

1216

Rose Canyon Road

1216

PASTY

FIELD BOOK

No. 385



F. B. 1216

? page 68  
also page 71

MICROFILMED  
DEC 22 1964

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**THE FREDERICK POST CO.**  
*ENGINEERING and DRAFTING SUPPLIES*  
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CHICAGO, ILL.







P.L. 1797

P.L. 1798

Sketch showing Location of two Cor's N.E. P.L. 1797:

Redd. Inc. 1

1.06  
3/4" pipe for Service Sta Cor unknown authority;

8.57'

P.L. Cor

5.77'

Not found.  
S. 1/4 Sec. 10  
by Hoopes.

P.L. 1797  
54.37'  
54.8'  
sinks  
Hoopes  
iron pin alongside

32.38'

0.22'

0.22'

N.E. Cor 1797 used by Hoopes: Old hub 11" deep. New hub set above old one is 5" deep.

Cor hub for Lane's Sta unknown authority.  
102.80'

3/4" Pipe: Cor

15.87'

hub with iron pin alongside  
by Hoopes: hub has been hit  
See owner of Rose Canyon  
Service Sta for plat of  
Hoopes survey.  
Mr Harris owner.

4 mi. W. of Balboa Ave.

110.83 mi.



## Random Line:

	Lt	Rt	Col	Mag.
50+60 <sup>20</sup>				
53+66	9° 10'	1° 47' 30"	N 41° 54' W	N 57° 20' W
521				
48+45	9° 15'		N 43° 41' 30" W	N 59° 15' W
248				
45+97		8° 16' 30"	N 34° 26' 30" W	N 49° 20' W
270				
42+27	16° 28'		N 42° 43' W	N 57° 55' W
164				
41+63		8° 31' 30"	N 26° 15' W	N 41° 35' W
753				
34+10		2° 05'	N 34° 46' 30" W	N 50° 30' W
187				
32+23	27° 02' 30"		N 56° 51' 30" W	N 72° 00' W
639				
25+84		2° 9' 30"	N 22° 49' W	N 45° 0' W
334				
22+50	5° 24' 30"		N 31° 58' 30" W	N 47° 30' W
275				
17+75	17° 49' 30"		N 26° 34' W	N 42° 15' W
1100				
9+75	5° 8' 30"		N 8° 47' 30" W	N 24° 00' W
315				
5+60		14° 03'	N 3° 36' W	N 19° 30' W
560				
0+00 sea sketch			N 17° 39' W	N 33° 10' W

Alignment crosses  
S.W. P.h. 1787 between  
Sta 25+84 & Sta 32+23

start here







True Line thru Pk. 1778 and 1777:

21 32 7  
2 84  
34 16 7

	L	R	Cor	Mag.
			N 16° 34' E	
37+937		11° 42' 30"		
	3053		N 4° 51' 30" E	
33+907		27° 29'		
	393		N 22° 37' 30" W N 37° 30' W	
30+877		7° 27'		
	6310		N 30° 4' 30" W	
24+462		12° 09'		
	284		N 48° 13' 30" W	
21+827	9° 12'			
	166		N 39° 1' 30" W N 54° 10' W	
19+667		28° 25' 30"		
	175		N 67° 27' W N 82° 30' W	
17+912	41° 35'			
	164		N 21° 52' W	
16+872		27° 20'		
	265		N 53° 12' W N 68° 00' W	
13+622		17° 10'		
	144		N 70° 22' W N 85° 30' W	
12+182	33° 59'			
	768		N 36° 23' W N 51° 30' W	
4+507		5° 31'		
	450.7		N 41° 54' W N 57° 20' W	
0+00	= S.L. Pk. 1778			

Alignment crosses S.L.  
P.L. 1777 between Sta.  
24+162 & Sta. 30+472

69+2195

67+77.95

60+09.95

Hub 1074 West of S.L. Cor. 1778 See page 5

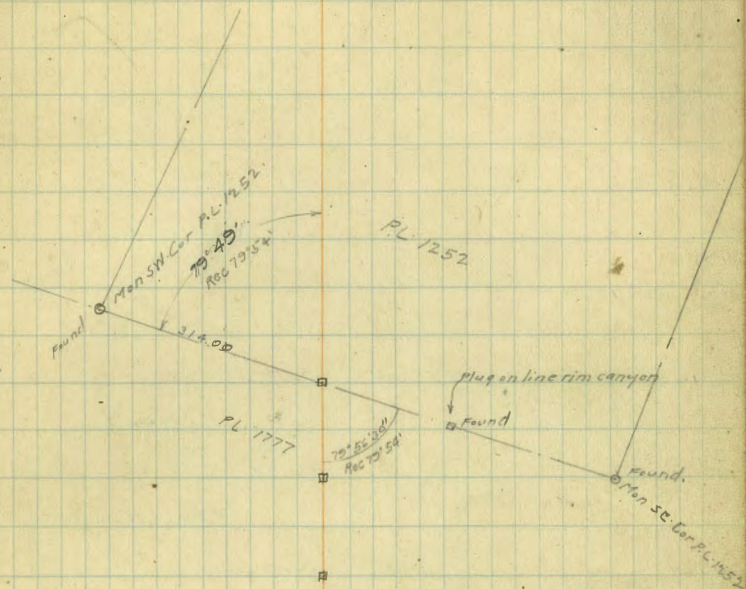


Lt Rt Cal 1999

60009  
5823.7  
177.2

60+0090 - Rumsey 115+67 Book 125 Page 54 - N.L. R.L. 1777 - S.L. 1252 115+6015

Distance	Angle	Bearing
58+232	18° 32' 30"	N 25° 7' W
138		N 43° 39' 30" W
56+857	33° 0' 30"	N 10° 39' W
296		N 51° 56' W
53+897	41° 17'	N 7° 14' 30" W
158		N 29° 41' E
52+312	44° 41' 30"	N 10° 39' W
83		N 7° 14' 30" W
51+982	36° 55' 30"	N 29° 41' E
200		N 10° 39' W
53+892	54° 12'	N 7° 14' 30" W
134		N 10° 39' W
42+142	16° 31'	N 29° 41' E
168		N 10° 39' W
40+462	24° 34'	N 7° 14' 30" W





	Lt	Rt	Cal	Mag.
277			N 26° 03' 30" W	
22+46	35° 34' 30"			
198			N 7° 31' E	
20+98		46° 4' 30"		
168			N 36° 33' 30" W	
19+30	28° 56'			
120			N 7° 37' 30" W	
18+10	26° 50' 30"			
172			N 19° 13' E	
16+38		23° 09'		
169			N 3° 56' W	
14+67		12° 43'		
298			N 16° 39' W	
11+71		41° 46'		
257			N 58° 25' W	
9+14	30° 56'			
136			N 27° 29' W	
7+78	13° 56' 30"			
126			N 13° 32' 30" W	
6+52	21° 43'			
200			N 8° 10' 20" E	
4+52		33° 17' 30"		
452			N 25° 07' W	

452  
 177.2  
 629.2



True line thru RL 1252

9

Lt R+ Cal Mag

22+8

20+9

19+3

18+10

16+3

14+6

11+71

9+15

7+78

6+52

$28+00^{60} = \text{Rumsey } 143+81 = \text{M.C. RL } 1252 = \text{S.L. P.L. } 1267$

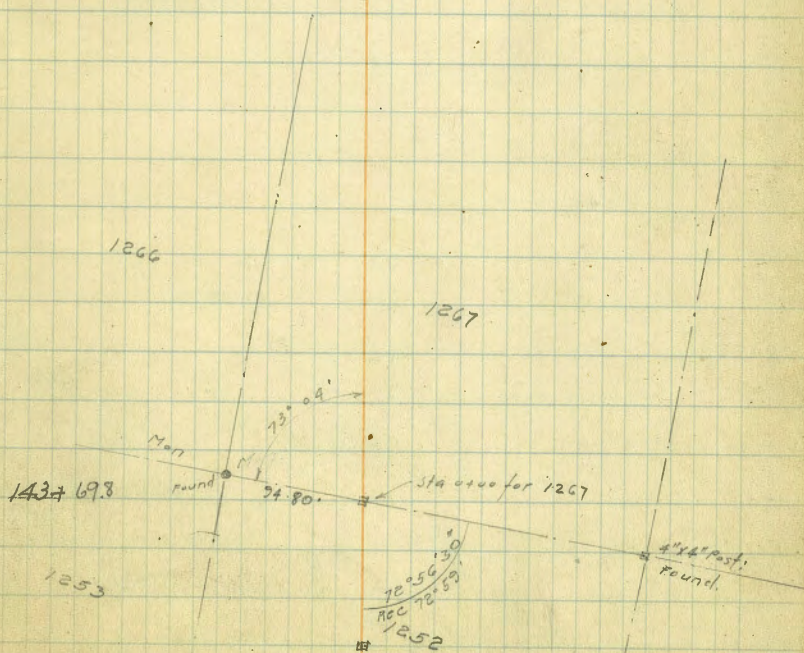
4+52

2+00

25+18

5° 36'

N 31° 39' 36" W





	Lt	R+	Cal	Mag
	167'		N 58° 59' E	
27+03		68° 16' 30"		
	161'		N 9° 47' 30" W	
24742	43° 44'			
	181'		N 33° 56' 30" E	
23+61	37° 52' 30"			
	123'		N 71° 49' E	
22+36		62° 23'		
	99'		N 9° 26' E	
21+37	20° 04'			
	259'		N 29° 30' E	
18+78		32° 28'		
	278'		N 2° 58' W	
16+00		19° 30'		
	212'		N 22° 28' W	
13+88	11° 34'			
	500'		N 10° 54' W	
8+88	5° 32' 30"			
	269'		N 5° 21' 30" W	
5+19		43° 00'		
	100'		N 48° 21' 30" W	
4+19	16° 42'			
	419'		N 31° 39' 30" W	

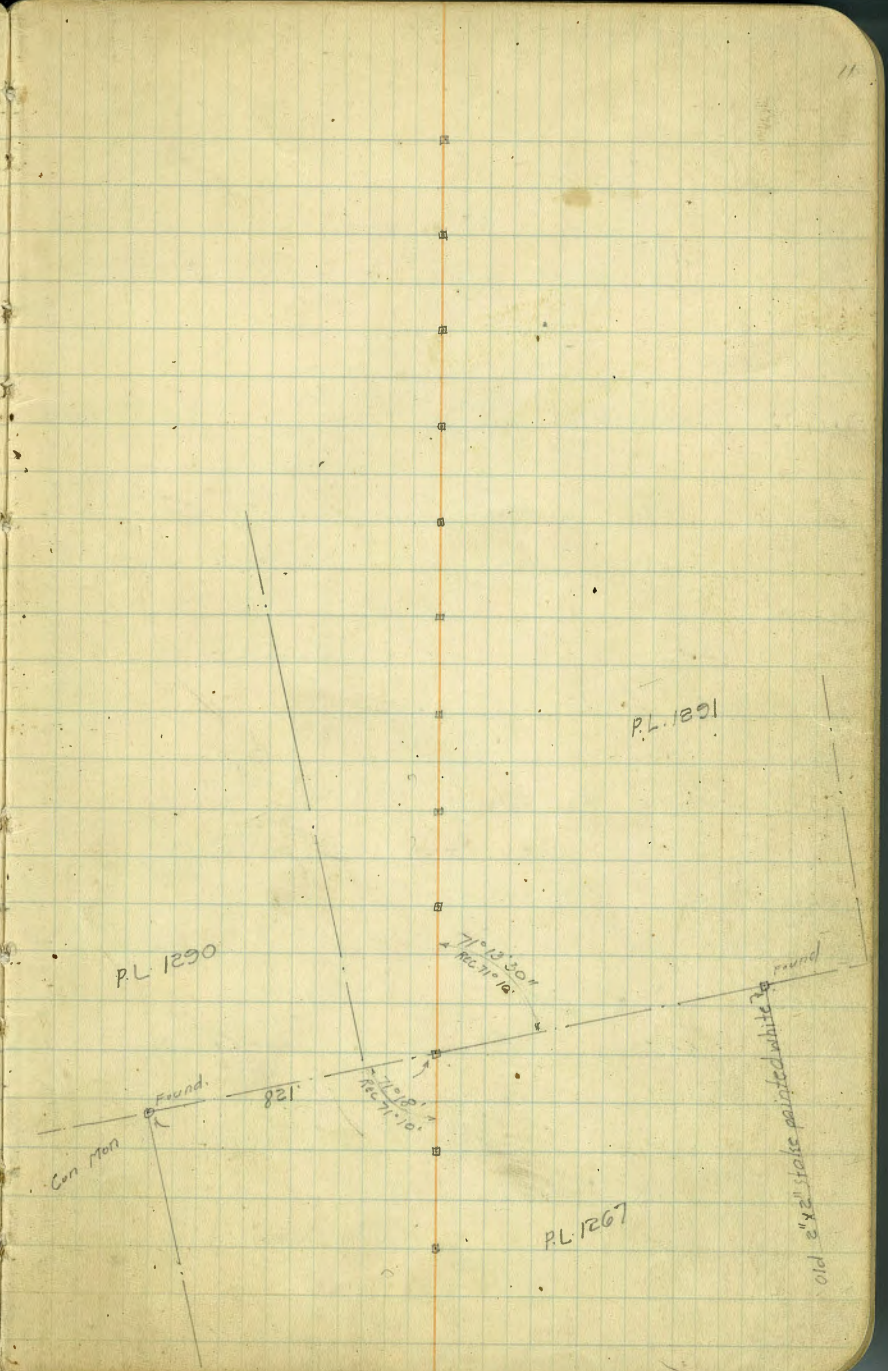
0+00 = S.L. P.L. 1267 = 7480 E of Mon. See sketch page 9.



