres	× 4840	= square yards
Cubic inches	× .00058	= cubic feet
Cubic feet	× .03704	= cubic yards
Links	× .22	= yards
Links	× .66	= feet
Feet	× 1.5	= links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790^\circ$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654$$

$$\sqrt{\frac{1}{A}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163$$

$$\sqrt{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776$$

$$\pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167$$

$$\frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776$$

$$\sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205$$

$$\frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)<sup>2</sup>

Difference between arc and chord length, 0.05 feet in  $11\frac{1}{2}$  miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE.

$$\text{Horizontal Distance} = R - R \sin^2 a + C \cos a$$

$$\text{Vertical Distance} = R \frac{1}{2} \sin 2a + C \sin a$$

distance from Object glass to cross hairs

$$R = \text{Reading} \times \frac{\text{distance between cross hairs}}{\text{distance from Object glass to cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

15  
1965  
105765

1775 00  
421  
279

6031  
463  
6094  
606  
5777

87 87  
20-04-30  
67-55-30

696136 - 1707185  
10430 1.277121  
1.689236

360 x 1  
30  
1681230



287.43  
90  
377.43

1.41.42  
60  
84.852.2

1.1V(3260)  
6877920

44157  
267  
2126-7  
645  
5781-BM

179.60  
13.15  
15.21  
Rich. Sk

39°15'30" = P

179-60  
98-48  
81-12

60.60  
2271  
8779  
2174

180  
4 26  
6.06

65374  
34035  
31336 =

0.00  
0.15  
+40  
+53  
+76  
+100  
+128  
+140  
+170  
+200  
+250

ENGINEERING DEPARTMENT  
CITY OF CALIFORNIA  
SAN DIEGO

1165  
1063  
2062

179.60  
60.43  
119.17