	Lt	Rt	Cal	Mag.
44+87	8° 0' 30"			
	138'		N 5° 24' 30" W	
42+49		15° 41'		
	265'		N 21° 5' 30" W	
40+84	10° 50'			
	214'		N 10° 15' 30" W	
38+70	8° 23' 30"			
	172'		N 1° 52' W	
36+98		15° 46'		
	146'		N 71° 38' W	
35+57	52° 45' 30"			
	131'		N 31° 27' 30" E	
34+21		83° 28'		
	155'		N 52° 26' 30" W	
32+66	37° 07' 30"			
	111'		N 15° 13' W	
31+55	19° 10'			
			N 3° 57' E	
			Alignment crosses	
			St. PL 1291 between	
			Sta. 24491 & 31+55	
		0° 4' 30"		
			N 3° 57' E	
			N 23° 51' E	
29+94	19° 54'			
	124'			
28+70	35° 08'			

$\left. \begin{matrix} 31+55 \\ 30+15 \end{matrix} \right\} = \text{Rumsey } 174+864 \text{ B=4 } 125 \text{ } 199057$

Not a regular equation



PL 1291

PL 1290

PL 1267

old 2" x 2" stake painted white

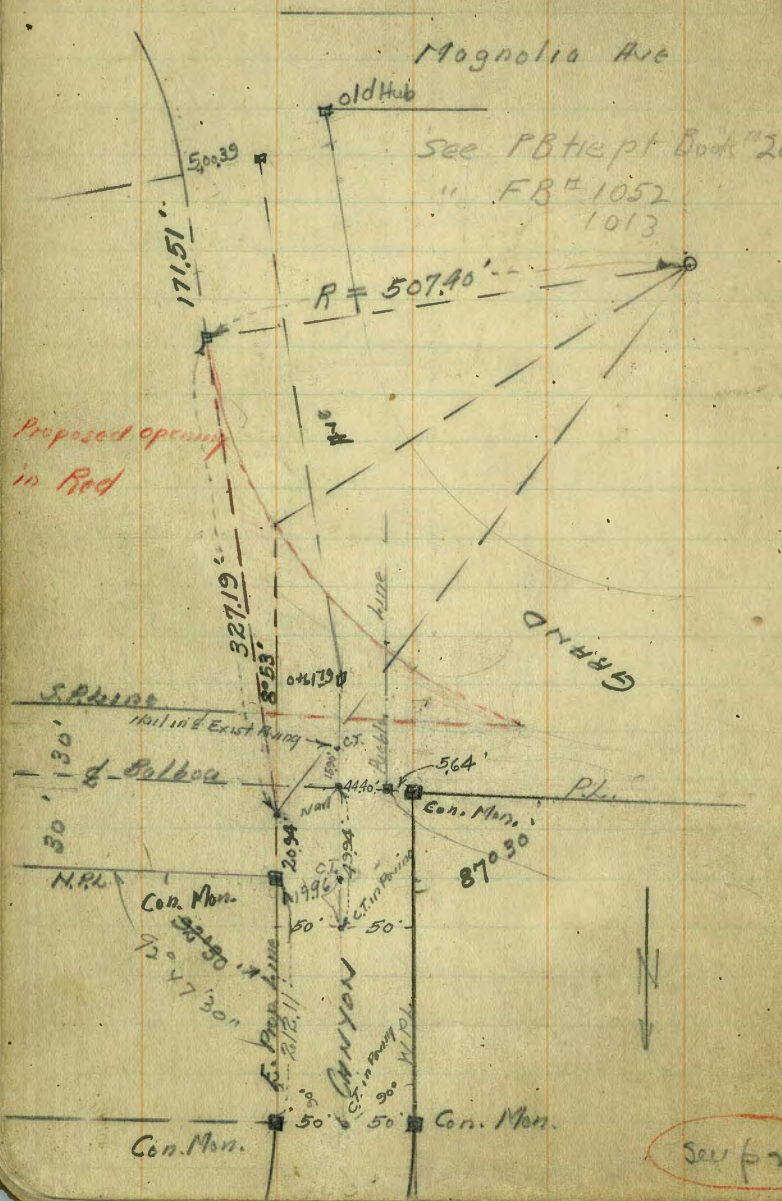






Walker  
Bliss  
Debert  
McDon  
6-21-30

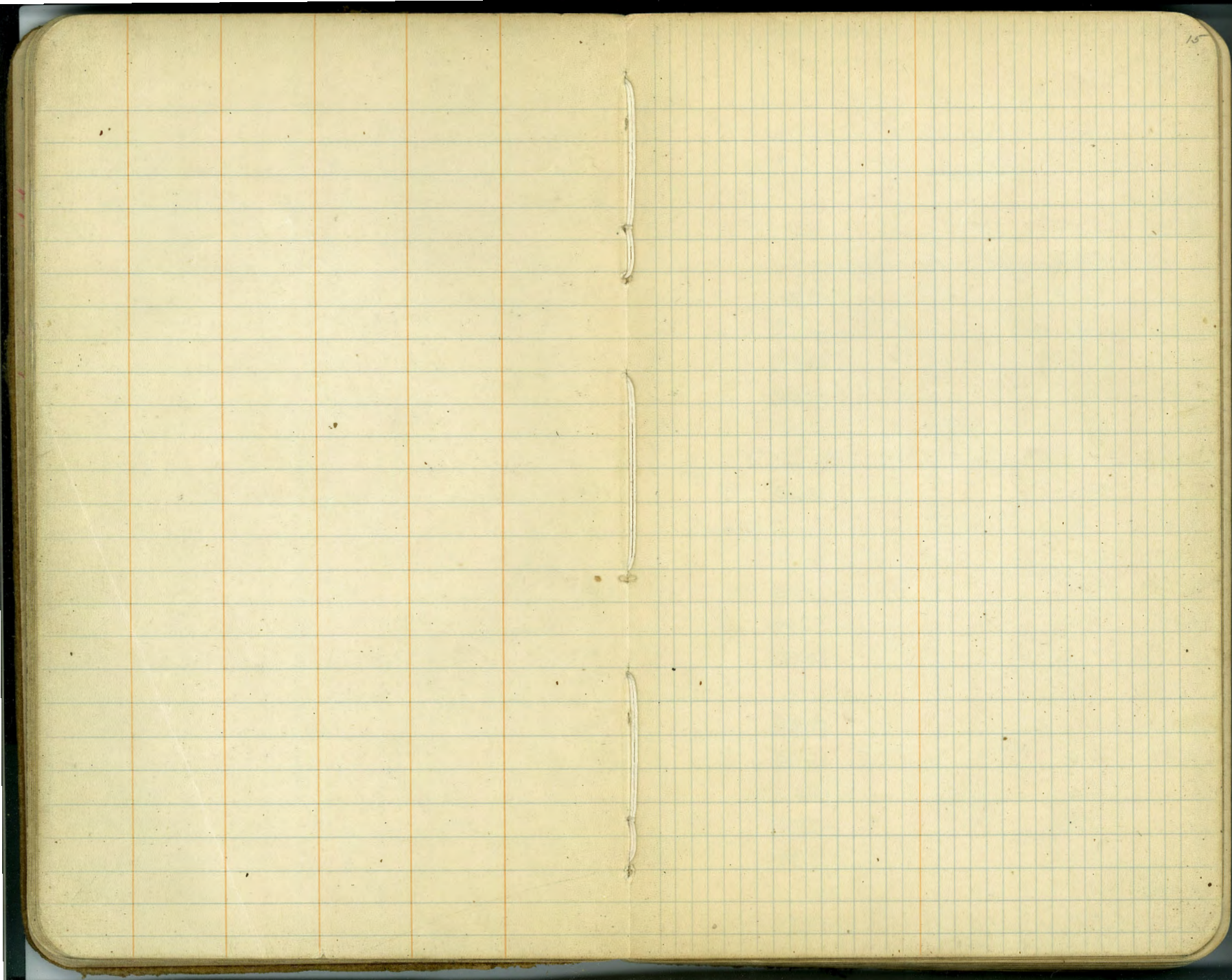
# SURVEY For Opening of Portion of GRAND AVE at Rose Canyon And Balboa Ave













McHugh  
Flood  
Ruplinger  
12/5/27

# X section Notes Rose Canyon Road

B.M. S.L. Balboa Ave U.S.G.S. 2543

corresponding City Elev =  $\frac{6.12}{19.31}$  ✓

Station  $\frac{22.60}{3.29}$  19.31

Edge Pavement  
-5.87

E.L. 3.59 19.17

C.L. 4.08 18.52

W.L. 4.57 18.03

0+00 = S.L. PL 1988

W.L. 4.3 18.30 ✓

C.L. 4.0 18.60

EL 3.5 19.10

0+50

E.L. 4.0 18.60

+7 4.8 Edge of Graded Road 17.80

+13 4.5 18.10

C.L. 4.6 18.00 ✓

+15 5.0 " " " 17.60

W.L. 4.6 18.00

1+00

W.L. 5.1 17.50

+8 5.6 " " " 17.00 ✓

C.L. 5.0 17.60

+13 5.6 " " " 17.00

EL 4.2 18.40

1+50

EL 5.1 17.50

Bench data received from  
County Engineer's Office

U.S.C + G.S. @ 0.00

✓ U.S.G.S. = 2.80

City = 6.119

U.S.G.S. = -9.01 City

N.G.



	-	$\pi$	+	Elev.
		22.60		16.70
+ 8	5.9	Edge of Graded Road		
CL	5.7			16.90 ✓
+ 14	6.1	"	"	16.50
WL	5.4			17.20
2+00				
W.L.	6.1			16.50
+ 6	6.5	"	"	16.10 ✓
CL	6.2			16.40
+ 12	6.1	"	"	16.50
EL	5.7			16.90
2+50				
EL	6.0			16.60
+ 10	6.3	"	"	16.30 ✓
CL	6.3			16.30
+ 14	6.9	"	"	15.70 "
WL	6.4			16.20
3+00				
W.L.	6.4			16.20
+ 7	7.1	"	"	15.50 "
CL	6.5			16.10 ✓
+ 12	6.7	"	"	15.90 "
E.L.	6.3			16.30
3+50				
EL	6.7			15.90
+ 8	7.1	"	"	15.50 "



	-	$\pi$ 22.60	+	Elev.
C.L.	6.7			15.90
+13	7.3	Edge of Graded Road		15.30
W.L.	6.7			15.90 ✓
T.P.	6.74	18.17	2.31	15.86 ✓
4+00				
W.L.	3.0			15.17
+7	3.1	"	"	15.07
C.L.	2.7			15.47 ✓
+11	3.1	"	"	15.07
E.L.	2.4			15.77
4+50				
E.L.	2.8			15.37
+8	3.5	"	"	14.67
C.L.	3.1			15.07 ✓
+13	3.4	"	"	14.77
W.L.	3.0			15.17
5+00				
W.L.	3.4			14.77
+11	4.0	"	"	14.17
C.L.	4.0			14.17 ✓
+13	4.7	"	"	13.47
E.L.	3.4			14.77
5+50 = Two Sycamore trees on East 8' Back				
5+57.59 Rt L. to back fence				
E.L.	5.9			12.27



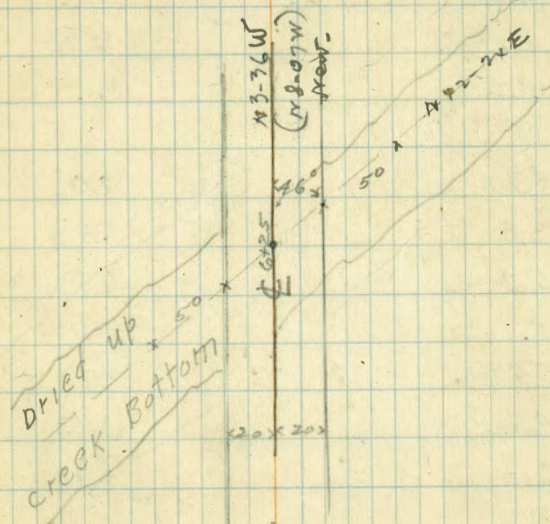
	$\bar{x}$	$\bar{y}$	-	Elev.
CL	6.7	18.17		11.47
+10	4.1			14.07
W.L.	5.4			12.77
+10	5.5			12.67
+20	6.3			11.87
5+60	$\Delta$	Split of L		14'03'
WL-20	7.2			10.97
-10	6.0			12.17
W.L.	5.4			12.77
+10	4.2			13.97
C.L.	6.5			11.67
EL	5.9			12.27
+10	4.2			13.97
+15	4.2			13.97
5+62 <sup>46</sup>		Rt 13 to forward Tang		
EL	5.9			12.27
CL	6.7			11.47
+10	4.2			13.97
WL	5.6			12.57
+20	7.3			10.87
6+00				
W.L.	10.5			7.67
+13	10.0			8.17
+17	8.3			9.87
CL	8.0			10.17



	-	$\pi$ 18.17	+	Elev.
+18	7.7			10.47
EL	8.0			10.17
+7	8.2			9.97
+18	3.3			14.87
+20	2.3			14.87
T.P.	8.31	15.73	5.87	9.86
6+25				
EL-50	7.7			8.03
E.L.	8.0			7.73
+12	7.8			7.93
+15	6.2			9.53
CL	6.0			9.73
+6	6.2			9.53
+12	7.6			8.13
W.L	8.0			7.73
+50	8.2			7.53
6+50				
WL-13	5.2			10.53
WL-8	7.8			7.93
WL	7.6			8.13
+10	7.6			8.13
+12	6.0			9.73
C.L.	5.9			9.83
+10	6.1			9.63
+15	6.7			9.03

£ creek Bottom 46°R

£ Creek Bottom taken on L 46°R



45-60  
 336  
 ---  
 42-24



	$\bar{x}$	$\frac{\pi}{15.73}$	+	Elev.
E.L.	7.8			7.93
6+65				
EL-10	7.8			7.93
EL	6.2			9.53
+12	6.4			9.33
+13	5.5			10.23
CL	5.6			10.13
+10	5.6			10.13
+15	6.4			9.33
WL	4.5			11.23
6+75				
W.L.	3.7			12.03
+5	3.8			11.93
+10	5.4			10.33
CL	5.7			10.03
+10	5.7			10.03
+15	4.6			11.13
E.L.	6.3			9.43
7+00				
EL	3.5			12.23
+7	3.4			12.33
+12	4.7			11.03
CL	4.7			11.03
+12	5.0			10.73
+13	3.8			11.93



	+	$\pi$ 1573	+	Elev.
W.L.	3.7			12.03
7+50				
W.L.	5.0			10.73
+10	4.4			11.33
C.L.	4.0			11.73
+10	3.8			11.93
E.L.	5.1			10.63
8+00				
E.L.-10	5.1			10.63
E.L.	4.8			10.93
+9	3.5			12.23
C.L.	3.3			12.43
+11	3.5			12.23
W.L.	3.5			12.23
8+50				
W.L.	3.0			12.73
+10	3.1			12.63
C.L.	2.7			13.03
+12	2.5			13.23
E.L.	4.3			11.43
T.P.	2.24	2010'	6.61	13.49
8+75	△ 5°08'30"lt (Split of L)			
E.L.-10	10.0			10.10
E.L.	7.2			12.90
+5	6.5			13.60

Tree 4' in diam 5' in Road = First of a series of 18 Eucalyptus trees on west ranging from 2' to 5' in road and from 1' to 4' in diam



	-	R 20.10	+	Elev.
CL	6.6			13.50
+11	6.9			13.20 ✓
WL	8.2			11.90
9+00				
WL	6.6			13.50
+0	6.3			13.80 ✓
CL	6.1			14.10
+15	6.4			13.70
EL	8.3			11.80
+5	8.3			11.80
9+50				
EL-20	12.1			8.00
EL	5.9			14.20 ✓
+7	5.6			14.50
CL	5.6			14.50
+12	5.4			14.70
WL	4.6			15.50
10+00				
WL	3.9			16.20
+8	5.3			14.80
CL	5.0			15.10
+10	5.6			14.50 ✓
EL	5.3			14.80
E.L+24	14.2			5.90
EL+38	5.1			15.00



	-	$\pi$ 20.10	+	Elev.
10+30				
EL	-40	5.0		15.10
EL	-20	5.6		14.50
EL		4.8		15.30
+	11	5.1		15.00 ✓
C L		4.9		15.20
+	13	4.9		15.20
W L		3.6		16.50
11+00				
W L		3.0		17.10
+	10	3.9		16.20
C L		4.1		16.00 ✓
+	15	4.2		15.90
EL		4.3		15.80
11+50				
EL		3.6		16.50
+	5	3.7		16.40
C L		3.5		16.60
+	11	3.1		17.00
W L		2.4		17.70
12+00				
W L		2.2		17.90
+	10	2.4		17.70 ✓
C L		2.8		17.30
+	18	2.9		17.20



	-	$\pi$ 20.10	+	Elev
EL	2.6			17.50
T.P.	1.38	2391	5.19	18.72
12+50				
EL-25	8.0			15.91
EL-6	5.7			18.21
EL	6.2			17.71
CL	6.4			17.51
+10	6.5			17.41
WL	6.7			17.21
WL+25	6.9			17.01
13+00				
WL-25	6.0			17.91
WL	6.0			17.91
+7	fence			
+13	6.4			17.51
CL	6.4			17.51
EL	5.4			18.51
+6	5.0			19.91
+25	8.1			15.81
13+50				
EL-25	8.9			15.01
EL-15	5.4			18.51
EL-4	Fence			
EL	5.8			18.11

519

20

~~Instrument adjusted for level and  
bench line run. Difference in  
elevation 0.15~~

= last of line of eucalyptus trees

34.44 = B.M.  
2.61  

---

37.05  
6.47  

---

30.58  
2.27  

---

32.85  
5.77  

---

27.08  
6.78  

---

33.86  
.01  

---

33.85

= barbed wire fence

= Start of small eucalyptus grove on west  
5' back, average diam about 6"

Barbed wire fence

" " "

" " "



	-	$\Delta$ 23.91	+	Elev.
C L	5.7			18.21
+7	6.0			17.91
+14	fence			
W.L.	5.7			18.21
+25	5.7			18.21
14+00				
WL-25	5.8			18.11
WL	5.5			18.41
+8	fence			
+15	5.7			18.21
C L	5.4			18.51
EL	4.9			19.01
+3	fence			
+10	5.6			18.31
+25	8.7			15.21
14+50				
EL-25	8.8			15.11
EL-16	5.6			18.31
EL-1	fence			
EL	4.4			19.51
C L	4.7			19.21
+6	5.0			18.91
+14	fence			
WL	5.2			18.71
+25	5.2			18.71



	-	$\pi$ 2391	+	Elev.
15+00				
WL-25	5.4			18.51
WL	5.0			18.91
+6	fence			
+13	4.4			19.51
CL	4.1			19.81
EL	4.8			19.11
+2	fence			
+16	5.4			18.51
+25	8.3			15.61
15+50				
EL-25	8.6			15.31
-15	8.3			15.61
-5	4.0 fence			19.91
E.L.	3.2			20.71
CL	3.6			20.31
+7	3.9			20.01
W.L.	4.3			19.61
+25	4.5			19.41
T.P.	2.78	3042	9.29	21.13
16+00				
WL-25	10.3			20.12
WL	10.3			20.12
+14	9.6			20.82
CL	9.2			21.22

15+40 = End of fence on West  
and end of eucalyptus grove also



	-	$\pi$ 30.42	+	Elev
EL	9.1			21.32
+6	Fence			
+7	9.7			20.12
+12	12.4			18.02
+25	14.8			15.62
16+50				
EL-30	14.5			15.92
-6	Fence			
EL	8.0			22.42
CL	8.1			22.32
WL	9.2			21.22
+25	9.3			21.12
16+80				
WL-25	6.8			23.62
WL	7.0			23.42
+16	7.8			22.62
CL	7.2			23.22
EL	7.1			23.32
+5	8.5 Fence			21.92
+18	9.9			20.32
+25	12.7			17.72
+40	14.3			16.12
17+50				
EL-50	14.0			16.42
-25	8.2			22.22



	-	+	Elev.
-7	4.5 Fence	30.42	25.92
EL	5.2		25.22
CL	5.3		25.12
+7	5.6		24.82
+10	3.4		27.02
WL	3.5		26.92
+25	3.1		27.32
18+00	Creek bed starts following toe of slope here		
WL-25	1.5		28.92
WL	2.9		27.52
+8	2.9		27.52
+13	5.1		25.32
CL	4.5		25.92
EL	4.6		25.82
+6	3.8 Fence		26.62
+25	9.0		21.42
+50	12.4	stream bed.	18.02
18+70			
-50	9.3		21.12
-25	8.3		22.12
-7	6.3		24.12
-5	Fence		
EL	3.8		26.62
CL	4.1		26.32
+7	4.6		25.82

creek bottom is rather thickly wooded with willows, and the bottom partly covered with debris.



	-	$\pi$	+	Elev
WL	0.6	30.42		29.82
+10	0.4			30.02
+25			+1.5	31.92
T.P.	2.43	34.52	6.53	27.99

From this point on the + rods will be in the second column. The - rods in the forth column

	+	$\pi$	-	Elev
		34.52		27.99
19+50				
WL-10	+5.6			40.1
WL-5			0.0	34.5
WL			4.5	30.0
+6			7.6	28.9
CL			7.0	27.5
+16			6.9	27.6
EL			7.9	26.6
+1	Fence			
+5			11.5	23.0
+25			11.5	23.0
19+75	$\Delta$			
EL-35			14.1	20.3
-18			13.6	20.9
-4			9.8	24.7
-2	Fence			

T.P. nail in fencepost 25' Right of 18+60



	+	$\pi$ 34.52	-	Elev	
EL			6.5	28.0	✓
¢			6.4	28.1	
+14			6.9	27.6	
WL			5.4	29.1	
20+50					
WL-10	+29.2			63.7	
-5			0.0	34.5	✓
W.L.			3.6	29.9	
C.L.			5.8	28.7	
EL			6.1	28.3	
+5			6.3	28.2	
+12			12.5	22.0	
+25			12.5	22.0	
21+00					
EL-25			12.3	22.2	
-13			11.0	25.5	
-3			5.5	29.0	
E.L.			5.4	29.1	✓
¢			5.1	29.4	
+14			5.5	29.0	
WL			4.4	30.1	
+7			0.9	33.6	
+12	+32.0		3	66.5	
21+75					
WL-18	+36.0			70.5	



	+	$\pi$ 34.52	-	Elev.
--	---	----------------	---	-------

WL-12			0.00	34.5
-------	--	--	------	------

-7			3.1	31.4
----	--	--	-----	------

WL			3.8	30.7
----	--	--	-----	------

$\phi$			4.0	30.5
--------	--	--	-----	------

E.L.			4.1	30.4
------	--	--	-----	------

+3			4.1	30.4
----	--	--	-----	------

+16			11.4	23.1
-----	--	--	------	------

+40	same fence		12.7	21.8
-----	---------------	--	------	------

22+49 <sup>7/8</sup>	$\Delta$ 5°24'30" LT Taken Rt Ls to		Back tan.	
----------------------	----------------------------------------	--	-----------	--

EL			3.9	30.6
----	--	--	-----	------

+3			2.6	31.9
----	--	--	-----	------

$\phi$			3.2	31.3
--------	--	--	-----	------

WL			3.3	31.2
----	--	--	-----	------

22+50 <sup>D</sup>	Taken on split of L		5°24'30" LT.	
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WL-10			0.0	34.5
-------	--	--	-----	------

W.L.			3.3	31.2
------	--	--	-----	------

$\phi$			3.2	31.3
--------	--	--	-----	------

+17			2.6	31.9
-----	--	--	-----	------

EL			3.9	30.6
----	--	--	-----	------

+13			11.5	23.0
-----	--	--	------	------

+25			11.5	23.0
-----	--	--	------	------

22+50 <sup>A</sup>	Taken Rt Ls to		forward tan	
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EL			3.9	30.6
----	--	--	-----	------

+3			2.6	31.9
----	--	--	-----	------

$\phi$			3.2	31.3
--------	--	--	-----	------



	+	$\Delta$ 21.52	-	ELEV
WL			3.3	31.2
T.P.	572	38.57 ✓	16.7	32.85 ✓
23+00				
WL-12			2.0	36.5
- 5			4.8	33.7
WL			6.6	31.9
¢			6.7	31.8 ✓
+17			6.9	31.6
EL			7.9	30.6
+10			14.9	23.6
+25			14.9	23.6
23+50				
EL-30			14.9	23.6
-11			14.3	24.2
EL			7.0	31.5 ✓
¢			6.4	32.1
WL			6.0	32.5
+18			1.3	37.2
24+00				
WL-18			1.0	37.5
-2			4.3	34.2
WL			4.5	34.0
+4			6.9	32.1
¢			6.1	32.4
EL			6.5	32.0



	+	$\pi$ 38.57	-	Elev.
EL+2			6.5	32.0 ✓
+10			12.7	25.8
+17			14.8	23.7
+25			15.0	23.5
24+50				
EL-25			14.1	24.4
-14			14.1	24.4
EL			6.5	32.0 ✓
E			5.6	32.9
+14			5.5	33.0
W.L.			3.3	35.2
+6			0.6	37.9
+9	+19.0			57.5
25+00				
WL-7	+2			40.7
-4			0.0	38.5
WL			3.3	35.2
+7			5.2	33.3
E			5.0	33.5 ✓
EL			5.9	32.6
+13			14.4	24.1
+25			14.4	24.1
$\Delta$ 25+34	2° 9' 30" RT.			
EL-25			14.2	24.3
-17			14.2	24.3



	+	π 38.67	-	Elev.	
EL-5			9.3	29.2	
EL			3.8	34.7	
¢			4.2	34.3	
+13			4.8	33.7	✓
WL	+1.0			39.5	
+5	+6.3			44.8	
+15	+11.5			50.0	
26+50					
WL-15	+13.0			51.5	
W.L.	+1.5			40.0	
+15			4.2	34.3	
¢			3.9	34.6	
+17			3.8	34.7	✓
EL			6.2	32.3	
+9			10.4	28.1	
+25			11.4	27.1	
27+00					
EL-35			12.0	26.5	
-7			9.5	29.0	
EL			6.8	31.7	
+5			3.3	35.2	✓
¢			3.5	35.0	
+17			3.8	34.7	
WL			1.7	36.8	
+12	+8.5			47.1	



	+	$\pi$	-	Elev.
WL+25	+15.6	38.57		54.1
27+50				
WL-25	+15.5			54.0
-7	+6.5			45.0
WL			0.7	37.8
+2			3.1	35.4
$\phi$			3.2	35.3
+13			3.2	35.3
EL			7.6	30.9
+30			12.0	26.5
+40			11.0	27.5
28+00				
E.L.-40			11.1	27.4
-15			9.5	29.0
EL			7.0	31.5
+6			2.0	36.5
T.P.	7.14	43.62	2.09	36.48
$\phi$			7.2	36.4
+17			7.4	36.2
WL			4.3	39.3
+8	+8.2			51.8
+25	+15.7			59.3
28+50				
W.L.-25	+20.2			63.8
-5	+11.2			54.8



	+	$\pi$ 43.62	-	Elev.
WL			4.6	39.0
+9			7.2	35.4
¢			6.9	36.7
+16			6.6	37.0
EL			9.5	34.1
+7			12.7	30.9
+35			17.3	26.3
29+00				
E.L. +45			21.8	21.8
-12			13.6	30.0
EL			8.1	35.5
+2			6.7	36.9
¢			6.8	36.8
WL			5.1	38.5
+2	+8.0			37.6
+22	+18.2			61.8
29+50				
WL-20	+20.0			63.6
-2	+8.5			52.1
WL			5.0	38.6
¢			6.6	37.0
EL.			6.3	37.3
+18			13.8	29.8
+50			16.5	27.1

30+00 at this point ¢ runs off graded road



	+	$\pi$ 43.62	-	Elev.
EL-50			16.4	27.2
-38			15.0	28.6
-10			11.8	31.8
-2			6.0	37.6
EL			6.0	37.6
+18			6.3	37.3
Q			4.8	38.8
WL	+11.0			54.6
+20	+22.4			66.0
30+50				
WL-18	+24.0			67.6
WL	+11.5			55.1
+10	+6.0			49.6
Q			4.3	39.3
+2			5.7	37.9
EL			5.2	38.4
+2			5.2	38.4
+5	beginning of barbed wire fence			
+15			12.4	31.2
+50			16.0	27.6
31+00				
EL-50			15.6	28.0
-10			11.4	32.2
-5	Fence			
EL			5.0	38.6

	+	$\pi$ 43.62	-	ELEV
EL+18			5.0	38.6
Q			3.5	40.1
+18	+12.0			55.6
WL	+12.7			56.3
+20	+26.3			69.9
31+50				
WL-21	+23.4			67.0
WL	+9.5			53.1
+7	+6.3			49.9
+18			2.5	41.1
Q			4.5	39.1
EL			4.0	39.6
+2			4.4	39.2
+5	fence			
+9			10.8	32.8
+40			14.2	29.4
+60			14.0	29.6
T.P.	6.90	46.48	40.4	39.58
32+00				
EL-50			18.2	28.3
EL-25			17.2	29.3
-4			15.0	31.5
-1	Fence			
EL			11.6	34.9
+7			6.6	40.9

39.58  
B.M. of Fence Post 31+30



	+	$\pi$ 46.48	-	Elev.
2			7.0	39.5
+8			7.5	39.0
+9			5.3	41.2
+15			3.6	42.9
+16	+1.4			47.9 ✓
W.L.	+3.3			49.8
+25	+21.2			67.7
<u>32+23</u>		27° 02' 30" Lt (split of L)		
WL-34	+26.0			72.5
-11	+9.5			56.0
WL			3.0	43.5
+5			5.0	41.5
+6			7.3	39.2
2			6.3	40.2 ✓
+8			5.6	40.9
+18	FENCE			
EL			14.3	32.2
+39			17.7	28.8
+40			18.7	27.8
+50			19.0	27.5
<u>32+50</u>				
EL-40			17.	29.5
-30			17.5	29.0
-15			17.5	29.0
-8	FENCE			

27° 02' 30" Lt. Taken on split of L



	+	$\pi$ 46.98	-	Elev.
EL-6			13.3	33.2
EL			9.2	37.3
+7			4.7	41.0
EL			5.9	40.6
+11			6.5	40.0
+12			4.6	39.9
WL	+1			47.5
+8	+14			60.5
+25	+24.7			71.2
<u>33+00</u>				
WL-25	+45.5			92.0
-5	+25.0			71.5
WL	+19.5			66.0
+4	+7.0			53.5
+12			1.5	45.0
+13			4.2	42.3
EL			3.9	42.6
#4			3.4	43.1
EL			8.0	38.5
+13			15.1	31.4
+33			16.0	30.5
<u>33+70</u>				
EL-50			14.7	31.8
-22			14.7	31.8
EL			2.9	43.6

	+	$\pi$ 46.98	-	Elev.
EL			2.4	43.1
+9			2.4	43.1
WL	+15.5			62.0
+21	+34.4			80.9
<u>34+10</u> $\triangle$ 22° 05' Rt (split of L)				
WL-17	+47.4			93.9
WL	+31.4			77.9
+9	+27.0			73.5
T.P.	9.36	53.77 <sup>v</sup>	2.07	44.41
+10			5.6	48.2
+19			8.6	45.2
EL			8.6	45.2
EL			8.9	44.9
+8			8.6	45.2
+28			21.0	32.8
+38			24.0	29.8
+50			24.5	29.3
<u>34+50</u>				
EL-75			25.7	28.1
EL-32			23.7	30.0
EL			7.5	46.3
EL			7.0	46.8
+6			7.0	46.8
+13	+1.2			55.0
WL	+27.1			80.9



	+	$\pi$ 53.77	-	Elev.
WL+26	+45.4			109.2
<u>35+00</u>				
WL-25	+46.0			109.8
WL	+26.2			80.0
+5	+20.0			73.8
+14			6.0	47.8
℄			5.5	48.2
EL			6.0	47.8
+26			23.5	30.3
+50			23.3	30.5
+70			23.3	30.5
<u>35+50</u>				
EL-45			22.9	30.9
-23			23.4	30.4
EL			5.4	48.4
+5			4.6	49.2
℄			4.5	49.3
+5			4.4	49.4
+10	+6.0			59.8
WL	+14.			67.8
+10	+31.			84.8
<u>36+00</u>				
WL-2	+20.		Slope Constant	73.8
WL	+18.0			71.8
℄			3.4	50.4

	+	$\pi$ 53.77	-	Elev.
EL			3.8	50.0
+30			21.5	32.3
+50			21.5	32.3
<u>36+50</u>				
EL-50			23.3	30.5
-23			21.3	32.5
EL			3.6	50.2
+4			2.0	51.8
+19			3.1	50.7
℄			1.0	52.8
WL	+25.6			79.4
+10	+36.0			89.8
<u>37+00</u> erect bottom branches off 2.5°Rt at this point				
WL-20	+38.4			92.2
WL	+23.4			77.2
+13	+11.3			65.1
+16			0.8	53.0
℄			0.8	53.0
+15			1.9	51.9
EL			4.4	49.4
+18			19.5	34.3
+50			21.0	32.8
TP	9.09	61.78	1.08	52.69
<u>37+50</u>				
EL-50			27.0	34.8



	+	$\pi$	-	Elev.
EL-35 fence		61.78		
-21			25.4	36.4
EL			13.0	48.8
+7			7.5	54.3
¢			7.2	54.6
+4			7.2	54.6
+7			1.4	60.4
+15	+7.7			69.5
WL	+12.5			74.3
+20	+29.5			91.3
T.P.	2.94	64.72	0.0	61.78
<u>38+00</u>				
WL-25	+24.0			88.7
WL	+5.5			70.2
+15			7.4	57.3
+16			9.0	55.7
¢			9.1	55.6
+13			8.7	56.0
EL.			13.9	50.8
+33 Fence				
+50			28.0	36.7
+60			29.1	35.6
<u>38+50</u>				
EL-80			29.0	35.7
-32 FENCE				

point 5165

	+	$\pi$	-	Elev.
EL		64.72		
+7			7.5	57.2
¢			7.7	57.0
+6			7.5	57.2
+7			5.7	59.0
WL	+6.8			71.5
+25	+24.5			89.2
<u>39+00</u>				
WL-25	+30.0			94.7
WL	+11.0			75.7
+10	+2.0			66.7
+17			6.4	58.3
¢			6.4	58.3
+14			6.4	58.3
EL			11.8	52.9
+26 Fence				
+50			23.5	41.2
+100			29.7	35.0
<u>39+50</u>				
EL-100			26.9	37.8
-50			21.2	43.5
-21 Fence				
-12			13.1	51.6
EL			7.1	57.6
+4			4.2	60.5



*	$\pi$	-	Elev.
	64.72		
¢		4.6	60.1
+1		2.8	61.9
+7	4.7		69.4
WL	11.5		76.2
+13	23.2		87.9
+25	30.0		94.7
39+75 Fence Jogs	EL+6		70.7
40+00			92.7
WL-25	28.0		92.7
WL	12.5		77.2
+19		1.5	63.2
¢		3.5	61.2
EL		2.3	62.4
+6 Fence			
+13		10.1	54.6
+50		17.5	47.2
+100		25.0	39.7
40+50			
EL-100		24.5	40.2
-50		18.0	46.7
-7 Fence		7.8	52.9
EL		2.7	62.0
+2		2.1	62.6
¢		2.8	61.9
+2		2.8	61.9
+3		0.0	64.7

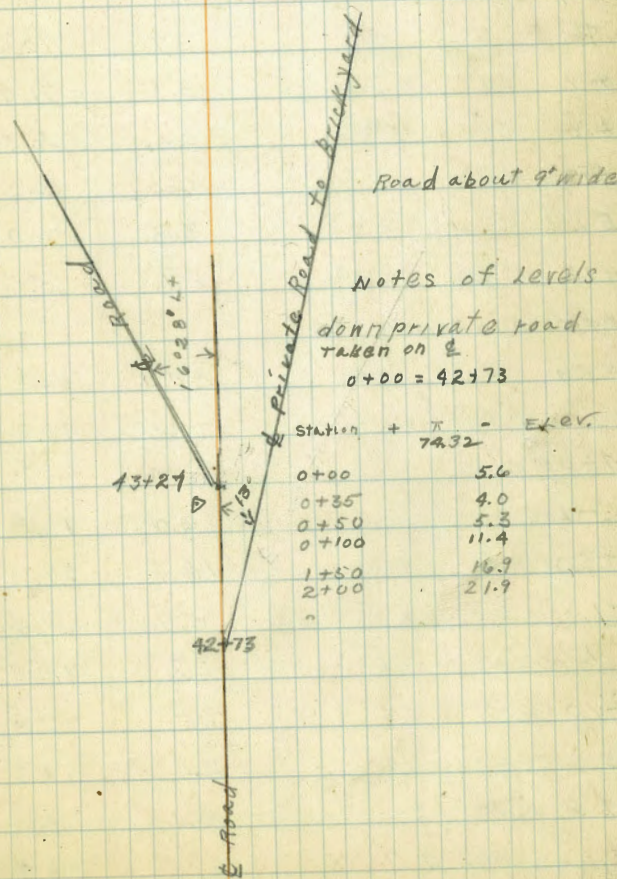
+	$\pi$	-	Elev.
	64.72		
+9	4.5		69.2
W.L.	11.2		75.9
+25	25.3		90.0
41+00			
WL-25	28.0		92.7
WL	15.0		79.7
+7	11.0		75.7
+17	2.4		67.1
+18		1.1	63.6
¢		1.1	63.6
+16		0.9	63.8
EL		3.4	61.3
+6 Fence			
+8		9.2	55.5
+50		19.0	45.7
+100		23.0	41.7
T.P.	10.85	74.32	1.25
41+63	$\Delta$	8°31'30" RT	sec. taken on split of L
EL-100		30.0	44.3
-50		24.2	50.1
-10		17.5	56.8
-8 Fence			
EL		11.2	63.1
+3		9.1	65.2
¢		9.2	65.3



	+	$\pi$	-	Elev
		74.32		
±12			9.1	65.2
+3			7.9	66.4
+12			1.5	72.8
W.L.	+2.0			76.3
+25	16.1			90.4
<u>42+18</u>				
W.L.-25	21.6			95.9
W.L.	5.2			79.5
+7	1.0			75.3
+13			5.8	68.5
+14			7.3	67.0
±			7.3	67.0
+14			7.4	66.9
E.L.			11.3	63.0
+5	Fence			
+8			16.5	57.8
+50			22.6	51.7
+100			28.0	46.3
<u>42+73</u>				
E.L.-100			27.0	47.3
-50			19.8	54.5
-5			9.7	64.6
-3	Fence			
E.L.			6.5	67.8
+5			4.4	69.9

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	+	$\pi$	-	Elev.
		74.32		
±			5.6	67.7
+10			6.0	68.3
+11			4.5	69.8
W.L.	+2			76.3
+25	+15			89.3





	+	$\bar{\pi}$ 74.3 ✓	-	Elev.
43+27	△ Taken on split of L			
WL-25	13.0			87.3
WL-5	4.7			79.0
WL			0.4	73.9
+2			2.0	72.3
+3			4.4	69.9
♀			3.7	70.6
+7			3.3	71.0
+10			6.0	68.3
+19			6.0	68.3
EL			3.3	71.0
+12			8.7	65.6
+15	Air Fence			
+50		20.0		54.3
+100		27.5		46.8
<u>44+00</u>				
EL-100		26.0		48.3
-50		16.4		57.9
-1		5.9		68.4
EL		2.8		71.5
+10		1.5		72.8
♀		2.1		72.3
+16		2.7		71.6
WL	2.0			76.3
+4	6.3			80.6

	+	$\bar{\pi}$ 74.3 ✓	-	Elev.
WL-25	12.7			87.0
<u>44+50</u>				
WL-25	7.1			81.4
-10	3.7			78.0
WL			0.8	73.5
+8			1.1	73.2
♀			0.6	73.7
+9			0.5	73.8
EL			4.3	70.0
+10			8.3	66.0
+50			17.7	56.6
+100			26.3	48.0
<u>45+00</u>				
EL-50			17.3	57.0
-10			5.3	69.0
EL			1.2	73.1
T.P.	10.06	82.17 ✓	2.21	72.11
+9			7.3	74.9
+12			8.2	74.0
♀			8.2	74.0
+15			8.4	73.8
WL			5.6	74.6
+4			1.2	81.0
+25	4.6			86.8
<u>45+50</u>				

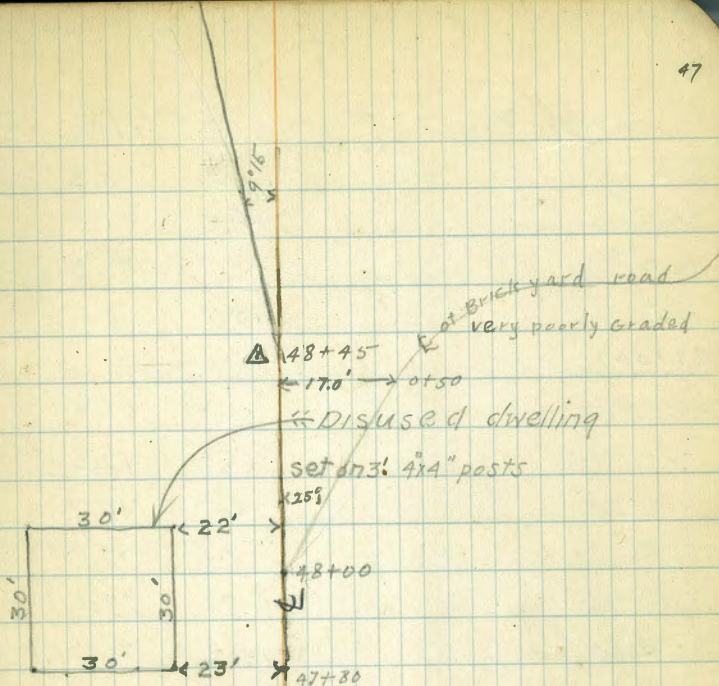


	+	T	-	Elev.
WL-25		82.11		
T.P.	1.84	83.33	0.62	81.49
WL-25	11.0			94.3
W.L.	1.9			85.2
+6			5.1	78.2
+7			7.1	76.2
℄			6.7	76.6
+13			7.9	75.4
E.L.			7.2	76.1
+4			8.3	75.0
+12			13.4	69.9
+48			20.6	62.7
+60			26.4	56.9
+75			28.6	54.7
<u>Δ45+97</u>	8°16'30"RT			
E.L.-75			28.0	53.3
-60			24.3	59.0
-55			20.7	62.6
-15			11.7	71.6
-6			6.3	77.0
E.L.			5.7	77.6
+10			5.2	78.1
℄			5.5	77.8
+12			5.6	77.7
W.L.	0.7			82.9

	+	T	-	Elev.
WL+25	11.9	88.33		95.2
<u>46+50</u>				
WL-25	9.9			93.2
-5			2.3	81.0
W.L.			3.9	79.4
℄			4.2	79.1
+12			5.1	78.2
E.L.			8.9	74.4
+50			2.14	61.9
+75			25.6	57.7
T.P.	2.90	85.24	0.49	82.84
<u>47+00</u>				
E.L.-75			23.4	61.8
-50			19.0	66.2
E.L.			13.4	71.8
+7			12.0	73.2
+16			5.2	80.0
℄			5.0	80.2
W.L.			4.2	81.0
+10	1.0			86.2
+13	4.0			89.2
+25	10.5			95.7
<u>47+50</u>				
WL-25	11.4			96.6
-20	7.2			92.4



	+	$\pi$	-	Elev.
		85.24		
WL-10	beginning of clay pit		0.5	84.7
	Toe of slope			
WL			2.2	83.0
+6			3.6	81.6
L			3.1	81.8
+12			2.9	82.3
EL			7.5	77.7
+25			13.8	71.4
+50			17.4	67.8
+75			22.3	62.9
<u>48+00</u>				
EL-75			19.6	65.6
-25			10.2	75.0
EL			3.1	82.1
+2			2.2	83.0
L			2.3	82.9
+17			2.4	82.8
WL			0.9	84.3
+50	2.5			87.7
<u>48+45</u>	Taken on split of L			
WL-75	5.3			90.5
-25	1.0			86.2
-13			0.8	84.4
WL			1.1	84.1
L			1.0	84.2
+6			5.6	79.6



Levels on Brickyard road

road 0+00 = 48+00

Sta	+	$\pi$	-	Elev
		85.24		
0+00				2.3
+13				1.9
+25				4.0
+50				5.8
+75				6.9
+100				8.2

= Top of slope of clay pit

" " " " " "



	+	$\pi$ 85.24	-	Elev.
EL			5.9	79.3
+25			8.3	76.9
+50			13.7	71.5
+75			18.8	66.4
<u>49+00</u>				
EL-75			16.3	68.9
-50			13.0	72.2
-25			8.5	76.7
-12			7.5	77.7
EL			8.1	77.1
£			7.0	78.2
+15			5.8	79.4
W.L.			2.9	82.3
+5			1.1	84.1
+25			0.9	84.3
+35	Wedge of graded road		0.4	84.8
+90	toe of Slope		1.0	84.2
<u>49+20</u>				
WL-115	0.2	toe of Slope		85.4
-15			1.0	84.2
-11			1.7	83.5
WL			6.5	78.7
£			7.3	77.9
EL			7.9	77.3
+13			7.9	77.3

	+	$\pi$ 85.24	-	Elev.
+25			14.7	70.5
+26			19.8	65.4
+40	Flat of Brick yard		26.0	59.2
+60			26.8	58.4
<u>50+00</u>				
EL-60			27.0	58.2
-30			26.0	59.2
-17			7.7	77.5
EL			9.3	75.9
£			9.5	75.7
W.L.			8.2	77.0
+35			4.0	81.2
+65			2.6	82.6
WL+130	toe of Slope		3.5	81.7
<u>50+50</u>				
WL-130			2.8	82.4
-75			5.5	79.7
-30			6.0	79.2
WL			8.7	76.5
£			9.3	75.9
EL			9.7	75.5
+18			9.8	75.4
+19	Flat of Brick yard		26.4	58.8
+50			28.	57.2
<u>51+00</u>				



	+	$\pi$	-	Elev.
EL-60		85.24	29.0	56.2
-25			28.3	56.9
-22			11.4	73.8
EL			10.2	75.0
£			9.6	75.6
W.L.			9.2	76.0
+50			6.3	78.9
+85			5.9	79.3
+140			3.6	81.6

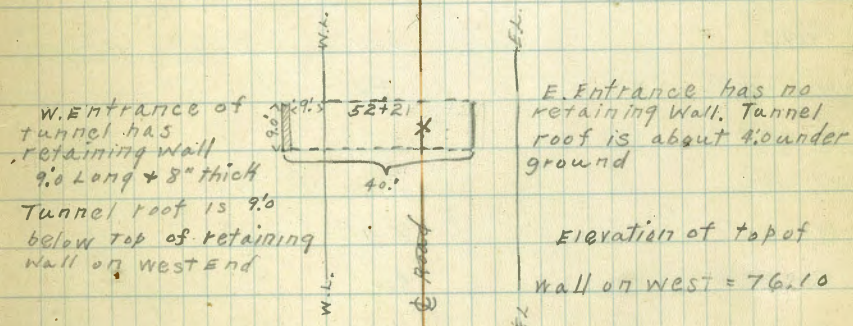
51+50  
T.P. 5.01 86.13 4.12 81.12

WL-110			6.1	80.0
-85			6.5	79.6
-50			6.1	80.0
-15			10.1	76.0
WL			9.1	77.1
£			10.4	75.7
EL			12.5	73.6
+11			14.0	72.1
+12			21.0	65.1
+25			27.0	59.1
+50			28.4	57.7
52+00				
EL-50			28.8	57.3
-18			26.0	60.1

nail in pipe  
50+90

	+	$\pi$	-	Elev.
-17		86.13	15.5	70.6
EL			13.3	72.8
£			10.0	76.1
WL			9.5	76.6
+10			9.9	76.2
+35			6.3	79.8
+70			6.5	79.6
+90			6.0	80.1
+110			4.8	81.3

52+21 = £ of tunnel under road. made of brick



W. Entrance of tunnel has retaining wall 9% Long x 8" thick

Tunnel roof is 9% below top of retaining wall on west end

E. Entrance has no retaining wall. Tunnel roof is about 4' under ground

Elevation of top of wall on west = 76.10

WL-9			10.03	76.10
WL			10.0	76.1
£			10.6	75.5
+11 = dirt at east end of tunnel			12.2	73.9
EL			13.6	72.5
52+50				



	+	$\pi$ 86.13	-	Elev.
EL-35			29.0	57.1
-14			29.0	57.1
-7			19.6	66.5
-6			14.2	71.9
EL			12.5	73.6
+6			13.4	72.7
+9			11.5	74.6
$\phi$			9.5	76.6
WL			9.3	76.8
+10			8.8	77.3
+50			5.7	80.4
+70			6.3	79.8
+90			5.9	80.2
+120			5.6	80.5
<u>53+00</u>				
WL-130			35	82.6
WL-80			54	80.7
-50			4.6	81.5
WL			7.6	78.5
$\phi$			8.3	77.8
EL			8.0	78.1
+7			12.0	74.1
+8			27.0	59.1
+35			30.0	56.1

50

	+	$\pi$ 86.13	-	Elev.
<u>A 53+66</u>			1°47'30" RT	spit of L
EL-35			32.2	53.9
-20			7.1	79.0
-10			5.2	80.9
EL			6.2	79.9
$\phi$			6.2	79.9
WL			5.7	80.4
+30			2.2	83.9
+50			3.3	82.8
+70			3.7	82.4
+135			2.0	84.1
T.P.	554	90.01 ✓	1.66	84.47
<u>54+00 = End of Brickyard Flat</u>				
WL-140			3.5	86.5
-65			6.1	83.9
-40			6.2	83.8
WL			8.2	81.8
$\phi$			8.4	81.6
EL			7.8	82.2
+10			9.1	80.9
+12			18.2	71.8
+40			30.4	59.6
+75			35.7	54.3
<u>54+20</u>				
EL-50			23.3	66.7



	+	$\pi$ 90.01	-	Elev.
-35			24.9	65.1
-7			12.2	77.8
-5			6.0	84.0
FL			6.5	83.5
$\xi$			8.2	81.8

54+40

FL-50			13.0	77.0
-45			11.4	78.6
-25			0.8	89.2
-4	2.0			92.0
FL			6.0	84.0
$\xi$			7.7	82.3
WL			7.4	82.6
+35			4.0	86.0
+60			4.9	85.1
+75			1.6	88.4
+140	1.3			91.3

54+55

<u>55+00</u>				
WL-140	10.3			100.3
-45			2.2	87.8
-10			2.1	87.9
WL			6.5	83.5
$\xi$			6.0	84.0

	+	$\pi$ 90.01	-	Elev.
$\xi$ +15			6.1	83.9
+17	3.0			93.0
FL	3.0			93.0

$\xi$  Water tank on East diam. 12.0 Height 10'  
6' Back

$\xi$  Two story dwelling on East Frontage 24.0'  
8' Back



Equation  
 $55 + 59^{25} = 0 + 00$

<u>A 55+59<sup>25</sup></u>	+	$\pi$ 90.01	-	Elev.
EL-35			5.2	84.8
EL			1.2	88.8
+3			2.4	87.6
+4			4.9	85.1
±			5.8	84.2
+5			5.1	84.9
+12			1.2	88.8
WL			1.7	88.3
+33			0.4	89.6
+60	5.0			95
<u>0+41</u>				
WL-30	6.6			96.6
-1			1.1	88.9
WL			3.0	87.0
±			2.7	87.3
+15			4.0	86.0
+16			2.6	87.4
EL			2.6	87.4
+25			5.4	84.6
<u>0+65</u>	beginning of barbed wire fence on East			
<u>0+91</u>				
EL-30			12.1	77.9
-15			8.4	81.6
EL			7.0	83.0
+8	fence			

	+	$\pi$ 90.01	-	Elev.
+10			3.9	86.1
±			4.3	85.7
+15			5.2	84.8
WL			1.7	88.3
+5	0.8			90.8
+30	4.8			94.8
<u>+0.6</u>	beginning of fence on west			
<u>+41</u>				
WL-30	2.0			92.
-8	Fence			
WL			3.8	86.2
+5			6.9	83.1
±			6.0	84.
+12			6.1	83.9
+16	Fence			
EL			9.3	80.7
+20			10.6	79.4
+30			13.3	76.7
+40			16.2	73.8
+40			16.7	73.3
<u>+91</u>				
EL-40			19.4	70.6
-30			19.0	71.0
-20			13.6	76.4
EL			9.8	80.2
+2	Fence			



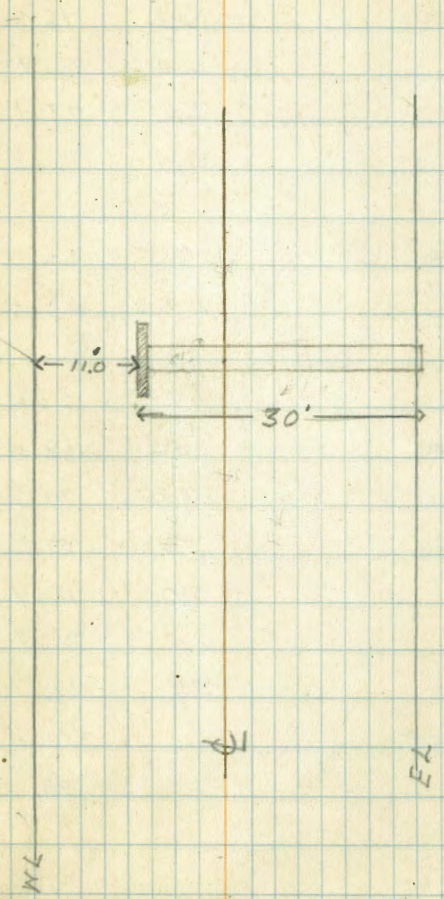
	+	$\pi$	-	Elev.
+8		90.01	6.7	83.3
♀			7.4	82.6
+14			8.1	81.9
WL			1.5	88.5
+9	Fence			
+30	9.5			94.5
<u>2+41</u>				
WL-30	6.0			96.
-8	Fence			
-1	2.0			92.
WL			0.0	90
+7			9.0	81
♀			8.8	81.2
+10			8.0	82.
EL	Fence		8.9	81.1
+40			18.8	71.2
<u>2+91</u>				
EL-40			17.8	72.2
-3	Fence			
EL			9.2	80.8
♀			9.9	80.1
+11			10.5	79.5
WL			3.6	86.4
+2			2.5	87.5
+7	Fence			

	+	$\pi$	-	Elev.
+30	5.3	90.01		95.3
<u>3+41</u>				
WL-30	8.2			98.2
-3	Fence			
WL			3.7	86.3
+11			11.9	78.1
♀			11.3	78.7
+10			10.7	79.3
+15			11.0	79.0
EL			14.2	75.8
+5	Fence			
+40			22.5	67.5
<u>3+91</u>				
T.P.	2.74	82.55 <sup>v</sup>	10.20	79.81 <sup>v</sup>
EL-40			21.6	61.0
-10	Fence		14.8	67.8
EL			8.4	74.2
+7			4.2	79.4
♀			5.0	77.6
+8			5.0	77.6
WL	Fence			83.8
+30	14.3			96.9
<u>4+50<sup>02</sup></u>	Δ			
WL-30	15.0			97.6
WL	2.2			84.8

SPLIT of L



	+	π	-	Elev.
+2	Fence	82.55		
+13			5.8	76.8
⊥			6.1	76.5
+16			5.5	77.0
EL			7.8	74.7
+12	Fence			
+15			18.6	64.0
+40			24.5	58.1
T.P.	5.16	82.71	5.00	77.55
Pole # 3587 on Rt.				
5+18 = ⊥ 18" iron culvert. mand set in concrete headwall				
Flow line pipe		8.80		73.91
Flow Line: F End		9.60		73.11
<u>5+00</u>				
EL-50		27.5		55.2
-15		21.2		61.5
EL-9	Fence			
EL		10.4		72.3
+5		6.0		76.7
⊥		6.3		76.4
+8		6.4		76.3
WL		0.4		92.3
+1	Fence			
+30	14.0			96.7
<u>6+00</u>				
WL-30	17.0			99.7





	+	$\pi$	-	Elev.
WL-5	Fence	82.71		
WL	0.3			83.0
+11			6.5	76.2
♀			6.0	76.7
+14			5.6	77.1
EL			10.4	72.3
+10	Fence			
+13			17.5	65.2
+40			24.3	68.4
<u>6+50</u>				
EL-40			19.1	63.6
-10	Fence		14.2	68.5
EL			8.0	74.7
+3			5.7	77.0
♀			6.0	76.7
+10			6.4	76.3
WL			3.9	78.8
+6	Fence			
+30	6.6			89.3
<u>7+50</u>				
WL-30	12.8			95.5
-5	Fence			
WL	1.8			84.5
+6	0.5			83.2
+11			5.8	76.9

	+	$\pi$	-	Elev.
♀		82.71	5.1	77.6
+19			4.8	77.9
EL			5.5	77.2
+9	Fence			
+11			11.7	71.0
+40			16.7	66.0
<u>8+50</u>				
EL-40			12.4	70.3
-5	Fence			
EL			6.3	76.4
+5			3.6	79.1
♀			3.9	78.8
+11			4.4	78.3
+16			0.0	82.7
WL	11			83.8
+30	6.8			89.5
<u>9+50</u>				
WL-30	18.3			101.0
-2.5	Fence		7.5	90.2
WL			0.0	82.7
+7			3.0	79.7
♀			2.4	80.3
+14			2.1	80.6
EL			6.6	76.1
+7	Fence			



	+	π	-	Elev.
EL+40		82.71	10.9	71.8
T.P.	10.02	91.88	0.85	81.86
<u>10+50</u>				
EL-40			13.5	78.4
-5 FENCE				
-EL			9.4	82.5
+7			8.1	92.8
£			9.1	92.8
+15			9.9	92.0
WL			3.2	89.7
+46 FENCE				
+50	5.3			97.2
<u>11+50</u>				
WL-62 FENCE	8.5			100.4
-9			0.5	91.2
WL			3.9	88.5
+3			7.7	84.2
£			6.3	85.6
EL			6.2	85.9
+2 FENCE				
+40			11.1	80.8
<u>12+18</u> $\Delta$ 33°59' Lt				Taken on split of L
EL-40			12.6	79.3
EL FENCE			6.8	85.1
£			4.3	87.6

	+	π	-
WL		91.88	5.5
+7			5.8
+13	2.2		94.0
+80 FENCE	14.0		105.9
T.P.	8.1	97.59	2.70
<u>13+00</u>			
WL-60	10.6		108.2
-46 FENCE			
WL			2.4
+5			3.1
+9			9.4
£			9.2
+15			8.0
EL			9.1
+14 FENCE			
+30			15.6
<u><math>\Delta</math> 13+62</u> 17°10' Rt			(SPLIT of L)
EL-40			17.4
-11 FENCE			12.5
-2			7.4
EL			7.4
£			8.4
+10			2.5
WL	0.8		98.4
+20 FENCE			

PJ 3594



	T	$\bar{\Pi}$	-	Elev.
WL+40	15.2	97.59		112.8
<u>14+00</u>				
WL-40	18.6			116.2
-12	Fence			
WL	3.1			100.7
+10		2.0		95.6
+15		7.3		90.3
♀		7.2		90.4
+17		6.7		90.9
EL		9.4		88.2
+4	Fence			
+10		15.1		82.5
+40		20.0		77.6
<u>15+00</u>				
EL-40		23.2		74.4
-13	Fence	13.8		83.9
EL		7.6		90.0
+5		4.5		93.1
♀		4.5		93.2
+7		4.6		93.0
+10	1.7			99.8
WL	7.0			104.6
+5	Fence			
+40	23.5			121.1
<u>15+75</u>				

	T	$\bar{\Pi}$	-	Elev
WL-40	21.2	97.59		118.8
WL	6.0			103.6
+1 Fence				
+14		3.0		94.6
♀		2.7		94.9
+16		2.8		94.8
EL		5.1		92.5
+5 Fence				
+10		9.8		87.8
+40		16.0		81.6
<u>16+27</u> A	27°20' RT		Split of L	
EL-40		11.1		86.5
-14 Fence		6.7		90.9
-5		1.7		95.9
EL		1.7		95.9
♀		2.1		95.5
+14 Fence	3.3			100.9
WL	5.8			103.4
+40	21.2			118.8
<u>17+00</u>				
WL-40	17.4			115.0
-22 Fence	10.4			108.0
WL	6.7			104.3
+5	6.2			103.8
+11		0.0		97.6



	+	$\pi$	-	Elev.
♀	0.7	97.59		98.3
EL	1.3			98.9
+13	Fence		2.6	96.0
+40			8.2	89.4
T.P.	10.80	107.59	0.80	96.79 <sup>Pole #4249</sup>
<u>17+84<sup>10</sup></u>	Right $\angle$ s to back tan			
EL			11.0	97.6
+15			6.3	101.3
♀			6.8	100.8
W.L.			7.9	99.7
<u>17+91<sup>12</sup></u>	$\Delta$ 41°35' Lt taken on split of L			
W.L.-65	10.0			127.6
-50	Fence			
-12			0.5	107.1
-6			7.4	100.2
W.L.			7.5	100.1
♀			6.6	101.0
+6			6.8	100.8
EL	Fence		11.3	96.3
+50			21.3	86.3
<u>17+99<sup>30</sup></u>	Right $\angle$ s to forward tan.			
EL			10.8	96.8
+12			6.4	101.2
♀			6.4	101.2
W.L.			7.5	100.1

	+	$\pi$	-	Elev.
<u>19+00</u>				
W.L.-50	18.7	107.59		126.3
-17	Fence			
W.L.	2.0			109.6
+12			0.2	107.4
+14			6.1	101.5
♀			5.9	101.7
+18			4.6	103.0
EL			6.1	101.5
+11			9.6	98.0
+13	Fence			
+65			20.4	87.2
<u>19+66<sup>20</sup></u>	$\Delta$ 28°25'30" Rt taken on split of L			
EL-80			20.9	86.7
-13	Fence			
-11			9.4	98.2
-3			4.6	103.0
EL			4.6	103.0
♀			4.7	102.9
+15	Fence			
W.L.	5.8			113.4
+25	19.0			126.6
<u>20+50</u>				
W.L.-25	19.5			127.1
-13	Fence			
W.L.	5.3			112.9



	+	$\pi$	-	Elev.
WL+5	3.8	107.59		111.4
+7			2.5	105.1
£			2.5	105.1
+10			2.7	104.9
EL			9.9	97.8
+4	Fence			
+65			23.0	84.6
<u>21+32.2</u>	A	9°12'41"	Taken on split of L	
EL-60			16.9	90.7
-7	Fence			
EL			6.1	100.5
+7			2.6	105.0
£			1.1	106.5
WL			2.0	105.5
+4			2.0	105.5
+14	12.7			120.3
+23	Fence			
+25	16.0			123.6
T.P.	8.38	109.56	6.1	101.18
				Pole 42.47
<u>22+00</u>				
WL-27	4.7			114.3
-16	1.0			110.6
-13			5.3	104.3
WL			5.0	104.6
+14			4.9	104.7

59

	+	$\pi$	-	Elev.
£		109.56	6.8	102.8
+10			10.9	99.7
EL			11.4	98.2
+1	Fence			
+46			18.4	91.2
+50			24.5	85.1
<u>22+15</u>				
EL-55			29.6	82.0
-50			22.0	87.6
-40			19.7	89.9
EL Fence			15.7	93.9
+12			15.0	94.6
£			9.5	100.1
+9			4.9	104.7
WL			5.1	104.5
+11			5.1	104.5
+22			7.0	102.6
+35	Fence			
+60			4.9	104.7
<u>22+45</u>	= £ 12" iron pipe culvert. Should be replaced by larger pipe.			
<u>22+60</u>				
WL-50			3.0	106.6
-40			6.1	103.5
-25			8.6	101.0



	+	$\pi$	-	Elev.
WL-19		109.56	4.8	104.8
WL			4.7	104.9
♀			19.2	89.4
EL Fence			28.4	81.2
EL+80			47.2	62.4
<u>23+00</u>				
EL-70			36.0	72.6
-6.0			29.8	79.8
E.L.			11.7	97.9
+1 Fence				
+12			6.1	103.5
♀			4.8	104.8
WL			4.3	105.3
+8			4.3	105.3
+18 4.5				114.1
+29 9.0 Fence				118.6
+40 13.0				122.6
T.P. 10.99 118.29			22.6	107.30 <sup>pole</sup> *4245
<u>24+16<sup>20</sup></u> $\Delta$ 18°09' RT taken on split of L				
WL-25 11.0				128.3
WL 1.8				120.1
WL+2 Fence				
+18			10.4	107.9
♀			9.6	108.7
+18			9.7	108.6

	+	$\pi$	-	Elev.
EL		118.29	11.0	107.3
+2 Fence				
+22			17.4	100.9
+40			30.3	88.0
<u>25+00</u>				
EL-35			27.0	91.3
-20			18.8	99.5
EL Fence			11.0	107.3
+6			7.5	110.8
♀			7.4	110.9
+10			8.1	110.2
+19 Fence				
W.L.			0.8	117.5
+25 8.0				126.3
<u>26+00</u>				
WL-25 5.4				123.7
-5 Fence				
W.L. 0.4				118.7
+6			0.2	118.1
+11			6.9	111.4
♀			6.3	112.0
+17			5.2	113.1
EL			6.4	111.9
+10 Fence				
+40			16.2	102.1



	*	π	-	Elev.
+50		118.29	22.3	96.0
<u>27+00</u>				
EL-50			22.0	96.3
-40			18.8	99.5
-15	FENCE			
-5			8.0	110.3
EL			6.0	112.3
+2			5.1	113.2
♀			5.4	112.9
+10			5.5	112.8
+17			0.0	118.3
WL	1.6			119.4
+13	Fence			
+25	5.6			123.9
<u>28+00</u>				
WL-25	0.8			119.1
-15	Fence			
WL			2.1	116.2
+7			5.3	113.0
♀			5.1	113.2
+14			4.7	113.6
EL			8.4	109.9
+3	Fence			
+40			15.0	103.3
<u>29+00</u>				

	*	π	-	
EL-40		118.29	16.7	101.6
EL			9.5	108.8
+4 Fence			8.2	110.1
+10			4.8	113.5
♀			4.8	113.5
+15			5.3	113.0
WL			2.4	115.9
+22	Fence			
+25	3.0			121.3
<u>30+00</u>				
WL-25	6.2			124.5
WL	Fence		0.5	119.5
+10	1.6		4.8	113.5
♀			4.4	113.9
+12			4.2	114.1
EL			8.0	110.3
+4 Fence				
+40			17.0	101.3
T.P.	6.78	119.61	5.46	112.83
<u>30+47<sup>20</sup></u>	Δ	7.027'	RT.	taken on split of L
EL-40			16.2	103.4
-9 Fence				
EL			7.8	111.8
+5			4.6	115.0
♀			5.5	114.1



	+	$\pi$	-	Elev.
±7		119.61	5.7	113.9
+10			0.8	118.8
+18	Fence			
WL	1.3			119.9
+25	6.4			126.0
<u>31+50</u>				
WL-25	2.8			122.4
-16			0.3	119.3
-14	Fence			
WL			5.3	114.3
±			4.6	115.0
+7			4.8	114.8
+16			9.9	109.7
EL			10.3	109.3
+10	Fence			
+40			16.0	103.6
<u>32+00</u>				
EL-40			14.8	104.8
-10	Fence		10.3	109.3
EL			8.1	111.5
+13			4.2	115.4
±			4.4	115.2
WL			5.1	114.5
+10			1.0	118.6
+18	Fence		0.0	119.6

	+	$\pi$	-	Elev.
WL+50	3.7	119.61		123.3
<u>32+20 = Private road.</u>				
<u>32+50</u>				
WL-25	4.2			123.8
-13	Fence			
-4	1.0			120.6
WL			5.1	114.5
±			4.4	115.2
+10			4.4	115.2
EL			7.9	111.7
+16	Fence			
+40			13.6	106.0
<u>33+50</u>				
EL-40			10.9	108.7



	+	$\pi$	-	Elev.
EL.		119.61	3.0	116.0
♀			4.2	115.4
+7			4.6	115.0
WL	1.4			121.0
+1	Fence			
+25	5.2			124.8
<u>34+35<sup>20</sup></u>	Right 1/2 to back tangent			
WL			1.6	118.0
♀			3.8	115.8
EL			4.0	115.6
<u>34+40<sup>20</sup></u>	$\Delta$	27°29'	RT	Split of $\angle$
EL-60			12.4	109.2
-40			10.9	108.7
-17			8.2	111.4
-7			4.2	115.4
EL			4.0	115.6
♀			3.8	115.8
+9	Fence			
WL			1.6	118.0
+25	3.4			123.0
<u>34+45<sup>20</sup></u>	Right 1/2 to forward tangent			
WL			1.6	118.0
♀			3.8	115.8
EL			4.0	115.6
TP	3.94	122.61	0.94	118.67

	+	$\pi$	-	
		122.61		
<u>35+50</u>	35+70: Start of fence on East			
EL-80			16.5	106.1
EL			8.9	113.7
♀			5.8	116.8
+16			5.3	117.3
WL			4.3	118.3
+10	Fence			
+25	3.0			125.6
<u>36+50</u>				
WL-35	3.0			125.6
-8	Fence			
WL			3.2	119.4
+5			5.5	117.1
♀			5.0	117.6
+11			5.0	117.6
+16	Fence		8.6	114.0
EL			9.3	113.3
+75			18.2	104.4
<u>37+50</u>				
EL-75			22.4	100.2
WL	Fence		10.6	112.0
+8			5.4	117.2
♀			5.1	117.5
+12			5.5	117.1
+18			0.0	122.6



	+	π	-	Elev.
WL		122.61		122.6
+5	Fence		0.0	
+25	8.6			131.2
<u>37+93<sup>20</sup></u> Δ 71°42'30" Rt (Split of L)				
WL-25	12.7			135.3
WL	3.4			126.0
+13			5.2	117.4
⊥			5.1	117.5
+13			5.6	117.0
EL			9.9	112.7
+4	Fence		12.2	110.4
+80			24.0	98.6
T.P.	39.4	123.89	2.66	119.95
<u>39+00</u>				
EL-75			33.2	90.7
-15			22.0	101.9
-3	Fence			
EL			12.3	111.6
+8			6.6	117.3
⊥			6.4	117.5
+8			6.3	117.6
WL.	2.8	Fence		126.7
25	15.0			138.9
<u>40+00</u>				
WL-25	16.4			140.3

Point by Δ 40+46

	+	π	-
-4	FENCE	123.89	
WL.	4.1		128.0
+7			1.8
			122.1
+8			5.5
			118.4
⊥			5.5
			118.4
+8			5.2
			118.7
EL			12.2
			111.7
+2	Fence		
+10			17.6
			106.3
+75			33.5
			90.4
<u>40+46<sup>20</sup></u> Split of L Δ 24°34' Lt			
EL-75			33.0
			90.9
EL.			15.6
			108.3
+7	FENCE		
⊥			5.3
			118.6
WL			5.7
			119.2
+20	12.0	Fence	
			135.9
+25	14.7		
			138.6
<u>41+00</u>			
WL-25	18.0		
			141.9
-10	FENCE		
-17	10.0		
			133.9
WL	1.2		
			125.1
+8			5.9
			118.0
⊥			5.7
			118.2



	+	π	-	Elev.
♀+11		123.89	5.7	118.2
EL Fence			10.7	113.2
+40			22.6	101.3
<u>42+14<sup>20</sup></u> Δ		16°31' Lt	Split of L	
EL-40			16.2	107.7
-3 Fence				
EL			10.0	113.9
+10			4.9	119.0
♀			5.0	118.9
+16			5.7	118.2
WL			3.5	120.4
+8 2.5				126.4
+15 Fence				
+25 9.3				133.2
+35 15.0				138.9
<u>43+00</u>				
WL-35 8.5				132.4
-25 5.0				128.9
WL			1.6	122.3
+7 Fence				
+13			6.5	117.4
♀			5.2	118.7
EL			5.4	118.5
+31 Fence				
+40			12.5	111.4

	+	π	-	Elev.
+75		123.89	15.0	108.9
<u>43+38<sup>42</sup></u>			RT Ls to back tangent	
EL			5.6	118.3
♀			5.4	118.5
+6			7.0	116.9
+15			6.9	117.5
WL			3.7	120.2
<u>43+48<sup>20</sup></u> Δ		54°12' Rt	split of L	
WL-35			2.0	121.9
WL			3.9	120.0
+11			11.3	112.6
♀			5.6	118.3
EL			5.6	118.3
+8			5.8	118.1
+20			16.5	107.4
+37 Fence				
+75			25.4	98.2
<u>43+58<sup>93</sup></u>			RT Ls to forward tangent	
EL			5.6	118.3
♀			5.3	118.6
+8			5.3	118.6
+10			14.1	109.8
WL			13.1	110.9
+35			9.6	114.3
T.P. 948		124.82	8.55	115.34

pole # 4235







	+	π	-	Elev.
WL+2		124.82	1.0	123.8
+5			5.5	119.3
♀			5.1	119.7
+11			4.9	119.9
EL			9.3	115.6
+20	FENCE			
+75			21.8	103.0
<u>47+00</u>				
EL-75			28.1	96.7
-25	FENCE		21.7	103.1
EL			12.5	112.3
+13			5.0	119.8
♀			5.0	119.8
+14			5.5	119.3
WL			2.3	122.5
+15	6.9	FENCE		131.7
+25	10.7			135.9
<u>48+00</u>				
WL-25	12.5			137.3
-13	8.2	FENCE		133.0
WL	2.5			127.3
+6			4.4	120.4
♀			4.2	120.6
+8			4.3	120.5
EL			13.1	111.7

	+	π	-	Elev.
-24	FENCE	124.82		
-50			31.0	93.8
-75			32.9	91.9
<u>49+00</u>				
-75			36.1	88.7
-50			33.8	91.0
-28	FENCE			
EL			13.4	111.4
+16			3.6	121.2
♀			3.6	121.2
+13			3.7	121.1
WL	3.1			127.9
+11	9.8	FENCE		134.6
+35	2.1			145.9
<u>50+00</u>				
WL-40	26.0			150.8
-8		FENCE		
WL	8.6			133.4
+5	4.0			128.8
+10			3.0	121.8
♀			3.0	121.8
+7			2.5	122.3
EL			11.8	113.0
+30	FENCE			
+60			31.3	93.5



	+	$\pi$	-	Elev.
+75		<del>124.82</del> <del>139.95</del>	32.0	93.8
<u>51+00</u>				
EL-75			28.0	96.8
-35 FENCE			23.2	101.6
EL			8.7	116.1
+12			1.0	123.8
♀			1.8	123.4
+7			1.5	123.3
+15	10.5			135.3
WL	12.2			137.0
+11		Fence		
+40	31.5			156.3
T.P.	5.44	129.49	0.77	124.05
<u>51+42.0</u>	Right 15 to back tangent			
WL			1.4	128.1
+4			5.3	124.2
♀			4.8	124.7
EL			15.8	113.7
<u>51+48.2</u>	$\Delta 36^{\circ} 55' 30''$ Lt Split of L			
EL-50			27.0	102.5
-35 FENCE				
-25			24.0	105.5
EL			16.5	108.0
♀			5.3	119.2
+2			4.9	124.6

	+	$\pi$	-	Elev.
+16		129.49		
WL			5.4	124.1
			1.4	128.1
+4	4.8			134.3
+34 FENCE				
+40	22.4			151.9
+50	26.0			155.5
<u>51+55.38</u>	Right 15 forward tangent			
WL			1.4	128.1
+4			5.4	124.1
♀			4.8	124.7
+2			4.8	124.7
EL			15.8	113.7
<u>52+23.48</u>	Rt 15 to back tan			
EL			14.0	115.5
+17			4.8	124.7
♀			4.8	124.7
+18			6.6	122.9
WL			4.1	125.4
<u>52+31.20</u>	$\Delta 44^{\circ} 41' 30''$ Lt Split of L			
WL-60	20.5			150.0
-53 FENCE				
-35	14.5			144.0
-5	2.4			131.9
WL			1.4	128.1
+2			6.6	122.9



	+	π	-	Elev.
		129.49		
+18			5.1	124.4
⊥			6.0	123.5
+13			13.4	116.1
EL			15.1	114.4
+16			17.8	111.7
+21	Fence		22.6	106.9
+27			19.8	109.7
+45			18.0	111.5
+50			19.4	110.1
+60			19.4	110.1
<u>52+39<sup>90</sup> Rt. 15 forward turn</u>				
EL			14.2	115.3
+7			12.0	117.5
+17			5.5	124.0
⊥			5.5	124.0
+18			6.6	122.9
WL			1.4	128.1
<u>52+67</u>				
WL-60	17.6			147.1
-40	13.3	Fence		142.8
-7	7.0			136.5
WL			3.1	126.4
+7			8.3	121.2
⊥			7.7	121.8
+10			7.6	121.9

	+	π	-	
		129.49		
EL			13.8	115.7
+5			15.0	114.5
+8			18.0	111.5
+17			20.2	109.2
+22			15.6	113.9
+24	Fence			
+35			18.6	110.9
+40			17.4	112.1
+50			16.0	113.5
+60			16.4	113.1
<u>53+00</u>				
EL-60			14.6	114.9
-50			14.1	115.4
-35			16.6	112.9
-25			15.1	114.4
-23	Fence			
EL			14.3	116.2
+10			8.8	120.7
⊥			8.9	120.6
WL			8.6	120.9
+36	Fence			
+40			7.0	122.5
A 36" culvert should be placed at 53+00				
<u>53+82<sup>20</sup> Rt 15 to back turn</u>				
T.P	10.15	130.62	9.02	120.47

A HUB  
53.825



	+	$\pi$ 130.62	-	Elev.
WL			9.0	121.6
+3	Fence			
±			10.20	120.4
EL			10.8	119.8
<u>53+89.20</u>	$\Delta$ 41°17' Rt			Split of L
EL-75			15.2	115.4
-50			15.8	114.8
-40			12.5	118.1
-30			15.3	115.3
-23	Fence		13.4	117.2
EL			10.8	119.8
±			10.2	120.4
+17	Fence			
WL			9.0	121.6
+50			4.6	126.0
<u>53+97.20</u>	Rt is Forward tan			
WL			9.0	121.6
+3	Fence			
±			10.20	120.4
EL			10.8	119.8
<u>54+50</u>				
EL-50			16.0	114.6
-2	FENCE			
EL			11.4	119.2
+3			9.6	121.0

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	+	$\pi$ 130.62	-	Elev.
±			9.6	121.0
+9			10.0	120.6
+10			4.9	125.7
WL, Fence			3.4	127.2
+25	10.5			141.1
<u>55+00</u>				
WL-30	16.3			146.9
WL	3.3			133.9
+1	Fence			
+8			0.4	130.2
+13			8.8	121.8
±			8.8	121.8
+11			8.1	122.5
+19	Fence			
EL			12.4	118.2
+50			17.6	113.0
<u>56+00</u>				
EL-50			15.0	115.6
EL			11.0	119.6
+5	FENCE		10.0	120.6
+12			6.5	124.1
±			6.7	123.8
+14			7.2	123.3
WL			2.3	128.2
+4	Fence		0.5	130.1



	+	$\pi$	-	Elev.
+25	8.0	130.62		138.6
<u>56+85<sup>20</sup></u>	$\Delta$	33° 0' 30" Lt	Split of L	
WL-50	6.1			136.7
-22	Fence			
-7			0.0	130.6
-5			4.6	126.0
W.L.			4.5	126.1
$\phi$			3.3	127.3
+11	Fence			
EL			5.9	124.7
+50			11.7	118.9
<u>57+86</u>				
EL-50			10.9	120.2
-4	Fence			
EL			5.1	120.5
+5			3.2	127.4
$\phi$			3.3	127.3
+10			3.5	127.1
WL			0.5	130.1
+2	Fence			
+40	7.4			138.0
<u>58+232<sup>20</sup></u>	$\Delta$	18° 32' 30" Rt	split of L	
WL-40	16.4			147.0
-20	8.0			138.6
WL	4.0			134.6

	+	$\pi$	-	Elev.
WL+7	Fence	145.75		130.62
+14			0.3	130.3
+15			2.6	128.0
$\phi$			2.6	128.0
+16			3.1	127.5
EL			5.4	125.2
+4	Fence			
+50			11.8	118.8
T.P. P.12		137.69	1.05	129.57
<u>59+00</u>				
EL-50			22.7	115.2
EL			14.0	123.7
+7	Fence			
+10			11.8	125.9
+15			8.4	129.3
$\phi$			8.4	129.3
+12			8.1	129.6
+16			4.2	133.5
W.L. Fence			2.6	135.1
+25	6.5			144.2
<u>60+00<sup>20</sup></u>	= intersection of $\phi$ & P.L. 1252			
SPLIT of L				
WL-25	4.4			142.1
-4	Fence		2.6	135.1
WL			6.6	131.1



137.69  
π

	+	-	Elev.
±		68	120.9
+15	Fence	11.1	126.6
EL		12.2	125.5
+50		22.0	115.7

Present H.I. continued in other book  
 (No 1226)



STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
"A" 0+00				220.00	+ 85			6.5	220.1 ✓
	6.59	226.59		✓	80			6.8	219.8 ✓
5'			6.2	220.3 ✓	75			6.6	220.0 ✓
10'			5.8	220.7 ✓	70			7.3	219.3 ✓
15'			5.4	221.2 ✓	65			8.0	218.6 ✓
20'			5.1	221.5 ✓	60			7.8	218.8 ✓
25'			5.0	221.6 ✓	55			7.8	218.8 ✓
30'			4.7	221.9 ✓	50			6.9	219.7 ✓
35'			4.4	222.2 ✓	48			Elev. 6.4 - 4.2 (222.1) ✓	
40'			4.1	222.5 ✓	45			4.2	222.4 ✓
45'			3.9	222.7 ✓	40			4.2	222.2 ✓
50'			3.6	223.0 ✓	39			4.2	5.8 (220.8) ✓
55'			3.7	222.9 ✓	35			5.9	220.7 ✓
60'			4.1	222.5 ✓	30			6.5	220.1 ✓
65'			4.2	222.4 ✓	25			7.1	219.5 ✓
70'			4.6	222.0 ✓	20			7.9	218.7 ✓
75'			4.4	222.2 ✓	15			8.3	218.3 ✓
80'			4.1	222.5 ✓	10			9.0	217.6 ✓
85'			3.7	222.9 ✓	5			9.2	217.4 ✓
90'			3.9	222.7 ✓	0			9.8	216.8 ✓
95'			4.3	222.3 ✓	C - 0			13.5	213.1 ✓
1+00			4.0	222.6 ✓	+ 5			13.2	213.4 ✓
"B" 1+00			7.2	219.2 ✓	10			13.2	213.4 ✓
95			7.0	219.6 ✓	15			12.7	213.9 ✓
90			7.0	219.6 ✓	20			11.8	214.8 ✓
					25			11.4	215.2 ✓
					30			10.8	215.8 ✓



STA	+	H.I.	-	Elev.	STA	+	H.I.	-	Elev.
35			10.8	215.8✓	55			5.8	213.0✓
40			10.0	216.6✓	50			5.5	213.3✓
45			10.1	216.5✓	45			5.4	213.4✓
50			11.0	215.6✓	40			6.2	212.6✓
55			11.2	215.4✓	35			6.3	212.5✓
60			11.6	215.0✓	30			6.3	212.5✓
65			11.7	214.9✓	25			6.6	212.2✓
70			11.5	215.1✓	20			8.0	210.8✓
75			11.8	214.8✓	15			8.1	210.7✓
80			12.2	214.4✓	10			8.1	210.7✓
85			12.6	214.0✓	5			8.9	209.9✓
90			12.2	214.4✓	0			8.6	210.2✓
95			11.0	215.6✓	E-0+00			12.1	206.7✓
100			9.0	217.6✓	+75			11.5	207.3✓
T.P.			9.56	217.03	10			11.3	207.5✓
	1.73	218.76			15			11.9	206.9✓
D-100			6.1	212.7✓	20			10.6	208.2✓
95			5.8	213.0✓	25			10.0	208.8✓
90			6.4	212.4✓	30			8.8	210.0✓
85			6.4	212.4✓	35			9.8	209.0✓
80			6.3	212.5✓	40			9.0	209.8✓
75			5.9	212.9✓	45			8.2	210.6✓
70			5.8	213.0✓	50			8.0	210.8✓
65			5.7	213.1✓	55			8.6	210.2✓
60			5.2	213.6✓	60			8.0	210.8✓



STA	+	H.I.	-	Elev.
65			9.0	209.8
70			8.5	210.3
75			9.5	209.3
80			9.3	209.5
85			10.2	208.6
90			9.7	209.1
95			8.5	210.3
1+00			6.2	212.6
F-1+00			8.5	210.3
95			8.9	209.9
90			9.1	209.7
85			10.1	208.7
80			10.4	208.4
75			10.7	208.1
70			11.1	207.7
65			10.5	208.3
60			9.8	209.0
55			9.7	209.1
50			9.8	209.0
45			10.6	208.2
40			11.0	207.8
35			12.0	206.8
30			12.2	206.6
25			12.3	206.5
20			12.4	206.4

STA	+	H.I.	-	Elev.
15			12.9	205.9
10			13.1	205.7
5			13.3	205.5
0			13.7	205.1
G-0+00			15.0	203.8
5			14.7	204.1
10			14.1	204.7
15			13.6	205.2
20			13.2	205.6
25			13.0	205.8
30			12.8	206.0
35			12.3	206.5
40			12.1	206.7
45			11.8	207.0
50			11.8	207.0
55			11.7	207.1
60			11.7	207.1
65			11.7	207.1
70			11.2	207.6
75			8.2	210.6
80			8.4	210.4
85			8.3	210.5
90			6.8	212.0
95			6.2	212.6
1+00			7.8	211.0



B.M.'s Rose Canyon  
Road

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Sta.	+	H.I.	-	Elev.		ELEV.
H-1400			4.20	212.6 ✓	No. 1	50' West of station 17+00
95			3.6	215.2 ✓		
90			4.3	214.5 ✓		
85			5.3	213.5 ✓	132.69	182.79
80			5.9	212.9 ✓	707	2.83
75			7.2	211.6 ✓	130.62 Pole 4225	185.62 π
70			7.8	211.0 ✓	1297	3.88 Nail in Guard
65			8.7	210.1 ✓	143.59 π	176.74 Post at brick yd.
60			9.3	209.5 ✓	252	5.11
55			10.4	208.4 ✓	171.07 Fence Post	181.85 π
50			10.1	208.7 ✓	656	10.19 Peg by road
45			10.3	208.5 ✓	147.63 π	171.66 Right.
40			10.5	208.3 ✓	103	2.99
35			11.3	207.5 ✓	146.60 Pole 4221	174.65 π
30			11.5	207.3 ✓	841	7.40
25			12.7	206.1 ✓	153.01 π	170.25 ON USGS B.M. 17059
20			13.0	205.8 ✓	259	17025
15			13.3	205.5 ✓	152.92 rock	0.27
10			13.5	205.3 ✓	686	continued in
5			13.8	205.1 ✓	159.28 π	other book
0			13.7	205.1 ✓	291	
					156.37 Fence post	
					319	
					159.56 π	
					724	
					152.32 Pole 4215	
					278	
					155.10 π	
					246	
					152.64 Pole 4213	
					846	
					161.10 π	
					562	
					155.48 Pole 4211	
					1288	
					168.36 π	
					4.88	
					163.48 Pole 4209	
					12.74	
					175.92 π	
					0.00 Guard Post by	
					175.92 Pole 4207	
					8.82	
					184.74 π	
					1.95	
					182.79 Pole 4205	







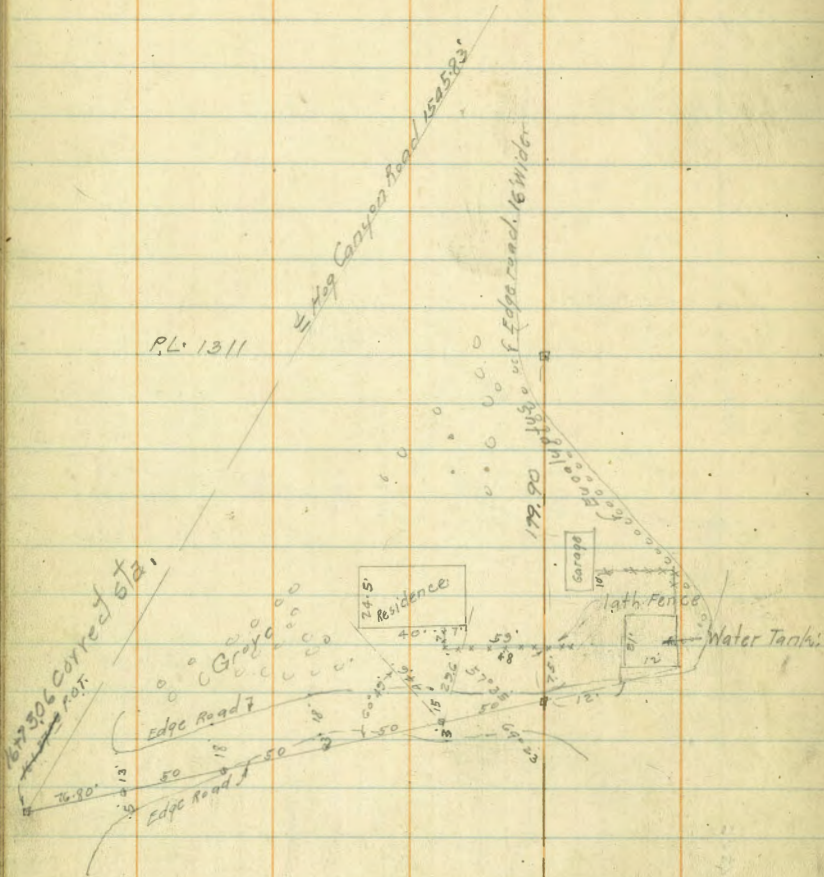




Nov 15th 1927

Dunnan  
Flood.  
Rauner.

Portion of McLaughlin Lease in P.L. 1311

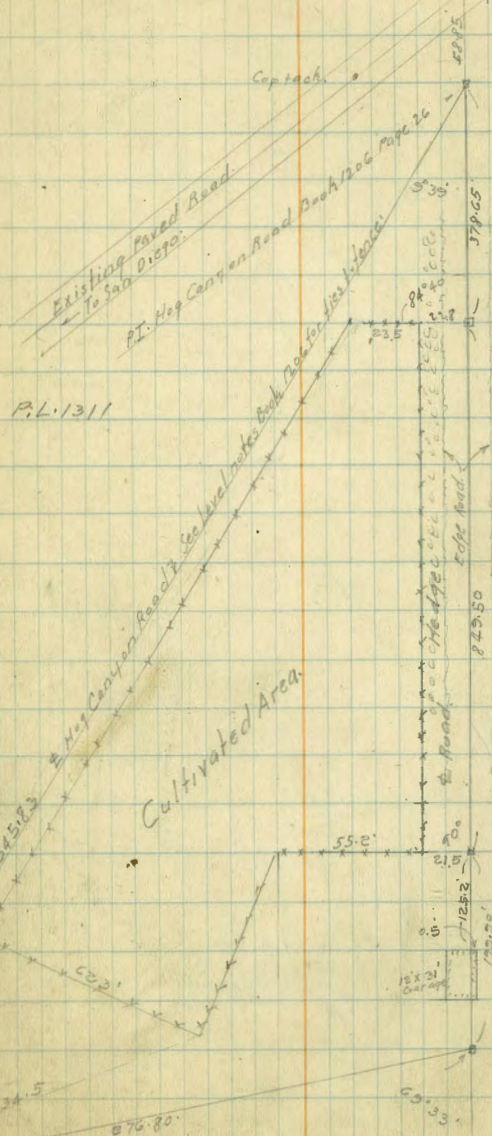


Sta 16773.06 Hog Canyon  
P.O.T. Sta 16773.06 Hog Canyon Road

Cap Tach

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Cap Tach Book 1206 Page 26



Cultivated Area







	410	1510	1100	Sta 7
			5.2	9.9
1+ East channel			2-	8.1
2+ ✓	✓		6.9	8.2
3+ ✓	✓		6.7	8.4
1+ West	✓		7.2	7.9
2+ ✓	✓		7.6	7.5
3+ ✓	✓		7.8	7.3

Channel 40 to 50' wide

+	-			
1.9	75.40		74.-	45+00
0.7		11.75	64.45	
	64.85 ✓			
- .05		11.72 ✓	53.13	
	53.08 ✓			
		12.13 ✓	40.95	
7.93	43.78 ✓			
		4.7	39.1	W.S.
		5.3	38.5	✓
		7.5	36.2	W. on Piles
		11.2	32.5	Chan. at Trest. S.F.

Top R1 = 43.8

Bridge on Baltra - Some channel -  
 140' long - 8' Depth - abt 12" from floor -  
 1120' opening -

## IMPROVED TABLES AND INFORMATION

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections. Degree of curve with a given  $L$  may be found by dividing tangent, (or external) opposite  $L$  by given tangent, (or external).  
 The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.







TABLE X.  
MIDDLE ORDINATES OF RAILS  
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.  
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.  
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.  
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000



$$\begin{array}{r} 210.2 \\ - 6.4 \\ \hline 203.8 \end{array}$$
$$\begin{array}{r} 210.2 \\ - 7.2 \\ \hline 203.0 \end{array}$$
$$\begin{array}{r} 203.0 \\ + 5.4 \\ \hline 208.4 \end{array}$$
$$\begin{array}{r} 210.2 \\ - 3.4 \\ \hline 206.8 \end{array}$$
$$\begin{array}{r} 206.8 \\ + 3.2 \\ \hline 210.0 \end{array}$$
$$\begin{array}{r} 210.2 \\ - 3.2 \\ \hline 207.0 \end{array}$$
$$\begin{array}{r} 210.2 \\ + 1.7 \\ \hline 211.9 \end{array}$$
$$\begin{array}{r} 211.9 \\ - 9.4 \\ \hline 202.5 \end{array}$$
$$\begin{array}{r} 202.5 \\ + 5.2 \\ \hline 207.7 \end{array}$$
$$\begin{array}{r} 91.33 \\ - 51.6 \\ \hline 39.73 \end{array}$$
$$\begin{array}{r} 47.02 \\ - 41.2 \\ \hline 5.82 \end{array}$$
$$\begin{array}{r} 600 \\ - 26000 \\ \hline \end{array}$$
$$\begin{array}{r} 5099 \\ - 5525925 \\ \hline \end{array}$$
$$\begin{array}{r} 9825 \\ - 854 \\ \hline 8971 \end{array}$$
$$\begin{array}{r} 11137 \\ - .80 \\ \hline 11136.20 \end{array}$$
$$\begin{array}{r} 110.57 \\ + 188.12 \\ \hline 298.69 \end{array}$$
$$\begin{array}{r} 188.12 \\ + 273 \\ \hline 461.12 \\ - 268.46 \\ \hline 192.66 \end{array}$$
$$\begin{array}{r} 110.57 \\ - 10.86 \\ \hline 99.71 \end{array}$$
$$\begin{array}{r} 74 \\ - 31 \\ \hline 43 \end{array}$$
$$\begin{array}{r} 5792 \\ - 220 \\ \hline 5572 \end{array}$$
$$\begin{array}{r} 37.30 \\ - 22.37 \\ \hline 14.93 \end{array}$$
$$\begin{array}{r} 291.65 \\ - 2018 \\ \hline 2309.40 \end{array}$$